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No. 9

American Practical Navigator

An Epitome of Navigation and Nautical Astronomy

By NATHANIEL BOWDITCH, LL. D., Etc.

HYDROGRAPHIC OFFICE

Washington : : : Government Printing Office : : : 1910

ORDERS RELATING TO REVISION.

Bureau of Navigation,
Navy Department, January 1, 1881.

In accordance with the purpose contemplated in the purchase of the copyright of the New American Practical Navigator, a thorough and complete revision has been made by Commander P. H. Cooper, U. S. Navy, acting under the direction of the Bureau. The revision consists principally in the substitution of the more concise and convenient methods of the present day for the obsolete methods of the past, and a complete rearrangement under proper chapters and paragraphs for ready reference, keeping in view, however, the character of the work as a Practical Navigator.

The revision having been completed, it was submitted to Capt. Ralph Chandler, U. S. Navy, for a final review, and having received a satisfactory report from that officer it has been accepted by the Bureau and will hereafter be substituted for the former editions of the work.

William D. Whiting,
Chief of Bureau.

Bureau of Equipment,
Navy Department, March 18, 1903.

A revision of Bowditch's American Practical Navigator having become necessary, the work has been completed by Lieut. G. W. Logan, U. S. Navy, under the supervision of the Hydrographer to the Bureau of Equipment. The revision was approved by a Board consisting of Capt. Colby M. Chester, U. S. Navy, Commander C. J. Badger, U. S. Navy, and Lieut. Commander C. C. Rogers, U. S. Navy. It is directed that this revised edition be substituted for all former editions.

R. B. Bradford,
Chief of Bureau.

PREFACE.

The copyright of the New American Practical Navigator, by the late Dr. Bowditch, became the property of the United States Government under the provision of an act of Congress to establish a Hydrographic Office in the Navy Department, approved June 21, 1866.

Under the direction of the Bureau of Navigation, at that time charged with such publications, the work was revised in 1880 by Commander P. H. Cooper, U. S. Navy, certain chapters being contributed by Lieuts. Richard Wainwright and Charles H. Judd, U. S. Navy, and the whole being reviewed by Capt. Ralph Chandler, U. S. Navy. The object of this revision was to improve the general arrangement, and to introduce the more convenient and precise methods of navigation that had come into practice since the book was originally written.

The progress that has been made in the science of navigation since 1880 has rendered necessary a second extensive revision, to take cognizance of the changes of methods and instruments that have accompanied the general introduction of high-speed vessels built of iron and steel. This work has been carried out, under the direction of the Bureau of Equipment, by Lieut. G. W. Logan, U. S. Navy, who was aided in the collection of data and preparation for publication by Lieut. T. A. Kearney, U. S. Navy; the chapters on Winds and Cyclonic Storms were contributed by Mr. James Page, nautical expert, Hydrographic Office.

There has been an extensive rewriting of the text, with the object of amplifying those matters that are of the greatest importance in the modern practice of navigation, and of omitting or condensing those of lesser importance; and the revision of the tables has proceeded along similar lines. This has involved, among other things, a much wider treatment of the subject of the compass; an extension of the traverse table for degrees to distances up to 600 miles; an improved table for reducing circum-meridian altitudes; the combination of the tables of maritime positions and tidal data; the omission of certain special methods for finding position by two observations; the addition of a series of annotated forms for the working of all sights, and the introduction of a number of new tables of use to the navigator.

The explanation of the method of lunar distances, with its accompanying tables, has been retained, in order to be available for use when required; but since this observation is so rarely employed in modern navigation, everything pertaining thereto has been incorporated in an appendix, that it may be distinct from matter of every-day use to the navigator.

For convenience in use the work has been divided into two parts, of which the first comprises the text and its appendices, and the second the tables.

W. H. H. Southerland,
Commander, U. S. Navy, Hydrographer.

Hydrographic Office,
Bureau of Equipment, Navy Department,
Washington, D. C., March 19, 1903.

NOTE.

This edition is a reprint of the revised edition, 1903, with no change made in the text or tables of that edition except the correction of such errors as have been discovered in it to the present date.

JOHN J. KNAPP,
Captain, U. S. Navy, Hydrographer.

HYDROGRAPHIC OFFICE,
BUREAU OF NAVIGATION, NAVY DEPARTMENT,
Washington, D. C., July 8, 1910.

PART I.

TEXT AND APPENDICES.

CONTENTS OF PART I.

ABBREVIATIONS USED IN THIS WORK.

Alt. (or *h*)	Altitude.
A. M	Ante meridian.
Amp	Amplitude.
App	Apparent.
App. t	Apparent time.
Ast	Astronomical.
Ast. t	Astronomical time.
Aug	Augmentation.
Az. (or Z)	Azimuth.
C	Course.
C. C	Chronometer correction.
C—W	Chronometer *minus* watch.
Chro. t	Chronometer time.
Co. L	Co. latitude.
Col	Column.
Corr	Correction.
Cos	Cosine.
Cosec	Cosecant.
Cot	Cotangent.
d (or Dec.)	Declination.
D (or DLo)	Difference longitude.
Dep	Departure.
Dev	Deviation.
Diff	Difference.
Dist	Distance.
DL	Difference latitude.
D. R	Dead reckoning.
E., Ely	East, easterly.
Elap. t	Elapsed time.
Eq. eq. alt	Equation equal altitude.
Eq. t	Equation of time.
G. (or Gr.)	Greenwich.
G. A. T	Greenwich apparent time.
G. M. T	Greenwich mean time.
G. S. T	Greenwich sidereal time.
h	Altitude.
H	Meridian altitude.
H. A. (or *t*)	Hour angle.
H. D	Hourly difference.
H. P. (or Hor. par.)	Horizontal parallax.
Hr-s	Hour-s.
H. W	High water.
I. C	Index correction.
L. (or Lat.)	Latitude.
L. A. T	Local apparent time.
L. M. T	Local mean time.
L. S. T	Local sidereal time.
Lo. (or Long)	Longitude.
Log	Logarithm.
Lun. Int	Lunitidal interval.
L. W	Low water.
m	Meridional difference.
Merid	Meridian or noon.
Mag	Magnetic.
M. D	Minute's difference.
Mid	Middle.
Mid. L	Middle latitude.
M. T	Mean time.
N., Nly	North, northerly.
N. A. (or Naut. Alm.)	Nautical Almanac.
Np	Neap.
Obs	Observation.
p (or P. D.)	Polar distance.
p. c	Per compass.
P. D. (or *p*)	Polar distance.
P. L. (or Prop. Log.)	Proportional logarithm.
P. M	Post meridian.
p. & r	Parallax and refraction.
Par	Parallax.
R. A	Right ascension.
R. A. M. S	Right ascension mean sun.
Red	Reduction.
Ref	Refraction.
S., Sly	South, southerly.
S. D	Semi-diameter.
Sec	Secant.
Sid	Sidereal.
Sin	Sine.
Spg	Spring.
t	Hour angle.
T	Time.
Tab	Table.
Tan	Tangent.
Tr. (or Trans.)	Transit.
Var	Variation.
Vert	Vertex or vertical.
W., Wly	West, westerly.
W. T	Watch time
z	Zenith distance.
Z	Azimuth.

SYMBOLS.

☉	The Sun.
☾	The Moon.
✱	A Star or Planet.
$\overline{☉☾}$	Alt. upper limb.
$\underline{☉☾}$	Alt. lower limb.
⌽☉	Azimuthal angle.
°	Degrees.
′	Minutes of Arc.
″	Seconds of Arc.
^{h}	Hours.
^{m}	Minutes of Time.
^{s}	Seconds of Time.

GREEK LETTERS.

$A\ \alpha$	Alpha.
$B\ \beta$	Beta.
$\Gamma\ \gamma$	Gamma.
$\Delta\ \delta$	Delta.
$E\ \varepsilon$	Epsilon.
$Z\ \zeta$	Zeta.
$H\ \eta$	Eta.
$\Theta\ \theta$	Theta.
$I\ \iota$	Iota.
$K\ \kappa$	Kappa.
$\Lambda\ \lambda$	Lambda.
$M\ \mu$	Mu.
$N\ \nu$	Nu.
$\Xi\ \xi$	Xi.
$O\ o$	Omicron.
$\Pi\ \pi$	Pi.
$P\ \rho$	Rho.
$\Sigma\ \sigma$ (ς)	Sigma.
$T\ \tau$	Tau.
$\Upsilon\ \upsilon$	Upsilon.
$\Phi\ \phi$	Phi.
$X\ \chi$	Chi.
$\Psi\ \psi$	Psi.
$\Omega\ \omega$	Omega.

CHAPTER I.

DEFINITIONS RELATING TO NAVIGATION.

1. That science, generally termed *Navigation*, which affords the knowledge necessary to conduct a ship from point to point upon the earth, enabling the mariner to determine, with a sufficient degree of accuracy, the position of his vessel at any time, is properly divided into two branches: *Navigation* and *Nautical Astronomy*.

2. *Navigation*, in its limited sense, is that branch which treats of the determination of the position of the ship by reference to the earth, or to objects thereon. It comprises (*a*) *Piloting*, in which the position is ascertained from visible objects upon the earth, or from soundings of the depth of the sea, and (*b*) *Dead Reckoning*, in which the position at any moment is deduced from the direction and amount of a vessel's progress from a known point of departure.

3. *Nautical Astronomy* is that branch of the science which treats of the determination of the vessel's place by the aid of celestial objects—the sun, moon, planets, or stars.

4. Navigation and Nautical Astronomy have been respectively termed *Geo-Navigation* and *Celo-Navigation*, to indicate the processes upon which they depend.

5. As the method of piloting can not be employed excepting near land or in moderate depths of water, the navigator at sea must fix his position either *by dead reckoning* or *by observation* (*of celestial objects*); the latter method is more exact, but as it is not always available, the former must often be depended upon.

6. The Earth.—The Earth is an oblate spheroid, being a nearly spherical body slightly flattened at the poles; its longer or equatorial axis measures about 7,927 statute miles, and its shorter axis, around which it rotates, about 7,900 statute miles.

The Earth (assumed for purposes of illustration to be a sphere) is represented in figure 1.

The *Axis of Rotation*, usually spoken of simply as the *Axis*, is PP′.

The *Poles* are the points, P and P′, in which the axis intersects the surface, and are designated, respectively, as the *North Pole* and the *South Pole*.

The *Equator* is the great circle EQMW, formed by the intersection with the earth's surface of a plane perpendicular to the axis; the equator is equidistant from the poles, every point upon it being 90° from each pole.

Meridians are the great circles PQP′, PMP′, PM′P′, formed by the intersection with the earth's surface of planes secondary to the equator (that is, passing through its poles and therefore perpendicular to its plane).

Parallels of Latitude are small circles NT*n*, N′*n*′T′, formed by the intersection with the earth's surface of planes passed parallel to the equator.

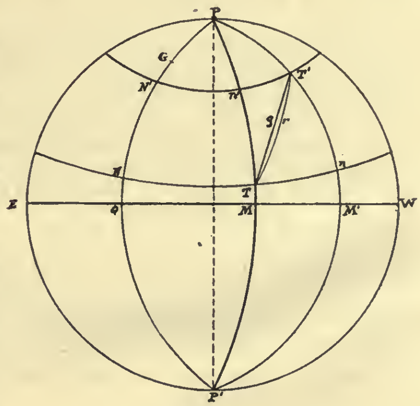

Fig. 1.

The *Latitude* of a place on the surface of the earth is the arc of the meridian intercepted between the equator and that place. Latitude is reckoned *North* and *South*, from the equator as an origin, through 90° to the poles; thus, the latitude of the point T is MT, north, and of the point T′, M′T′, north. The *Difference of Latitude* between any two places is the arc of a meridian intercepted between their parallels of latitude, and is called *North* or *South*, according to direction; thus, the difference of latitude between T and T′ is T*n*′ or T′*n*, north from T or south from T′.

The *Longitude* of a place on the surface of the earth is the arc of the equator intercepted between its meridian and that of some place from which the longitude is reckoned. Longitude is measured *East* or *West* through 180° from the meridian of a designated place, such meridian being termed the *Prime Meridian;* the prime meridian used by most nations, including the United States, is that of Greenwich, England. If, in the figure, the prime meridian be PGQP′, then the longitude of the point T is QM, east, and of T′, QM′, east. The *Difference of Longitude* between any two places is the arc of the equator intercepted between their meridians, and is called *East* or *West*, according to direction; thus, the difference of longitude between T and T′ is MM′, east from M or west from M′. The *Departure* is the linear distance, measured on a parallel of latitude, between two meridians; unlike the various quantities previously defined, departure is reckoned in miles; the departure between two meridians varies with the parallel of latitude upon which it is measured; thus, the departure between the meridians of T and T′ is the number of miles corresponding to the distance T*n* in the latitude of T, or to *n*′T′ in the latitude of T′.

The curved line which joins any two places on the earth's surface, cutting all the meridians at the same angle, is called the *Rhumb Line, Loxodromic Curve,* or *Equiangular Spiral.* In the figure, this line is represented by T*r*T′. The constant angle which this line makes with the meridians is called the *Course;* and the length of the line between any two places is called the *Distance* between those places.

The unit of linear measure employed by navigators is the *Nautical* or *Sea Mile,* or *Knot.* It is equal to one minute of latitude—that is, to the length of that portion of a meridian which subtends at the earth's center the angular measure of one minute; since, however, on account of the fact that the earth is not a perfect sphere, this distance is not exactly the same in all latitudes, a mean value is adopted for the length of the knot, and it is regarded as equal to 6,080.27 feet. For the purposes of navigation, the variation from this value in different latitudes is so small that it may be neglected, and the knot may be assumed equal to a minute of latitude in all parts of the earth; hence, when a vessel changes her position to the north or south by one nautical mile, it may always be considered that the latitude has changed 1′. Owing to the fact that the meridians all converge toward the poles, the difference of longitude produced by a change of position of one mile to the east or west will vary with the latitude; thus a departure of one mile will equal a difference of longitude of 1′.0 at the equator, of 1′.1 in the latitude of 30°, and of 2′.0 in the latitude of 60°.

The *Great Circle Track* or *Course* between any two places is the route between those places along the circumference of the great circle which joins them. In the figure, this line is represented by T*g*T′. From the properties of a great circle (which is a circle upon the earth's surface formed by the intersection of a plane passed through its center) the distance between two points measured on a great circle track is shorter than the distance upon any other line which joins them. Except when the two points are on the same meridian or when both lie upon the equator, the great circle track will always differ from the rhumb line, and the great circle track will intersect each intervening meridian at a different angle.

CHAPTER II.

INSTRUMENTS AND ACCESSORIES IN NAVIGATION.

DIVIDERS OR COMPASSES.

7. This instrument consists of two legs movable about a joint, so that the points at the extremities of the legs may be set at any required distance from each other. It is used to take and transfer distances and to describe arcs and circles. When used for the former purpose it is termed *dividers*, and the extremities of both legs are metal points; when used for describing arcs or circles, it is called a *compass*, and one of the metal points is replaced by a pencil or pen.

PARALLEL RULERS.

8. *Parallel rulers* are used for drawing lines parallel to each other in any direction, and are particularly useful in transferring the rhumb-line on the chart to the nearest compass-rose to ascertain the course, or to lay off bearings and courses.

PROTRACTOR.

9. This is an instrument used for the measurement of angles upon paper; there is a wide variation in the material, size, and shape in which it may be made. (For a description of the *Three Armed Protractor*, see art. 432, Chap. XVII.)

THE CHIP LOG.

10. This instrument, for measuring the rate of sailing, consists of three parts; viz, the *log-chip*, the *log-line*, and the *log-glass*. A light substance thrown from the ship ceases to partake of the motion of the vessel as soon as it strikes the water, and will be left behind on the surface; after a certain interval, if the distance of the ship from this stationary object be measured, the approximate rate of sailing will be given. The *log-chip* is the float, the *log-line* is the measure of the distance, and the *log-glass* defines the interval of time.

The *log-chip* is a thin wooden quadrant of about 5 inches radius, loaded with lead on the circular edge sufficiently to make it swim upright in the water. There is a hole in each corner of the log-chip, and the log-line is knotted in the one at the apex; at about 8 inches from the end there is seized a wooden socket; a piece of line of proper length, being knotted in the other holes, has seized into its bight a wooden peg to fit snugly into the socket before the log-chip is thrown; as soon as the line is checked this peg pulls out, thus allowing the log-chip to be hauled in with the least resistance.

The *log-line* is about 150 fathoms in length, one end made fast to the log-chip, the other to a reel upon which it is wound. At a distance of from 15 to 20 fathoms from the log-chip a permanent mark of red bunting about 6 inches long is placed to allow sufficient *stray line* for the log-chip to clear the vessel's eddy or wake. The rest of the line is divided into lengths of 47 feet 3 inches called *knots*, by pieces of fish-line thrust through the strands, with one, two, three, etc., knots, according to the number from stray-line mark; each knot is further subdivided into five equal lengths of two-tenths of a knot each, marked by pieces of white rag.

The length of a knot depends upon the number of seconds which the log-glass measures; the length of each knot must bear the same ratio to the nautical mile ($\frac{1}{60}$ of a degree of a great circle of the earth or 6,080 feet) that the time of the glass does to an hour.

In the United States Navy all log-lines are marked for log glasses of 28 seconds, for which the proportion is:

$$3600 : 6080 = 28^s : x,$$

x being the length of the knot.

Hence,

$$x = 47^{ft}.29, \text{ or } 47^{ft}\ 3^{in}.$$

The speed of the ship is estimated in knots and tenths of a knot.

The *log-glass* is a sand glass of the same shape and construction as the old hour-glass. Two glasses are used, one of 28 seconds and one of 14 seconds; the latter is employed when the ship is going at a high rate of speed, the number of knots indicated on a line marked for a 28-second glass being doubled to obtain the true rate of speed.

11. The log in all its parts should be frequently examined and adjusted; the peg must be found to fit sufficiently tight to keep the log-chip upright; the log-line shrinks and stretches and should often be verified; the log-glass should be compared with a watch. One end of the glass is stopped with a cork, by removing which the sand may be dried or its quantity corrected.

12. A *ground log* consists of an ordinary log-line, with a lead attached instead of a chip; in shoal water, where there are no well-defined objects available for fixing the position of the vessel and the course and speed are influenced by a tidal or other current, this log is sometimes used, its advantage being that the lead marks a stationary point to which motion may be referred, whereas the chip would drift with the stream. The speed, which is marked in the usual manner, is the speed over the ground, and the trend of the line gives the course actually made good by the vessel.

THE PATENT LOG.

13. This is a mechanical contrivance for registering the distance actually run by a vessel through the water. There are various types of patent logs, but for the most part they act upon the same principle, consisting of a registering device, a fly or rotator, and a log or tow line; the rotator is a small spindle with a number of wings extending radially in such manner as to form a spiral, and, when drawn through the water in the direction of its axis, rotates about that axis after the manner of a screw propeller; the rotator is towed from the vessel by means of a log or tow line from 20 to 50 fathoms in length, made fast at its apex, the line being of special make so that the turns of the rotator are transmitted through it to the worm shaft of the register, to which the inboard end of the line is attached; the registering device is so constructed as to show upon a dial face the distance run, according to the number of turns of its worm shaft due to the motion of the rotator; the register is carried at some convenient point on the vessel's quarter; it is frequently found expedient to rig it out upon a small boom, so that the rotator will be towed clear of the wake.

14. Though not a perfect instrument, the patent log affords the most accurate means available for determining the vessel's speed through the water. It will usually be found that the indications of the log are in error by a constant percentage, and the amount of this error should be determined by careful experiment and applied to all readings.

Various causes may operate to produce inaccuracy of working in the patent log, such as the bending of the wings of the rotator by accidental blows, fouling of the rotator by sea weed or refuse from the ship, or mechanical wear of parts of the register. The length of the tow-line has much to do with the working of the log, and by varying the length the indications of the instrument may sometimes be adjusted when the percentage of error is small; it is particularly important that the line shall not be too short. The readings of the patent log can not be depended upon for accuracy at low speeds, when the rotator does not tow horizontally, nor in a head or a following sea, when the effect depends upon the wave motion as well as upon the speed of the vessel.

15. Electrical registers for patent logs are in use, the distance recorded by the mechanical register being communicated electrically to some point of the vessel which is most convenient for the purposes of those charged with the navigation.

16. A number of instruments based upon different physical principles have been devised for recording the speed of a vessel through the water and have been used with varying degrees of success.

17. The revolutions of the screw propeller afford in a steamer a valuable check upon the patent log and a means of replacing it if necessary. To be of service the number of revolutions per knot must be carefully determined for the vessel by experiment under varying conditions of speed, draft, and foulness of bottom.

THE LEAD.

18. This device, for ascertaining the depth of water, consists essentially of a suitably marked line, having a lead attached to one of its ends. It is an invaluable aid to the navigator in shallow water, particularly in thick or foggy weather, and is often of service when the vessel is out of sight of land.

Two leads are used for soundings—the *hand-lead*, weighing from 7 to 14 pounds, with a line marked to about 25 fathoms, and the *deep-sea lead*, weighing from 30 to 100 pounds, the line being 100 fathoms or upward in length.

Lines are generally marked as follows:

2 fathoms from the lead, with 2 strips of leather.
3 fathoms from the lead, with 3 strips of leather.
5 fathoms from the lead, with a white rag.
7 fathoms from the lead, with a red rag.
10 fathoms from the lead, with leather having a hole in it.
13 fathoms from the lead, same as at 3 fathoms.
15 fathoms from the lead, same as at 5 fathoms.
17 fathoms from the lead, same as at 7 fathoms.
20 fathoms from the lead, with 2 knots.
25 fathoms from the lead, with 1 knot.
30 fathoms from the lead, with 3 knots.
35 fathoms from the lead, with 1 knot.
40 fathoms from the lead, with 4 knots.
And so on.

Fathoms which correspond with the depths marked are called *marks;* the intermediate fathoms are called *deeps;* the only fractions of a fathom used are a half and a quarter.

A practice sometimes followed is to mark the hand-lead line in feet around the critical depths of the vessel by which it is to be used.

Lead lines should be measured frequently while wet and the correctness of the marking verified. The distance from the leadsman's hand to the water's edge should be ascertained in order that proper allowance may be made therefor in taking soundings at night.

19. The deep-sea lead may be *armed* by filling with tallow a hole hollowed out in its lower end, by which means a sample of the bottom is brought up.

THE SOUNDING MACHINE.

20. This machine possesses advantages over the deep-sea lead, for which it is a substitute, in that soundings may be obtained at great depths and with rapidity and accuracy without stopping the ship. It consists essentially of a stand holding a reel upon which is wound the sounding wire, and which is controlled by a suitable brake. Crank handles are provided for reeling in the wire after the sounding has been taken. Attached to the outer end of the wire is the lead, which has a cavity at its lower end for the reception of the tallow for arming. Above the lead is a cylindrical case containing the depth-registering mechanism; various devices are in use for this purpose, all depending, however, upon the increasing pressure of the water with increasing depths.

21. In the *Lord Kelvin machine* a slender glass tube is used, sealed at one end and open at the other, and coated inside with a chemical substance which changes color upon contact with sea water; this tube is placed, closed end up, in the metal cylinder; as it sinks the water rises in the tube, the contained air being compressed with a force dependent upon the depth. The limit of discoloration is marked by a clearly defined line, and the depth of the sounding corresponding to this line is read off from a scale. Tubes that have been used in comparatively shallow water may be used again where the water is known to be deeper.

22. A tube whose inner surface is *ground* has been substituted for the chemical-coated tube, ground glass, when wet, showing clear. The advantage of these tubes is that they may be used an indefinite number of times if thoroughly dried. To facilitate drying, a rubber cap is fitted to the upper end, which, when removed, admits of a circulation of the air through the tube.

23. As a substitute for the glass tubes a mechanical *depth recorder* contained in a suitable case has been used. In this device the pressure of the water acts upon a piston against the tension of a spring. A scale with an index pointer records the depth reached. The index pointer must be set at zero before each sounding.

24. Since the action of the sounding machine, when glass tubes are used, depends upon the compression of the air, the barometric pressure of the atmosphere must be taken into account when accurate results are required. The correction consists in *increasing* the indicated depth by a fractional amount according to the following table:

Bar. reading.	Increase.
"	
29. 75	One-fortieth.
30. 00	One-thirtieth.
30. 50	One-twentieth.
30. 75	One-fifteenth.

THE MARINER'S COMPASS.

25. The *Mariner's Compass* is an instrument consisting either of a single magnet, or, more usually, of a series of magnets, which, being attached to a graduated circle pivoted at the center and allowed to

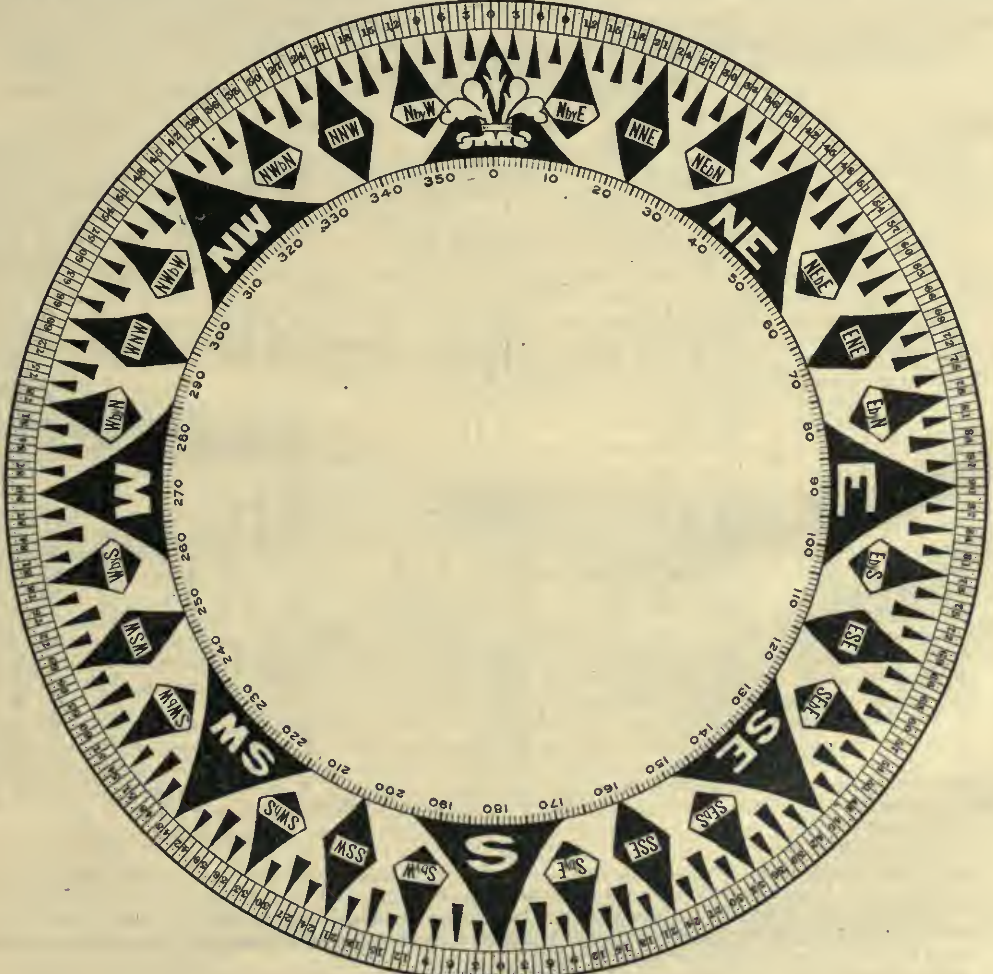

FIG. 2.

swing freely in a horizontal plane, has a tendency to lie with its magnetic axis in the plane of the earth's magnetic meridian, thus affording a means of determining the azimuth, or horizontal angular distance from that meridian, of the ship's course and of all visible objects, terrestrial or celestial.

26. The circular card of the compass (fig. 2) is divided on its periphery into 360°, numbered from 0° at North and South to 90° at East and West; also into thirty-two divisions of $11\frac{1}{4}$° each, called *points*, the latter being further divided into *half-points* and *quarter-points;* still finer subdivisions, *eighth-points*, are sometimes used, though not indicated on the card. A system of numbering the degrees from 0° to 360°, always increasing toward the right, is shown in the figure. This system is in use by the mariners of some nations, and its general adoption would carry with it certain undoubted advantages.

27. *Boxing the Compass* is the process of naming the points in their order, and is one of the first things to be learned by the young mariner. The four principal points are called *cardinal points* and are named North, South, East, and West; each differs in direction from the adjacent one by 90°, or 8 points. Midway between the cardinal points, at an angular distance of 45°, or 4 points, are the *inter-cardinal* points, named according to their position Northeast, Southeast, etc. Midway between each cardinal and inter-cardinal point, at an angular distance of $22\frac{1}{2}$°, or 2 points, is a point whose name is made up of a combination of that of the cardinal with that of the inter-cardinal point: North-Northeast, East-Northeast, East-Southeast, etc. At an angular distance of 1 point, or $11\frac{1}{4}$°, from each cardinal and inter-cardinal point (and therefore midway between it and the $22\frac{1}{2}$°-division last described), is a point which bears the name of that cardinal or inter-cardinal point joined by the word *by* to that of the cardinal point in the direction of which it lies: North by East, Northeast by North, Northeast by East, etc.

In boxing by fractional points, it is evident that each division may be referred to either of the whole points to which it is adjacent; for instance, NE. by N. $\frac{1}{2}$ N. and NNE. $\frac{1}{2}$ E. would describe the same division. It is the custom in the United States Navy to box *from* North and South *toward* East and West, excepting that divisions adjacent to a cardinal or inter-cardinal point are always referred to that point; as N. $\frac{1}{2}$ E., N. by E. $\frac{1}{2}$ E., NNE. $\frac{1}{2}$ E., NE. $\frac{1}{2}$ N., etc. Some mariners, however, make it a practice to box *from* each cardinal and inter-cardinal point *toward* a $22\frac{1}{2}$°-point (NNE., ENE., etc.); as N. $\frac{1}{2}$ E., N. by E. $\frac{1}{2}$ E., NE. by N. $\frac{1}{2}$ N., NE. $\frac{1}{2}$ N., etc.

The names of the whole points, together with fractional points (according to the nomenclature of the United States Navy), are given in the following table, which shows also the degrees, minutes, and seconds from North or South to which each division corresponds:

N. to E.	N. to W.	S. to E.	S. to W.	Pts.	Angular measure.
North:	North:	South:	South:		° ′ ″
N. $\frac{1}{4}$ E	N. $\frac{1}{4}$ W	S. $\frac{1}{4}$ E	S. $\frac{1}{4}$ W	$\frac{1}{4}$	2 48 45
N. $\frac{1}{2}$ E	N. $\frac{1}{2}$ W	S. $\frac{1}{2}$ E	S. $\frac{1}{2}$ W	$\frac{1}{2}$	5 37 30
N. $\frac{3}{4}$ E	N. $\frac{3}{4}$ W	S. $\frac{3}{4}$ E	S. $\frac{3}{4}$ W	$\frac{3}{4}$	8 26 15
N. by E	N. by W	S. by E	S. by W	1	11 15 00
N. by E. $\frac{1}{4}$ E	N. by W. $\frac{1}{4}$ W	S. by E. $\frac{1}{4}$ E	S. by W. $\frac{1}{4}$ W	$1\frac{1}{4}$	14 03 45
N. by E. $\frac{1}{2}$ E	N. by W. $\frac{1}{2}$ W	S. by E. $\frac{1}{2}$ E	S. by W. $\frac{1}{2}$ W	$1\frac{1}{2}$	16 52 30
N. by E. $\frac{3}{4}$ E	N. by W. $\frac{3}{4}$ W	S. by E. $\frac{3}{4}$ E	S. by W. $\frac{3}{4}$ W	$1\frac{3}{4}$	19 41 15
NNE	NNW	SSE	SSW	2	22 30 00
NNE. $\frac{1}{4}$ E	NNW. $\frac{1}{4}$ W	SSE. $\frac{1}{4}$ E	SSW. $\frac{1}{4}$ W	$2\frac{1}{4}$	25 18 45
NNE. $\frac{1}{2}$ E	NNW. $\frac{1}{2}$ W	SSE. $\frac{1}{2}$ E	SSW. $\frac{1}{2}$ W	$2\frac{1}{2}$	28 07 30
NNE. $\frac{3}{4}$ E	NNW. $\frac{3}{4}$ W	SSE. $\frac{3}{4}$ E	SSW. $\frac{3}{4}$ W	$2\frac{3}{4}$	30 56 15
NE. by N	NW. by N	SE. by S	SW. by S	3	33 45 00
NE. $\frac{3}{4}$ N	NW. $\frac{3}{4}$ N	SE. $\frac{3}{4}$ S	SW. $\frac{3}{4}$ S	$3\frac{1}{4}$	36 33 45
NE. $\frac{1}{2}$ N	NW. $\frac{1}{2}$ N	SE. $\frac{1}{2}$ S	SW. $\frac{1}{2}$ S	$3\frac{1}{2}$	39 22 30
NE. $\frac{1}{4}$ N	NW. $\frac{1}{4}$ N	SE. $\frac{1}{4}$ S	SW. $\frac{1}{4}$ S	$3\frac{3}{4}$	42 11 15
NE	NW	SE	SW	4	45 00 00
NE. $\frac{1}{4}$ E	NW. $\frac{1}{4}$ W	SE. $\frac{1}{4}$ E	SW. $\frac{1}{4}$ W	$4\frac{1}{4}$	47 48 45
NE. $\frac{1}{2}$ E	NW. $\frac{1}{2}$ W	SE. $\frac{1}{2}$ E	SW. $\frac{1}{2}$ W	$4\frac{1}{2}$	50 37 30
NE. $\frac{3}{4}$ E	NW. $\frac{3}{4}$ W	SE. $\frac{3}{4}$ E	SW. $\frac{3}{4}$ W	$4\frac{3}{4}$	53 26 15
NE. by E	NW. by W	SE. by E	SW. by W	5	56 15 00
NE. by E. $\frac{1}{4}$ E	NW. by W. $\frac{1}{4}$ W	SE. by E. $\frac{1}{4}$ E	SW. by W. $\frac{1}{4}$ W	$5\frac{1}{4}$	59 03 45
NE. by E. $\frac{1}{2}$ E	NW. by W. $\frac{1}{2}$ W	SE. by E. $\frac{1}{2}$ E	SW. by W. $\frac{1}{2}$ W	$5\frac{1}{2}$	61 52 30
NE. by E. $\frac{3}{4}$ E	NW. by W. $\frac{3}{4}$ W	SE. by E. $\frac{3}{4}$ E	SW. by W. $\frac{3}{4}$ W	$5\frac{3}{4}$	64 41 15
ENE	WNW	ESE	WSW	6	67 30 00
ENE. $\frac{1}{4}$ E	WNW. $\frac{1}{4}$ W	ESE. $\frac{1}{4}$ E	WSW. $\frac{1}{4}$ W	$6\frac{1}{4}$	70 18 45
ENE. $\frac{1}{2}$ E	WNW. $\frac{1}{2}$ W	ESE. $\frac{1}{2}$ E	WSW. $\frac{1}{2}$ W	$6\frac{1}{2}$	73 07 30
ENE. $\frac{3}{4}$ E	WNW. $\frac{3}{4}$ W	ESE. $\frac{3}{4}$ E	WSW. $\frac{3}{4}$ W	$6\frac{3}{4}$	75 56 15
E. by N	W. by N	E. by S	W. by S	7	78 45 00
E. $\frac{3}{4}$ N	W. $\frac{3}{4}$ N	E. $\frac{3}{4}$ S	W. $\frac{3}{4}$ S	$7\frac{1}{4}$	81 33 45
E. $\frac{1}{2}$ N	W. $\frac{1}{2}$ N	E. $\frac{1}{2}$ S	W. $\frac{1}{2}$ S	$7\frac{1}{2}$	84 22 30
E. $\frac{1}{4}$ N	W. $\frac{1}{4}$ N	E. $\frac{1}{4}$ S	W. $\frac{1}{4}$ S	$7\frac{3}{4}$	87 11 15
East	West	East	West	8	90 00 00

28. The compass card is mounted in a bowl which is carried in *gimbals*, thus enabling the card to retain a horizontal position while the ship is pitching and rolling. A vertical black line called the *lubber's line* is marked on the inner surface of the bowl, and the compass is so mounted that a line joining its pivot with the lubber's line is parallel to the keel line of the vessel; thus the lubber's line always indicates the compass direction of the ship's head.

29. According to the purpose which it is designed to fulfill, a compass is designated as a *Standard*, *Steering*, *Check*, or *Boat Compass.*

30. There are two types of compass in use, the *wet* or *liquid* and the *dry;* in the former the bowl is filled with liquid, the card being thus partially buoyed, with consequent increased ease of working on the pivot, and the liquid further serving to decrease the vibrations of the card when deflected by reason of the motion of the vessel or other cause. On account of its advantages the liquid compass is used in the United States Navy.

31. THE NAVY SERVICE 7½-INCH LIQUID COMPASS.—This consists of a skeleton card 7½ inches in diameter, made of tinned brass, resting on a pivot in liquid, with provisions for two pairs of magnets symmetrically placed.

The magnet system of the card consists of four cylindrical bundles of steel wires; these wires are laid side by side and magnetized as a bundle between the poles of a powerful electromagnet. They are afterwards placed in a cylindrical case, sealed, and secured to the card. Steel wires made up into a bundle were adopted because they are more homogeneous, can be more perfectly tempered, and for the same weight give greater magnetic power than a solid steel bar.

Two of the magnets are placed parallel to the north and south diameter of the card, and on the chords of 15° (nearly) of a circle passing through their extremities. These magnets penetrate the air vessel, to which they are soldered, and are further secured to the bottom of the ring of the card. The other two magnets of the system are placed parallel to the longer magnets on the chords of 45° (nearly) of a circle passing through their extremities, and are secured to the bottom of the ring of the card.

The card is of a curved annular type, the outer ring being convex on the upper and inner side, and is graduated to read to one-fourth point, a card circle being adjusted to its outer edge and divided to half-degrees, with legible figures at each 3°, for use in reading bearings by an azimuth circle or in laying the course to degrees.

The card is provided with a concentric spheroidal air vessel, to buoy its own weight and that of the magnets, allowing a pressure of between 60 and 90 grains on the pivot at 60° F.; the weight of the card in air is 3,060 grains. The air vessel has within it a hollow cone, open at its lower end, and provided with the pivot bearing, or cap, containing a sapphire, which rests upon the pivot and thus supports the card; the cap is provided with adjusting screws for accurately centering the card. The pivot is fastened to the center of the bottom of the bowl by a flanged plate and screws. Through this plate and the bottom of the bowl are two small holes which communicate with the expansion chamber and admit of a circulation of the liquid between it and the bowl. The pivot is of gun metal with an iridium cap.

The card is mounted in a bowl of cast bronze, the glass cover of which is closely packed with rubber, preventing the evaporation or leakage of the liquid, which entirely fills the bowl. This liquid is composed of 45 per cent pure alcohol and 55 per cent distilled water, and remains liquid below —10° F.

The lubber's line is a fine line drawn on an enameled plate on the inside of the bowl, the inner surface of the latter being covered with an insoluble white paint.

Beneath the bowl is a metallic self-adjusting expansion chamber of elastic metal, by means of which the bowl is kept constantly full without the show of bubbles or the development of undue pressure caused by the change in volume of the liquid due to changes of temperature.

The rim of the compass bowl is made rigid and its outer edge turned strictly to gauge to receive the azimuth circle.

32. THE DRY COMPASS.—The *Lord Kelvin Compass*, which may be regarded as the standard for the nonliquid type, consists of a strong paper card with the central parts cut away and its outer edge stiffened by a thin aluminum ring. The pivot is fitted with an iridium point, upon which rests a small light aluminum boss fitted with a sapphire bearing. Radiating from this boss are 32 silk threads whose outer ends are made fast to the inner edge of the compass card; these threads sustain the weight of the suspended card, and, as they possess some elasticity, tend to decrease the shocks due to motion.

Eight small steel wire needles, 3¼ to 2 inches long, are secured normally to two parallel silk threads, and are slung from the aluminum rim of the card by other silk threads which pass through eyes in the ends of the outer pair of needles. The needles are below the radial threads, thus keeping the center of gravity low.

33. THE AZIMUTH CIRCLE.—This is a necessary fitting for all compasses employed for taking bearings—that is, noting the directions—of either celestial or terrestrial objects. The instrument varies widely in its different forms; the essential features which all share consist in (a) a pair of sight vanes, or equivalent device, at the extremities of the diameter of a circle that revolves concentrically with the compass bowl, the line of sight thus always passing through the vertical axis of the compass; and (b) a system, usually of mirrors and prisms, by which the point of the compass card cut by the vertical plane through the line of sight—in other words, the compass direction—is brought into the field of view of the person making the observation. In some circles, for observing azimuths of the sun advantage is taken of the brightness of that body to reflect a pencil of light upon the card in such a manner as to indicate the bearing; such an azimuth circle is used in the United States Navy.

34. BINNACLES.—Compasses are mounted for use in stands known as *Binnacles*, of which there are two principal types—the *Compensating* and the *Non-Compensating Binnacle*, so designated according as they are or are not equipped with appliances by which the deviation of the compass, or error in its indications due to disturbing magnetic features within the ship, may be compensated.

Binnacles may be of wood or of some nonmagnetic metal; all contain a compass chamber within which the compass is suspended in its gimbal ring, the knife edges upon which it is suspended resting in V-shaped bearings; an appropriate method is supplied for centering the compass. A hood is provided for the protection of the compass and for lighting it at night. Binnacles must be rigidly secured to the deck of the vessel in such position that the lubber's line of the compass gives true indications of the direction of the ship's head.

The position of the various binnacles on shipboard and the height at which they carry the compass must be chosen with regard to the purpose which the compass is to serve, having in mind the magnetic conditions of the ship.

Compensating binnacles contain the appliances for carrying the various correctors used in the compensation of the deviation of the compass. These consist of (a) a system of permanent magnets for

semicircular deviation, placed in a magnet chamber lying immediately beneath the compass chamber, so arranged as to permit variation in the height and direction of the magnets employed; (*b*) a pair of arms projecting horizontally from the compass chamber and supporting masses of soft iron for quadrantal deviation; (*c*) a central tube in the vertical axis of the binnacle for a permanent magnet used to correct the heeling error, and (*d*) an attachment, sometimes fitted, for securing a vertical soft iron rod, or "Flinders bar," used in certain cases for correction of a part of the semicircular deviation. An explanation of the various terms here used, together with the method of compensating the compass, will be given in Chapter III.

THE PELORUS.

35. This instrument consists of a circular plate, mounted horizontally in gimbals upon a vertical standard, at some point on board ship affording a clear view for taking bearings; radial scores upon a raised flange on the periphery of this plate indicate true directions from its center parallel with the keel line of the vessel and perpendicular thereto—in other words, lines of bearing directly ahead, astern, and abeam. Revolving about a common center, which is also the center of the plate, are (*a*) a dumb compass card, usually engraved on metal, whose face is level with the raised periphery of the plate on which are marked the scores, and (*b*) a pivoted horizontal bar carrying at its extremities a pair of sight vanes so arranged that the line of sight always passes through the vertical axis of the instrument, and having an index showing the point at which the line of sight cuts the dumb compass. The dumb compass and the sight-vane bar can each be rigidly clamped.

The instrument is used for taking bearings, and may be more convenient than the compass for that purpose because of the better view that it affords, as well as because it may be made to eliminate the compass error from observed bearings. Suppose that the dumb compass be revolved until the degree or division which is coincident with the right-ahead score of the plate is the same as that which is abreast the lubber's line of the ship's compass. Then all directions indicated by the dumb compass will be parallel to the corresponding directions of the live one, and all bearings taken by the pelorus will be identical with those taken by the compass (leaving out of the question the diffence due to the distance that separates them). Suppose, now, that it is known that the ship's compass has a certain error and that the correct direction that we seek (which is the one indicated on the charts) is a certain angular distance to the right or left of that which the compass shows; if, in such a case, instead of setting the pelorus for the direction indicated by compass, we set it for the correct direction in which we know the ship to be heading, all bearings observed by the pelorus will be correct bearings as given by the chart and may be plotted directly thereon without the necessity for the intermediate process of correction to which the bearings shown by compass are subject. It will at once be evident that the indications of the pelorus will be accurate only when bearings are taken at an instant when the ship is heading exactly in the direction for which it is set, and care must be taken accordingly in its use.

The most modern types of pelorus are fitted for illuminating the dumb compass, thus greatly facilitating night work.

THE CHART.

36. A nautical *chart* is a miniature representation upon a plane surface, in accordance with a definite system of projection or development, of a portion of the navigable waters of the world. It generally includes the outline of the adjacent land, together with the surface forms and artificial features that are useful as aids to navigation, and sets forth the depths of water, especially in the near approaches to the land, by soundings that are fixed in position by accurate determinations. Except in charts of harbors or other localities so limited that the curvature of the earth is inappreciable on the scale of construction, a nautical chart is always framed over with a network of parallels of latitude and meridians of longitude in relation to which the features to be depicted on the chart are located and drawn; and the mathematical relation between the meridians and parallels of the chart and those of the terrestrial sphere determines the method of measurement that is to be employed on the chart and the special uses to which it is adapted.

37. There are three principal systems of projection in use: (*a*) the *Mercator*, (*b*) the *polyconic*, and (*c*) the *gnomonic;* of these, the Mercator is by far the most generally used for purposes of navigation proper, while the polyconic and the gnomonic charts are employed for nautical purposes in a more restricted manner, as for plotting surveys or for facilitating great circle sailing.

38. The Mercator Projection.—The *Mercator Projection*, so called, may be said to result from the development, upon a plane surface, of a cylinder which is tangent to the earth at the equator, the various points of the earth's surface having been projected upon the cylinder in such manner that the *loxodromic curve* or *rhumb line* (art. 6, Chap. I) appears as a right line preserving the same angle of bearing with respect to the intersected meridians as does the ship's track.

In order to realize this condition, the line of tangency, which coincides with the earth's equator, being the circumference of a right section of the cylinder, will appear as a right line on the development; while the series of elements of the cylinder corresponding to the projected terrestrial meridians will appear as equidistant right lines, parallel to each other and perpendicular to the equator of the chart, maintaining the same relative positions and the same distance apart on that equator as the meridians have on the terrestrial spheroid. The series of terrestrial parallels will also appear as a system of right lines parallel to each other and to the equator, and will so intersect the meridians as to form a system of rectangles whose altitudes, for successive intervals of latitude, must be variable, increasing from the equator in such manner that the angles made by the rhumb line with the meridian on the chart may maintain the required equality with the corresponding angles on the spheroid.

39. Meridional Parts.—At the equator a degree of longitude is equal to a degree of latitude, but in receding from the equator and approaching the pole, while the degrees of latitude remain always of the same length (save for a slight change due to the fact that the earth is not a perfect sphere), the degrees of longitude become less and less.

Since, in the Mercator projection, the degrees of longitude are made to appear everywhere of the same length, it becomes necessary, in order to preserve the proportion that exists at different parts of the earth's surface between degrees of latitude and degrees of longitude, that the former be increased from their natural lengths, and such increase must become greater and greater the higher the latitude.

The length of the meridian, as thus increased, between the equator and any given latitude, expressed in minutes at the equator as a unit, constitutes the number of *Meridional Parts* corresponding to that latitude. The Table of Meridional Parts or Increased Latitudes (Table 3), computed for every minute of latitude between 0° and 80°, affords facilities for constructing charts on the Mercator projection and for solving problems in Mercator sailing.

40. To Construct a Mercator Chart.—If the chart for which a projection is to be made includes the equator, the values to be measured off are given directly by Table 3. If the equator does not come upon the chart, then the parallels of latitude to be laid down should be referred to a *principal parallel*, preferably the lowest parallel to be drawn on the chart. The distance of any other parallel of latitude from the principal parallel is then the difference of the values for the two taken from Table 3.

The values so found may either be measured off, without previous numerical conversion, by means of a diagonal scale constructed on the chart, or they may be laid down on the chart by means of any properly divided scale of yards, meters, feet, or miles, after having been reduced to the scale of proportions adopted for the chart.

If, for example, it be required to construct a chart on a scale of one-quarter of an inch to five minutes of arc on the equator, a diagonal scale may first be constructed, on which ten meridional parts, or ten minutes of arc on the equator, have a length of half an inch.

It may often be desirable to adapt the scale to a certain allotment of paper. In this case, the lowest and the highest parallels of latitude may first be drawn on the sheet on which the transfer is to be made. The distance between these parallels may then be measured, and the number of meridional parts between them ascertained. Dividing the distance by this number will then give the length of one meridional part, or the quantity by which *all* the meridional parts taken from Table 3 must be multiplied. This quantity will represent the *scale of the chart*. If it occurs that the limits of longitude are a governing consideration, the case may be similarly treated.

Example: Let a projection be required for a chart of 14° extent in longitude between the parallels of latitude 20° 30′ and 30° 25′, and let the space allowable on the paper between these parallels measure 10 inches.

Entering the column in Table 3 headed 20°, and running down to the line marked 30′ in the side column, will be found 1248.9; then, entering the column 30°, and running down to the line of 25′, will be found 1905.5. The difference, or 1905.5 — 1248.9 = 656.6, is the value of the meridional arc between these latitudes, for which 1′ of arc of the equator is taken as the unit. On the intended projection, therefore, 1′ of arc of longitude will measure $\frac{10^{\text{in}}}{656.6} = 0.0152$ inch, which will be the scale of the chart. For the sake of brevity call it 0.015. By this quantity all the values derived from Table 3 will have to be multiplied before laying them down on the projection, if they are to be measured on a diagonal scale of one inch.

Draw in the center of the sheet a straight line, and assume it to be the middle meridian of the chart. Construct very carefully on this line a perpendicular near the lower border of the sheet, and assume this perpendicular to be the parallel of latitude 20° 30′; this will be the southern inner neat line of the chart. From the intersection of the lines lay off on the parallel, on each side of the middle meridian, seven degrees of longitude, or distances each equal to $0.015 \times 60 \times 7 = 6.3$ inches; and through the points thus obtained draw parallel lines to the middle meridian, and these will be the eastern and western neat lines of the chart.

In order to construct the parallel of latitude for 21° 00′, find, in Table 3, the meridional parts for 21° 00′, which are 1280.8. Subtracting from this number the number for 20° 30′, and multiplying the difference by 0.015, we obtain 0.478 inch, which is the distance on the chart between 20° 30′ and 21° 00′. On the meridians lay off distances equal to 0.478 inch, and through the three points thus obtained draw a straight line, which will be the parallel of 21° 00′.

Proceed in the same manner to lay down all the parallels answering to full degrees of latitude; the distances will be respectively:

$$0^{\text{in}}.015\times(1344.9-1248.9)=1.440 \text{ inches},$$
$$0^{\text{in}}.015\times(1409.5-1248.9)=2.409 \text{ inches},$$
$$0^{\text{in}}.015\times(1474.5-1248.9)=3.384 \text{ inches, etc.}$$

Thus will be shown the parallels of latitude 22° 00′, 23° 00′, 24° 00′, etc. Finally, lay down in the same way the parallel of latitude 30° 25′, which will be the northern inner neat line of the chart.

A degree of longitude will measure on this chart $0^{\text{in}}.015\times60=0^{\text{in}}.9$. Lay off, therefore, on the lowest parallel of latitude drawn on the chart, on a middle one, and on the highest parallel, measuring from the middle meridian toward each side, the distances of $0^{\text{in}}.9$, $1^{\text{in}}.8$, $2^{\text{in}}.7$, $3^{\text{in}}.6$, etc., in order to determine the points where meridians answering to full degrees cross the parallels drawn on the chart. Through the points thus found draw the meridians. Draw then the outer neat lines of the chart at a convenient distance outside of the inner neat lines, and extend to them the meridians and parallels. Between the inner and outer neat lines of the chart subdivide the degrees of latitude and longitude as minutely as the scale of the chart will permit, the subdivisions of the degrees of longitude being found by dividing the degrees into equal parts, and the subdivisions of the degrees of latitude being accurately found in the same manner as the full degrees of latitude previously described, though it will generally be found sufficiently exact to make even subdivisions of the degrees, as in the case of the longitude.

The subdivisions between the two eastern as well as those between the two western neat lines will serve for measuring or estimating terrestrial distances. Distances between points bearing North and South of each other may be ascertained by referring them to the subdivisions between the same parallels. Distances represented by lines at an angle to the meridians (loxodromic lines) may be measured

by taking between the dividers a small number of the subdivisions near the middle latitude of the line to be measured, and stepping them off on that line. If, for instance, the terrestrial length of a line running at an angle to the meridians between the parallels of latitude of 24° 00′ and 29° 00′ be required, the distance shown on the neat space between 26° 15′ and 26° 45′ (=30 nautical miles) may be taken between the dividers and stepped off on that line.

41. Coast lines and other positions are plotted on the chart by their latitude and longitude. A chart may be transferred from any other projection to that of Mercator by drawing a system of corresponding parallels of latitude and meridians over both charts so close to each other as to form minute squares, and then the lines and characters contained in each square of the map to be transferred may be copied by the eye in the corresponding squares of the Mercator projection.

Since the unit of measure, the mile or minute of latitude, has a different value in every latitude, there is an appearance of distortion in a Mercator chart that covers any large extent of surface; for instance, an island near the pole will be represented as being much larger than one of the same size near the equator, due to the different scale used to preserve the character of the projection.

42. The Polyconic Projection.—This projection is based upon the development of the earth's surface on a series of cones, a different one for each parallel of latitude, each one having the parallel as its base, and its vertex in the point where a tangent to the earth at that latitude intersects the earth's axis. The degrees of latitude and longitude on this chart are projected in their true length, and the general distortion of the figure is less than in any other method of projection, the relative magnitudes being closely preserved.

A straight line on the polyconic chart represents a great circle, making a slightly different angle with each successive meridian as the meridians converge toward the pole and are theoretically curved lines; but it is only on charts of large extent that this curvature is apparent; the parallels are also curved, this fact being apparent to the eye upon all excepting the largest scale charts.

This method of projection is especially adapted to the plotting of surveys; it is also employed for nearly all of the charts of the United States Coast and Geodetic Survey.

43. Gnomonic Projection.—This is based upon a system in which the plane of projection is tangent to the earth at some given point; the eye of the spectator is situated at the center of the sphere, where, being at once in the plane of every great circle, it will see all such circles projected as straight lines where the visual rays passing through them intersect the plane of projection. In a gnomonic chart, a straight line between any two points is projected as an arc of a great circle, and is therefore the shortest line between those points.

Excepting in the Polar regions, for which latitudes the Mercator projection can not be constructed, the gnomonic charts are not used for general navigating purposes. Their greatest application is to afford a ready means of finding the course and distance at any time in great circle sailing, the method of doing which will be explained in Chapter V.

44. Meridians Employed in Chart Construction.—The United States, England, Germany, Italy, Russia, Norway, Sweden, Denmark, Holland, Austria, Portugal, and Japan adopt as a prime meridian the *meridian of Greenwich.*

France adopts the *meridian of Paris* in Long. 2° 20′ 14″.5 E. of Greenwich.

Spain adopts the *meridian of San Fernando, Cadiz,* in Long. 6° 12′ 20″ W. of Greenwich.

The Pulkowa Observatory of St. Petersburg (sometimes referred to in Russian charts) is in Long. 30° 19′ 39″.6 E. of Greenwich.

The Royal Observatory of Naples (sometimes referred to in Italian charts) is in Long. 14° 14′ 06″ E. of Greenwich.

The meridian of Genoa is 8° 55′ 21″ E.; of Lisbon, 9° 08′ 36″ W.; of Rio de Janeiro, 43° 10′ 21″.2 W.; of Amsterdam, 4° 53′ 03″.8 E.; of Washington, 77° 03′ 56″.7 W.

45. Quality of Bottom.—The following table shows the qualities of the bottom, as expressed on charts of various nations:

United States.	English.	French.	Italian.	Spanish.	German.
Clay.............C.	Clay ....cl.	Argile.........A.	Argila..............	Arcillo or Barro.....	Lehm ....L.
Coral..........Co.	Coral.........crl.	Corail ....Cor.	Corállo..............	Coral..............cl.	Korallen.........K.
Gravel ....G.	Gravel.........g.	Gravier ......Gr.	Rena or Ghiaja.....	Cascájo ....Co.	Grob sand ......g. s.
Mud ....M.	Mud ....m.	Vase ....V.	Fango..............	Fango or Luno...F.	Schlemm ......Sch.
Rocky........rky.	Rock ....rk.	Roche..........R.	Roccia..............	Piedra or Roca...P.	Fels ....F.
Sand.............S.	Sand........ ..s.	Sable ....S.	Sábia or Aréna.....	Arena.............A.	Sand...............S.
Shells ....Sh.	Shells ....sh.	Coquille ....Coq.	Conchiglia	Conchuela.......ca.	Muschel ....M.
Stone ....St.	Stones.........st.	Pierre ....P.	Pietre	Piedra............P.	Stein.
Weed.........Wd.	Weed........wd.	Herb..........H.	Alga................	Alga ....A.	Gras...............G.
Fine..........fne.	Fine ....f.	Fin ....fin.	Fino................	Fina ....f.	Fein ....f.
Coarse ....crs.	Coarse ....c.	Gros ....g.	Grosso..............	Gruesa................	Grob...............g.
Stiff ....stf.	Stiff ....stf.	Dure ....d.	Tenace.............	Tenaz................	Zahe ....Z.
Soft ....sft.	Soft ....sft.	Molle ....m.	Molle...............	Muelle	Weich ....W.
Black ....bk.	Black ....blk.	Noire..........n.	Nero................	Negro	Schwarz......schw.
Red ....rd.	Red ....rd.	Rouge ....r.	Rosse...............	Rojo.................	Roth.
Yellow.........yl.	Yellow ....y.	Jaune..........j.	Giallo	Amarillo	Gelb.
Gray ....gy.					

46. Measures of Depth.—The following table shows the measures of depth employed in the charts of certain foreign nations, with their equivalents in English measures:

		English feet.	English fathoms.
Austrian	fathom (klafter)	6.222	1.030
Danish and Norwegian	fathom (farn)	6.175	1.029
Dutch	fathom (vaden)	5.575	0.929
French	fathom (brasse)	5.329	0.888
	meter (mètre)	3.281	0.547
Portuguese	fathom (braça)	6.004	1.000
Prussian	fathom (faden)	5.906	0.984
Russian	fathom (sajen)	6.000	1.000
Spanish	fathom (braza)	5.492	0.915
Swedish	fathom (famn)	5.843	0.974

The Dutch *elle*, the Spanish, Portuguese, and Italian *metro*, and the French *mètre* are identical.

A *pied usuel*=13.124 inches, or 1.094 feet. A *mètre* is 3 *pieds;* a *pied du roi*=12.7896 inches; *brasse* is used upon old French charts instead of *mètre*. Upon some Italian charts soundings are in French *pieds.*

THE BAROMETER.

47. The *barometer* is an instrument for measuring the pressure of the atmosphere, and is of great service to the mariner in affording a knowledge of existing meteorological conditions and of the probable changes therein. There are two classes of barometer—*mercurial* and *aneroid.*

Fig. 3.

Fig. 4.

48. The Mercurial Barometer.—This instrument, invented by Torricelli in 1643, indicates the pressure of the atmosphere by the height of a column of mercury.

If a glass tube of uniform internal diameter somewhat more than 30 inches in length and closed at one end be completely filled with pure mercury, and then placed, open end down, in a cup of mercury (the open end having been temporarily sealed to retain the liquid during the process of inverting), it will be found that the mercury in the tube will fall until the top of the column is about 30 inches above the level of that which is in the cup, leaving in the upper part of the tube a perfect vacuum. Since the weight of the column of mercury thus left standing in the tube is equal to the pressure by which it is held in position—namely, that of the atmospheric air—it follows that the height of the column is subject to variation upon variation of that pressure; hence the mercury falls as the pressure of the atmosphere decreases and rises as that pressure increases. The mean pressure of the atmosphere is equal to nearly 15 pounds to the square inch; the mean height of the barometer is about 30 inches.

49. In the practical construction of the barometer the glass tube which contains the mercury is encased in a brass tube, the latter terminating at the top in a ring to be used for suspension, and at the bottom in a flange, to which the several parts forming the cistern are attached. The upper part of the brass tube is partially cut away to expose the mercurial column for observation; abreast this opening is fitted a scale for measuring the height, and along the scale travels a *vernier* for exact reading; the motion of the vernier is controlled by a rack and pinion, the latter having a milled head accessible to the observer, by which the adjustment is made. In the middle of the brass tube is fixed a thermometer, the bulb of which is covered from the outside but open toward the mercury, and which, being nearly in contact with the glass tube, indicates the temperature of the mercury and not that of the external air; the central position of the column is selected in order that the mean temperature may be obtained—a matter of importance, as the temperature of the mercurial column must be taken into account in every accurate application of its reading.

50. In the arrangement of further details mercurial barometers are divided into two classes, according as they are to be used as *Standards* (fig. 4) on shore, or as *Sea Barometers* (fig. 3) on shipboard.

In the Standard Barometer the scale and vernier are so graduated as to enable an observer to read the height of the mercurial column to the nearest 0.002 inch, while in the Sea Barometer the reading can not be made closer than 0.01 inch.

The instruments also differ in the method of obtaining the true height of the mercurial column at varying levels of the liquid in the cistern. It is evident that as the mercury in the tube rises, upon increase of atmospheric pressure, the mercury in the cistern must fall; and, conversely, when the mercurial column falls the amount of fluid in the cistern will thereby be increased and a rise of level will occur. As the height of the mercurial column is required above the existing level in the cistern, some means must be adopted to obtain the true height under varying conditions. In the Standard Barometer the mercury of the cistern is contained in a leather bag, against the bottom of which presses the point of a vertical screw, the milled

head of the screw projecting from the bottom of the instrument and thus placing it under control of the observer. By this means the surface of the mercury in the cistern (which is visible through a glass casing) may be raised or lowered until it exactly coincides with that level which is chosen as the zero of the scale, and which is indicated by an ivory pointer in plain view.

In the Sea Barometer there is no provision for adjusting the level of the cistern to a fixed point, but compensation for the variable level is made in the scale graduations; a division representing an inch on the scale is a certain fraction short of the true inch, proper allowance being thus made for the rise in level which occurs with a fall of the column, and for the reverse condition.

Further modification is made in the Sea Barometer to adapt it to the special use for which intended. The tube toward its lower end is much contracted to prevent the oscillation of the mercurial column known as "pumping," which arises from the motion of the ship; and just below this point is a trap to arrest any small bubbles of air from finding their way upward. The instrument aboard ship is suspended in a revolving center-ring, in gimbals, supported on a horizontal brass arm which is screwed to the bulkhead; a vertical position is thus maintained by the tube at all times.

51. The *vernier* is an attachment for facilitating the exact reading of the scale of the barometer, and is also applied to many other instruments of precision, as, for example, the sextant and theodolite. It consists of a metal scale similar in general construction to that of the instrument to which it is fitted, and arranged to move alongside of and in contact with the main scale.

The general principle of the vernier requires that its scale shall have a total length exactly equal to some whole number of divisions of the scale of the instrument and that this length shall be subdivided into a number of parts equal to 1 more or 1 less than the number of divisions of the instrument scale which are covered; thus, if a space of 9 divisions of the main scale be designated as the length of the vernier, the vernier scale would be divided into either 8 or 10 parts.

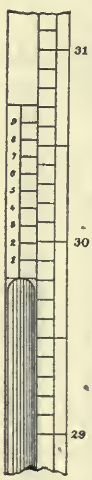

Fig. 5.

Suppose that a barometer scale be divided into tenths of an inch and that a length of 9 divisions of such a scale be divided into 10 parts for a vernier (fig. 5); and suppose that the divisions of the vernier be numbered consecutively from zero at the origin to 10 at the upper extremity. If, now, by means of the movable rack and pinion, the bottom or zero division of the vernier be brought level with the top of the mercurial column, and that division falls into exact coincidence with a division of the main scale, then the height of the column will correspond with the scale reading indicated. In such a case the top of the vernier will also exactly coincide with a scale division, but none of the intermediate divisions will be evenly abreast of such a division; the division marked "1" will fall short of a scale division by one-tenth of 1 divison of the scale, or by 0.01 inch; that marked "2" by two-tenths of a division, or 0.02 inch, and so on. If the vernier, instead of having the zero coincide with a scale division, has the division "1" in such coincidence, it follows that the mercurial column stands at 0.01 inch above that scale division which is next below the zero; for the division "2," at 0.02 inch; and similarly for the others. In the case portrayed in figure 5, the reading of the column is 29.81 inches, the scale division next below the zero being 29.80 inches, while the fact that the first division is abreast a mark of the scale shows that 0.01 inch must be added to this to obtain the exact reading.

Had an example been chosen in which 8 vernier divisions covered 9 scale divisions—that is, where the number of vernier divisions was 1 less than the number of scale divisions covered—the principle would still have applied. But, instead of the length of 1 division of the vernier falling short of a division of the scale by one-tenth the length of the latter, it would have fallen beyond by one-eighth. To read in such a case it would therefore be necessary to number the vernier divisions from up downward and to regard the subdivisions as $\frac{1}{80}$ instead of 0.01 inch.

It is a general rule that the smallest measure to which a vernier reads is equal to the length of 1 division of the scale divided by the number of divisions of the vernier; hence, by varying either the scale or the vernier, we may arrive at any subdivision that may be desired.

52. The Sea Barometer is arranged as described for the instrument assumed in the illustration; the scale divisions are tenths of an inch, and the vernier has 10 divisions, whence it reads to 0.01 inch. It is not necessary to seek a closer reading, as complete accuracy is not attainable in observing the height of a barometer on a vessel at sea, nor is it essential. The Standard Barometer on shore, however, is capable of very exact reading; hence each scale division is made equal to half a tenth, or 0.05 inch, while a vernier covering 24 such divisions is divided into 25 parts; hence the column may be read to 0.002 inch.

53. To adjust the vernier for reading the height of the mercurial column the eye should be brought exactly on a level with the top of the column; that is, the line of sight should be at right angles to the scale. When properly set, the front and rear edges of the vernier and the uppermost point of the mercury should all be in the line of sight. A piece of white paper, held at the back of the tube so as to reflect the light, assists in accurately setting the vernier by day, while a small bull's-eye lamp held behind the instrument enables the observer to get a correct reading at night. When observing the barometer it should hang freely, not being inclined by holding or even by touch, because any inclination will cause the column to rise in the tube.

54. Other things being equal, the mercury will stand higher in the tube when it is warm than when it is cold, owing to expansion. For the purposes of comparison, all barometric observations are reduced to a standard which assumes 32° F. as the temperature of the mercurial column, and 62° F. as that of the metal scale; it is therefore important to make this reduction, as well as that for instrumental error (art. 56), in order to be enabled to compare the true barometric pressure with the normal that may be expected for any locality. The following table gives the value of this correction for each 2° F.,

the plus sign showing that the correction is to be added to the reading of the ship's barometer and the minus sign that it is to be subtracted:

Temperature.	Correction.	Temperature.	Correction.	Temperature.	Correction.	Temperature.	Correction.
°	*Inch.*	°	*Inch.*	°	*Inch.*	°	*Inch.*
20	+0.02	40	−0.03	60	−0.09	80	−0.14
22	+0.02	42	−0.04	62	−0.09	82	−0.14
24	+0.01	44	−0.04	64	−0.09	84	−0.15
26	+0.01	46	−0.05	66	−0.10	86	−0.15
28	0.00	48	−0.05	68	−0.10	88	−0.16
30	0.00	50	−0.06	70	−0.11	90	−0.16
32	−0.01	52	−0.06	72	−0.12	92	−0.17
34	−0.02	54	−0.07	74	−0.12	94	−0.17
36	−0.02	56	−0.07	76	−0.13	96	−0.18
38	−0.03	58	−0.08	78	−0.13	98	−0.18

As an example, let the observed reading of the mercurial barometer be 29.95 inches, and the temperature as given by the attached thermometer 74°; then we have:

	″
Observed height of the mercury	29.95
Correction for temperature (74°)	−0.12
Height of the mercury at standard temperature	29.83

55. The Aneroid Barometer.—This is an instrument in which the pressure of the air is measured by means of the elasticity of a plate of metal. It consists of a cylindrical brass box, the metal in the sides being very thin; the contained air having been partially, though not completely, exhausted, the box is hermetically sealed. When the pressure of the atmosphere increases the inclosed air is compressed, the capacity of the box is diminished, and the two flat ends approach each other; when the pressure of the atmosphere decreases, the ends recede from one another in consequence of the expansion of the inclosed air. By means of a combination of levers, this motion of the ends of the box is communicated to an index pointer which travels over a graduated dial plate, the mechanical arrangement being such that the motion of the ends of the box is magnified many times, a very minute movement of the box making a considerable difference in the indication of the pointer. The graduations of the aneroid scale are obtained by comparison with the correct readings of a standard mercurial barometer under normal and reduced atmospheric pressure.

The thermometer attached to the aneroid barometer is merely for convenience in indicating the temperature of the air, but as regards the instrument itself, no correction for temperature can be applied with certainty. Aneroids, as now manufactured, are almost perfectly compensated for temperature by the use of different metals having unequal coefficients of expansion; they ought, therefore, to show the same pressure at all temperatures.

The aneroid barometer, from its small size and the ease with which it may be transported, can often be usefully employed under circumstances where a mercurial barometer would not be available. It also has an advantage over the mercurial instrument in its greater sensitiveness, and the fact that it gives earlier indications of change of pressure. It can, however, be relied upon only when frequently compared with a standard mercurial barometer; moreover, considerable care is required in its handling; while slight shocks will not ordinarily affect it, a severe jar or knock may change its indications by a large amount.

When in use the aneroid barometer may be suspended vertically or placed flat, but changing from one position to another ordinarily makes a sensible change in the readings; the instrument should always, therefore, be kept in the same position, and the errors determined by comparisons made while occupying its customary place.

56. Comparison of Barometers.—To determine the reliability of the ship's barometer, whether mercurial or aneroid, comparisons should from time to time be made with a standard barometer. Nearly all instruments read either too high or too low by a small amount. These errors arise, in a mercurial barometer, from the improper placing of the scale, lack of uniformity of caliber of the glass tube, or similar causes; in an aneroid, which is less accurate and in which there is even more necessity for frequent comparisons, errors may be due to derangement of any of the various mechanical features upon which its working depends. The errors of the barometer should be determined for various heights, as they are seldom the same at all parts of the scale.

In the principal ports of the world standard barometers are observed at specified times each day, and the readings, reduced to zero and to sea level, are published. It is therefore only necessary to read the barometer on shipboard at those times, and, if a mercurial instrument is used, to note the attached thermometer and apply the correction for temperature (art. 54). It is evident that a comparison of the heights by reduced standard and by the ship's barometer will give the correction to be applied to the latter, including the instrumental error, the reduction to sea level, and the personal error of the observer. In the United States, standard barometer readings are made by the Weather Bureau and Branch Hydrographic offices.

Aneroid barometers may be adjusted for instrumental error by moving the index hand, but this is usually done only in the case of errors of considerable magnitude.

57. Determination of Heights by Barometer.—The barometer may be used to determine the difference in heights between any two stations by means of the difference in atmospheric pressure

between them. An approximate rule is to allow 0.0011 inch for each difference in level of one foot, or, more roughly, 0.01 inch for every 9 feet.

A very exact method is afforded by Babinet's formula. If B_o and B represent the barometric pressure (corrected for all sources of instrumental error) at the lower and at the upper stations respectively, and t_0 and t the corresponding temperatures of the air; then,

$$\text{Diff. in height} = C \times \frac{B_o - B}{B_o + B};$$

if the temperatures be taken by a Farhenheit thermometer,

$$C \text{ (in feet)} = 52{,}494 \left(1 + \frac{t_0 + t - 64}{900}\right);$$

if a centigrade thermometer is used,

$$C \text{ (in meters)} = 16{,}000 \left(1 + \frac{2(t_o + t)}{1000}\right).$$

THE THERMOMETER.

58. The *Thermometer* is an instrument for indicating temperature. In its construction advantage is taken of the fact that bodies are expanded by heat and contracted by cold. In its most usual form the thermometer consists of a bulb filled with mercury, connected with a tube of very fine cross-sectional area, the liquid column rising or falling in the tube according to the volume of the mercury due to the actual degree of heat, and the height of the mercury indicating upon a scale the temperature; the mercury contained in the tube moves in a vacuum produced by the expulsion of the air through boiling the mercury and then closing the top of the tube by means of the blowpipe.

There are three classes of thermometer, distinguished according to the method of graduating the scale as follows: the *Fahrenheit*, in which the freezing point of water is placed at 32° and its boiling point (under normal atmospheric pressure) at 212°; the *Centigrade*, in which the freezing point is at 0° and the boiling point at 100°; and the *Réaumur*, in which these points are at 0° and 80°, respectively. The Fahrenheit thermometer is generally used in the United States and England. Tables will be found in this work for the interconversion of the various scale readings (Table 31).

59. The thermometer is a valuable instrument for the mariner, not only by reason of the aid it affords him in judging meteorological conditions from the temperature of the air and the amount of moisture it contains, but also for the evidences it furnishes at times, through the temperature of the sea water, of the ship's position and the probable current that is being encountered.

60. The thermometers employed in determining the temperature of the air (wet and dry bulb) and of the water at the surface, should be mercurial, and of some standard make, with the graduation etched upon the glass stem; they should be compared with accurate standards, and not accepted if their readings vary more than 1° from the true at any point of the scale.

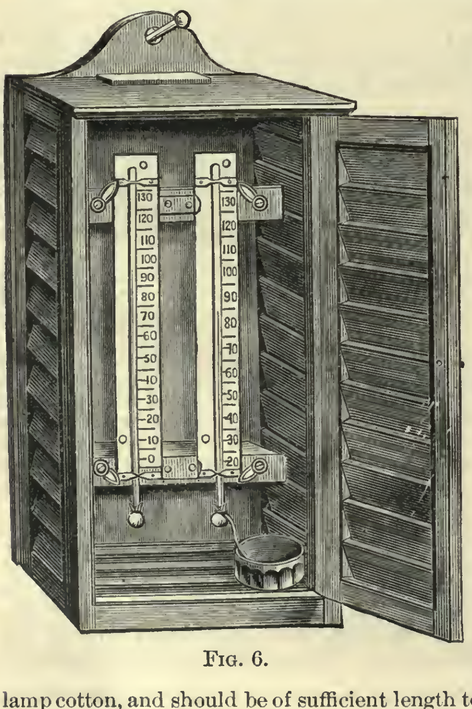

FIG. 6.

61. The dry-bulb thermometer gives the temperature of the free air. The wet-bulb thermometer, an exactly similar instrument the bulb of which is surrounded by an envelope of moistened cloth, gives what is known as the *temperature of evaporation*, which is always somewhat less than the temperature of the free air. From the difference of these two temperatures the observer may determine the proximity of the air to saturation; that is, how near the air is to that point at which it will be obliged to precipitate some of its moisture (water vapor) in the form of liquid. With the envelope of the wet bulb removed, the two thermometers should read precisely the same; otherwise they are practically useless.

The two thermometers, the wet and the dry bulb, should be hung within a few inches of each other, and the surroundings should be as far as possible identical. In practice the two thermometers are generally inclosed within a small lattice case, such as that shown in figure 6; the case should be placed in a position on deck remote from any source of artificial heat, sheltered from the direct rays of the sun, and from the rain and spray, but freely exposed to the circulation of the air; the door should be kept closed except during the process of reading. The cloth envelope of the wet bulb should be a single thickness of fine muslin, tightly stretched over the bulb, and tied with a fine thread. The wick which serves to carry the water from the cistern to the bulb should consist of a few threads of lamp cotton, and should be of sufficient length to admit of two or three inches being coiled in the cistern. The muslin envelope of the wet bulb should be at all times thoroughly moist, but not dripping.

When the temperature of the air falls to 32° F. the water in the wick freezes, the capillary action is at an end, the bulb in consequence soon becomes quite dry, and the thermometer no longer shows the temperature of evaporation. At such times the bulb should be thoroughly wetted with ice-cold water shortly before the time of observation, using for this purpose a camel's hair brush or feather; by

this process the temperature of the wet bulb is temporarily raised above that of the dry, but only for a brief time, as the water quickly freezes; and inasmuch as evaporation takes place from the surface of the ice thus formed precisely as from the surface of the water, the thermometer will act in the same way as if it had a damp bulb. The wet-bulb thermometer can not properly read higher than the dry, and if the reading of the wet bulb should be the higher, it may always be attributed to imperfections in the instruments.

62. Knowing the temperature of the wet and dry bulbs, the relative humidity of the atmosphere at the time of observation may be found from the following table:

Temperature of the air, dry-bulb thermometer.	Difference between dry-bulb and wet-bulb readings.									
	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°
°	*Per ct.*	*Per ct.*	*Per ct.*	*Per ct.*	*Per ct.*	*Per ct.*	*Per ct.*	*Per ct.*	*Per ct.*	*Per ct.*
24	87	75	62	50	38	26				
26	88	76	65	53	42	30				
28	89	78	67	56	45	34	24			
30	90	79	68	58	48	38	28			
32	90	80	70	61	51	41	32	23		
34	90	81	72	63	53	44	35	27		
36	91	82	73	64	55	47	38	30	22	
38	92	83	75	66	57	50	42	34	26	
40	92	84	76	68	59	52	44	37	30	22
42	92	84	77	69	61	54	47	40	33	26
44	92	85	78	70	63	56	49	43	36	29
46	93	85	79	72	65	58	51	45	38	32
48	93	86	79	73	66	60	53	47	41	35
50	93	87	80	74	67	61	55	49	43	37
52	94	87	81	75	69	63	57	51	46	40
54	94	88	82	76	70	64	59	53	48	42
56	94	88	82	77	71	65	60	55	50	44
58	94	89	83	78	72	67	61	56	51	46
60	94	89	84	78	73	68	63	58	53	48
62	95	89	84	79	74	69	64	59	54	50
64	95	90	85	79	74	70	65	60	56	51
66	95	90	85	80	75	71	66	61	57	53
68	95	90	85	81	76	71	67	63	58	54
70	95	90	86	81	77	72	68	64	60	55
72	95	91	86	82	77	73	69	65	61	57
74	95	91	86	82	78	74	70	66	62	58
76	95	91	87	82	78	74	70	66	63	59
78	96	91	87	83	79	75	71	67	63	60
80	96	92	87	83	79	75	72	68	64	61
82	96	92	88	84	80	76	72	69	65	62
84	96	92	88	84	80	77	73	69	66	63
86	96	92	88	84	81	77	73	70	67	63
88	96	92	88	85	81	77	74	71	67	64
90	96	92	88	85	81	78	74	71	68	65

The table may be readily understood. For example, if the temperature of the air (dry bulb) be 60°, and the temperature of evaporation (wet bulb) be 56°, the difference being 4°, look in the column headed "Temperature of the air" for 60°, and for the figures on the same line in column headed 4°; here 78 will be found, which means that the air is 78 per cent saturated with water vapor; that is, that the amount of water vapor present in the atmosphere is 78 per cent of the total amount that it could carry at the given temperature (60°). This total amount, or saturation, is thus represented by 100, and if there occurred any increase of the quantity of vapor beyond this point, the excess would be precipitated in the form of liquid. Over the ocean's surface the relative humidity is generally about 90 per cent, or even higher in the doldrums; over the land in dry winter weather it may fall as low as 40 per cent.

63. The sea water of which the temperature is to be taken should be drawn from a depth of 3 feet below the surface, the bucket used being weighted in order to sink it. The bulb of the thermometer should remain immersed in the water at least three minutes before reading, and the reading should be made with the bulb immersed.

THE LOG BOOK.

64. The *Log Book* is a record of the ship's cruise, and, as such, an important accessory in the navigation. It should afford all the data from which the position of the ship is established by the method of dead reckoning; it should also comprise a record of meteorological observations, which should be made not only for the purpose of foretelling the weather during the voyage, but also for contribution to the general fund of knowledge of marine meteorology.

65. A convenient form for recording the data, which is employed for the log books of United States naval vessels, is shown on page 26; beside the tabulated matter thus arranged, to which one page of the book is devoted, a narrative of the miscellaneous events of the day, written and signed by the proper officers, appears upon the opposite page.

Hour.	Speed.		Reading of patent log.	Course steered by standard compass.	Wind.		Heel.	Lee-way.	Barometer.		Temperature.			State of weather by symbols.	Clouds.			State of sea by symbols.
	Knots.	Tenths.			Direction by standard compass.	Force.			Height in inches.	Thermometer attd.	Air, dry bulb.	Air, wet bulb.	Water at surface.		Form by symbols.	Moving from.	Amount, scale 0 to 10.	
A. M.																		
1																		
2																		
3																		
4																		
5																		
6																		
Etc.																		

° ′ ″

Position at 8.00 a. m. {Lat. by ....
{Long. by ....

Position at noon .... {Lat. by Obs ....
{Long. by Obs ....
{Lat. by D. R ....
{Long. by D. R ....

Course made good since preceding noon .... true.
Distance made good since preceding noon .... knots.
Distance by log since preceding noon .... knots.
Current per hour ...... knots; setting .... true.

° ′ ″

Position at 8.00 p. m. {Lat. by ....
{Long. by ....

Variation of compass ....
Error of compass observed at ....
Deviation of compass on ....
Water expended during preceding 24 hrs .... gals.
Water .... during preceding 24 hrs .... gals.
Water remaining on hand fit for use at noon .... gals.
Coal consumed during preceding 24 hrs .... tons.
Coal remaining on hand at noon .... tons.

66. For the most part, the nature of the information called for, with the method of recording it, will be apparent. A brief explanation is here given of such points as seem to require it.

67. The Wind.—In recording the force of the wind the scale devised by the late Admiral Sir F. Beaufort is employed. According to this scale the wind varies from 0, a calm, to 12, a hurricane, the greatest velocity it ever attains. In the lower grades of the scale the force of the wind is estimated from the speed imparted to a man-of-war of the early part of the nineteenth century sailing full and by; in the higher grades, from the amount of sail which the same vessel could carry when closehauled. The scale, with the estimated velocity of the wind in both statute and nautical miles per hour, is as follows:

Force of wind.	Conditions.	Velocity.		Mean pressure in pounds per square foot.
		Statute miles per hour.	Nautical miles per hour.	
0.—Calm	Full-rigged ship, all sails set, no headway.	0 to 3	0 to 2.6	0.03
1.—Light air	Just sufficient to give steerage way	8	6.9	0.23
2.—Light breeze	Speed of 1 or 2 knots, "full and by"	13	11.3	0.62
3.—Gentle breeze	Speed of 3 or 4 knots, "full and by"	18	15.6	1.2
4.—Moderate breeze	Speed of 5 or 6 knots, "full and by"	23	20.0	1.9
5.—Fresh breeze	All plain sail, "full and by"	28	24.3	2.9
6.—Strong breeze	Topgallantsails over single-reefed topsails	34	29.5	4.2
7.—Moderate gale	Double-reefed topsails	40	34.7	5.9
8.—Fresh gale	Treble-reefed topsails (or reefed upper-topsails and courses).	48	41.6	8.4
9.—Strong gale	Close-reefed topsails and courses (or lower topsails and courses).	56	48.6	11.5
10.—Whole gale	Close-reefed main topsail and reefed foresail (or lower main topsail and reefed foresail).	65	56.4	15.5
11.—Storm	Storm staysails	75	65.1	20.6
12.—Hurricane	Under bare poles	90 and over.	78.1 and over.	29.6

68. When steaming or sailing with any considerable speed, the apparent direction and force of the wind, as determined from a vane, flag, or pennant aboard ship, may differ materially from the true direction and force, the reason being that the air appears to come from a direction and with a force dependent, not only upon the wind itself, but also upon the motion of the vessel. For instance, suppose that the wind has a velocity of 20 knots an hour (force 4), and take the case of two vessels, each steaming 20 knots, the first with the wind dead aft, the second with the wind dead ahead. The former vessel will be moving with the same velocity as the air and in the same direction; the velocity of the wind relatively to the ship will thus be zero; on the vessel an apparent calm will prevail and the pennant will hang up and down. The latter vessel will be moving with the same velocity as the air, but in the opposite direction; the relative velocity of the two will thus be the sum of the two velocities, or 40 knots an hour, and on the second vessel the wind will apparently have the velocity corresponding very nearly with a fresh gale. Again, it might be shown that in the case of a vessel steaming west at the rate of 20 knots, with the wind blowing from north with the velocity of 20 knots an hour, the velocity with which the air strikes the ship as a result of the combined motion will be 28 knots an hour, and the direction from which it comes will be NW. If, therefore, the effect of the the speed of the ship is neglected the wind will be recorded as NW., force 6, when in reality it is north, force 4.

In order to make a proper allowance for this error and arrive at the true direction and force of the wind, Table 32 may be entered with the ship's speed and the apparent direction and force of the wind as arguments, and the true direction and force will be found.

69. Weather.—To designate the weather a series of symbols devised by the late Admiral Beaufort is employed. The system is as follows:

b.—Clear blue sky.
c.—Clouds.
d.—Drizzling, or light rain.
f.—Fog, or foggy weather.
g.—Gloomy, or dark, stormy-looking weather.
h.—Hail.
l.—Lightning.
m.—Misty weather.
o.—Overcast.
p.—Passing showers of rain.
q.—Squally weather.
r.—Rainy weather, or continuous rain.
s.—Snow, or snowy weather.
t.—Thunder.
u.—Ugly appearances, or threatening weather.
v.—Visibility of distant objects.
w.—Wet, or heavy dew.
z.—Hazy.

To indicate great intensity of any feature, its symbol may be underlined; thus: $\underline{r}$., heavy rain.

70. Clouds.—The following are the principal forms of clouds, named in the order of the altitude above the earth at which they usually occur, beginning with the most elevated. The symbols by which each is designated follows its name:

1. Cirrus, (*Ci.*).—Detached clouds, delicate and fibrous looking, taking the form of feathers, generally of a white color, sometimes arranged in belts which cross a portion of the sky in great circles, and, by an effect of perspective, converging toward one or two opposite points of the horizon.

2. Cirro-Stratus, (*Ci.-S.*).—A thin, whitish sheet, sometimes completely covering the sky and only giving it a whitish appearance, or at others presenting, more or less distinctly, a formation like a tangled web. This sheet often produces halos around the sun and moon.

3. Cirro-Cumulus, (*Ci.-Cu.*).—Small globular masses or white flakes, having no shadows, or only very slight shadows, arranged in groups and often in lines.

4. Alto-Cumulus, (*A.-Cu.*).—Rather large globular masses, white or grayish, partially shaded, arranged in groups or lines, and often so closely packed that their edges appear confused. The detached masses are generally larger and more compact at the center of the group; at the margin they form into finer flakes. They often spread themselves out in lines in one or two directions.

5. Alto-Stratus, (*A.-S.*).—A thick sheet of a gray or bluish color, showing a brilliant patch in the neighborhood of the sun or moon, and which, without causing halos, may give rise to coronæ. This form goes through all the changes like the Cirro-Stratus, but its altitude is only half so great.

6. Strato-Cumulus, (*S.-Cu.*).—Large globular masses or rolls of dark cloud, frequently covering the whole sky, especially in winter, and occasionally giving it a wavy appearance. The layer of Strato-Cumulus is not, as a rule, very thick, and patches of blue sky are often visible through the intervening spaces. All sorts of transitions between this form and the Alto-Cumulus are noticeable. It may be distinguished from Nimbus by its globular or rolled appearance and also because it does not bring rain.

7. Nimbus, (*N.*).—Rain clouds; a thick layer of dark clouds, without shape and with ragged edges, from which continued rain or snow generally falls. Through the openings of these clouds an upper layer of Cirro-Stratus or Alto-Stratus may almost invariably be seen. If the layer of Nimbus separates into shreds or if small loose clouds are visible floating at a low level underneath a large nimbus, they may be described as Fracto-Nimbus (Fr.-N.), the "scud" of sailors.

8. Cumulus, (*Cu.*).—Wool-pack clouds; thick clouds of which the upper surface is dome-shaped and exhibits protuberances, while the base is horizontal. When these clouds are opposite the sun the surfaces usually presented to the observer have a greater brilliance than the margins of the protuberances. When the light falls aslant, they give deep shadows; when, on the contrary, the clouds are on the same side as the sun, they appear dark, with bright edges. The true Cumulus has clear superior and inferior limits. It is often broken up by strong winds, and the detached portions undergo continual changes. These may be distinguished by the name of Fracto-Cumulus (*Fr.-Cu.*).

9. Cumulo-Nimbus, (*Cu.-N.*).—The thunder-cloud or shower-cloud; heavy masses of clouds rising in the form of mountains, turrets, or anvils, generally having a sheet or screen of fibrous appearance above, and a mass of clouds similar to Nimbus underneath. From the base there usually fall local showers of rain or of snow (occasionally hail or soft hail).

10. Stratus, (*S.*).—A horizontal sheet of lifted fog; when this sheet is broken up into irregular shreds by the wind or by the summits of mountains, it may be distinguished by the name of Fracto-Stratus (*Fr.-S.*).

71. In the scale for the amount of clouds 0 represents a sky which is cloudless and 10 a sky which is completely overcast.

72. State of Sea.—The state of the sea is expressed by the following system of symbols:

B.—Broken or irregular sea.
C.—Chopping, short, or cross sea.
G.—Ground swell.
H.—Heavy sea.
L.—Long rolling sea.
M.—Moderate sea or swell.
R.—Rough sea.
S.—Smooth sea.
T.—Tide-rips.

CHAPTER III

THE COMPASS ERROR.

CAUSES OF THE ERROR.

73. When two magnets are near enough together to exert a mutual influence, their properties are such as to cause those poles which possess similar magnetism to repel, and those which possess magnetism of opposite sorts to attract one another.

The earth is an immense natural magnet, having in each hemisphere a pole lying in the neighborhood of the geographical pole, though not exactly coincident therewith; consequently, when a magnet, such as that of a compass, is allowed to revolve freely in a horizontal plane, it will so place itself as to be parallel to the lines of magnetic force in that plane created by the earth's magnetic poles, the end which we name north pointing to the north, and the south end in the opposite direction. The north end of the compass—north-seeking, as it is sometimes designated for clearness—will be that end which has opposite polarity to the earth's north magnetic pole, this latter possessing the same sort of magnetism as the so-called south pole of the compass.

74. By reason of the fact that the magnetic pole differs in position from the geographical pole, the compass needle will not indicate true directions, but each compass point will differ from the corresponding true point by an amount dependent upon the angle between the geographical and the magnetic pole at the position of the observer. The amount of this difference, expressed in angular measure, is the *Variation of the Compass* (sometimes called also the *Declination*, though this term is seldom employed by navigators).

The variation not only changes as one travels from point to point on the earth, being different in different localities, but, as it has been found that the earth's magnetic poles are in constant motion, it undergoes certain changes from year to year. In taking account of the error it produces, the navigator must therefore be sure that the variation used is correct not only for the *place*, but also for the *time* under consideration. The variation is subject to a small diurnal fluctuation, but this is not a material consideration with the mariner.

75. Besides the error thus produced in the indications of the compass, a further one, due to *Local Attraction*, may arise from extraneous influences due to natural magnetic attraction in the vicinity of the vessel. Instances of this are quite common when a ship is in port, as she may be in close proximity to vessels, docks, machinery, or other masses of iron or steel. It is also encountered at sea in localities where the mineral substances in the earth itself possess magnetic qualities—as, for example, at certain places in Lake Superior and at others off the coast of Australia. When due to the last-named cause, it may be a source of great danger to the mariner, but, fortunately, the number of localities subject to local attraction is limited. The amount of this error can seldom, if ever, be determined; if known, it might properly be included with the variation and treated as a part thereof.

76. In addition to the variation, the compass ordinarily has a still further error in its indications, which arises from the effect exerted upon it by masses of magnetic metal within the ship itself. This is known as the *Deviation of the Compass*. For reasons that will be explained later, it differs in amount for each heading of the ship, and, further, the character of the deviations undergo modification as a vessel proceeds from one geographical locality to another.

APPLYING THE COMPASS ERROR.

77. From what has been explained, it may be seen that there are three methods by which bearings or courses may be expressed: (*a*) *true*, when they refer to the angular distance from the earth's geographical meridian; (*b*) *magnetic*, when they refer to the angular distance from the earth's magnetic meridian, and must be corrected for variation to be converted into true; and (*c*) *by compass*, when they refer to the angular distance from the north indicated by the compass on a given heading of the ship, and must be corrected for the deviation on that heading for conversion to magnetic, and for both deviation and variation for conversion to true bearings or courses. The process of applying the errors under all circumstances is one of which the navigator must make himself a thorough master; the various problems of conversion are constantly arising; no course can be set nor bearing plotted without involving the application of this problem, and a mistake in its solution may produce serious consequences. The student is therefore urged to give it his most careful attention.

78. When the effect of a compass error, whether arising from variation or from deviation, is to draw the north end of the compass needle to the right, or eastward, the error is named *east*, or is marked +; when its effect is to draw the north end of the needle to the left or westward, it is named *west*, or marked −.

Figures 7 and 8 represent, respectively, examples of easterly and westerly errors. In both cases consider that the circles represent the observer's horizon, N and S being the correct north and south points in each case. If N′ and S′ represent the corresponding points indicated by a compass whose needle is deflected by a compass error, then in the first case, the north end of the needle being drawn to the right or east, the error will be easterly or positive, and in the second case, the north end of the needle being drawn to the left or west, the compass error will be westerly or negative.

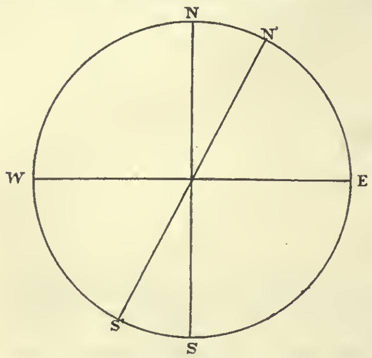

Fig. 7.

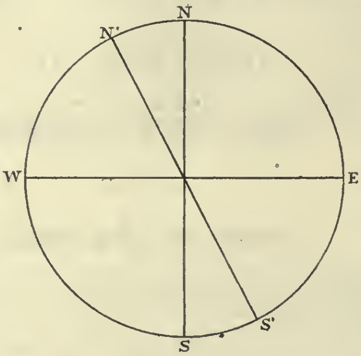

Fig. 8.

Considering figure 7, if we assume the easterly error to amount to one point, it will be seen that if a direction of N. by W. is indicated by the compass, the correct direction should be north, or one point farther to the right. If the compass indicates north, the correct bearing is N. by E.; that is, still one point to the right. If we follow around the whole card, the same relation will be found in every case, the corrected bearing being always one point to the right of the compass bearing. Conversely, if we regard figure 8, assuming the same amount of westerly error, a compass bearing of N. by E. is the equivalent of a correct bearing of north, which is one point to the left; and this rule is general throughout the circle, the corrected direction being always to the left of that shown by the compass.

79. Having once satisfied himself that the general rule holds, the navigator may save the necessity of reasoning out in each case the direction in which the error must be applied, and need only charge his mind with some single formula which will cover all cases. Such a one is the following:

When the CORRECT *direction is to the* RIGHT, *the error is* EAST.

The words *correct-right-east*, in such a case, would be the key to all of his solutions. If he had a compass course to change to a corrected one with easterly deviation, he would know that to obtain the result the error must be applied to the right; if it were desired to change a correct course to the one indicated by compass, the error being westerly, the converse presents itself—the correct must be to the left—the uncorrected will therefore be to the right; if a correct bearing is to be compared with a compass bearing to find the compass error, when the correct is to the right the error is east, or the reverse.

80. It must be remembered that the word *east* is equivalent to *right* in dealing with the compass error, and *west* to *left*, even though they involve an apparent departure from the usual rules. If a vessel steers NE. by compass with one point easterly error, her corrected course is NE. by E.; but if she steers SE., the corrected course is not SE. by E., but SE. by S. Another caution may be necessary to avoid confusion; the navigator should always regard himself as facing the point under consideration when he applies an error; one point westerly error on South will bring a corrected direction to S. by E.; but if we applied one point to the left of South while looking at the compass card in the usual way—north end up—S. by W. would be the point arrived at, and a mistake of two points would be the result.

81. In the foregoing explanation reference has been made to "correct" directions and "compass errors" without specifying "magnetic" and "true" or "variation" and "deviation." This has been done in order to make the statements apply to all cases and to enable the student to grasp the subject in its general bearing without confusion of details.

Actually, as has already been pointed out, directions given may be true, magnetic, or by compass. By applying variation to a magnetic bearing we correct it and make it true, by applying deviation to a compass bearing we correct it to magnetic, and by applying to it the combined deviation and variation we correct it to true. Whichever of these operations is undertaken, and whichever of the errors is considered, the process of correction remains the same; the correct direction is always to the right, when the error is east, by the amount of that error.

Careful study of the following examples will aid in making the subject clear:

EXAMPLES: A bearing taken by a compass free from deviation is N. 76° E.; variation, 5° W.; required the true bearing. N. 71° E.

A bearing taken by a similar compass is NW. by W. ½ W.; variation, ¼ pt. W.; required the true bearing. NW. by W. ¾ W.

A vessel steers S. 27° E. by compass; deviation on that heading, 3° W.; variation in the locality, 12° E.; required the true course. S. 18° E.

A vessel steers S. by W. ½ W.; deviation, ¼ pt. W.; variation, 1 pt. E.; required the true course. SSW. ¼ W.

It is desired to steer the magnetic course N. 38° W.; deviation, 4° E.; required the course by compass. N. 42° W.

The true course between two points is found to be W. ⅞ N.; variation 1¼ pt. E.; no deviation; required the compass course. W. ⅜ S.

True course to be made, N. 55° E.; deviation, 7° E.; variation, 14° W.; required the course by compass. N. 62° E.

A vessel passing a range whose direction is known to be S. 20° W., magnetic, observes the bearing by compass to be S. 2° E.; required the deviation. 22° E.

The sun's observed bearing by compass is S. 89° E.; it is found by calculation to be N. 84° E. (true); variation, 8° W.; required the deviation. 1° E.

FINDING THE COMPASS ERROR.

82. The variation of the compass for any given locality is found from the charts. A nautical chart always contains information from which the navigator is enabled to ascertain the variation for any place within the region embraced and for any year. Beside the information thus to be acquired from local charts, special charts are published showing the variation at all points on the earth's surface.

83. The deviation of the compass, varying as it does for every ship, for every heading, and for every geographical locality, must be determined by the navigator, for which purpose various methods are available.

Whatever method is used, the ship must be swung in azimuth and an observation made on each of the headings upon which the deviation is required to be known. If a new iron or steel ship is being swung for the first time, observations should be made on each of the thirty-two points. At later swings, especially after correctors have been applied, or in the case of wooden ships, sixteen points will suffice—or, indeed, only eight. In case it is not practicable to make observations on exact compass points, they should be made as near thereto as practicable and platted on the Napier diagram (to be explained hereafter), whence the deviations on exact points may be found.

84. In swinging ship for deviations the vessel should be on an even keel and all movable masses of iron in the vicinity of the compass secured as for sea. The vessel, upon being placed on any heading, should be steadied there for three to four minutes before the observation is made in order that the compass card may come to rest and the magnetic conditions assume a settled state. To assure the greatest accuracy the ship should first be swung to starboard, then to port, and the mean of the two deviations on each course taken. Ships may be swung under their own steam, or with the assistance of a tug, or at anchor, where the action of the tide tends to turn them in azimuth (though in this case it is difficult to get them steadied for the requisite time on each heading), or at anchor, by means of springs and hawsers.

85. The deviation of all compasses on the ship may be obtained from the same swing, it being required to make observations with the standard only. To accomplish this it is necessary to record the ship's head by all compasses at the time of steadying on each even point of the standard; applying the deviation, as ascertained, to the heading by standard, gives the magnetic heads, with which the direction of the ship's head by each other compass may be compared, and the deviation thus obtained. Then a complete table of deviations may be constructed as explained in article 94.

86. There are four methods for ascertaining the deviations from swinging; namely, by *reciprocal bearings*, by *bearings of the sun*, by *ranges*, and by a *distant object*.

87. Reciprocal Bearings.—One observer is stationed on shore with a spare compass placed in a position free from disturbing magnetic influences; a second observer is at the standard compass on board ship. At the instant when ready for observation a signal is made, and each notes the bearing of the other. The bearing by the shore compass, reversed, is the magnetic bearing of the shore station from the ship, and the difference between this and the bearing by the ship's standard compass represents the deviation of the latter.

In determining the deviations of compasses placed on the fore-and-aft amidship line, when the distribution of magnetic metal to starboard and port is symmetrical, the shore compass may be replaced by a dumb compass, or pelorus, or by a theodolite in which, for convenience, the zero of the horizontal graduated circle may be termed north; the reading of the shore instrument will, of course, not represent magnetic directions, but by assuming that they do we obtain a series of fictitious deviations, the mean value of which is the error common to all. Upon deducting this error from each of the fictitious deviations, we obtain the correct values.

If ship and shore observers are provided with watches which have been compared with one another, the times may be noted at each observation, and thus afford a means of locating errors due to misunderstanding of signals.

88. Bearings of the Sun.—In this method it is required that on each heading a bearing of the sun be observed by compass and the time noted at the same moment by a chronometer or watch. By means which will be explained in Chapter XIV, the true bearing of the sun may be ascertained from the known data, and this, compared with the compass bearing, gives the total compass error; deducting from the compass error the variation, there remains the deviation. The variation used may be that given by the chart, or, in the case of a compass affected only by symmetrically placed iron or steel, may be considered equal to the mean of all the total errors. Other celestial bodies may be observed for this purpose in the same manner as the sun.

This method is important as being the only one available for determining the compass error at sea.

89. Ranges.—In many localities there are to be found natural or artificial range marks which are clearly distinguishable, and which when in line lie on a known magnetic bearing. By steaming about on different headings and noting the compass bearing of the ranges each time of crossing the line that they mark, a series of deviations may be obtained, the deviation of each heading being equal to the difference between the compass and the magnetic bearing.

90. Distant Object.—A conspicuous object is selected which must be at a considerable distance from the ship and upon which there should be some clearly defined point for taking bearings. The direction of this object by compass is observed on successive headings. Its true or magnetic bearing is then found and compared with the compass bearings, whence the deviation is obtained.

The true or the magnetic bearing may be taken from the chart. The magnetic bearing may also be found by setting up a compass ashore, free from foreign magnetic disturbance, in range with the object and the ship, and observing the bearing of the object; or the magnetic bearing may be assumed to be the mean of the compass bearings.

In choosing an object for use in this method care must be taken that it is at such a distance that its bearing from the ship does not practically differ as the vessel swings in azimuth. If the ship is swung at anchor, the distance should be not less than 6 miles. If swung under way, the object must be so far that the parallax (the tangent of which may be considered equal to half the diameter of swinging divided by the distance) shall not exceed about 30′.

91. In all of the methods described it will be found convenient to arrange the results in tabular form. In one column record the ship's head by standard compass, and abreast it in successive columns the observations from which the deviation is determined on that heading, and finally write the deviation itself. When the result of the swing has been worked up another table is constructed showing simply the headings and the corresponding deviations. This is known as the *Deviation Table* of the compass. If compensation is to be attempted, this table is the basis of the operation; if not, the deviation tables of the standard and steering compass should be posted in such place as to be accessible to all persons concerned with the navigation of the ship.

92. Let it be assumed that a deviation table has been found and that the values are as follows:

Deviation table.

Ship's head by standard compass.	Deviation.	Ship's head by standard compass.	Deviation.	Ship's head by standard compass.	Deviation.	Ship's head by standard compass.	Deviation.
	° ′		° ′		° ′		° ′
North	− 1 00	East	−19 55	South	0 00	West	+19 30
N. by E	− 1 50	E. by S	−22 00	S. by W	+10 20	W. by N	+17 00
NNE	− 3 00	ESE	−23 30	SSW	+17 00	WNW	+13 00
NE. by N	− 5 15	SE. by E	−24 00	SW. by S	+21 50	NW. by W	+11 10
NE	− 7 10	SE	−23 30	SW	+24 30	NW	+ 7 40
NE. by E	−10 15	SE. by S	−20 30	SW. by W	+26 20	NW. by N	+ 5 05
ENE	−13 05	SSE	−16 00	WSW	+25 00	NNW	+ 3 00
E. by N	−17 10	S. by E	− 8 50	W. by S	+23 30	N. by W	+ 1 00

We have from the table the amount of deviation on each compass heading; therefore, knowing the ship's head by compass, it is easy to pick out the corresponding deviation and thus to obtain the magnetic heading. But if we are given the magnetic direction in which it is desired to steer and have to find the corresponding compass course, the problem is not so simple, for we are not given deviations on magnetic heads, and where the errors are large it may not be assumed that they are the same as on the corresponding compass headings. For example, with the deviation table just given, suppose it is required to determine the compass heading corresponding to N. 79° W., magnetic.

The deviation corresponding to N. 79° W., per compass, is + 17° 00′. If we apply this to N. 79° W., magnetic, we have S. 84° W. as the compass course. But, consulting the table, it may be seen that the deviation corresponding to S. 84° W., per compass, is + 21½°, and therefore if we steer that course the magnetic direction will be N. 74½° W., and not N. 79° W., as desired.

A way of arriving at the correct result is to make a series of trials until a course is arrived at which fulfills the conditions. Thus, in the example given:

First trial.

Mag. course required	N. 79° W.
Try dev. on N. 79° W., p. c	17° E.
Trial comp. course	S. 84° W.
Dev. on S. 84° W., p. c	21½° E.
Mag. course made good	N. 74½° W.

Since this assumption carries the course 4½° too far to the right, assume next a deviation on a course 5° farther to the left than the one used here.

Second trial.

Mag. course required	N. 79° W.
Try dev. on S. 79° W., p. c	23½° E.
Trial comp. course	S. 77½° W.
Dev. on S. 77½° W., p. c	24° E.
Mag. course made good	N. 78½° W.

This is as close to the required course as the ship can be steered. It may occur that further trials will be necessary in some cases.

93. The Napier Diagram.—A much more expeditious method for the solution of this problem is afforded by the *Napier Diagram*, and as that diagram also facilitates a number of other operations connected with compass work it should be clearly understood by the navigator. This device admits of a graphic representation of the table of deviations of the compass by means of a curve; besides furnishing a ready means of converting compass into magnetic courses and the reverse, one of its chief merits is that if the deviation has been determined on a certain number of headings it enables one to obtain the most probable value of the deviation on any other course that the ship may head. The last-named feature renders it useful in making a table of deviations of compasses other than the standard when their errors are found as described in article 85.

94. The Napier diagram (fig. 9) represents the margin of a compass card cut at the north point and straightened into a vertical line; for convenience, it is usually divided into two sections, representing, respectively, the eastern and western semicircles. The vertical line is of a convenient length and divided into thirty-two equal parts corresponding to the points of the compass, beginning at the top with North and continuing around to the right; it is also divided into 360 degrees, which are appropriately marked.

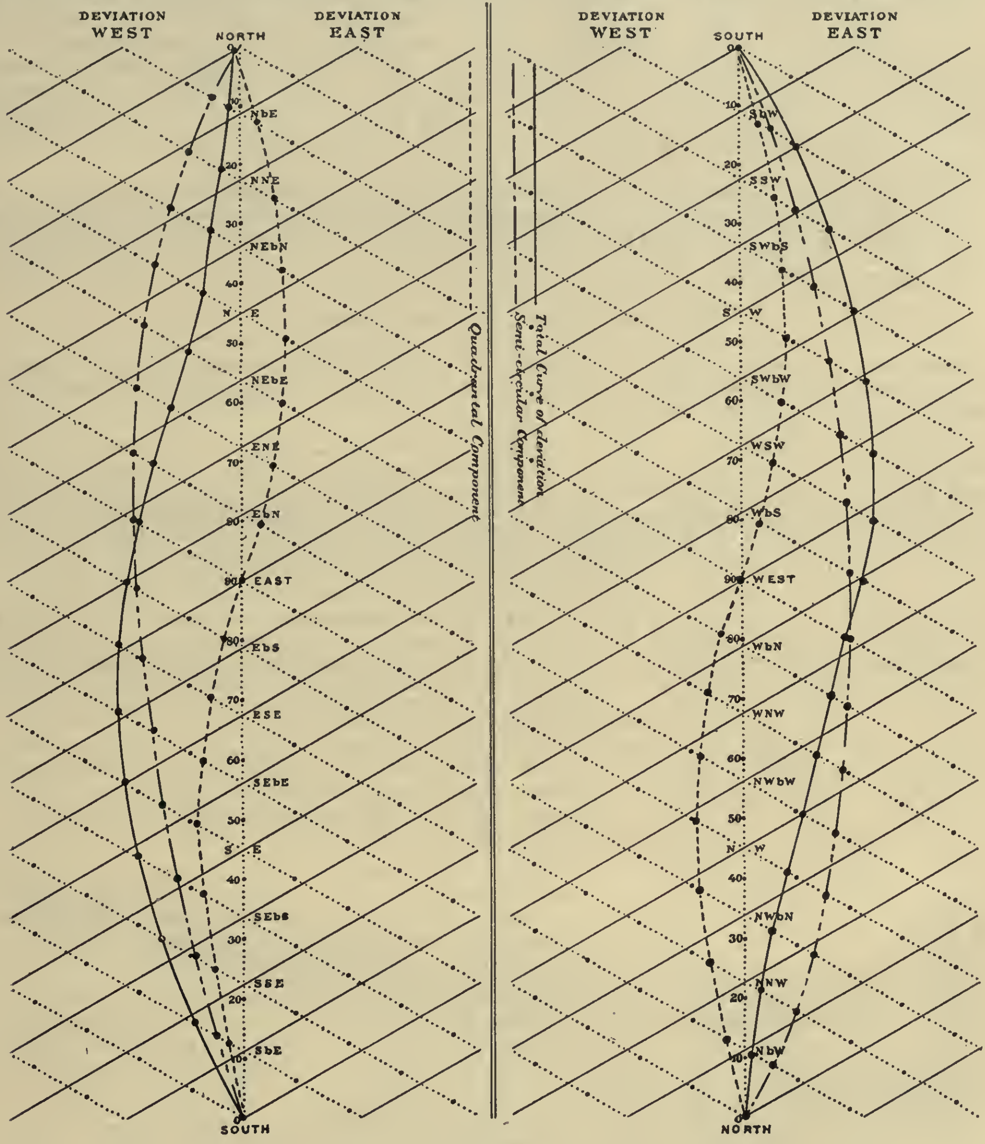

FIG. 9.

The vertical line is intersected at each compass point by two lines inclined to it at an angle of 60°, that line which is inclined upward to the right being drawn plain and the other dotted.

To plot a curve on the Napier diagram, if the deviation has been observed with the ship's head on given *compass* courses (as is usually the case with the standard compass), measure off on the vertical scale the number of degrees corresponding to the deviation and lay it down—to the right if easterly and to the left if westerly—on the *dotted* line passing through the point representing the ship's head; or, if the observation was not made on an even point, then lay it down on a line drawn parallel to the dotted ones through that division of the vertical line which represents the compass heading; if the deviation has been observed with the ship on given *magnetic* courses (as when deviations by steering compass are obtained by noting the ship's head during a swing on even points of the standard), proceed in the same way, excepting that the deviation must be laid down on a *plain* line or a line parallel thereto. Mark each point thus obtained with a dot or small circle, and draw a free curve passing, as nearly as possible, through all the points.

To obtain a complete curve, a sufficient number of observations should be taken while the ship swings through an entire circle. Generally, observations on every alternate point are enough to establish a good curve, but in cases where the maximum deviation reaches 40° it is preferable to observe on every point.

The curve shown in the full line on figure 9 corresponds to the table of deviations given in article 92.

From a given compass course to find the corresponding magnetic course, through the point of the vertical line representing the given compass course, draw a line parallel to the *dotted* lines until the curve is intersected, and from the point of intersection draw another line parallel to the plain lines; the point on the scale where this last line cuts the vertical line is the magnetic course sought. The correctness of this solution will be apparent when we consider that the 60° triangles are equilateral, and therefore the distance measured along the vertical side will equal the distance measured along the inclined sides—that is, the deviation; and the direction will be correct, for the construction is such that magnetic directions will be to the right of compass directions when the deviation is easterly and to the left if westerly.

From a given magnetic course to find the corresponding compass course, the process is the same, excepting that the first line drawn should follow, or be parallel to, the *plain* lines, and the second, or return line, should be parallel to the dotted; and a proof similar to that previously employed will show the correctness of the result. As an example, the problem given in article 92 may be solved by the diagram, and the result will be found to accord with the solution previously given.

THE THEORY OF DEVIATION.[a]

95. Features of the Earth's Magnetism.—It has already been stated that the earth is an immense natural magnet, with a pole in each hemisphere which is not coincident with the geographical pole; it has also a magnetic equator which lies close to, but not coincident with, the geographical equator.

A magnetic needle freely suspended at a point on the earth's surface, and undisturbed by any other than the earth's magnetic influence, will lie in the plane of the magnetic meridian and at an angle with the horizon depending upon the geographical position.

The magnetic elements of the earth which must be considered are shown in figure 10. The earth's *total force* is represented in direction and intensity by the line AB. Since compass needles are mechanically arranged to move only in a horizontal plane, it becomes necessary, when investigating the effect of the earth's magnetism upon them, to resolve the total force into two components which in the figure are represented by AC and AD. These are known, respectively, as the *horizontal* and *vertical components* of the earth's total force, and are usually designated as H and Z. The angle CAB, which the line of direction makes with the plane of the horizon, is called the *magnetic inclination* or *dip*, and denoted by θ.

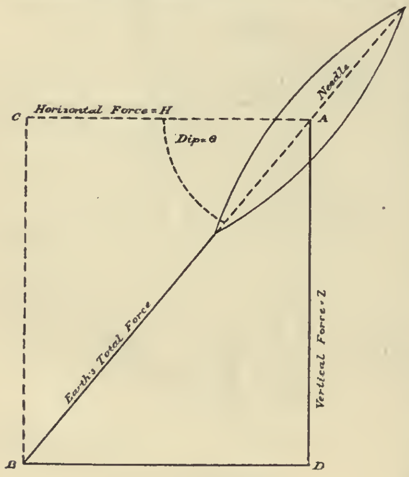

Fig. 10.

It is clear that the horizontal component will reduce to zero at the magnetic poles, where the needle points directly downward, and that it will reach a maximum at the magnetic equator, where the free needle hangs in a horizontal direction. The reverse is true of the vertical component and of the angle of dip.

Values representing these different terms may be found from special charts.

96. Induction; Hard and Soft Iron.—When a piece of unmagnetized iron or steel is brought within the influence of a magnet, certain magnetic properties are immediately imparted to the former, which itself becomes magnetic and continues to remain so as long as it is within the sphere of influence of the permanent magnet; the magnetism that it acquires under these circumstances is said to be *induced*, and the properties of *induction* are such that that end or region which is nearest the pole of the influencing magnet will take up a polarity opposite thereto. If the magnet is withdrawn, the induced magnetism is soon dissipated. If the magnet is brought into proximity again, but with its opposite pole nearer, magnetism will again be induced, but this time its polarity will be reversed. A further property is that if a piece of iron or steel, while temporarily possessed of magnetic qualities through induction, be subjected to blows, twisting, or mechanical violence of any sort, the magnetism is thus made to acquire a permanent nature.

The softer the metal, from a physical point of view, the more quickly and thoroughly will induced magnetism be dissipated when the source of influence is withdrawn; hard metal, on the contrary, is slow to lose the effect of magnetism imparted to it in any way. Hence, in regarding the different features which affect deviation, it is usual to denominate as hard iron that which possesses retained magnetism of a stable nature, and as soft iron that which rapidly acquires and parts with its magnetic qualities under the varying influences to which it is subjected.

97. Magnetic Properties Acquired by an Iron or Steel Vessel in Building.—The inductive action of the earth's magnetism affects all iron or steel within its influence, and the amount and permanency of the magnetism so induced depends upon the position of the metal with reference to the earth's total force, upon its character, and upon the degree of hammering, bending, and twisting that it undergoes.

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[a] As it is probable that the student will not have practical need of a knowledge of the theory of deviation and the compensation of the compass until after he has mastered all other subjects pertaining to Navigation and Nautical Astronomy, it may be considered preferable to omit the remainder of this chapter at first and return to it later.

An iron bar held in the line of the earth's total force instantly becomes magnetic; if held at an angle thereto it would acquire magnetic properties dependent for their amount upon its inclination to the line of total force; when held at right angles to the line there would be no effect, as each extremity would be equally near the poles of the earth and all influence would be neutralized. If, while such a bar is in a magnetic state through inductive action, it should be hammered or twisted, a certain magnetism of a permanent character is impressed upon it, which is never entirely lost unless the bar is subjected to causes equal and opposite to those that produced the first effect.

A sheet of iron is affected by induction in a similar way, the magnetism induced by the earth diffusing itself over the entire plate and separating itself into regions of opposite polarity divided by a neutral area at right angles to the earth's line of total force. If the plate is hammered or bent, this magnetism takes up a permanent character.

If the magnetic mass has a third dimension, and assumes the form of a ship, a similar condition prevails. The whole takes up a magnetic character; there is a magnetic axis in the direction of the line of total force, with poles at its extremities and a zone of no magnetism perpendicular to it. The distribution of magnetism will depend upon the horizontal and vertical components of the earth's force in the locality and upon the direction of the keel in building; its permanency will depend upon the amount of mechanical violence to which the metal has been subjected by the riveting and other incidents of construction, and upon the nature of the metal employed.

98. Causes that Produce Deviation.—There are three influences that operate to produce deviation; namely, (*a*) *subpermanent magnetism;* (*b*) *transient magnetism induced in vertical soft iron,* and (*c*) *transient magnetism induced in horizontal soft iron.* Their effect will be explained.

Subpermanent magnetism is the name given to that magnetic force which originates in the ship while building, through the process explained in the preceding article; after the vessel is launched and has an opportunity to swing in azimuth, the magnetism thus induced will suffer material diminution until, after the lapse of a certain time, it will settle down to a condition that continues practically unchanged; the magnetism that remains is denominated subpermanent. The vessel will then approximate to a permanent magnet, in which the north polarity will lie in that region which was north in building, and the south polarity (that which exerts an attracting influence on the north pole of the compass needle), in the region which was south in building.

Transient magnetism induced in vertical soft iron is that developed in the soft iron of a vessel through the inductive action of the vertical component only of the earth's total force, and is transient in nature. Its value or force in any given mass varies with and depends upon the value of the vertical component at the place, and is proportional to the sine of the dip, being a maximum at the magnetic pole and zero at the magnetic equator.

Transient magnetism induced in horizontal soft iron is that developed in the soft iron of a vessel through the inductive action of the horizontal component only of the earth's total force, and is transient in nature. Its value or force in any given mass varies with and depends upon the value of the horizontal component at the place, and is proportional to the cosine of the dip, being a maximum at the magnetic equator and reducing to zero at the magnetic pole.

The needle of a compass in any position on board ship will therefore be acted upon by the earth's total force, together with the three forces just described. The poles of these forces do not usually lie in the horizontal plane of the compass needle, but as this needle is constrained to act in a horizontal plane, its movements will be affected solely by the horizontal components of these forces, and its direction will be determined by the resultant of those components.

The earth's force operates to retain the compass needle in the plane of the magnetic meridian, but the resultant of the three remaining forces, when without this plane, deflects the needle, and the amount of such deflection constitutes the deviation.

99. Classes of Deviation.—Investigation has developed the fact that the deviation produced as described is made up of three parts, which are known respectively as *semicircular*, *quadrantal*, and *constant* deviation, the latter being the least important. A clear understanding of the nature of each of these classes is essential for a comprehension of the methods of compensation.

100. *Semicircular Deviation* is that due to the combined influence, exerted in a horizontal plane, of the subpermanent magnetism of a ship and of the magnetism induced in soft iron by the vertical component of the earth's force. If we regard the effect of these two forces as concentrated in a single resultant pole exerting an attracting influence upon the north end of the compass needle, it may be seen that there will be some heading of the ship whereon that pole will lie due north of the needle and therefore produce no deviation; now consider that, from this position, the ship's head swings in azimuth to the right; throughout all of the semicircle first described an easterly deviation will be produced, and, after completing 180°, the pole will be in a position diametrically opposite to that from which it started, and will again exert no influence that tends to produce deviation. Continuing the swing, throughout the next semicircle the direction of the deviation produced will be always to the westward, until the circle is completed and the ship returns to her original neutral position. From the fact that this disturbing cause acts in the two semicircles with equal and opposite effect it is given the name of *semicircular* deviation.

In figure 9, a curve is depicted which shows the deviations of a semicircular nature separated from those due to other disturbing causes, and from this the reason for the name will be apparent.

101. Returning to the two distinct sources from which the semicircular deviation arises, it may be seen that the force due to subpermanent magnetism remains constant regardless of the geographical position of the vessel; but since the horizontal force of the earth, which tends to hold the needle in the magnetic meridian, varies with the magnetic latitude, the deviation due to subpermanent magnetism varies inversely as the horizontal force, or as $\frac{1}{H}$; this may be readily understood if it is considered that the stronger the tendency to cling to the direction of the magnetic meridian, the less will be the deflection due to a given disturbing force. On the other hand, that part of the semicircular force due to magnetism induced in vertical soft iron varies as the earth's vertical force, which is proportional to the

sine of the dip; its effect in producing deviation, as in the preceding case, varies inversely as the earth's horizontal force—that is, inversely as the cosine of the dip; hence the ratio representing the change of deviation arising from this cause on change of latitude is $\frac{\sin\theta}{\cos\theta}$, or $\tan\theta$.

If, then, we consider the change in the semicircular deviation due to a change of magnetic latitude, it will be necessary to separate the two factors of the deviation and to remember that the portion produced by subpermanent magnetism varies as $\frac{1}{H}$, and that due to vertical induction as $\tan\theta$. But for any consideration of the effect of this class of deviation in one latitude only, the two parts may be joined together and regarded as having a single resultant.

102. If we now resume our former assumption, that all the forces tending to produce semicircular deviation are concentrated in a single pole exerting an attracting influence upon the north pole of the compass, we may consider a line to be drawn joining that theoretical pole with the center of the compass, then the angle made by this line with the keel line of the vessel, measured from right ahead, around to the right is called the *starboard angle.* From this it follows that the disturbing force producing semicircular deviation may be considered to have the same effect as a single magnet whose center is in the vertical axis of the compass, and whose *south* pole (attracting to the north pole of the compass) is in the direction given by the starboard angle; if, therefore, a magnet be placed with its center in the vertical axis of the compass, its *north* (or repelling) pole in the direction of the starboard angle, and its distance so regulated that it exerts upon the compass a force equal to that of the ship's combined subpermanent magnetism and vertical induced magnetism, the disturbing effect of these two forces will be counterbalanced, and, so far as they are concerned, the compass deviations will be corrected, provided that the ship does not change her magnetic latitude.

103. It is evident that the force of the single magnet may be resolved into two components—one fore-and-aft, and one athwartship; in this case, instead of being represented by a single magnet with its south pole in the starboard angle, the semicircular forces will be represented by two magnets, one fore-and-aft and the other athwartship, and compensation may be made by two separate magnets lying respectively in the directions stated, but with their north or repelling poles in the position occupied by the south or attracting poles of the ship's force.

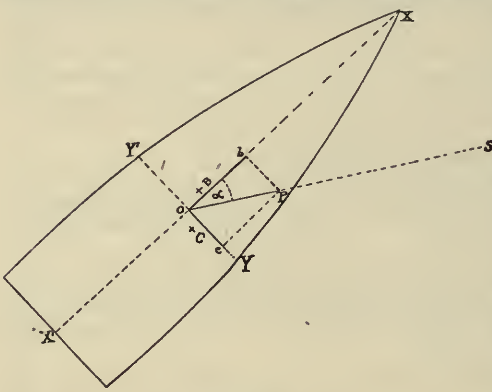

Fig. 11.

Figure 11 represents the conditions that have been described. If O be the center of the compass, XX′ and YY′, respectively, the fore-and-aft and athwartship lines of the ship, and OS the direction in which the attracting pole of the disturbing force is exerted, then XOS is the starboard angle, usually designated α. Now, if OP be laid off on the line OS, representing the amount of the disturbing force according to some convenient scale, then Ob and Oc, respectively, represent, on the same scale, the resolved directions of that force in the keel line and in the transverse line of the ship. Each of these resolved forces will exert a maximum effect when acting at right angles to the needle, the athwartship one when the ship heads north or south by compass, and the longitudinal one when the heading is east or west. On any other heading than those named the deviation produced by each force will be a fraction of its maximum whose magnitude will depend upon the azimuth of the ship's head. The maximum deviation produced, therefore, forms in each case a basis for reckoning all of the various effects of the disturbing force, and is called a *coefficient.*

The coefficient of semicircular deviation produced by the force in the fore-and-aft line is called B, and is reckoned as positive when it attracts a north pole toward the bow, negative when toward the stern; that produced by the athwartship force is C, and is reckoned as positive to starboard and negative to port. These coefficients are expressed in degrees.[a]

Referring again to figure 11, it will be seen that:

$$\tan\alpha = \frac{Oc}{Ob};$$

or (what may be shown to be the same thing):

$$\tan\alpha = \frac{\sin C}{\sin B};$$

and when the maximum deviations are small, this becomes:

$$\tan\alpha = \frac{C}{B}.$$

Since the starboard angle is always measured to the right, it will be seen that, for positive values of B and C, α will be between 0° and 90°; for a negative B and a positive C, between 90° and 180°; for

[a] It should be remarked that in a mathematical analysis of the deviations, it would be necessary to distinguish between the *approximate coefficients*, B and C, here described, as also A, D, and E, to be mentioned later, and the *exact coefficients* denoted by the corresponding capital letters of the German alphabet. In the practical discussion of the subject here given, the question of the difference need not be entered into.

negative values of both B and C, between 180° and 270°; and for a positive B and negative C, between 270° and 360°.

104. The coefficient B is approximately equal to the deviation on East; or to the deviation on West with reversed sign; or to the mean of these two. Thus in the ship having the table of deviations previously given (art. 92), B is equal to $-19^\circ 55'$, or to $-19^\circ 30'$, or to $\frac{1}{2}(-19^\circ 55' - 19^\circ 30') = -19^\circ 43'$.

The coefficient C is approximately equal to the deviation on North; or to the deviation on South with reversed sign; or to the mean of these two. In the example C is equal to $-1^\circ 00'$ or $0^\circ 00'$, or $\frac{1}{2}(-1^\circ 00' \pm 0^\circ 00') = -0^\circ 30'$.

105. The value of the subpermanent magnetism remaining practically constant under all conditions, it will not alter when the ship changes her latitude; but that due to induction in vertical soft iron undergoes a change when, by change of geographical position, the vertical component of the earth's force assumes a different value, and in such case the correction by means of one or a pair of permanent magnets will not remain effective. If, however, by series of observations in two magnetic latitudes, the values of the coefficients can be determined under the differing circumstances, it is possible, by solving equations, to determine what effect each force has in producing the semicircular deviation; having done which, the subpermanent magnetism can be corrected by permanent magnets after the method previously described, and the vertical induction in soft iron can be corrected by a piece of vertical soft iron placed in such a position near the compass as to produce an equal but opposite force to the ship's vertical soft iron. This last corrector is called a *Flinders bar*.

Having thus opposed to each of the component forces a corrector of magnetic character identical with its own, a change of latitude will make no difference in the effectiveness of the compensation, for in every case the modified conditions will produce identical results in the disturbing and in the correcting force.

106. *Quadrantal Deviation* is that which arises from horizontal induction in the soft iron of the vessel through the action of the horizontal component of the earth's total force. Let us consider, in figure 12, the effect of any piece of soft iron which is symmetrical with respect to the compass—that is, which lies wholly within a plane passing through the center of the needle in either a fore-and-aft or an athwartship direction. It may be seen (a) that such iron produces no deviation on the cardinal points (for on north and south headings the fore-and-aft iron, though strongly magnetized, has no tendency to draw the needle from a north-and-south line, while the athwartship iron, being at right angles to the meridian, receives no magnetic induction, and therefore exerts no force; and on east and west headings similar conditions prevail, the athwartship and the fore-and-aft iron having simply exchanged positions); and (b) the direction of the deviation produced is opposite in successive quadrants. The action of unsymmetrical soft iron is not quite so readily apparent, but investigation shows that part of its effect is to produce a deviation which becomes zero at the inter-cardinal points and is of opposite name in successive quadrants. From the fact that deviations of this class change sign every 90° throughout the circle, they gain the name of *quadrantal deviations*. One of the curves laid down in the Napier diagram (fig. 11) is that of quadrantal deviations, whence the nature of this disturbance of the needle may be observed.

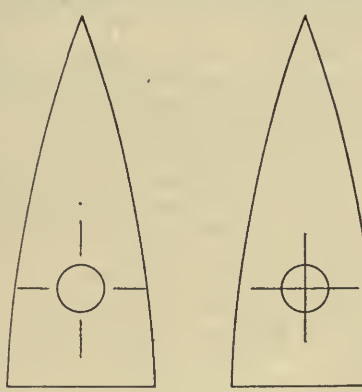

Fig. 12.

107. All deviations produced by soft iron may be considered as fractions of the maximum deviation due to that disturbing influence; and consequently the maximum is regarded as a coefficient, as in the case of semicircular deviations. The coefficient due to symmetrical soft iron is designated as D, and is considered positive when it produces easterly deviations in the quadrant between North and East; the coefficient of deviations arising from unsymmetrical soft iron is called E, and is reckoned as positive when it produces easterly deviations in the quadrant between NW. and NE.; this latter attains importance only when there is some marked inequality in the distribution of metal to starboard and to port, as in the case of a compass placed off the midship line.

108. D is approximately equal to the mean of the deviations on NE. and SW.; or to the mean of those on SE. and NW., with sign reversed; or to the mean of those means. In the table of deviations given in article 92, D is equal to $\frac{1}{2}(-7^\circ 10' + 24^\circ 30') = +8^\circ 40'$; or to $\frac{1}{2}(+23^\circ 30' - 7^\circ 40') = +7^\circ 55'$; or to $\frac{1}{2}(+8^\circ 40' + 7^\circ 55') = +8^\circ 23'$. By reason of the nature of the arrangement of iron in a ship, D is almost invariably positive.

E is approximately equal to the mean of the deviations on North and South; or to the mean of those on East and West with sign reversed; or to the mean of those means. In the example, E is equal to $\frac{1}{2}(-1^\circ 00' \pm 0^\circ 00') = -0^\circ 30'$; or to $\frac{1}{2}(+19^\circ 55' - 19^\circ 30') = +0^\circ 13'$; or to $\frac{1}{2}(-0^\circ 30' + 0^\circ 13') = -0^\circ 09'$.

109. Quadrantal deviation does not, like semicircular, undergo a change upon change of magnetic latitude; being due to induction in horizontal soft iron, the magnetic force exerted to produce it is proportional to the horizontal component of the earth's magnetism; but the directive force of the needle likewise depends upon that same component; consequently, as the disturbing force exerted upon the needle increases, so does the power that holds it in the magnetic meridian, with the result that on any given heading the deflection due to soft iron is always the same.

110. Quadrantal deviation is corrected by placing masses of soft iron (usually two hollow spheres in the athwartship line, at equal distances on each side of the compass), with the center of mass in the horizontal plane of the needle. The distance is made such that the force exerted exactly counteracts that of the ship's iron. As the correcting effect of this iron will, like the directive force and the quadrantal disturbing force, vary directly with the earth's horizontal component, the compensation once properly made will be effective in all latitudes.

In practice, the quadrantal deviation due to unsymmetrical iron is seldom corrected; the correction may be accomplished, however, by placing the soft iron masses on a line which makes an angle to the athwartship line through the center of the card.

111. *Constant Deviation* is due to induction in horizontal soft iron unsymmetrically placed about the compass. It has already been explained that one effect of such iron is to produce a quadrantal deviation, represented by the coefficient E; another effect is the *constant* deviation, so called because it is uniform in amount and direction on every heading of the ship. If plotted on a Napier diagram, it would appear as a straight line parallel with the initial line of the diagram.

112. Like other classes of deviation, the effect of the disturbing force is represented by a coefficient; this coefficient is designated as A, and is considered *plus* for easterly and *minus* for westerly errors. It is approximately equal to the mean of the deviations on any number of equidistant headings. In the case previously given, it might be found from the four headings, North, East, South, and West, and would then be equal to $\frac{1}{4}$ $(-1° 00'-19° 55'\pm0° 00'+19° 30')=-0° 21'$; or from all of the 32 headings, when it would equal $+0° 16'$.

For the same reason as in the case of E, the value of A is usually so small that it may be neglected; it only attains a material size when the compass is placed off the midship line, or for some similar cause.

113. Like quadrantal deviation, since its force varies with the earth's horizontal force, the constant deviation will remain uniform in amount in all latitudes.

No attempt is made to compensate this class of error.

114. Coefficients.—The chief value of coefficients is in mathematical analyses of the deviations and their causes. It may, however, be a convenience to the practical navigator to find their approximate values by the methods that have been given, in order that he may gain an idea of the various sources of the error, with a view to ameliorating the conditions, when necessary, by moving the binnacle or altering the surrounding iron. The following relation exists between the coefficients and the deviation:

$$d=A + B \sin z' + C \cos z' + D \sin 2z' + E \cos 2z',$$

where d is the deviation, and z' the ship's heading by compass, measured from compass North.

115. Mean Directive Force.—The effect of the disturbing forces is not confined to causing deviations; it is only those components acting at right angles to the needle which operate to produce deflection; the effect of those acting in the direction of the needle is exerted either in increasing or diminishing the directive force of the compass, according as the resolved component is northerly or southerly.

It occurs, with the usual arrangement of iron in a vessel, that the mean effect of this action throughout a complete swing of the ship upon all headings is to reduce the directive force—that is, while it varies with the heading the average value upon all azimuths is *minus* or southerly. The result of such a condition is unfavorable from the fact that the compass is thus made more "sluggish," is easily disturbed and does not return quickly to rest, and a given deflecting force produces a greater deviation when the directive force is reduced. The usual methods of compensation largely correct this fault, but do not entirely do so; it is therefore the case that the mean combined horizontal force of earth and ship to north is generally less than the horizontal force of the earth alone; but it is only in extreme cases that this deficiency is serious.

116. Heeling Error.—This is an additional cause of deviation that arises when the vessel heels to one side or the other. Heretofore only those forces have been considered which act when the vessel is on an even keel; but if there is an inclination from the vertical certain new forces arise, and others previously inoperative become effective. These forces are (*a*) the vertical component of the subpermanent magnetism acquired in building; (*b*) the vertical component of the induced magnetism in vertical soft iron, and (*c*) the magnetism induced by the vertical component of the earth's total force in iron which, on an even keel, was horizontal. The first two of these disturbing causes are always present, but, when the ship is upright, have no tendency to produce deviation, simply exerting a downward pull on one of the poles of the needle; the last is a new force that arises when the vessel heels.

The maximum disturbance due to heel occurs when the ship heads North or South. When heading East or West there will be no deviation produced, although the directive force of the needle will be increased or diminished. The error will increase with the amount of inclination from the vertical.

117. For the same reason as was explained in connection with semicircular deviations, that part of the heeling error due to subpermanent magnetism will vary, on change of latitude, as $\frac{1}{H}$, while that due to vertical induction will vary as $\tan \theta$. In south magnetic latitude the effect of vertical induction will be opposite in direction to what it is in north.

118. The heeling error is corrected by a permanent magnet placed in a vertical position directly under the center of the compass. Such a magnet has no effect upon the compass when the ship is upright; but since its force acts in an opposite direction to the force of the ship which causes heeling error, is equal to the latter in amount, and is exerted under the same conditions, it affords an effective compensation. For similar reasons to those affecting the compensation of B and C, the correction by means of a permanent magnet is not general, and must be rectified upon change of latitude.

PRACTICAL COMPENSATION.

119. In the course of explanation of the different classes of deviation occasion has been taken to state generally the various methods of compensating the errors that are produced. The practical methods of applying the correctors will next be given.

120. Order of Correction.—The following is the order of steps to be followed in each case. It is assumed that the vessel is on an even keel, that all surrounding masses of iron or steel are in their normal positions, all correctors removed, and that the binnacle is one in which the semicircular deviation is corrected by two sets of permanent magnets at right angles to each other.

1. Place quadrantal correctors by estimate.
2. Correct semicircular deviations.

3. Correct quadrantal deviations.
4. Swing ship for residual deviations.

The heeling corrector may be placed at any time after the semicircular and quadrantal errors are corrected. A Flinders bar can be put in place only after observations in two latitudes.

121. The ship is first placed on some magnetic cardinal point. If North or South, the only force (theoretically speaking) which tends to produce deflection of the needle will be the athwartship component of the semicircular force, whose effect is represented by the coefficient C. If East or West, the only deflecting force will be the fore-and-aft component of the semicircular force, whose effect is represented by the coefficient B. This will be apparent from a consideration of the direction of the forces producing deviation, and is also shown by the equation connecting the terms (where A and E are zero):

$$d = \text{B} \sin z' + \text{C} \cos z' + \text{D} \sin 2z'.$$

If the ship is headed North or South, z' being equal to 0° or 180°, the equation becomes $d = \pm$ C. If on East or West, z' being 90° or 270°, we have $d = \pm$ B.

This statement is exact if we regard only the forces that have been considered in the problem, but experience has demonstrated that the various correctors when in place create certain additional forces by their mutual action, and in order to correct the disturbances thus accidentally produced, as well as those due to regular causes, it is necessary that the magnetic conditions during correction shall approximate as closely as possible to those that exist when the compensation is completed; therefore the quadrantal correctors should first be placed on their arms at the positions which it is estimated that they will occupy later when exactly located. An error in the estimate will have but slight effect under ordinary conditions. It should be understood that the placing of these correctors has no corrective effect while the ship is on a cardinal point. Its object is to create at once the magnetic field with which we shall have to deal when compensation is perfected.

This having been done, proceed to correct the semicircular deviation. If the ship heads North or South, the force producing deflection is, as has been stated, the athwartship component of the semicircular force, which is to be corrected by permanent magnets placed athwartships; therefore enter in the binnacle one or more such magnets, and so adjust their height that the heading of the ship by compass shall agree with the magnetic heading. When this is done all the deviation on that azimuth will be corrected.

Similarly, if the ship heads East or West, the force producing deviation is the fore-and-aft component of the semicircular force, and this is to be corrected by entering fore-and-aft permanent magnets in the binnacle and adjusting the height so that the deviation on that heading disappears.

With the deviation on two adjacent cardinal points corrected, the semicircular force has been completely compensated. Next correct the quadrantal deviation. Head the ship NE., SE., SW., or NW. The coefficients B and C having been reduced to zero by compensation, and $2z'$, on the azimuths named, being equal to 90° or 270°, the equation becomes $d = \pm$ D. The soft-iron correctors are moved in or out from the positions in which they were placed by estimate until the deviation on the heading (all of which is due to quadrantal force) disappears. The quadrantal disturbing force is then compensated.

122. Determination of Magnetic Headings.—To determine when the ship is heading on any given magnetic course, and thus to know when the deviation has been corrected and the correctors are in proper position, four methods are available:

(*a*) Swing the ship and obtain by the best available method the deviations on a sufficient number of compass courses to construct a curve on the Napier diagram for one quadrant, and thus find the compass headings corresponding to two adjacent magnetic cardinal points and the intermediate intercardinal point, as North, NE., and East, magnetic.[a] Then put the ship successively on these courses, noting the corresponding headings by some other compass, and when it is desired to head on the various magnetic azimuths during the process of correction the ship may be steadied upon them by the auxiliary compass. Variations of this method will suggest themselves and circumstances may render their adoption convenient. The compass courses corresponding to the magnetic directions may be obtained from observations made with the auxiliary compass itself, or while making observations with another compass the headings by the auxiliary may be noted and a curve for the latter constructed, as explained in article 94, and the required headings thus deduced.

(*b*) By the methods to be explained hereafter (Chap. XIV), ascertain in advance the true bearing of the sun at frequent intervals during the period which is to be devoted to the compensation of the compasses; apply to these the variation and obtain the magnetic bearings; record the times and bearings in a convenient tabular form; set the watch accurately for the local apparent time; then when it is required to steer any given magnetic course, set that point of the pelorus for the ship's head and set the sight vanes for the magnetic bearing of the sun corresponding to the time by watch. Maneuver the ship with the helm until the sun comes on the sight vanes, when the azimuth of the ship's head will be that which is required. The sight vanes must be altered at intervals to accord with the table of times and bearings.

(*c*) Construct a table showing times and corresponding magnetic bearings of the sun, and also set the watch, as explained for the previous method. Then place the sight vanes of the azimuth circle of the compass at the proper angular distance to the right or left of the required azimuth of the ship's head; leave them so set and maneuver the ship with the helm until the image of the sun comes on with the vanes. The course will then be the required one. As an example, suppose that the table shows that the magnetic azimuth of the sun at the time given by the watch is N. 87° E., and let it be required to head magnetic North; when placed upon this heading, therefore, the sun must bear 87° to the right, or east, of the direction of the ship's head; when steady on any course, turn the sight vane to the required bearing relative to the keel. If on N. 11° W., for example, turn the circle to N. 76° E.; leave the vane

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[a] This is all that is required for the purposes of compensation, but if there is opportunity it is always well to make a complete swing and obtain a full table of deviations, which may give interesting information of the existing magnetic conditions.

undisturbed and alter course until the sun comes on. The magnetic heading is then North, and adjustment may be made accordingly.

(*d*) When ranges are available, they may be utilized for determining magnetic headings.

123. Summary of Ordinary Corrections.—To summarize, the following is the process of correcting a compass for a single latitude, where magnets at right angles are employed for compensating the semicircular deviation and where the disturbances due to unsymmetrical soft iron are small enough to be neglected:

First. All correctors being clear of the compass, place the quadrantal correctors in the position which it is estimated that they will occupy when adjustment is complete. The navigator's experience will serve in making the estimate, or if there seems no other means of arriving at the probable position they may be placed at the middle points of their supports.

Second. Steady the ship on magnetic North, East, South, or West, and hold on that heading by such method as seems best. By means of permanent magnets alter the indications of the compass until the heading coincides with the magnetic course. If heading North, magnets must be entered N. ends to starboard to correct easterly deviation and to port to correct westerly, and the reverse if heading South. If heading East, enter N. ends forward for easterly and aft for westerly deviations, and the reverse if heading West. (Binnacles differ so widely in the methods of carrying magnets that details on this point are omitted. It may be said, however, that the magnetic intensity of the correctors may be varied by altering either their number or their distance from the compass; generally speaking, several magnets at a distance are to be preferred to a small number close to the compass.)

Third. Steady the ship on an adjacent magnetic cardinal point and correct the compass heading by permanent magnets to accord therewith in the same manner as described for the first heading.

Fourth. Steady the ship on an intercardinal point (magnetic) and move the quadrantal correctors away from or toward the compass, keeping them at equal distances therefrom, until the compass and magnetic headings coincide.

124. The compensation being complete, the navigator should proceed immediately to swing ship and make a table of the residual deviations. Though the remaining errors will be small, it is seldom that they will be reduced to zero, and it must never be assumed that the compass may be relied upon without taking the deviation into account. Observations on eight equidistant points will ordinarily suffice for this purpose.

125. To Correct Semicircular Deviation with a Single Magnet.—In certain binnacles provision is made for correcting the semicircular deviation by a single magnet (or series of magnets) in the starboard angle, the magnet tray having motion in azimuth as well as vertically. In this case the process of correcting semicircular deviation is somewhat different from that described for correction by rectangular magnets. Either of the two following methods may be employed:

(*a*) By computation determine the starboard angle. An approximate method for doing this is given in article 103, and a more exact one may be found in works treating this subject mathematically. Head the ship on a cardinal point (magnetic); enter the magnets in the tray and revolve it until their N. ends lie at an angular distance from ahead (measured to the right) equal to the starboard angle; raise or lower the tray until the deviation disappears.

(*b*) Head the ship on a cardinal point (magnetic), enter the magnets, and turn the tray to an east-and-west position, the N. ends in such direction as will tend to reduce the deviation; raise or lower the tray until the deviation disappears. Alter course 90° and head on an adjacent magnetic cardinal point; observe the amount of deviation that the compass shows; correct half of this by altering the starboard angle and the other half by raising or lowering the tray. Return to first course, note deviation, and correct one-half in each way, as before. Continue the operation, making a series of trials until the deviations disappear on both headings, when the compensation will be correct. This operation may be considerably hastened by finding the first position of the magnets from a rough calculation of the starboard angle (art. 103).

126. Correcting the Heeling Error.—The heeling error may be corrected by a method involving computation, together with certain observations on shore. A more practical method, however, is usually followed, though its results may be less precise. The heeling corrector is placed in its vertical tube, N. end uppermost in north latitudes, as this is almost invariably the required direction; the ship being on a course near North or South and rolling, observe the vibrations of the card, which, if the error is material, will be in excess of those due to the ship's real motion in azimuth; slowly raise or lower the corrector until the abnormal vibrations disappear, when the correction will be made for that latitude; but it must be readjusted upon any considerable change of geographical position.

In making this observation care must be taken to distinguish the vessel's "yawing" in a seaway, from the apparent motion due to heeling error; for this reason it may be well to have an assistant to watch the ship's head and keep the adjuster informed of the real change in azimuth, by which means the latter may better judge the effect of the heeling error.

In the case of a sailing vessel, or one which for any reason maintains a nearly steady heel for a continuous period, the amount of the heeling error may be exactly ascertained by observing the azimuth of the sun, and corrected with greater accuracy than is possible with a vessel which is constantly rolling.

127. Flinders Bar.—The simplest method that presents itself for the placing of the Flinders bar is one which is available only for a vessel crossing the magnetic equator. Magnetic charts of the world show the geographical positions at which the dip becomes zero—that is, where a freely suspended needle is exactly horizontal and where there exists no vertical component of the earth's total magnetic force. In such localities it is evident that the factor of the semicircular deviation due to vertical induction disappears and that the whole of the existing semicircular deviation arises from subpermanent magnetism. If, then, when on the magnetic equator the compass be carefully compensated, the effect of the subpermanent magnetism will be exactly opposed by that of the semicircular correcting magnets. Later, as the ship departs from the magnetic equator, the semicircular deviation will gradually acquire a material value, which will be known to be due entirely to vertical induction, and if the Flinders bar be so placed as to correct it, the compensation of the compass will be general for all latitudes.

In following this method it may usually be assumed that the soft iron of the vessel is symmetrical with respect to the fore-and-aft line and that the Flinders bar may be placed directly forward of the compass or directly abaft it, disregarding the effect of components to starboard or port. It is therefore merely necessary to observe whether a vertical soft iron rod must be placed forward or abaft the compass to reduce the deviation, and, having ascertained this fact, to find by experiment the exact distance at which it completely corrects the deviation.

The Flinders bar frequently consists of a bundle of soft iron rods contained in a case, which is secured in a vertical position near the compass, its upper end level with the plane of the needles; in this method, the distance remaining fixed, the intensity of the force that it exerts is varied by increasing or decreasing the number of rods; this arrangement is more convenient and satisfactory than the employment of a single rod at a variable distance.

128. When it is not possible to correct the compass at the magnetic equator there is no ready practical method by which the Flinders bar may be placed; the operation will then depend entirely upon computation, and as a mathematical analysis of deviations is beyond the scope laid out for this work the details of procedure will not be gone into; the general principles involved are indicated, and students seeking more must consult the various works that treat the subject fully.

It has been explained that each coefficient of semicircular deviation (B and C) is made up of a sub-permanent factor varying as $\frac{1}{H}$ and of a vertical induction factor varying as $\tan\theta$. If we indicate by the subscripts $_s$ and $_v$, respectively, the parts due to each force, we may write the equations of the coefficients:

$$B = B_s \times \frac{1}{H} + B_v \times \tan\theta; \text{ and}$$

$$C = C_s \times \frac{1}{H} + C_v \times \tan\theta.$$

Now if we distinguish by the subscripts $_1$ and $_2$ the values in the first and in the second position of observation, respectively, of those quantities that vary with the magnetic latitude, we have:

$$B_1 = B_s \times \frac{1}{H_1} + B_v \times \tan\theta_1,$$

$$B_2 = B_s \times \frac{1}{H_2} + B_v \times \tan\theta_2; \text{ and}$$

$$C_1 = C_s \times \frac{1}{H_1} + C_v \times \tan\theta_1,$$

$$C_2 = C_s \times \frac{1}{H_2} + C_v \times \tan\theta_2.$$

The values of the coefficients in both latitudes are found from the observations made for deviations; the values of the horizontal force and of the dip at each place are known from magnetic charts; hence we may solve the first pair of equations for B_s and B_v, and the second pair for C_s and C_v; and having found the values of these various coefficients, we may correct the effects of B_s and C_s by permanent magnets in the usual way and correct the remainder—that due to B_v and C_v—by the Flinders bar.

Strictly, the Flinders bar should be so placed that its repelling pole is at an angular distance from ahead equal to the "starboard angle" of the attracting pole of the vertical induced force, this angle depending upon the coefficients B_v and C_v; but since, as before stated, horizontal soft iron may usually be regarded as symmetrical, C_v is assumed as zero and the bar placed in the midship line.

129. To Correct Adjustment on Change of Latitude.—The compensation of quadrantal deviation, once properly made, remains effective in all latitudes; but unless a Flinders bar is used a correction of the semicircular deviation made in one latitude will not remain accurate when the vessel has materially changed her position on the earth's surface. With this in mind the navigator must make frequent observations of the compass error during a passage and must expect that the table of residual deviations obtained in the magnetic latitude of compensation will undergo considerable change as that latitude is departed from. The new deviations may become so large that it will be found convenient to readjust the semicircular correcting magnets. This process is very simple.

When correctors at right angles are used, provide for steadying the ship, by an auxiliary compass or by the pelorus, upon two adjacent magnetic cardinal points (art. 122). Put the ship on heading North or South (magnetic), and raise or lower the athwartship magnets or alter their number until the deviation disappears; then steady on East or West (magnetic) and similarly adjust the fore-and-aft magnets. Swing ship for a new table of residual deviations.

When correctors in the starboard angle are used, arrange as before for heading on two adjacent cardinal magnetic courses. Steady on one of these, observe amount of compass error, correct half by changing the starboard angle and half by raising or lowering magnets; steady on the adjacent cardinal point and repeat the operation. Continue until adjustment is made on both headings, then swing for residual deviations.

CHAPTER IV.

PILOTING.

130. Definition.—*Piloting,* in the sense given the word by modern and popular usage, is the art of conducting a vessel in channels and harbors and along coasts, where landmarks and aids to navigation are available for fixing the position, and where the depth of water and dangers to navigation are such as to require a constant watch to be kept upon the vessel's course and frequent changes to be made therein.

131. Requisites.—As requisites to successful piloting, the navigator should be provided with the best available chart of the locality to be traversed, together with the sailing directions and descriptions of aids to navigation; and all of these should be corrected for the latest information, published in notices to mariners or otherwise, that bear upon the locality. The vessel should be equipped with the usual instruments employed in navigation. The deep-sea sounding-machine, if provided, should be ready for use when there is a chance that it may be needed. The lead lines should be correctly marked, and as shoal water is entered one or two men should be stationed to sound. The index errors of the sextants should be known, and, above all, there should be at hand a table showing correctly the deviation of the compass on each heading.

132. Laying the Course.—Mark a point upon the chart at the ship's position; then mark another point for which it is desired to steer; join the two by a line drawn with the parallel ruler, and, maintaining the direction of the line, move the ruler until its edge passes through the center of the compass rose and note the direction. If the compass rose indicates *true* directions, this will be the true course, and must be corrected for variation and deviation (by applying each in the *opposite* direction to its name) to obtain the compass course; if it is a *magnetic* rose, the course need be corrected for deviation only.

Before putting the ship on any course a careful look should be taken along the line over which it leads to be assured that it clears all dangers.

133. Methods of Fixing Position.—A navigator in sight of objects whose positions are shown upon the chart may locate his vessel by either of the following methods: (*a*) cross bearings of two known objects; (*b*) the bearing and distance of a known object; (*c*) the bearing of a known object and the angle between two known objects; (*d*) two bearings of a known object separated by an interval of time, with the run during that interval; (*e*) sextant angles between three known objects. Besides the foregoing there are two methods by which, without obtaining the precise position, the navigator may assure himself that he is clear of any particular danger. These are: (*f*) the danger angle; (*g*) the danger bearing.

The choice of the method will be governed by circumstances, depending upon which is best adapted to prevailing conditions.

134. Cross Bearings of two Known Objects.—Choose two objects whose position on the chart can be unmistakably identified and whose respective bearings from the ship differ, as nearly as possible, by 90°; observe the bearing of each, either by compass or pelorus, taking one as quickly as possible after the other; see that the ship is on an even keel at the time the observation is made, and, if using the pelorus, be sure also that she heads exactly on the course for which the pelorus is set. Correct the bearings so that they will be either true or magnetic, according as they are to be plotted by the true or magnetic compass rose of the chart—that is, if observed by compass, apply deviation and variation to obtain the true bearing, or deviation only to obtain the magnetic; if observed by pelorus, that instrument should be set for the true or magnetic heading, according as one or the other sort of reading is required, and no further correction will be necessary. Draw on the chart, by means of the parallel rulers, lines which shall pass through the respective objects in the direction that each was observed to bear. As the ship's position on the chart is known to be at some point of each of these lines, it must be at their intersection, the only point that fulfills both conditions.

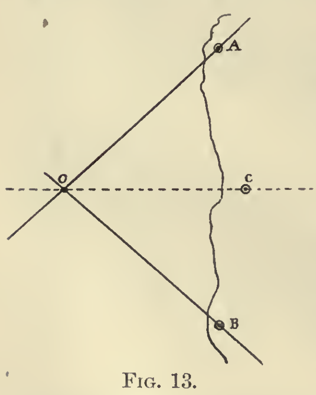

Fig. 13.

In figure 13, if A and B are the objects and OA and OB the lines passing through them in the observed directions, the ship's position will be at O, their intersection.

135. If it be possible to avoid it, objects should not be selected for a cross bearing which subtend an angle at the ship of less than 30° or more than 150°, as, when the lines of bearing approach parallelism, a small error in an observed bearing gives a large error in the result. For a similar reason objects near the ship should be taken in preference to those at a distance.

136. When a third object is available a bearing of that may be taken and plotted. If this line intersects at the same point as the other two (as the bearing OC of the object C in the figure), the navigator may have a reasonable assurance that his "fix" is correct; if it does not, it indicates an error somewhere, and it may have arisen from inaccurate observation, incorrect determination or application of the deviation, or a fault in the chart.

137. What may be considered as a form of this method can be used when only one known object is in sight by taking, at the same instant as the bearing, an altitude of the sun or other heavenly body and noting the time; work out the sight and obtain the Sumner line (as explained in Chapter XV), and the intersection of this with the direction-line from the object will give the observer's position in the same way as from two terrestrial bearings.

138. Bearing and Distance of a Known Object.—When only one object is available, the ship's position may be found by observing its bearing and distance. Follow the preceding method in the matters of taking, correcting, and plotting the bearing; then, on this line, lay off the distance from the object, which will give the point occupied by the observer. In figure 14, if A represents the object and AO the bearing and distance, the position sought will be at O.

Fig. 14.

139. It is not ordinarily easy to find directly the distance of an object at sea. The most accurate method is when its height is known and it subtends a fair-sized angle from the ship, in which case the angle may be measured by a sextant,[a] and the distance computed or taken from a table. Table 33 of this work gives distances up to 5 miles, corresponding to various heights and angles. Captain Lecky's "Danger Angle and Offshore Distance Tables" carries the computation much further. The use of this method at great distances must not be too closely relied upon, as small errors, such as those due to refraction, may throw out the results to a material extent; but it affords an excellent approximation, and as this method of fixing position is employed only when no other is available the best possible approximation has to suffice.

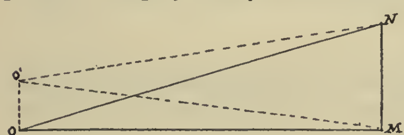

Fig. 15.

In measuring vertical angles, strictness requires that the observation should be so made that the angle at the foot of the object should equal 90° and that the triangle be a right triangle, as OMN, figure 15, where the line OM is truly horizontal, and not as in the triangle O′MN, where the condition is not fulfilled. This error is inappreciable, however, save at very close distances, when it may be sufficiently corrected by getting down as low as possible on board the vessel, so that the eye is near the water-line. One condition exists, however, where the error is material—that shown in figure 16, where the visible shore-line is at M′, a considerable distance from M, the point vertically below the summit. In this case there is nothing to mark M in the observer's eye, and it is essential that all angles be measured from a point close down to the water-line.

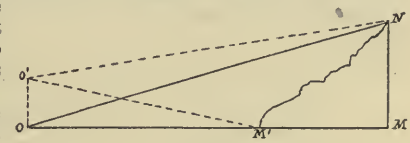

Fig. 16.

If a choice of objects can be made, the best results will be obtained by observing that one which subtends the greatest angle, as small errors will then have the least effect.

There is another method for determining the distance of an object, which is available under certain circumstances. This consists in observing, from a position aloft, the angle between the object and the line of the sea horizon beyond. By reference to Table 34 will be found the distance in yards corresponding to different angles for various heights of the observer from 20 to 120 feet. The method is not accurate beyond moderate distances (the table being limited to 5,000 yards) and is obviously only available for finding the distance of an isolated object, such as an islet, vessel, or target, over which the horizon may be seen. In employing this method the higher the position occupied by the observer the more precise will be the results.

140. In observing small angles, such as those that occur in the methods just described, it is sometimes convenient to measure them *on and off* the limb of the sextant. First look at the bottom of the object and reflect the top down into coincidence; then look through the transparent part of the horizon glass at the top and bring the bottom up by its reflected ray. The mean of the two readings will be the true angle, the index correction having been eliminated by the operation.

141. When the methods of finding distance by a vertical or a horizon angle are not available, it must be obtained by such means as exist. Estimate the distance by the appearance; take a sounding, and note where the depth falls upon the line of bearing; at night, if atmospheric conditions are normal, consider that the distance of a light when sighted is equal to its maximum range of visibility, remembering that its range is stated for a height of eye of 15 feet; or employ such method as suggests itself under the circumstances, regarding the result, however, as an approximation only.

142. The Bearing of a Known Object and the Angle between two Known Objects.—This method is seldom employed, as the conditions always permit of cross bearings being taken, and the latter is generally considered preferable.

Take a bearing of a known object by compass or pelorus and observe the sextant angle between some two known objects. The line of bearing is plotted as in former methods. In case one of the objects of the observed angle is that whose bearing is taken, the angle is applied, right or left as the case may be, to the bearing, thus giving the direction of the second object, which is plotted from the compass rose and parallel rulers. If the object whose bearing is taken is not one of the objects of the angle, lay off the angle on a three-armed protractor, or piece of tracing paper, and swing it (keeping the legs or lines always over the two objects) until it passes over the line of bearing, which defines the position of the ship; there will, except in special cases, be two points of intersection of the line with the circle thus described, and the navigator must know his position with sufficient closeness to judge which is correct.

143. Two Bearings of a Known Object.—This is a most useful method, which is frequently employed, certain special cases arising thereunder being particularly easy of application. The process

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[a] The use of the sextant is explained in Chapter VIII.

is to take a careful bearing and at the same moment read the patent log; then, after running a convenient distance, take a second bearing and again read the log, the difference in readings giving the intervening run; when running at a known speed, the time interval will also afford a means for determining the distance run.

The problem is as follows: In figure 17, given OA, the direction of a known object, A, at the first observation; PA, the direction at the second observation; and OP, the distance traversed between the two; to find AP, the distance at the second observation.

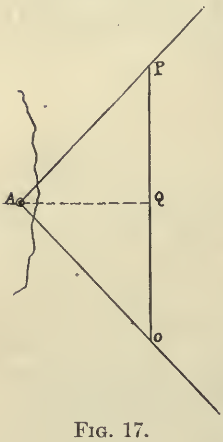

FIG. 17.

Knowing the angle POA, the angular distance of the object from right ahead at the first bearing; OPA, the angular distance from right astern at the second bearing; and OP, the distance run; we have by Plane Trigonometry:

$$PAO = 180° - (POA + OPA); \text{ and}$$
$$AP = OP \times \frac{\sin POA}{\sin PAO}.$$

If, as is frequently the case, we desire to know the distance of passing abeam, we have:

$$AQ = AP \times \sin OPA.$$

Tables 5A and 5B give solutions for this problem, the former for intervals of bearing of quarter points, the latter for intervals of two degrees. The first column of each of these tables gives the value of AP, the distance of the ship from the observed object at the time of taking the last bearing, for values of OP equal to unity; that is, for a run between bearings of 1 mile. The second column gives AQ, the distance of the object when it bears abeam, likewise for a value of OP of 1 mile. When the run between bearings is other than 1 mile, the number taken from the table must be used as a multiplier of that run to give the required distance.

EXAMPLE: A vessel steering north takes a bearing of a light NW. ½ W.; then runs 4.3 miles, when the bearing is found to be WSW. Required the distance of the light at the time of the second bearing.

Difference between course and first bearing, 4½ pts.
Difference between course and second bearing, 10 pts.
Multiplier from first column, Table 5A, 0.88.
4.3 miles × 0.88 = 3.8 miles, distance at second bearing.

EXAMPLE: A vessel on a course S. 52° E. takes the first bearing of an object at S. 26° E., and the second at S. 2° W., running in the interval 0.8 mile. Required the distance at which she will pass abeam.

Difference between course and first bearing, 26°.
Difference between course and second bearing, 54°.
Multiplier from second column, Table 5B, 0.76.
0.8 mile × 0.76 = 0.6 mile, distance of passing abeam.

144. As has been said, there are certain special cases of this problem where it is exceptionally easy of application; these arise when the multiplier is equal to unity, and the distance run is therefore equal to the distance from the object. When the angular distance on the bow at the second bearing is twice as great as it was at the first bearing, the distance of the object from the ship *at second bearing* is equal to the run, the multiplier being 1.0. For if, in figure 18, when the ship is in the first position, O, the object A bears α° on the bow, and at the second position, P, 2α°, we have in the triangle APO, observing that $APO = 180° - 2\alpha$, and $POA = \alpha$:

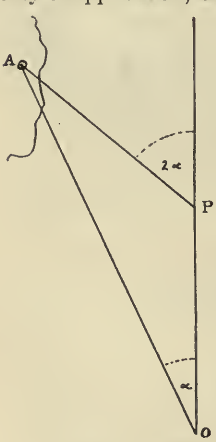

FIG. 18.

$$\begin{aligned} PAO &= 180° - (POA + APO), \\ &= 180° - (\alpha + 180° - 2\alpha), \\ &= \alpha. \end{aligned}$$

Or, since the angles at O and at A are equal to each other, the sides OP and AP are equal, or the distance at second bearing is equal to the run. This is known as *doubling the angle on the bow.*

145. A case where this holds good is familiar to every navigator as the *bow and beam bearing,* where the first bearing is taken when the object is broad on the bow (four points or 45° from ahead) and the second when it is abeam (eight points or 90° from ahead); in that case the distance at second bearing and the distance abeam are identical and equal to the run between bearings.

146. When the first bearing is 26½° from ahead, and the second 45°, the distance *at which the object will be passed abeam* will equal the run between bearings; this may be proved by computation or by reference to the tables and is a very convenient fact to remember, as it shows the navigator at once, if about to pass a point, how wide a berth he is going to give the offlying dangers.

147. There is a *graphic method* of solving this problem that is considered by some more convenient than the use of multipliers. Draw upon the chart the lines OA and PA (fig. 19), passing through the object on the two observed bearings; set the dividers to the distance run, OP; lay down the parallel rulers in a direction parallel to the course and move them toward or away from the observed object until some point is found where the distance between the lines of bearing is exactly equal to the distance between the points of the dividers; in the figure this occurs when the rulers lie along the line

OP, and therefore O represents the position of the ship at the first bearing and P at the second. For any other positions O′P′, O″P″, the condition is not fulfilled.

148. Another graphic solution is given by the *Distance Finder*, devised by Lieut. J. B. Blish, U. S. Navy. This consists of a semicircle whose circumference is graduated in degrees. Two pieces of thread, made to swing about a pin-head at the center, are laid down to represent the lines of bearing, and ease in measuring distances is afforded by series of cross lines similar to those on a piece of profile paper.

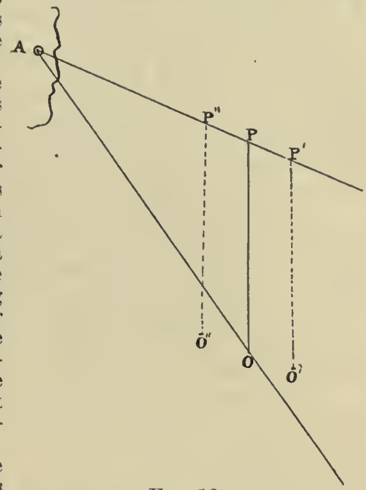

FIG. 19.

149. The method of obtaining position by two bearings of the same object is one of great value, by reason of the fact that it is frequently necessary to locate the ship when there is but one landmark in sight. Careful navigators seldom, if ever, miss the opportunity for a bow and beam bearing in passing a light-house or other well-plotted object; it involves little or no trouble, and always gives a feeling of added security, however little the position may be in doubt. If about to pass an object abreast of which there is a danger—a familiar example of which is when a light-house marks a point off which are rocks or shoals—a good assurance of clearance should be obtained before bringing it abeam, either by doubling the angle on the bow, or by using the 26½°–45° bearing; the latter has the advantage over the former if the object is sighted in time to permit of its use, as it may be assumed that the 45° (bow) bearing will always be observed in any event, and this gives the distance abeam directly, saving the necessity of plotting the position at second bearing (as obtained by doubling the angle) and then carrying it forward.

150. It must be remembered that, however convenient, the fix obtained by two bearings of the same object will be in error unless the course and distance are correctly estimated, the course "made good" and the distance "over the ground" being required. Difficulty will occur in estimating the exact course when there is bad steering, a cross current, or when a ship is making leeway; errors in the allowed run will arise when she is being set ahead or back by a current or when the logging is inaccurate. To take a not extreme case, a vessel making 10 knots through the water, running against a 2-knot tide, will overestimate her distance one-fifth of its true amount in taking a bow and beam bearing if no allowance is made for the tide, or she will underestimate her distance by one-fifth of its apparent amount if going with the same tide. Therefore, if in a current of any sort, due allowance must be made, and it should be remembered that more dependence can be placed upon a position fixed by simultaneous bearings or angles, when two or more objects are available, than by two bearings of a single object.

151. SEXTANT ANGLES BETWEEN THREE KNOWN OBJECTS.—This method, involving the solution of the *three-point problem*, will, if the objects be well chosen, give the most accurate results of any. It is largely employed in surveying, because of its precision; and it is especially valuable in navigation, because it is not subject to errors arising from imperfect knowledge of the compass error, improper logging, or the effects of current, as are the methods previously described.

Three objects represented on the chart are selected and the angles measured with sextants of known index error between the center one and each of the others. Preferably there should be two observers and the two angles be taken simultaneously, but one observer may first take the angle which is changing more slowly, then take the other, then repeat the first angle, and consider the mean of the first and last observations as the value of the first angle. The position is usually plotted by means of the three-armed protractor, or station-pointer (see art. 432, Chap. XVII). Set the right and left angles on the instrument, and then move it over the chart until the three beveled edges pass respectively and simultaneously through the three objects. The center of the instrument will then mark the ship's position, which may be pricked on the chart or marked with a pencil point through the center hole. When the three-armed protractor is not at hand, the tracing-paper protractor will prove an excellent substitute, and may in some cases be preferable to it, as, for instance, when the objects angled on are so near the observer as to be hidden by the circle of the instrument. A graduated circle printed upon tracing paper permits the angles being readily laid off, but a plain piece of tracing paper may be used and the angles marked by means of a small protractor. The tracing-paper protractor permits the laying down, for simultaneous trial, of a number of angles, where special accuracy is sought.

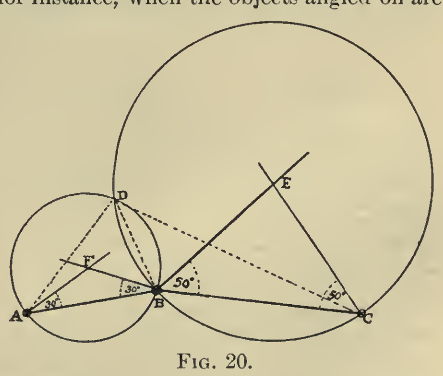

FIG. 20.

152. The three-point problem, by which results are obtained in this method, is: To find a point such that three lines drawn from this point to three given points shall make given angles with each other.

Let A, B, and C, in figure 20, be three fixed objects on shore, and from the ship, at D, suppose the angles CDB and ADB are found equal, respectively, to 40° and 60°.

With the complement of CDB, 50°, draw the lines BE and CE; the point of intersection will be the center of a circle, on some point of whose circumference the ship must be. Then, with the complement of the angle ADB, 30°, draw the lines AF and BF, meeting at F, which point will be the center of another circle, on some point of whose circumference the ship must be. Then D, the point of intersection of the circumference of the two circles, will be the position of the ship.

The correctness of this solution may be seen as follows: Take the first circle, DBC; in the triangle EBC, the angle at E, the center, equals $180° - 2 \times 50° = 2(90° - 50°)$, twice the complement of 50°, which is twice the observed angle; now if the angle at the center subtended by the chord BC equals twice the observed angle, then the angle at any point on the circumference subtended by that chord, which equals half the angle at the center, equals the observed angle; so the required condition is fulfilled. Should either of the angles exceed 90°, the excess of the angle over 90° must be laid off on the opposite side of the lines joining the stations.

153. It may be seen that the intersection of the circles becomes less sharp as the centers E and F approach each other; and finally that the problem becomes indeterminate when the centers coincide, that is, when the three observed points and the observer's position all fall upon the same circle; the two circles are then identical and there is no intersection; such a case is called a "revolver," because the protractor will revolve around the whole circle, everywhere passing through the observed points. The avoidance of the revolver and the employment of large angles and short distances form the keys to the selection of favorable objects.

Generally speaking, the observer, in judging which objects are the best to be taken, can picture in his eye the circle passing through the three points and note whether it comes near to his own position. If it does, he must reject one or more of the objects for another or others. It should be remembered that he must avoid not only the condition where the circle passes exactly through his position (when the problem is wholly indeterminate), but also all conditions approximating thereto, for in such cases the circles will intersect at a very acute angle, and the inevitable small errors of the observation and plotting will produce large errors in the resulting fix.

Without giving an analysis of reasons, which may be found in various works that treat the problem in detail, the following may be enumerated as the general conditions which result in a *good* fix:

(*a*) When the center object of the three lies between the observer and a line joining the other two, or lies nearer than either of the other two.

(*b*) When the sum of the right and left angles is equal to or greater than 180°.

(*c*) When two of the objects are in range, or nearly so, and the angle to the third is not less than 30°.

(*d*) When the three objects are in the same straight line.

A condition that limits all of these is that angles should be large—at least as large as 30°—excepting in the case where two objects are in range or nearly so, and then the other angle must be of good size. When possible, near objects should be used rather than distant ones. The navigator should not fall into the error of assuming that objects which would give good cuts for a cross bearing are necessarily favorable for the three-point solution.

In a revolver, the angle formed by lines drawn from the center object to the other two, added to the sum of the two observed angles, equals 180°. A knowledge of this fact may aid in the choice of objects.

If in doubt as to the accuracy with which the angles will plot, a third angle to a fourth object may be taken. Another way to make sure of a doubtful fix is to take one compass bearing, by means of which even a revolver may be made to give a good position.

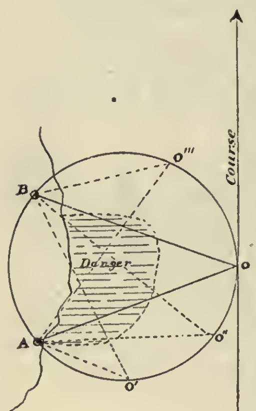

Fig. 21.

154. The Danger Angle.—When running in sight of the land, it is frequently of the greatest importance for the navigator to assure himself that the course leads clear of outlying dangers, and the *Danger Angle* affords a convenient means of so doing. There are two sorts of danger angles—the horizontal angle taken between two objects, and the vertical angle of a single one. The former will be first described.

155. Suppose, in figure 21, that a vessel standing along the coast on the course indicated must pass an offshore danger between two well-marked objects, A and B, and that, allowing a safe margin, it is desired to approach no closer than the point O. Through the points A, B, and O draw a circle, by the usual methods of geometry, and observe that no portion of the danger lies without the circle. Measure the angle AOB with a protractor, and consider this the danger angle; as the ship draws near, take frequent observations with a sextant of the angle subtended by the objects A and B. As long as the angle is less than the danger angle the ship is without the circle; but if the angle increases to the amount of the danger angle, she is on the circle, and should at once sheer off to avoid approaching closer. The reason will be evident from the consideration that all angles AOB, AO′B, AO″B, AO‴B, subtended at points on the circumference of the circle by the chord AB, are equal.

156. The vertical danger angle is an application of the same principle where there is in sight only one well-charted object and that is of known height. Draw a circle with that object as a center and of such radius that no neighboring dangers lie beyond its circumference; note, from Table 33, the vertical angle which is subtended by the known height at the distance chosen as a radius, and, by frequent observations in passing, make sure that this danger angle is not exceeded. By a simple modification, a ship passing *inshore* of an isolated rock or shoal could be navigated clear by means of a vertical danger angle which was not allowed to *decrease* below that corresponding to a safe distance.

Considerations governing the taking of vertical angles are given in the description of finding position by one bearing and the distance (arts. 139, 140).

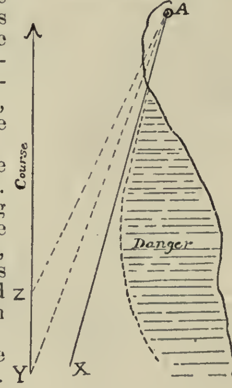

Fig. 22.

157. The Danger Bearing.—This is a method by which the navigator is warned by a compass bearing when the course is leading into danger. Suppose a vessel to be steering a course, as indicated in figure 22, along a coast which must not be approached within a certain distance, the landmark A being a guide. Let the navigator draw through A the line

XA, clear of the danger at all points, and note its direction by the compass rose; then let frequent bearings be taken as the ship proceeds, and so long as the bearings, YA, ZA, are to the *right* of XA he may be assured that he is on the *left* or safe side of the line.

If, as in the case given, there is but one object in sight and that nearly ahead, it would be very difficult to get an exact position, but this method would always show whether or not the ship was on a good course, and would, in consequence, be of the greatest value. And even if there were other objects visible by which to get an accurate fix it would be a more simple matter to note, by an occasional glance over the sight-vane of the pelorus or compass, that the ship was making good a safe course than to be put to the necessity of plotting the position each time.

158. It will occasionally occur that two natural objects will so lie that when in range they mark a danger bearing; advantage should be taken of all such, as they are easier to observe than a compass bearing; but if in a locality with which the navigator has not had previous acquaintance the compass bearing of all ranges should be observed and compared with that indicated on the chart in order to make sure of the identity of the objects. The utility of ranges, either artificial or natural, as guides in navigation is well recognized.

159. SOUNDINGS.—The practice should be followed of employing one or two leadsmen to take and report soundings continuously while in shoal water or in the vicinity of dangers. The soundings must not be regarded as fixing a position, but they afford a check upon the positions obtained by other methods. An exact agreement with the soundings on the chart need not be expected, as there may be some little inaccuracies in reporting the depth on a ship moving with speed through the water, or the tide may cause a discrepancy, or the chart itself may lack perfection; but the soundings should agree in a general way, and a marked departure from the characteristic bottom shown on the chart should lead the navigator to verify his position and proceed with caution; especially is this true if the water is more shoal than expected.

160. But if the soundings in shallow water when landmarks are in sight serve merely as an auxiliary guide, those taken (usually with the patent sounding machine or deep-sea lead) when there exist no other means of locating the position, fulfill a much more important purpose. In thick weather, when approaching or running close to the land, and at all times when the vessel is in less than 100 fathoms of water and her position is in doubt, soundings should be taken continuously and at regular intervals, and, with the character of the bottom, systematically recorded. By laying the soundings on tracing paper, along a line which represents the track of the ship according to the scale of the chart, and then moving the paper over the chart, keeping the various courses parallel to the corresponding directions on the chart, until the observed soundings agree with those laid down, the ship's position will in general be quite well determined. While some localities, by the sharpness of the characteristics of their soundings, lend themselves better than others to accurate determinations by this method, there are few places where the mariner can not at least keep out of danger by the indications, even if they tell him no more than that the time has come when he must anchor or lie off till conditions are more favorable.

161. LIGHTS.—Before coming within range of a light the navigator should acquaint himself with its characteristics, so that when sighted it will be recognized. The charts, sailing directions, and light lists give information as to the color, character, and range of visibility of the various lights. Care should be taken to note all of these and compare them when the light is seen. If the light is of the flashing, revolving, or occulting variety the duration of its periods should be noted to identify it. If a fixed light, a method that may be employed to make sure that it is not a vessel's light is to descend several feet immediately after sighting it and observe if it disappears from view; a navigation light will usually do so, excepting in misty weather, while a vessel's light will not. The reason for this is that navigation lights are as a rule sufficiently powerful to be seen at the farthest point to which the ray can reach without being interrupted by the earth's curvature. They are therefore seen at the first moment that the ray reaches an observer on a ship's deck, and are cut off if he lowers the eye. A vessel's light, on the other hand, is usually limited by its intensity and does not carry beyond a distance within which it it is visible at all heights.

Care must be taken to avoid being deceived on first sighting a light, as there are various errors into which the inexperienced may fall. The glare of a powerful light is often seen beyond the distance of visibility of its direct rays by the reflection downward from particles of mist in the air; the same mist may also cause a white light to have a distinctly reddish tinge, or it may obscure a light except within short distances. When a light is picked up at the extreme limit at which the height of the observer will permit, a fixed light may appear flashing, as it is seen when the ship is on the crest of a wave, and lost when in the hollow.

Many lights are made to show different colors in different sectors within their range, and by consulting his chart or books, the navigator may be guided by the color of the ray in which he finds himself; in such lights one color is generally used on bearings whence the approach is clear, and another covers areas where dangers are to be encountered.

The visibility of lights is usually stated for an assumed height of the observer's eye of 15 feet, and must be modified accordingly for any other height. But it should be remembered that atmospheric and other conditions considerably affect the visibility, and it must not be positively assumed, on sighting a light, even in perfectly clear weather, that a vessel's distance is equal to the range of visibility; it may be either greater or less, as the path of a ray of light near the horizon receives extraordinary deflection under certain circumstances; the conditions governing this deflection are discussed in article 301, Chapter X.

162. BUOYS.—While buoys are valuable aids, the mariner should always employ a certain amount of caution in being guided by them. In the nature of things it is never possible to be certain of finding buoys in correct position, or, indeed, of finding them at all. Heavy seas, strong currents, ice, or collisions with passing vessels may drag them from their places or cause them to disappear entirely, and they are especially uncertain in unfrequented waters, or those of nations that do not keep a good lookout upon their aids to navigation. When, therefore, a buoy marks a place where a ship must be navigated with caution, it is well to have a danger angle or bearing as an additional guide instead of placing too much dependence upon the buoy being in place.

Different nations adopt different systems of coloring for their buoys; an important feature of many such systems, including those adopted by the United States and various other great maritime

nations (though not all), consists in placing black buoys to be left on the starboard hand of a vessel *going out* of a harbor or fairway, and red buoys (the color of the port side light) on the port hand. In these various systems the color and character of the buoy are such as to denote the special purpose for which it is employed.

163. Fogs and Fog Signals.—As with lights, the navigator should, in a fog, acquaint himself with the characteristics of the various sound signals which he is likely to pick up, and when one is heard, its periods should be timed and compared with those given in the light lists to insure its proper identity.

Experiment has demonstrated that sound is conveyed through the atmosphere in a very uncertain way; that its intensity is not always increased as its origin is approached, and that areas within its range at one time will seem silent at another. Add to these facts the possibility that, for some cause, the signal may not be working as it should be, and we have reason for observing the rule to proceed with the utmost caution when running near the land in a fog.

The best guide is the lead, and that should be kept going constantly. The method of plotting soundings described in article 160 will give the most reliable position that is obtainable. Moreover, the lead will warn the navigator of the approach to shallow water, when, if his position is at all in doubt, it is wisest to anchor before it becomes too late.

When running slowly in a fog (which caution, as well as the law, requires that one should do) it must be borne in mind that the relative effect of current is increased; for instance, the angle of deflection from the course caused by a cross-set is greater at low than at high speed.

It is worth remembering that when in the vicinity of a bold bluff shore vessels are sometimes warned of a too close approach by having their own fog signals echoed back from the cliffs; indeed, from a knowledge of the velocity of sound (art. 314, Chap. XI) it is possible to gain some rough idea of the distance in such a case.

164. Tides and Currents.[a]—The information relating to the tides given on the chart and in other publications should be studied, as it is of importance for the navigator to know not only the height of the tide above the plane of reference of the chart, but also the direction and force of the tidal current.

The plane of reference adopted for soundings varies with different charts; on a large number it is that of mean low water, and as no plane of reference above that of mean low water is ever employed, the navigator may with safety refer his soundings to that level when in doubt.

When traversing waters in which the depth exceeds the vessel's draft by but a small margin, account must be taken of the fact that strong winds or a high barometer may cause the water to fall below even a very low plane of reference. On coasts where there is much diurnal inequality in the tides, the amount of rise and fall can not be depended upon, and additional caution is necessary.

A careful distinction should be made between the vertical *rise and fall* of the tide, which is marked at the transition periods by a stationary height, or *stand*, and the tidal current, which is the horizontal transfer of water as a result of the difference of level, producing the *flood and ebb*, and the intermediate condition, or *slack*. It seldom occurs that the turn of the tidal stream is exactly coincident with the high and low water, and in some channels the current may outlast the vertical movement which produces it by as much as three hours, the effect being that when the water is at a stand the tidal stream is at its maximum, and when the current is slack the rise or fall is going on with its greatest rapidity. Care must be taken to avoid confounding the two. Usually, more complete data is furnished in charts and tide tables regarding the rise and fall, and it frequently occurs that the information regarding the tidal current is comparatively meager; the mariner must therefore take every means to ascertain for himself the direction and force of the tidal and other currents, either from the set shown between successive well-located positions of the ship, or by noting the ripple of the water around buoys, islets, or shoals, the direction in which vessels at anchor are riding, and the various other visible effects of the current.

Current arrows on the chart must not be regarded as indicating absolutely the conditions that are to be encountered. They represent the mean of the direction and force observed, but the observations upon which they are based may not be complete, or there may be reasons that bring about a departure from the normal state.

Generally speaking, the rise and fall and strength of current are at their minimum along straight stretches of coast upon the open ocean, while bays, bights, inlets, and large rivers operate to augment the tidal effects, and it is in the vicinity of these that one finds the highest tides and strongest currents. The navigator need therefore not be surprised, in cruising along a coast, to notice that his vessel is set more strongly toward or from the shore in passing an indentation, and that the evidences of tide will appear more marked as he nears its mouth.

165. Charts.[b]—The chart should be carefully studied, and among other things all of its notes should be read, as valuable information may be given in the margin which it is not practicable to place upon the chart abreast the locality affected.

The mariner will do well to consider the source of his chart and the authority upon which it is based. He will naturally feel the greatest confidence in a chart issued by the Government of one of the more important maritime nations which maintains a well-equipped office for the especial purpose of acquiring and treating hydrographic information. He should note the character of the survey from which the chart has been constructed; and, finally, he should be especially careful that the chart is of recent issue or bears correction of a recent date—facts that should always be clearly shown upon its face.

It is well to proceed with caution when the chart of the locality is based upon an old survey, or one whose source does not carry with it the presumption of accuracy. Even if the original survey was a good one, a sandy bottom, in a region where the currents are strong or the seas heavy, is liable to undergo in time marked changes; and where the depth is affected by the deposit or removal of silt, as in the vicinity of the estuaries of large river systems, the behavior is sometimes most capricious. Large blank spaces on the chart, where no soundings are shown, may be taken as an indication that no sound-

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[a] See also Chapter XX.

[b] See also article 36 and following articles, Chapter II.

ings were made, and are to be regarded with suspicion, especially if the region abounds in reefs or pinnacle rocks, in which case only the the closest sort of a survey can be considered as revealing all the dangers. All of these facts must be duly weighed.

When navigating by landmarks the chart of the locality which is on the largest scale should be used. The hydrography and topography in such charts appear in greater detail, and—a most important consideration—bearings and angles may be plotted with increased accuracy.

166. Records.—It will be found a profitable practice to pay careful attention to the recording of the various matter relating to the piloting of the ship. A notebook should be kept at hand on deck or on the bridge, in which are to be entered all bearings or angles taken to fix the position, all changes of course, important soundings, and any other facts bearing upon the navigation. (This book should be different from the one in which astronomical sights and offshore navigation are worked.) The entries, though in memorandum form, should be complete; it should be clear whether bearings and courses are true, magnetic, or by compass; and it is especially important that the time and patent log reading should be given for each item recorded. The value of this book will make itself apparent in various directions; it will afford accurate data for the writing of the ship's log; it will furnish interesting information for the next run over the same ground; it will provide a means by which, if the ship be shut in by fog, rain, or darkness, or if there be difficulty in recognizing landmarks ahead, the last accurate fix can be plotted and brought forward; and, finally, if there should be a mishap, the notebook would furnish evidence as to where the trouble has been.

The chart on which the work is done should also be made an intelligible record, and to this end the pencil marks and lines should not be needlessly numerous, heavy, or long. In plotting bearings, draw lines only long enough to cover the probable position. Mark intersections or positions by drawing a small circle around them, and writing neatly abreast them the time and patent log reading. Indicate the courses and danger bearings by full lines and mark them appropriately, preferably giving both magnetic (or true) and compass directions. A great number of lines extending in every direction may lead to confusion; however remote the chance may seem, the responsibilities of piloting are too serious to run even a small risk.

Finally, on anchoring, record and plot the position by bearings or angles taken after coming to; observe that the berth is a safe one, or, if in doubt, send a boat to sound in the vicinity of the ship to make sure.

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CHAPTER V.

THE SAILINGS.

167. In considering a ship's position at sea with reference to any other place, either one that has been left or one toward which the vessel is bound, five terms are involved—the *Course*, the *Distance*, the *Difference of Latitude*, the *Difference of Longitude*, and the *Departure*.[a] The solutions of the various problems that arise from the mutual relation of these quantities are called *Sailings*.

168. Kinds of Sailings —When the only quantities involved are the course, distance, difference of latitude, and departure, the process is denominated *Plane Sailing*. In this method the earth is regarded as a plane, and the operation proceeds as if the vessel sailed always on a perfectly level surface. When two or more courses are thus considered, they are combined by the method of *Traverse Sailing*. It is evident that the number of *miles* of latitude and departure can thus be readily deduced; but, while one mile always equals one minute in difference of latitude, one mile of departure corresponds to a difference of longitude that will vary with the latitude in which the vessel is sailing. Plane sailing, therefore, furnishes no solution where difference of longitude is considered, and for such solution resort must be had to one of several methods, which, by reason of their taking account of the spherical figure of the earth, are called *Spherical Sailings*.

When a vessel sails on an east or west course along a parallel of latitude, the method of converting departure into difference of longitude is called *Parallel Sailing*. When the course is not east or west, and thus carries the vessel through various latitudes, the conversion may be made either by *Middle Latitude Sailing*, in which it is assumed that the whole run has been made in the mean latitude, or by *Mercator Sailing*, in which the principle involved in the construction of the Mercator chart (art. 38, Chap. II) is utilized.

Great Circle Sailing deals with the courses and distances between any two points when the track followed is a great circle of the terrestial sphere. A modification of this method which is adopted under certain circumstances is called *Composite Sailing*.

PLANE SAILING.

169. In Plane Sailing, the curvature of the earth being neglected, the relation between the elements of the rhumb track joining any two points may be considered from the plane right triangle formed by the meridian of the place left, the parallel of the place arrived at, and the rhumb line. In figure 23, T is the point of departure; T′, the point of destination; T*n*, the meridian of departure; T′*n*, the parallel of destination; and TT′, the rhumb line between the points. Let C represent the course, T′T*n;* Dist., the distance, TT′; DL, the difference of latitude, T*n;* and Dep., the departure, T′*n*. Then from the triangle TT′*n*, we have the following:

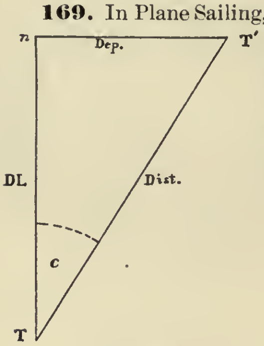

Fig. 23.

$$\sin C = \frac{\text{Dep.}}{\text{Dist.}};$$

$$\cos C = \frac{\text{D L}}{\text{Dist.}};$$

$$\tan C = \frac{\text{Dep.}}{\text{D L}}.$$

From these equations are derived the following formulæ for working the various problems that may arise in Plane Sailing:

Given.	Required.	Formulæ.	
Course and distance	Difference of latitude	D L = Dist. cos C.	Log D L = log Dist. + log cos C.
	Departure	Dep. = Dist. sin C.	Log Dep. = log Dist. + log sin C.
Difference of latitude and departure.	Course	$\text{Tan C} = \frac{\text{Dep.}}{\text{D L}}$.	Log tan C = log Dep. − log D L.
	Distance	$\text{Dist.} = \frac{\text{Dep.}}{\sin C}$.	Log Dist. = log Dep. − log sin C.
Course and difference of latitude.	Distance	$\text{Dist.} = \frac{\text{D L}}{\cos C}$.	Log Dist. = log D L − log cos C.
	Departure	Dep. = D L tan C.	Log Dep. = log D L + log tan C.

[a] For the definition of these terms, see article 6, Chapter I.

Given.	Required.	Formulæ.	
Course and departure	Distance	Dist. $=\frac{\text{Dep.}}{\sin C}$.	Log Dist. = log Dep. − log sin C.
	Difference of latitude	D L $=\frac{\text{Dep.}}{\tan C}$.	Log D L = log Dep. − log tan C.
Distance and difference of latitude.	Course	Cos C $=\frac{\text{D L}}{\text{Dist.}}$.	Log cos C = log D L − log Dist.
	Departure	Dep. = Dist. sin C.	Log Dep. = log Dist. + log sin C.
Distance and departure	Course	Sin C $=\frac{\text{Dep.}}{\text{Dist.}}$.	Log sin C = log Dep. − log Dist.
	Difference of latitude	D L = Dist. cos C.	Log D L = log Dist. + log cos C.

170. The solution of the plane right triangle may be accomplished either by Plane Trigonometry, by Traverse Tables, or by construction. If the former method is adopted, the logarithms of numbers may be found in Table 42, and of the functions of angles in Table 44. A more expeditious method is available, however, in the Traverse Tables, which give by inspection the various solutions. Table 1 contains values of the various parts for each unit of Dist. from 1 to 300, and for each quarter-point (2° 49′), of C; Table 2 contains values for each unit of Dist. from 1 to 600, and for each degree of C. The method of solving by construction consists in laying down the various given terms by scale upon a chart or plain paper, and measuring thereon the terms required.

171. Of the various problems that may arise, the first two given in the foregoing table are of much the most frequent occurrence. In the first, the given quantities are course and distance, and those to be found are difference of latitude and departure; this is the case where a navigator, knowing the distance run on a given course, desires to ascertain the amount made good to north or south and to east or west. In the second case the conditions are reversed; this arises where the course and distance between two points are to be obtained from their known difference of latitude and departure.

Example: A ship sails SW. by W., 244 miles. Required the difference of latitude and the departure made good.

By Computation.

Dist.	244	log	2.38739
C	56° 15′	log cos	9.74474
DL	135.6	log	2.13213
Dist.	244	log	2.38739
C	56° 15′	log sin	9.91985
Dep.	202.9	log	2.30724

By Inspection.

In Table 1, find the course SW. by W. (5 points); it occurs at the bottom of the page, therefore take the names of the columns from the bottom as well; opposite 244 in the Dist. column will be seen Lat. 135.6 and Dep. 202.9.

Example: A ship sails N. 5° E., 188 miles. Required the difference of latitude and the departure.

By Computation.

Dist.	188	log	2.27416
C	5°	log cos	9.99834
DL	187.3	log	2.27250
Dist.	188	log	2.27416
C	5°	log sin	8.94030
Dep.	16.4	log	1.21446

By Inspection.

In Table 2, find the course 5°; it occurs at the top of the page, therefore take the names of the columns from the top; opposite 188 in the Dist. column will be seen Lat. 187.3 and Dep. 16.4.

Example: A vessel is bound to a port which is 136 miles to the north and 203 miles to the west of her position. Required the course and distance.

By Computation.

Dep.	203	log	2.30750
DL	136	log	2.13354
C	(N.) 56° 11′ (W.)	log tan	0.17396
Dep.	203	log	2.30750
C	56° 11′	log sin	9.91951
Dist.	244.3	log	2.38799

By Inspection.

Enter Table 1 and turn the pages until a course is found whereon the numbers 136 and 203 are found abreast each other in the columns marked respectively Lat. and Dep. This occurs most nearly at the course for 5 points, the angle being taken from the bottom, because the appropriate names of the columns are found there. The course is therefore NW. by W. Interpolating for intermediate values, the corresponding number in the Dist. column is about 244.3.

Example: As the result of a day's run a vessel changes latitude 244 miles to the south and makes a departure of 171 miles to the east. What is the course and distance made good?

By Computation.

Dep.	171	log	2.23300
DL	244	log	2.38739
C	(S.) 35° 02′ (E.)	log tan	9.84561
Dep.	171	log	2.23300
C	35° 02′	log sin	9.75895
Dist.	297.9	log	2.47405

By Inspection.

Enter Table 2 and the nearest agreement will be found on course (S.) 35° (E.), the appropriate names being found at the top of the page. The nearest corresponding Dist. is 298 miles.

TRAVERSE SAILING.

172. A *Traverse* is an irregular track made by a ship in sailing on several different courses, and the method of *Traverse Sailing* consists in finding the difference of latitude and departure corresponding to several courses and distances and reducing all to a single equivalent course and distance. This is done by determining the distance to north or south and to east or west made good on each course, taking the algebraic sum of these various differences of latitude and departure and finding the course and distance corresponding thereto. The work can be most expeditiously performed by adopting a tabular form for the computation and using the traverse tables.

Example: A ship sails SSE., 15 miles; SE., 34 miles; W. by S., 16 miles; WNW., 39 miles; S. by E., 40 miles. Required the course and distance made good.

Courses.	Dist.	N.	S.	E.	W.
SSE.	15		13.9	5.7	
SE.	34		24.0	24.0	
W. by S.	16		3.1		15.7
WNW.	39	14.9			36.0
S. by E.	40		39.2	7.8	
		14.9	80.2	37.5	51.7
			14.9		37.5
S. by W.	66.8		65.3		14.2

The result of the various courses is, therefore, to carry the vessel S. by W., 66.8 miles from her original position.

PARALLEL SAILING.

173. Thus far the earth has been regarded as an extended plane, and its spherical figure has not been taken into account; it has thus been impossible to consider one of the important terms involved—namely, difference of longitude. *Parallel Sailing* is the simplest of the various forms of Spherical Sailing, being the method of interconverting departure and difference of longitude when the ship sails upon an east or west course, and therefore remains always on the same parallel of latitude.

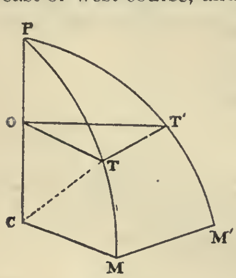

Fig. 24.

In figure 24 T and T′ are two places in the same latitude; P, the adjacent pole; TT′, the arc of the parallel of latitude through the two places; MM′, the corresponding arc of the equator intercepted between their meridians PM and PM′; and TT′, the departure on the parallel whose latitude is TCM = OTC, and whose radius is OT.

Let DLo represent the arc of the equator MM′, which is the measure of MPM′, the difference of longitude of the meridians PM and PM′; R, the equatorial radius of the earth, CM = CT; r, the radius OT of the parallel TT′; and L, the latitude of that parallel.

Then, since TT′ and MM′ are similar arcs of two circles, and are therefore proportional to the radii of the circles, we have:

$$\frac{\mathrm{TT'}}{\mathrm{MM'}} = \frac{\mathrm{OT}}{\mathrm{CM}}; \text{ or, } \frac{\mathrm{Dep.}}{\mathrm{DLo}} = \frac{r}{\mathrm{R}}.$$

From the triangle COT, $r = \mathrm{R} \cos \mathrm{L}$; hence

$$\frac{\mathrm{Dep.}}{\mathrm{DLo}} = \frac{\mathrm{R} \cos \mathrm{L}}{\mathrm{R}}; \text{ or, DLo} = \text{Dep. sec. L; or, Dep.} = \text{DLo} \cos \mathrm{L}.$$

Thus the relations are expressed between *minutes* of longitude and *miles* of departure.

174. Two cases arise under Parallel Sailing: First, where the difference of longitude between two places on the same parallel is given, to find the departure; and, second, where the departure is given, to find the difference of longitude.

In working these problems, the computation can be made by logarithms; but the traverse tables may more conveniently be employed. Remembering that those tables are based upon the formulæ,

$$DL = \text{Dist.} \cos C, \text{ and Dist.} = DL \sec C,$$

we may substitute for the column marked Lat. the departure, for that marked Dist. the difference of longitude, and for the courses at top and bottom of the page the latitude. The tables then become available for making the required conversions.

Example: A ship in the latitude of 49° 30′ sails directly east until making good a difference of longitude of 3° 30′. Required the departure.

By Computation.

L	49° 30′	log cos	9.81254
DLo	210′	log	2.32222
Dep.	136.4	log	2.13476

By Inspection.

Enter Table 2 with the latitude as C and the difference of longitude as Dist. As the table is calculated only to single degrees, we must find the numbers in the pages of 49° and 50° and take the mean. Corresponding to Dist. 210 in the former is Lat. 137.8, and in the latter Lat. 135.0. The mean, which is the required departure, is 136.4.

Example: A ship in the latitude of 38° sails due west a distance of 215.5 miles. Required the difference of longitude.

By Computation.

L	38°	log sec	0.10347
Dep.	215.5	log	2.33345
DLo	273′.5 / 4° 33′.5	log	2.43692

By Inspection.

Entering Table 2 with the latitude, 38°, as a course, corresponding with the number 215.5 in column of Lat., is 273.5 in the column of Dist. This is therefore the required difference of longitude, being equal to 4° 33′.5.

MIDDLE LATITUDE SAILING.

175. When a ship follows a course obliquely across the meridian the latitude is constantly changing, and the method of converting departure and difference of longitude by Parallel Sailing, just described, ceases to be applicable.

In figure 25, T is the point of departure; T′, the point of destination; P, the earth's pole; TT′, the rhumb track; n_1TT′, the course; Tn, n_1T′, the respective parallels of latitude; and MM′, the equator.

The difference of longitude between T and T′ is MPM′, which may be measured by the arc of the equator, MM′, intercepted between their meridians. This corresponds to a departure Tn in the latitude of T, and to the smaller departure T′n_1 in the higher latitude of T′; but since the vessel neither makes all of the departure in the latitude T, nor all of it in the latitude T′, the departure actually made in the passage must have some intermediate value between these extremes. Dividing the total difference of longitude into a number of equal parts MPm_1, m_1Pm_2, etc., of such small extent that, for the purposes of conversion, the change of latitude corresponding to each may be neglected, we have the total departure made up of the sum of a number of small departures, each equal to the same difference of longitude, but each different from the other. These will be $d_1 r_1$ in the latitude T, $d_2 r_2$ in the latitude r_1, etc. Hence we have:

$$MM' = d_1 r_1 \sec MT + d_2 r_2, \sec m_1 r_1 + d_3 r_3, \sec m_2 r_2, + \text{etc.}$$

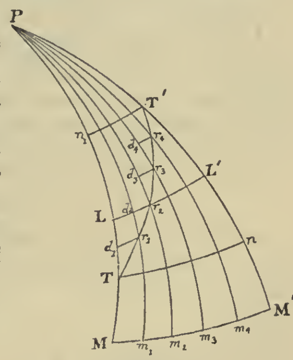

Fig. 25.

Now, if LL′ be a parallel of latitude lying midway between Tn and T′n_1, since there will be as many of the small parts lying above as below it, and since for moderate distances the ratio to be employed in the conversion of departure and difference of longitude may be regarded as varying directly with the latitude, it may be assumed for such distances that the sum of all of the different small departures equals the single departure between the meridians measured in the latitude LL′, and therefore that the departure obtained by the method of plane sailing on any course may be converted into difference of longitude by multiplying by the secant of the Middle Latitude.

The method of conversion based upon this assumption is denominated *Middle Latitude Sailing*, and by reason of its convenience and simplicity is usually employed for short distances, such as those covered by a vessel in a day's run.

176. In Middle Latitude Sailing, having found the mean of the latitudes, the solution is identical with that of Parallel Sailing (art. 173), substituting the Middle Latitude for the single latitude therein employed.

177. It may be remarked that the Middle Latitude should not be used when the latitudes are of opposite name; if of different names and the distance is small, the departure may be assumed equal to the difference of longitude, since the meridians are sensibly parallel near the equator; but if the distance is great the two portions of the track on opposites of the equator must be treated separately.

Example: A ship in Lat. 42° 30′ N., Long. 58° 51′ W., sails SE. by S., 300 miles. Required the latitude and longitude arrived at.

From Table 1: Course SE. by S., Dist., 300, we find Lat., 249.4 S. (4° 09′.4), Dep., 166.7 E.

Latitude left,	42° 30′.0 N.
DL,	4 09 .4 S.
Latitude arrived at,	38 20 .6 N.

Latitude left,	42° 30′ N.
Latitude arrived at,	38 21 N.
	2)80 51
Mid. latitude,	40 25 N.

Enter Table 2 with the middle latitude, 40°, as a course; the difference of longitude (Dist.) corresponding to the departure (Lat.) 166.7 is 217.6; entering with 41°, it is 220.9; the mean is 219.2 (3° 39′.2).

Longitude left,	58° 51′.0 W.
DLo,	3 39 .2 E.
Longitude arrived at,	55 11 .8 W.

EXAMPLE: A ship in Lat. 39° 42′ S., Long. 3° 31′ E., sails S. 42° W., 236 miles. Required the latitude and longitude arrived at.

From Table 2: Course, S. 42° W., Dist., 236 miles; we find Lat., 175.4 S. (2° 55′.4), Dep., 157.9 W.

Latitude left,	39° 42′.0 S.	Latitude left,	39° 42′ S.
DL,	2 55 .4 S.	Latitude arrived at,	42 37 S.
Latitude arrived at,	42 37 .4 S.		2)82 19
		Mid. latitude,	41 09 S.

From Table 2: Mid. Lat. (course), 41°, Dep. (Lat.), 157.9; we find DLo (Dist.), 209.3 (3° 29′.3).

Longitude left,	3° 31′.0 E.
DLo,	3 29 .3 W.
Longitude arrived at,	0 01 .7 E.

EXAMPLE: A vessel leaves Lat. 49° 57′ N., Long. 15° 16′ W., and arrives at Lat. 47° 18′ N., Long. 20° 10′ W. Required the course and distance made good.

Latitude left,	49° 57′ N.	Longitude left,	15° 16′ W.
Latitude arrived at,	47 18 N.	Longitude arrived at,	20 10 W.
DL,	{2° 39′ / 159′} S.	DLo,	{4° 54′ / 294′} W.
	2)97° 15′ N.		
Mid. latitude,	48 38 N.		

From Table 2: Mid. Lat. (course), 49°, DLo (Dist.), 294; we find Dep. (Lat.), 192.9.

From Table 2: DL 159 S., Dep. 192.9 W., we find course S. 51° W., Dist., 251 miles.

178. The assumption upon which Middle Latitude sailing is based—that the conversion may be made as if the whole distance were sailed upon a parallel midway between the latitudes of departure and destination—while sufficiently accurate for moderate distances, may be materially in error where the distances are large. In such case, either the method of Mercator Sailing (art. 179) must be employed, or else the correction given in the following table should be applied to the mean latitude to obtain what may be termed the latitude of conversion, being that latitude in which the required conditions are accurately fulfilled. The table is computed from the formula:

$$\cos L_c = \frac{l}{m},$$

where L_c represents the latitude of conversion, and l and m are respectively the differences of latitude and of meridional parts (art. 39, Chap. II) between the latitudes of departure and destination.[a]

Mid. Lat.	*Difference of latitude.*															Mid. Lat.
	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	12°	14°	16°	18°	20°	
°	′	′	′	′	′	′	′	′	′	′	′	′	′	′	′	°
15	−86	−85	−84	−83	−81	−79	−76	−73	−69	−65	−56	−46	−34	−21	− 6	15
18	−67	−67	−66	−65	−63	−61	−59	−56	−53	−50	−43	−34	−23	−12	1	18
21	−54	−54	−53	−52	−51	−49	−47	−44	−42	−39	−32	−24	−15	− 5	7	21
24	−44	−44	−44	−42	−41	−40	−38	−36	−33	−31	−24	−17	− 8	1	12	24
30	−31	−30	−29	−29	−28	−26	−24	−23	−20	−18	−12	− 6	1	11	21	30
35	−23	−22	−21	−21	−19	−18	−17	−15	−12	−10	− 5	2	10	18	28	35
40	−17	−16	−15	−14	−13	−12	−10	− 8	− 6	− 4	2	8	16	25	34	40
45	−12	−11	−11	−10	− 8	− 7	− 5	− 3	− 1	1	7	14	22	31	41	45
50	− 8	− 8	− 7	− 6	− 5	− 3	− 1	1	3	6	12	20	28	38	49	50
55	− 5	− 5	− 4	− 3	− 2	0	2	5	7	10	17	25	35	46	58	55
58	− 4	− 3	− 3	− 1	0	2	4	7	10	13	20	29	39	51	64	58
60	− 3	− 3	− 2	− 1	1	3	5	8	11	14	22	32	43	55	69	60
62	− 3	− 2	− 1	0	2	4	7	9	13	17	25	35	46	60	75	62
64	− 2	− 1	0	1	3	5	8	11	14	18	27	38	50	65	81	64
66	− 2	− 1	0	2	4	6	9	12	16	20	30	42	55	71	89	66
68	− 1	0	1	2	5	7	10	14	18	22	33	46	61	78	98	68
70	− 1	0	1	3	5	8	12	16	20	25	37	51	67	87	109	70
72	0	0	2	4	6	10	13	18	23	28	41	57	76	97	123	72

[a] The statement often made, that the latitude of conversion is always greater than the middle latitude, is not correct when the compression of the earth is taken into account, as an inspection of the table will show; that statement is based upon an assumption that the earth is a perfect sphere, and it was upon that assumption that a table which appeared in early editions of this work was computed. The value of the compression adopted for this table is $\frac{1}{293.465}$.

EXAMPLE: A vessel sails from Lat. 10° 13′ S. to Lat. 20° 21′ S., making a departure of 432 miles. Required the difference of longitude.

Latitude left,	10° 13′ S.	
Latitude arrived at,	20 21 S.	
	2)30 34	For Mid. Lat. 15° and Diff. of Lat. 10°, Correction, −65′.
Mid. latitude,	15 17 S.	
Correction,	− 1 05	
L_c,	14 12 S.	

L_c	14° 12′	log sec	.01348
Dep.	432	log	2.63548
DLo	445′.6	log	2.64896

MERCATOR SAILING.

179. *Mercator Sailing* is the method by which values of the various elements are determined from considering them in the relation in which they are plotted upon a chart constucted according to the Mercator projection.

180. Upon the Mercator chart (art. 38, Chap. II), the meridians being parallel, the arc of a parallel of latitude is shown as equal to the corresponding arc of the equator; the length of every such arc is, therefore, expanded; and, in order that the rhumb line may appear as a straight line, the meridians are also expanded by such amount as is necessary to preserve, in any latitude, the proper proportion existing between a unit of latitude and a unit of longitude. The lengths of small portions of the meridian thus increased are called *meridional parts* (art. 39, Chap. II), and these, computed for every minute of latitude from 0° to 80°, form the Table of Meridional Parts (Table 3), by means of which a Mercator chart may be constructed and all problems of Mercator Sailing may be solved.

In the triangle ABC (fig. 26), the angle ACB is the course, C; the side AC, the distance, Dist.; the side BC, the difference of latitude, DL; and the side AB, the departure, Dep. Then corresponding to the difference of latitude BC in the latitude under consideration, if CE be laid off to represent the meridional difference of latitude, m, completing the right triangle CEF, EF will represent the difference of longitude, DLo. The triangle ABC gives the relations involved in Plane Sailing as previously described; the triangle CEF affords the means for the conversion of departure and difference of longitude by Mercator Sailing.

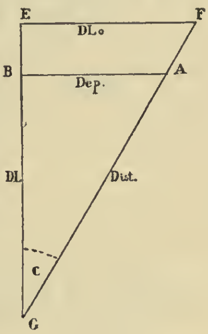

FIG. 26.

181. To find the arc of the expanded meridian intercepted between any two parallels, or the *meridional difference of latitude*, when both places are on the same side of the equator, subtract the meridional parts of the lesser latitude, as given by Table 3, from the meridional parts of the greater: the remainder will be the meridional difference of latitude; but if the places are on different sides of the equator, the sum of the meridional parts will be the meridional difference of latitude.

182. To solve the triangle CEF by the traverse tables it is only necessary to substitute meridional difference for Lat., and difference of longitude for Dep. Where long distances are involved, carrying the computation beyond the limits of the traverse table, as frequently occurs in this method, either of two means may be adopted: the problems may be worked by the trigonometrical formulæ, using logarithms, or the given quantities involved may all be reduced by a common divisor until they fall within the traverse table, and the results, when obtained, correspondingly increased. The former method is generally preferable, especially when the distances are quite large and accurate results are sought. The formulæ for the various conversions are as follows:

$$\tan C = \frac{DLo}{m};\ DLo = m \tan C;\ m = DLo \cot C.$$

EXAMPLE: A ship in Lat. 42° 30′ N., Long. 58° 51′ W., sails SE. by S., 300 miles. Required the latitude and longitude arrived at.

From Table 1: Course, SE. by S., Dist., 300; we find Lat. 249.4 S. (4° 09.′4).

Latitude left,	42° 30′.0 N.	Merid. parts,	+2806.4
DL,	4 09 .4 S.		
Latitude arrived at,	38 20 .6 N.	Merid. parts,	−2480.4
		m,	326.0

By Computation.

m	326.0	log	2.51322
C	33° 45′	log tan	9.82489
DLo	217′.8 / 3° 37′.8	log	2.33811

By Inspection.

Enter Table 1, course 3 points; since the quantities involved exceed the limits of the table, divide by 2; abreast $\frac{m}{2}$ (Lat.), 163.0, find $\frac{DLo}{2}$ (Dep.), 108.9; hence DLo=217′.8 or 3° 37′.8.

Longitude left,	58° 51′.0 W.
DLo,	3 37 .8 E.
Longitude arrived at,	55 13 .2 W.

EXAMPLE: A ship in Lat. 4° 37′ S., Long. 21° 05′ W., sails N. 14° W., 450 miles. Required the latitude and longitude arrived at.

From Table 2: Course, (N.) 14° (W.), Dist., 450; we find Lat. 436.6 N. (7° 16′.6).

Latitude left,	4° 37′.0 S.	Merid. parts,	+275.4
DL,	7 16 .6 N.		
Latitude arrived at,	2 39 .6 N.	Merid. parts,	+159.0
		m,	434.4

By Computation.

m	434.4	log	2.63789
C	14°	log tan	9.39677
DLo	108′.3 (1° 48′.3)	log	2.03466

By Inspection.

From Table 2: Course, 14°, m (Lat.), 434.4, we find DLo (Dep.) 108′.3 W., or 1° 48′.3.

Longitude left,	21° 05′.0 W.
DLo,	1 48 .3 W.
Longitude arrived at,	22 53 .3 W.

EXAMPLE: Required the course and distance by rhumb line from a point in Lat. 42° 03′ N., Long. 70° 04′ W., to another in Lat. 36° 59′ N., Long. 25° 10′ W.

Lat. departure, 42° 03′ N.	Merid. pts., +2770.1		Long. departure, 70° 04′ W.
Lat. destination, 36 59 N.	Merid. pts., −2377.3		Long. destination, 25 10 W.
DL 5° 04′ (304′) S.	m, 392.8		DLo 44° 54′ (2694′) E.
DLo 2694	log 3.43040		
m 392.8	log 2.59417		
C (S.) 81° 42′ (E.)	log tan .83623	log sec .84056	
DL 304′		log 2.48287	
Dist. 2106		log 3.32343	

The course is therefore S. 81° 42′ E., and the distance is 2,106 miles. Since the figures involved are so large, it is best to employ only the method by computation. The formula by which the Dist. is obtained comes from Plane Sailing.

GREAT CIRCLE SAILING.

183. The shortest distance between any two points on the earth's surface is measured by the arc of the great circle which passes through those points; and the method of sailing in which the arc of a great circle is employed for the track of the vessel, taking advantage of the fact that it is the shortest route possible, is denominated *Great Circle Sailing.*

184. It frequently happens when a great circle route is laid down that it is found to lead across the land, or to carry the vessel into a region of dangerous navigation or extreme cold which it is expedient to avoid; in such a case a certain parallel should be fixed upon as a limit of latitude, and a route laid down such that a great circle is followed as far as the limiting parallel, then the parallel itself, and finally another great circle to the port of destination. Such a modification of the great circle method is called *Composite Sailing.*

185. The *rhumb line* (art. 6, Chap. I) also called the *loxodromic curve*, which cuts all the meridians at the same angle, has been largely employed as a track by navigators on account of the ease with which it may be laid down on a Mercator chart. But as it is a longer line than the great circle between the same points, intelligent navigators of the present day use the latter wherever practicable. On the Mercator chart, however, the arc of a great circle joining two points (unless both are on the equator or both on the same meridian) will not be projected as a straight line, but as a curve which seems to be longer than the rhumb line; hence the shortest route appears as a circuitous one, and this is doubtless the reason that a wider use of the great circle has not been made.

It should be clearly understood that it is the rhumb line which is in fact the indirect route, and that in following the great circle the vessel is always heading for her port, exactly as if it were in sight, while on the course which is shown as a straight line on the Mercator chart the vessel never heads for her port until at the very end of the voyage.

186. The method of great circle sailing is of especial value to steamers, as such vessels need not, in the choice of a route, have regard for the winds to the same extent as must a sailing vessel; but even in navigating vessels under sail a knowledge of the great circle course may prove of great value. For example, suppose a ship to be bound from Sydney to Valparaiso; the first great circle course is SE. by S., while the Mercator course is almost due east. The distance is 748 miles shorter by the former route (if the

great circle is followed throughout, though this would lead to a latitude of 61° S.). With the wind at E. ½ S. the ship would lie nearer to the Mercator course on the starboard tack, assuming that she sailed within six points of the wind; but if she took that tack she would be increasing her distance from the port of destination by 4½ miles in every 10 that she sailed; while on the port tack, heading one point farther from the rhumb, the gain toward the port would be 9½ miles out of every 10. Any course between East and SSW. would be better than the Mercator course; and if the wind were anything to the eastward of SE. by S., the ship would gain by taking the port tack in preference to the starboard.

187. As the great circle makes a different angle with each meridian that is crossed, it becomes necessary to make frequent changes of the ship's course; in practice, the course is a series of chords joining the various points on the track line.

If, while endeavoring to follow a great circle, the ship is driven from it, as by unfavorable weather, it will not serve the purpose to return to the old track at convenience, but it is required that another great circle be laid down, joining the actual position in which the ship finds herself with the port of destination.

188. The methods of determining the great circle course may be divided generally into four classes; namely, by *Great Circle Sailing Charts*, by *Computation*, by the methods of the *Time Azimuth*, and by *Graphic Approximations*.

189. Great Circle Sailing Charts.—Of the available methods, that by means of charts especially constructed for the purpose is considered greatly superior to all others.

A series of great circle sailing charts covering the navigable waters of the globe is published by the United States Hydrographic Office. Being on the gnomonic projection (art. 43, Chap. II), all great circles are represented as straight lines, and it is only necessary to join any two points by such a line to represent the great circle track between them. The courses and distance are readily obtainable by a method explained on the charts. The track may be transferred to a chart on the Mercator projection by plotting a number of its points by their coordinates and joining them with a curved line.

The navigator who contemplates the use of great circle tracks will find it of the greatest convenience to be provided with these gnomonic charts for the regions which his vessel is to traverse.

190. By Computation.—This method consists in determining a series of points on the great circle by their coordinates of latitude and longitude, plotting them upon a Mercator chart, and tracing the curve that joins them. The first point determined is the *vertex*, or point of highest latitude, even when, as sometimes occurs, it falls without that portion of the great circle which joins the points of departure and destination.

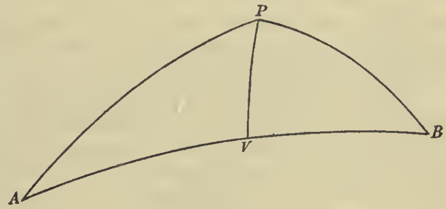

Fig. 27.

In figure 27, A represents the point of departure; B, the point of destination; AVB, the great circle joining them, with its vertex at V; and P, the pole of the earth.

Let C_A = PAB, the initial course;
C_B = PBA, the final course;
L_A, L_V, L_B = the latitudes of the respective points A, V, B = (90° − PA), (90° − PV), (90° − PB).
Lo_{AB}, Lo_{AV}, Lo_{BV} = the differences of longitude between A and B, A and V, B and V, respectively, = APB, APV, BPV.
D = the great circle distance between A and B; and
φ = an auxiliary angle introduced for the computation.

We then have:

$$\tan \varphi = \cos Lo_{AB} \cot L_B;$$
$$\cot C_A = \cot Lo_{AB} \cos (L_A + \varphi) \operatorname{cosec} \varphi;$$
$$\cot D = \cos C_A \tan (L_A + \varphi);$$
$$\cos L_V = \sin C_A \cos L_A;$$
$$\cot Lo_{AV} = \tan C_A \sin L_A.$$

By these formulæ are determined the initial course and the total distance by great circle; also the latitude of the vertex and its longitude with respect to A. By interchanging the subscript letters $_A$ and $_B$ throughout, we should obtain the final course, and the longitude of the vertex with respect to B; also the same total distance and latitude of the vertex as before.

In performing this computation, strict regard must be had to the signs of the quantities. If the points of departure and destination are in different latitudes, the latitude of one of these points must be regarded as negative with respect to the other, and they must be marked with opposite signs. Should Lo_{AV} or Lo_{BV} assume a negative value, it indicates that the vertex does not lie between A and B, and is to be laid off accordingly.

To find other points of the great circle, M, N, etc., let their latitudes be represented by L_M, L_N, etc., and their longitudes from the vertex by Lo_{VM}, Lo_{VN}, etc.; then

$$\tan L_M = \tan L_V \cos Lo_{VM}; \text{ or, } \cos Lo_{VM} = \tan L_M \cot L_V;$$
$$\tan L_N = \tan L_V \cos Lo_{VN}; \text{ or, } \cos Lo_{VN} = \tan L_N \cot L_V;$$

and so on. By these formulæ intervals of longitude from the vertex of 5°, 10°, or any amount, may be assumed, and the corresponding latitudes deduced; or any latitude may be assumed and its corresponding interval of longitude from the vertex found. Two positions will result from each solution, and the appropriate ones may be chosen by keeping in mind the signs involved.

EXAMPLE: Givèn two places, one in Lat. 40° N., Long. 70° W., the other in Lat. 30° S., Long. 10° W., find the great circle distance between them; also the initial course, and the longitude of equator crossing.

$$L_A = +40°;\ L_B = -30°;\ Lo_{AB} = 60°.$$

Lo_{AB}	60°	cos 9.69897	cot 9.76144			
L_B	− 30°	cot (−) .23856				
L_A	+ 40°				cos 9.88425	sin 9.80807
φ	− 40° 54′	tan (−) 9.93753	cosec (−) .18393			
$(L_A+\varphi)$	− 0° 54′		cos 9.99995	tan (−) 8.19616		
C_A	131° 24′ *or* S. 48° 36′ E		cot (−) 9.94532	cos (−) 9.82041	sin 9.87513	tan (−) .05472
D	89° 24′ *or* 5,364 miles			cot 8.01657		
L_V	+ 54° 56′				cos 9.75938	
Lo_{AV}	− 53° 54′					cot (−) 9.86279

The initial course is therefore S. 48° 36′ E., and the distance 5,364 nautical miles. (It may be found that the course by rhumb line is S. 38° 45′ E. and the distance 5,751 miles.) The vertex of the great circle is in Lat. 54° 56′ N., and is 53° 54′ in longitude from the point A, in a direction away from B; hence it is in Long. 123° 54′ W. To find the longitude of equator crossing let $L_M = 0°$; then in the equation,

$$\cos Lo_{VM} = \tan L_M \cot L_V,$$

since tan L_M equals zero, cos Lo_{VM} also equals zero, or the longitude interval from the vertex is 90°, which is evident from the properties of the great circle; therefore the longitude of equator crossing is 123° 54′ W.—90°=33° 54′ W.

191. BY TIME AZIMUTH METHODS.—A convenient method of obtaining the initial and final courses in great circle sailing is afforded by the tables and graphic methods which are prepared for the solution of the *Time Azimuth* problem (art. 359, Chap. XIV). It will be found by comparison that if the latitude of the point of departure be substituted for the latitude of the observer in that problem, the latitude of destination for the declination of the celestial body, and the longitude interval for the hour angle; the solution for the initial course will coincide with that for the azimuth; by interchanging the latitudes of the points of departure and destination the final course will be similarly obtained. Advantage may thus be taken of the various methods provided for facilitating the determination of the azimuth to ascertain the great circle courses from one point to another.

192. BY GRAPHIC APPROXIMATIONS.—Of the numerous methods that fall within this class only two need be given.

193. By the use of a *Terrestrial Globe* the two given points between which the great circle track is required may be joined by the shortest line between them, either by means of a piece of thread or by moving the globe until they are brought to the fixed horizon which is usually provided; the coordinates of the various points of the track are then transferred to the chart. The number of minutes of arc, as measured on the scale of the horizon between the points, equals the number of miles of distance; if there be no horizon, the measure may be made by a thread along the equator or a meridian.

194. The *Method of Professor Airy* consists in drawing on the chart a rhumb line joining the two points, and erecting at its middle point a perpendicular; the following table should then be entered with the middle latitude as an argument, and the "corresponding parallel" of latitude taken out (noting whether it is the same or opposite in name to the middle latitude); where this parallel is intersected by the perpendicular that was drawn will be the center from which may be swept an arc approximately representing the great circle between the two points.

Middle latitude.	Corresponding parallel.	Name.	Middle latitude.	Corresponding parallel.	Name.
°	° ′		°	° ′	
20	81 13	Opposite.	52	11 33	Opposite.
22	78 16	Do.	54	6 24	Do.
24	74 59	Do.	56	1 13	Do.
26	71 26	Do.	58	4 00	Same.
28	67 38	Do.	60	9 15	Do.
30	63 37	Do.	62	14 32	Do.
32	59 25	Do.	64	19 50	Do.
34	55 05	Do.	66	25 09	Do.
36	50 36	Do.	68	30 30	Do.
38	46 00	Do.	70	35 52	Do.
40	41 18	Do.	72	41 14	Do.
42	36 31	Do.	74	46 37	Do.
44	31 38	Do.	76	52 01	Do.
46	26 42	Do.	78	57 25	Do.
48	21 42	Do.	80	62 51	Do.
50	16 39	Do.			

COMPOSITE SAILING.

195. It has already been stated that when, for any reason, it is impracticable or unadvisable to follow the great circle track to its highest latitude, a limiting parallel is chosen and the route modified accordingly. This method is denominated *Composite Sailing.*

196. The shortest track between points where a fixed latitude is not exceeded is made up as follows:

1. A great circle through the point of departure tangent to the limiting parallel.
2. A course along the parallel.
3. A great circle through the point of destination tangent to the limiting parallel.

The composite track may be determined by *Great Circle Sailing Chart*, by *Computation*, or by *Graphic Approximation.*

197. On a *Great Circle Sailing Chart,* draw lines from the points of departure and destination, respectively, tangent to the limiting parallel; transfer these great circles to a Mercator chart in the usual manner, by the coordinates of several points, including in each case the point of tangency to the parallel. Follow the first great circle to the parallel; then follow the parallel; then the second great circle. Determine great circle courses and distances from the gnomonic chart as thereon described; determine the distance along the parallel by Parallel Sailing.

198. *By computation,* the problem consists in finding the great circles which pass, respectively, through the points of departure and destination and have their vertices in the latitude of the limiting parallel. Resuming the designation of terms already employed (art. 190), we have:

$$\cos Lo_{VA} = \tan L_A \cot L_V\,;$$
$$\cos Lo_{VB} = \tan L_B \cot L_V\,;$$

where Lo_{VA} and Lo_{VB} represent the distances in longitude from A and from B to the respective points of tangency; other features of each of the great circles may be determined in the usual manner.

EXAMPLE: A vessel in Lat. 30° S., Long. 18° W., is bound to a point in Lat. 39° S., Long. 145° E., and it is decided not to go south of the parallel of 55° S. Find the longitude of reaching that parallel and the longitude at which it should be left.

$$L_A = 30°\text{ S.};\quad L_B = 39°\text{ S.};\quad L_V = 55°\text{ S.}$$
$$Lo_A = 18°\text{ W.};\quad Lo_B = 145°\text{ E.}$$

L_A	30°	tan 9.76144	L_B	39°	tan 9.90837
L_V	55°	cot 9.84523	L_V	55°	cot 9.84523
Lo_{VA}	66° 09′ E.	cos 9.60667	Lo_{VB}	55° 27′ W.	cos 9.75360
Lo_A	18 00 W.		Lo_B	145 00 E.	
Lo_V	48 09 E.		Lo_V	89 33 E.	

199. A *graphic approximation* to the composite track may be obtained by drawing a straight line between the given points on a Mercator chart and erecting at its middle point a perpendicular, which should be extended until it intersects the limiting parallel. Then through this intersection and the two points describe the arc of a circle, and this will approximate to the shortest distance within the assigned limit of latitude.

200. A terrestrial globe may be employed for the determination of the composite track; the method of its use will suggest itself.

201. Another approximation is obtained by joining the two points with a single great circle, and following this to its intersection with the limiting parallel; thence sailing along the parallel until the great circle is again intersected; then resuming the circle and following it to the destination.

CHAPTER VI.

DEAD RECKONING.

202. *Dead Reckoning* is the process by which the position of a ship at any instant is found by applying to the last well-determined position the run that has since been made, using for the purpose the ship's course and the distance indicated by the log.

203. Positions by dead reckoning, also spoken of as positions *by account*, differ from those determined by bearings of terrestrial objects or by observations of celestial bodies in being less exact, as the correctness of dead reckoning depends upon the accuracy of the estimate of the run, and this is always liable to be at fault to a greater or less extent. The course made good by a ship may differ from that which it is believed that she is making good, by reason of imperfect steering, improper allowance for compass error and leeway, and the effects of unknown currents; the allowed distance over the ground may be in error on account of inaccurate logging and unknown currents.

Notwithstanding its recognized defects as compared with the more exact methods, the dead reckoning is an invaluable aid to the mariner. It affords him a means of plotting the position of the ship at any desired time between astronomical determinations; it also gives him an approximate position at the moment of taking astronomical observations which is a great convenience in working up those observations; and finally it affords the only available means of determining the location of a vessel at sea during those periods (which may continue for several days together) when the weather is such as to render the observation of celestial bodies an impossibility.

204. Taking Departure.—Before losing sight of the land, and preferably while objects remain in good view, it is the duty of the navigator to *take a departure;* this consists in fixing the position of the ship by the best means available (Chap. IV), and using this position as the origin for dead reckoning. There are two methods of reckoning the departure. The first and simpler consists in taking from the chart the latitude and longitude of the position found, and applying the future run thereto. The other requires that the bearing and distance of an object of known latitude and longitude be found; the position of the object then forms the basis of the reckoning, and the *reversed* direction of the bearing, with the distance, forms the first course and distance; thus it may be considered that the ship starts from the position of the object and sails to the position where the bearing was taken; the correction for deviation in such a case should be that due to the heading of the ship when the bearing was taken. Each time that a new position is determined it is used as a new departure for the dead reckoning.

This meaning of the term *departure* should not be confounded with the other, which refers to the distance run toward east or west.

205. Methods.—The working of dead reckoning merely involves an application of the methods of Traverse Sailing (art. 172) and Middle Latitude Sailing (art. 175), as explained in Chapter V.

The various compass courses are set down in a column, and abreast each are written the errors by reason of which the course steered by compass differs from the true course made good over the ground; thence the true course made good is determined and recorded; next, the distance is written in, and afterwards, by means of Tables 1 or 2 (according as the courses are expressed in quarter points or degrees), the difference of latitude and departure are found, separate columns being kept for distances to the north, south, east, and west.

When the position of the ship at any moment is required, add up all the differences of latitude and departure, and write in the column of the greater the difference between the northing and southing, and the easting and westing. Apply the difference of latitude to the latitude of the last determined position, which will give the latitude by D. R., and from which may be found the middle latitude; with the middle latitude find the difference of longitude corresponding to the departure, apply this to the longitude of last position, and the result will be the longitude by D. R.

The employment of the tabular form will be found to facilitate the work and guard against errors. It will be a convenience to include in that form columns showing the hour, together with the reading of the patent log (if used) each time that the course is changed or the dead reckoning worked up.

The employment of minutes and tenths in dead reckoning rather than minutes and seconds is recommended.

Example: A vessel under sail heading NE. $\frac{3}{4}$ E. (on which course deviation is $\frac{1}{4}$ pt, Easterly) takes departure from Cape Henry light-house (see Appendix IV for position), bearing SSW. $\frac{1}{2}$ W. per compass, distant 1.4 miles. She then sails on a series of courses, with errors and distances as indicated below; wind about SE. by E. Required the position by dead reckoning; also the course and distance made good by dead recokning.

Comp. course.	Var.	Dev.	Leeway.	Error.	True course.	Dist.	N.	S.	E.	W.	D.
NNE. ½ E.	½ W.	¼ E.		¼ W.	NNE. ¼ E.	1.4	1.3		0.6		
NE. ¾ E.	½ W.	¼ E.	¼ W.	½ W.	NE. ¼ E.	27.6	18.5		20.5		
S. by W.	½ W.	0	¼ E.	¼ W.	S. ¾ W.	31.5		31.2		4.6	
ENE.	½ W.	¼ E.	½ W.	¾ W.	NE. by E. ¼ E.	14.2	7.3		12.2		
S. ¼ E.	½ W.	0	½ E.	0	S. ¼ E.	11.0		11.0	0.5		
NE. ¼ N.	¾ W.	¼ E.	¼ W.	¾ W.	NE. by N.	87.0	72.3		48.3		
							99.4	42.2	82.1	4.6	
Made good,					NE. ¾ E.	96.5	57.2		77.5		97.0

	Latitude.		Longitude.
Point of departure,	36° 55′.6 N.		76° 00′.5 W.
Run,	57 .2 N.	Mid. L., 37°	1 37 .0 E.
By D. R.	37 52 .8 N.		74 23 .5 W.

Example: A steamer's position by observation at noon, patent log reading 27.3, is Lat. 49° 15′ N., Long. 7° 32′ W. Thence she steers S. 82° W. (per compass), the total compass error on that course being 20° W., until 12.30, at which time, patent log reading 33.9, the course is changed to S. 80° W. (*p. c.*), same error. At 4.12, patent log 80.5, sights are taken from which it is found that the true longitude is 8° 46′ W., and the compass error 19° W. At 6.15, patent log reading 6.1, a sight is taken from which it is found that the true latitude is 48° 34′ 30″ N. At 8 p. m. the patent log reads 27.5. Required the positions by D. R. at each sight and at 8 o'clock.

Time.	Comp. course.	Error.	True course.	Pat. Log.	Dist.	S.	W.	D.
Noon.				27.3				
12.30	S. 82° W.	20° W.	S. 62° W.	33.9	6.6	3.1	5.8	
4.12	S. 80° W.	20° W.	S. 60° W.	80.5	46.6	23.3	40.3	
						26.4	46.1	70.3
6.15	S. 80° W.	19° W.	S. 61° W.	6.1	25.6	12.4	22.4	34.1
8.00	S. 80° W.	19° W.	S. 61° W.	27.5	21.4	10.4	18.7	27.9

	Latitude.		Longitude.
By obs. at noon,	49° 15′.0 N.		7° 32′.0 W.
Run to 4.12 sight,	26.4 S.	Mid. L., 49°	1 10.3 W.
By D. R. at 4.12 sight,	48 48.6 N.		8 42.3 W.
By obs. at 4.12 sight,			8 46.0 W.
Run to 6.15 sight,	12.4 S.	Mid. L., 49°	34.1 W.
By D. R. at 6.15 sight,	48 36.2 N.		9 20.1 W.
By obs. at 6.15 sight,	48 34.5 N.		
Run to 8 p. m.,	10.4 S.	Mid. L., 48°	27.9 W.
By D. R. at 8 p. m.,	48 24.1 N.		9 48.0 W.

206. Allowance for Current.—When a vessel is sailing in a known current whose strength may be estimated with a fair degree of accuracy, a more correct position may be arrived at by regarding the set and drift of the current as a course and distance to be regularly taken account of in the dead reckoning.

Example: A vessel in the Gulf Stream at a point where the current is estimated to set N. 48° E. at the rate of 1.8 miles an hour, sails S. 3° W. (true), making 9.5 knots an hour through the water for $3^h\ 30^m$. Middle latitude 35°. Required the course and distance made good.

	True course.	Dist.	N.	S.	E.	W.	D.
Run	S. 3° W.	33.3		33.3		1.7	
Current	N. 48° E.	6.3	4.2		4.7		
Made good	S. 6° E.	29.3		29.1	3.0		3.6

207. Finding the Current.—It is usual, upon obtaining a good position by observation (as the navigator usually does at noon), to compare that position with the one obtained by dead reckoning, and to attribute such discrepancy as may be found to the effects of current. It has already been pointed out that other causes than the motion of the water tend to make the dead reckoning inaccurate, so that it must not be assumed that currents proper are thus determined with complete correctness.

Current is said to have *set* and *drift*, referring respectively to the direction toward which it is flowing and the velocity with which it moves.

It is evident that, in calculating current by the method of comparing positions by observation with those by account, the navigator must limit himself to the periods during which the dead reckoning has been brought forward independently, without receiving any corrections due to new points of departure. In case it is desired to find the current covering a period during which fresh departures have been used, as from noon to noon, find the algebraical sums of all the differences of latitude and longitude from the table, and apply these to the latitude and longitude of original departure—that of the preceding noon; this gives the position from the ship's run proper, and the difference between this and the position by observation gives the set and drift for the twenty-four hours; if an allowance has been made for current, as explained in the preceding article, that must be omitted in bringing up the position which is to take account of the run only.

208. Day's Run.—It is usual to calculate, each day at noon, the ship's total run for the preceding twenty-four hours. Having the positions at noon of each day, the course and distance between them is found as explained in article 175, Chapter V. The position by observation is used in each case, if such has been found; otherwise, the position by dead reckoning.

Example: At noon, January 22, the position of a vessel by observation was Lat. 35° 10′ N., Long. 134° 01′ W. During the next 24 hours, the run by account was 60.1 miles north and 153.2 miles east. At noon, January 23, the position by observation was Lat. 36° 03′ N., Long. 131° 14′ W. Required the position by D. R. at the latter time; also the run and current for the 24 hours.

	Latitude.		*Longitude.*
By obs., noon, 22d,	35° 10′.0 N.	Mid. L., 36°	134° 01′.0 W.
Run,	1 00 .1 N.	Dep., 153.2 E.	3 09 .4 E.
By D. R., noon, 23d,	36 10 .1 N.	D, 189.4 E.	130 51 .6 W.
By obs., noon, 23d,	36 03 .0 N.	D, 22.4 W.	131 14 .0 W.
Current,	6 .9 S.	Dep., 18.1 W.	22 .4 W.

Current for 24 hours, 6.9 S., 18.1 W. = S. 69° W., 19.4 miles.
Current per hour, S. 69° W., 0.8 mile.

	Latitude.		*Longitude.*
By obs., noon, 23d,	36° 03′.0 N.	Mid. L., 36°	131° 14′.0 W.
By obs., noon, 22d,	35 10 .0 N.	D, 167.0 E.	134 01 .0 W.
Run,	0 53 .0 N.	Dep., 135.1	2 47 .0 E.

Run for 24 hours, 53.0 N., 135.1 E. = N. 68° E., 146 miles.

CHAPTER VII.

DEFINITIONS RELATING TO NAUTICAL ASTRONOMY.

209. *Nautical Astronomy*, or *Celo-Navigation*, has been defined (art. 3, Chap. I) as that branch of the science of Navigation in which the position of a ship is determined by the aid of celestial objects—the sun, moon, planets, or stars.

210. The Celestial Sphere.—An observer upon the surface of the earth appears to view the heavenly bodies as if they were situated upon the surface of a vast hollow sphere, of which his eye is the center. In reality we know that this apparent vault has no existence, and that we can determine only the relative directions of the heavenly bodies—not their distances from each other or from the observer. But by adopting an imaginary spherical surface of an infinite radius, the eye of the observer being at the center, the places of the heavenly bodies can be projected upon this *Celestial Sphere*, or *Celestial Concave*, at points where the lines joining them with the center intersect the surface of the sphere. Since, however, the center of the earth should be the point from which all angular distances are measured, the observer, by transferring himself there, will find projected on the celestial sphere, not only the heavenly bodies, but the imaginary points and circles of the earth's surface. The actual position of the observer on the surface will be projected in a point called the *zenith;* the meridians, equator, and all other lines and points may also be projected.

211. An observer on the earth's surface is constantly changing his position with relation to the celestial bodies projected on the sphere, thus giving to the latter an apparent motion. This is due to three causes: first, the diurnal motion of the earth, arising from its rotation upon its axis; second, the annual motion of the earth, arising from its motion about the sun in its orbit; and third, the actual motion of certain of the celestial bodies themselves. The changes produced by the diurnal motion are different for observers at different points upon the earth, and therefore depend upon the latitude and longitude of the observer. But the changes arising from the other causes named are independent of the observer's position, and may therefore be considered at any instant in their relation to the center of the earth. To this end the elements necessary for any calculation are tabulated in the *Nautical Almanac* from data based upon laws which have been found by long series of observations to govern the actual and apparent motion of the various bodies.

212. The *Zenith* of an observer on the earth's surface is the point of the celestial sphere vertically overhead. The *Nadir* is the point vertically beneath.

213. The *Celestial Horizon* is the great circle of the celestial sphere formed by passing a plane through the center of the earth at right angles to the line which joins that point with the zenith of the observer. The celestial horizon differs somewhat from the *Visible Horizon*, which is that line appearing to an observer at sea to mark the intersection of earth and sky. This difference arises from two causes: first, the eye of the observer is always elevated above the sea level, thus permitting him a range of vision exceeding 90° from the zenith; and second. the observer's position is on the surface, instead of at the center of the earth. These causes give rise, respectively, to *dip of the horizon* and *parallax*, which will be explained later (Chap. X).

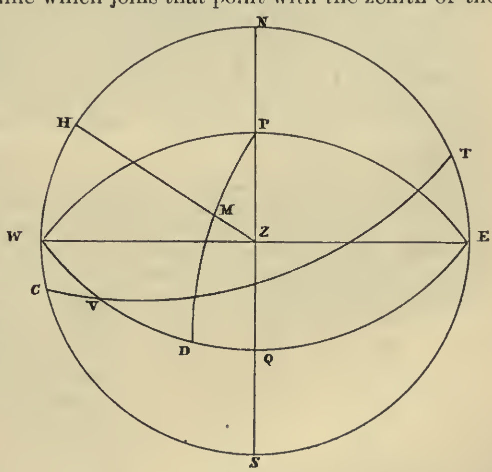

Fig. 28.

214. In figure 28 the celestial sphere is considered to be projected upon the celestial horizon, represented by NESW.; the zenith of the observer is projected at Z, and that pole of the earth which is elevated above the horizon, assumed for illustration to be the north pole, appears at P, the *Elevated Pole* of the celestial sphere. The other pole is not shown in the figure.

215. The *Equinoctial*, or *Celestial Equator*, is the great circle formed by extending the plane of the earth's equator until it intersects the celestial sphere. It is shown in the figure in the line EQW. The equinoctial intersects the horizon in E and W, its east and west points.

216. *Hour Circles, Declination Circles*, or *Celestial Meridians* are great circles of the celestial sphere passing through the poles; they are therefore secondary to the equinoctial, and may be formed by extending the planes of the respective terrestrial meridians until they intersect the celestial sphere. In the figure, PW, PS, PE, are hour circles, and that one, PS, which contains the zenith and is therefore formed by the extension of the terrestrial meridian of the observer, intersects the horizon in N and S, its north and south points.

217. *Vertical Circles*, or *Circles of Altitude*, are great circles of the celestial sphere which pass through the zenith and nadir; they are therefore secondary to the horizon. In the figure, ZH, WZE, NZS, are projections of such circles; the vertical circle NZS, which passes through the poles, coincides with the

216 Hour or Declination Circle are the same see II 213

meridian of the observer. The vertical circle WZE, whose plane is at right angles to that of the meridian, intersects the horizon in its eastern and western points, and, therefore, at the points of intersection of the equinoctial; this circle is distinguished as the *Prime Vertical.*

218. The *Declination* of any point in the celestial sphere is its angular distance from the equinoctial, measured upon the hour or declination circle which passes through that point; it is designated as *North* or *South* according to the direction of the point from the equinoctial; it is customary to regard north declinations as positive (+), and south declinations as negative (—). In the figure, DM is the declination of the point M. Declination upon the celestial sphere corresponds with latitude upon the earth.

219. The *Polar Distance* of any point is its angular distance from the pole (generally, the elevated pole of an observer), measured upon the hour or declination circle passing through the point; it must therefore equal 90° *minus* the declination, if measured from the pole of the same name as the declination, or 90° *plus* the declination, if measured from the pole of opposite name. The polar distance of the point M from the elevated pole, P, is PM.

220. The *Altitude* of any point in the celestial sphere is its angular distance from the horizon, measured upon the vertical circle passing through the point; it is regarded as positive when the body is on the same side of the horizon as the zenith. The altitude of the point M is HM.

221. The *Zenith Distance* of any point is its angular distance from the zenith, measured upon the vertical circle passing through the point; the zenith distance of any point which is above the horizon of an observer must therefore equal 90° *minus* the altitude. The zenith distance of M, in the figure, is ZM.

222. The *Hour Angle* of any point is the angle at the pole between the meridian of the observer and the hour circle passing through that point; it may also be regarded as the arc of the equinoctial intercepted between those circles. It is measured toward the west as a positive direction through the twenty-four hours, or 360 degrees, which constitute the interval between the successive returns to the meridian, due to the diurnal rotation of the earth, of any point in the celestial sphere. The hour angle of M is the angle QPD, or the arc QD.

223. The *Azimuth* of a point in the celestial sphere is the angle at the zenith between the meridian of the observer and the vertical circle passing through the point; it may also be regarded as the arc of the horizon intercepted between those circles. It is measured from either the north or the south point of the horizon (usually that one of the same name as the elevated pole) to the east or west through 180°, and is named accordingly; as, N. 60° W., or S. 120° W. The azimuth of M is the angle NZH, or the arc NH, from the north point, or the angle SZH, or the arc SH, from the south point of the horizon.

224. The *Amplitude* of a point is the angle at the zenith between the prime vertical and the vertical circle of the point; it is measured from the east or the west point of the horizon through 90°, as W. 30° N. It is closely allied with the azimuth and may always be deduced therefrom. In the figure, the amplitude of H is the angle WZH, or the arc WH. The amplitude is only used with reference to points in the horizon.

225. The *Ecliptic* is the great circle representing the path in which, by reason of the annual revolution of the earth, the sun appears to move in the celestial sphere; the plane of the ecliptic is inclined to that of the equinoctial at an angle of 23° 27½′, and this inclination is called the *obliquity of the ecliptic.* The ecliptic is represented by the great circle CVT.

226. The *Equinoxes* are those points at which the ecliptic and the equinoctial intersect, and when the sun occupies either of these positions the days and nights are of equal length throughout the earth. The *Vernal Equinox* is that one at which the sun appears to an observer on the earth when passing from southern to northern declination, and the *Autumnal Equinox* that one at which it appears when passing from northern to southern declination. The Vernal Equinox is also designated as the *First Point of Aries,* and is used as an origin for reckoning right ascension; it is indicated in the figure at V.

227. The *Solstitial Points,* or *Solstices,* are points of the ecliptic at a distance of 90° from the equinoxes, at which the sun attains its highest declination in each hemisphere. They are called respectively the *Summer* and the *Winter Solstice,* according to the season in which the sun appears to pass these points in its path.

228. The *Right Ascension* of a point is the angle at the pole between the hour circle of the point and that of the First Point of Aries; it may also be regarded as the arc of the equinoctial intercepted between those circles. It is measured from the First Point of Aries to the eastward as a positive direction, through twenty-four hours or 360 degrees. The right ascension of the point M is VD.

229. *Celestial Latitude* is measured to the north or south of the ecliptic upon great circles secondary thereto. *Celestial Longitude* is measured upon the ecliptic from the First Point of Aries as an origin, being regarded as positive to the eastward throughout 360°.

230. Coordinates.—In order to define the position of a point in space, a system of lines, angles, or planes, or a combination of these, is used to refer it to some fixed line or plane adopted as the primitive; and the lines, angles, or planes by which it is thus referred are called *coordinates.*

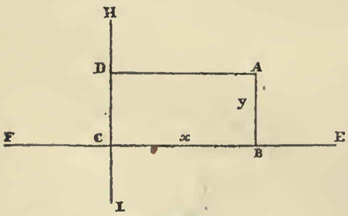

Fig. 29.

231. In figure 29 is shown a system of rectilinear coordinates for a plane. A fixed line FE is chosen, and in it a definite point C, as the *origin.* Then the position of a point A is defined by $CB = x$, the distance from the origin, C, to the foot of a perpendicular let fall from A on FE; and by $AB = y$, the length of the perpendicular. The distance x is called the *abscissa* and y the *ordinate.* Assuming two intersecting right lines FE and HI as standard lines of reference, the location of the point A is defined by regarding the distances measured to the right hand of HI and above FE as *positive;* those to the left hand of HI and below FE as *negative.*

An exemplification of this system is found in the chart, on which FE is represented by the equator, HI by the prime meridian; the coordinates x and y being the longitude and latitude of the point A.

232. The great circle is to the sphere what the straight line is to the plane; hence, in order to define the position of a point on the surface of a sphere, some great circle must be selected as the primary, and some particular point of it as the origin. Thus, in figure 30, which represents the case of a sphere, some fixed great circle, CBQ, is selected as the axis and called the *primary;* and a point C is chosen as the origin. Then to define the position of any point A, the abscissa x equals the distance from C to the point B, where the secondary great circle through A intersects the primary; the ordinate y equals the distance of A from the primary measured on the secondary—that is, $x = \text{CB}$ and $y = \text{AB}$.

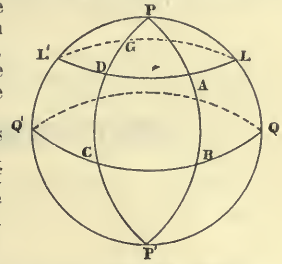

Fig. 30.

233. In the case of the earth, the primary selected is the equator (its plane being perpendicular to the earth's axis), and upon this are measured the abscissæ, while upon the secondaries to it are measured the ordinates of all points on the earth's surface. The initial point for reference on the equator is determined by the *prime meridian* chosen, West longitudes and North latitudes being called *positive*, East longitudes and South latitudes, *negative*.

234. In the case of the celestial sphere, there are four systems of coordinates in use for defining the position of any point; these vary according to the circle adopted as the primary and the point used as an origin. They are as follows:

1. Altitude and azimuth.
2. Declination and hour angle.
3. Declination and right ascension.
4. Celestial latitude and longitude.

235. In the system of *Altitude and Azimuth*, the primary circle is the celestial horizon, the secondaries to which are the vertical circles, or circles of altitude. The horizon is intersected by the celestial meridian in its northern and southern points, of which one—usually that adjacent to the elevated pole—is selected as an origin for reckoning coordinates. The azimuth indicates in which vertical circle the point to be defined is found, and the altitude gives the position of the point in that circle. In figure 28 the point M is located, according to this system, by its azimuth NH and altitude HM.

236. In the system of *Declination and Hour Angle*, the primary circle is the equinoctial, the secondaries to which are the circles of declination, or hour circles. The point of origin is that point of intersection of the equinoctial and celestial meridian which is above the horizon. The hour angle indicates in which declination circle the point to be defined is found, and the declination gives the position of the point in that circle. In figure 28 the point M is located, according to this system, by its hour angle QD and declination DM.

237. In the system of *Declination and Right Ascension*, the primary and secondaries are the same as in the system just described, but the point of origin differs, being assumed to be at the First Point of Aries, or vernal equinox. The right ascension indicates in which declination circle the point to be defined may be found, and the declination gives the position in that circle. In figure 28 the point M is located by VD, the right ascension, and DM, the declination. It should be noted that this system differs from the preceding in that the position of a point is herein referred to a fixed point in the celestial sphere and is independent of the zenith of the observer as well as of the position of the earth in its diurnal motion, while, in the system of declination and hour angle, both of these are factors in determining the coordinates.

238. In the system of *Celestial Latitude and Longitude*, the primary circle is the ecliptic; the point of origin, the First Point of Aries. The method of reckoning by this system, which is of only slight importance in Nautical Astronomy, will appear from the definitions of celestial latitude and longitude already given (art. 229).

CHAPTER VIII.

INSTRUMENTS EMPLOYED IN NAUTICAL ASTRONOMY.

THE SEXTANT.

239. The *sextant* is an instrument for measuring the angle between two objects by bringing into coincidence at the eye of the observer rays of light received directly from the one and by reflection from the other, the measure being afforded by the inclination of the reflecting surfaces. By reason of its small dimensions, its accuracy, and, above all, the fact that it does not require a permanent or a stable mounting but is available for use under the conditions existing on shipboard, it is a most important instrument for the purposes of the navigator. While the sextant is not capable of the same degree of accuracy as fixed instruments, its measurements are sufficiently exact for navigation.

240. Description.—A usual form of the sextant is represented in figure 31. The frame is of brass or some similar alloy. The graduated arc, AA, generally of silver, is marked in appropriate divisions; in the finer sextants, each division represents 10′, and the vernier affords a means of reading to 10″. A wooden handle, H, is provided for holding the instrument. The *index mirror*, M, and *horizon mirror*, *m*, are of plate glass, and are silvered, though the upper half of the horizon glass is left plain to allow direct rays to pass through unobstructed. To give greater distinctness to the images, a small *telescope*, E, is placed in the line of sight; it is supported in a ring, K, which can be moved by a screw in a direction at right angles to the plane of the sextant, thus shifting the axis of the telescope, and therefore the plane of reflection; this plane, however, always remains parallel to that of the instrument, the motion of the telescope being intended merely to regulate the relative brightness of the direct and reflected images. In the ring K are small screws for the purpose of adjusting the telescope by making its axis parallel with the plane of the sextant. The vernier is carried on the end of an index bar pivoted beneath the index mirror, M, and thus travels along the graduated scale, affording a measure for any change of inclination of the index mirror; a reading glass, R, attached to the index bar and turning upon a pivot, S, facilitates the reading of vernier and scale. The index mirror, M, is attached to the head of the index bar, with its surface perpendicular to the plane of the instrument; an adjusting screw is fitted at the back to permit of adjustment to the perpendicular plane. The fixed glass *m*, half silvered and half plain, is called the *horizon glass*, as it is through this that the horizon is observed in measuring altitudes of celestial bodies; it is provided with screws, by which its perpendicularity to the plane of the instrument may be adjusted. At P and Q are colored glasses of different shades, which may be used separately or in combination to protect the eye from the intense light of the sun. In order to observe with accuracy and make the images come precisely in contact, a *tangent-screw*, B, is fixed to the index, by means of which the latter may be moved with greater precision than by hand; but this screw does not act until the index is fixed by the screw C at the back of the sextant; when the index is to be moved any considerable amount, the screw C is loosened; when it is brought near to its required position the screw must be tightened, and the index may then be moved gradually by the tangent-screw.

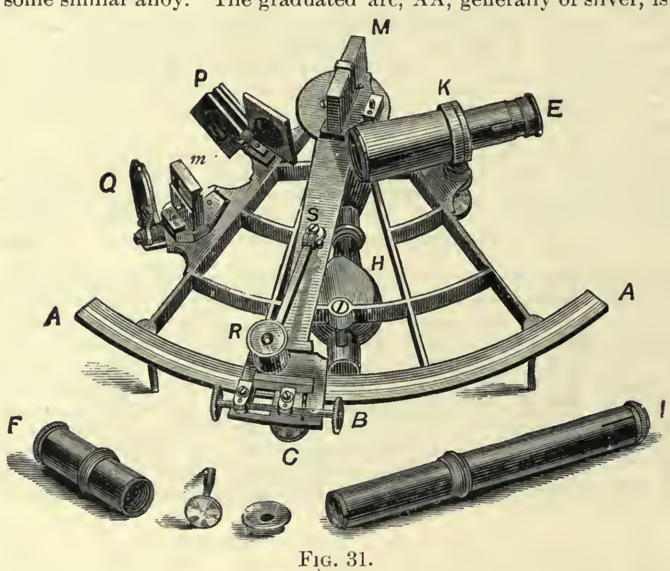

Fig. 31.

Besides the telescope, E, the instrument is usually provided with an inverting telescope, I, and a tube without glasses, F; also, with a cap carrying colored glasses, which may be put on the eye-end of the telescope, thus dispensing with the necessity for the use of the colored shades, P and Q, and eliminating any possible errors which might arise from nonparallelism of their surfaces.

241. The *vernier* is an attachment for facilitating the exact reading of the scale of a sextant, by which aliquot parts of the smallest divisions of the graduated scale are measured. The principle of the sextant vernier is identical with that of the barometer vernier, a complete description of which will be found in article 51, Chapter II. The arc of a sextant is usually divided into 120 or more parts, each

division representing 1°; each of these degree divisions is further subdivided to an extent dependent upon the accuracy of reading of which the sextant is capable. In the instruments for finer work, the divisions of the scale correspond to 10′ each, and the vernier covers a length corresponding to 59 such divisions, which is subdivided into 60 parts, thus permitting a reading of 10″; all sextants, however, are not so closely graduated.

Whatever the limits of subdivision, all sextants are fitted with verniers which contain one more division than the length of scale covered, and in which, therefore, scale-readings and vernier-readings increase in the same direction—toward the left hand. To read any sextant, it is merely necessary to observe the scale division next below, or to the right of, the zero of the vernier, and to add thereto the angle corresponding to that division of the vernier scale which is most nearly in exact coincidence with a division of the instrument scale.

242. Optical Principle.—When a ray of light is reflected from a plane surface, the angle of incidence is equal to the angle of reflection. From this it may be proved that when a ray of light undergoes two reflections in the same plane the angle between its first and its last direction is equal to twice the inclination of the reflecting surfaces. Upon this fact the construction of the sextant is based.

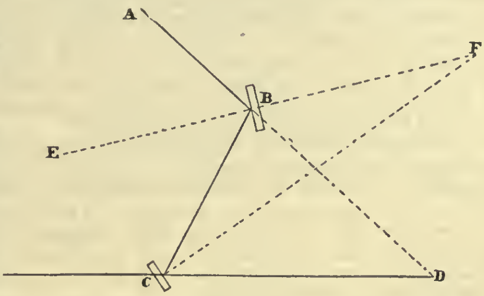

Fig. 32.

In figure 32 let B and C represent respectively the index mirror and horizon mirror of a sextant; draw EF perpendicular to B, and CF perpendicular to C; then the angle CFB represents the inclination of the two mirrors. Suppose a ray to proceed from A and undergo reflection at B and at C, its last direction being CD; then ADC is the angle between its first and last directions, and we desire to prove that ADC = 2 CFB.

From the equality of the angles of incidence and reflection:

$$ABE = EBC, \text{ and } ABC = 2\ EBC;$$
$$BCF = FCD, \text{ and } BCD = 2\ BCF.$$

From Geometry:

$$ADC = ABC - BCD = 2\ (EBC - BCF) = 2\ CFB,$$

which is the relation that was to be proved.

243. In the sextant, since the index mirror is immovably attached to the index arm, which also carries the vernier, it follows that no change can occur in the inclination between the index mirror and the horizon mirror, excepting such as is registered by the travel of the vernier upon the scale.

If, when the index mirror is so placed that it is nearly parallel with the horizon mirror, an observer direct the telescope toward some well-defined object, there will be seen in the field of view two separate images of the object; and if the inclination of the index mirror be slightly changed by moving the index bar, it will be seen that while one of the images remains fixed the other moves. The fixed image is the direct one seen through the unsilvered part of the horizon glass, while the movable image is due to rays reflected by the index and horizon mirrors. When the two images coincide these mirrors must be parallel (assuming that the object is sufficiently distant to disregard the space which separates the mirrors); in this position of the index mirror the vernier indicates the true zero of the scale. If, however, instead of observing a single object, the instrument is so placed that the direct ray from one object appears in coincidence with the reflected ray of a second object, then the true angle between the objects will be twice the angle of inclination between the mirrors, or twice the angle measured by the vernier from the true zero of the scale. To avoid the necessity of doubling the angle on the scale, the latter is so marked that each half degree appears as a whole degree, whence its indications give the whole angle directly.

244. Adjustments of the Sextant.—The theory of the sextant requires that, for accurate indications, the following conditions be fulfilled:

(*a*) The two surfaces of each mirror and shade glass must be parallel planes.

(*b*) The graduated arc or limb must be a plane, and its graduations, as well as those of the vernier. must be exact.

(*c*) The axis must be at the center of the limb, and perpendicular to the plane thereof.

(*d*) The index and horizon glasses must be perpendicular, and the line of sight parallel, to the plane of the limb.

Of these, only the last named ordinarily require the attention of the navigator who is to make use of the sextant; the others, which may be called the *permanent adjustments*, should be made before the instrument leaves the hands of the maker, and with careful use will never be deranged.

245. The *Adjustment of the Index Mirror* consists in making the reflecting surface of this mirror truly perpendicular to the plane of the sextant. In order to test this, set the index near the middle of the arc, then, placing the eye very nearly in the plane of the sextant and close to the index mirror, observe whether the direct image of the arc and its image reflected from the mirror appear to form one continuous arc; if so, the glass is perpendicular to the plane of the sextant; if the reflected image appears to droop from the arc seen directly, the glass leans backward; if it seems to rise, the glass leans forward. The adjustment is made by the screws at the back of the mirror.

246. The *Adjustment of the Horizon Mirror* consists in making the reflecting surface of this mirror perpendicular to the plane of the sextant. The index mirror having been adjusted, if, in revolving it by means of the index arm, there is found one position in which it is parallel to the horizon glass, then the latter must also be perpendicular to the plane of the sextant. In order to test this, put in the telescope and direct it toward a star; move the index until the reflected image appears to pass the direct image; if one passes directly over the other the mirrors must be parallel; if one passes on either side of the other the horizon glass needs adjustment, which is accomplished by means of the screws attached.

The sea horizon may also be used for making this adjustment. Hold the sextant vertically and bring the direct and the reflected images of the horizon line into coincidence; then incline the sextant until its plane makes but a small angle with the horizon; if the images still coincide the glasses are parallel; if not, the horizon glass needs adjustment.

247. The *Adjustment of the Telescope* must be so made that, in measuring angular distances, the line of sight, or axis of the telescope, shall be parallel to the plane of the instrument, as a deviation in that respect, in measuring large angles, will occasion a considerable error. To avoid such error, a telescope is employed in which are placed two wires, parallel to each other and equidistant from the center of the telescope; by means of these wires the adjustment may be made. Screw on the telescope, and turn the tube containing the eyeglass till the wires are parallel to the plane of the instrument; then select two clearly-defined objects whose angular distance must be not less than 90°, because an error is more easily discovered when the distance is great; bring the reflected image of one object into exact coincidence with the direct image of the other at the inner wire; then, by altering slightly the position of the instrument, make the objects appear on the other wire; if the contact still remains perfect, the axis of the telescope is in its right situation; but if the two objects appear to separate or lap over at the outer wire the telescope is not parallel, and it must be rectified by turning one of the two screws of the ring into which the telescope is screwed, having previously unturned the other screw; by repeating this operation a few times the contact will be precisely the same at both wires, and the axis of the telescope will be parallel to the plane of the instrument.

Another method of making this adjustment is to place the sextant upon a table in a horizontal position, look along the plane of the limb, and make a mark upon a wall, or other vertical surface, at a distance of about 20 feet; draw another mark above the first at a distance equal to the height of the axis of the telescope above the plane of the limb; then so adjust the telescope that the upper mark, as viewed through the telescope, falls midway between the wires. Some sextants are accompanied by small sights whose height is exactly equal to the distance between the telescope and the plane of the limb; by the use of these, the necessity for employing the second mark is avoided and the adjustment can be very accurately made.

248. The errors which arise from defects in what have been denominated the *permanent adjustments* of the sextant may be divided into three classes, namely: Errors due to faulty centering of the axis, called *eccentricity;* errors of graduation; and errors arising from lack of parallelism of surfaces in index mirror and in shade glasses.

The errors due to eccentricity and faulty graduation are constant for the same angle, and should be determined once for all at some place where proper facilities for doing the work are at hand; these errors can only be ascertained by measuring known angles with the sextant. If angles of 10°, 20°, 30°, 40°, etc., are first laid off with a theodolite or similar instrument and then measured by the sextant, a table of errors of the sextant due to eccentricity and faulty graduation may be made, and the error at any intermediate angle found by interpolation; this table will include the error of graduation of the theodolite and also the error due to inaccurate reading of the sextant, but such errors are small. Another method for determining the combined errors of eccentricity and graduation is by measuring the angular distance between stars and comparing the observed and the computed arc between them, but this process is liable to inaccuracies by reason of the uncertainty of allowances for atmospheric refraction.

Errors of graduation, when large, may be detected by "stepping off" distances on the graduated arc with the vernier; place the zero of the vernier in exact coincidence with a division of the arc, and observe whether the final division of the vernier also coincides with a division of the arc; this should be tried at numerous positions of the graduated limb, and the agreement ought to be perfect in every case.

The error due to a prismatic index mirror may be found by measuring a certain unchangeable angle, then taking out the glass and turning the upper edge down, and measuring the angle again; half the difference of these two measures will be the error at that angle due to the mirror. From a number of measures of angles in this manner, a table similar to the one for eccentricity and faulty graduation can be made; or the two tables may be combined. When possible to avoid it, however, no sextant should be used in which there is an index mirror which produces a greater error than that due to the probable error of reading the scale. Mirrors having a greater angle than 2″ between their faces are rejected for use in the United States Navy. Index mirrors may be roughly tested by noting if there is an elongated image of a well-defined point at large angles.

Since the error due to a prismatic horizon mirror is included in the index correction (art. 249), and consequently applied alike to all angles, it may be neglected.

Errors due to prismatic shade glasses can be determined by measuring angles with and without the shade glasses and noting the difference. They may also be determined, where the glasses are so arranged that they can be turned through an angle of 180°, by measuring the angle first with the glass in its usual position and then reversed, and taking the mean of the two as the true measure.

249. Index Error.—The *Index Error* of a sextant is the error of its indications due to the fact that when the index and horizon mirrors are parallel the zero of the vernier does not coincide with the zero of the scale. Having made the adjustments of the index and horizon mirrors and of the telescope, as previously described, it is necessary to find that point of the arc at which the zero of the vernier falls when the two mirrors are parallel, for all angles measured by the sextant are reckoned from that point. If this point is to the left of the zero of the limb, all readings will be too great; if to the right of the zero, all readings will be too small.

If desirable that the reading should be zero when the mirrors are parallel, place the zero of the vernier on zero of the arc; then, by means of the adjusting screws of the horizon glass, move that glass until the direct and reflected images of the same object coincide, after which the perpendicularity of the horizon glass should again be verified, as it may have been deranged by the operation. This adjustment is not essential, since the correction may readily be determined and applied to the reading. In certain sextant work, however, such as surveying, it will be very convenient to be relieved of the

necessity of correcting each angle observed. The sextant should never be relied upon for maintaining a constant index correction, and the error should be ascertained frequently. It is a good practice to verify the correction each time a sight is taken.

250. The *Index Correction* may be found (*a*) by a star, (*b*) by the sea horizon, and (*c*) by the sun.

(*a*) Bring the direct and reflected images of a star into coincidence, and read off the arc. The index correction is numerically equal to this reading, and is positive or negative according as the reading is on the right or left of the zero.

(*b*) The same method may be employed, substituting for a star the sea horizon, though this will be found somewhat less accurate.

(*c*) Measure the apparent diameter of the sun by first bringing the upper limb of the reflected image to touch the lower limb of the direct image, and then bringing the lower limb of the reflected image to touch the upper limb of the direct image.

Denote the readings in the two cases by r and r'; then, if S = apparent diameter of the sun, and R = the reading of the sextant when the two images are in coincidence, we have:

$$r = \mathrm{R} + \mathrm{S},$$
$$r' = \mathrm{R} - \mathrm{S},$$
$$\mathrm{R} = \tfrac{1}{2}(r + r').$$

As R represents the *error*, the *correction* will be − R. Hence the rule: Mark the readings when *on* the arc with the *negative* sign; when *off*, with the *positive* sign; then the index correction is one-half the algebraic sum of the two readings.

Example: The sun's diameter is measured for index correction as follows: On the arc, 31′ 20″; off the arc, 33′ 10″. Required the correction.

On the arc,	− 31′ 20″
Off the arc,	+ 33 10
2)	+ 1 50
I. C.,	+ 0 55

251. From the equations previously given, it is seen that:

$$\mathrm{S} = \tfrac{1}{2}(r - r');$$

hence, if the observations are correct, it will be found that the sun's semidiameter, as given in the Nautical Almanac for the day of observation, is equal to one-half the algebraic difference of the readings. If required to obtain the index correction with great precision, several observations should be taken and the mean used, the accuracy being verified by comparing the tabulated with the observed semidiameter. If the sun is low, the horizontal semidiameter should be observed, to prevent the error that may arise from unequal refraction.

252. Use of the Sextant.—To measure the angle between any two visible objects, point the telescope toward the lower one, if one is above the other, or toward the left-hand one, if they are in nearly the same horizontal plane. Keep this object in direct view through the unsilvered part of the horizon glass, and move the index arm until the image of the other object is seen by a double reflection from the index mirror and the silvered portion of the horizon glass. Having gotten the direct image of one object into nearly exact contact with the reflected image of the other, clamp the index arm and, by means of the tangent-screw, complete the adjustment so that the contact may be perfect; then read the limb.

In measuring the altitude of a celestial body above the sea horizon, it is necessary that the angle shall be measured to that point of the horizon which lies vertically beneath the object. To determine this point, the observer should move the instrument slightly to the right and left of the vertical, swinging it about the line of sight as an axis, taking care to keep the object in the middle of the field of view. The object will appear to describe the arc of a circle, and the lowest point of this arc marks the true vertical.

The shade-glasses should be employed as may be necessary to protect the eye when observing objects of dazzling brightness, such as the sun, or the horizon when the sun is reflected from it at a low altitude. Care must be taken that the images are not too bright or the eye will be so affected as to interfere with the accuracy of the observations.

253. Choice of Sextants.—The choice of a sextant should be governed by the kind of work which is required to be done. In rough work, such as surveying, where angles need only be measured to the nearest 30″ the radius may be as small as 6 inches, which will permit easy reading, and the instrument can be correspondingly lightened. Where readings to 10″ are desired, as in nice astronomical work, the radius should be about 7½ inches, and the instrument, to be strongly built, should weigh about 3½ pounds.

The parts of an instrument should move freely, without binding or gritting. The eyepieces should move easily in the telescope tubes; the bracket for carrying the telescope should be made very strong. It is frequently found that the parallelism of the line of sight is destroyed in focusing the eyepiece, either on account of the looseness of the fit or because of the telescope bracket being weak. The vernier should lie close to the limbs to prevent parallax in reading. If it is either too loose or too tight at either extremity of its travel, it may indicate that the pivot is not perpendicular. The balls of the tangent-screw should fit snugly in their sockets, so that there may be no lost motion.

Where possible, the sextant should always be submitted to expert examination and test as to the accuracy of its permanent adjustments before acceptance by the navigator.

254. Resilvering Mirrors.—Occasion may sometimes arise for resilvering the mirrors of a sextant, as they are always liable to be damaged by dampness or other causes. For this purpose some

clean tin foil and mercury are required. Upon a piece of glass about 4 inches square lay a piece of tin foil whose dimensions exceed by about a quarter of an inch in each direction those of the glass to be silvered; smooth out the foil carefully by rubbing; put a small drop of mercury on the foil and spread it with the finger over the entire surface, being careful that none shall find its way under the foil; then put on a few more drops of mercury until the whole surface is fluid. The glass which is to be silvered having been carefully cleaned, it should be laid upon a piece of tissue paper whose edge just covers the edge of the foil and transferred carefully from the paper to the tin foil, a gentle pressure being kept upon the glass to avoid the formation of bubbles; finally, place the mirror face downward and leave it in an inclined position to allow the surplus mercury to flow off, the latter operation being hastened by a strip of tin foil at its lower edge. After five or six hours the tin foil around the edges may be removed, and the next day a coat of varnish made from spirits of wine and red sealing wax should be applied. For a horizon mirror care must be taken to avoid silvering the plain half. The mercury drawn from the foil should not be placed with clean mercury with a view to use in the artificial horizon or the whole will be spoiled.

255. Octants and Quintants.—Properly speaking, a sextant is an instrument whose arc covers one-sixth of a complete circle, and which is therefore capable of measuring an angle of 120°. Other instruments are made which are identical in principle with the sextant as heretofore described, and which differ from that instrument only in the length of the arc. These are the *octant*, an eighth of a circle, by which angles may be measured to 90°, and the *quintant*, a fifth of a circle, which measures angles up to 144°. The distinction between these instruments is not always carefully made, and in such matters as have been touched upon in the foregoing articles the sextant may be regarded as the type of all kindred reflecting instruments.

THE ARTIFICIAL HORIZON.

256. The *Artificial Horizon* is a small, rectangular, shallow basin of mercury, over which, to protect the mercury from agitation by the wind, is placed a roof consisting of two plates of glass at right angles to each other. The mercury affords a perfectly horizontal surface which is at the same time an excellent mirror. The different parts of an artificial horizon are furnished in a compact form, a metal bottle being provided for containing the mercury when not in use, together with a suitable funnel for pouring.

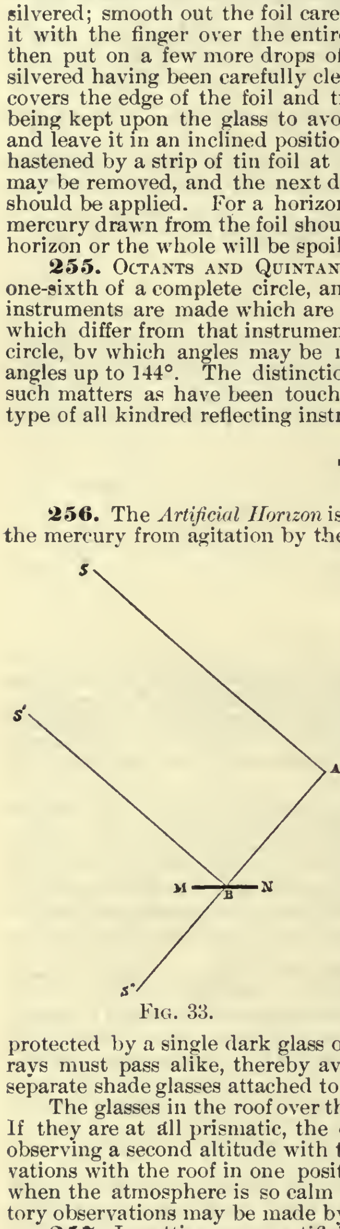

Fig. 33.

If MN, in figure 33, is the horizontal surface of the mercury; S′B a ray of light from a celestial object, incident to the surface at B; BA the reflected ray; then an observer at A will receive the ray BA as if it proceeded from a point S″, whose angular depression, MBS″, below the horizontal plane is equal to the altitude, MBS′, of the object above that plane. If, then, SA is a direct ray from the object parallel to S′B, an observer at A can measure with the sextant the angle SAS″= S′BS″= 2 S′BM, by bringing the image of the object reflected by the index mirror into coincidence with the image S″ reflected by the mercury and seen through the horizon glass. The instrumental measure, corrected for index error, will be double the apparent altitude of the body.

The sun's altitude will be measured by bringing the lower limb of one image to touch the upper limb of the other. Half the corrected instrumental reading will be the apparent altitude of the sun's *lower* or *upper* limb, according as the lower or upper limb of the *reflected* image was the one employed in the observation.

In observations of the sun with the artificial horizon, the eye is protected by a single dark glass over the eyepiece of the telescope through which direct and reflected rays must pass alike, thereby avoiding the errors that might possibly arise from a difference in the separate shade glasses attached to the frame of the sextant.

The glasses in the roof over the mercury should be made of plate-glass, with perfectly parallel faces. If they are at all prismatic, the observed altitude will be erroneous. The error may be removed by observing a second altitude with the roof reversed, and, in general, by taking one half of a set of observations with the roof in one position and the other half with the roof reversed. On the rare occasions when the atmosphere is so calm that the unsheltered mercury will remain undisturbed, most satisfactory observations may be made by leaving off the roof.

257. In setting up an artificial horizon, care should be taken that the basin is free from dust and other foreign matter, as small particles floating upon the surface of the mercury interfere with a perfect reflection. The basin should be so placed that its longer edge lies in the direction in which the observed body will bear at the middle of the observations. The spot selected for taking the sights should be as free as possible from causes which will produce vibration of the mercury, and precautions should be taken to shelter the horizon from the wind, as the mere placing of the roof will not ordinarily be sufficient to accomplish this. Embedding the roof in earth serves to keep out the wind, while setting the whole horizon upon a thick towel or a piece of such material as heavy felt usually affords ample protection from wind, tends to reduce the vibrations from mechanical shocks, and also aids in keeping out the moisture from the ground. In damp climates the roof should be kept dry by wiping, or the moisture deposited from the inclosed air will form a cloud upon the glass.

Molasses, oil, or other viscous fluid may, when necessary, be employed as a substitute for mercury.

258. Owing to the perfection of manufacture that is required to insure accuracy of results with the artificial horizon, navigators are advised to accept only such instrument as has satisfactorily stood the necessary tests to prove the correctness of its adjustment as regards the glasses of the roof.

THE CHRONOMETER.

259. The *Chronometer* is simply a correct time-measurer, differing from an ordinary watch in having the force of its main-spring rendered uniform by means of a variable lever. Owing to the fact that on a sea voyage a chronometer is exposed to many changes of temperature, it is furnished with an expansion balance, formed of a combination of metals of different expansive qualities, which produces the required compensation. In order that its working may not be deranged by the motion of the ship in a seaway, the instrument is carried in gimbals.

As the regularity of the chronometer is essential for the correct determination of a ship's position, it is of the greatest importance that every precaution be taken to insure the accuracy of its indications. There is no more certain way of doing this than to provide a vessel with several of these instruments—preferably not less than three—in order that if an irregularity develop in one, the fact may be revealed by the others.

260. Care of Chronometers on Shipboard.—The box in which the chronometers are kept should have a permanent place as near as practicable to the center of motion of the ship, and where it will be free from excessive shocks and jars, such as those that arise from the engines or from the firing of heavy guns; the location should be one free from sudden and extreme changes of temperature, and as far removed as possible from masses of vertical iron. The box should contain a separate compartment for each chronometer, and each compartment should be lined with baize cloth padded with curled hair, for the double purpose of reducing shocks and equalizing the temperature within. An outer cover of baize cloth should be provided for the box, and this should be changed or dried out frequently in damp weather. The chronometers should all be placed with the XII mark in the same position.

For transportation for short distances by hand, an instrument should be rigidly clamped in its gimbals, for if left free to swing, its performance may be deranged by the violent oscillations that are imparted to it.

For transportation for a considerable distance, as by express, the chronometer should be allowed to run down, and should then be dismounted and the balance corked.

261. Since it is not possible to make a perfect instrument which will be uninfluenced by the disturbing causes incident to a sea voyage, it becomes the duty of the navigator to determine the *error* and to keep watch upon the variable *rate* of the chronometer.

The *error of the chronometer* is the difference between the time indicated and the standard time to which it is referred—usually Greenwich mean time.

The amount the chronometer *gains* or *loses* daily is the *daily rate.*

The indications of a chronometer at any given instant require a correction for the accumulated error to that instant; and this can be found if the error at any given time, together with the daily rate, are known.

262. Winding.—Chronometers are ordinarily constructed to run for 56 hours without rewinding, and an indicator on the face always shows how many hours have elapsed since the last winding. To insure a uniform rate, they must be wound regularly every day, and, in order to avoid the serious consequences of their running down, the navigator should take some means to guard against neglecting this duty through a fault of memory. To wind, turn the chronometer gently on its side, enter the key in its hole and push it home, steadying the instrument with the hand, and wind to the left, the last half turn being made so as to bring up gently against the stop. After winding, cover the keyhole and return the instrument to its natural position. Chronometers should always be wound in the same order to prevent omissions, and the precaution taken to inspect the indicators, as a further assurance of the proper performance of the operation.

After winding each day, the comparisons should be made, and, with the readings of the maximum-and-minimum thermometer and other necessary data, recorded in a book kept for the purpose.

The maximum-and-minimum thermometer is one so arranged that its highest and lowest readings are marked by small steel indices that remain in place until reset. Every chronometer box should be provided with such an instrument, as a knowledge of the temperature to which chronometers have been subjected is essential in any analysis of the rate. To draw down the indices for the purpose of resetting, a magnet is used. This magnet should be kept at all times at a distance from the chronometers.

263. Comparison of Chronometers.—The instrument believed to be the best is regarded as the *Standard,* and each other is compared with it. It is usual to designate the Standard as A, and the others as B, C, etc. Chronometers are made to beat half-seconds, and any two may be compared by following the beat of one with the ear and of the other with the eye.

To make a comparison, say of A and B, open the boxes of these two instruments and close all others. Get the cadence and, commencing when A has just completed the beat of some even 5-second division of the dial, count "half-one-half-two-half-three-half-four-half-five," glancing at B in time to note the position of its second-hand at the last count; the seconds indicated by A will be five greater than the number at the beginning of the count. The hours and minutes are also recorded for each chronometer, and the subtraction made. A good check upon the accuracy is afforded by repeating the operation, taking the tick from B.

Where necessary for exact work, it is possible to estimate the fraction between beats, and thus make the comparison to tenths of a second; but the nearest half-second is sufficiently exact for the purposes of ordinary navigation at sea.

264. The following form represents a convenient method of recording comparisons:

STAND. A, No. 777. CHRO. B, No. 1509. CHRO. C, No. 1802.

Date, 1903.	Designation of comparisons.	Chro. B with Stand. A.	2d diff.	Chro. C with Stand. A.	2d diff.	Therm.			Bar.	Remarks.
						Max.	Min.	Air.		
		h. m. s.	s.	h. m. s.	s.	°	°	°	″	
January 1	Stand. A. B and C.	1 13 40 1 12 21.5		1 14 20 2 04 11		63	59	60	30.07	Found errors by time-ball.
	Difference.	1 18.5	—	11 10 09	—					
2	Stand. A. B and C.	1 16 30 1 15 10		1 17 00 2 06 51.5		64	58	57	30.12	Left New York for San Juan, P. R.
	Difference.	1 20	+1.5	11 10 08.5	−0.5					

265. The *second difference* in the form is the difference between the comparisons of the same instruments for two successive days. When a vessel is equipped with only one chronometer there is nothing to indicate any irregularity that it may develop at sea—and even the best instruments may undergo changes from no apparent cause. When there are two chronometers, the second difference, which is equal to the algebraic difference between their daily rates, remains uniform as long as the rates remain uniform, but changes if one of the rates undergoes a change; in such a case, there is no means of knowing which chronometer has departed from its expected performance, and the navigator must proceed with caution, giving due faith to the indications of each. If, however, there are three chronometers, an irregularity on the part of one is at once located by a comparison of the second differences. Thus, if the predicted rates of the chronometers were such as to give for the second difference of A − B, $+1^s.5$, and of A − C, $-0^s.5$, suppose on a certain day those differences were $+4^s.5$ and $-0^s.5$, respectively; it would at once be suspected that the irregularity was in B, and that that chronometer had lost 3^s on its normal rate during the preceding day. Suppose, however, the second differences were $+4^s.5$ and $+2^s.5$; it would then be apparent that A had gained 3^s.

266. TEMPERATURE CURVES.—Notwithstanding the care taken to eliminate the effect of a change of temperature upon the rate of a chronometer, it is rare that an absolutely perfect compensation is attained, and it may therefore be assumed that the rates of all chronometers vary somewhat with the temperature. Where the voyage of a vessel is a long one and marked changes of climate are encountered, the accumulated error from the use of an incorrect rate may be very material, amounting to several minutes' difference of longitude. Careful navigators will therefore take every means to guard against such an error. By the employment of a *temperature curve* in connection with the chronometer rate the most satisfactory results are arrived at.

267. There should be furnished with each chronometer a statement showing its daily rate under various conditions of temperature; and this may be supplemented by the observations of the navigator during the time that the chronometer remains on board ship. With all available data a temperature curve should be constructed which will indicate graphically the performance of the instrument. It is most convenient to employ for this purpose a piece of "profile paper," on which parallel lines are ruled at equal intervals at right angles to each other. Let each horizontal line represent, say, a degree of temperature, numbered at the left edge, from the bottom up; draw a vertical line in red ink to represent the zero rate, and let all rates to the right be *plus*, or gaining, and those to the left *minus*, or losing; let the intervals between vertical lines represent intervals of rate (as one-tenth of a second) numbered at the top from the zero rate; then on this scale plot the rate corresponding to each temperature; when there are several observations covering one height of the thermometer, the mean may be used. Through all the plotted points draw a fair curve, and the intersection of this curve with each temperature line gives the mean rate at that temperature. The mean temperature given by the maximum and minimum thermometer shows the rate to be used on any day.

268. HACK OR COMPARING WATCH.—In order to avoid derangement, the chronometers should never be removed from the permanent box in which they are kept on shipboard. When it is desired to mark a certain instant of time, as for an astronomical observation or for obtaining the chronometer error by signal, the time is marked by a "hack" (an inferior chronometer used for this purpose only), or by a comparing watch. Careful comparisons are taken—preferably both before and afterwards—and the chronometer time at the required instant is thus deduced. The correction represented by the chronometer time *minus* the watch time (twelve hours being added to the former when necessary to make the subtraction possible) is referred to as C − W.

Suppose, for example, the chronometer and watch are compared and their indications are as follows:

$$
\begin{array}{ll}
\text{Chro. t.,} & 5^h\ 27^m\ 30^s \\
\text{W. T.,} & -2\ \ 36\ \ 45.5 \\
\hline
\text{C} - \text{W,} & \ \ 2\ \ 50\ \ 44.5
\end{array}
$$

If then a sight is taken when the watch shows $3^h\ 01^m\ 27^s.5$, we have:

$$
\begin{array}{ll}
\text{W. T.,} & 3^h\ 01^m\ 27^s.5 \\
\text{C} - \text{W,} & +2\ \ 50\ \ 44.5 \\
\hline
\text{Chro. t.,} & \ \ 5\ \ 52\ \ 12.0
\end{array}
$$

It may occur that the values of C — W, as obtained from comparisons before and after marking the desired time, will vary; in that case the value to be used will be the mean of the two, if the time marked is about midway between comparisons, but if much nearer to one comparison than the other, allowance should be made accordingly.

Thus suppose, in the case previously given, a second comparison had been taken after the sight as follows:

Chro. t.,	$6^h\ 12^m\ 45^s$
W. T.,	$-3\ \ 21\ \ 59.5$
C — W,	$2\ \ 50\ \ 45.5$

The sight having been taken at about the middle of the interval, the C — W to be used would be the mean of the two, or $2^h\ 50^m\ 45^s.0$.

Let us assume, however, that the second comparison showed the following:

Chro. t.,	$6^h\ 38^m\ 25^s$
W. T.,	$-3\ \ 47\ \ 39$
C — W,	$2\ \ 50\ \ 46$

Then, the sight having been taken when only about one-third of the interval had elapsed between the first and second comparisons, it would be assumed that only one-third of the total change in the C — W had occurred up to the time of sight, and the value to be used would be $2^h\ 50^m\ 45^s.0$.

269. It is considered a good practice always to subtract watch time from chronometer time whatever the relative values, and thus to employ C — W invariably as an additive correction. It is equally correct to take the other difference, W — C, and make it subtractive; it may sometimes occur that a few figures will thus be saved, but a chance for error arises from the possibility of inadvertently using the wrong sign, which is almost impossible by the other method. Thus, the following example may be taken:

Comparison	C,	$10^h\ 57^m\ 38^s$	W,	$11^h\ 42^m\ 35^s$
	W,	$-11\ \ 42\ \ 35$	C,	$-10\ \ 57\ \ 38$
	C — W,	$11\ \ 15\ \ 03$	W — C,	$0\ \ 44\ \ 57$
Sight	W,	$11\ \ 50\ \ 21$	W,	$11\ \ 50\ \ 21$
	C — W,	$+11\ \ 15\ \ 03$	W — C,	$-\ 0\ \ 44\ \ 57$
	C,	$11\ \ 05\ \ 24$	C,	$11\ \ 05\ \ 24$

CHAPTER IX.

TIME AND THE NAUTICAL ALMANAC.

270. The subjects of *Time* and the *Nautical Almanac* are two of the most important ones to be mastered in the study of Nautical Astronomy, as they enter into every operation for the astronomical determination of a ship's position. They will be treated in conjunction, as the two are interdependent.

METHODS OF RECKONING TIME.

271. The instant at which any point of the celestial sphere is on the meridian of an observer is termed the *transit, culmination,* or *meridian passage* of that point; when on that half of the meridian which contains the zenith, it is designated as *superior* or *upper* transit; when on the half containing the nadir, as *inferior* or *lower* transit.

272. Three different kinds of time are employed in astronomy—(*a*) *apparent* or *solar time,* (*b*) *mean time,* and (*c*) *sidereal time.* These depend upon the hour angle from the meridian of the points to which they respectively refer. The point of reference for apparent or solar time is the *Center of the Sun;* for mean time, an imaginary point called the *Mean Sun;* and for sidereal time, the *Vernal Equinox,* also called the *First Point of Aries.*

The unit of time is the *Day,* which is the period between two successive transits over the same branch of the meridian of the point of reference. The day is divided into 24 equal parts, called *Hours;* these into 60 equal parts, called *Minutes,* and these into 60 equal parts, called *Seconds.*

273. Apparent or Solar Time.—The hour angle of the center of the sun affords a measure of *Apparent* or *Solar Time.* An *Apparent* or *Solar Day* is the interval of time between two successive transits over the same meridian of the center of the sun. It is *Apparent Noon* when the sun's hour circle coincides with the celestial meridian. This is the most natural and direct measure of time, and the unit of time adopted by the navigator at sea is the apparent solar day. Apparent noon is the time when the latitude can be most readily determined, and the ordinary method of determining the longitude by the sun involves a calculation to deduce the apparent time first.

Since, however, the intervals between the successive returns of the sun to the same meridian are not equal, apparent time can not be taken as a standard. The apparent day varies in length from two causes: first, the sun does not move in the equator, the great circle perpendicular to the axis of rotation of the earth, but in the ecliptic; and, secondly, the sun's motion in the ecliptic is not uniform. Sometimes the sun describes an arc of 57′ of the ecliptic, and sometimes an arc of 61′ in a day. At the points where the ecliptic and equinoctial intersect, the direction of the sun's apparent motion is inclined at an angle of 23° 27′ to the equator, while at the solstices it moves in a direction parallel to the equator.

274. Mean Time.—To avoid the irregularity of time caused by the want of uniformity in the sun's motion, a fictitious sun, called the *Mean Sun,* is supposed to move in the *equinoctial* with a uniform velocity that equals the *mean velocity of the true sun in the ecliptic.* This mean sun is regarded as being in coincidence with the true sun at the vernal equinox, or First Point of Aries.

Mean Time is the hour angle of the mean sun. A *Mean Day* is the interval between two successive transits of the mean sun over the meridian. *Mean Noon* is the instant when the mean sun's hour circle coincides with the meridian.

Mean time lapses uniformly; at certain times it agrees with apparent time, while sometimes it is behind, and at other times in advance of it. It is this time that is measured by the clocks in ordinary use, and to this the chronometers used by navigators are regulated.

275. The difference between apparent and mean time is called the *Equation of Time;* by this quantity, the conversion from one to the other of these times may be made. Its magnitude and the direction of its application may be found for any moment from the Nautical Almanac.

276. Sidereal Time.—*Sidereal Time* is the hour angle of the First Point of Aries. This point, which is identical with the vernal equinox, is the origin of all coordinates of right ascension. Since the position of the point is fixed in the celestial sphere and does not, like the sun, moon, and planets, have actual or apparent motion therein, it shares in this respect the properties of the fixed stars. It may therefore be said that intervals of sidereal time are those which are measured by the stars.

A *Sidereal Day* is the interval between two successive transits of the First Point of Aries across the same meridian. *Sidereal Noon* is the instant at which the hour circle of the First Point of Aries coincides with the meridian. In order to interconvert sidereal and mean times an element is tabulated in the Nautical Almanac. This is the *Sidereal Time of Mean Noon,* which is also the *Right Ascension of the Mean Sun.*

277. Civil and Astronomical Time.—The *Civil Day* commences at midnight and comprises the twenty-four hours until the following midnight. The hours are counted from 0 to 12, from midnight to noon; then, again, from 0 to 12, from noon to midnight. Thus the civil day is divided into two periods of twelve hours each, the first of which is marked a. m. (ante meridian), while the last is marked p. m. (post meridian).

The *Astronomical* or *Solar Day* commences at noon of the civil day of the same date. It comprises twenty-four hours, reckoned from 0 to 24, from noon of one day to noon of the next. Astronomical time (apparent or mean) is the hour angle of the sun (true or mean) measured to the westward throughout its entire circuit from the time of its upper transit on one day to the same instant of the next.

The civil day, therefore, begins twelve hours before the astronomical day, and a clear understanding of this fact is all that is required for interconverting these times. For example:

January 9, 2 a. m., civil time, is January 8, 14^h, astronomical time.

January 9, 2 p. m., civil time, is January 9, 2^h, astronomical time.

278. Hour Angle.—The *hour angle* of a heavenly body is the angle at the pole of the celestial concave between the declination circle of the heavenly body and the celestial meridian. It is measured by the arc of the celestial equator between the declination circle and the celestial meridian.

or hour circle

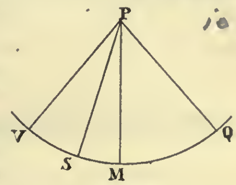

Fig. 34.

In figure 34 let P be the pole of the celestial sphere, of which VMQ is the equator, PQ, the celestial meridian, and PM, PS, PV, the declination circles of the mean sun, a heavenly body, and the First Point of Aries, respectively.

Then QPM, or its arc, QM, is the hour angle of the mean sun, or the mean time; QPS, or QS, the hour angle of the heavenly body; QPV, or QV, the hour angle of the First Point of Aries, or the right ascension of the meridian, both of which are equivalent to the sidereal time; VPS, or VS, the right ascension of the heavenly body; and VPM, or VM, the right ascension of the mean sun.

279. Time at Different Meridians.—The hour angle of the true sun at any meridian is called the *local apparent time;* that of the mean sun, the *local mean time;* that of the First Point of Aries, the *local sidereal time.* The hour angles of the same body and points from Greenwich are respectively the *Greenwich apparent, mean,* and *sidereal times.* The difference between the local time at any meridian and the Greenwich time is equal to the longitude of that place from Greenwich expressed in time; the conversion from time to arc may be effected by a simple mathematical calculation or by the use of Table 7.

In comparing corresponding times of different meridians the most easterly meridian may be distinguished as that at which the time is *greatest* or *latest.*

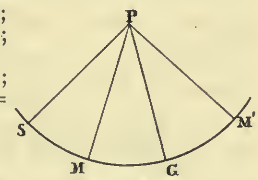

Fig. 35.

In figure 35 PM and PM′ represent the celestial meridians of two places; PS, the declination circle through the sun, and PG, the Greenwich meridian; let T_G = the Greenwich time = GPS;

T_M = the corresponding local time at all places on the meridian PM = MPS;

$T_{M'}$ = the corresponding local time at all places on the meridian PM′ = M′PS;

Lo = west longitude of meridian PM = GPM; and

Lo′ = east longitude of meridian PM′ = GPM′.

If west longitudes and hour angles be reckoned as positive, and east longitudes and hour angles as negative, we have:

$$Lo = T_G - T_M; \text{ and}$$
$$Lo' = T_G - T_{M'}; \text{ therefore,}$$
$$Lo - Lo' = T_{M'} - T_M.$$

Thus it may be seen that the difference of longitude between two places equals the difference of their local times. This relation may be shown to hold for any two meridians whatsoever.

Both local and Greenwich times in the above formulæ must be reckoned westward, always from their respective meridians and from 0^h to 24^h; in other words, it is the astronomical time which should be used in all astronomical computations.

The formula $Lo = T_G - T_M$ is true for any kind of time, solar or sidereal; or, in general terms, T_G and T_M are the hour angles of any point of the sphere at the two meridians whose difference of longitude is Lo. S may be the sun (true or mean) or the vernal equinox.

280. Finding the Greenwich Time.—Since nearly every computation made by the navigator requires a knowledge of the Greenwich date and time as a preliminary to the use of the Nautical Almanac, the first operation necessary is to deduce from the local time the corresponding Greenwich date, either exact or approximate, and thence the Greenwich time expressed astronomically.

The formula is:

$$T_G = T_M + Lo,$$

remembering that west longitudes are positive, east longitudes are negative. Hence the following rule for converting local to Greenwich time:

Having expressed the local time astronomically, *add* the longitude if *west, subtract* it if *east;* the result is the corresponding Greenwich time.

Example: In longitude 81° 15′ W. the local time is, 1879, April, $15^d\ 10^h\ 17^m\ 30^s$ a. m. Required the Greenwich time.

Local Ast. time, April,	14^d	22^h	17^m	30^s
Longitude,	+	5	25	00
Greenwich time,	15	3	42	30

Example: In longitude 81° 15′ E. the local time is, August, $5^d\ 2^h\ 10^m\ 30^s$ p. m. Required the Greenwich time.

Local Ast. time,	5^d	2^h	10^m	30^s
Longitude,	−	5	25	00
Greenwich time,	4	20	45	30

EXAMPLE: In longitude 17° 28′ W. the local time is, May, $1^d\ 3^h\ 10^m$ p. m. Required the Greenwich time.

Local Ast. time,	$1^d\ 3^h\ 10^m\ 00^s$
Longitude,	+ 1 09 52
Greenwich time,	1 4 19 52

EXAMPLE: In longitude 125° 30′ E. the local time is, May, $1^d\ 8^h\ 10^m\ 30^s$ a. m. Required the Greenwich time.

Local Ast. time, April,	$30^d\ 20^h\ 10^m\ 30^s$
Longitude,	− 8 22 00
Greenwich time,	30 11 48 30

281. From the preceding article we have:

$$T_G = T_M + Lo; \text{ hence,}$$
$$T_M = T_G - Lo;$$

thus it will be seen that, to find the local time corresponding to any Greenwich time, the above process is simply reversed.

Since all observations at sea are referred to chronometers regulated to Greenwich mean time, and as these instruments are usually marked on the dial from 0^h to 12^h, it becomes necessary to distinguish whether it is a.m. or p.m. at Greenwich. Therefore, an approximate knowledge of the longitude and local time is necessary to determine the Greenwich date.

EXAMPLE: In longitude $5^h\ 00^m\ 00^s$ W., about $3^h\ 30^m$ p.m. April 15th, the Greenwich chronometer read $8^h\ 25^m$, and was fast of Gr. time $3^m\ 15^s$. Required the local astronomical time.

Aprox. local time,	$15^d\ 3^h\ 30^m$	Gr. chro.,	$8^h\ 25^m\ 00^s$	Gr. Ast. time 15^d,	$8^h\ 21^m\ 45$
Longitude,	+ 5 00	Corr.,	− 3 15	Longitude,	−5 00 00
Approx. Gr. time,	15 8 30	Gr. Ast. time 15^d,	8 21 45	Local Ast. time 15^d,	3 21 45

EXAMPLE: In longitude $5^h\ 00^m\ 00^s$ E., about 8 a. m. May 3d, the Gr. chro. read $3^h\ 15^m\ 20^s$, and was fast of Gr. time $3^m\ 15^s$. Required the local astronomical time.

Approx. local time, May,	$2^d\ 20^h$	Gr. chro.,	$3^h\ 15^m\ 20^s$	Gr. Ast. time 2^d,	$15^h\ 12^m\ 05$
Longitude,	− 5	Corr.,	− 3 15	Longitude,	+ 5 00 00
Approx. Gr. time,	2 15	Gr. Ast. time 2^d,	15 12 05	Local Ast. time 2^d,	20 12 05

THE NAUTICAL ALMANAC.[a]

282. *The American Ephemeris and Nautical Almanac* is divided into four parts, as follows: Part I, Ephemeris for the meridian of Greenwich, gives the ephemerides of the sun and moon, the geocentric and heliocentric positions of the major planets, the sun's coordinates, and other fundamental astronomical data for equidistant intervals of Greenwich mean time; Part II, Ephemeris for the meridian of Washington, gives the ephemerides of the fixed stars, sun, moon, and major planets for transit over the meridian of Washington; Part III, Phenomena, contains predictions of phenomena to be observed, with data for their computation; and Part IV, Star Numbers and other data, contains matter relating to certain fixed stars. Tables are also appended for the interconversion of mean and sidereal time and for finding the latitude by an altitude of Polaris.

The American Nautical Almanac is a smaller book made up of extracts from the "Ephemeris and Almanac" just described, and is designed especially for the use of navigators, being adapted to the meridian of Greenwich. It contains the positions of the sun and moon, the distances of the moon from the center of the sun, from the centers of the four most conspicuous planets, and from certain fixed stars, together with the ephemerides of the planets Mercury, Venus, Mars, Jupiter, and Saturn, and the mean places of 150 fixed stars; solar and lunar eclipses are described, and the tables for the interconversion of mean and sidereal time and for finding the latitude by Polaris are included.

The elements dependent upon the sun and moon are placed at the beginning of the book, arranged according to the months of the year; eighteen pages are devoted to each month, numbered in Roman notation from I to XVIII. Of these, page I contains the Apparent Right Ascension and Declination of the sun and the Equation of Time for the instant of Greenwich *apparent* noon; throughout the remaining seventeen pages Greenwich *mean* time forms the basis of reckoning. Page I is used in computations from observations that depend upon the time of the sun's meridian passage, at which instant the local apparent time is 0^h, and the Greenwich apparent time is equal to the longitude, if west, or to 24^h *minus* the longitude, if east; this page therefore affords a means for reducing the elements for such observations from a knowledge of the longitude alone. In all other observations the calculation is made for some definite instant of Greenwich *mean* time (usually as noted by the chronometer), in which case Pages II to XVIII are employed.

283. REDUCTION OF ELEMENTS.—The reduction of elements in the Nautical Almanac is usually accomplished by *Interpolation*, but in certain cases where extreme precision is necessary the method of *Second Differences* must be used.

[a] See extracts from Ephemeris and Nautical Almanac for 1879, Appendix I.

The Ephemeris, being computed for the Greenwich meridian, contains the right ascensions, declinations, equations of time, and other elements for given equidistant intervals of Greenwich time. Hence, before the value of any of these quantities can be found for a given local time it is necessary to determine the corresponding Greenwich time. Should that time be one for which the Nautical Almanac gives the value of the required element, nothing more is necessary than to employ that value. But if the time falls between the Almanac times, the required quantity must be found by interpolation.

The Almanac contains the rate of change or difference of each of the principal quantities for some unit of time, and, unless great precision is required, the first differences only need be regarded. In order to use the difference columns to advantage, the Greenwich date should be expressed in the unit of time for which the difference is given. Thus, for using the hourly differences, the Greenwich time should be expressed in hours and decimal parts of an hour; when using the differences for one minute, the time should be in minutes and decimal parts of a minute. Instead of using decimal parts, some may prefer the use of aliquot parts.

Since the quantities in the Almanac are approximate numbers, given to a certain decimal, any interpolation of a lower order than that decimal is unnecessary work. Moreover, since, in computations at sea, the Greenwich time is more or less inexact, too great refinement need not be sought in reducing the Almanac elements.

Simple interpolation assumes that the differences of the quantities are proportional to the differences of the times; in other words, that the differences given in the Almanac are constant; this is seldom the case, but the error arising from the assumption will be smaller the less the interval between the times in the Almanac. Hence those quantities which vary most irregularly are given for the smallest units of time; as the variations are more regular, the units for which the differences are given increase.

In taking from the Almanac the elements relating to the fixed stars the data may be found either in the table which gives the "mean place" of each star for the year or in that which gives the "apparent place" occupied by each one on every tenth day throughout the year. As the annual variation of position of the fixed stars is small, the results will not vary greatly whichever table may be used. Yet, as it is proper to seek always the greatest attainable accuracy, the use of the table showing the exact positions is recommended. That table is, however, published in the "Ephemeris and Nautical Almanac" only, and is omitted from the abridged "Nautical Almanac;" hence, where the larger book is not at hand, the table of mean places must be employed.

284. To find from the Nautical Almanac a required element for any given time and place, it is first necessary to express the time astronomically and to convert it to Greenwich time and date. Then take from the Almanac, for the nearest given *preceding* instant, the required quantity, together with its corresponding "Diff. for 1^h" or "Diff. for 1^m," noting the name or sign in each case; for the sun use Page I of the proper month in the Almanac when *apparent* time is to be the basis for correction, but otherwise use Page II. Multiply the "Diff. for 1^h" by the number of hours and fraction of an hour, or the "Diff. for 1^m" by the number of minutes and fraction of a minute, corresponding to the interval between the time for which the quantity is given in the Almanac and the time for which required; apply the correction thus obtained, having regard to its sign.

A modification of this rule may be adopted if the time for which the quantity is desired falls considerably nearer a *subsequent* time given in the Almanac than it does to one preceding; in this case the interpolation may be made backward, the sign of application of the correction being reversed.

EXAMPLE: At a place in longitude 81° 15′ W., April 17, 1879, find the sun's declination and the equation of time at apparent noon.

Long. $=81° 15'$ W. G. A. T. $= 17^d\ 5^h\ 25^m = 17^d + 5^h.42$.

Dec., $17^d\ 0^h$,	(+)	10° 26′ 42″.3 N.	Eq. t., $17^d\ 0^h$,		$0^m\ 24^s.46$
Corr.,	+	4 46 .2	Corr.,	+	3 .18
Dec., $17^d\ 5^h\ 25^m$,		10 31 28 .5 N.	Eq. t., $17^d\ 5^h\ 25^m$,		0 27 .64
H. D.,	+	52″.80	H. D.,	+	$0^s.587$
G. A. T.,	+	$5^h.42$	G. A. T.,	+	$5^h.42$
Corr.,	+	286″.18 / 4′46″.18	Corr.,	+	$3^s.182$
			(*Subtract* from *apparent* time.)		

EXAMPLE: At a place in Long. 81° 15′ E., April 17, 1879, find the sun's declination and the equation of time at apparent noon.

Long. $=81° 15'$ E. G. A. T. $= 16^d\ 18^h\ 35^m = 17^d - 5^h.42$.

Dec., $17^d\ 0^h$,	(+)	10° 26′ 42″.3 N.	Eq. t., $17^d\ 0^h$,		$0^m\ 24^s.46$
Corr.,	—	4 46 .2	Corr.,	—	3 .18
Dec., $16^d\ 18^h\ 35^m$,		10 21 56 .1 N.	Eq. t., $16^d\ 18^h\ 35^m$,		0 21 .28
H. D.,	+	52″.80	H. D.,	+	$0^s.587$
G. A. T.,	—	$5^h.42$	G. A. T.,	—	$5^h.42$
Corr.,	—	286″.18 / 4′ 46″.18	Corr.,	—	$3^s.182$

EXAMPLE: April 16, 1879, at $11^h\ 55^m\ 30^s$ a. m., local mean time, in Long. 81° 15′ W., required the declination and semidiameter of the sun, the equation of time, and the right ascension, declination, horizontal parallax, and semidiameter of the moon and Jupiter.

Local mean time,		$15^d\ 23^h\ 55^m\ 30^s$
Longitude,	+	$5^h\ 25^m\ 00^s$
Greenwich mean time,		$16^d\ 5^h\ 20^m\ 30^s$
		$16^d\ 5^h\ 20^m.5$
		$16^d\ 5^h.34$

For the Sun.

Dec., 0^h,	(+)	10° 05′ 30″. 1 N.	S. D., 15′ 58″. 0	Eq. t., 0^h,		$0^m\ 10^s.15$
Corr.,	+	4 44 . 3	(Same as at G. A. Noon.)	Corr.,	+	3 . 22
Dec.,		10 10 14 . 4 N.		Eq. t.,		0 13 . 37
H. D.,	+	53″. 24		H. D.,	+	0^s. 604
G. M. T.,	+	5^h. 34		G. M. T.,	+	5^h. 34
Corr.,	+	284″. 30 / 4′ 44″. 30		Corr.,	+	3^s. 22
				(*Add* to *mean* time.)		

For the Moon.

R. A., 5^h,		$22^h\ 14^m\ 39^s.29$	Dec., 5^h,	(−)	7°59′ 36″.1 S.	Hor. Par., 0^h,		55′ 13″.6	S. D., 0^h,		15′ 04″.7
Corr.,	+	38 .31	Corr.,	+	4 27 .1	Corr.,	−	7 .2	Corr.,	−	1 .8
R. A.,		22 15 17 .60	Dec.,		7 55 09 .0 S.	Hor. Par.,		55 06 .4	S. D.,		15 02 .9
M. D.,	+	$1^s.869$	M. D.,	+	13″.03	H. D.,	−	1.″34	H. D.,	−	0″.34
No. min.,	+	$20^m.5$	No. min.,	+	$20^m.5$	G. M. T.,	+	$5^h.34$	G. M. T.,	+	$5^h.34$
Corr.,	+	$38^s.31$	Corr.,	+	267″.12 / 4′ 27″.1	Corr.,	−	7″.15	Corr.,	−	1″.81

For Jupiter.

R. A., 0^h,		$22^h\ 26^m\ 35^s$. 54	Dec., 0^h,	(−)	10° 40′ 28″. 0 S.	Hor. Par., 16^d,	1″. 6
Corr.,	+	9 . 71	Corr.,	+	53 . 6		
R. A.,		22 26 45 . 25	Dec.,		10 39 34 . 4 S.		
H. D.,	+	1^s. 819	H. D.,	+	10″. 03	S. D., 16^d,	16″.9
G. M. T.,	+	5^h. 34	G. M. T.,	+	5^h. 34		
Corr.,	+	9^s. 71	Corr.,	+	53″. 6		

285. Should greater precision be required than that attainable by simple interpolation, resort must be had to the reduction for second differences.

The differences between successive values of the quantities given in the Nautical Almanac are called the *first differences;* the differences between successive first differences are called the *second differences.* Simple interpolation, which satisfies the necessities of sea computations, assumes the first differences to be constant; but if the variation of the first differences be regarded, a further interpolation is required for the second difference.

The difference for a unit of time in the American Nautical Almanac abreast any element expresses the rate at which the element is changing at that precise instant of Greenwich time. Now, regarding the second difference as constant, the first difference varies uniformly with the Greenwich time; therefore its value may be found for any intermediate time by simple interpolation.

Hence the following rule for second differences: Employ the interpolated value of the first difference which corresponds to the *middle* of the interval for which the correction is to be computed.

EXAMPLE: For the Greenwich date 1879, April. $10^d\ 18^h\ 25^m\ 30^s$, find the moon's declination.

Dec., 18^h,	(−)	26° 19′ 41″.1 S.	First diff.,	+ 0″.044	Second diff.,	+ 0″.181
Corr.,	+	2 .1	Corr.,	+ 0 .039	Interval,	+ 0^h.213
Dec.,		26 19 39 .0 S.	M. D.,	+ 0 .083	Corr.,	+ 0″.039
			No. min.,	+ 25^m.5		
			Corr.,	+ 2″.12		

The difference for one minute being + 0″.044 at 18^h, and + 0″.225 at 19^h, the difference for one minute undergoes a change of + 0″.181 during one hour. The time for which it is desired to obtain the difference is at the middle instant between $18^h\ 0^m$ and $18^h\ 25^m.5$—that is, at $18^h\ 12^m.75$, or its equivalent, 18^h 213. With a change of + 0″.181 in one hour, the change in $0^h.213$ is readily obtainable; correcting the minute's difference at $18^h.0$ accordingly, the process of correcting the declination becomes the same as in simple interpolation.

CONVERSION OF TIMES.

286. *Conversion of Time* is the process by which any instant of time that is defined according to one system of reckoning may be defined according to some other system; and also by which any interval of time expressed in units of one system may be converted into units of another.

287. Sidereal and Mean Times.—Mean time is the hour angle of the Mean Sun; sidereal time is the hour angle of the First Point of Aries. Since the Right Ascension of the Mean Sun is the angular distance between the hour circles of the Mean Sun and of the First Point of Aries, mean time may be converted into sidereal time by adding to it the Right Ascension of the Mean Sun; and similarly, sidereal time may be converted into mean time by subtracting from it the Right Ascension of the Mean Sun.

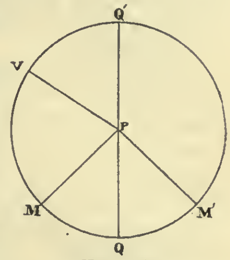

Fig. 36.

This is explained in figure 36, which represents a projection of the celestial sphere upon the equator. If P be the pole; QPQ′, the meridian; V, the First Point of Aries; M, the position of the mean sun (west of the meridian); then QPV, or the arc QV, is the sidereal time; QPM, or the arc QM, is the mean time; and VPM, or the arc VM, is the Right Ascension of the Mean Sun. From this it will appear that:

$$QV = QM + VM, \text{ or}$$
$$\text{Sidereal time} = \text{Mean time} + \text{Right Ascension of Mean Sun.}$$

If the mean sun be on the opposite side of the meridian, at M′, then the mean time equals $24^h - M'Q$. In this case:

$$QV = VM' - M'Q, \text{ or}$$
$$\text{Sidereal time} = \text{Right Ascension of Mean Sun} - (24^h - \text{Mean time}),$$
$$= \text{Right Ascension of Mean Sun} + \text{Mean time} - 24^h.$$

Right ascension being measured to the east and hour angle to the west, the sidereal time will therefore always equal the sum of these two; but 24^h must be subtracted when the sum exceeds that amount.

From the preceding equations, we also have:

$$QM = QV - VM; \text{ and}$$
$$M'Q = VM' - QV, \text{ or}$$
$$(24^h - M'Q) = (24^h + QV) - VM'.$$

From this it may be seen that the mean time equals the sidereal time *minus* the Right Ascension of the Mean Sun, but the former must be increased by 24^h when necessary to make the subtraction possible.

288. Apparent and Mean Times.—Apparent time is the angle between the meridian and the hour circle which contains the center of the sun; mean time is the angle between the meridian and the hour circle which contains the mean sun. Since the equation of time represents the angle between the hour circles of the mean and apparent suns, it is clear that the conversion of mean time to apparent time may be accomplished by the application of the equation of time, with its proper sign, to the mean time; and the reverse operation by the application of the same quantity, in an opposite direction, to the apparent time.

The resemblance of these operations to the interconversion of mean and sidereal times may be observed if, in figure 36, we assume that PV is the hour circle of the true sun, PM remaining that of the mean sun; then the arc QM will be the mean time; QV, the apparent time; and VM, the equation of time; whence we have as before:

$$QV = QM + VM, \text{ or}$$
$$\text{Apparent time} = \text{Mean time} + \text{Equation of time;}$$

the equation of time will be positive or negative according to the relative position of the two suns.

289. Sidereal and Mean Time Intervals.—The sidereal year consists of 366.25636 sidereal days or of 365.25636 mean solar days. If, therefore, M be any interval of mean time, and S the corresponding interval of sidereal time, the relations between the two may be expressed as follows:

$$\frac{S}{M} = \frac{366.25636}{365.25636} = 1.0027379;$$

$$\frac{M}{S} = \frac{365.25636}{366.25636} = 0.9972696.$$

$$\text{Therefore, } S = 1.0027379\ M = M + .0027379\ M;$$
$$M = 0.9972696\ S = S - .0027304\ S.$$

If $M = 24^h$, $S = 24^h + 3^m\ 56^s.6$; or, in a mean solar day, sidereal time gains on mean time $3^m\ 56^s.6$, the gain each hour being $9^s.8565$.

If $S = 24^h$, $M = 24^h - 3^m\ 55^s.9$; or, in a sidereal day, mean time loses on sidereal time $3^m\ 55^s.9$, the loss each hour being $9^s.8296$.

If M and S be expressed in hours and fractional parts thereof,

$$S = M + 9^s.8565\ M;$$
$$M = S - 9^s.8296\ S.$$

Tables for the conversion of the intervals of mean into those of sidereal time and the reverse are based upon these relations. Tables 8 and 9 of this work give the values for making these conversions, and similar tables are to be found in the Nautical Almanac.

290. To Convert Mean Solar into Sidereal Time.—Apply to the local mean time the longitude, adding if west and subtracting if east, and thus obtain the Greenwich mean time. Take from the Nautical Almanac the Right Ascension of the Mean Sun at Greenwich mean noon, and correct it for the Greenwich mean time by Table 9 or by the hourly difference of $9^s.857$. Add to the local mean time this corrected right ascension, rejecting 24^h if the sum is greater than that amount. The result will be the local sidereal time.

Example: April 22, 1879, in Long. 81° 15′ W., the local mean time is $2^h\ 00^m\ 00^s$ p. m. Required the corresponding local sidereal time:

L. M. T.,	$22^d\ 2^h\ 00^m\ 00^s$	R. A. M. S., $22^d\ 0^h$,	$2^h\ 00^m\ 41^s.24$	L. M. T.,	$2^h\ 00^m\ 00^s$
Long., +	5 25 00	Red. for $7^h\ 25^m$ (Tab. 9), +	1 13 .10	R. A. M. S., +	2 01 54.34
G. M. T.,	22 7 25 00	R. A. M. S., $7^h\ 25^m$,	2 01 54 .34	L. S. T.,	4 01 54.34

Example: April 22, 1879, in Long. 75° E., the local mean time is $4^h\ 00^m\ 00^s$ a. m. Required the local sidereal time.

L. M. T.,	$21^d\ 16^h\ 00^m\ 00^s$	R. A M. S. $21^d\ 0^h$,	$1^h\ 56^m\ 44^s.69$	L. M. T.,	$21^d\ 16^h\ 00^m\ 00^s$
Long., −	5 00 00	Red. for 11^h (Tab. 9), +	1 48 .42	R. A. M. S., +	1 58 33.11
G. M. T.,	21 11 00 00	R. A. M. S., 11^h,	1 58 33 .11	L. S. T.,	21 17 58 33.11

In these examples the reduction of the R. A. M. S. has formed a separate operation in order to make clear the process. It would be as accurate to add together directly L. M. T., R. A. M. S., and Red., and the work would thus be rendered more brief.

291. To Convert Sidereal into Mean Solar Time.—Take from the Nautical Almanac the Right Ascension of the Mean Sun for Greenwich mean noon of the given astronomical day, and apply to it the reduction for longitude, either by Table 9 or by the hourly difference of $9^s.857$, and the result will be the Right Ascension of the Mean Sun at local mean noon, which is equivalent to the local sidereal time at that instant. Subtract this from the given local sidereal time (adding 24^h to the latter if necessary), and the result will be the interval from local mean noon, expressed in units of sidereal time. Convert this sidereal time interval into a mean time interval by subtracting the reduction as given by Table 8 or by the hourly difference of $9^s.830$; the result will be the local mean time.

Example: April 22, 1879, a. m., in Long. 75° E., the local sidereal time is $17^h\ 58^m\ 33^s.11$. What is the local mean time?

Astronomical day, April 21.

L. S. T.,	$17^h\ 58^m\ 33^s.11$	R. A. M. S., Gr. $21^d\ 0^h$,	$1^h\ 56^m\ 44^s.69$
R. A M. S.,	− 1 55 55 .41	Red. for -5^h long. (Tab. 9), −	49 .28
Sid. interval from L. M. noon,	16 02 37 .70	R. A. M. S., local 0^h,	1 55 55 .41
Red. for sid. interval (Tab. 8),	2 37 .70		
L. M. T., 21^d,	16 00 00 .00		

Example: April 22, 1879, p. m., at a place in Long. 81° 15′ W., the sidereal time is $4^h\ 01^m\ 54^s.34$. What is the corresponding mean time?

Astronomical day, April 22.

L. S. T.,	$4^h\ 01^m\ 54^s.34$	R. A. M. S , Gr. $22^d\ 0^h$,	$2^h\ 00^m\ 41^s.24$
R. A. M. S.,	−2 01 34 .63	Red. for $+5^h\ 25^m$ long. (Tab. 9), +	0 53 .39
Sid. interval from L. M. Noon,	2 00 19 .71	R. A. M. S., local 0^h,	2 01 34 .63
Red. for sid. interval (Tab. 8), −	0 19 .71		
L. M. T., 22^d,	2 00 00 .00		

292. To Covert Mean into Apparent Time and the Reverse.—Find the Greenwich time corresponding to the given local time. If apparent time is given, find the Greenwich apparent time and take the equation of time from Page I of the Almanac. If mean time, find the Greenwich mean time and take the equation of time from Page II. Correct the equation of time for the required instant and apply it with its proper sign to the given time.

Example: April 21, 1879, in Long. 81° 15′ W., find the local apparent time corresponding to a local mean time of $3^h\ 05^m\ 00^s$ p. m.

L. M. T.,	$21^d\ 3^h\ 05^m\ 00^s$	L. M. T.,	$21^d\ 3^h\ 05^m\ 00^s$	Eq. t., 0^h,	$1^m\ 17.61$
Long., +	5 25 00	Eq. t., +	1 22.01	Corr., +	4.40
G. M. T.,	21 8 30 00	L. A. T.,	21 3 06 22.01	Eq. t.,	1 22.01
				H. D., +	$0^s.518$
				G.M.T., +	$8^h.5$
				Corr., +	$4^s.403$
					(*Add* to *mean* time.)

EXAMPLE: April 3, 1879, in Long. 81° 15′ E., the local apparent time is $8^h\ 45^m\ 00^s$ a. m. Required the mean time.

L. A. T.,	$2^d\ 20^h\ 45^m\ 00^s$	L. A. T.,	$2^d\ 20^h\ 45^m\ 00^s$	Eq. t., 0^h,	$3^m\ 42^s.46$
Long., —	5 25 00	Eq. t., +	3 30.90	Corr., —	11 .56
G. A. T.,	2 15 20 00	L. M. T.,	2 20 48 30.90	Eq. t.,	3 30 .90
				H. D., —	$0^s.754$
				G. M. T., —	$15^h.33$
				Corr., —	$11^s.56$
					(*Add* to *apparent* time.)

293. TO FIND THE HOUR ANGLE OF A BODY FROM THE TIME, AND THE REVERSE.—In figure 36, if M and M′ represent the positions of celestial bodies instead of those of the mean sun as before assumed, then the hour angles of the bodies will be Q M and 24^h — M′ Q, respectively, and their right ascensions will be V M and V M′.

As before, we have:

$$
\begin{aligned}
Q\,V &= Q\,M + V\,M,\\
&= V\,M' - M'\,Q;\\
Q\,M &= Q\,V - V\,M;\\
M'\,Q &= V\,M' - V\,Q, \text{ or}\\
(24^h - M'\,Q) &= (24^h + Q\,V) - V\,M'.
\end{aligned}
$$

Substituting, therefore, *hour angle of the body* for *mean time*, and *right ascension of the body* for *Right Ascension of the Mean Sun*, the rules previously given for the conversion of mean and sidereal times will be applicable for the conversion of hour angle and sidereal time. Thus, the sidereal time is equal to the sum of the right ascension of the body and its hour angle, subtracting 24^h when the sum exceeds that amount; and the hour angle equals the sidereal time *minus* the right ascension of the body, 24^h being added to the former when necessary to render the subtraction possible.

EXAMPLE: In Long. 81° 15′ W., on April 25, 1879, at $12^h\ 10^m\ 30^s$ (astronomical) mean time, find the hour angle of Sirius.

L. M. T.,	$12^h\ 10^m\ 30^s$	L. M. T.,	$12^h\ 10^m\ 30^s$
Long., +	5 25 00	R. A. M. S., 0^h, +	2 12 30.91
		Red. (Tab. 9), +	2 53.39
G. M. T.,	17 35 30	L. S. T.,	14 25 54.30
		R. A. Sirius, —	6 39 49.83
		H. A. Sirius,	7 46 04.47

EXAMPLE: May 9, 1879, Arcturus being $2^h\ 27^m\ 42^s.52$ east of the meridian, find the local sidereal time

	$24^h\ 00^m\ 00^s$	H. A.,	$21^h\ 32^m\ 17^s.48$
H. A.,	2 27 42.52 E.	R. A., +	14 10 11.71
H. A.,	21 32 17.48 W.	L. S. T.,	11 42 29.19

Or thus:

H. A., —	$2^h\ 27^m\ 42^s.52$
R. A., +	14 10 11 .71
L. S. T.,	11 42 29 .19

CHAPTER X.

CORRECTION OF OBSERVED ALTITUDES.

294. The *true altitude* of a heavenly body at any place on the earth's surface is the altitude of its center, as it would be measured by an observer at the center of the earth, above the plane passed through the center of the earth at right angles to the direction of the zenith.

The *observed altitude* of a heavenly body, as measured at sea, may be converted to the true altitude by the application of the following-named corrections: *Index Correction, Dip, Refraction, Parallax*, and *Semidiameter*. The corrections for parallax and semidiameter are of inappreciable magnitude in observations of the fixed stars, and with planets are so small that they need only be regarded in refined calculations. In observations with the artificial horizon there is no correction for dip.

For theoretical accuracy, the corrections should be applied in the order in which they are named, but in ordinary nautical practice the order of application makes no material difference, except in the case of the parallax of the moon as explained in article 306.

INDEX CORRECTION.

295. This correction is fully explained in articles 249 and 250, Chapter VIII.

REFRACTION.

296. It is known by various experiments that the rays of light deviate from their rectilinear course in passing obliquely from one medium into another of a different density; if the latter be more dense, the ray will be bent toward the perpendicular to the line of junction of the media; if less dense, it will be bent away from that perpendicular.

The ray of light before entering the second medium is called the *incident* ray; after it enters the second medium it is called the *refracted* ray, and the difference of direction of the two is called the *refraction*.

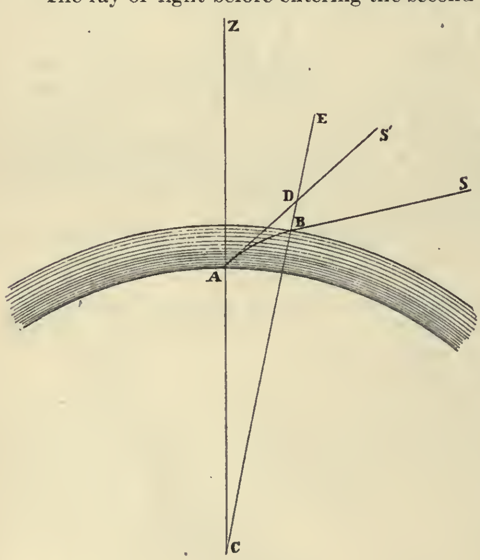

Fig. 37.

The rays of light from a heavenly body must pass through the atmosphere before reaching the eye of an observer upon the surface of the earth. The earth's atmosphere is not of a uniform density, but is most dense near the earth's surface, gradually decreasing in density toward its upper limit; hence the path of a ray of light, by passing from a rarer medium into one of continually increasing density becomes a curve, which is concave toward the earth. The last direction of the ray is that of a tangent to the curved path at the eye of the observer, and the difference of the direction of the ray before entering the atmosphere and this last direction constitutes the refraction.

297. To illustrate this, consider the earth's atmosphere as shown in figure 37; let SB be a ray from a star S, entering the atmosphere at B, and bent into the curve BA; then the apparent direction of the star is AS′, the tangent to the curve at the point A, the refraction being the angle between the lines BS and AS′. If CAZ is the vertical line of the observer, by a law of Optics the vertical plane of the observer which contains the tangent AS′ must also contain the whole curve BA and the incident ray BS. Hence refraction increases the apparent altitude of a star without affecting its azimuth.

At the zenith the refraction is nothing. The less the altitude the more obliquely the rays enter the atmosphere and the greater will be the refraction. At the horizon the refraction is the greatest.

298. The refraction for a mean state of the atmosphere (barometer 30^{in}, Fahr. thermometer 50°) is given in Table 20 A; the combined refraction and sun's parallax in Table 20 B; and the combined refraction and moon's parallax in Table 24.

Since the amount of the refraction depends upon the density of the atmosphere, and the density varies with the pressure and the temperature, which are indicated by the barometer and thermometer, the *true* refraction is found by applying to the mean refraction the corrections to be found in Tables 21 and 22; these are deduced from Bessel's formulæ, and are regarded as the most reliable tables constructed. It should be remembered, however, that under certain conditions of the atmosphere a very extraordinary deflection occurs in rays of light which reach the observer's eye from low altitudes

(that is, from points near the visible horizon), the amount of which is not covered by the ordinary corrections for pressure and temperature; the error thus created is discussed under *Dip* (art. 301); on account of it, altitudes less than 10° should be avoided.

Example: Required the refraction for the apparent altitude 5°, when the thermometer is at 20° and the barometer at 30$^{\text{in}}$ .67.

The mean refraction by Table 20 A is,	9′ 52″
The correction for height of barometer is,	+ 13
The correction for the temperature,	+ 42
True refraction,	10 47

299. The correction for refraction should always be subtracted, as also that for combined refraction and parallax of the sun; the correction for combined refraction and parallax of the moon is invariably additive.

DIP.

Using sea for horizon

300. *Dip of the Horizon* is the angle of depression of the visible sea horizon below the true horizon, due to the elevation of the eye of the observer above the level of the sea.

In figure 38 suppose A to be the position of an observer whose height above the level of the sea is AB. CAZ is the true vertical at the position of the observer, and AH is the direction of the true horizon, S being an observed heavenly body. Draw ATH′ tangent to the earth's surface at T. Disregarding refraction, T will be the most distant point visible from A. Owing to refraction, however, the most distant visible point of the earth's surface is more remote from the observer than the point T, and is to be found at a point T′, in figure 39. But to an observer at A the point T′ will appear to lie in the direction of AH″, the tangent at A to the curve AT′. If the vertical plane were revolved about CZ as an axis, the line AH would generate the plane of the true horizon, while the point T′ would generate a small circle of the terrestrial sphere called the *Visible* or *Sea Horizon.* The *Dip of the Horizon* is HAH″, being the angle between the true horizon and the apparent direction of the sea horizon. Values of the dip are given in Table 14 for various heights of the observer's eye, and in the calculation of the table allowance has been made for the effect of atmospheric refraction as it exists under normal conditions.

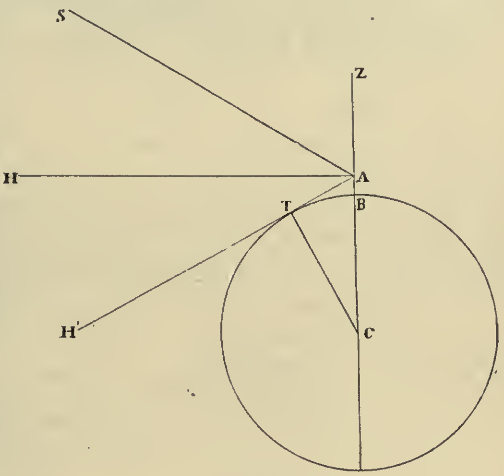

Fig. 38.

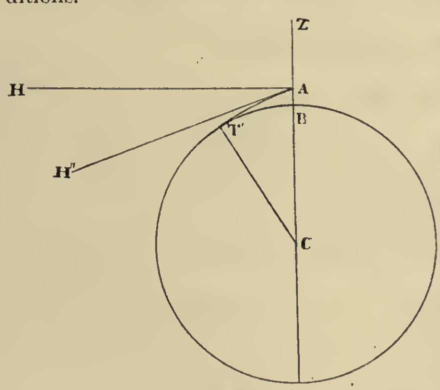

Fig. 39.

301. The fact must be emphasized, however, that under certain conditions the deflection of the ray in its path from the horizon to the eye is so irregular as to give a value of the dip widely different from that which is tabulated for the mean state of atmosphere. These irregularities usually occur when there exists a material difference between the temperature of the sea water and that of the air, and they attain a maximum value in calm or nearly calm weather, when the lack of circulation permits the air to arrange itself in a series of horizontal strata of different densities, the denser strata being below when the air is warmer, and the reverse condition obtaining when the air is cooler. The effect of such an arrangement is that a ray of light from the horizon, in passing through media of different densities, undergoes a refraction quite unlike that which occurs in the atmosphere of much more nearly homogeneous density that exists under normal conditions.

Various methods have been suggested for computing the amount of dip for different relative values of temperature of air and water, but none of these afford a satisfactory solution, there being so many elements involved which are not susceptible of determination by an observer on shipboard that it will always be difficult to arrive at results that may be depended upon. [a]

As the amount of difference between the actual and tabulated values of the dip due to this cause may sometimes be very considerable—reliable observations having frequently placed it above 10′, and values as high as 32′ having been recorded—it is necessary for the navigator to be on his guard against the errors thus produced, and to recognize the possible inaccuracy of all results derived from observations taken under unfavorable conditions. Without attempting to give any method for the determination of the amount of the extraordinary variation in dip, the following rules may indicate to the navigator the conditions under which caution must be observed, and the direction of probable error:

(*a*) A displacement of the horizon should always be suspected when there is a marked difference between the temperatures of air and sea water; this fact should be especially kept in mind in regions such as those of the Red Sea and the Gulf Stream, where the difference frequently exists.

[a] A sextant attachment devised by Lieutenant-Commander J. B. Blish, U. S. Navy, enables an observer to measure the actual dip at any time.

(*b*) The error in the tabulated value of the dip will increase with an increase in the difference of temperature, and will diminish with an increase in the force of the wind.

(*c*) The error will decrease with the height of the observer's eye; hence it is expedient, especially when error is suspected, to make the observation from the most elevated position available.

(*d*) When the sea water is colder than the air the visible horizon is raised and the dip is decreased; therefore the true altitude is greater than that given by the use of the ordinary dip table. When the water is warmer than the air, the horizon is depressed and the dip is increased. At such times the altitude is really less than that found from the use of the table.

The same cause, it may be mentioned here, affects the kindred matter of the visibility of objects. When the air is warmer, terrestrial objects are sighted from a greater distance and appear higher above the horizon than under ordinary conditions. When the water is warmer than the air, the distance of visibility is reduced, and terrestrial objects appear at a less altitude.

302. What has been said heretofore about the dip supposes the horizon to be free from all intervening land or other objects; but it often happens that an observation is required to be taken from a ship sailing along shore or at anchor in harbor, when the sun is over the land and the shore is nearer the ship than the visible sea-horizon would be if it were unconfined; in this case the dip will be different from that of Table 14, and will be greater the nearer the ship is to that point of the shore to which the sun's image is brought down. In such case Table 15 gives the dip at different heights of the eye and at different distances of the ship from the land.

303. The dip is always to be subtracted from the observed altitude.

PARALLAX.

304. The *parallax* of a heavenly body is, in general terms, the angle between two straight lines drawn to the body from different points. But in Nautical Astronomy *geocentric parallax* is alone considered, this being the difference between the positions of a heavenly body as seen at the same instant from the center of the earth and from a point on its surface.

The zenith distance of a body, S (fig. 40), seen from A, on the surface of the earth, is ZAS; seen from C it is ZCS; the *parallax* is the difference of these angles, ZAS—ZCS=ASC.

Parallax in altitude is, then, the angle at the heavenly body subtended by the radius of the earth.

If the heavenly body is in the horizon as at H′, the radius, being at right angles to AH′, subtends the greatest possible angle at the star for the same distance, and this angle is called the *horizontal parallax*. The parallax is less as the bodies are farther from the earth, as will be evident from the figure.

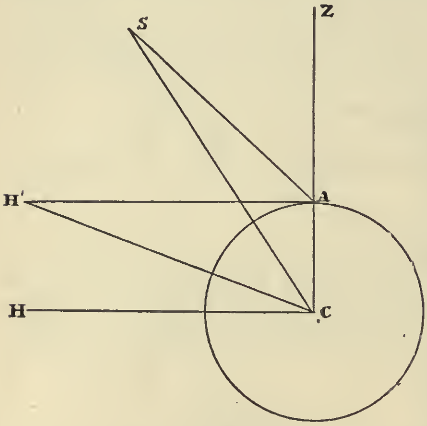

Fig. 40.

Let par. = parallax in altitude, ASC;
Z = SAZ, the apparent zenith distance (corrected for refraction);
R = AC, the radius of the earth; and
D = CS, the distance of the object from the center of the earth.

Then, since SAC = 180° — SAZ, the triangle ASC gives:

$$\sin \text{par.} = \frac{R \sin Z}{D}.$$

If the object is in the horizon at H′, the angle AH′C is the horizontal parallax, and denoting it by H. P. the right triangle AH′C gives:

$$\sin \text{H. P.} = \frac{R}{D}.$$

Substituting this value of $\frac{R}{D}$ in the above,

$$\sin \text{par.} = \sin \text{H. P.} \sin Z.$$

If h = SAH′, the apparent altitude of the heavenly body, then $Z = 90° - h$; hence,

$$\sin \text{par.} = \sin \text{H. P.} \cos h.$$

Since par. and H. P. are always small, the sines are nearly proportional to the angles; hence,

$$\text{par.} = \text{H. P.} \cos h.$$

305. The Nautical Almanac gives the horizontal parallax of the moon, as well as of the planets Mercury, Venus, Mars, Jupiter, Saturn, Uranus, and Neptune.

In Table 16 will be found the values of the sun's parallax for altitude intervals of 5° or 10°, while Table 20 B contains the combined values of the sun's parallax and the refraction. In Table 24 is given the parallax of the moon, combined with the refraction, at various altitudes and for various values of the horizontal parallax.

306. Parallax is always additive; combined parallax and refraction additive in the case of the moon, but subtractive for the sun.

As the correction for parallax of the moon is so large, it is essential that it be taken from the table with considerable accuracy; the corrections for index correction, semidiameter, and dip should therefore be applied first, and the "approximate altitude" thus obtained should be used as an argument in entering Table 24 for parallax and refraction.

SEMIDIAMETER.

307. The *semidiameter* of a heavenly body is half the angle subtended by the diameter of the visible disk at the eye of the observer. For the same body the semidiameter varies with the distance; thus, the difference of the sun's semidiameter at different times of the year is due to the change of the earth's distance from the sun; and similarly for the moon and the planets.

In the case of the moon, the earth's radius bears an appreciable and considerable ratio to the moon's distance from the center of the earth; hence the moon is materially nearer to an observer when in or near his zenith than when in or near his horizon, and therefore the semidiameter, besides having a menstrual change, has a semidiurnal one also.

The increase of the moon's semidiameter due to increase of altitude is called its *augmentation*. This reduction may be taken from Table 18.

The semidiameters of the sun, moon, and planets are given in their appropriate places in the Nautical Almanac.

308. The semidiameter is to be added to the observed altitude in case the lower limb of the body is brought into contact with the horizon, and to be subtracted in the case of the upper limb. When the artificial horizon is used, the limb of the *reflected* image is that which determines the sign of this correction, it being additive for the lower and subtractive for the upper.

EXAMPLE: May 6, 1879, the observed altitude of the sun's upper limb was 62° 10′ 40″; I. C., + 3′ 10″; height of the eye, 25 feet. Required the true altitude.

Index correction

Obs. alt. $\overline{\odot}$,	62° 10′ 40″	I. C.,	+ 3′ 10″
Corr.,	− 18 04		
		S. D. (Naut. Alm.),	− 15′ 53″
True alt.,	61 52 36	dip (Tab. 14),	− 4 54
		p. & r. (Tab. 20 B),	− 27
			− 21 14
		Corr.,	− 18′ 04″

EXAMPLE: The altitude of Sirius as observed with an artificial horizon was 50° 59′ 30″; I. C., − 1′ 30″. Required the true altitude.

Obs. 2 alt. ✱,	50° 59′ 30″
I. C.,	− 1 30
	2)50 58 00
Obs. alt.,	25 29 00
ref. (Tab. 20 A),	− 2 02
True alt.,	25 26 58

EXAMPLE: April 16, 1879, observed altitude of Venus 53° 26′ 10″; I. C., + 2′ 30″; height of eye, 20 feet. Required the true altitude.

Obs. alt. ✱,	53° 26′ 10″	par. (Tab. 17),	+ 0′ 04″	Hor. Par. (Naut. Alm.), 7″
Corr.,	− 2 32	I. C.,	+ 2 30	
	53 23 38		+ 2 34	
		dip (Tab. 14),	− 4′ 23″	
		ref. (Tab. 20 A),	− 43	
			− 5 06	
		Corr.,	− 2′ 32″	

EXAMPLE: May 6, 1879, at $13^h\ 24^m$ G. M. T., the observed altitude of the moon's lower limb was 25° 30′ 30″; I. C., −1′ 30″; height of eye, 20 feet. Required the true altitude.

Obs. alt. ☾,	25° 30′ 30″	S. D. (Naut. Alm.),	+ 16′ 42″	Hor. Par. (Naut. Alm.)	61′ 10″
1st corr.,	+ 10 57	Aug. (Tab. 18),	+ 08		
Approx. alt.,	25 41 27		+ 16 50		
p. & r. (Tab. 24),	+ 53 07	dip (Tab. 14),	− 4′ 23″		
True alt.,	26 34 34	I. C.,	− 1 30		
			− 5 53		
		1st corr.,	+ 10′ 57″		

Or, the following modification may be adopted:

Obs. alt. ☾,	25° 30′ 30″	S. D.,	+ 16′ 42″	H. P.,	3670″	log 3.56467
1st corr.,	+ 8 56	Aug.,	+ 08	App. alt.,	25° 39′	cos 9.95494
Approx. alt.,	25 39 26		+ 16 50	par.,	3308″ / 55′ 08″	log 3.51961
par.,	+ 55 08	dip,	− 4′ 23″			
True alt.,	26 34 34	ref.,	− 2 01			
		I. C.,	− 1 30			
			− 7 54			
		1st corr.,	+ 8′ 56″			

CHAPTER XI.

THE CHRONOMETER ERROR.

309. It has already been explained (art. 261, Chap. VIII) that the *error* of a chronometer is the difference between the time indicated by it and the correct standard time to which it is referred; and that the *daily rate* is the amount that it gains or loses each day. In practice, chronometer errors are usually stated with reference to Greenwich mean time. It is not required that either the error or the rate shall be zero, but in order to be enabled to determine the correct time it is essential that both rate and error be known, and that the rate shall have been uniform since its last determination.

310. Determining the Rate.—Since all chronometers are subject to some variation in rate under the changeable conditions existing on shipboard, it is desirable to ascertain a new rate as often as possible. The process of obtaining a rate involves the determination of the error on two different occasions separated by an interval of time of such length as may be convenient; the change of error during this interval, divided by the number of days, gives the daily rate.

Example: On March 10, at noon, found chronometer No. 576 to be $0^m\ 32^s.5$ fast of G. M. T.; on March 20, at noon, the same chronometer was $0^m\ 48^s.0$ fast of G. M. T. What was the rate?

Error, March $10^d\ 0^h$,	$+0^m\ 32^s.\ 5$
Error, March $20^d\ 0^h$,	$+0\ \ 48\ .\ 0$
Change in 10 days,	$+\ \ 15\ .\ 5$
Daily rate,	$+\ \ 1^s.55$

The chronometer is therefore *gaining* $1^s.55$ per day.

311. Determining Error from Rate.—The error on any given day being known, together with the daily rate, to find the error on any other day it is only necessary to multiply the rate by the number of days that may have elapsed, and to apply the product, with proper sign, to the given error.

Example: On December 17 a chronometer is $3^m\ 27^s.5$ slow of G. M. T. and losing $0^s.47$ daily. What is the error on December 26?

Error Dec. 17,	$-3^m\ 27^s.5$	Daily rate,	$-0^s.47$
Correction,	$-\ \ 4\ .2$	No. days,	9
Error Dec. 26,	$-3\ \ 31\ .7$	Corr.,	$-4\ .23$

The chronometer is therefore *slow* of G. M. T. on December 26, $3^m\ 31^s.7$.

312. It is necessary to distinguish between the signs of the chronometer *correction* and of the chronometer *error*. A chronometer fast of the standard time is considered as having a *positive error*, since its readings are positive to (greater than) those of an instrument showing correct time; but the same chronometer has a *negative correction*, as the amount must be subtracted to reduce chronometer readings to correct readings.

313. Numerous methods are available for determining the error of a chronometer in port. The principal of these will be given.

BY TIME SIGNALS.

314. In nearly all of the important ports of the world a time signal is made each day at some defined instant. In many cases this consists in the dropping of a time-ball—the correct instant being given telegraphically from an observatory. In a number of places where there is no time-ball a signal may be received on the instruments at the telegraph offices, whereby mariners may ascertain the errors of their chronometers. Such signals are to be had in almost every port of the United States.

The time signal may be given by a gun-fire or other sound, in which case allowance must be made by the observer for the length of time necessary for the sound to travel from the point of origin to his position. Sound travels 1,090 feet per second at 32° F., and its velocity increases at the rate of 1.15 feet per second with each degree increase of temperature. If V be the velocity of sound in feet per second at the existing temperature, and D the distance in feet to be traversed, $\frac{D}{V}$ is the number of seconds to be subtracted from the chronometer reading at the instant of hearing the signal, to ascertain the reading at the instant the signal was made.

This method of obtaining the chronometer error consists in taking the difference between the standard time and chronometer time at the time of observation and marking the result with appropriate sign.

EXAMPLE: A time-ball drops at $5^h\ 0^m\ 0^s$, G. M. T., and the reading of a chronometer at the same moment is $4^h\ 57^m\ 52^s.5$. What is the chronometer error?

G. M. T.,	$5^h\ 00^m\ 00^s$
Chro. t.,	4 57 52 .5
Chro. error, —	2 07 .5

That is, chronometer *slow* $2^m\ 07^s.5$; chronometer *correction* additive.

BY TRANSITS.

315. The most accurate method of finding the chronometer correction is by means of a transit instrument well adjusted in the meridian, noting the times of transit of a star or the limbs of the sun across the threads of the instrument.

At the instant of the body's passage over the meridian wire, mark the time by the chronometer. The hour angle at the instant is 0^h; therefore the local sidereal time is equal to the right ascension of the body in the case of a star, or the local apparent time is 0^h in the case of the sun's center. By converting this sidereal or apparent time into the corresponding mean time and applying the longitude, the Greenwich mean time of transit is given. By comparing with this the time shown by chronometer the error is found.

EXAMPLE: 1879, May 9 (Ast. day), in Long. 44° 39′ E., observed the transit of Arcturus over the middle wire of the telescope, the time noted by a chronometer regulated to Greenwich mean time being $8^h\ 05^m\ 33^s.5$. Required the error.

L. S. T. (R. A. ✳),		14^h	10^m	$11^s.71$
Long.,	—	2	58	36
G. S. T.,		11	11	35.71
R. A. M. S., $9^d\ 0^h$,	—	3	07	42.69
Sid. int. from 0^h,		8	03	53.02
Reduction (Tab. 8),	—		1	19.27
G. M. T.,		8	02	33.75
Chro. t.,		8	05	33.50
Chro. fast,			2	59.75

EXAMPLE: June 25, 1879, in Long. 60° E., observed the transit of both limbs of the sun over the meridian wire of the telescope, noting the times by a chronometer. Find the error of the chronometer on G. M. T.

Transit of western limb,		$8^h\ 04^m\ 02^s.5$		Eq. t.,	$2^m\ 16^s.72$
Transit of eastern limb,		8 06 20 .0		H. D.,	+ $0^s.532$
Chro. time, loc. app. noon,		8 05 11 .25		Long.,	— 4^h
L. A. T., loc. app. noon,		$0^h\ 00^m\ 00^s$		Corr.,	— $2^s.128$
Eq. t.,	+	2 14 .59		Eq. t.,	$2^m\ 14^s.59$
L. M. T., loc. app. noon,		0 02 14 .59		*Add* to *apparent* time.	
Long.,	—	4 00 00			
G. M. T., loc. app. noon,		8 02 14 .59			
Chro. time, loc. app. noon,		8 05 11 .25			
Chro. fast,		2 56 .66			

BY A SINGLE ALTITUDE (TIME SIGHT).

316. The problem involved in this solution, by reason of its frequent application in determining the longitude at sea, is one of the most important ones in Nautical Astronomy. It consists in finding the hour angle from given values of the altitude, latitude, and polar distance. The hour angle thus obtained is converted by means of the longitude and equation of time in the case of the sun, or longitude and right ascension in the case of other celestial bodies, into Greenwich mean time; and this, compared with the chronometer time, gives the error.

317. It should be borne in mind that the most favorable position of the heavenly body for time observations is when near the prime vertical. When exactly in the prime vertical a small error in the latitude produces no appreciable effect. Therefore, if the latitude is uncertain, good results may be obtained by observing the sun or other body when bearing east or west. If observations are made at the same or nearly the same altitude on each side of the meridian and the mean of the results is taken, various errors are eliminated of which it is otherwise impossible to take account, and a very accurate determination is thus afforded.

318. With a sextant and artificial horizon or good sea horizon, several altitudes of a body should be observed in quick succession, noting in each case the time as shown by a hack chronometer or comparing watch whose error upon the standard chronometer is known. Condensing the observation into

a brief interval justifies the assumption that the altitude varies uniformly with the time. A very satisfactory method is to set the sextant in advance at definite intervals of altitude and note the time as contact is observed.

319. Correct the observed altitude for instrumental and other errors, reducing the apparent to the true altitude.

If the sun, the moon, or a planet is observed, the declination is to be taken from the Nautical Almanac for the time of the observation. If the chronometer correction is not approximately known and it is therefore impossible to determine the Greenwich mean time of observation with a fair degree of accuracy, the first hour angle found will be an approximate one; the declination corrected by this new value of the time will produce a more exact value of the hour angle, and the operation may be repeated until a sufficiently precise value is determined.

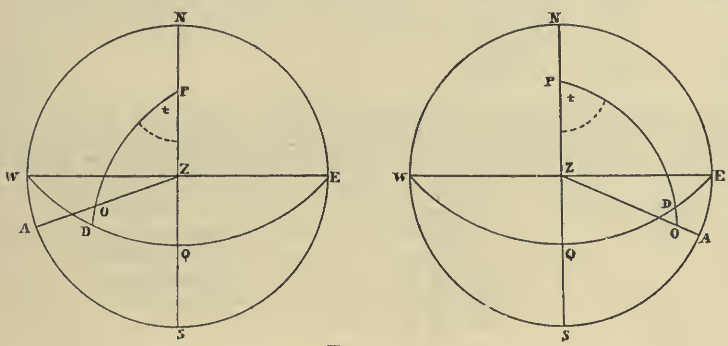

FIG. 41.

320. In figure 41 there are given:

AO $= h$, the altitude of the body O;

DO $= d$, the declination; and

QZ $=$ L, the latitude of the place.

In the astronomical triangle POZ there may be found from the foregoing:

ZO $= z$, the zenith distance of the body, $= 90° - h$;

PO $= p$, the polar distance, $= 90° \pm d$; and

PZ $=$ co-L, the co-latitude of the place, $= 90° -$ L.

From this data it is required to find the angle OPZ, the hour angle of the body, $= t$. This is given by the formula:

$$\sin^2 \tfrac{1}{2} t = \frac{\cos \frac{1}{2} (h + \mathrm{L} + p) \sin \frac{1}{2} (\mathrm{L} + p - h)}{\cos \mathrm{L} \sin p}.$$

If we let $s = \frac{1}{2} (h + \mathrm{L} + p)$, this becomes:

$$\sin \tfrac{1}{2} t = \sqrt{\sec \mathrm{L} \operatorname{cosec} p \cos s \sin (s - h)}.$$

The polar distance is obtained by adding the declination to 90° when of different name from the latitude and subtracting it from 90° when of the same name. Like latitude and altitude it is always positive.

If the sun is the body observed, the resulting hour angle is the local apparent time and is to be taken from the a. m. or p. m. column of Table 44 according as the altitude is observed in the forenoon or afternoon. If the moon, a star, or a planet be taken, the hour angle is always found in the p. m. column.

Local apparent time as deduced from an observation of the sun is converted to local mean time by the application of the equation of time; then, by adding the longitude if west, and subtracting it if east, the Greenwich mean time is obtained.

The hour angle of any other body, added to its right ascension when it is west of the meridian at observation or subtracted therefrom when east, gives the local sidereal time, which may be reduced to Greenwich sidereal time by the application of the longitude, and thence to Greenwich mean time by methods previously explained.

A comparison of the Greenwich mean time with the chronometer time of sight gives the error of the chronometer.

EXAMPLE: January 20, 1879, p. m., in Lat. 48° 41′ 00″ S., Long. 69° 03′ 00″ E., observed a series of altitudes of the sun with a sextant and artificial horizon; mean double altitude, 59° 03′ 10″, images approaching; mean of times by comparing watch, $4^h 40^m 56^s$; C—W, $7^h 23^m 25^s$; index correction, —1′ 30″; approximate chronometer correction, $-0^m 10^s$. What was the exact chronometer error?

W. T.,	$4^h 40^m 56^s$	Obs. 2 alt. ⊙,	59° 03′ 10″	Dec.,	20° 08′ 26″.6 S.	Eq. t.,	$11^m 14^s.60$
C—W,	7 23 25	I. C.,	— 1 30				
				H. D.,	+ 32″.5	H. D.,	+ $0^s.74$
Chro. t.,	0. 04 21		2)59 01 40	G. M. T.,	$0^h.07$	G. M. T.,	$0^h.07$
App. C. C.,	— 0 10						
		⊙	29 30 50	Corr.,	+ 2″.275	Corr.,	+ $0^s.052$
App. G. M. T.,	0 04 11	Corr.,	+ 14 43				
				Dec.,	20° 08′ 24″.3 S.	Eq. t.,	$11^m 14^s.7$
			29 45 33				
				p,	69° 51′ 36″		(*Add* to *apparent* time.)
		S. D.,	+ 16′ 17″				
		p. & r.,	— 1′ 34″				
		Corr.,	+ 14′ 43″				

polar dist = 90°± d

h	29° 45′ 33″			L. A. T.,	$4^h\ 29^m\ 46^s.7$
L	48 41 00	sec	.18031	Eq. t.,	+ 11 14.7
p	69 51 36	cosec	.02740	L. M. T.,	4 41 01.4
	2)148 18 09			Long.,	−4 36 12.0
s	74 09 05	cos	9.43631	G. M. T.,	0 04 49.4
$s-h$	44 23 32	sin	9.84483	Chro. t.,	0 04 21.0
			2)19.48885	Chro. slow,	0 00 28.4
L. A. T.,	$4^h\ 29^m\ 46^s.7$	sin ½ t	9.74442		

EXAMPLE: May 18, 1879, p. m., in Lat. 8° 03′ 22″ S., Long. 34° 51′ 57″ W., observed a series of altitudes of the star Arcturus, east of the meridian, using artificial horizon; mean double altitude, 60° 10′; mean watch time, $6^h\ 50^m\ 32^s$; C—W, $2^h\ 20^m\ 59^s.5$; I. C., +2′ 00″. Find the true error of the chronometer.

W. T.,	$6^h\ 50^m\ 32^s$	Obs. 2 alt. *,		60° 10′ 00″	R. A. *,	$14^h\ 10^m\ 11^s.7$
C—W,	2 20 59.5	I. C.,	+	2 00	Dec. *,	19° 48′ 33″.5 N.
Chro. t.,	9 11 31.5			2)60 12 00	p,	109° 48′ 34″
				30 06 00		
		ref.,	—	1 41		
		h,		30 04 19		

h	30° 04′ 19″			R. A. *,		$14^h\ 10^m\ 11^s.7$
L	8 03 22	sec	.00431	H. A.,	—	3 35 41
p	109 48 34	cosec	.02650	L. S. T.,		10 34 30.7
	2)147 56 15			Long.,	+	2 19 27.8
s	73 58 08	cos	9.44116	G. S. T.,		12 53 58.5
$s-h$	43 53 49	sin	9.84096	R. A. M. S., 0^h,	—	3 43 11.7
			2)19.31293	Sid. int. from 0^h,		9 10 46.8
				Red. (Tab. 8),	—	1 30.2
H. A.	$3^h\ 35^m\ 41^s$ E.	sin ½ t	9.65647			
				G. M. T.,		9 09 16.6
				Chro. t.,		9 11 31.5
				Chro. fast,		2 14.9

BY EQUAL ALTITUDES.

321. The method of observing *equal altitudes* of the same body on opposite sides of the meridian is usually employed for accurate determinations of the chronometer error when the method of transits is not available.

In the case of a star, the mean of the two chronometer times corresponding to the equal altitudes is the chronometer time of transit; but in the case of the sun the mean of these times differs somewhat from the time of transit, since, in consequence of the change of the sun's declination between the observations, the equal altitudes do not occur at equal intervals before and after the transit.

The small correction necessary, when the sun is observed, to reduce the mean of the times to the time of transit is called the *equation of equal altitudes.*

322. EQUAL ALTITUDES OF THE SUN.[a]—On shore, at a place whose longitude is *accurately* known, and whose latitude is *approximately* known, observe, with an artificial horizon, the same altitude both before and after meridian passage, as near the prime vertical as convenient when the altitude is more than 10°, noting the times. In low latitudes the method of equal altitudes will often give very accurate results, even when the observations are quite near the meridian.

It is most convenient, as well as conducive to accuracy, to take the observations in series, setting the sextant in advance of the altitude and marking the time at the instant that the contact is observed; about five or seven sights may compose a series, and several series may be observed; with the images of the sun alternately approaching and separating; thus the mean of the results (working each series of sights separately) will eliminate various possible errors. Ten minutes of double altitude will usually be found a convenient interval for observing.

The sights may be taken on opposite sides of the meridian for either upper or lower transit. If at upper transit, the first altitudes are taken in the forenoon and the times recorded; then in the afternoon the times corresponding to the same altitudes are observed, the last altitude taken in the morning being the first to come on in the afternoon; series taken with separating images in the forenoon should be observed with approaching images in the afternoon, and the reverse. If the time of lower transit is to be determined, the first set of sights is taken in the afternoon of one day and the second set in the forenoon of the next, care being taken as before to observe with images moving in opposite directions on opposite sides of the meridian.

[a] Chauvenet's method.

323. The mean of the a. m. times call the *A. M. Chronometer Time*, the mean of the p. m. times, the *P. M. Chronometer Time.* If, instead of noting the times by the chronometer, a watch is used (compared with the chronometer both before and after each observation), it will generally be found necessary to make an allowance for its gain or loss on the chronometer, so as to obtain the exact difference between the watch and chronometer at the instant of observation. The difference applied to the mean of the watch times gives the mean chronometer time the same as would have been found by employing the chronometer directly.

The half sum of the A. M. and P. M. Chronometer Times is the *Middle Chronometer Time;* the P. M. *minus* the A. M. time in the case of observations for upper transit, or the A. M. *minus* the P. M. time for lower transit, gives the *Elapsed Time.* Twelve hours should be added to the chronometer time at second observation in any case where the chronometer has passed XII^h during the interval between sights.

Take from the Nautical Almanac, page I, the sun's declination, the hourly difference of declination, and the equation of time, reducing each to the instant of local apparent noon by applying the differences due to the longitude.

Mark *north* latitude and declination +, *south* latitude and declination —.

Mark hourly difference of declination when *toward north* +, when *toward south* —.

Enter Table 37 with the elapsed time, and take out log A and log B, prefixing to each its proper sign as given in the table at the head of the page.

To log A add the logarithm of the hourly diff. (Table 42) and the log tangent of the latitude (Table 44). Prefix to each logarithm the sign of the quantity it represents, and to their sum the sign which results from the algebraic multiplication of the quantities. This sum is the logarithm (Table 42) of the number of seconds of time in the *first part* of equation of equal altitudes, to be marked + or —, like its logarithm.

To log B add the logarithm of the hourly diff. and the log tangent of the declination, marking the signs as before. The sum is the logarithm of the *second part* of the equation of equal altitudes, to be marked + or — like its logarithm.

Combine the two parts, having regard to signs, to obtain the *equation of equal altitudes;* apply this, with proper sign, to the Middle Chronometer Time and the result is the *Chronometer Time of Local Apparent Noon* or *Chronometer Time of Local Apparent Midnight,* according as observations were taken on opposite sides of the meridian at upper or at lower transit.

Apply the equation of time (adding when it is additive to mean time, otherwise subtracting); the result is the *Chronometer Time of Local Mean Noon,* or *Midnight,* which, if the chronometer is regulated to local time, will be $12^h\ 0^m\ 0^s$ when the chronometer is right, more than 12^h when fast, less than 12^h when slow.

If the chronometer is regulated to Greenwich time, apply the longitude (in time) to the chronometer time of mean noon (subtracting in west, adding in east longitude); the result will be more or less than 12^h, according as the chronometer is fast or slow.

EXAMPLE: April 13, 1879, at a place in Lat. 30° 25′ N., Long. $5^h\ 25^m\ 42^s$ W., observed the following equal altitudes of the sun with a sextant and artificial horizon, noting the times by a watch compared with a chronometer regulated to Greenwich mean time. What is the error of the chronometer?

A. M. COMPARISONS.		P. M. COMPARISONS.					
Chro.,	$2^h\ 22^m\ 30^s$	Chro.,	$8^h\ 04^m\ 30^s$	Dec.,	9° 00′ 54″.1 N.	H. D. (13th),	+54″.40
Watch,	8 52 02	Watch,	2 34 01			H. D. (14th),	+54 .03
				H. D. at noon,	+ 54″.32		
C−W,	5 30 28	C−W,	5 30 29	Long.,	+ 5^h.43	Diff., 24 hrs.,	− 0 .37
Chro.,	$2^h\ 56^m\ 30^s$	Chro.,	$8^h\ 33^m\ 30^s$	Corr.,	+ {294″.96 4′55″.0	Diff., 1 hr.,	−0″.015
Watch,	9 26 02	Watch,	3 03 01			Diff., 5^h.43,	−0 .03
C−W,	5 30 28	C−W,	5 30 29	Dec.,	9° 05′ 49″ N.	H.D. at noon,	+54″.32

WATCH, A. M.	ALTS.	WATCH, P. M.			
$9^h\ 12^m\ 30^s$	91° 00′	$2^h\ 45^m\ 45^s$			
12 55	10	45 20			
13 20	20	44 55	Tab. 37	log A (−)9.4445	log B (+)9.3193
13 45	30	44 30	H. D. +54″.32	log (+)1.7350	log (+)1.7350
14 10	40	44 05	Lat. +30° 25′ tan	(+)9.7687	d + 9°6′ tan (+)9.2045

Mean, W. T., A. M.,	$9^h\ 13^m\ 20^s$	Mean, W. T., P. M.,	$2^h\ 44^m\ 55^s$	1st Part —8^s.88	log (−)0.9482	
C−W,	+ 5 30 28	C−W,	+ 5 30 29	2d Part +1 .81		log (+)0.2588
A. M. Chro. T.,	2 43 48	P. M. Chro. T.,	8 15 24	Eq. eq. alt.	−7 .07	
P. M. Chro. T.,	+ 8 15 24	A. M. Chro. T.,	− 2 43 48			
	2)10 59 12	Elapsed Time,	5 31 36			
Mid. Chro. T.,	5 29 36	Eq. t.,	$0^m\ 35^s$.02			
Eq. eq. alt.,	− 7.1	H. D.,	+ 0^s.65			
Chro. t. L. A. Noon,	5 29 28.9	Long.,	+ 5^h.43			
Eq. t.,	− 0 31.5	Corr.,	+ 3^s.53			
Chro. t. L. M. Noon,	5 28 57.4					
Long.,	− 5 25 42.0	Eq. t.,	$0^m\ 31^s$.5			
		(*Minus* to *mean* time.)				
Chro. fast.	0 03 15.4					

324. A quicker method of solving the same problem[a] is available when results are not required to be accurate to the fraction of a second.

If h' is the change of altitude in minutes of arc, due to the total change in declination in the time elapsed between sights (the latitude and hour angle remaining the same), and t' the number of seconds it requires for the sun to change its altitude one minute of arc, then:

$$\text{Equation of equal altitudes} = \frac{1}{2}\, h' \times t'.$$

Table 25 gives the change of altitude of an object arising from a change of 100 seconds in declination at various altitudes, declinations, and latitudes. By multiplying the appropriate quantity taken from this table by the total change of declination between sights, dividing by 100, and converting the result from seconds to minutes of arc, h' is found. It is marked with the sign indicated in the table.

By dividing the number of seconds of time between the first and last sights of one of the series by the number of minutes difference of altitude, we find t'. When the sights are taken on opposite sides of the upper meridian t' is *minus;* for the lower meridian it is *plus.*

When the artificial horizon is used, if t' is computed on a basis of the change of the *double* altitude, its value is only half of the true one and the second term of the equation becomes $h' \times t'$ instead of as given above.

The example given in illustration of the preceding method when worked by this method is as follows:

Change in declination between sights = H. D. × elapsed time = $54''.32 \times 5^h.53 = 300''$.
Change in altitude due to 100″ declination (Tab. 25) = $+56''$.

$$h' = +\frac{56 \times 300}{100 \times 60} = +2'.80.$$

$$t' = -\frac{2^h45^m45^s - 2^h44^m05^s}{91^\circ 40' - 91^\circ 00'} = -\frac{100^s}{40'} = -2^s.5.$$

Eq. equal alt. $= +2.80 \times -2^s.5 = -7^s.00$.

325. If equal altitudes of a planet were observed, the correction due to change of declination could be computed as in the case of the sun. It is not ordinarily expedient to use a planet, however, for if night sights are to be taken facility of working would make it preferable to employ a fixed star.

On account of its rapid and excessive change of declination the moon would never be observed for equal altitudes.

326. Equal Altitudes of a Fixed Star.—In selecting stars for this observation, it is to be remarked that the nearer to the zenith the star passes the less may the elapsed time be; and when a star passes exactly through the zenith the two altitudes may be taken within a few minutes of each other. But, with the ordinary sextants, altitudes near 90° can not be taken with the artificial horizon, as the double altitude is then nearly 180°. A limit is thus placed upon the extreme altitude that it is practicable to observe.

The sextant should be set and the coincidences of the two images of the star awaited, as in the case of the sun's limb, and the times by chronometer or watch noted as usual.

327. Take the mean of the times before the meridian passage as the *A. M. Chronometer Time,* and the mean of those after the meridian passage as the *P. M. Chronometer Time.* The mean of these two (adding 12^h to the later one in case the chronometer has passed XII^h in the interval between sights) is the *Chronometer Time of Star's Transit.* At the instant of transit the local sidereal time will equal the right ascension of the star in case of the upper transit, or it will equal the right ascension *plus* 12^h in case of the lower transit. By converting local sidereal into Greenwich sidereal and thence into Greenwich mean time in the usual way, the chronometer error is found.

Example:—June 8, 1879, at Cape Town, Lat. 33° 56′ S., Long. 18° 28′ 40″ E., using sextant and artificial horizon, observed equal altitudes of star Antares before and after upper transit, as stated below. Required the chronometer error on Greenwich mean time.

Chro. A. M.	Altitudes.	Chro. P. M.
$7^h\ 32^m\ 10^s.5$	125° 30′	$11^h\ 34^m\ 20^s.3$
7 32 35.0	40	11 33 56.0
7 32 59.3	50	11 33 32.0

A. M. Chro. t.,	7 32 34.9
P. M. Chro. t.,	11 33 56.1
	2)19 06 31.0
Chro. t. Transit,	9 33 15.5
G. M. T. Transit,	9 59 30.9
Chro. slow,	26 15.4

P. M. Chro. t.,	11 33 56.1
L. S. T. (R. A. ✱),	$16^h\ 22^m\ 03^s.5$
Long.,	− 1 13 54.7
G. S. T.,	15 08 08.8
R. A. M. S., 0^h,	− 5 05 59.4
Sid. int. from 0^h,	10 02 09.4
Red. (Tab. 8),	− 1 38.5
G. M. T.,	10 00 30.9

[a] Suggested by Commander W. E. Sewell, U. S. Navy.

328. Degree of Dependence.—An error of 5′ in the latitude would not affect the corresponding part of the equation of equal altitudes by more than one-hundredth of its amount in the most unfavorable case, and in general would have no sensible effect. It is one of the advantages of the equal altitude method, therefore, that it does not require an accurate knowledge of the latitude. It is also plain that errors in the longitude affecting the declination and its hourly difference produce but small proportionate effects upon the computed equation. The absolute error of the chronometer on Greenwich will be affected by the whole error in the longitude, but the *rate* will still be correct. Hence, we conclude that by this method the chronometer may be accurately *rated* at a place whose latitude and longitude are both imperfectly known.

The chief source of error is in the observation itself. The best observers with the sextant can not depend on the noted time of a *single* contact within $0^s.5$, and hence the intervals between the successive chronometer times (which, if observations could be perfectly taken, would be sensibly equal) may differ 2^s. But the greatest probable error of the chronometer time of sun's or star's transit, from the mean of six such observations on each side of the meridian, is found to be not more than $0^s.2$, provided the rate of the chronometer between the observations is uniform.

CHAPTER XII.

LATITUDE.

BY MERIDIAN ALTITUDE.

329. The latitude of a place on the surface of the earth, being its angular distance from the equator, is measured by an arc of the meridian between the zenith and the equator; hence, if the zenith distance of any heavenly body when on the meridian be known, together with the declination of the body, the latitude can thence be found.

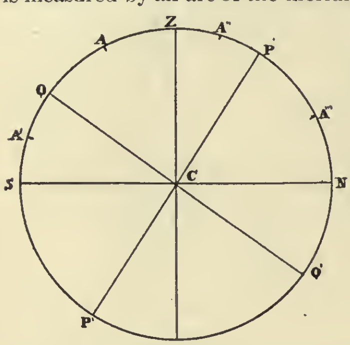

FIG. 42.

Let figure 42 represent a projection of the celestial sphere on the plane of the meridian NZS; C, the center of the sphere; NS, the horizon; P and P′, the poles of the sphere; QCQ′, the equator; Z, the zenith of the observer. Then, by the above definition, ZQ will be the latitude of the observer; and NP, the altitude of the elevated pole, will also equal the latitude.

Let A be the position of a heavenly body north of the equator, but south of the zenith; QA $=d$, its declination; AS $=h$, its altitude; and ZA $=z=90°-h$, its zenith distance.

From the figure we have:

$$\begin{aligned} QZ &= QA + AZ, \text{ or} \\ L &= d + z. \end{aligned}$$

By attending to the names of z and d, marking the zenith distance north or south according as the zenith is north or south of the body, the above equation may be considered general for any position of the body at upper transit, as A, A′, A″.

In case the body is below the pole, as at A‴—that is, at its lower culmination—the same formula may be used by substituting $180°-d$ for d. Another solution is given in this case by observing that:

$$\begin{aligned} NP &= PA''' + NA''', \text{ or} \\ L &= p + h. \end{aligned}$$

330. A common practice at sea is to commence observing the altitude of the sun's lower limb above the sea horizon about 10 minutes before noon, and then, by moving the tangent-screw, to follow the sun as long as it rises; as soon as the highest altitude is reached, the sun begins to fall and the lower limb will appear to *dip*. When the sun dips the reading of the limb is taken, and this is regarded as the meridian observation.

It will, however, be found more convenient, and frequently more accurate, for the observer to have his watch set for the local apparent time of the prospective noon longitude, or to know the error of the watch thereon, and to regard as the *meridian* altitude that one which is observed when the watch indicates noon. This will save time and try the patience less, for when the sun transits at a low altitude it may remain "on a stand" without appreciable decrease of altitude for several minutes after noon; moreover, this method contributes to accuracy, for when the conditions are such that the motion in altitude due to change of hour angle is a slow one, the motion therein due to change of the observer's latitude may be very material, and thus have considerable influence on the time of the sun's dipping. This error is large enough to take account of in a fast-moving vessel making a course in which there is a good deal of northing or southing.

In observing the altitude of any other heavenly body than the sun, the watch time of transit should previously be computed and the meridian altitude taken by time rather than by the dip. This is especially important with the moon, whose rapid motion in declination may introduce still another element of inaccuracy.

331. The watch time of transit for the sun, or other heavenly body, may be found by the forms given below, knowing the prospective longitude, the chronometer error, and the amount that the watch is slow of the chronometer.

For the Sun.

L. A. T. noon,		$0^h\ 00^m\ 00^s$
Long. (+ if west),	$\pm$	________
G. A. T.,		
Eq. t.,	$\pm$	________
G. M. T.,		
C. C. (sign reversed),	$\mp$	________
Chro. time,		
C—W,	—	________
Watch time noon,		

For other Bodies.

		h m s
L. S. T. transit,		(Right ascension.)
Long. (+ if west),	$\pm$	________
G. S. T.,		
R. A. M. S., 0^h,	—	________
Sid int. from 0^h,		
Red. (Tab. 8),	—	________
G. M. T.,		
C. C. (sign reversed),	$\mp$	________
Chro. time,		
C—W,	—	________
Watch time transit,		

332. From the observed altitude deduce the true altitude, and thence the true zenith distance. Mark the zenith distance North if the zenith is north of the body when on the meridian, South if the zenith is south of the body.

Take out the declination of the body from the Nautical Almanac for the time of meridian passage, having regard for its proper sign or name.

The algebraic sum of the declination and zenith distance will be the latitude. Therefore, add together the zenith distance and the declination if they are of the same name, but take their difference if of opposite names; this sum or difference will be the latitude, which will be of the same name as the greater.

EXAMPLE: At sea, June 21, 1879, in Long. 60° W., the observed meridian altitude of the sun's lower limb was 40° 4′; sun bearing south; I. C., +3′ 0″; height of the eye, 20 feet; required the latitude.

Obs. alt.,	40° 04′ 00″	S. D.,	+ 15′ 46″	Dec.,	23° 27′ 20″.5 N. at G.A. noon
Corr.,	+ 13 21	I. C.,	+ 3 00		
				H. D., +	0″.32
h,	40 17 21		+ 18 46	Long.,	4^h.
z,	49° 42′ 39″ N.	dip,	− 4′ 23″	Corr., +	1″.28
d,	23 27 22 N.	$p.$ & $r.$,	− 1 02		
				Dec.,	23° 27′ 22″
L,	73 10 01 N.		− 5 25		
		Corr.,	+ 13′ 21″		

EXAMPLE: At sea, April 14, 1879, in Long. 140° E., the observed meridian altitude of the sun's lower limb was 81° 15′ 30″; sun bearing north; I. C.,—2′ 30″; height of the eye, 20 feet.

Obs. alt.,	81° 15′ 30″	S. D.,	+ 15′ 59″	Dec.,	9° 22′ 35″.4 N.
Corr.,	+ 8 59				
		dip,	− 4 23	H. D., +	54″.03
h,	81 24 29	$p.$ & $r.$,	− 0 07	Long., −	9^h.33
		I. C.,	− 2 30		
z,	8° 35′ 31″ S.			Corr., −	{ 504″.1 / 8′ 24″.1
d,	9 14 11 N.		− 7 00		
L,	0 38 40 N.	Corr.,	+ 8′ 59″	Dec.,	9° 14′ 11″ N.

EXAMPLE: At sea, May 15, 1879, Long. 0°, the observed meridian altitude of the sun's lower limb was 30° 13′ 10″; sun bearing north; I. C., +1′ 30″; height of the eye, 15 feet.

Obs. alt.,	30° 13′ 10″	S. D.,	+ 15′ 51″	Dec., Gr. 0^h,	18° 50′ 48″.5 N.
Corr.,	+ 12 02	I. C.,	+ 1 30		
h,	30 25 12		+ 17 21		
z,	59° 34′ 48″ S.	dip,	− 3′ 48″		
d,	18 50 49 N.	$p.$ & $r.$,	− 1 31		
L,	40 43 59 S.		− 5 19		
		Corr.,	+ 12′ 02″		

EXAMPLE: January 1, 1879, the observed meridian altitude of Sirius was 53° 23′ 40″, bearing south; I. C., +5′ 0″; height of the eye, 17 feet.

Obs. alt.,	53° 23′ 40″	I. C.,	+ 5′ 00″	Dec. ✱,	16° 33′ 04″ S.
Corr.,	+ 15				
		dip,	− 4′ 02″		
h,	53 23 55	ref.,	− 43		
z,	36° 36′ 05″ N.		− 4 45		
d,	16 33 04 S.				
		Corr.,	+ 0′ 15″		
L,	20 03 01 N.				

EXAMPLE: June 13, 1879, in Long. 65° W., and in a high northern latitude, the meridian altitude of the sun's lower limb was 8° 16′ 10″, below the pole; height of the eye, 20 feet; I. C., 0′ 00″.

Greenwich apparent time of lower culmination, June 13, 16^h 20^m (= Long. + 12^h).

Obs. alt.,	8° 16′ 10″	S. D.,	+ 15′ 47″	Dec.,	23° 13′ 03″.8 N.
Corr.,	+ 5 12				
		dip,	− 4 23	H. D., +	8″.58
h,	8 21 22	$p.$ & $r.$,	− 6 12	G. M. T.,	16^h .33
z,	81° 38′ 38″ S.		− 10 35	Corr., +	{ 140″.5 / 2′ 20″.5
180°−d,	156 44 36 N.				
		Corr.,	+ 5 12		
	75 05 58 N.			Dec.,	23° 15′ 24″ N.
Alternative method.					
h,	8° 21′ 22″			p,	66° 44′ 36″
p,	66 44 36				
				180°−d,	156° 44′ 36″
L,	75 05 58 N.				

EXAMPLE: June 26, 1879, in Long. 80° W., the observed meridian altitude of the moon's upper limb was 59° 6′ 40″, bearing south; I. C., + 2′ 0″; height of the eye, 19 feet.

h, 59° 18′ 00″	Obs. alt., .	59° 06′ 40″	G. M. T., Gr. trans.,	$5^{h}\ 27^{m}.6$	Dec. (11^{h}),	4° 51′ 36″.5 S.
			Corr. for Long (Tab. 11), +	11 .0		
z, 30° 42′ 00″ N.	I. C.,	+ 2′ 00″			M. D., −	15″.07
d, 4 51 06 S.			L. M. T., local trans.,	5 38 .0	No. min., −	$2^{m}.0$
	S. D.,	− 16′ 03″	Long.,	+ 5 20 .0		
L, 25 50 54 N.	Aug.,	− 14			Corr., +	30″.1
	dip,	− 4 16	G. M. T., local trans.,	+ 10 58 .0		
					Dec.,	4° 51′ 06″ S.
		− 20 33				
	1st Corr.,	− 18′ 33″				
	Approx. alt.,	58° 48′ 07″			Hor. Par.,	58′ 46″.3
	p. & r. (Tab. 24), +	29 53				
	h,	59 18 00				

EXAMPLE: At sea, September 16, 1879, in Long. 75° E., the observed meridian altitude of Jupiter was 51° 25′ 24″, bearing north; I. C., + 3′ 0″; height of the eye, 16 feet.

Obs. alt.,	51° 25′ 24″	par., + 0′ 01″	G. M. T., Gr. trans.,	$10^{h}\ 49^{m}.8$	Dec.,		10° 44′ 20″.5 S.
Corr.,	− 1 41	I. C., + 3 00	Corr. for Long.,	+ 0 .9			
					H. D.,	−	6″.58
h,	51 23 43	+ 3 01	L. M. T., local trans.,	10 50 .7	G. M. T.,		$5^{h}.84$
			Long.,	− 5 00 .0			
z,	38° 36′ 17″ S.	dip, − 3′ 55″			Corr.,	−	38″.43
d,	10 44 59 S.	ref., − 47	G. M. T. local trans.,	5 50 .7			
					Dec.,		10° 44′ 59″ S.
L,	49 21 16 S.	− 4 42					
					H. P.,		2″.2
		Corr., − 1′ 41″			par. (Tab. 17),		1″

333. CONSTANT.—In working a meridian altitude, especially the daily noon observation of the sun, it is frequently a convenience to so arrange the terms of the problem that all computation, excepting the application of the observed altitude, is completed beforehand; then the ship's latitude will be known immediately after the sight has been taken, it being necessary only to add or subtract the altitude.

It is assumed that the noon longitude will be sufficiently accurately known in advance to enable the navigator to correct the declination; also the approximate meridian altitude to correct the parallax and refraction; if the latter is not known, it may readily be found from the declination and approximate latitude.

Generally speaking,

$$\begin{aligned}\text{Lat.} &= \text{Zenith distance} + \text{Dec.},\\ &= 90° - \text{True alt.} + \text{Dec.},\\ &= 90° - (\text{Obs. alt.} + \text{Corr.}) + \text{Dec.},\\ &= (90° + \text{Dec.} - \text{Corr.}) - \text{Obs. alt.},\end{aligned}$$

in which the quantity (90° + Dec. — Corr.) may be termed a *Constant* for the meridian altitude of the day, as it remains the same regardless of what the observed altitude may prove to be. The constant having been worked up before the observation is made, the latitude will be known as soon as the observed altitude is applied.

To avoid the confusion that might arise from the necessity of combining the terms *algebraically* according to their different names, it may be convenient to divide the problem into four cases and lay down rules for the *arithmetical* combination of the terms, disregarding their respective names as follows:

Case I. Lat. and Dec. same name, Lat. greater, + 90° + Dec. — Corr. — Obs. alt.
Case II. Lat. and Dec. same name, Dec. greater, — 90° + Dec. + Corr. + Obs. alt.
Case III. Lat. and Dec. opposite names, + 90° — Dec. — Corr. — Obs. alt.
Case IV. Lat. and Dec. same name, lower transit, + 90° — Dec. + Corr. + Obs. alt.

The correctness of such an arrangement will become readily apparent from an inspection of figure 42. The assumption has been made that the correction to the observed altitude is positive; when this is not true the sign of the correction must be reversed.

As examples of this method, the first, second, third, and fifth of the examples previously given illustrating the meridian altitude will be worked, using the constant; the details by which Corr. and Dec. are obtained are omitted, being the same as in the originals.

1ST EXAMPLE.		2D EXAMPLE.		3D EXAMPLE.		5TH EXAMPLE.	
	Case I.		*Case II.*		*Case III.*		*Case IV.*
	+ 90° 00′ 00″		− 90° 00′ 00″		+ 90° 00′ 00″		+ 90° 00′ 00″
Dec.,	+ 23 27 22	Dec.,	+ 9 14 11	Dec.,	− 18 50 49	Dec.,	− 23 15 24
Corr.,	− 13 21	Corr.,	+ 8 59	Corr.,	− 12 02	Corr.,	+ 5 12
Constant,	+ 113 14 01	Constant,	− 80 36 50	Constant,	+ 70 57 09	Constant,	+ 66 49 48
Obs. alt.,	− 40 04 00	Obs. alt.,	+ 81 15 30	Obs. alt.,	− 30 13 10	Obs. alt.,	+ 8 16 10
Lat.,	73 10 01 (N.)	Lat.,	0 38 40 (N.)	Lat.,	40 43 59 (S.)	Lat.,	75 05 58 (N.)

BY REDUCTION TO THE MERIDIAN.

334. Should the meridian observation be lost, owing to clouds or for other reason, altitudes may be taken near the meridian and the times noted by a watch compared with the chronometer, from which, knowing the longitude, the hour angle may be deduced.

If the observations are within 26^m from the meridian, before or after, the correction to be applied to the observed altitude to reduce it to the meridian altitude may be found by inspection of Tables 26 and 27. Table 26 contains the variation of the altitude for one minute from the meridian, expressed in seconds and tenths of a second. Table 27 contains the product obtained by multiplying the square of the minutes and seconds by the change of altitude in one minute.

Let a = change of altitude (in seconds of arc) in one minute from the meridian:
H = meridian altitude;
h = corrected altitude at observation; and
t = interval from meridian passage.

The value of the reduction to the meridian altitude of each altitude is found by the formula:

$$H = h + at^2,$$

a being found in table 26, and at^2 in Table 27; hence the following rule:

Find the hour angle of the body in minutes and seconds of time. Take from Table 26 the value of a corresponding to the declination and the latitude. Take from Table 27 the value of at^2 corresponding to the a thus found and to the interval, in minutes and seconds, from meridian passage. This quantity will represent the amount necessary to reduce the corrected altitude at the time of observation to the corrected altitude at the meridian passage; it is always additive when the body is near upper transit, and always to be subtracted when near lower transit.

If the mean of a number of sights is to be taken, determine each reduction separately, take the mean of all the reductions, and apply it to the mean of the altitudes; it is incorrect, in such a case, to take the mean of the times and work the sight with this single value of t. The differences of altitude being small, the parallax and refraction will be sensibly the same for all, and one computation of the correction to the observed altitude will suffice.

Knowing the meridian altitude, the latitude is to be found as previously explained.

335. When several sights are taken, the most expeditious method of calculating will be to find first the watch time of transit, and thence obtain the hour angle of each observation by comparing the watch time of observation. The watch time of transit may be found as already explained (art. 331) for computing that quantity as a guide in taking the meridian altitude, but the hour angle thus obtained is subject to a correction. The difference between watch time of transit and watch time of observation gives the watch time—that is, the mean time—elapsing between transit and observation. A fixed star covers in that time an angle corresponding to the sidereal and not to the mean time interval, and a reduction should be made accordingly to give its true hour angle at the instant of observation. A planet's hour angle should be corrected in the same way (for we may disregard its very small change in right ascension). The correction may be entirely neglected in the case of the sun, as the difference between mean and apparent time intervals is immaterial. The reduction of the hour angle in the case of the moon becomes rather cumbersome, so much so that it is better to find the hour angle of this body by the more usual method of converting watch time to G. M. T., and thence to L. S. T., and finding the difference between the latter and the R. A.; an additional reason for this is that the G. M. T. of observation must be known exactly, with the moon, for the correction of the declination (art. 338).

336. Table 26 includes values of the latitude up to 60°, and those of the declination up to 63°, thus taking in all frequented waters of the globe and all heavenly bodies that the navigator is likely to employ. No values of a are given when the altitudes are above 86° or below 6°, as the method of reduction to the meridian is not accurate when the body transits very near the zenith, and the altitudes themselves are questionable when very low. In case it is desired to find the change of altitude in one minute from noon for conditions not given in the tables, it may be computed by the formula:

$$a = \frac{1''.9635 \cos L \cos d}{\sin (L - d)}.$$

In working sights by this method where great accuracy is required, as in determining latitudes on shore for surveying purposes, it is well to compute the a rather than to take it from the table, as one is thus enabled to employ the value as found to the second decimal place.

Due regard must be paid to the names of the declination and latitude in working this formula; if they are of opposite names, the declination is negative, and L and d should be added together to obtain $L - d$.

337. Table 27 contains values of at^2 up to the limits within which the method is considered to apply with a fair degree of accuracy. It must not be understood that the plan of reduction to the meridian is not available for wider limits, but it would seem preferable to employ the $\varphi' \ \varphi''$ formula, described hereafter, when the hour angle falls beyond that for which the table is computed. On the other hand, the reduction is not exact in all cases covered by the table; while sufficiently so for sea navigation, the limits given are far too wide for the precise determinations required in surveying, where the aim should be to observe bodies under such conditions that the total reduction at^2 shall not exceed 1′.

338. It should be kept clearly in mind when employing the method of reduction to the meridian that the resulting latitude is that of the ship at the instant of observation, and to bring it up to noon the run must be applied. The declination should properly be corrected for the instant of observation; with the sun or a planet, it is sufficiently accurate to use the declination at meridian passage, unless the interval from the meridian be quite large; but the moon's declination changes so rapidly that the exact time of observation must be used in its correction when working with this body.

6583—06——7

EXAMPLE: In latitude 47° S., having previously worked up the constant for meridian altitude, 78° 42′ 10″, observed altitude of sun near meridian, 31° 11′ 50″; Dec. 11° N.; watch time, $11^h\ 40^m\ 21^s$, watch fast of L. A. T., 7^s. Find the latitude.

Watch time,	$11^h\ 40^m\ 21^s$	Obs. alt.,	31° 11′ 50″	a (Tab. 26),	1.″6
Watch fast,	07	at^2, +	10 24		
L. A. T.,	11 40 14	Mer. alt.,	31 22 14	at^2 (Tab. 27),	1.″0 = 6′ 30″
		Constant,	78 42 10		. 6 = 3 54
t,	$19^m\ 46^s$	Lat.,	47 19 56 S.		1. 6 = 10 24

EXAMPLE: At sea, July 12, 1879, in Lat. 50° N., Long. 40° W., observed circum-meridian altitude of the sun's lower limb, 61° 48′ 30″, the time by a chronometer regulated to Greenwich mean time being $2^h\ 41^m\ 39^s$; chro. corr., $-2^m\ 30^s$; I. C., $-3′\ 0″$; height of the eye, 15 feet. Find the latitude.

Chro. t.,	$2^h\ 41^m\ 39^s$	☉	61° 48′ 30″	Dec.,	22° 00′ 23″.2 N.	Eq. t.,	$5^m\ 17^s.99$
C. C.,	− 2 30	Corr.,	+ 8 31	H.D., −	20″.7	H. D.,	+ $0^s.32$
G.M.T.,	2 39 09	h,	61 57 01	Long.,	$2^h.7$	Long.,	$2^h.7$
Eq. t.,	− 5 19						
G. A. T.,	2 33 50	S. D.,	+ 15′ 46″	Corr., −	55″.9	Corr.,	+ .86
Long.,	− 2 40 00	dip,	− 3 48	Dec.,	21° 59′ 27″ N.	Eq. t.,	$5^m\ 18^s.9$
		$p.\ \&\ r.$,	− 0 27				(*Subtract* from *mean* time.)
L. A. T.,	11 53 50	I. C.,	− 3 00				
t,	6 10		− 7 15				
		Corr.,	+ 8 31			a (Tab. 26),	2.″5

h,	61° 57′ 01″	at^2 (Tab. 27),	2.″0 = 1′ 16″
at^2, +	1 35		0. 5 = 0 19
H,	61 58 36		2. 5 = 1 35
z,	28 01 24 N.		
d,	21 59 27 N.		
L,	50 00 51 N.		

EXAMPLE: May 31, 1879, in Lat. 30° 25′ N., Long. $5^h\ 25^m\ 42^s$ W., about 9 p. m., observed with a sextant and artificial horizon a series of altitudes of Spica; mean observed double altitude 98° 06′ 34″; noted times as enumerated below by a watch compared with a chronometer which was $2^m\ 33^s$ fast of G. M. T.; C—W, $5^h\ 29^m\ 40^s$; I. C., $-3′\ 00″$. Find the latitude.

R. A. ✱ (L. S. T. transit),	$13^h\ 18^m\ 52^s.2$	Mean 2 alt. ✱,	98° 06′ 34″	R. A. ✱,	$13^h\ 18^m\ 52^s.2$
Long.,	+ 5 25 42	I. C.,	− 3 00	Dec.,	10° 32′ 04″ S.
G. S. T.,	18 44 34 .2		2)98 03 34	a (Tab. 26),	2″.5
R. A. M. S. Gr. 0^h,	4 34 26 .9		49 01 47		
Sid. int. from 0^h,	14 10 07 .3	ref.,	− 50		
Red. (Tab. 8),	− 2 19 .4	h,	49 00 57		
G. M. T.,	14 07 47 .9				
C. C. (sign reversed),	+ 2 33				
Chro. time transit,	14 10 20 .9				
C—W,	− 5 29 40				
Watch time transit,	8 40 41				

	Intervals from transit.		at^2 (Tab. 27).				
Watch times.	Mean time.	Sid. time.	2.0	0.5	2.5		
$8^h\ 31^m\ 18^s.0$	− $9^m\ 23^s.0$	− $9^m\ 24^s$	2′ 56″	0′ 44″	3′ 40″	h,	49° 00′ 57″
33 19 .5	7 21 .5	7 23	1 49	0 27	2 16	at^2, +	1 40
36 07 .0	4 34 .0	4 35	0 42	0 10	0 52	H,	49 02 37
38 50 .0	1 51 .0	1 51	0 07	0 01	0 08		
41 07 .5	+ 0 26 .5	+ 0 27	0 01	0 00	0 01	z,	40 57 23 N.
43 45 .5	3 04 .5	3 05	0 19	0 04	0 23	d,	10 32 04 S.
45 46 .0	5 05 .0	5 06	0 52	0 13	1 05		
47 33 .0	6 52 .0	6 53	1 35	0 23	1 58	L,	30 25 19 N.
51 12 .5	10 31 .5	10 33	3 42	0 55	4 37		
					9)15 00		
					1 40		

Example: August 6, 1879, Lat. 59° S., Long. 175° 27′ E., during evening twilight, observed an altitude of Achernar, near lower transit, 26° 52′; watch time, $4^h\ 31^m\ 12^s$; C—W, $0^h\ 18^m\ 07^s$; chro. fast of G. M. T., $12^m\ 42^s$; I. C., +1′ 20″; height of eye, 24 ft. Find hour angle by both methods; thence the latitude.

R. A. ✱ + 12^h } L. S. T. lower trans. }		$13^h\ 33^m\ 15^s.4$
Long.,	—	11 41 48
G. S. T.,		1 51 27 .4
R. A. M. S. Gr. $5^d 0^h$,	—	8 54 39 .8
Sid. int.,		16 56 47 .6
Red. (Tab. 8),	—	2 46 .6
G. M. T.,		16 54 01 .0
C. C. (sign reversed),	+	12 42
Chro. time,		5 06 43
C—W,	—	0 18 07
Watch time transit,		4 48 36
Watch time obs.,		4 31 12
t { Mean time,		17 24
t { Sid. time,		17 27

Watch time,		$4^h\ 31^m\ 12^s$
C—W,	+	0 18 07
Chro. t.,		4 49 19
C. C.,	—	12 42
G. M. T. 5^d,		16 36 37
R. A. M. S. Gr. $5^d 0^h$,	+	8 54 39 .8
Red. (Tab. 9),	+	2 43 .7
G. S. T.,		1 34 00 .5
Long.,	+	11 41 48
L. S. T.,		13 15 48 .5
R. A. ✱ + 12^h,		13 33 15 .4
t,		17 27

Obs. alt. ✱,		26° 52′ 00″
I. C.,	+	1′ 20″
dip,	—	4′ 48″
ref.,	—	1 55
	—	6 43
Corr.,	—	5′ 23″
h,		26° 46′ 37″
at^2,	—	3 03
H,		26 43 34
p,		32 09 32
L,		58 53 06 S.

R. A. ✱,	$1^h\ 33^m\ 15^s.4$
Dec.,	57° 50′ 28″ S.
p,	32° 09′ 32″
a (Tab. 26),	0″.6
at^2 (Tab. 27),	3′ 03″

BY A SINGLE ALTITUDE AT A GIVEN TIME.

339. This observation should be limited to conditions where the body is within three hours of meridian passage and where it is not more than 45° from the meridian in azimuth; also where the declination is at least 3°. On the prime vertical the solution by this method is inexact, and when the hour angle is 6^h, or the declination 0°, it is impracticable.

The problem is: Given the hour angle, declination, and altitude, to find the latitude. The solution is accomplished by letting fall, in the usual astronomical triangle, a perpendicular from the body to the meridian, and considering separately the distances on the meridian, from the pole and zenith, respectively, to the point of intersection of the perpendicular; the sum or difference of these distances is the co-latitude.

Following the usual designation of terms and introducing the auxiliaries φ' and φ'', the formulæ are as follows:

$$\tan \varphi'' = \tan d \sec t;$$
$$\cos \varphi' = \sin h \sin \varphi'' \operatorname{cosec} d;$$
$$L = \varphi' + \varphi''.$$

The terms φ' and φ'' will have different directions of application according to the position of the body relatively to the observer. From a knowledge of the approximate latitude, the method of combining them will usually be apparent; it is better, however, to have a definite plan for so doing, and this may be based upon the following rule:

Mark φ'' north or south, according to the name of the declination; mark φ' north or south, according to the name of the zenith distance, it being *north* if the body bears south and east or south and west, and *south* if the body bears north and east or north and west. Then combine φ'' and φ' according to their names; the result will be the latitude, except in the case of bodies near lower transit, when $180° - \varphi''$ must be substituted for φ'' to obtain the latitude.

It may readily be noted that if we substitute φ'' for declination and φ' for zenith distance, the problem takes the form of a meridian altitude; indeed, the method resolves itself into the finding of the zenith distance and declination of that point on the meridian at which the latter is intersected by a perpendicular let fall from the observed body.

The time should be noted at the instant of observation, from which is found the local time, and thence the hour angle of the celestial object.

If the sun is observed, the hour angle is the L. A. T. in the case of a p. m. sight, or 12^h − L. A. T. for an a. m. sight. If any other body, the hour angle may be found as hitherto explained.

Example: June 7, 1879, in Lat. 30° 25′ N., Long. 81° 25′ 30″ W., by account; chro. time, $6^h\ 22^m\ 52^s$; obs. ⊙ 75° 13′, bearing south and east; I. C. — 3′ 00″; height of the eye, 25 feet; chro. corr. — $2^m\ 36^s$. Find the latitude.

Chro. t.,	$6^h\ 22^m\ 52^s$	Obs. alt. ⊙,	75° 13′ 00″	Dec.,	22° 45′ 09″.9 N.	Eq. t.,	$1^m\ 28^s.85$
C. C.,	— 2 36	Corr.,	+ 7 40				
				H. D.,	+ 14″.6	H. D.,	— $0^s.46$
G. M. T.,	6 20 16	h,	75 20 40	G. M. T.,	+ $6^h.3$	G. M. T.,	+ $6^h.3$
Eq. t.,	+ 1 26						
		S. D.,	+ 15′ 48″	Corr.,	{ + 91″.98 ; + 1′ 32″	Corr.,	— $2^s.85$
G. A. T.,	6 21 42						
Long.,	— 5 25 42	dip,	— 4′ 54″			Eq. t.,	$1^m\ 26^s.0$
		$p.\ \&\ r.$,	— 14	Dec.,	22° 46′ 42″ N.	(*Add* to *mean* time.)	
L. A. T. = t,	{ $0^h\ 56^m\ 00^s$ E. ; 14° 00′ 00″	I. C.,	— 3 00				
			— 8 08				
		Corr.,	+ 7′ 40″				

t	14° 00′ 00″	sec	.01310		
d	22 46 42	tan	9.62317	cosec	.41210
h	75 20 40			sin	9.98563
φ''	23 24 07 N.	tan	9.63627	sin	9.59898
φ'	7 02 30 N.			cos	9.99671
Lat.	30 26 37 N.				

Example: May 28, 1879, p. m., in Lat. 6° 20′ S. by account, Long. 30° 21′ 30″ W.; chro. time, $7^h\ 35^m\ 10^s$; observed altitude of moon's upper limb, 75° 33′ 00″, bearing north and east; I. C., — 3′ 00″; height of eye, 26 feet; chro. fast of G. M. T., $1^m\ 37^s.5$. Required the latitude.

Chro. t.,	$7^h\ 35^m\ 10^s$	Obs. alt. ☾,	75° 33′ 00″	R. A. ☾,	$10^h\ 21^m\ 07^s.78$	Dec.,	6° 49′ 52″.4 N.
C. C.,	— 1 37.5						
		S. D.,	— 15′ 51″	M. D.,	+ $2^s.06$	M. D.,	— 14″.46
G. M. T.,	7 33 32.5	Aug.,	— 0 16	No. min.,	$33^m.54$	No. min.,	$33^m.54$
R. A. M. S.,	+ 4 22 37.3	dip,	— 5 00				
Red. (Tab. 9),	+ 1 14.5	I. C.,	— 3 00	Corr.,	+ { $69^s.09$; $1^m\ 09^s$	Corr.,	— { 485″ ; 8′ 05″
G. S. T.,	11 57 24.3	1st Corr.,	— 24 07			Dec.,	6° 41′ 47″ N.
R. A. ☾,	— 10 22 17			R. A.,	$10^h\ 22^m\ 17^s$		
H. A. from Gr.,	1 35 07 W.	Approx. alt.,	75° 08′ 53″				
Long.,	2 01 26 W.	$p.\ \&\ r.$ (Tab. 24),	+ 14 37			Hor. Par.,	58′ 03″
		h,	75 23 30				
t,	{ $0^h\ 26^m\ 19^s$ E. ; 6° 34′ 45″						

t	6° 34′ 45″	sec	.00286		
d	6 41 47	tan	9.06973	cosec	.93324
h	75 23 30			sin	9.98573
φ''	6 44 26 N.	tan	9.07259	sin	9.06959
φ'	13 05 40 S.			cos	9.98856
Lat.	6 21 14 S.				

Example: August 6, 1879, p. m., in Lat. 52° 47′ S. by D. R., Long. 146° 32′ E., observed altitude of Achernar, near lower transit, 24° 01′ 20″ bearing south and west; watch time, $6^h\ 48^m\ 22^s$; C—W, $9^h\ 46^m\ 27^s$; chro. corr. on G. M. T., + $1^m\ 57^s$; height of eye, 18 feet; I. C. + 1′ 00″. Find the latitude.

Watch time,	$6^h\ 48^m\ 22^s$	Obs. alt. ✱,	24° 01′ 20″	R. A. ✱,	$1^h\ 33^m\ 15^s.3$
C−W,	+ 9 46 27	Corr.,	— 5 19		
				Dec.,	57° 50′ 28″ S.
Chro. t.,	4 34 49	h,	23 56 01		
C. C.,	+ 1 57				
		I. C.,	+ 1′ 00″		
G. M. T., 5^d,	16 36 46				
R. A. M. S.,	+ 8 54 39.8	dip,	— 4′ 09″		
Red. (Tab. 9),	+ 2 43.7	ref.,	— 2 10		
			— 6 19		
G. S. T.,	1 34 09.5				
R. A. ✱,	1 33 15.3				
		Corr.,	— 5′ 19″		
H. A. from Gr.,	0 00 54 W.				
Long.,	9 46 08 E.				
H. A.,	9 47 02 W.				
	{ $2^h\ 12^m\ 58^s$; 33° 14′ 30″				

t	33° 14′ 30″	sec .07760			
d	57 50 28	tan .20153	cosec	.07233
h	23 56 01		sin	9.60818
$180°-\varphi''$	117 44 18 S.	tan .27913	sin	9.94699
φ'	64 54 15 N.		cos	9.62750
Lat.	52 50 03 S.			

BY THE POLE STAR.

340. This method, confined to northern latitudes, is available when the star Polaris and the horizon are distinctly visible, the time of the observation being noted at the moment the altitude is measured.

Two methods will be given. The first is sufficiently precise for nautical purposes, involving the computation of the formula:

$$L = h - p \cos t,$$

in which,

h = true altitude, deduced from the observed altitude;
p = polar distance $= 90° - d$, the apparent declination being taken from the Nautical Almanac for the date;
t = star's hour angle.

Find the right ascension and declination of Polaris from the Nautical Almanac; then find the hour angle in the usual way.

To the log cosine of the hour angle add the logarithm of the polar distance in minutes; the number corresponding to the resulting logarithm will be a correction in minutes to be subtracted from the star's true altitude to find the latitude.

Attention must be paid to the sign of the correction $p \cos t$. If t is more than 6^h and less than 18^h, the sign of $\cos t$ is $-$; hence the formula becomes arithmetically:

$$L = h + p \cos t.$$

Example: June 11, 1879, from an observed altitude of Polaris the true altitude was found to be 29° 5′ 55″. The time noted by a Greenwich chronometer was $13^h\ 41^m\ 26^s$; chro. corr. $-2^m\ 22^s$; Long. $5^h\ 25^m\ 42^s$ W.

Chro. time,	$13^h\ 41^m\ 26^s$
C. C.,	$-$ 2 22
G. M. T., 11^d,	13 39 04
R. A. M. S.,	+ 5 17 49
Red. (Tab. 9),	+ 2 15
G. S. T.,	18 59 08
R. A. ✳,	$-$ 1 14 04
H. A. from Gr.,	17 45 04 W.
Long.,	5 25 42 W.
H. A.,	12 19 22 W.
t,	$\begin{cases} 11^h\ 40^m\ 38^s \text{ E.} \\ 175°\ 09'\ 30'' \end{cases}$

h,	29° 05′ 55″
$p \cos t$,	+ 1 19 54
Lat.,	30 25 49 N.

R. A. ✳,		$1^h\ 14^m\ 04^s$
Dec.,		88° 39′ 47″ N.
p,		$\begin{cases} 1°\ 20'\ 13'' \\ 80'.2 \end{cases}$
p, 80′.2	log	1.90417
t, 175° 09′ 30″	cos	($-$) 9.99845
$p \cos t, -$	$\begin{cases} 79'.9 \text{ log } (-) \\ 1°\ 19'\ 54'' \end{cases}$	1.90262

341. The second method is more rigorous, and should be employed when greater accuracy is sought. It is embodied in Table 28.

Reduce the observed altitude of the star to the true altitude. Find from the Nautical Almanac the apparent right ascension and declination of the star at the time of observation. Find the hour angle in the usual manner.

With the hour angle take out the *first correction*, A, from Table 28, giving to it the sign $-$ when the hour angle is numerically less than 6^h; the sign + when the hour angle is greater than 6^h.

With the hour angle and altitude take out the *second correction*, B, from Table 28. The sign of this correction is always +. (If the altitude is greater than 60°, this correction may be found by taking that for 45° and multiplying it by the tangent of the altitude; adding, if desirable, the second term in the expression for B, viz: $+ 0''.0076 \sin^4 t \tan^3 h$.)

With B and the declination take out the *third correction*, C, from Table 28, giving it the sign + when the declination is less than 88° 48′; $-$ when the declination is greater than 88° 48′.

With A and the declination take out the *fourth correction*, D, from Table 28, giving it the same sign as that of A when the declination is less than 88° 48′; the opposite sign when the declination is greater than 88° 48′.

Combine these corrections with the true altitude according to their signs; the result is the latitude of the place of observation.

If, when several sights are taken, great precision is required, or the intervals are great, it will be necessary to take out the *first* and *second* corrections for each observation separately; in other cases the

mean of the times may be used. The means of these two corrections may always be used for finding the *third* and *fourth* corrections; and these four quantities may be combined with the mean of the altitudes.

If the nearest 10″ suffices for each, the corrections may be taken out for the nearest arguments without interpolation, and all but the *first* may thus be taken out when a precision of 3″ is required. If a precision of 1′ is sufficient for each correction, as is ordinarily the case at sea, an hour angle within 3^m will suffice for A; C and D may be neglected, and B used only when the altitude exceeds 47°.

Example: January 1, 1903, about 9 p. m., Longitude 79° 54′ 07″ W., observed double altitude of Polaris with artificial horizon, 81° 57′ 20″; chro. time $1^h\ 55^m\ 12^s$; chro. corr. on G. M. T. $+1^m\ 07^s$; I. C. $-0'\ 50''$. (The necessary quantities, taken from the Nautical Almanac for 1903, are given below.) Required the latitude.

Chro. time,		1^h	55^m	12^s
C. C.,	+		1	07
G. M. T.,		13	56	19
R. A. M. S.,	+	18	39	50.9
Red. (Tab. 9),	+		2	17.4
G. S. T.,		8	38	27.3
R. A. ✳,		1	24	33.3
H. A. from Gr.,		7	13	54 W.
Long.,		5	19	37 W.
H. A.,		1	54	17 W.

Obs. 2 alt. ✳,		81°	57′	20″
I. C.,	−		0	50
		2)81	56	30
		40	58	15
ref.,	−		1	07
h,		40	57	08
A,	−	1	03	13.9
B,	+			08.9
C,				00.0
D,	−			15.7
Lat.,		39	53	47 N.

R. A. ✳,	$1^h\ 24^m\ 33^s.3$
Dec.,	88° 47′ 42″ N.

CHAPTER XIII.

LONGITUDE.

342. The *longitude* of a position on the earth's surface is measured by the arc of the equator intercepted between the *prime meridian* and the meridian passing through the place, or by the angle at the pole between those two meridians.

Meridians are great circles of the terrestrial sphere passing through the poles.

The *prime meridian* is that one assumed as the origin, passing through the location of some principal observatory, such as Greenwich, Paris, or Washington. That of Greenwich is the prime meridian not only for English but also for American navigators, and those of many other nations.

Secondary meridians are those connected with the primary meridian, directly or indirectly, by exchange of telegraphic time signals.

Tertiary meridians are those connected with secondaries by carrying time in the most careful manner with all possible corrections.

Longitude is found by taking the difference between the hour angle of a celestial body from the prime meridian and its hour angle, at the same instant, from the local meridian. In determinations ashore the hour angle from the prime meridian may be found either from chronometers or from telegraphic signals; the local hour angle may be found by transit instruments or by sextant. In determinations at sea the chronometer and sextant give the only means available.

DETERMINATION ASHORE.

343. Telegraphic Determination of Secondary Meridians.—In order to locate with accuracy the positions of prominent points on the coasts, it is necessary to refer them, by chronometric measurements, to secondary meridians of longitude which have been determined with the utmost degree of care.

Before the establishment of telegraphic cables, this was attempted principally through the observation of moon culminations, which seemed always to carry with them unavoidable errors, or by transporting to and fro a large number of chronometers between the principal observatory and the position to be located; and in this method it can be conceived that errors would be involved, no matter how thorough the theoretical compensation for error of the instruments.

By the aid of the electric telegraph, differences of longitude are determined with great accuracy, and an ever-increasing number of secondary meridional positions are thus established over the world; these afford the necessary bases in carrying on the surveys to map correctly the various coast lines, and render possible the publication of reliable and accurate navigators' charts.

344. To determine telegraphically the difference of longitude between two points, a small observatory containing a transit instrument, chronograph, break-circuit sidereal chronometer, and a set of telegraph instruments is established at each of the two points, and, being connected by a temporary wire with the cable or land line at each place, the two observatories are placed in telegraphic communication with each other.

By means of transit observations of stars, the error of the chronometer at each place on its own local sidereal time is well determined, and the chronometers are then accurately compared by signals sent first one way and then the other, the times of sending and receiving being very exactly noted at the respective stations. The error of each chronometer on local sidereal time being applied to its reading, the difference between the local times of the two places may be found, and consequently the difference of longitude. The time of transmission over the telegraph line is eliminated by sending signals both ways. By the employment of chronometers keeping sidereal time, the computation is simplified, though mean-time chronometers may be used.

345. Establishment of Tertiary Meridians.—Let it be supposed that the meridional distance between A and B is to be measured, of which A is a *secondary* meridional position accurately determined, and B a *tertiary* meridional position to be determined.

If possible, two sets of observations should be taken at A to ascertain the errors and rates of the chronometers. The run is then made to B, and observations made to determine local time, and hence the difference of longitude; and on the same spot altitudes of the sun, or of a number of pairs of stars, or both, should be taken to determine the latitude.

Now, if chronometer rates could be relied on to be uniform, this measurement would suffice, but since variations may always arise, the run back to A should be made, or to another secondary meridional position, C, and new rates there obtained. Finally, the errors of the chronometers on the day when the observations were made at the tertiary position should be corrected for the loss or gain in rate, and for the difference of the errors as thus determined.

When opportunity does not permit obtaining a *rate* at the secondary meridional station or stations, both before and after the observations at B, the navigator may obtain the *errors* only, and assume that the rate has been uniform between those errors.

A modification of the foregoing method that may sometimes prove convenient is to make the first and third sets of observations at the position of the tertiary meridian, and the intermediate one at the secondary meridian; in this case the error will be obtained at the secondary station, and the rate at the tertiary.

EXAMPLE: A vessel at a station A, of known longitude, obtained chronometer errors as follows:

May 27, noon, chro. slow, $7^m\ 18^s.9$,
June 3, noon, chro. slow, $7\ \ 12\ .7$;

then proceeding to a station B a series of observations for longitude was taken on June 17; after which, returning to A, the following errors were obtained:

July 3, noon, chro. slow, $7^m\ 00^s.7$,
July 10, noon, chro. slow, $6\ \ 59\ .8$.

Required the correct error on June 17.

May 27,	$-7^m\ 18^s.9$	July 3,	$-7^m\ 00^s.7$
June 3,	$-7\ \ 12\ .7$	July 10,	$-6\ \ 59\ .8$
Change, +	6 .2	Change, +	0 .9
Daily rate, +	$0^s.89$	Daily rate, +	$0^s.13$

Therefore, assuming that these rates were correct at the middle of the periods for which they were determined, we have,

May 30, Midnight, Rate,	$+0^s.89$
July 6, Midnight, Rate,	$+0\ .13$
Change of rate, 37 days,	$-0\ .76$
Daily change of rate,	$-0^s.021$

Change of rate for $3\frac{1}{2}$ days, $-0^s.07$; rate June 3, noon, $+0^s.89-0^s.07=$	$+0^s.82$
Change of rate for $17\frac{1}{2}$ days, $-0^s.37$; rate June 17, noon, $+0\ .89-0\ .37=$	$+0\ .52$
Mean daily rate, June 3 to 17,	$+0\ .67$
Total change of error, June 3 to 17,	$+0^m\ 09^s.38$
Error, June 3,	$-7\ \ 12\ .7$
Error, June 17,	$-7\ \ 03\ .3$

346. SINGLE ALTITUDES.—The determination of longitudes ashore by single altitudes of a celestial body is identical in principle with the determination at sea by that method, which will be explained hereafter (art. 349). It may be remarked, however, that by taking observations on opposite sides of the meridian, at altitudes as nearly equal as possible, a means is afforded, which is not available at sea, of eliminating certain constant errors of observation.

347. EQUAL ALTITUDES.—The method of equal altitudes, explained in article 321, Chapter XI, is available for the determination of longitudes as well as for chronometer error. In the case of the sun, the sight gives the chronometer time of L. A. noon or midnight; applying the chronometer correction and equation of time (the latter with its sign for mean time), we obtain the G. A. T., which equals the longitude, if west, or 24^h *minus* the longitude, if east. For any other body, the sight gives the chronometer time of transit; apply the chronometer correction and there results G. M. T., which may be reduced to G. S. T.; the difference between the latter and the R. A. of the body (this being L. S. T.), is the longitude.

EXAMPLE: April 20 p. m. and April 21 a. m., 1879, in Lat. 30° 25′ N., Long. (approx.) 81° 26′ W., chro. corr. $-3^m\ 11^s.4$, observed times and equal altitudes of the sun as stated below; C—W for p. m. sights, $5^h\ 31^m\ 58^s.5$, and for a. m. sights, $5^h\ 32^m\ 01^s$. Required the longitude.

	WATCH, P. M.	ALTS.	WATCH, A. M.
	$2^h\ 51^m\ 40^s$	90° 0′	$8^h\ 59^m\ 00^s$
	52 05	89 50	58 34 .5
	52 30	40	58 09 .5
	52 55	30	57 46 .0
	53 20	20	57 20 .0
Mean, W. T., P. M.,	$2^h\ 52^m\ 30^s.0$	Mean, W. T., A. M.,	$8^h\ 58^m\ 10^s$
C − W,	+5 31 58 .5	C - W,	+ 5 32 01
P. M. Chro. T.,	8 24 28 .5	A. M. Chro. T. + 12^h,	26 30 11 .0
A. M. Chro., T. + 12^h,	26 30 11 .0	P. M. Chro. T.,	8 24 28 .5
	2)10 54 39 .5	Elapsed Time,	18 05 42 .5
Mid. Chro. T.,	5 27 19 .75		
Eq. eq. alt.,	+ 19 .35	Eq. t.,	$1^m\ 04^s.9$
Chro. t., L. A. Mid.,	5 27 39 .1	H. D.,	+ $0^s.54$
Eq. t.,	+ 1 14 .3	Long. + 12^h,	$17^h.43$
Chro. t., L. M. Mid.,	5 28 53 .4	Corr.,	+ $9^s.4$
C. C.,	− 3 11 .4	Eq. t.,	$1^m\ 14^s.3$
Long., W.,	$5^h\ 25^m\ 42^s.0$ / 81° 25′ 30″	(*Plus* to *mean* time.)	

Dec.,	11° 29′ 17″.1 N.	H. D. (20th),	+51″.45
		H. D. (21st),	+50 .97
H. D. at Mid., +	51″.10		
Long. + 12^h,	$17^h.43$	Diff. 24^h,	− 0 .48
Corr., +	890″.7 / 14′ 51″	Diff. 1^h,	− 0″.02
		Diff. $17^h.43$,	− 0″.35
Dec.,	11° 44′ 08″ N.		
		H. D. at Mid.,	+51″.10

Tab. 37	log A (+)9.9364		log B (−)9.7912
H. D. +51″.10 log	(+)1.7084		log (+)1.7084
Lat. 30° 25′ tan	(+)9.7687	d +11° 44′ tan	(+)9.3175
1st Part $+25^s.91$	log (+)1.4135		
2d Part − 6 .56			log (−)0.8171
Eq. eq. alt.,	+19 .35		

348. In the same example the equation of equal altitudes may be found by the less exact method heretofore given (art. 324), as follows:

Change in declination between sights = H. D. × Elapsed time = 51″.10 × 18^h.1 = 925″.
Change in altitude due to 100″ declination (Tab. 25) = + 53″.

$$h' = +\frac{53 \times 925}{100 \times 60} = +8'.19.$$

$$t' = +\frac{2^h 53^m 20^s - 2^h 51^m 40^s}{90^\circ 00' - 89^\circ 20'} = +\frac{100^s}{40'} = +2^s.5.$$

$$\text{Eq. eq. alt.} = +8.19 \times 2^s.5 = +20^s.5.$$

DETERMINATION AT SEA.

349. The Time Sight.—The method of determining longitude at sea which is employed almost to the exclusion of all others is that of the *time sight*, sometimes called the *chronometer method*. The altitude of the body above the sea horizon is measured with a sextant and the chronometer time noted; the hour angle of the body is then found by the process described in article 316, Chapter XI.

If the sun is observed, the hour angle is equal to the local apparent time; the Greenwich apparent time may be determined by applying the equation of time to the Greenwich mean time as shown by the chronometer; the longitude is then equal to the difference between the local and the Greenwich apparent times, being east when the local time is the later, and west when it is the earlier of the two.

If any other celestial body is employed, the hour angle from the local meridian, found from the sight, is compared with the hour angle from the Greenwich meridian to obtain the longitude; the Greenwich hour angle is found by converting the Greenwich mean time into Greenwich sidereal time in the usual manner, and then taking the difference between the latter and the right ascension of the body, the remainder being marked east or west, according as the Greenwich sidereal time is the lesser or greater of the two quantities; and as the local hour angle may be marked east or west according to the side of the meridian upon which it was observed, the name of the longitude will be indicated in combining the quantities.

350. As has been stated, the most favorable position of the celestial body for finding the hour angle from its altitude is when nearest the prime vertical, provided the altitude is not so small as to be seriously affected by refraction.

351. In determining the longitude at sea by this method, it is necessary to employ the latitude by account. This is seldom exactly correct, and a chance of error is therefore introduced in the resulting hour angle; the magnitude of such an error depends upon the position of the body relatively to the observer. The employment of the Sumner line, which is to be explained in a later chapter, insures the navigator against being misled from this cause, and its importance is to be estimated accordingly.

Example: At sea, May 18, 1879, a. m.; Lat. 41° 33′ N.; Long. 33° 30′ W., by D. R., the following altitudes of the sun's lower limb were observed, and times noted by a watch compared with the Greenwich chronometer. Chro. corr., + 4^m 59^s.2; I. C., − 30″; height of the eye, 23 feet; C − W, 2^h 17^m 06^s. Required the true longitude.

W. T.,		7^h 20^m 15^s
		20 47
		21 14
Mean,		7 20 45.3
C − W,	+	2 17 06
Chro. t.,		9 37 51.3
C. C.,	+	4 59.2
G. M. T., 17^d,		21 42 50.5
Eq. t.,	+	3 47.9
G. A. T.,		21 46 38.4

Obs. alt. ⊙,		29° 35′ 30″
		41 20
		46 10
Mean,		29 41 00
Corr.,	+	9 05
h,		29 50 05
S. D.,	+	15′ 51″
dip,	−	4′ 42″
p. & r.,	−	1 34
I. C.,	−	0 30
	−	6 46
Corr.,	+	9′ 05″

Dec.,		19° 32′ 01″.8 N.
H. D.,	+	33″.09
G. M. T.,	−	2^h.3
Corr.,	−	{76″.1 / 1′ 16″}
Dec.,		19° 30′ 46″ N.
p,		70° 29′ 14″

Eq. t.,		3^m 47^s.68
H. D.,	−	0^s.09
G. M. T.,	−	2^h.3
Corr.,	+	0^s.21
Eq. t.,		3^m 47^s.9
(*Plus* to *mean* time.)		

h	29° 50′ 05″		
L	41 33 00	sec	.12588
p	70 29 14	cosec	.02569
	2)141 52 19		
s	70 56 09	cos	9.51406
s − *h*	41 06 04	sin	9.81782
			2)19.48345
G. A. T.	21^h 46^m 38^s		
L. A. T.	19 32 07	sin ½ *t*	9.74172
Long.	{2^h 14^m 31^s / 33° 37′ 45″} W.		

EXAMPLE: At sea, April 16, 1879, p. m., in Lat. 11° 47′ S., Long. 0° 20′ E., by D. R., observed an altitude of the star Aldebaran, west of the meridian, 23° 13′ 20″; chronometer time, $6^h\ 56^m\ 32^s$; chronometer fast of G. M. T., $2^m\ 27^s$; I. C. −2′ 00″; height of eye, 26 feet. What was the longitude?

Chro. t.,	$6^h\ 56^m\ 32^s$	Obs.alt. ✱,	23° 13′ 20″	R. A. ✱,	$4^h\ 28^m\ 59^s.6$
C. C.,	− 2 27	Corr.,	− 9 16		
G. M. T.,	6 54 05	h,	23 04 04	Dec.,	16° 15′ 59″ N.
R. A. M. S.,	+1 37 01.9			p,	106° 15′ 59″
Red. (Tab. 9),	+ 1 08.0	I. C.,	− 2′ 00″		
		dip,	− 5 00		
G. S. T.,	8 32 14.9	ref.,	− 2 16		
R. A. ✱,	4 28 59.6				
		Corr.,	− 9 16		
H.A. from Gr.,	4 03 15 W.				

h	23° 04′ 04″		
L	11 47 00	sec	.00925
p	106 15 59	cosec	.01774
	2)141 07 03		
s	70 33 32	cos	9.52223
$s-h$	47 29 28	sin	9.86757
			2)19.41679
Gr. H. A.	$4^h\ 03^m\ 15^s$ W.		
H. A.	4 05 50 W.	sin $\frac{1}{2}t$	9.70839

Long. $\left.\begin{cases} 0^h\ 02^m\ 35^s \\ 0°\ 38'\ 45'' \end{cases}\right\}$ E.

EXAMPLE: At sea, April 17, 1879, a. m., in Lat. 25° 12′ S., Long. 31° 32′ W., by D. R., observed an altitude of the planet Jupiter, east of the meridian, 45° 40′; watch time, $5^h\ 48^m\ 02^s$; C −W, $2^h\ 05^m\ 42^s$; C. C., $+2^m\ 18^s$; I. C., +1′ 30″; height of eye, 18 feet. Required the longitude.

W. T.,	$5^h\ 48^m\ 02^s$	Obs. alt. ✱,	45° 40′ 00″	R. A. ($17^d\ 0^h$),	$22^h\ 27^m\ 19^s.0$	Dec. ($17^d\ 0^h$),	10° 36′ 28″.1 S.
C−W,	2 05 42	Corr.,	− 3 36	H. D.,	+ $1^s.8$	H. D.,	+ 10″.0
Chro. t.,	7 53 44	h,	45 36 24	G. M. T.,	− $4^h.1$	G. M. T.,	− $4^h.1$
C. C.,	+ 2 18	I. C.,	+ 1′ 30″	Corr.,	− $7^s.4$	Corr..	− 41″.
G. M. T., 16^d,	19 56 02	dip,	− 4′ 09″	R. A.,	$22^h\ 27^m\ 11^s.6$	Dec.,	10° 37′ 09″ S.
R. A. M. S., 0^h,	+ 1 37 01.9	ref.,	− 0 57			p,	79° 22′ 51″
Red. (Tab. 9),	+ 3 16.5		− 5 06				
G. S. T.,	21 36 20.4						
R. A. ✱,	22 27 11.6	Corr.,	− 3′ 36″				
H. A. from Gr.,	0 50 51 E.						

h	45° 36′ 24″		
L	25 12 00	sec	.04343
p	79 22 51	cosec	.00750
	2)150 11 15		
s	75 05 38	cos	9.41032
$s-h$	29 29 14	sin	9.69217
			2)19.15342
Gr. H. A.	$0^h\ 50^m 51^s$E.		
H. A.	2 57 21 E.	sin $\frac{1}{2}t$	9.57671

Long. $\left.\begin{cases} 2^h\ 06^m 30^s \\ 31°\ 37'\ 30'' \end{cases}\right\}$ W.

EXAMPLE: At sea, June 26, 1879, p. m., in Lat. 49° 50′ N., Long. 6° 16′ W., by account, observed an altitude of the moon's lower limb 21° 18′ 10″, the body bearing east; chronometer time, $2^h\ 26^m\ 58^s$; chronometer slow of G. M. T., 42^s; I. C., −1′ 45″; height of eye, 22 feet. Find the longitude.

Chro. t.,		$2^h\ 26^m\ 58^s$
C. C.,	+	42
G. M. T.,		2 27 40
R. A. M. S.,	+	6 16 57.5
Red. (Tab. 9),	+	0 24.3
G. S. T.,		8 45 01.8
R. A. ☾,		11 38 39.3
H. A. from Gr.,		2 53 37 E.

Obs. alt. ☾,		21° 18′ 10″
S. D.,	+	15′ 59″
Aug.,	+	6
	+	16 05
dip,	−	4′ 36″
I. C.,	−	1 45
	−	6 21
1st corr.,	+	9′ 44″
Approx. alt.,		21° 27′ 54″
p.&r. (Tab. 24),	+	52 06
h,		22 20 00

R. A.,		$11^h\ 37^m\ 41^s.96$
M. D.,	+	$2^s.07$
No. min.,		$27^m.7$
Corr.,	+	$57^s.34$
R. A.,		$11^h\ 38^m\ 39^s.3$
Hor. par.,		58′ 35″

Dec.,		2° 35′ 36″.4 S.
M. D.,	−	15″.1
No. min.,		$27^m.7$
Corr.,	−	419″.3 = 6′ 59″.3
Dec.,		2° 42′ 36″ S.
p,		92° 42′ 36″

h	22° 20′ 00″		
L	49 50 00	sec	.19043
p	92 42 36	cosec	.00049
	2)164 52 36		
s	82 26 18	cos	9.11923
s—*h*	60 06 18	sin	9.93799
			2)19.24814
Gr. H. A.	$2^h\ 53^m\ 37^s$ E.		
H. A.	3 19 04 E.	sin $\frac{1}{2}t$	9.62407
Long.	$\left\{\begin{matrix} 0^h\ 25^m\ 27^s \\ 6°\ 21'\ 45'' \end{matrix}\right\}$ W.		

352. EQUAL ALTITUDES.—The method of finding the longitude at sea by observation of *equal altitudes* of a heavenly body is one that may be conveniently employed when applicable, though the limits of applicability are narrow.

If, on board a vessel which is either stationary in position or moving at a uniform rate of speed in a true east or west direction, equal altitudes of the sun, a planet, or a star be observed before and after transit, and the times noted by chronometer or watch, the interval from meridian being not greater than ten minutes of time and the altitude not less than 75°, the mean of the times will be the time (by the chronometer or watch used) of the meridian passage of the body; from this may be found the Greenwich mean time of transit and thence the longitude.

If (the limits of time and altitude remaining as stated) observations be taken when the body bears not less than 80° from the meridian, the time of meridian passage may with accurracy be regarded as equal to the mean of the times of observation, no matter what course may have been steered by the vessel in the interval.

But if the azimuth of the body is less than 80° from the north or south point of the horizon the method is not available for vessels making a material amount of northing or southing; and if the hour angle is greater than 10^m or the altitude less than 75°, it can not be accurately employed by any vessel, no matter what course is steered. The navigator should not yield to the temptation offered by the simplicity of this method to follow it beyond the limits within which it may properly be considered to apply.

353. To deduce the longitude by this method take the mean of the watch times before and after transit, which will give the watch time of transit; correct this watch time in the usual manner for C—W and chronometer correction, from which is derived the Greenwich mean time of transit.

In the case of the sun, apply to the Greenwich mean time the equation of time, giving it its sign of application to mean time; the result is the Greenwich apparent time of transit, which is equal to the longitude if the latter is west, or to 24^h *minus* the longitude if east.

For other bodies, convert Greenwich mean time into Greenwich sidereal time by the usual method; the body being on the meridian, the local sidereal time is equal to the body's right ascension; the difference between Greenwich and local sidereal times is the longitude—east if the local time is greater, and west if it is less.

Example: April 2, 1879, in Lat. 3° 30′ N., Long. 86° 00′ E., by D. R., observed equal altitudes of ☉ before and after noon, using same sextant and same height of eye. Watch: a. m., $11^h 52^m 37^s$; p.m., $12^h 07^m 22^s$; C — W, $6^h 17^m 48^s$; C. C., + $2^m 32^s$. Vessel steering west between sights. Required the longitude at noon.

W. T., A. M.,	11^h 52^m 37^s		Eq. t.,		3^m $42^s.5$
W. T., P. M.,	12 07 22		H. D.,	—	$0^s.75$
	2)23 59 59		G. M. T.,	—	$5^h.7$
W. T., L. A., noon,	11 59 59.5		Corr.,	+	$4^s.3$
C—W,	+ 6 17 48		Eq. t.,		3^m $46^s.8$
Chro. t., L. A., noon,	6 17 47.5		(*Subtract* from *mean* time.)		
C. C.,	+ 2 32				
G. M. T., L. A., noon, 1^d,	18 20 19.5				
Eq. t.,	— 3 46.8				
G. A. T., L. A., noon,	18 16 33				
Longitude,	$\left\{ \begin{array}{l} 5^h\ 43^m\ 27^s \\ 85°\ 51'\ 45'' \end{array} \right\}$ E.				

Example: August 6, 1879, p. m., in Lat. 25° 55′ S., by obs., and Long. 36° 58′ W., by account, observed equal altitudes of the star Antares, the chronometer times before and after passage being $9^h 42^m 38^s$ and $10^h 00^m 26^s$, and the true azimuths S. 81° E. and S. 81° W., respectively; chro. fast of G. M. T., $1^m 27^s$. The ship was steaming on a course SSW. What was the longitude?

Chro. time before,	9^h 42^m 38^s
Chro. time after,	10 00 26
	2)19 43 04
Chro. time passage,	9 51 32
C. C.,	— 1 27
G. M. T. passage,	9 50 05
R. A. M. S.,	+ 8 58 36.3
Red. (Tab. 9),	+ 1 36.9
G. S. T. passage,	18 50 18.2
L. S. T. passage (R. A. ✱),	16 22 03.4
Longitude,	$\left\{ \begin{array}{l} 2^h\ 28^m\ 15^s \\ 37°\ 03'\ 45'' \end{array} \right\}$ W.

CHAPTER XIV.

AZIMUTH.

354. The *azimuth* of a body has been defined (art. 223, Chap. VII) as the arc of the horizon intercepted between the meridian and the vertical circle passing through the body; and the *amplitude* (art. 224) as the arc measured between the position of the body when its true altitude is zero and the east or west point of the horizon. The amplitude is measured from the east point at rising and the west point at setting, and, if added to or subtracted from 90°, will agree with the azimuth of the body when in the true horizon. The azimuth is usually measured from the north point of the horizon in north latitude, and from the south point in south latitude, through 180° to the east or west; thus, if a body bore N. by E., its azimuth would be named N. 11¼° E. in north, or S. 168¾° E. in south latitude.

The determination of the azimuth of a celestial body is an operation of frequent necessity. At sea, the comparison of the true bearing with a bearing by compass affords the only means of ascertaining the error of the compass due to variation and deviation; on shore, the azimuth is required in order to furnish a knowledge of the variation, and is further essential in all surveying operations, the true direction of the base line being thus obtained.

355. There are various methods of obtaining the true azimuth of a celestial body, which will be described as follows: (*a*) *Amplitudes*, (*b*) *Time Azimuths*, (*c*) *Altitude Azimuths*, (*d*) *Time and Altitude Azimuths*. A further method, by means of the Sumner line, will be explained later (Chap. XV). Still another operation pertains to this subject, namely: (*e*) The determination of the *True Bearing of a Terrestrial Object*.

AMPLITUDES.

356. The method of obtaining the compass error by amplitudes consists in observing the compass bearing of the sun or other celestial body when its center is in the true horizon, the true bearing, under such conditions, being obtained by a short calculation. Since the true horizon is not marked by any visible line (differing as it does from the visible horizon by reason of the effects of refraction, parallax, and dip), allowance may be made for the difference by an estimate of the eye, or else the observation may be made in the visible horizon and a correction applied.

357. When the center of the sun is at a distance above the horizon equal to its own diameter it is almost exactly in the true horizon; at such a time, note its bearing by compass, and also note (as in all observations for determining compass error) the ship's head by compass, and the angle and direction of the ship's heel.

Or, note the bearing at the instant at which the center of the body is in the visible horizon; in the case of the sun and moon, the correct bearing at that time may be most accurately ascertained by taking the mean of the bearings when the upper and the lower limbs of the disk are just appearing or disappearing.

358. *To find the true amplitude by computation* there are given the latitude, L, and declination, *d*. The quantities are connected by the formula,

$$\sin \text{Amp.} = \sec L \sin d,$$

from a solution of which the amplitude is obtained.

To find the true amplitude by inspection enter Table 39 with the declination at the top and the latitude in the side column; under the former and opposite the latter will be given the true amplitude. To obtain accurate results, interpolate for minutes of latitude and declination.

To reduce the observed amplitude when taken in the visible horizon to what it would have been if taken in the true horizon, enter Table 40 with the latitude and declination to the nearest degree and apply the correction there found to the observed amplitude; the result will be the corrected amplitude by compass, which, by comparison with the true amplitude, gives the compass error. When the body observed is the sun, a star, or a planet, apply the correction, at rising in north latitude or at setting in south latitude, to the *right*, and at setting in north latitude or at rising in south latitude, to the *left*. For the moon, apply half the correction in a contrary direction.

Example: At sea, in Lat. 11° 29′ N., the observed bearing of the sun, at the time of rising when its center was estimated to be one diameter above the visible horizon, was E. 31° N.; corrected declination 22° 32′ N. Required the compass error.

By computation.

L	11° 29′	sec	.00878
d	22 32	sin	9.58345
True amp.	E. 23° 01′ N.	sin	9.59223
Obsd. amp.	E. 31 00 N.		
Error,	7° 59′ E.		

By inspection (Table 39).

L, 11°.5 N.; *d*, 22 .5 N.	True amp.	E. 23°.0 N.
Obsd. amp.		E. 31 .0 N.
Error,		8°.0 E.

Example: At sea, in Lat. 25° 03′ S., the observed bearing of Venus when in the visible horizon at rising was E. 18° 30′ N., its declination being 21° 44′ N. Required the compass error.

By computation.

L	25° 03′	sec	.04290
d	21 44	sin	9.56854
True amp.	E. 24° 08′ N.	sin	9.61144
Comp. amp.	E. 18 48 N.		
Error,	5° 20′ W.		

By inspection (Table 39).

L,		25°. 0 S.	True amp.	E. 24°. 1 N.
d,		21 . 7 N.		
Obsd. amp.	E. 18°. 5 N.		Comp. amp.	E. 18 . 8 N.
Corr. (Tab. 40)		0. 3 left.		
Error,				5°. 3 W.

Example: At sea, in Lat. 40° 27′ N., the mean of the observed bearings of the upper and lower limbs of the moon when in contact with the visible horizon at setting was W. 17° S.; declination, 21° 12′ S. What was the error of the compass?

By computation.

L	40° 27′	sec	.11863
d	21 12	sin	9.55826
True amp.	W. 28° 22′ S.	sin	9.67689
Comp. amp.	W. 16 42 S.		
Error,	11° 40′ W.		

By inspection (Table 39).

L,		40°. 5 N.	True amp.	W. 28°.4 S.
d,		21 . 2 S.		
Obsd. amp.	W. 17°. 0 S.		Comp. amp.	W. 16 .7 S.
Corr. (Tab. 40)		0. 3 right.		
Error,				11°.7 W.

TIME AZIMUTHS.

359. In this method are given the hour angle at time of observation, t, the polar distance, p, and the latitude, L; to find the azimuth, Z.

Any celestial body bright enough to be observed with the azimuth circle may be employed for observation; the conditions are, however, most favorable for solution when the altitude is low.

360. Take a bearing of the object, bisecting it if it has an appreciable disk, and note the time with a watch of known error. Record, as usual, the ship's head by compass and the amount of heel. If preferred, a series of bearings may be taken with their corresponding times, and the means taken.

361. First prepare the data as follows:

(a) Find the Greenwich time corresponding to the local time of observation.

(b) Take out the declination of the body from the Nautical Almanac; if the method of computation is employed the polar distance and the co-latitude should be noted.

(c) Find the hour angle of the body by rules heretofore given.

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This having been done, the true azimuth may be determined either by *Time Azimuth Tables*, by the graphic method of an *Azimuth Diagram*, or by *Solution of the Astronomical Triangle*. Owing to the possibility of more expeditious working, either of the first-named two is to be considered preferable to the last, and the navigator is recommended to supply himself with a copy of a book of Azimuth Tables, or with an Azimuth Diagram; an explanation of the method of use accompanies each of these.

362. To solve the triangle:

Let $S = \frac{1}{2}$ sum of polar distance and co-Lat.
$D = \frac{1}{2}$ difference of polar distance and co-Lat.
$\frac{1}{2}t = \frac{1}{2}$ hour angle.
$Z =$ true azimuth.

$$\text{Then, } \tan X = \sin D \operatorname{cosec} S \cot \tfrac{1}{2} t;$$
$$\tan Y = \cos D \sec S \cot \tfrac{1}{2} t;$$
$$Z = X + Y, \text{ or } X \sim Y.$$

First Case.—If the half-sum of the polar distance and co-Lat. is *less* than 90°: take the sum of the angles X and Y if the polar distance is *greater* than the co-Lat.; take the difference if the polar distance is *less* than the co-Lat.

Second Case.—If the half-sum of the polar distance and co-Lat. is *greater* than 90°: always take the difference of X and Y, which subtract from 180°, and the result will be the true azimuth.

In either case, mark the true azimuth N. or S. according to the latitude, and E. or W. according to the hour angle. It may sometimes be convenient to use the supplement of the true azimuth, by subtracting it from 180° and reversing the prefix N. or S., in order to make it correspond to the compass azimuth when the latter is less than 90°.

The cotangent of half the hour angle may be found from Table 44 abreast the *whole* hour angle in the column headed "Hour P. M."

EXAMPLE: December 3, 1879, a. m., in Lat. 30° 25′ N., Long. 5^h 25^m 42^s W., the observed bearing of sun's center was N. 135° 30′ E., and the Greenwich mean time, December 3, 2^h 36^m 11^s. The corrected declination of the sun was 22° 07′ S.; the equation of time (additive to mean time), 10^m 03^s. Required the error of the compass.

G. M. T. (Dec. 3),	2^h 36^m 11^s	co-Lat.,	59° 35′	t	2^h 39^m 28^s	cot ½ t	.44051	cot ½ t	.44051
Long.,	− 5 25 42	p,	112 07	S	85° 51′	cosec	.00114	sec	1.14045
				D	26 16	sin	9.64596	cos	9.95267
L. M. T. (Dec. 2),	21 10 29	p+co-L,	171 42						
Eq. t.,	+ 10 03			X	50 44	tan	.08761		
		S,	85 51	Y	88 19			tan	1.53363
L. A. T.,	21 20 32								
		p−co-L,	52° 32′	X+Y	139 03				
t,	2^h 39^m 28^s								
		D,	26 16						

True azimuth, N. 139° 03′ E.
Comp. azimuth, N. 135 30 E.

Compass error, 3 33 E.

EXAMPLE: April 9, 1879, in Lat. 2° 16′ N., the observed bearing of the sun's center was N. 85° 15′ E: sun's hour angle, 3^h 44^m 16^s, and its declination, 7° 38′ N. Required the compass error.

co-Lat.,	87° 44′	t	3^h 44^m 16^s	cot ½ t	.27372	cot ½ t	.27372
p,	82 22	S	85° 03′	cosec	.00162	sec	1.06406
		D	2 41	sin	8.67039	cos	9.99952
p+co-L,	170 06						
		X	5 03	tan	8.94573		
S,	85 03	Y	87 22			tan	1.33730
co-L−p,	5° 22′	Y−X	82 19				
D,	2 41						

True azimuth, N. 82° 19′ E.
Comp. azimuth, N. 85 15 E.

Compass error, 2 56 W.

EXAMPLE: April 26, 1879, Lat. 16° 32′ S., observed bearing of Venus 56° 00′ W., its hour angle being 4^h 27^m 31^s, and its declination 23° 12′ N. What was the error of the compass?

co-Lat.,	73° 28′	t	4^h 27^m 31^s	cot ½ t	.18022	cot ½ t	.18022
p,	113 12	S	93° 20′	cosec	.00074	sec	1.23549
		D	19 52	sin	9.53126	cos	9.97335
p+co-L,	186 40						
		X	27 16	tan	9.71222		
S,	93 20	Y	87 40			tan	1.38906
p−co-L,	39° 44′	Y−X	60 24				
D,	19 52	Z	119° 36′				

True azimuth, S. 119° 36′ W.
Comp. azimuth, S. 124 00 W.

Compass error, 4 24 W.

ALTITUDE AZIMUTHS.

363. This method is employed when the altitude of the body is observed at the same time as the azimuth; in such a case the hour angle need not be known, though the time of observation should be recorded with sufficient accuracy for the correction of the declination of the sun, moon, or a planet.

There are given the altitude, h, the polar distance, p, and the latitude, L; to find the azimuth, Z.

364. Take a bearing of the body by compass, bisecting it if the disk is of appreciable diameter, and simultaneously measure the altitude; note the time approximately. Observe also the ship's heading (by compass) and the heel.

Or a series of azimuths, with corresponding altitudes, may be observed, and the mean employed.

365. Calculate the true altitude and declination from the observed altitude and the time. Then compute the true azimuth from the following formula:

$$\cos \tfrac{1}{2} Z = \sqrt{\cos s \cos (s-p) \sec L \sec h},$$

in which $s = \frac{1}{2}(h + L + p)$. The resulting azimuth is to be reckoned from the north in north latitude and from the south in south latitude.

It may occur that the term $(s-p)$ will have a negative value, but since the cosine of a negative angle less than 90° is positive, the result will not be affected thereby.

EXAMPLE: December 3, 1879, in Lat. 30° 25′ N., the observed bearing of the sun's center was N. 135° 30′ E., and its corrected altitude 24° 59′; the approximate G. M. T. was $2^h.6$, the declination at that time being 22° 07′ S. Required the compass error.

h	24° 59′	sec	.04267
L	30 25	sec	.06431
p	112 07		
	2)167 31		
s	83 45	cos	9.03690
$s-p$	−28 22	cos	9.94445
			2)19.08833
$\frac{1}{2}$Z	69 30	cos	9.54416
Z	139 00		

True azimuth,	N. 139° 00′ E.
Comp. azimuth,	N. 135 30 E.
Compass error,	3 30 E.

TIME AND ALTITUDE AZIMUTHS.

366. When, at the time of observing the compass bearing of a celestial body, the altitude is measured and the exact time noted, the true azimuth may be very expeditiously determined, a knowledge of the latitude being unnecessary.

In view of the simplicity of the computation this method strongly commends itself to observers not provided with an azimuth table or diagram.

367. The observation is identical with that of the altitude azimuth (art. 364), with the exception that the times of observation must be *exactly* instead of *approximately* noted.

368. Ascertain the declination of the body at time of sight, and correct the observed altitude; compute the hour angle. We then have:

$$\sin Z = \sin t \cos d \sec h,$$

from which the azimuth may be found.

This method has a defect in that there is nothing to indicate whether the resulting azimuth is measured from the north or the south point of the horizon; but as the approximate azimuth is always known, cases are rare when the solution will be in question.

EXAMPLE: December 3, 1879, in Lat. 30° 25′ N., Long. $5^h\ 25^m\ 42^s$ W., the observed bearing of the sun's center was N. 135° 30′ E.; its altitude at the time was 24° 59′; hour angle, $2^h\ 39^m\ 28^s$ (39° 52′), and declination 22° 07′ S. Find the compass error. (See example under Altitude Azimuths and first example under Time Azimuths.)

t	39° 52′	sin 9.80686	
d	22 07	cos 9.96681	
h	24 59	sec .04267	
Z S. 40° 56′ E.		sin 9.81634	

True azimuth,	N. 139° 04′ E.
Comp. azimuth,	N. 135 30 E.
	3 34 E.

TRUE BEARING OF A TERRESTRIAL OBJECT.

369. Thus far, sea observations for combined variation and deviation have been discussed, but if it becomes necessary, as in surveying, to ascertain the *True Bearing of a Terrestrial Object*, or to find the variation at a shore station, more accurate methods than the foregoing must be resorted to.

The most reliable method is that by an *Astronomical Bearing*. This consists in finding the true bearing of some well-defined object by taking the angle between it and the sun or other celestial body with a sextant or a theodolite, and simultaneously noting the time by chronometer, or measuring the altitude, or observing both time and altitude. It should always be noted whether the object is right or left of the sun.

370. *By Sextant.*—Measure the angular distance between the object and the sun's limb; and if there is a second observer, measure the altitude of the sun at the same moment and note the time. In the absence of an assistant, first measure the altitude of the sun; next, the angular distance between the sun and the object; then, a second altitude of the sun, noting the time of each observation. Also measure the altitude of the defined point above the sea or shore horizon.

By Theodolite.—This instrument is far more convenient than the sextant, for, being leveled, the horizontal angle between the sun and the object is at once given, no matter what may be the altitudes of the objects. In case the altitude of the sun is needed, it may be read accurately enough from the vertical circle, although not as finely graduated as the limb of the sextant. The error in altitude must, however, be found by the level attached to the telescope, since it will usually be found to differ from the levels of the horizontal circle. If, in directing the telescope to the sun, there is no colored eye-piece, an image of the sun may be cast on a piece of white paper held at a little distance from the eye-piece, and by adjusting the focus the shadow of the cross-wires will be seen.

It should be understood that any celestial body may be used as well as the sun, and there are, in fact, certain advantages in the use of the stars; the sun is chosen for illustration, because it will usually be found most convenient to employ that body.

371. Find the true azimuth of the celestial body by any one of the methods previously explained in this chapter and apply to it the azimuth difference, or horizontal angle between the celestial and the terrestrial body, having regard to the direction of one from the other.

To find the azimuth difference from sextant observations, change the observed altitudes of the bodies into *apparent* altitudes by correcting them for index error of the sextant, dip, and semidiameter; change the observed angular distance into *apparent* angular distance, by correcting for index error and semidiameter. Then if $S = \frac{1}{2}$ (App. Dist. + App. Alt. ☉ + App. Alt. Object), we have:

$$\cos \tfrac{1}{2} \text{ Az. Diff.} = \sqrt{\sec \text{App. Alt.} \odot \sec \text{App. Alt. Object} \cos S \cos (S - \text{App. Dist.})},$$

whence the azimuth difference is deduced.

When the theodolite is used, the horizontal angle is given directly. If only one limb of the sun is observed, it will be necessary to apply a correction for semidiameter (S. D. × sec h), but it is usual to eliminate this correction by taking the mean of observations of both limbs.

EXAMPLE: December 10, 1879, a. m., in Lat. 30° 25′ 24″ N., Long. 81° 25′ 24″ W., made observations with a sextant and obtained the following data for finding the true bearing of a station:

Watch time,	$11^h\ 22^m\ 36^s$	Obs. Ang. Dist. ⨀,	117° 07′ Left.	Dec. S.,	22° 56′ 27″
C − W,	5 21 18	Obs. 2☉,	71° 37′ 20″	Eq. t., +	$7^m\ 00^s$
Chro. corr., +	2 16	Obs. alt. Station,	20′	S. D.,	16′ 17″
		I. C.,	zero.		

Required the true bearing of the object.

W. T.,	$11^h\ 22^m\ 36^s$	2☉,	71° 37′ 20″	t	8° 08′ 00″	sin 9.15069
C − W,	5 21 18	☉,	35 48 40	d	22 56 27	cos 9.96422
Chro. t.,	4 43 54	S. D., +	16 17	h	36 03 37	sec .09239
C. C., +	2 16	App. Alt.,	36 04 57	Z {S.	9° 17′ E.	sin 9.20730
G. M. T., Dec. 10,	4 46 10	$p.$ & $r.$, −	1 13	Z {N.	170 43 E.	
Eq. t., +	7 00	h,	36 03 44			
G. A. T.,	4 53 10					
Long., −	5 25 42					
L. A. T.,	23 27 28					
t,	$0^h\ 32^m\ 32^s$ / 8° 08′ 00″					

Obs. Ang. Dist.,	117° 07′ 00″	App. Dist.	117° 23′		True bearing ☉,	N. 170° 43′ E.
☉'s S. D., +	16 17	App. Alt. ☉	36 05	sec 0.09250	Az. Diff.,	125 00 Left.
App. Ang. Dist.,	117 23 17	App. Alt. Object	20	sec 0.00001	True bearing object,	N. 45° 43′ E.
			2)153 48			
		S	76 54	cos 9.35536		
		S − App. Dist.	−40 29	cos 9.88115		
				2)19.32902		
		½ Az. Diff.	62° 30′	cos 9.66451		
		Az. Diff.	125 00			

EXAMPLE: Same date and place and same objects as in the preceding example; measurement made with a theodolite, angular distance ⦶, 123° 17′; object left of sun. Watch time, $11^h\ 16^m\ 34^s.5$; watch slow of L. A. T., $4^m\ 53^s.5$. Dec. ☉, 22° 56′ S. Required the true bearing.

W. T.,	$11^h\ 16^m\ 34^s.5$	co-Lat.,	59° 35′	t	$0^h\ 38^m\ 32^s$	cot ½ t 1.07435	cot ½ t 1.07435
W. slow, +	4 53.5	p,	112 56	S	86° 15′	cosec .00093	sec 1.18440
L. A. T.,	23 21 28.0	p + co-L,	172 31	D	26 41	sin 9.65230	cos 9.95110
t,	0 38 32	S,	86 15	X	79° 24′	tan .72758	
		p − co-L,	53 21	Y	89 39		tan 2.20985
		D,	26 41	X + Y	169 03		

Using formula in ¶ 362

True bearing ☉,	N. 169° 03′ E.
Az. Diff.,	123 17 Left.
True bearing object,	N. 45 46 E.

CHAPTER XV.

THE SUMNER LINE.

DESCRIPTION OF THE LINE.

372. The method of navigation involving the use of the Sumner line takes its name from Capt. Thomas H. Sumner, an American shipmaster, who discovered it and published it to the world. As a proof of its value, the incident which led to its discovery may be related:

"Having sailed from Charleston, S. C., 25th November, 1837, bound for Greenock, a series of heavy gales from the westward promised a quick passage; after passing the Azores the wind prevailed from the southward, with thick weather; after passing longitude 21° W. no observation was had until near the land, but soundings were had not far, as was supposed, from the bank. The weather was now more boisterous, and very thick, and the wind still southerly; arriving about midnight, 17th December, within 40 miles, by dead reckoning, of Tuskar light, the wind hauled SE. true, making the Irish coast a lee shore; the ship was then kept close to the wind and several tacks made to preserve her position as nearly as possible until daylight, when, nothing being in sight, she was kept on ENE. under short sail with heavy gales. At about 10 a. m. an altitude of the sun was observed, and the chronometer time noted; but, having run so far without observation, it was plain the latitude by dead reckoning was liable to error and could not be entirely relied upon."

The longitude by chronometer was determined, using this uncertain latitude, and it was found to be 15′ E. of the position by dead reckoning; a second latitude was then assumed 10′ north of that by dead reckoning, and toward the danger, giving a position 27 miles ENE. of the former position; a third latitude was assumed 10′ farther north, and still toward the danger, giving a third position ENE. of the second 27 miles. Upon plotting these three positions on the chart, they were seen to be in a straight line, and this line passed through Smalls light.

"It then at once appeared that the observed altitude must have happened at all the three points and at Smalls light and at the ship at the same instant."

Then followed the conclusion that, although the absolute position of the ship was uncertain, she must be somewhere on that line. The ship was kept on the course ENE., and in less than an hour Smalls light was made, bearing ENE. ½ E. and close aboard.

The latitude by dead reckoning was found to be 8′ in error, and if the position given by that latitude had been assumed correct the error would have been 8 miles too far S. and 31′ 30″ of longitude too far W., and the result to the ship might have been disastrous had this wrong position been adopted. This represents one of the practical applications of the Sumner line.

The properties of the line thus found will now be explained.

373. Circles of Equal Altitude.—In figure 43, if EE′E″ represent the earth projected upon the horizon of a point A, and if it be assumed that, at some particular instant of time, a celestial body is in the zenith of that point, then the true altitude of the body as observed at A will be 90°. In such a case the great circle EE′E″, which forms the horizon of A, will divide the earth into two hemispheres, and from any point on the surface of one of those hemispheres the body will be visible, while over the whole of the other hemisphere it will be invisible. The great circle EE′E″, from the fact of its marking the limit of illumination of the body, is termed the *circle of illumination*, and from any point on its circumference the true altitude of the center of the body will be zero. If, now, we consider any small circle of the sphere, BB′B″, CC′C″, DD′D″, whose plane is parallel to the plane of the circle of illumination and which lies within the hemisphere throughout which the body is visible, it will be apparent that the true altitude of the body at any point of one of these circles is equal to its true altitude at any other point of the same circle; thus, the altitude of the body at B is equal to its altitude at B′ or B″, and its altitude at D is the same as at D′ or D″.

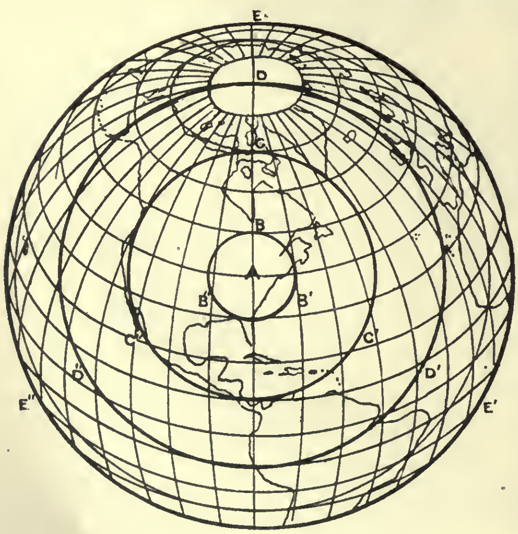

Fig. 43.

It therefore follows that at any instant of time there is a series of positions on the earth at which a celestial body appears at the same given altitude, and these positions lie in the circumference of a circle described upon the earth's surface whose center is at that position which has the body in the zenith, and whose radius depends upon the zenith distance, or—what is the same thing—upon the altitude. Such circles are termed *circles of equal altitude*.

374. The data for an astronomical sight comprise merely the time, declination, and altitude. The first two fix the position of the body and may be regarded as giving the latitude and longitude of that point on the earth in whose zenith the body is found; the zenith distance (the complement of the altitude) indicates the distance of the observer's zenith from that point; but there is nothing to show at which of the numerous positions fulfilling the required conditions the observation may have been taken. A number of navigators may measure the same altitude of a body at the same instant of time, at places thousands of miles apart; and each proceeds to work out his position with identical data, so far as this sight is concerned. It is therefore clear that a single observation is not enough, in itself, to locate the point occupied by the observer, and it becomes necessary, in order to fix the position, to employ a second circle, which may be either that of another celestial body or that of the same body given by an observation when it is in the zenith of some other point than when first taken; knowing that the point of observation lies upon each of two circles, it is only possible that it can be at one of their two points of intersection; and since the position of the ship is always known within fairly close limits, it is easy to choose the proper one of the two. Figure 44 shows the plotting of observations of two bodies vertically over the points A and A′ upon the earth, the zenith distances corresponding respectively to the radii AO and A′O.

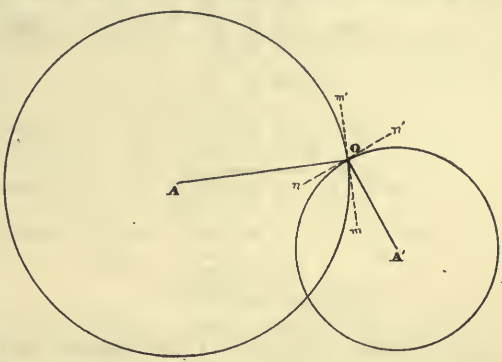

Fig. 44.

375. The Sumner Line.—In practice, under the conditions existing at sea, it is never necessary to determine the whole of a circle of equal altitude, as a very small portion of it will suffice for the purposes of navigation; the position is always known within a distance which will seldom exceed thirty miles under the most unfavorable conditions, and which is usually very much less; in the narrow limits thus required, the arc of the circle will practically coincide with the tangent at its middle point, and may be regarded as a straight line. Such a line, comprising so much of the circle of equal altitude as covers the probable limits of position of the observer, is called a *Sumner line* or *Line of position.*

376. Since the direction of a circle at any point—that is, the direction of the tangent—must be perpendicular to the radius at that point, it follows that the Sumner line always lies in a direction at right angles to that in which the body bears from the observer. Thus, in figure 44, it may be seen that $m\,m'$ and $n\,n'$, the extended Sumner lines corresponding to the bodies at A and A′, are respectively perpendicular to the bearings of the bodies OA and OA′. This fact has a most important application in the employment of the Sumner line.

377. Uses of the Sumner Line.—The Sumner line is valuable because it gives to the navigator a knowledge of all of the probable positions of his vessel, while a sight worked with a single assumed latitude or longitude gives but one of the probable positions; it must be recognized that, in the nature of things, an error in the assumed coordinate will almost invariably exist, and its possible effect should be taken into consideration; the line of position reveals the difference of longitude due to an error in the latitude, or the reverse.

Since the Sumner line is at right angles to the bearing, it may be seen that when the body bears east or west—that is, when it is on the prime vertical—the resulting line runs north and south, coinciding with a meridian; if, in this case, two latitudes are assumed, the deduced longitudes will be the same. When the body bears north or south, or is on the meridian, the line runs east and west and becomes identical with a parallel of latitude; in such a case, two assumed longitudes will give the same latitude. Any intermediate bearing gives a Sumner line inclined to both meridians and parallels; if the line agrees in direction more nearly with the meridian, latitude should generally be assumed and the longitude worked; if it is nearer a parallel, the reverse course is usually preferable. The values of the assumed coordinates may vary from 10′ to 1°, according to circumstances.

378. The greatest benefit to be derived from the Sumner method is when two lines are worked and their intersections found. The two lines may be given by different bodies, which is generally preferable, or two different lines may be obtained from the same body from observations taken at different times. The position given by the intersection of two lines is more accurate the more nearly the lines are at right angles to each other, as an error in one line thus produces less effect upon the result. When two observations of the same body are taken, the position of the ship at the time of first sight must be brought forward to that at the second in considering the intersection; if, for example, a certain line is determined, and the ship then runs NW. 27 miles, it is evident that her new position is on a line parallel with the first and 27 miles to the NW. of it; a second line being obtained, the intersection of this with the first line, as corrected for the run, gives the ship's position.

Besides the employment of two lines for intersections with each other, a single line may be made to serve various useful purposes for the navigator. These are described in article 400, Chapter XVI.

METHODS OF DETERMINATION.

379. Any line may be defined in either of two ways—by two of its points, or by one point and the direction. There are thus two methods by which a Sumner line may be determined:

(*a*) Assume two values of one coordinate and find the corresponding values of the other. Two values of the latitude may be assumed and the longitudes determined, as was done by Captain Sumner on the occasion that led to the discovery of the method; or else two values of the longitude may be assumed and the latitudes determined. Two points are fixed in this way, and the line joining them is the line of position.

(*b*) Assume either one latitude or one longitude and determine the corresponding coordinate. This gives one point of the line. The azimuth of the body is then ascertained, and a line is drawn through

the determined point at right angles to the direction in which the body bore at the time of sight. This will be the line of position.

380. It follows that if the Sumner line be located by the first method and its direction thus defined, the azimuth of the observed body may be determined by finding the angle made by the line with the meridian and adding or substracting 90°.

EXAMPLE: At sea April 17, 1879, A. M., in Lat. 25° 12′ S., Long. 31° 32′ W., by D. R., observed an altitude of the planet Jupiter, east of the meridian, 45° 40′; watch time, $5^h\ 48^m\ 02^s$; C — W, $2^h\ 05^m\ 42^s$; C. C., + $2^m\ 18^s$; I. C., + 1′ 30″; height of eye, 18 feet. Required the Sumner line.

From a solution of this same problem for a single longitude (art. 351, Chap. XIII), the following were found: H. A. from Gr., $0^h\ 50^m\ 51^s$ E.; h, 45° 36′ 24″; p, 79° 22′ 51″. Assume values of Lat. 25° 02′ and 25° 22′ S.

h	45° 36′ 24″						
L_1	25 02 00	sec	.04284	L_2	25° 22′ 00″	sec	.04403
p	79 22 51	cosec	.00750			cosec	.00750
	2)150 01 15						
s_1	75 00 38	cos	9.41270	s_2	75 10 38	cos	9.40794
$s_1 - h$	29 24 14	sin	9.69105	$s_2 - h$	29 34 14	sin	9.69328
Gr. H. A.	$0^h\ 50^m\ 51^s$ E.		2)19.15409	Gr. H. A.	$0^h\ 50^m\ 51^s$		2)19.15275
H. A.$_1$	2 57 29 E.	sin $\frac{1}{2} t_1$	9.57704	H. A.$_2$	2 57 12	sin $\frac{1}{2} t_2$	9.57638
Long.$_1$	$\left\{ \begin{matrix} 2^h\ 06^m\ 38^s \\ 31^\circ\ 39'\ 30'' \end{matrix} \right\}$ W.			Long.$_2$	$\left\{ \begin{matrix} 2^h\ 06^m\ 21^s \\ 31^\circ\ 35'\ 15'' \end{matrix} \right\}$ W.		

It should be observed that s_2 and $s_2 - h$ can be obtained, respectively, from s_1 and $s_1 - h$ by adding half the difference between L_1 and L_2; also that log cosec p is the same for both hour angles. The determination of the second hour angle is thus considerably simplified.

A comparison of these results with those obtained by the solution with a single latitude shows that the hour angle, and consequently the longitude, corresponding to the latitude 25° 12′ S. are the means of those corresponding to the latitudes here used; and therefore that the assumption that the Sumner line is a straight line is accurate.

The line of the same sight might also have been found as follows:

Working with the single latitude 25° 12′ S., it was found that the corresponding longitude was 31° 37′ 30″ W. Now by referring to an azimuth table or azimuth diagram, the azimuth corresponding to Lat., 25°.2 S., Dec., 10°.6 S., H. A., $2^h\ 57^m$. 3 E. is S. 100° 58′ E.; therefore the Sumner line extends S. 10° 58′ E.

The line may therefore be defined in either of two ways, thus:

$$A_1\left\{\begin{matrix} 25^\circ\ 02'\ 00''\ \text{S.} \\ 31\ \ 39\ \ 30\ \ \text{W.} \end{matrix}\right. \qquad A_2\left\{\begin{matrix} 25^\circ\ 22'\ 00''\ \text{S.} \\ 31\ \ 35\ \ 15\ \ \text{W.} \end{matrix}\right.$$

Or, $$A\left\{\begin{matrix} 25^\circ\ 12'\ 00''\ \text{S.} \\ 31\ \ 37\ \ 30\ \ \text{W.} \end{matrix}\right. \qquad \text{Line runs S. } 10^\circ\ 58'\ \text{E.}$$

By inspection of the coordinates of A_1 and A_2 it may be seen that—

+ 20′ diff. lat. makes — 4′.25 diff. long.; or,
+ 20 miles diff. lat. makes — 3.8 miles departure.

Therefore by reference to Table 2 it appears that the line runs about S. 11° E., and the azimuth of the body is S. 101° E.; thus the results obtained by the two methods agree.

EXAMPLE: At sea, May 18, 1879, A. M., Lat. 41° 33′ N., Long. 33° 30′ W., by D. R., the mean of a series of observed altitudes of the sun's lower limb was 29° 35′ 30″; the mean watch time, $7^h\ 20^m\ 45^s.3$; C. C., + $4^m\ 59^s.2$; I. C., — 30″; height of the eye, 23 feet; C — W, $2^h\ 17^m\ 06^s$. Required the Sumner line.

From a solution of this same problem for a single longitude (art. 351, Chap. XIII) the following were found: G. A. T., $21^h\ 46^m\ 38^s$; h, 29° 50′ 05″; p, 70° 29′ 14″. Assume values of the latitude 41° 03′ and 42° 03′ N.

h	29° 50′ 05″						
L_1	41 03 00	sec	.12255	L_2	42° 03′ 00″	sec	.12927
p	70 29 14	cosec	.02569			cosec	.02569
	2)141 22 19						
s_1	70 41 09	cos	9.51950	s_2	71 11 09	cos	9.50852
$s_1 - h$	40 51 04	sin	9.81564	$s_2 - h$	41 21 04	sin	9.81999
G. A. T.	$21^h\ 46^m\ 38^s$		2)19.48338	G. A. T.	$21^h\ 46^m\ 38^s$		2)19.48347
L. A. T.$_1$	19 32 08	sin $\frac{1}{2} t_1$	9.74169	L. A. T.$_2$	19 32 06	sin $\frac{1}{2} t_2$	9.74174
Long.$_1$	$\left\{ \begin{matrix} 2^h\ 14^m\ 30^s \\ 33^\circ\ 37'\ 30'' \end{matrix} \right\}$ W.			Long.$_2$	$\left\{ \begin{matrix} 2^h\ 14^m\ 32^s \\ 33^\circ\ 38'\ 00'' \end{matrix} \right\}$ W.		

$$A_1\left\{\begin{matrix} 41^\circ\ 03'\ 00''\ \text{N.} \\ 33\ \ 37\ \ 30\ \ \text{W.} \end{matrix}\right. \qquad A_2\left\{\begin{matrix} 42^\circ\ 03'\ 00''\ \text{N.} \\ 33\ \ 38\ \ 00\ \ \text{W.} \end{matrix}\right.$$

+ 60′ diff. lat. makes + 0′.5 long.
+ 60 miles diff. lat. makes + 0.4 mile departure.

Line runs, N. ½° W. Azimuth, N. 89½° E.

The same sight worked with a single latitude, 41° 33′ N., as was done in the original example, with azimuth taken from tables or diagram, gives:

A	41° 33′ 00″ N.	Azimuth, N. 89° 38′ E.
	33 37 45 W.	Line runs, N. 0° 22′ W.

This example illustrates the case in which an observation is taken practically on the prime vertical; the azimuth shows the bearing to be within 0° 22′ of true East, and the Sumner line is therefore within 0° 22′ of the meridian; a variation of 30′ in either direction from the dead reckoning latitude makes a difference of only 15″ in the longitude.

EXAMPLE: May 28, 1879, in Lat. 6° 20′ S. by account, Long. 30° 21′ 30″ W.; chro. time, $7^h\ 35^m\ 10^s$; observed altitude of moon's upper limb, 75° 33′ 00″, bearing north and east; I. C., — 3′ 00″; height of eye, 26 feet; chro. fast of G. M. T., $1^m\ 37^s.5$. Required the Sumner line.

From a solution of the same problem with a single longitude (art. 339, Chap. XII), the following values were obtained: H. A. from Greenwich, $1^h\ 35^m\ 07^s$ W.; h, 75° 23′ 30″; d, 6° 41′ 47″ N. Assume the longitudes 30° 10′ and 30° 30′ W.

Gr. H. A.	$1^h\ 35^m\ 07^s$ W.	Gr. H. A.	$1^h\ 35^m\ 07^s$
$Long._1$	2 00 40 W.	$Long._2$	2 02 00
t_1	$0^h\ 25^m\ 33^s$ / 6° 23′ 15″	t_2	$0^h\ 26^m\ 53^s$ / 6° 43′ 15″

t_1	6° 23′ 15″	sec .00270		
d	6 41 47	tan 9.06973	cosec .93324	
h	75 23 30		sin 9.98573	A_1 6° 27′ 03″ S. / 30 10 00 W.
φ''_1	6 44 17 N.	tan 9.07243	sin 9.06942	
φ'_1	13 11 20 S.		cos 9.98839	
$Lat._1$	6 27 03 S.			
t_2	6° 43′ 15″	sec .00299		
d	6 41 47	tan 9.06973	cosec .93324	
h	75 23 30		sin 9.98573	A_2 6° 16′ 27″ S. / 30 30 00 W.
φ''_2	6 44 33	tan 9.07272	sin 9.06972	
φ'_2	13 01 00		cos. 9.98869	
$Lat._2$	6 16 27 S.			

Working by the other method, and finding the azimuth, we have:

A	6° 21′ 14″ S.	Line runs N. 62° W.
	30 21 30 W.	

It might be shown that the results check with each other, as in previous cases.

EXAMPLE: At sea, July 12, 1879, in Lat. 50° N., Long. 40° W., observed circum-meridian altitude of the sun's lower limb, the time by a chronometer regulated to Greenwich mean time being $2^h\ 41^m\ 39^s$; chro. corr., — $2^m\ 30^s$; I. C., —3′ 0″; height of the eye, 15 feet. Find the Sumner line.

From the solution of the same problem for a single latitude (art. 338, Chap. XII) the following values were obtained: G. A. T., $2^h\ 33^m\ 50^s$; h, 61° 57′ 01″; d, 21° 59′ 27″ N.; a (Tab. 26), 2″ .5. Assume longitudes 39° 45′ and 40° 15′ W.

Gr. H. A.	$2^h\ 33^m\ 50^s$	Gr. H. A.	$2^h\ 33^m\ 50^s$
$Long._1$	—2 39 00	$Long._2$	—2 41 00
t_1	5 10	t_2	7 10
h	61° 57′ 01″	h	61° 57′ 01″
at_1^2	+ 1 06	at_2^2	+ 2 08
H_1	61 58 07	H_2	61 59 09
z_1	28 01 53 N.	z_2	28 00 51
d	21 59 27 N.	d	21 59 27
L_1	50 01 20 N.	L_2	50 00 18 N.

The line given by these coordinates is then:

A_1	50° 01′ 20″ N.	A_2	50° 00′ 18″ N.
	39 45 00 W.		40 15 00 W.

This shows that the Sumner line lies so nearly in a due east-and-west direction that a difference of longitude of 30′ makes a difference of latitude of only 1′.

From an azimuth table or diagram, it is found that the azimuth of the sun corresponding to Lat. 50° N. Dec. 22° N. and H. A. 6^m 10^s E., is N. 177° E. Therefore, using the values given by the earlier solution, the line is defined as follows:

$$A\begin{cases}50°\ 00'\ 51''\ N.\\40\ \ 00\ \ 00\ \ N.\end{cases}\qquad \text{Line runs N. 87° E.}$$

The direction of the line thus given and the one found from the double coordinates may be shown to agree as in examples before given.

FINDING THE INTERSECTION OF SUMNER LINES.

381. The intersection of Sumner lines may be found either graphically or by computation.

382. Graphic Methods.—Each line may be plotted upon the chart of the locality in which the ship is being navigated and the intersection thus found. The details of the plotting will be obvious, whether the line is defined by two of its points, or by one point and its direction. This plan will commend itself especially when the vessel is near shore, as the chart in use will then probably be one of conveniently large scale, and it will be an advantage to see where the position falls with reference to soundings and landmarks.

383. When clear of the land it is often inconvenient to follow this plan; a large scale chart may not be at hand, it may not be desired to deface the chart with numerous lines, or the necessary space for chart work may not be available. In such a case, the following method [a] is recommended, as it obviates the disadvantages of the other.

To understand the principle of this method, suppose that the lines are defined by the latitude and longitude of two points of each, and consider that they are plotted on a chart which is constructed upon a sheet of elastic rubber. It is evident that if, while holding it fast in the direction of the meridians, we stretch this rubber along the lines of the parallels in a uniform manner until the length of each minute of longitude is made to equal a minute of latitude, the chart, while losing its accuracy as portraying actual conditions on the earth's surface, still correctly represents the positions of the various points in terms of the new coordinates which have been created, namely, those in which a minute of latitude is equal to a minute of longitude. Thus, if on the true chart a point is m minutes north and n minutes east of another, on the stretched one it will still be m minutes north and n minutes east, the only difference being that the minutes of longitude will now be of a different length; and if on the original chart the two Sumner lines intersect at a point m minutes north and n minutes east (on the original scale) of some definite point of one of the lines, the intersection on the stretched chart will lie m minutes north and n minutes (of the new scale) to the east of the same point.

A stricter mathematical conception of the stretched chart and its properties may perhaps be obtained by considering the chart of the locality to be projected (with the eye at the zenith) upon a plane which passes through one of the meridians and makes an angle with the plane of the horizon which is equal to the latitude; each minute of longitude will then be increased by multiplying it by the secant of the latitude, and thus becomes equal to a minute of latitude.

From a consideration of the properties of this hypothetical chart it may be seen that the following rule may be laid down: If two or more Sumner lines be plotted by their latitude and longitude upon any sheet of paper, using a scale whereon latitude and longitude are equal regardless of the latitude of the locality, the intersection of those lines, measured by coordinates on the scale employed, correctly represents the intersection of the lines as it would be measured upon a true chart.

It follows from this that we may plot Sumner lines upon any piece of paper, measuring the coordinates with an ordinary scale ruler, and assigning any convenient length for the mile; the larger the scale the more accurate will be the determination. Or, what is even more convenient, we may employ "profile paper," whereon lines are ruled at right angles to each other and at equal distances apart, in which case no scale ruler is needed.

One caution must be observed in using this method; all longitudes employed on the paper for any purpose must be those of the scale, namely, one minute of longitude equals one minute of latitude. For instance, if the two Sumner lines be taken at different times, in bringing the first up to the position of the second by the intermediate run, that run must be laid down to scale; that is, the easting or westing must appear as so many minutes of longitude, not so many miles. To do this enter the traverse table with course and distance run, and pick out latitude and departure; then, by means of the middle latitude, convert departure into minutes of longitude and bring the first line to the second by laying off so many minutes of latitude north or south, and so many of longitude east or west.

In the case where the Sumner is defined by one position and its line of direction, it is not correct to lay down the angle to the meridian on the hypothetical chart, for all angles are distorted thereon. The best way is to find another position on the line by assuming a second latitude ten or twenty miles removed from that of the point given, entering the traverse table with the angle that the line makes with the meridian as a course, and abreast the latitude taking out the departure; convert departure into difference of longitude, and plot the second point by its coordinates from the first.

Example: Let it be required to find the intersection, by each of the methods, of the following lines:

$$A_1\begin{cases}40°\ 00'\ N.\\63\ \ 15\ \ W.\end{cases}\qquad A_2\begin{cases}40°\ 20'\ N.\\63\ \ 07\ \ W.\end{cases}$$

$$B_1\begin{cases}40\ \ 05\ \ N.\\63\ \ 03\ \ W.\end{cases}\qquad B_2\begin{cases}40\ \ 15\ \ N.\\63\ \ 12\ \ W.\end{cases}$$

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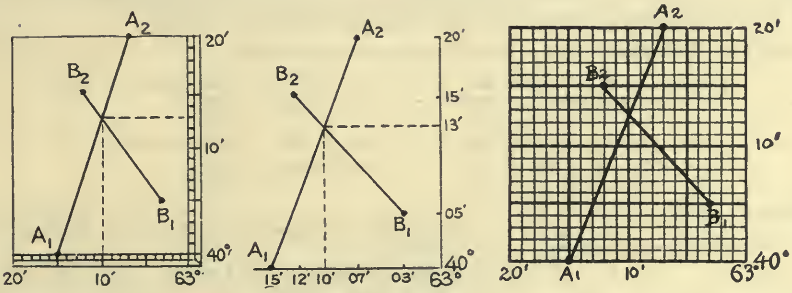
[a] Suggested by Lieut. G. W. Logan, U. S. Navy.

Figure 45 shows the intersection, (1) by Mercator chart, (2) by scale, and (3) on profile paper, as follows:



1 mile = .06 inch

FIG. 45.

Intersection: $\begin{cases} 40° \; 12'.8 \text{ N.} \\ 63 \;\; 09 .9 \text{ W.} \end{cases}$

Suppose, in the example just given, the first line had been defined as follows:

A $\begin{cases} 40° \; 00' \text{ N.} \\ 63 \;\; 15 \;\; \text{W.} \end{cases}$ Line runs N. 17° E.

To find a second coordinate by which to plot it, proceed as follows:

In Table 2, for 17°: Lat. 20′ N., Dep. 6.1 m. E. For Mid. Lat.: 40°, Dep. 6.1 m., diff. long. 8′.0 E. Hence, as previously given:

$A_1 \begin{cases} 40° \; 00' \text{ N.} \\ 63 \;\; 15 \;\; \text{W.} \end{cases}$ $\qquad A_2 \begin{cases} 40° \; 20' \text{ N.} \\ 63 \;\; 07 \;\; \text{W.} \end{cases}$

384. METHODS BY COMPUTATION.[a]—The finding of the intersection of two Sumner lines by computation may be divided into two cases:

Case I. When one line lies in a NE.–SW. direction, and the other in a NW.–SE. direction.

Case II. When both lie in a NE.–SW., or both in a NW.–SE. direction.

Suppose, first, that the lines are defined by the latitude and longitude of two points of each, and for the simplification of the problem consider the lines projected on a plane passing through one of the meridians and making an angle with the plane of the horizon equal to the latitude, the properties of which were explained under the graphic method, (art. 383); this saves the necessity of converting minutes of longitude into miles of departure before the solution and converting them back again afterwards; as all points are thus projected in corresponding relative positions, the results are as exact as if the longer method be followed of dealing with minutes of latitude and longitude of unequal length.

385. *Case I. One line NE.–SW., and the other NW.–SE.*—Suppose the two lines, projected as described, are as shown in figure 46, A_1 A_2 and B_1 B_2; for the present assume that the two points, A_1 and B_1, have a common latitude. Drop the perpendicular PO from the intersection; then the latitude of the intersection will be a distance OP above the common latitude of A_1 and B_1, and its longitude will be a distance A_1O to the right of A_1 and B_1O to the left of B_1.

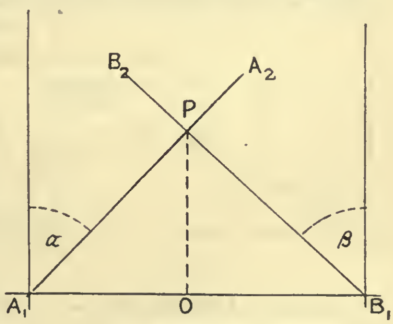


FIG. 46.

Find the angles α and β from the traverse table (Table 2), they being taken out with the difference of latitude between the two points of the same line in the column Lat. and the difference of longitude in the column Dep. (Do not overlook the fact that we are dealing now with the plane of projection and that α and β are not the angles made by the Sumner line with meridians on the earth's surface.) The solution may now be accomplished by either of two methods:

(a) Observe that the case is the same as if a ship were steaming along the line A_1 B_1 and took the first bearing of the point P when at A_1, at an angle from the course equal to $90°-\alpha$, and the second bearing when at B_1, at an angle from the course equal to $90°+\beta$, with an intervening run equal to the difference of longitude A_1 B_1; or, she may be considered as steaming from B_1 to A_1, in which case the first angle is $90°-\beta$ and the second $90°+\alpha$. Picking out of Table 5 B, corresponding to the angles given, the quantity in the *second* column, we shall have the ratio of the distance of *passing abeam*, OP, to the distance A_1 B_1; multiply the difference of longitude by this ratio, and we shall have the actual length of OP. Then entering the traverse table with this as a latitude and α as a course, we find in the departure column the distance A_1O by which the longitude of OP is defined; it is recommended also to pick out B_1O, using the angle β, which affords a proof of the correctness of all work done after the finding of α and β.

[a] Suggested by Lieut. G. W. Logan, U. S. Navy.

(b) The second method is to find by trial and error some latitude such that its departure corresponding to α, *plus* its departure corresponding to β, equals the difference of longitude A_1 B_1; then the point will be defined by the latitude, and by its longitude from A_1 and B_1, the agreement of the longitude as established from the different points furnishing a check upon the operation.

EXAMPLE: Find the intersection of the following Sumner lines:

A_1	49° 40′ N.	A_2	50° 00′ N.	+20′ lat.	Line runs NW.–SE.
	6 55.3 W.		7 20.0 W.	+24.7 long.	α=51°.
B_1	49 40 N.	B_2	50 00 N.	+20 lat.	Line runs NE.–SW.
	6 32.5 W.		6 11.3 W.	−21.2 long.	β=47°.

Longitude A_1 B_1=22′.8.

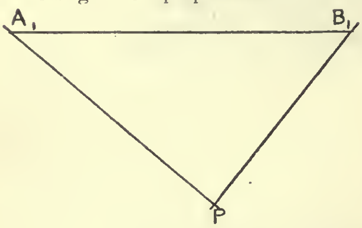


FIG. 47.

First draw a rough sketch (fig. 47) to illustrate the direction of coordinates.

Notice that A_1 is west of B_1. The line through A_1 runs NW.–SE. That through B_1, NE.–SW. The intersection is therefore south of both, east of A_1, and west of B_1.

(a) To solve by Table 5 B: First bearing $(90°-\alpha)=39°$; second bearing $(90°+\beta)=137°$. Corresponding ratio, 0.43, multiplied by $22'.8=9'.8$ lat. (The angles $90°-\beta$ and $90°+\alpha$ would have given the same ratio, 0.43.) Then (Table 2) with $\alpha=51°$, lat. $=9'.8$, dep. $=12'.1$; and with $\beta=47°$, lat. $=9'.8$, dep. $=10'.5$.

Hence, intersection:

9′.8 S. of lat. 49° 40′ N. = 49° 30′.2 N.
12 .1 E. of long. 6 55.3 W. = 6° 43 .2 W.
10 .5 W. of long. 6 32.5 W. = 6° 43 .0 W. } check.

(b) To solve by Table 2:

Assuming lat	5′	8′	10′	9′.9
Dep. for 51°	6.2	9.7	12.3	12.2
Dep. for 47°	5.3	8.5	10.7	10.6
Sum	11.5	18.2	23.0	22.8

Hence, intersection:

9′.9 S. of 49° 40′ = 49° 30′.1.
12 .2 E. of 6 55.3 = 6 43 .1
10 .6 W. of 6 32.5 = 6 43 .1 } check.

It may be seen that the results by the two methods substantially agree.

386. *Case II. Both lines NE.-SW., or both NW.-SE.*—Consider the lines as drawn in figure 48, and continue the assumption that A_1 and B_1 have a common latitude. The differences from the first case by both methods simply involve a change of signs.

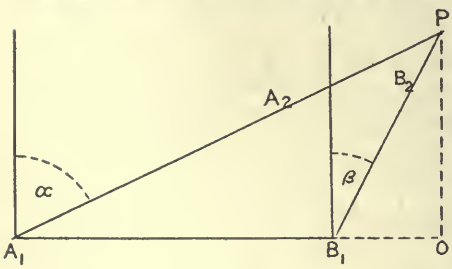


FIG. 48.

(a) If the ship is steaming from A_1 toward B_1, the first angle from the keel line is $90°-\alpha$, and the second, $90°-\beta$; if steaming from B_1 toward A_1, the first angle is $90°+\beta$, and the second $90°+\alpha$; in other words, either add both angles to 90° or subtract both from 90° and enter with the smaller angle as the first bearing.

(b) It may be seen that $OA_1-OB_1=A_1\,B_1$; in other words, to solve by the second method, the values must be so found that the *difference* of the corresponding departures equals the difference of longitude, instead of their sums, as before.

EXAMPLE: Find the intersection of the Sumner lines defined below:

A_1	49° 30′ N.	A_2	49° 50′	+20′ lat.	Line runs NE.-SW.
	5 24.8 W.		5 21.5	−3.3 long.	α=9°.
B_1	49 30 N.	B_2	49 50	+20 lat.	Line runs NE.-SW.
	5 25.8 W.		4 52.1	−33.7 long.	β=59°.

A_1 B_1=1′.0.

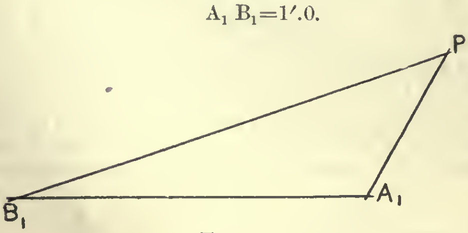


FIG. 49.

In this case (fig. 49) B_1 is west of A_1, the lines both run NE.–SW., and β is the greater angle; therefore intersection lies to the north and east of both points.

(a) By Table 5 B: First course $(90°+\alpha)=99°$; second course $(90°+\beta)=149°$; ratio $0.67\times1'.0=0'.7$; or, first course $(90°-\beta)=31°$; second course $(90°-\alpha)=81°$; ratio = 0.67, as before.

$\alpha=9°$, lat. $=0'.7$, dep. $=0'.1$; and $\beta=59°$, lat. $=0'.7$, dep. $=1'.2$.

Hence, intersection:

$$
\begin{array}{l}
0'.7 \text{ N. of } 49^\circ\ 30' \quad \text{N.} = 49^\circ\ 30'.7 \text{ N.} \\
\left.\begin{array}{l}
0\ .1 \text{ E. of } \ 5 \ \ 24\ .8 \text{ W.} = \ 5 \ \ 24\ .7 \text{ W.} \\
1\ .2 \text{ E. of } \ 5 \ \ 25\ .8 \text{ W.} = \ 5 \ \ 24\ .6 \text{ W.}
\end{array}\right\} \text{check.}
\end{array}
$$

(*b*) By Table 2:

Assuming lat	2′.0	0′.5	0′.6
Dep. for 9°	0 .3	0 .1	0 .1
Dep. for 59°	3 .3	0 .9	1 .1
Difference	3 .0	0 .8	1 .0

Hence, intersection:

$$
\begin{array}{l}
0'.6 \text{ N. of } 49^\circ\ 30' = 49^\circ\ 30'.6 \\
\left.\begin{array}{l}
0\ .1 \text{ E. of } \ 5 \ \ 24\ .8 = \ 5 \ \ 24\ .7 \\
1\ .1 \text{ E. of } \ 5 \ \ 25\ .8 = \ 5 \ \ 24\ .7
\end{array}\right\} \text{check.}
\end{array}
$$

387. In discussing these cases, we have assumed that there was a point of one line which had a common latitude with a point of the other line; this would be the case if two lines were worked from time sights taken at the same time. It may occur, however, either that they have not a common latitude, but do have a common longitude, as in the case of two lines worked from φ' φ'' (latitude) sights taken at the same time; or that they have neither a common latitude nor a common longitude, as with one time sight and one latitude sight, or with two sights taken at different times.

In case there is a common longitude (fig. 50), which will be rather a rare one, the problem is worked with OP as a *longitude* coordinate; the modification of the other method will suggest itself, the principal change rendered necessary being due to the fact that the angles from the course in Table 5 B will be complementary to what they were before, as we are now dealing with angles to the meridian instead of angles to the parallel.

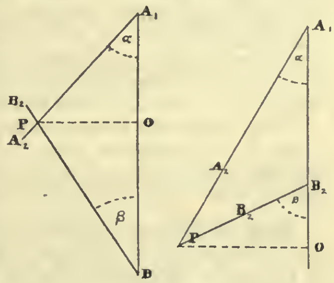


Fig. 50.

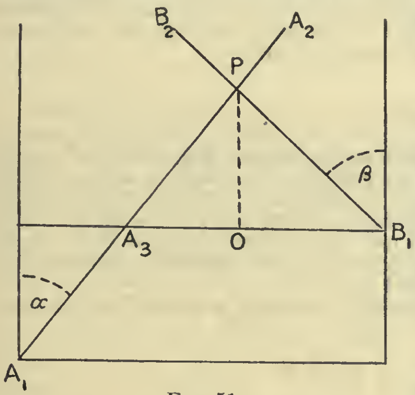


Fig. 51.

When there is no common coordinate of either latitude or longitude, the simplest way of solving is first to find some point on one line which corresponds in latitude with one of the points on the other line, then solve as before.

Thus, in figure 51, given A_1 A_2 and B_1 B_2, find α and β, and thence the longitude of a point A_3 corresponding to the difference of latitude between A_1 and B_1 on the course α; then find intersection of A_3 A_2 and B_1 B_2 in the usual way.

Example: Let it be required to find the intersection of Sumner lines as follows:

$$
A_1\begin{cases} 25^\circ\ 30'\ \text{S.} \\ 115 \ \ 22 \ \ \text{E.}\end{cases}
\quad
A_2\begin{cases} 25^\circ\ 50'\ \text{S.} \\ 115 \ \ 40 \ \ \text{E.}\end{cases}
\quad
\begin{array}{l} +20' \text{ lat.} \\ +18 \text{ long.}\end{array}
\quad
\begin{array}{l} \text{Line runs SE.–NW.} \\ \alpha = 42^\circ. \end{array}
$$

$$
B_1\begin{cases} 25 \ \ 15 \ \ \text{S.} \\ 115 \ \ 37 \ \ \text{E.}\end{cases}
\quad
B_2\begin{cases} 25 \ \ 35 \ \ \text{S.} \\ 115 \ \ 30 \ \ \text{E.}\end{cases}
\quad
\begin{array}{l} +20 \text{ lat.} \\ -\ 7 \text{ long.}\end{array}
\quad
\begin{array}{l} \text{Line runs NE.–SW.} \\ \beta = 19^\circ \end{array}
$$

Find where B_1 B_2 crosses parallel 25° 30′ S.
$\beta=19^\circ$, lat. $=+15'$, dep. $=-5'.1$. Hence, the line B_3 B_2 becomes:

$$
B_3\begin{cases} 25^\circ\ 30'\ \text{S.} \\ 115 \ \ 31.9\ \text{E.}\end{cases}
\quad A_1\ B_3 = 9'.9 \quad
\begin{array}{l} \text{Line runs NE.–SW.} \\ \beta = 19^\circ. \end{array}
$$

The directions of the lines (fig. 52) require us to follow Case I. A_1 is west of B_3. The line through A_1 runs SE.–NW., and that through B_3, SW.–NE. Therefore, the intersection is south of A_1 and B_3, east of A_1, and west of B_3.

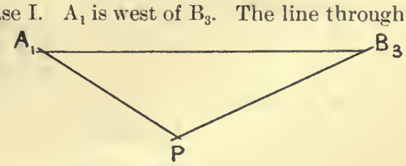


Fig. 52.

(*a*) By Table 5 B. $(90^\circ-\alpha)=48^\circ$, $(90^\circ+\beta)=109^\circ$. Ratio $0.81\times 9'.9=8'.0$ lat.; $\alpha=42^\circ$, lat. $=8'.0$, dep. $=7'.2$. $\beta=19^\circ$; lat. $=8'.0$, dep. $=2'.7$.

Hence, intersection:

$$
\begin{array}{l}
8' \ \text{S. of } \ 25^\circ\ 30' \ \ \text{S.} = \ 25^\circ\ 38' \ \ \text{S.} \\
\left.\begin{array}{l}
7.2 \text{ E. of } 115 \ \ 22 \ \ \ \text{E.} = 115 \ \ 29.2 \text{ E.} \\
2.7 \text{ W. of } 115 \ \ 31.9 \text{ E.} = 115 \ \ 29.2 \text{ E.}
\end{array}\right\} \text{check.}
\end{array}
$$

(*b*) By Table 2:

Assuming lat	6′	8′
Dep. for 42°	5.5	7.2
Dep. for 19°	2.1	2.7
Sum............	7.6	9.9

Intersection:

8′ S. of 25° 30′ = 25° 38′
7.2 E. of 115 22 = 115 29.2 } check.
2.7 W. of 115 31.9 = 115 29.2 }

388. The following is a summary of the method when lines are given by coordinates of two points of each:

(a) By Table 5 B.

1. Write down lines; find α and β.
2. If there are no points which have a common latitude, reduce one point of one line to latitude of some given point of the other.
3. Write down difference of longitude.
4. Draw rough sketch to illustrate direction of point of intersection.
5. Enter Table 5 B:
Case I, angles $(90° - \alpha)$ and $(90° + \beta)$ *or* $(90° - \beta)$ and $(90° + \alpha)$.
Case II, angles $(90° + \alpha)$ and $(90° + \beta)$ *or* $(90° - \beta)$ and $(90° - \alpha)$.
Take out ratio from *second* column, and multiply by difference of longitude; this gives difference of latitude of intersection from the common latitude.
6. Find departure corresponding respectively to α and β with latitude; this gives differences of longitude to the point of intersection from the respective points of common latitude.

(b) By Table 2.

1. Write down lines; find α and β.
2. If there are no points which have a common latitude, reduce one point of one line to latitude of some given point of the other.
3. Write down difference of longitude.
4. Draw rough sketch to illustrate direction of point of intersection.
5. Enter Table 2, at pages α and β; find by trial some latitude at which—
Case I, the sum of the corresponding departures equals the total difference of longitude;
Case II, the difference of the corresponding departures equals the total difference of longitude.
These give differences of latitude and longitude to the point of intersection from the respective points of common latitude.

389. If the lines, instead of being defined by coordinates of two points, are defined by the coordinates of one point of each with its direction as deduced from the azimuth of the body, it will be better not to consider the projection on the fictitious plane through the meridian, as there will then be no advantage in so doing. In this case, consider the angles of the lines with the meridian, as given, α and β; reduce the difference of longitude $A_1 B_1$ to departure, and use this in miles instead of the $A_1 B_1$ in minutes; and when A_1O and B_1O are found, being in miles of departure, they must be reduced to minutes of longitude before being applied to the longitude of A_1 and B_1.

EXAMPLE: The Sumner lines of the last example being expressed by a single point and the direction, as given below, find the intersection.

A { 25° 40′ S. / 115 31 E. } Line runs ($\alpha =$) N. 39° W.

B { 25 25 S. / 115 33.5 E. } Line runs ($\beta =$) N. 18° E.

First bring second line up to Lat. 25° 40′ S. $\beta = 18°$; lat. $= +15'$; dep. $= -4.9$ m.; diff. long. $= -5'.4$; hence we have:

B′ { 25° 40′ S. / 115 28.1 E. } Line runs ($\beta =$) N. 18° E.

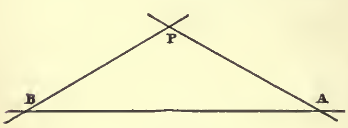


FIG. 53.

AB′ = 2′.9 = 2.6 miles.

B′ being west of A (fig. 53), and the lines through the two points running respectively NE. and NW., the intersection is north of both, east of B′, and west of A.

(*a*) By Table 5 B. $(90° - \alpha) = 51°$; $(90° + \beta) = 108°$. Ratio $0.88 \times 2.6 = 2'.3$ lat. $\alpha = 39°$, lat. $= 2'.3$, dep. $= 1.8$ m., diff. long. $= 2.0$. $\beta = 18°$, lat. $= 2'.3$, dep. $= 0.7$ m., diff. long. $= 0.8$.

Intersection:

2′.3 N. of 25° 40′ S. = 25° 37′.7 S.
2 .0 W. of 115 31 E. = 115 29 E. } check.
0 .8 E. of 115 28.1 E. = 115 28 .9 E. }

(*b*) By Table 2:

Assuming lat	4′	2′	2′.3
Dep. for 39°	3.2	1.6	1 .9 = 2′.1
Dep. for 18°	1.3	0.7	0 .7 = 0 .8
Sum	4.5	2.3	2 .6 = 2 .9

Intersection:

2′.3 N. of 25° 40′ = 25° 37′.7
2 .1 W. of 115 31 = 115 28 .9 } check.
0 .8 E. of 115 28.1 = 115 28 .9 }

The following summary gives the various steps when the lines are each given by the coordinates of one point with the direction:

(*a*) *By Table 5 B.*

1. Write down lines as given.
2. If the points have not a common latitude, reduce one point to latitude of the other.
3. Write down difference of longitude and convert it to departure.
4. Draw rough sketch to illustrate direction of point of intersection.
5. Enter Table 5 B:

Case I, angles $(90°-\alpha)$ and $(90°+\beta)$ *or* $(90°-\beta)$ and $(90°+\alpha)$.

Case II, angles $(90°+\alpha)$ and $(90°+\beta)$ *or* $(90°-\beta)$ and $(90°-\alpha)$.

Take out ratio from second column, and multiply by departure between the two points; this gives difference of latitude of intersection from common latitude.

6. Find departure corresponding respectively to α and β with this difference of latitude, and convert to difference of longitude; this gives differences of longitude to the point of intersection from the respective points of common latitude.

(*b*) *By Table 2.*

1. Write down lines as given.
2. If the points have not a common latitude, reduce one point to latitude of the other.
3. Write down difference of longitude and convert it to departure.
4. Draw rough sketch to illustrate direction of point of intersection.
5. Enter Table 2 at pages α and β; find by trial some latitude at which—

Case I, the sum of the corresponding departures equals the departure between the two points;

Case II, the difference of the corresponding departures equals the departure between the two points.

This difference of latitude, and these departures (converted into difference of longitude) give distance of point of intersection in latitude and longitude from the respective points of common latitude.

390. The modification of the methods for finding the intersection of two Sumner lines, where there is a run between the observations from which they are deduced, will be readily apparent. It is known that at the time of taking a sight the vessel is at one of the points of the Sumner line, but which of the various points represents her precise position must remain in doubt until further data are acquired. Suppose, now, that after an observation the vessel sails a given distance in a given direction; it is clear that while her exact position is still undetermined it must be at one of the series of points comprised in a line parallel to the Sumner line and at a distance and direction therefrom corresponding to the course and distance made good; hence, if a second sight is then taken, the position of the vessel may be found from the intersection of two lines—one, the Sumner line given by the second observation, and the other a line parallel to the first Sumner but removed from it by the amount of the intervening run.

Positions may be brought forward graphically on a chart by taking the course from the compass rose with parallel rulers, and the distance by scale with dividers. If the method given in article 383 be employed, runs in latitude and longitude must each be applied on their own scales, as explained in the description of the method. If one of the methods by computation be adopted, the point or points of the first line are brought forward by the traverse tables, using middle latitude sailing. The direction of a Sumner line as determined from the azimuth of the body always remains the same, whatever shift may be made in the position of the point by which the line is further defined.

CHAPTER XVI.

THE PRACTICE OF NAVIGATION AT SEA.

391. Having set forth in previous chapters the methods of working dead reckoning and of solving problems to find the latitude, longitude, chronometer correction, and azimuth from astronomical observations, it will be the aim of the present chapter to describe the conditions which govern the choice and employment of the various problems, together with certain considerations by which the navigator may be guided in his practical work at sea.

392. DEPARTURE AND DEAD RECKONING.—On beginning a voyage, a good departure must be taken while landmarks are still in view and favorably located for the purpose; this becomes the origin of the dead reckoning, which, with frequent new departures from positions by observation, is kept up to the completion of the voyage, thus enabling the mariner to know, with a fair degree of accuracy, the position of his vessel at any instant.

At the moment of taking the departure, the reading of the patent log (which should have been put over at least long enough previously to be regularly running) must be recorded, and thereafter at the time of taking each sight and at every other time when a position is required for any purpose, the log reading must also be noted. It is likewise well to read the log each hour, for general information as to the speed of the vessel as well as to observe that it is in proper running order and that the rotator has not been fouled by seaweed or by refuse thrown overboard from the ship. It is a good plan to record the time by ship's clock on each occasion that the log is read, as a supplementary means of arriving at the distance will thus be available in case of doubt. If a vessel does not use the patent log but estimates her speed by the number of revolutions of the engines or the indications of the chip log, the noting of the time becomes essential. A good sight is of no value unless one knows the point in the ship's run at which it was taken, so that the position it gave may be brought forward with accuracy to any later time.

393. ROUTINE DAY'S WORK.—The routine of a day's work at sea, no part of which should ever be neglected unless cloudy weather renders it impossible to follow, consists in working the dead reckoning, an a. m. time sight and azimuth taken when the sun is in its most favorable position for the purpose, a meridian altitude of the sun (or, when clouds interfere at noon, a sight for latitude as near the meridian as possible), and a p. m. time sight and azimuth. This represents the minimum of work, and it may be amplified as circumstances render expedient.

394. MORNING SIGHTS.—The morning time sight and azimuth should be observed, if possible, when the sun is on the prime vertical. As the body bears east at that time, the resulting Sumner line is due north and south, and the longitude will thus be obtained without an accurate knowledge of the latitude. Another reason for so choosing the time is that near this point of the sun's apparent path the body is changing most slowly in azimuth, and an error in noting the time will have the minimum effect in its computed bearing. The time when the sun will be on the prime vertical—that is, when its azimuth is 90°—may be found from the azimuth tables or the azimuth diagram. Speaking generally, during half the year the sun does not rise until after having crossed the prime vertical, and is therefore never visible on a bearing of east. In this case it is best to take the observation as soon as it has risen above the altitude of uncertain atmospheric effects—between 10° and 15°.

A series of several altitudes should be taken, partly because the mean is more accurate than a single sight, and partly because an error in the reading of the watch or sextant may easily occur when there is no repetition. If the sextant is set in advance of the altitude on even five or ten minute divisions of the arc, and the time marked at contacts, the method will be found to possess various advantages. As the sight is being taken the patent log should be read and ship's time recorded. It is well, too, to make a practice of noting the index correction of the sextant each time that the sextant is used. The bearing of the sun by compass should immediately afterward be observed, and the heading by compass noted, as also the time (by the same watch as was used for the sight).

Before working out the sight, the dead reckoning is brought up to the time of observation, and the latitude thus found used as the approximate latitude at sight. It is strongly recommended that *every sight be worked for a Sumner line*, either by assuming two latitudes, or by using one latitude and the azimuth, the advantages derived therefrom being always well worth the small additional labor expended.

The compass error is next obtained. From the time sight the navigator learns that his watch is a certain amount fast or slow of L. A. T., and he need only apply this correction to the watch time of azimuth to obtain the L. A. T. at which it was observed; thence he ascertains the sun's true bearing from the azimuth tables or azimuth diagram, compares it with the compass bearing, and obtains the compass error; he should subtract the variation by chart and note if the remainder, the deviation, agrees with that given in his deviation table; but in working the next dead reckoning, if the ship's course does not change, the total compass error thus found may be used without separating it into its component parts. It should be increased or decreased, however, as the ship proceeds, by the amount of any *change* of the variation that the chart may show.

395. If there is any fear of the weather being cloudy at noon, the navigator should take the precaution, when the sun has changed about 30° in azimuth, to observe a second altitude and to record the appropriate data for another sight, though this need not actually be worked unless the meridian

observation is lost. If it is required, it may be worked for either a time sight or φ' φ'' sight, according to circumstances, a second Sumner line obtained, and the intersection of the earlier Sumner with it will give the ship's position.

396. Noon Sights.—Between 11 and 11.30 o'clock (allowing for gain or loss of time due to the day's run) the ship's clocks should be set for the L. A. T. of the prospective noon position. The noon longitude may be closely estimated from the morning sight and the probable run. The navigator should also set his own watch for that time, to the nearest minute, and note exactly the number of seconds that it is in error. He may now compute the constant (art. 333, Chap. XII) for the meridian altitude. The daily winding of the chronometer is a most important feature of the day's routine, and may well be performed at this hour. At a convenient time before noon, the observations for meridian altitude are commenced and continued until the watch shows L. A. noon, at which time the meridian altitude is measured and the latitude deduced.

If the weather is cloudy and there is doubt of the sun being visible on the meridian, an altitude may be taken at any time within a few minutes of noon, the time noted, and the interval from L. A. noon found from the known error of the watch. It is then the work of less than a minute to take out the a from Table 26, the at^2 from Table 27, and apply the reduction to the observed altitude to obtain the meridian altitude. Indeed, the method is so simple that it may be practiced every day and several values of the meridian altitude thus obtained, instead of only one.

397. It now becomes necessary to find the longitude at noon. This may be done graphically by a chart, or by computation. The former plan needs no explanation. There are a number of variations in the methods of computation, one of which will be given as a type.

By the ship's run, work back the noon latitude to the latitude at a. m. time sight. If the Sumner line was found from two assumed latitudes which differed $+m$ minutes, while the corresponding longitudes differed $\pm n$ minutes, then $1'$ difference of latitude causes $\pm \frac{n}{m}$ minutes difference of longitude. If the true latitude at sight is $\pm x$ minutes from one of the assumed latitudes, then $\pm x \times \frac{n}{m}$ is the corresponding difference of longitude. If the Sumner line was found from one assumed latitude and an azimuth, Z, it makes an angle with the meridian equal to $90° - Z$. Enter the traverse table with this as a course and with the difference between the true and assumed latitudes as a latitude, and the departure will be found; convert this into difference of longitude at the latitude of observation, and apply the result with its proper sign to the longitude corresponding to the assumed latitude. Having thus the longitude at sight, the longitude at noon is worked forward for the run. If the sights show a considerable current it should be allowed for, both in working back the latitude and in bringing up the longitude for the run between the sight and noon.

398. Current and Run.—The current may be found by comparing the noon positions as obtained by observation and by dead reckoning; and the day's run is calculated from the difference between the day's noon position by observation and that of the preceding day. To "current" is usually attributed all discrepancies between the dead reckoning and observations; but it is evident that this is not entirely due to motion of the waters, as it includes errors due to faulty steering, improper allowance for the compass error, and inaccurate estimate of the vessel's speed through the water.

The noon position by observation becomes the departure for the dead reckoning that follows.

399. Afternoon Sights.—The p. m. time sight and azimuth is similar to the morning observation.

400. Sumner Lines.—By performing the work that has just been described a good position is obtained at noon each day, which, in a slow-moving vessel with plenty of sea room, may be considered sufficient; but conditions are such at times as to render it almost imperatively necessary that a more frequent determination of the latitude and longitude be made. If the vessel is near the land or in the vicinity of off-lying dangers, if she is running a great circle course requiring frequent changes, if she is making deep-sea soundings, if she has just come through a period of foggy or cloudy weather, or if the indications are that she is about to enter upon such a period, it is obviously inexpedient to await the coming of the next noon for a fix. The responsibilities resting upon the navigator require that he shall earlier find his ship's position; and, generally speaking, the greater the speed made by the vessel the more absolute is this requirement.

The key to all such determinations will lie in the Sumner line, and a clear understanding of the properties of such a line will greatly facilitate the solutions. The mariner must keep in mind two facts: First, that a single observation of a heavenly body can never, by itself, give the *point* occupied by an observer on the earth's surface; and second, that whenever any celestial body is visible, together with enough of the horizon to permit the measuring of its altitude, an observer may thereby determine a *line* which passes through his own position on the earth's surface in a direction at right angles to the bearing of the body.

It may readily be seen that if two Sumner lines are determined the observer's position must be at their intersection, and that that intersection will be most clearly marked when the angle between the lines equals 90°; hence, if two heavenly bodies are in sight at the same time the position may be found from the intersection of their Sumner lines, the angle of intersection being equal to the horizontal angle between the bodies. If only one body is in sight, as is generally the case when the sun is shining, one line of position may be gotten from an altitude taken at one time, and a second line from another altitude taken when it has changed some 30° in azimuth—usually, a couple of hours later. Bringing forward the first line for the intervening run, the intersection may be found.

With the general principles of the Sumner line clearly before him, the navigator will find no difficulty in making the choice of available bodies. If about to take a star sight, and sky and horizon are equally good in all quarters, two bodies should be taken whose azimuths differ as nearly as possible by 90°. If one body can be taken on or near the meridian, its bearing being practically north or south, the resulting Sumner line will be east and west—that is, it may be said that whatever the longitude (within its known limits) the latitude will be the same; the other sight may then be worked as a time sight with this single latitude and time will thus be saved. The same is true if Polaris is observed, and it is a very convenient practice to take an altitude of that star at dawn and obtain a latitude for working

the a. m. time sight of the sun. A similar case arises when a body is observed on the prime vertical; its Sumner line then runs north and south and coincides with a meridian; if the other body is favorably located for a $\varphi' \ \varphi''$ sight, it may be worked with a single longitude and the latitude thus found directly.

If it is not possible to obtain two lines and thus exactly locate the ship, the indications of a single line may be of great value to the navigator. A Sumner line and a terrestrial bearing will give the ship's position by their intersection in the same manner as two lines of position or two bearings; or the position of the ship on a line may be shown with more or less accuracy by a sounding or a series of soundings. If the body be observed when it bears in a direction at right angles to the trend of a neighboring shore line, the resulting line will be parallel with the coast and thus show the mariner his distance from the land, which may be of great importance even if his exact position on the line remains in doubt. If the bearing be parallel to the coast line, then the Sumner line will point toward shore; the value of a line that leads to the point that the vessel is trying to pick up is amply demonstrated by the experience of Captain Sumner that led to the discovery of the method (art. 372, Chap. XV).

For especially accurate work three Sumner lines may be taken, varying in azimuth about 120°; if they do not intersect in a point, the most probable position of the ship is at the center of the triangle that they form.

If two pairs of lines be determined, each pair based upon observation of two bodies bearing in nearly opposite directions and at about the same altitude, the mean position that results from the intersection of the four lines will be as nearly as possible free from those errors of the instrument, of refraction, and of the observer, which can not otherwise be eliminated. This is fully explained in article 451, Chapter XVII.

401. Use of Stars, Planets, and Moon.—It may be judged that the employment in navigation of other heavenly bodies than the sun is considered of the utmost importance, and mariners are urged to familiarize themselves with the methods by which observations of stars, planets, and the moon may be utilized to reveal to them the position of their vessels at frequent intervals throughout the twenty-four hours.

It should be remembered, however, that in order to be of value these observations must be accurate; and to measure an accurate altitude of the body above the horizon it is required not only that the body be visible but also that the horizon be distinctly in view. Care should therefore be taken to make the observations, if possible, at the time when the horizon is plainest—that is, during morning and evening twilight. It may be urgently required to get a position during hours of darkness, and a dim horizon line may sometimes be seen and an observation taken, using the star telescope of the sextant; if the moon is shining, its light will be a material aid; but results obtained from such sights should be regarded as questionable and used with caution. Altitudes measured, however, just before sunrise and just after sunset are open to no such criticism; a fairly well-practiced observer who takes a series of sights at such a time, setting the sextant for equal intervals of altitude, will find the regularity of the corresponding time intervals such as to assure him of accuracy.

402. Identification of Unknown Bodies.—On account of the very great value to be derived from the use of stars and planets in navigation, it is strongly recommended that all navigators familiarize themselves with the names and positions of those fixed stars whose magnitude renders possible their employment for observations, and also with the general characteristics—magnitude and color—of the three planets (Venus, Jupiter, and Mars) which are most frequently used. A study of the different portions of the heavens, with the aid of any of the numerous charts and books which bear upon the subject, will enable the navigator to recognize the more important constellations and single stars by their situation with relation to each other, and to the pole and the equator.

It may occur, however, that occasion will arise for observing a body whose name is not known, either because it has not been learned, or because the surrounding stars by which it is usually identified are obscured by clouds or rendered invisible by moonlight or daylight. In such a case the observer may estimate the hour angle and declination (the hour angle applied to local sidereal time giving the right ascension), and the star or planet may thus be recognized from a chart or from an inspection of the Nautical Almanac. This rough method will generally suffice when the body is the only one of its magnitude within an extensive region of the heavens; but cases often arise where a much closer approximation is necessary, and more exact data is required for identification.

403. If in doubt as to the name of the body at the time of taking the sight, it should be made an invariable rule to observe its bearing by compass, whence the true azimuth may be approximately deduced by applying the compass error. The method[a] to be described then affords a convenient means of identification. The quantities given are the corrected altitude of observation, h, the (approximate) true azimuth of the body, Z, and the latitude by dead reckoning, L; those to be determined are the declination, d, and the hour angle, t. From the astronomical triangle we have:

$$\frac{\sin Z}{\sin p}=\frac{\sin t}{\cos h}; \text{ or, } \sin Z \cos h=\sin t \cos d.$$

The value of sin Z cos h (calculated from the given azimuth and altitude) must therefore equal sin t cos d, whatever the values of t and d may prove to be.

From a given latitude, azimuth and declination, the hour angle may be found either by azimuth tables or an azimuth diagram; or from a given latitude, azimuth and hour angle, the declination may be found by the same means. If, therefore, some probable value of the declination be assumed, using the known latitude and azimuth, we may ascertain the corresponding hour angle; or, if the hour angle be assumed, the corresponding declination is obtained; then the product of sin t cos d may be calculated, and if it agrees substantially with sin Z cos h, the trial values of the hour angle and declination are the correct ones; if not, other trials may be made until the correct ones are found. It may be remembered that absolutely exact results are not sought, and in practice the operation may be made very short; the

[a] Suggested by Lieut. G. W. Logan, U. S. Navy.

values of the quantities may be taken in even degrees and the logarithms need not be carried beyond the third place; the sum of the logarithms will suffice and the corresponding numbers do not have to be taken out. The possibility that the observed body may have been a planet must always be kept in mind in looking it up in the star table or chart.

EXAMPLE: May 16, 1879, in Lat. 5° N., Long. $2^h\ 53^m$ W. by D. R., a star is observed whose corrected altitude is 38°, and true azimuth N. 107° E. The Greenwich sidereal time (as computed for use in the regular working of the sight) is $12^h\ 53^m$. Let it be required to identify the body.

First find the logarithm of sin Z cos h.

Z	107°	sin 9.981
h	38°	cos 9.897
sin Z cos h log		9.878

Now suppose the observer estimates from the position of the body that its declination is 3° S. Look in the azimuth table on the page of latitude 5° (declination contrary name to latitude), and find the hour angle (p. m.) corresponding to Dec. 3° and Az. 107°; this is about $1^h\ 40^m$; then with $d=3°$, $t=1^h\ 40^m$, find sin t cos d. (Sin t may be obtained either by converting time into arc and taking from the table in the usual way, or by multiplying by 2 and finding it from the column headed "Hour P. M." Thus in the present case find the sine of 25° 00′ or of $3^h\ 20^m$. In using the time column be careful to take the name from the foot of the page when the double angle exceeds 6^h.)

t	$1^h\ 40^m$	sin 9.626
d	3°	cos 9.999
sin t cos d log		9.625

As this logarithm should equal 9.878, it is seen that the assumption is incorrect. Try a value of the declination 5° farther south—that is, 8° S. The corresponding hour angle is $2^h\ 50^m$.

t	$2^h\ 50^m$	sin 9.830
d	8°	cos 9.996
sin t cos d log		9.826

The logarithm is not yet quite large enough; assume declination 10° S.; the hour angle is $3^h\ 20^m$.

t	$3^h\ 20^m$	sin 9.884
d	10°	cos 9.993
sin t cos d log		9.877

This is practically identical with the logarithm of sin Z cos h, and the correct values are, therefore, $t=3^h\ 20^m$, $d=10°$ S.

We now have:

G. S. T.	12^h	53^m	
Long.	2	53	W.
L. S. T.	10	00	
H. A.	3	20	E.
R. A.	13	20	

From the Nautical Almanac it is found that the right ascension of Spica is $13^h\ 19^m$ and the declination 10° 32′ S. This is therefore the body observed.

EXAMPLE: March 18, 1879, in Lat. 26° S., Long. $5^h\ 42^m$ E., by D. R., the altitude of a body is 41° and its azimuth S. 84° E., the Greenwich sidereal time being $10^h\ 52^m$. Required the name of the body.

Z	84°	sin 9.998
h	41°	cos 9.878
sin Z cos h log		9.876

Assume first an hour angle of $3^h\ 00^m$. The corresponding declination is 23° (same name as latitude).

t	$3^h\ 00^m$	sin 9.849
d	23°	cos 9.964
sin t cos d log		9.813

Next assume an hour angle of $3^h\ 30^m$. The declination is then 21° S.

t	$3^h\ 30^m$	sin 9.899
d	21°	cos 9.970
sin t cos d log		9.869

Assume hour angle $3^h\ 35^m$. Declination is still nearest to 21° S

t	$3^h\ 35^m$	sin	9.907
d	21°	cos	9.970
$\sin t \cos d$		log	9.877

The last assumption is therefore correct.
We then have:

G. S. T.	10^h	52^m	
Long.	5	42	E.
L. S. T.	16	34	
H. A.	3	35	E.
R. A.	20	09	

As there is no fixed star corresponding to these coordinates the tables for the planets should be consulted. On March 18, 1879, the right ascension of Mars is $20^h\ 09^m$, and the declination 21° 06′ S. This is therefore the body that was observed.

404. The following is a summary of the method employed:

1. Reduce time of observation to Greenwich sidereal time and find the true altitude to the nearest degree. (These operations must be performed before any sight can be worked; they are, therefore, not strictly a part of the process of identification.)
2. Correct the observed azimuth for deviation and variation.
3. Find the logarithm of $\sin Z \cos h$ to the third place.
4. Assume a declination and find the corresponding hour angle that will produce the given azimuth at the given latitude; or assume an hour angle and find the corresponding declination. (Use an azimuth table or diagram for the purpose.)
5. Find the logarithm of $\sin t \cos d$ to the third place.
6. Observe whether this agrees with the logarithm of $\sin Z \cos h$, and if it does not, repeat trials until an agreement is found.
7. Having found the hour angle and declination, convert the Greenwich sidereal time into local sidereal time and subtract the hour angle if west, or add it if east; the result is the right ascension of the observed body, by which, with the declination and magnitude, the identification is accomplished.

405. The exactness with which the comparison of logarithms is carried out will depend upon the possibility of errors of identification in the region of the heavens involved. It will not usually be necessary to find the correspondence as closely as has been done in the examples given, and the cases will be rare when, with a fair estimate of hour angle or declination at beginning, a sufficiently accurate knowledge of the values can not be arrived at after the second approximation; and frequently the first will suffice for identificaton.

406. Value of the Moon in Observations.—Next to the sun, the most conspicuous body in the heavens is the moon, and it may therefore frequently be employed by the mariner with advantage. Owing to its nearness to the earth and the rapidity with which it changes right ascension and declination, the various corrections entailed render observations of this body somewhat longer to work out, with consequent increased chances of error; and errors in certain parts of the work will have more serious results than with other bodies; the navigator will therefore usually pass the moon by if a choice of celestial bodies is offered for a determination of position; but so many occasions present themselves when there is no available substitute for the moon that the extra time and care necessary to devote to it are well repaid. During hours of daylight it is often clearly visible, and its line of position may cut with that of the sun at a favorable angle, giving a good fix from two observations taken at the same time, when the only other method of finding the position would be to take two sights of the sun separated by a time interval in which an imperfect allowance for the true run intervening would affect the accuracy of the result, or a clouding-over of the heavens would prevent any definite result whatever being reached; and during the night, the gleam upon the water directly below the moon may define the horizon and give opportunity for an altitude of that body when it is impossible to take an observation of any other. Navigators are therefore recommended to make use of the moon with complete confidence whenever it will serve their purposes. It has been the purpose of this work to point out the features of the various sights wherein the practice with the moon differs from that of the sun, stars, or planets; care and intelligent consideration will render these quite clear.

Besides its availability for determining Sumner lines of position, which it shares with other bodies, the moon affords a means for ascertaining the Greenwich mean time independently of the chronometer, thus rendering it possible to deduce the longitude and chronometer error. This is accomplished by the method of lunar distances, which is fully explained in Appendix V. If the Greenwich time given by an observation of lunar distance could be relied upon for accuracy, the method would be a great boon to the navigator; but this is not the case. The most practiced observer can not be sure of obtaining results as close as modern navigation demands, and the errors to which the method is subject are larger than the errors that may be expected in the chronometer, even when the instrument is only a moderately good one and its rate is carried forward from a long voyage. The method is not, therefore, recommended for use except where the chronometer is disabled or where it is known to have acquired some extraordinary error; and when lunar distances are resorted to care must be taken to navigate with due allowance for possible inaccuracy of the results. In this connection it is appropriate to say that the best safeguard against the dire consequences that may result from a disabled or unreliable chronometer is for every vessel to carry two—or, far better, three—of those instruments, the advantages of which plan are stated in article 265, Chapter VIII.

407. Employment of Bodies dependent upon their Position.—The practical navigator will soon observe that there are certain conditions in which bodies are especially well adapted for the finding of latitude, and others where the longitude is obtained most readily.

Taking the sun for an example, when a vessel is on the equator and the declination is zero, that body will rise due east of the observer and continue on the same bearing until noon, when for an instant it will be directly overhead, with a true altitude of 90°, and will then change to a bearing of west, which it will maintain until its setting. In such a case any observation taken throughout the day will give a true north-and-south Sumner line, defining longitude perfectly, but giving no determination of the latitude, excepting for a moment only when the body is on the meridian. With the exception noted, all efforts to determine the latitude will fail. The reduction to the meridian takes the form $\frac{0}{0}$, becoming indeterminate, and in the $\varphi' \varphi''$ sight the cosine of φ' will assume a value that corresponds alike to any angle within certain wide limits—the limits within which the circle of equal altitude has practically a north-and-south direction. In conditions approximating to this we may obtain a longitude position more easily than one for latitude, even within a few minutes of noon.

As the latitude and declination separate, conditions become more favorable for finding latitude and less so for longitude; the intermediate cases cover a wide range, wherein longitude may be well determined by observations three to five hours from the meridian, and latitude by those within two hours of meridian passage. As extreme conditions are approached the accuracy of longitude determinations continues to decrease; at a point in 60° north latitude, when the sun is near the southern solstice, its bearing differs only 39° from the meridian at rising; or, in other words, even if observed at the most favorable position, the resulting Sumner line is such that 1′ in latitude makes a difference of 1.3 miles of departure, or 2′.6 of longitude, and is far better for a latitude determination than for longitude. And in higher latitudes still this condition is even more marked.

Having grasped these general facts, the navigator must adapt his time for taking sights to the circumstances that prevail, and when the sun does not serve for an accurate determination of either latitude or longitude the ability to utilize the stars, planets, and moon as a substitute will be of the greatest advantage.

408. USE OF VARIOUS SIGHTS.—Having taken a sight, the navigator may sometimes be in doubt as to the best method of working it. No rigorous rules can be laid down, and experience alone must be his guide. In a general way it may be well, when the body is nearer to the prime vertical than to the meridian, to work it for longitude, assuming latitude, and using the time sight; and when nearer the meridian to work it for latitude, assuming longitude, by the $\varphi' \varphi''$ method. The time sight is more generally used than the other, it has wider limits of accurate application and is probably a little quicker; but as the meridian is approached and the hour angle decreases small errors in the terms make large ones in the results. The $\varphi' \varphi''$ or latitude method should not ordinarily be employed beyond three hours from the meridian, and then only when the body is within 45° of azimuth from the meridian and has a declination of at least 3°; with an hour angle of 6^h (90°) or a declination of 0° the trigonometric functions assume such form that the method is not available; nor does it give definite results when the azimuth is 90° or thereabouts.

When the body is close enough to the meridian for the method of reduction to the meridian to be applicable, that method is to be preferred because of its quickness and facility. It should be noted, however, that, though close enough to employ the reduction, it may not be sufficiently correct to assume that the body bears due north or south, and the sight should be worked with two longitudes, or the Sumner line determined by the azimuth, unless the bearing nearly coincides with the direction of the meridian.

In cases where a body transits near the zenith, a good fix both in latitude and longitude may be obtained by sights, a few minutes apart, near its meridian passage. Various special methods have been devised for doing this, but it seems simpler to treat the problem as an ordinary one for Sumner lines, except where it falls within the narrow limits of application of the equal altitude method (art. 352, Chap. XIII). The solution is possible, because in the condition where it is available (that of a high transit) the body makes a very rapid change of azimuth (from nearly east to nearly west) in a short space of time, and two observations separated by a short interval give Sumner lines that cut at a favorable angle. The time sight or latitude sight may be used according as the body's bearing is greater or less than 45° from the meridian. If one observation be taken when the bearing is about SE. and the other when it is about SW., the intersection, allowing for intervening run, will not only give the longitude, but will also afford a good check upon the meridian observation for latitude, which, in the case of high transits, it is difficult to make with perfect accuracy.

409. WORKING TO SECONDS AND ACCURACY OF DETERMINATIONS.—The beginner who seeks counsel from the more experienced in matters pertaining to navigation will find that he receives conflicting advice as to whether it is more expedient to carry out the terms to seconds of arc, or to disregard seconds and work with the nearest whole minute.

It is a well-recognized fact that exact results are not attainable in navigation at sea; the chronometer error, sextant error, error of refraction, and error of observation are all uncertain; it is impossible to make absolutely correct allowance for them, and the uncertainty increases if the position is obtained by two observations taken at different times, in which case an exactly correct allowance for the intervening run of the ship is an essential to the correctness of the determination. No navigator should ever assume that his position is not liable to be in error to some extent, the precise amount depending upon various factors, such as the age of the chronometer rate, the quality of the various instruments, the reliability of the observer, and the conditions at the time the sight was taken; perhaps a fair allowance for this possible error, under favorable circumstances, will be 2 miles; therefore, instead of plotting a position upon the chart, and proceeding with absolute confidence in the belief that the ship's position is on the exact point, one may describe, around the point as a center, a circle whose radius is 2 miles—if we accept that as the value of the possible error—and shape the future courses with the knowledge that the ship's position may be anywhere within the circle.

It is on account of this recognized inexactness of the determination of position that some navigators assume that the odd seconds may be neglected in dealing with the different terms of a sight; the average possible error due to this course is probably about one minute, though under certain conditions it may

be considerably more. It is possible that, in a particular case, the error thus introduced through one term would be offset by that from others, and the result would be the same as if the seconds had been taken into account; but that does not affect the general fact that the neglect of seconds as a regular thing renders any determination liable to be in error about one minute. Those that omit the seconds argue, however, that since, in the nature of things, any sight may be in error two minutes, it is immaterial if we introduce an additional possibility of error of one minute, because the new error is as liable to decrease the old one as to increase it; but the fallacy of the argument will be apparent when we return to the circle drawn around our plotted point. The eccentricity of the sextant may exactly offset the improper allowance for refraction, and the mistake in the chronometer error may offset the observer's personal error, but unless we know that such is the case—which we never can—we have no justification for doing otherwise than assume that the ship may be any place within the 2-mile circle. If, now, we increase the possible error by 1 mile, our radius of uncertainty must be increased to 3 miles, and the diameter of the circle, representing the range of uncertainty in any given direction, is thereby increased from 4 to 6 miles.

It is deemed to be the duty of the navigator to put forth every effort to obtain the *most probable* position of the ship, which requires that he shall eliminate possible errors as completely as it lies within his power to do. By neglecting seconds he introduces a source of error that might with small trouble be avoided. This becomes of still more importance since modern instruments and modern methods constantly tend to decrease the probability of error in the observation, and to place it within the power of the navigator to determine his ship's position with greater accuracy.

410. There is a more exact way of defining the area of the ship's possible position than that of describing a circle around the most probable point, as mentioned in the preceding article, and that is to draw a line on each side of each of the Sumner lines by which the position is defined, and at a uniform distance therefrom equal to the possible error that the navigator believes it most reasonable to assume under existing conditions; the parallelogram formed by these four auxiliary lines marks the limit to be assigned for the ship's position; this method takes account of the errors due to poor intersections, and warns the navigator of the direction in which his position is least clearly fixed and in which he must therefore make extra allowance for the uncertainty of his determination.

It must be remembered in this connection that no position can ever be obtained except from the intersection of two Sumner lines, whether or not the lines are actually plotted; thus, a meridian altitude gives a Sumner line that extends due east and west, and a sight on the prime vertical a line that extends north and south, though it may not have been considered necessary to work the former with two longitudes or the latter with two latitudes.

411. The Work Book and Forms for Sights.—The navigation work book, or sight book, being the official record of all that pertains to the navigation of the ship when not running by bearings of the land, should be neatly and legibly kept, so that it will be intelligible not only to the person who performed the work, but also to any other who may have reason to refer to it.

Each day's work should be begun on a new page, the date set forth clearly at the top, and preferably, also, a brief statement of the voyage upon which the ship is engaged. It is a good plan to have the dead reckoning begin the space allotted for the day, and then have the sights follow in the order in which taken. The page should be large enough to permit the whole of any one sight to be contained thereon without the necessity of carrying it forward to a second page. No work should be commenced at the bottom of a page if there is not room to complete it. Every operation pertaining to the working of the sights should appear in the book, and all irrelevant matter should be excluded.

It is well to observe a systematic form of work for each sight, always writing the different terms in the same position on the page; this practice will conduce to rapidity and lessen the chances of error. In order to facilitate the adoption of such a method, there are appended to this work (Appendix II) a series of forms that are recommended for dead reckoning, and for time sights, meridian altitudes, and latitude sights (both by φ' φ'' formula and method of reduction to the meridian), for the sun, stars, planets, and moon, respectively. For beginners, these are deemed of especial importance, and it is recommended that, until perfect familiarity with the different sights is acquired, the first step in working out an observation be to write down a copy of the appropriate blank form, indicating the proper sign of application of each quantity (for which the notes will be a guide), and not to put in any figures until the scheme has been completely outlined; then the remainder of the work will consist in writing down the various quantities in their proper places and performing the operations indicated.

CHAPTER XVII.

MARINE SURVEYING.

412. DEFINITIONS.—*Surveying* is the art of representing upon paper the surface of the earth, giving its characteristic features, such as, on land, the position of prominent objects, heights, and depressions, and on water, the depth, character of bottom, and position of shoals.

Topographical Surveying delineates the land, and *Hydrographic Surveying*, the water.

Geodesy is a higher kind of surveying, which takes into account the curvature of the earth. To points determined by a geodetic survey other surveys are referred.

It is not deemed appropriate to include in this work a complete treatise on Marine Surveying. The scope of this chapter will be to set forth such general information regarding the principles of surveying and the instruments therein employed as will give the navigator an intelligent understanding of the subject sufficient to enable him to comprehend the methods by which marine charts are made, and, if occasion should arise, to conduct a survey with such accuracy as the instruments ordinarily at hand on shipboard may permit. For a more detailed discussion of Marine Surveying, the student is referred to the various publications which treat the subject exhaustively.

INSTRUMENTS EMPLOYED IN MARINE SURVEYING.

413. THE THEODOLITE AND TRANSIT.—The *Theodolite* (fig. 54) is an instrument for the accurate measurement of horizontal and vertical angles. While these instruments vary in detail as to methods of construction, the essential principles are always identical.

A telescope carrying cross-hairs in the common focus of the object-glass and eye-piece is so mounted as to have motion about two axes at right angles to one another; graduated circles and verniers are provided by which angular motion in azimuth and (usually) in altitude may be measured; and the instrument is capable of such adjustment by levels that the planes of motion about the respective axes will correspond exactly with the horizontal and the vertical.

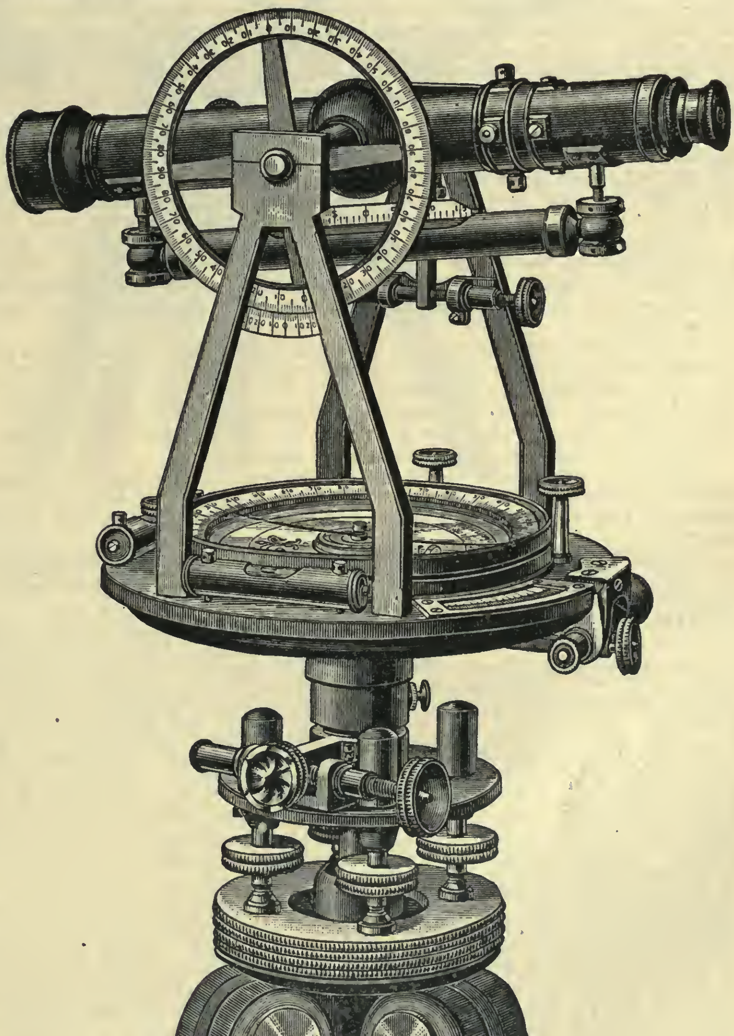


FIG. 54.

The telescope is carried in appropriate supports upon a horizontal plate which has, immovably attached to it, one or more verniers, and which revolves just over a graduated circle that is marked upon the periphery of a second horizontal plate, a means of measuring the motion of the upper plate relatively to the lower one being thus provided. Thumb-screws are fitted by which the upper plate may be clamped to the lower, and (excepting in some simpler forms of the instrument) others by which the lower plate may be made immovable in azimuth, or allowed free motion, at will; all clamping arrangements include slow-motion tangent-screws for finer control.

A vertical graduated circle, or arc, with a vernier, clamps, and tangent-screws, is fitted to most theodolites, for the measurement of the angular motion of the telescope in altitude.

The theodolite usually carries a magnetic needle, with a graduated circle and vernier for compass bearings. The instrument is mounted upon a tripod, and levels and leveling-screws afford a means of bringing the instrument to a truly horizontal position.

The *Transit* used in surveying is a modified form of the theodolite, and is generally employed where less accuracy is required; it takes its name from the fact that the telescope may be turned completely about its horizontal axis, or *transited*, without removal from its supports.

414. The *line of collimation* of a telescope is an imaginary line passing through the optical center of the object-glass in a direction at right angles to that of its axis of rotation. This is also called the *axis of collimation.* The *line of sight* is an imaginary line passing through the optical center of the object-glass and the point of intersection of the cross-hairs.

A theodolite or transit, before it can be used for the accurate measurement of angles, must be in adjustment in the following respects: (*a*) The vertical axes of revolution of the upper and lower horizontal plates must be coincident; (*b*) the axis must be vertical and the plates horizontal when the bubbles of the levels are in their central positions; (*c*) the vertical cross hair must be perpendicular to the horizontal axis of the telescope; (*d*) the line of collimation must coincide with the line of sight; (*e*) the horizontal axis of the telescope must be perpendicular to the vertical axis of the instrument; (*f*) the bubble of the telescope level must stand at the middle of its scale, and the vertical circle must read zero, when the line of collimation is horizontal.

The last-named condition may be disregarded if vertical angles are not to be measured.

415. The instrument being in adjustment, to observe angles it should be set up, leveled, and focused. This involves placing the tripod so that a plumb bob from the center of the instrument shall hang directly over the spot at which the measurement is to be made. The legs of the tripod should be firmly placed in such manner that the height shall be convenient for the observer and the instrument shall be nearly level. Then the horizontal plates are brought to a true level by means of the leveling screws and bubbles. The telescope should next be focused by moving the object glass and eyepiece in such manner that the object sighted and the cross hairs may be plainly seen and that the object will not appear to have motion relatively to the cross hairs as the eye is moved to the right or left in front of the eyepiece. This last condition insures the cross hairs being at the common focus of the eyepiece and objective.

To observe a horizontal angle with a theodolite or transit, clamp the upper plate to the lower at zero, leaving the lower plate unclamped; swing the telescope so that its vertical cross hair bisects one of the objects, and clamp the lower plate; unclamp the upper plate and bring the telescope to bisect the other object, and the reading of the vernier on the scale will give the required angle. (The final nice motion by which the cross-hair is brought exactly upon a point is always given by the tangent screw.)

In taking a *round of angles*, this operation is repeated successively upon each object to be observed about the horizon, the upper plate being always swung, while the lower is kept where set upon the first object, or *origin.* The result will give the angular distance of each object from the origin, and, if the observations have been accurately made, upon finally sighting back to the origin, the reading should be zero.

To *repeat an angle*, having made the first measurement of it in the usual way, unclamp the lower circle and swing back the telescope until it again points to the first object, and clamp it; then unclamp the upper circle, swing to the second object, and clamp. The scale-reading should now be double that of the first angle. Repeat as often as the importance of the angle requires, and the accepted value will be the final reading divided by the number of measurements. All angles of the main triangulation, and others of importance in the survey, are repeated.

Defects in adjustment of the instrument may be eliminated by taking one series of angles with the *telescope direct* and another with the *telescope reversed.* To reverse the telescope, revolve it about its horizontal axis through 180°, then swing it about its vertical axis through 180°—in other words, invert it.

Vertical angles are measured on the same principle as that described for horizontal ones.

The process of setting up the instrument at a station and observing the angles between the various objects that are visible is called *occupying* the station.

416. The Plane Table.—This is an instrument by which positions are plotted in the field directly upon a working sheet. It consists (fig. 55) of a drawing board mounted upon a tripod in such manner as to be capable of motion in azimuth, and with facilities for being brought to a perfect level; in connection with it is employed an alidade, consisting of a straightedge ruler, upon which is mounted a telescope with cross-hairs whose line of sight is exactly parallel to the vertical plane through the edge of the rule. It is evident that if a sheet representing a chart be placed upon such a board and turned so that the true meridians, as portrayed thereon, lie in the direction of the earth's meridian at that place, then all lines of bearings on the chart will coincide with the corresponding lines on the earth's surface; from which it follows that if the alidade be so placed that its rule passes through the spot on the chart representing the position of the observer, while the telescope is directed to some visible object, the position of that object on the chart lies somewhere upon the line drawn along the edge of the rule. Upon this general principle depend the various applications of the plane table.

The drawing board is usually made of several pieces of well-seasoned wood, tongued and grooved together, with the grain running in different directions to prevent warping; about its edge are several metal clips for securing the paper in place. It is supported upon three strong brass arms, to which it is attached by screws, thus permitting its removal at will. The arms are attached to a horizontal plate which revolves upon a second horizontal plate lying immediately below it; a clamp and tangent screw are fitted, by which the upper plate, and with it the drawing board, may be secured to the lower plate, or may be given a fine motion in azimuth. Three equidistant lugs of brass, grooved on the under side, project down from the lower plate, resting on screws in the top of the tripod, by which the instrument is leveled; when adjusted in this respect it is firmly clamped in position, and, as the tripod is made unusually large, the adjustment is not easily deranged.

The alidade is a metal straightedge with a vertical column at its center, at the top of which are the supports which carry the telescope; a vertical arc and vernier are provided for measuring the motion of the telescope in altitude. The telescope is usually so fitted that it may be revolved in azimuth through an arc of exactly 180°, for the purpose of adjusting the line of collimation. On top of the rule near its center is the level—sometimes replaced by two levels at right angles—by means of which it may be seen when the table is in a true horizontal position.

A magnetic needle mounted in a rectangular metal box, whose outer straightedge is parallel to the zero line of a graduated scale over which the needle swings, is provided for drawing the north-and-south line on the chart; this is called a *declinatoire.*

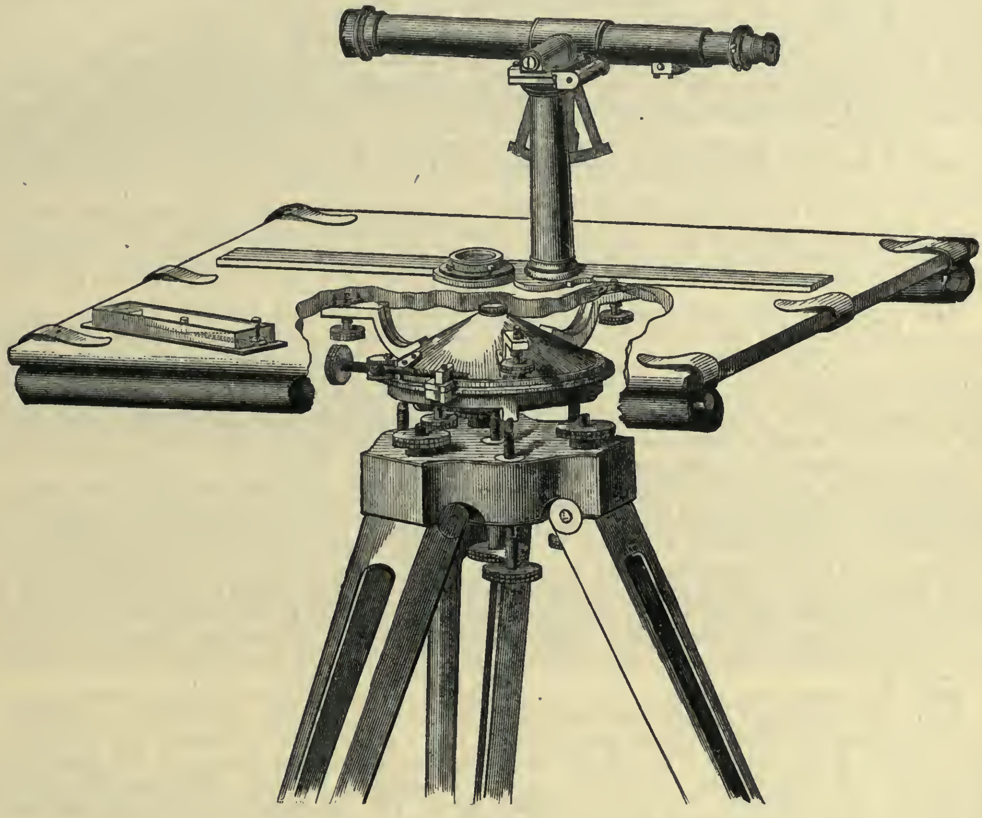


FIG. 55.

417. To be in correct adjustment, a plane table must comply with the following conditions:

(*a*) The fiducial edge of the rule must be perfectly straight. (*b*) The level must have the bubble in its central position when the table is truly horizontal. (*c*) The vertical cross hair must be perpendicular to the horizontal axis of the telescope. (*d*) The line of collimation must coincide with the line of sight. (*e*) The horizontal axis of the telescope must be parallel to the plane of the table. (*f*) The vertical circle should read zero when the line of collimation is horizontal.

418. The results derived from the use of the plane table, like all others dependent upon graphic methods, must be regarded as less accurate than those deduced by computation, and even less accurate than those derived from the careful plotting of theodolite angles. Hence it is that, in a careful marine survey, this instrument would be employed only for the topography and shore line.

For whatever purpose used, the plane table would not ordinarily be called into requisition until the survey had so far progressed that a chart could be furnished the observer showing certain stations whose positions were already established; with this chart, the first step would be to *occupy* one of the determined points. The table must be set up with the point on the chart directly over the center of the station; it must then be leveled and the telescope focused as described for the theodolite or transit; and finally it must be *oriented*, that is, so turned in azimuth that all lines of the chart are parallel to similar lines of the earth's surface. To orient, unclamp the table and swing it until the north-and-south line of the chart is approximately parallel to that of the earth, one means of doing which is afforded by the declinatoire; place the alidade so that the edge of the rule passes through the points on the chart representing the station occupied and some second station which is clearly in view; then, sighting through the telescope, perfect the adjustment of the table by swinging it until the second station is exactly bisected by the vertical cross hair, the final slow motion being obtained by clamping the table and working the tangent screw. If the adjustment has been correctly made, the rule may be laid along the line joining the station occupied and any other on the chart, and the telescope will point exactly to that other station.

Being properly oriented, if the alidade be so placed that the edge of the rule pass through the station occupied, and the telescope point directly to some unknown object whose position is to be determined,

then a line drawn along the rule will contain the point which represents the position of that object. If, now, the plane table be set up at a second station, oriented for its new position, and a line be similarly drawn from that station toward the one to be established, it will intersect the first line in the required point. This is the method of determining positions by *prosection.* Actually, the surveyor does not regard the point as well established until the intersection is checked by a line from a third station.

In practical work, of course, each station is not occupied separately for the determination of each point; the instrument is set up at a station, lines are drawn to all required points in view, and each line is appropriately marked; then a second station is occupied, and the operation repeated, and so on, the various intersections being marked as the work proceeds.

A second method of establishing positions is that of *resection;* in this the first line is drawn from some known station, as in the preceding method, and the observer next proceeds to the place whose position is required and occupies it; the plane table is there oriented by means of the line already drawn, placing the edge of the rule along the line, sighting back toward the first station, and swinging the table until that station is in the line of sight of the telescope; then choose some other established station as nearly as possible at right angles to the direction of the first; place the edge of the rule upon the plotted position of this station and swing the alidade (the rule always being kept on the plotted point) until the object is bisected by the telescope cross-hairs; draw this line, and its intersection with the first will give the required point, the accuracy of which can be checked from some other plotted station.

A third method of locating a point is by means of a single bearing from a known station, with the distance from the occupied station to the required one, the process of plotting being self-evident.

A fourth method is given by occupying an undetermined position from which three established stations are in view; the point occupied by the observer is then plotted by an application of the "three-point problem."

419. It may be seen that where the greatest accuracy is not essential the plane table may be employed for plotting all the points of a survey. In such a case it would only be necessary to begin with the two base stations, plotted on the sheet on any relative bearing whatsoever and at a distance apart equal to the length of the base line (reduced to scale), as measured by the most accurate means available. The work of plotting might even proceed before the base line had been measured, the two stations being laid off at any convenient distance apart; when, later, the base line was measured, the scale of the chart would be determined, being equal to the distance on the chart between base stations divided by the length of the base line.

420. A plane table could be improvised on shipboard which would greatly facilitate the operation of any surveying work that a vessel not equipped with instruments might be called upon to perform. A drawing board could be mounted upon a tripod (as, for example, the tripod supplied for compass work on shore) in such manner as to be capable of motion in azimuth; it could be brought nearly to the horizontal, if no better means offered, by moving the tripod legs, and this adjustment could be proved by any small spirit level; sight vanes could be erected upon an ordinary ruler to take the place of the alidade; in case there was difficulty in observing any object with such an alidade, because of its altitude or for other reasons, a horizontal angle might be observed with a sextant and plotted with a protractor. By this means work could be done which, even if it should lack complete accuracy, might be of great value.

421. The Telemeter and Stadia.—Any telescope fitted with a pair of horizontal cross-hairs at the focus may be used as a *telemeter*, and when accompanied by a graduated staff, called a *stadia*, affords a means of measuring distance (up to certain limits) with a close degree of accuracy; the method consists in observing the number of divisions of the scale subtended by the hairs when the stadia is held up vertically and perpendicular to the line of sight of the telescope, it being evident that the closer the distance the fewer divisions will appear between them. The facility with which distances can be measured by this method makes it most important that all telescopes of theodolites, transits, and plane tables be fitted as telemeters, and that stadia rods be provided for all surveying work.

Speaking approximately, it may be said that the number of divisions intercepted between the cross-hairs will vary directly as the distance of the stadia rod. This would be exactly true if we looked at the object through an empty tube, directly between the hairs. Since, however, the rays from the stadia are refracted by the object glass before they are intercepted by the wires, the statement, to be absolutely exact, must be slightly modified; but for practical surveying work it may be accepted as given.

422. There are two methods of installing the telemeter cross-hairs—the first, in which they are immovably secured in the telescope and always remain at the same distance apart, and the second, in which the distance of the cross hairs is made variable, being under the control of the observer. The former is generally regarded as the preferable method, and when it is employed it is evident that the subtended height of the stadia bears a constant ratio to the distance of the staff from the telescope. It proves most convenient in practice to space the hairs so that this constant ratio is some even multiple of 10, for facility in converting scale readings into distance; it is also advantageous to mark the stadia in the unit of the chart scale and decimals thereof; for example, if the ratio of stadia height to distance were 100, and the stadia were marked in meters and decimals, a reading of 2.07 would at once be converted into a distance of 207 meters. Any units and any ratio may, however, be employed, and for any given setting of cross-hairs it is very easy to graduate a stadia, by experiment, for any desired units; for example, if it is required to mark the stadia in feet, set up and level the telescope, measure off a distance of exactly 100 feet from it, hold up an unmarked staff and mark upon it the points intersected by the cross hairs; the interval between these marks will represent 100 feet of the scale; divide this length into 100 parts, each of which will represent a distance of one foot, and mark the whole staff on the same scale; then if the stadia be held up at any distance. the cross-hairs will intercept a number of divisions corresponding to the number of feet of distance.

When the cross-hairs are movable the ratio becomes variable, but the principle of measuring remains the same—namely, the distance of the staff from the telescope is equal to the existing ratio multiplied by the distance intercepted on the scale.

423. The stadia is made of a light, narrow piece of wood and is usually hinged for convenience in transporting. Ordinarily the background of the scale is painted white, while the main divisions are marked in red, with minor divisions in black, and geometrical figures are employed to facilitate the reading of fractional parts of the scale. Devices are furnished by which the man holding the stadia may know when it is at right angles to the line of sight of the telescope—an essential condition for accuracy of measurements.

424. The use of the telemeter and stadia for measuring distances is limited to the distance at which the scale divisions can be accurately read through the telescope. For fairly close work and with the class of telescope usually supplied with surveying instruments, 400 meters represents about the greatest distance at which it can be employed. With this limitation, the character of the survey determines the nature of its employment. In a careful survey its greatest use would be in connection with the theodolite or plane table in putting in shore lines, contour lines, and topography generally. In a survey where only approximate results are sought it might afford the best means for the measurement of the base.

425. If the telemeter be applied to a theodolite, transit, or plane table which is fitted with a graduated vertical arc or circle, it is possible to measure the distance to the stadia not only in a horizontal but also in a vertical direction. In this case the vertical angle must be observed as well as the stadia reading. Tables are computed giving the solution of the triangles involved.

426. In making a survey with the ordinary resources of a ship, the principle of the telemeter and stadia may be profitably employed, using a sextant and improvised staff. In this case it is usual to have the stadia of some convenient fixed length, as, for example, 10 feet, and of slight width and thickness; this is held at right angles to the line of sight from the observer, who notes the angle subtended by the total length; tables are prepared by which the distance corresponding to each angle is given.

427. The Sextant.—This instrument is of the greatest value in hydrographic surveying. It is fully described elsewhere in this work and its adjustment explained (Chap. VIII).

Sextants are manufactured of a form especially adapted to surveying work; they are smaller and lighter than those usually employed in astronomical observations, but have a longer limb, by which angles may be measured up to 135°; the vernier is marked for quick reading and has no finer graduation than half minutes; the telescope has a large field.

This instrument is principally employed in measuring the horizontal angles by means of which soundings are plotted. It may, however, be put to various uses when making an approximate survey, as has already been explained. It should be remembered, in measuring terrestrial angles with a sextant, that rigorous methods require a reduction to the horizontal if either of the objects has material altitude above the horizon.

428. The Level.—This is an instrument for the accurate measure of differences of elevation. It consists of a telescope, carried in a Y-shaped rest, which is mounted upon a tripod and leveled in a manner similar to a theodolite; but it differs from that instrument in that the telescope is not capable of motion about a horizontal axis, and in having no graduated circle for measurements of altitude and azimuth. The principle of its use contemplates placing the line of collimation of the telescope in a truly horizontal plane and keeping it so fixed.

429. It is principally employed in marine surveying to determine heights and contour lines—the latter being lines of equal elevation above the sea level—and for locating bench marks for tidal observations (Chap. XX). In connection with it is used a graduated staff called a *leveling rod*, carrying a conspicuous mark, adjustable in height, called a *target*. To ascertain the difference of level between any two points, set up the level with the telescope horizontal at some place between them; let an assistant take the leveling rod to one of the points, and, while holding it on the ground in a truly vertical position, move the target, under the direction of the observer at the telescope, to a point where it is exactly bisected by the horizontal cross-hair; the height of the target on the staff—that is, the height of the cross-hair above the level of the first point—is then accurately read with a vernier; now, without moving the level, shift the rod to the second point and again adjust the target and read it. It is evident that a comparison of the reading at the first position with that at the second will give the difference of height at the two points. The difference that can be read from one location of the instrument is limited by the length of the rod; but by making a sufficient number of shifts any difference may be measured.

The work of the level may be performed equally well by a theodolite whose telescope is adjusted to the true horizontal.

430. Heliotrope and Heliograph.—These are instruments sometimes employed in surveying, by means of which the sun's rays may be reflected in any given direction; the object of their use is to render conspicuous a station which is to be observed at a distance and which would not otherwise be distinguishable. The instruments vary widely in form of construction and, in the absence of those made for the purpose, substitutes may easily be devised.

431. Astronomical Transit Instruments.—Various instruments are employed for the astronomical determinations necessary in a marine survey. Among these are the *zenith telescope* and *portable transit*. While differing in detail they consist essentially of a telescope mounted upon a horizontal axis that is placed truly in the prime vertical, thus insuring the revolution of the line of collimation in the meridian; a vertical graduated circle and vernier are supplied, affording a measure of altitude; in the focus are a number of equidistant vertical cross-hairs or lines; a small lamp is so placed that its rays illuminate the cross-hairs and render possible observations at night. Latitude is obtained by observing the meridian altitude of stars; hour angle (and thence longitude) by observing the times of their meridian transit, which is taken from the mean of the times of passing all of the vertical cross-hairs.

Excepting in surveys of a most accurate nature, the astronomical determination of position by the sextant and artificial horizon is regarded as satisfactory.

432. The Three-Armed Protractor, or Station Pointer.—This is an instrument whereby positions are plotted on the principle of the "three-point problem," of which an explanation is given in article 152, Chapter IV. It consists (fig. 56) of a graduated circle with three arms pivoted at the center; each arm has one edge that is a true rule, the direction of which always passes through the center of the circle. The middle arm is immovably fixed at the zero of the scale; the right and left arms each revolve about the center on their own sides, and are provided with verniers giving the angular distance from the middle arm. The protractor being set for the right and left angles, it is so moved that the three arms pass through the respective stations, when the center marks the position of the observer. Center pieces of various forms are provided, being cylindrical plugs made to fit into a socket at the pivot, and by employing one or the other of them the true center may be pricked with a needle, dotted with a pencil, or its position indicated by cross-hairs. Adjustable arms are provided which can be fitted to the ends of the ordinary arms when working with distant signals.

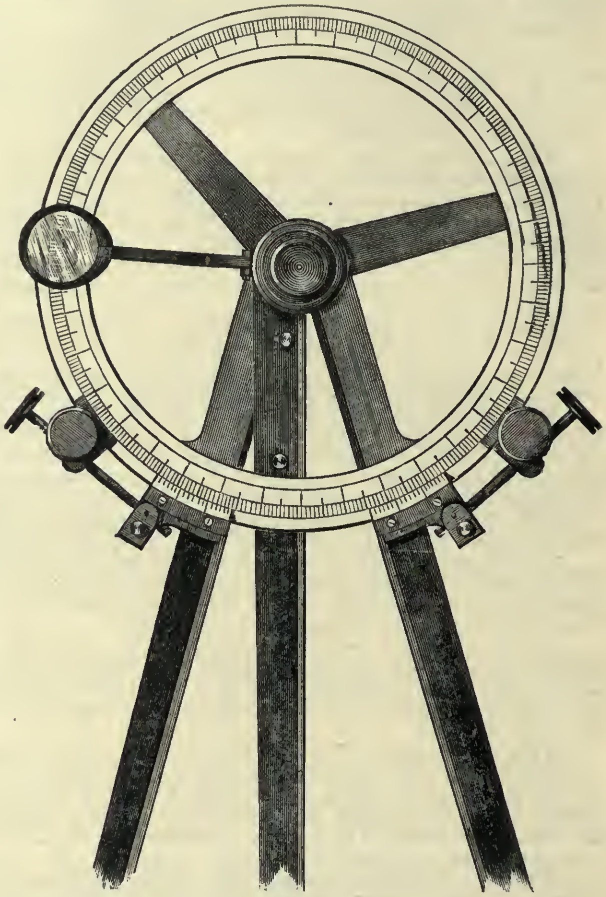


Fig. 56.

The most valuable use of the three-armed protractor is in plotting the positions of soundings taken in boats, where sextant angles between signals are observed. It may occur, however, that certain shore stations will be located by its use.

433. In default of a three-armed protractor, a piece of *tracing paper* may be made to answer its purpose. To use the tracing paper, draw a line, making a dot on it to represent the center station, and with the center of an ordinary protractor on the dot, lay off the two observed angles right and left of the line; then, laying this on the plan, move it about till the three lines pass exactly through the three stations observed. The dot from which they were laid off will be on the position of the observer, and must be pricked lightly through or marked underneath in pencil.

434. The Beam Compass.—This instrument (fig. 57) is employed in chart drafting and performs the functions of compasses and dividers when the distance that must be spanned is beyond the limits of those instruments in their ordinary form. It consists of an angular bar of wood or metal upon which two instruments termed beam heads are fitted in such a manner that the bar may slide easily through them. A clamping screw attached to one side of the beam head will fix it in any part of its course along the beam. Upon each head a socket is constructed to carry a plain point, exchangeable for an ink or a pencil point. For exact purposes the beam head placed at the end of the beam has a fine adjustment, which moves the point a short distance to correct any error in the first rough setting of the instrument. This adjustment generally consists of a milled-head screw, which passes through a nut fixed upon the end of the beam head, which it carries with its motion.

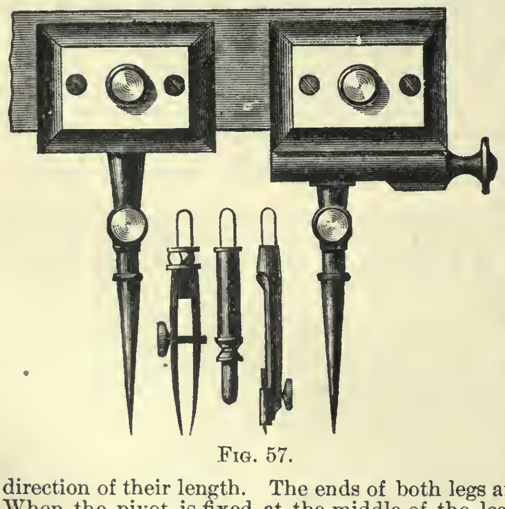


Fig. 57.

435. Proportional Dividers.—These are principally employed for reducing or enlarging drawings in any given proportion. They consist (fig. 58) of two narrow flat pieces of metal called *legs*, which turn upon a pivot whose position is movable in the direction of their length. The ends of both legs are shaped into points like those of ordinary dividers. When the pivot is fixed at the middle of the legs, any distance measured by the points at one end is just equal to that measured by those at the other; for any other location of the pivot, however, the

distances thus measured will not be equal, but with a given setting of the pivot any distance measured by one end bears a fixed ratio to that measured by the other. The path of travel of the pivot is graduated so that the ratio may be given any desired value. Being adjusted in this respect, if a distance is taken off a chart with the legs at one end of the instrument, then those at the other end will show the same distance on the scale of a chart enlarged or reduced in the proportion represented by the ratio for which the pivot was set.

FIG. 58.

METHODS EMPLOYED IN A HYDROGRAPHIC SURVEY.

436. A geodetic survey has for its object the determination, with the greatest attainable accuracy, of points on the surface of the earth, by the employment of a process of triangulation, all positions being located either trigonometrically or astronomically, and the curvature of the earth being taken into account.

Before commencing a survey a general inspection of the field is made; a *base line* is located and its extremities marked by *signals;* certain other positions, known as *main triangulation points*, are selected and also marked with signals, being so chosen that, starting with the base and proceeding thence from one to another of these points, a series of well-conditioned triangles or quadrilaterals may cover the field of survey. The base line is measured with the greatest degree of accuracy which the resources of the survey render possible. Each extremity of the base line and each other main triangulation point is occupied by an observer with a theodolite, who measures the angles at each station between all the other stations which are in sight. An *astronomical determination* is made of the latitude and longitude of some point of the survey (frequently one of the extremities of the base) and of the true azimuth of some known line (frequently the base line). Data is now at hand for the location upon the chart of the base line and main triangulation points.

If the survey is one of considerable extent it is expedient to measure a *check base* near the end of the triangulation, a comparison between the measured and the computed distance between any two stations showing the accuracy of the work and affording a means of reconciling discrepancies. The position of a second observation spot may be determined for a similar purpose.

The *primary triangulation* gives a skeleton of the field, but the points thus determined are not usually close enough together to afford a basis for all the detail work that must be done. A second system of points is therefore selected and signals erected thereon, and the position of these points is determined by a series of angles from the main triangulation points and from each other. This is known as the *secondary triangulation.* The points thus located are used in the plotting of the *topography* and *hydrography.* It is not essential that their determination be as accurate as that of main triangulation points.

The topography is put in, and includes the delineation of the features of the land—shore line, light-houses, beacons, contour lines, peaks, buildings, and, in short, everything that may be recognized by the navigator and utilized by him in locating the ship's position.

The hydrographic work is taken up and the depth of water and character of bottom determined as accurately as possible for the complete water area, especial care being taken to develop all shoals and dangers to navigation and to locate all aids to navigation, such as buoys, light-ships, and beacons.

One or more *tidal stations* are established where observations are taken, continually and at frequent intervals, of the height of the tide and direction and velocity of the tidal and other currents, whence data is derived for the reduction of all soundings to the plane of reference and for the information about tides and currents which is to appear upon the chart.

Observations are made to determine the *magnetic* variation and dip, and the intensity of the earth's magnetic force.

437. The foregoing represent, in outline, the various steps that must be taken in the accumulation of the data necessary for the construction of a complete hydrographic chart. In the following paragraphs the details of the various operations will be more fully set forth.

The navigator who is called upon to conduct a marine survey without having available the time, instruments, and general facilities necessary for the most thorough performance of the work must exercise his discretion as to the modifications of method that he will make, and call upon his ingenuity to adapt his means to the particular work in hand.

438. THE BASE LINE.—As the base line is the foundation for all distances on the chart, the correctness of the results of the survey will depend largely upon the degree of accuracy with which it is measured. The triangulation merely affords a measure of the various distances as compared with the distances between the two initial points from which it began; if that initial distance is 1,000 feet, we have certain values for the sides of the various triangles; if the same base line is 2,000 feet, the value of each side becomes twice as great as it was before; with the same triangulation, therefore, distances vary directly with the length of the base line; it may thus be seen that if an error exists in measurement which is only a small fraction of the total length, the error will become much more material as the more distant points of the survey are reached. In a base line 1,000 feet long, if a mistake of 10 feet be made, all distances measured upon the chart will be in error 1 per cent, and a point plotted by triangulation 10 miles from the observation spot (the point at which plotting begins), would be out of its correct position one-tenth of a mile.

It is important that the base line should be as long as possible, as an error in measurement will thus constitute a smaller percentage of the total length and will not accumulate so rapidly as the work proceeds. The position of the line must be such as to afford favorably conditioned triangles and quadri-

laterals with adjoining main triangulation points, and its extremities must be visible from those points and from each other. The character of the ground and the facility for measuring will of course form an important consideration in the choice.

439. In measuring a base by tape, chain, or similar means, a number of successive fleets are made with the measure, whatever its nature, the distance traversed being appropriately marked after each fleet, while an observer, with a theodolite or transit, insures the measurement being made accurately along the line.

440. The most careful measurements are made by a steel tape 100 feet long, stretched along a series of battens which are supported by metal crutches and made exactly horizontal by a level. The tape is stretched to a uniform tension by a spring balance; its exact length at that tension is known from comparison with some standard; a correction for temperature is applied. The ends of the fleets are marked by driving into the ground a peg carrying in its top a tack; the exact end of the tape is marked by a score filed on the head of the tack at a point marked by a plumb bob from the tape, and this score becomes the origin for the next fleet. An assistant precedes the measuring party before each shift of the battens, and is accurately aligned by the theodolite to mark the true direction of the base line. The result of this method of measurement gives the *horizontal* distance between the points. It can be depended upon for the greatest degree of accuracy of any method, excepting that with a special *base-measuring apparatus*, which is seldom employed in marine surveys.

441. A second method of base measurement is with the surveyor's chain. This depends for accuracy upon the surface traversed being plane and level, a condition that is well fulfilled on a sandy beach, where the chain is nearly as accurate as the tape and much more rapid. A surveyor's chain is usually 100 feet long; the exact value of its length must be obtained by comparison with a standard, and a correction applied for expansion or contraction due to temperature. The ends of the fleets are marked by steel pins driven into the ground; the alignment is kept by the theodolite.

442. Where neither chain nor tape is available substitutes may be improvised from sounding wire taken from the deep-sea sounding machine, or, failing this, from well-stretched cod line.

443. Measurements made by the telemeter and stadia afford a close approximation to the true result, and if these instruments are not at hand the sextant angle of a rod of fixed length can be employed. The masthead height of the vessel may be used in determining the length of base line on this principle, either by making the ship itself mark one of the extremities and observing the masthead angle from the other extremity, or by simultaneously observing the masthead angle from both ends of a shore base, and also the three horizontal angles of the triangle formed by the ship and the two base stations. The latter plan is far preferable where accuracy is sought, as, if the angles are all taken by different observers at the same instant (which can be marked by the hauling down of a flag), the error arising from the motion of the ship about her anchor is eliminated, and, moreover, the data furnished offers a double solution of the triangle and the mean may be taken as giving a closer result.

444. A crude method of measuring a base is by means of the velocity of sound, though this would never be used where close results are expected. Fire a gun at one end of the base and at the other note by the most accurate means available the time between seeing the flash and hearing the report. Repeat several times in each direction. The mean number of seconds and tenths of a second multiplied by the velocity of sound per second at the temperature of observation (art. 314, Chap. XI) gives the approximate length of base line.

445. When for any reason the existing conditions do not permit of a direct measurement being made along the line between the two base stations, recourse must be had to a *broken base,* that is, one in which the length of the base is obtained by reduction from the measured length of two or more auxiliary lines. Necessity for resorting to a broken base arises frequently when the two stations are situated on a curving shore line and the straight line between them passes across water, or where wooded or unfavorable country intervenes, or where a stream must be crossed. The most common form of broken base is that in which the auxiliary lines run from each extremity of the base at an acute angle and intersect; in addition to measuring each of these lines, the angles of the triangle formed by them with the base line must be observed and the true length of the base deduced by solution of the triangle. The form that is most frequently used where only a short section of the base is incapable of measurement (as is the case where a deep stream flows across) is that of an auxiliary right triangle whose base is the required distance along the base line and altitude a distance measured along a line perpendicular thereto to some convenient point; by this measured distance and the angles which are observed, the triangle is solved and the length of the unmeasured section determined.

446. In a survey of considerable extent, where good means are at hand for the correct determination of latitude and longitude, a base line actually measured upon the earth may be dispensed with, and, instead of that, the positions of the two stations which are most widely separated may be determined astronomically and plotted; the triangulation is then plotted upon any assumed scale, and when it has been brought up to connect the two stations the true value of the scale is ascertained. This is called the method of an *astronomical base.*

447. SIGNALS.—All points in the survey whose positions are to be located from other stations, or from which other positions are to be located, must be marked by signals of such character as will render them distinguishable at the distance from which they are observed. The methods of constructing signals are of a wide variety.

A vessel regularly fitted out for surveying would carry scantlings, lumber, bolts, nuts, nails, whitewash, and sheeting for the erection of signals; however meager the equipment, the whitewash and sheeting (or some substitute for sheeting, preferably half of it white and half dark in color,) should be provided, if possible, before beginning any surveying work. Regular tripod signals, which are quickly erected and are visible, under favorable circumstances, for many miles, are almost invariably employed to mark the main triangulation stations; among other advantages the tripod form permits the occupation with the theodolite of the exact center of the station, and avoids the necessity for the reduction which must otherwise be applied. Signals on secondary stations take an innumerable variety of forms, the require-

ment being only that they shall be seen throughout the area over which they are to be made use of; a whitewashed spot on a rock, a whitewashed trunk of a tree, a whitewashed cairn of stones, a sheeting flag, a piece of sheeting wrapped about a bush or hung, with stones attached, over a cliff, or a whitewashed barrel or box filled with rocks or earth and surmounted by a flag, suggest some of the secondary signals that may be employed; sometimes objects are found that are sufficiently distinct in themselves to be used as signals without further marking, as a cupola or tower, a hut, a lone tree, or a bowlder; but it is seldom that an object is not rendered more conspicuous by the flutter of a flag above it, or by the dead-white ray reflected from a daub of whitewash.

For convenience, each signal is given some short name by which it is designated in the records.

448. The Main Triangulation.—The points selected as stations for the main triangulation mark in outline the whole area to be surveyed; they are close enough together to afford an accurate means of plotting all intermediate stations of the secondary triangulation; and they are so placed with relation to one another that the triangles or quadrilaterals derived from them are well conditioned. The points are generally so chosen that small angles will be avoided. In order to fulfill the other conditions, it frequently becomes necessary to carry forward the triangulation by means of stations located on points a considerable distance inland, such as mountain peaks, which would not otherwise be regarded as properly within the limits of the survey.

Great care should be taken in observing all angles upon which the main triangulation is based; the best available instrument should be employed; angles taken with a theodolite or transit should be repeated, and observed with telescope direct and reversed, and the mean result taken; if the sextant is used, a number of separate observations of each angle should be taken and averaged for the most probable value. It must be remembered that while, in any other part of the work, an error in an angle affects only the results in its immediate vicinity, a mistake in the main triangulation goes forward through all the plotting that comes after it.

It frequently occurs that the purposes of the survey are sufficiently well fulfilled by a graphic plotting of the main triangulation, but where more rigorous methods prevail, the results are obtained by calculation. The sum of the angles of each triangle is taken, and if it does not exactly equal 180° the values are adjusted to make them comply with this condition. The lengths of the various sides are then computed, regarding the stations, usually, as forming a series of quadrilaterals, and allowing for the curvature of the earth where the sides are sufficiently long to render it expedient to do so.

449. The Secondary Triangulation.—The points of the secondary triangulation are located, as far as possible, by angles from the main triangulation stations; these angles, having less dependent upon them, need not be repeated. A graphic plotting of these stations, without calculation, will suffice.

450. Astronomical Work.—This comprises the determination of the correct latitude and longitude of some point of the survey, which is the first position plotted, and of the true direction of some other point from the observation spot, which is the first line to be laid down on the chart; it is evident that these determinations form the origin of all positions and of all directions, without which the chart could not be constructed.

The methods of finding latitude, longitude, and the true bearing of a terrestrial object are fully set forth in previous chapters. The feature that distinguishes such work in surveying from that of determining the position of a ship at sea lies in the greater care that is taken to eliminate possible errors. At sea, results of absolute exactness are recognized as unattainable and are not required; but in a careful survey no step which will contribute to accuracy should be neglected.

The results should therefore be based upon a very large number of observations, employing the best instruments that are available, and the various sights being so taken that probable errors are offset in reckoning the mean.

451. By taking a number of sights the observer arrives at the most probable result of which his instruments and his own faculties render him capable; but this result is liable to an error whose amount is indeterminate and which is equal to the algebraic sum of a number of small errors due, respectively, to his instruments (which must always lack perfection in some details), to an improper allowance for refraction under existing atmospheric conditions, and to his own personal error. Assuming, as we may, that the personal error is approximately constant, these three causes give rise to an error by which all altitudes appear too great or too small by a uniform but unknown amount. Let us assume, for an illustration, that this error has the effect of making all altitudes appear 30″ too great; if an observer attempted to work his latitude from the meridian altitude of a star bearing south, the result of this unknown error would give a latitude 30″ south of the true latitude; if another star to the southward were observed, this mistake would be repeated; but if a star to the north were taken, the resulting latitude would be 30″ to the north. It is evident, therefore, that the true latitude will be the mean of the results of observation of the northern and the southern star, or the mean of the average of several northern stars and the average of several southern stars. A similar process of reasoning will show that errors in the determination of hour angle are offset by taking the mean of altitudes of objects respectively east and west of the meridian.

452. It must be remembered that the uniformity of the unknown error only exists where the altitude remains approximately the same, as instrumental and refraction errors may vary with the altitude; another condition of uniformity requires that the instrument and the observer remain the same, and that all observations be taken about the same time, in order that atmospheric conditions remain unchanged; to preserve uniformity, if the artificial horizon is used, the same end of the roof should always be the near one to the observer; in taking the sun, however, as the personal error may not be the same for approaching as for separating limbs, every series of observations should be made up of an equal number of sights taken under each condition.

453. With all of this in mind, we arrive at the general rule that astronomical determinations shall be based upon the mean of observations, under similar conditions, of bodies whose respective distances from the zenith are nearly equal, and which bear in opposite directions therefrom.

454. This condition eliminates the sun from availability for observations for latitude, though it properly admits the use of that body for longitude where equal altitudes or single a. m. and p. m. sights are taken. Opposite stars of approximately equal zenith distance should always be used for latitude, circum-meridian altitudes being observed during a few minutes before and after transit; excellent results are also obtained from stellar observations for longitude; but very low stars should be avoided, on account of the uncertainty of refraction, and likewise very high ones, as the reflection from the index mirror of the sextant may not be perfectly distinct when the ray strikes at an acute angle.

455. If there is telegraphic communication, an endeavor should be made to obtain a time signal from a reliable source, instead of depending upon the chronometers.

456. Topography.—The plane-table, with telemeter and stadia, affords the most expeditious means of plotting the topography, and should be employed when available. Points on shore may also be plotted by sextant angles, using the three-point problem, or by any other reliable method.

457. Hydrography.—The correct delineation of the hydrographic features being one of the most important objects of the survey, great care should be devoted to this part of the work. Soundings are run in one or more series of parallel lines, the direction and spacing of which depend upon the scope of the survey. It is usual for one series of lines to extend in a direction normal to the general trend of the shore line. In most cases a second series runs perpendicular to the first, and in surveys of important bodies of water still other series of lines cross the system diagonally. In developing rocks, shoals, or dangers the direction of the lines is so chosen as will best illustrate the features of the bottom. When lines cross, the agreement of the reduced soundings at their intersection affords a test of the accuracy of the work.

As the depth of water increases, if there is no reason to suspect dangers, the interval between lines may be increased.

Lines are run by the ship or boat in such manner as to follow as closely as possible the scheme of sounding that has been laid out. The position is located by angles at the beginning of each line, at each change of course, at frequent intervals along the line, and at the point where each line is finished. Soundings taken between *positions* are plotted by the time interval or patent-log distances.

458. There are a number of methods for determining positions while sounding, which may be described briefly as follows:

By two sextant angles.—Two observers with sextants measure simultaneously the angles between three objects of known position, and the position is located by the three-point problem. This is the method most commonly employed in boat work, and has the great advantage that the results may be plotted at once on the working sheet in the boat and the lines as run thus kept nearly in coincidence with those laid out in the scheme. A study of the three-point problem (art. 153, Chap. IV) will give the considerations that must govern in the selection of objects.

By two theodolite angles.—Two stations on shore are occupied by observers with theodolites, and at certain instants, indicated by a signal from the ship or boat, they observe the angular distance thereof from some known point. The intersection of the direction lines thus given is at the required position. This method is expeditious where the signals are small or not numerous. Its disadvantage is that the plotting can not be kept up as the work proceeds.

By one sextant and one theodolite angle.—An observer ashore occupies a station with a theodolite and cuts in the ship or boat, while one on board takes a sextant angle between two objects, of which one should preferably be the occupied station. It is plotted by laying off the direction line from the theodolite and finding with a three-armed protractor or piece of tracing paper what point of that line subtends the observed angle between the objects. Its advantages and disadvantages are the same as those of the preceding method.

In running lines of soundings offshore, where signals are lost sight of, the best method is to get an accurate departure, before dropping the land, by the best means that offers, keeping careful note of the the dead reckoning, and on running in again, to get a position as soon as possible, note the drift and reconcile the plotting of intermediate soundings accordingly. Where circumstances require, the position may be located by astronomical observations as usually taken at sea.

459. A careful record of soundings must be kept, showing the time of each (so that proper tidal correction may be applied), the depth, the character of bottom, and such data as may be required to locate the position.

460. Tidal Observations.—These should begin as early as practicable and continue throughout the survey, it being most important that they shall, if possible, cover the period of a lunar month. In the chapter on Tides (Chap. XX) the nature of the data to be obtained is explained.

461. Magnetic Observations.—The feature of the earth's magnetism with which the navigator is most concerned is the variation, which is set forth on the chart, and upon the determination of which will depend the correctness of all courses and bearings on shipboard. It is usually obtained by noting the compass direction from the observation spot of the object whose true bearing is known by calculation, and comparing the true and compass bearings; or it may be observed by mounting the ship's compass in a place on shore free from foreign magnetic influence, and finding the compass error as it is found on board. Observations for dip and intensity are also made when the proper instruments are at hand.

462. Running Survey.—Where time and opportunity permit only a superficial examination of a coast line or water area, or where the interests of navigation require no more, recourse is had to a *Running Survey*, in which shore positions are determined and soundings are made while the ship steams along the coast stopping only occasionally to fix her position, and in which the assistance of boat or shore parties may or may not be employed.

In this method the ship starts at one end of the field from a known position, fixed either by astronomical observations or by angles or bearings of terrestrial objects having a determined location. Careful compass bearings or sextant angles are taken from this position to all objects ashore which can be recognized, and a series of direction lines is thus obtained. The ship then steams along the coast, at a convenient distance therefrom, keeping accurate account of her run by compass courses and patent log.

From time to time other series of bearings or angles are taken upon those objects ashore which are to be located, the direction lines plotted from the estimated position of the ship, and the various objects located by the intersections with their other direction lines. During all the time that the ship is under way, soundings are taken at regular intervals and plotted from the dead reckoning. As frequently as circumstances permit, the ship is stopped and her position located by the best available means, and the intervening dead reckoning reconciled for any current that may be found.

If a steam launch can be employed in connection with a running survey, it is usually sent to run a second line inshore of the ship. The boat's position is obtained by bearings of objects ashore which are located by the ship, or by bearings and mast-head angles of the ship, or by such other means as offer. The duty of the boat is to take a series of soundings, and to collect data for shore line and topography.

If circumstances allow the landing of a shore party, its most important duty is to mark the various objects on shore by some sort of signals which will render them unmistakable. Beyond this, it can perform such of the duties assigned to shore parties in a regular survey as opportunity permits.

CHAPTER XVIII.

WINDS.

463. *Wind* is air in approximately horizontal motion. Observations of the wind should include its true direction, and its force or velocity. The direction of the wind is designated by the point of the compass from which it proceeds. The force of the wind is at sea ordinarily expressed in terms of the Beaufort Scale, each degree of this scale corresponding to a certain velocity in miles per hour, as explained in article 67, Chapter II.

464. The Cause of the Wind.—Winds are produced by differences of atmospheric pressure, which are themselves ultimately, and in the main, attributable to differences of temperature.

To understand how the air can be set in motion by these differences of pressure it is necessary to have a clear conception of the nature of the air itself.

The atmosphere which completely envelops the earth may be considered as a fluid sea at the bottom of which we live, and which extends upward to a considerable height, probably 200 miles, constantly diminishing in density as the altitude increases.

The air, or material of which this atmosphere is composed, is a transparent gas, which, like all other gases, is perfectly elastic and highly compressible. Although extremely light, it has a perfectly definite weight, a cubic foot of air at ordinary pressure and temperature weighing 1.22 ounces, or about one seven hundred and seventieth part of the weight of an equal volume of water. In consequence of this weight it exerts a certain pressure upon the surface of the earth, amounting on the average to 15 pounds for each square inch. To accurately measure this pressure, which is constantly undergoing slight changes, we ordinarily employ a mercurial barometer (art. 48, Chap. II), an instrument in which the weight of a column of air of given cross section is balanced against that of a column of mercury having an equal cross section; and instead of saying that the pressure of the atmosphere is a certain number of pounds on each square inch, we say that it is a certain number of inches of mercury, meaning thereby that it is equivalent to the pressure of a column of mercury that many inches in height, and one square inch in cross section.

All gases, air included, are highly sensitive to the action of heat, expanding or increasing in volume as the temperature rises, contracting or diminishing in volume as the temperature falls. Suppose now that the atmosphere over any considerable region of the earth's surface is maintained at a higher temperature than that of its surroundings. The warmed air will expand, and its upper layers will flow off to the surrounding regions, cooling as they go. The atmospheric pressure at sea level throughout the heated areas will thus be diminished, while that over the circumjacent cooler areas will be correspondingly increased. As the result of this difference of pressure, there will be movement of the surface air away from the region of high pressure and towards the region of low, somewhat similar to the flow of water which takes place through the connecting bottom sluice as soon as we attempt to fill one compartment of a divided vessel to a slightly higher level than that found in the other.

A difference of atmospheric pressure at sea level is thus immediately followed by a movement of the surface air, or by winds; and these differences of pressure have their origin in differences of temperature. If the atmosphere were everywhere of uniform temperature it would lie at rest on the earth's surface—sluggish, torpid and oppressive—and there would be no winds. This, however, is fortunately not the case. The temperature of the atmosphere is continually or periodically higher in one region than in another, and the chief variations in the distribution of temperature are systematically repeated year after year, giving rise to like systematic variations in the distribution of pressure.

465. The Normal Distribution of Pressure.—The winds, while thus due primarily to differences of temperature, stand in more direct relation to differences of pressure, and it is from this point of view that they are ordinarily studied.

In order to furnish a comprehensive view of the distribution of atmospheric pressure over the earth's surface, charts have been prepared showing the average reading of the barometer for any given period, whether a month, a season, or a year, and covering as far as possible the entire globe. These are known as isobaric charts, from the fact that all points at which the barometer has the same reading are joined by a continuous line or isobar.

The isobaric chart for the year (fig. 59) shows in each hemisphere a well-defined belt of high pressure (30.20 inches) completely encircling the globe, that in the northern hemisphere having its middle line about in latitude 35° North, that in the southern hemisphere about in latitude 30° South, these constituting the so-called meteorological tropics. From the summit or ridge of each of these belts the pressure falls off alike toward the equator and toward the pole, although much less rapidly in the former direction than in the latter. The equator itself is encircled by a belt of somewhat diminished pressure (29.90 inches), the middle line of which is ordinarily found in northern latitudes. In the northern hemisphere the diminution of pressure on the poleward slope is much less marked and much less regular than in the southern hemisphere, minima (29.70 inches) occurring in the North Atlantic Ocean near Iceland, and in the North Pacific Ocean near the Aleutian Islands, beyond which the pressure increases. In the southern hemisphere no such minima are apparent, the pressure continuing to diminish uninterruptedly as higher and higher latitudes are attained. Along the sixtieth parallel of south latitude the average barometric reading is 29.30 inches.

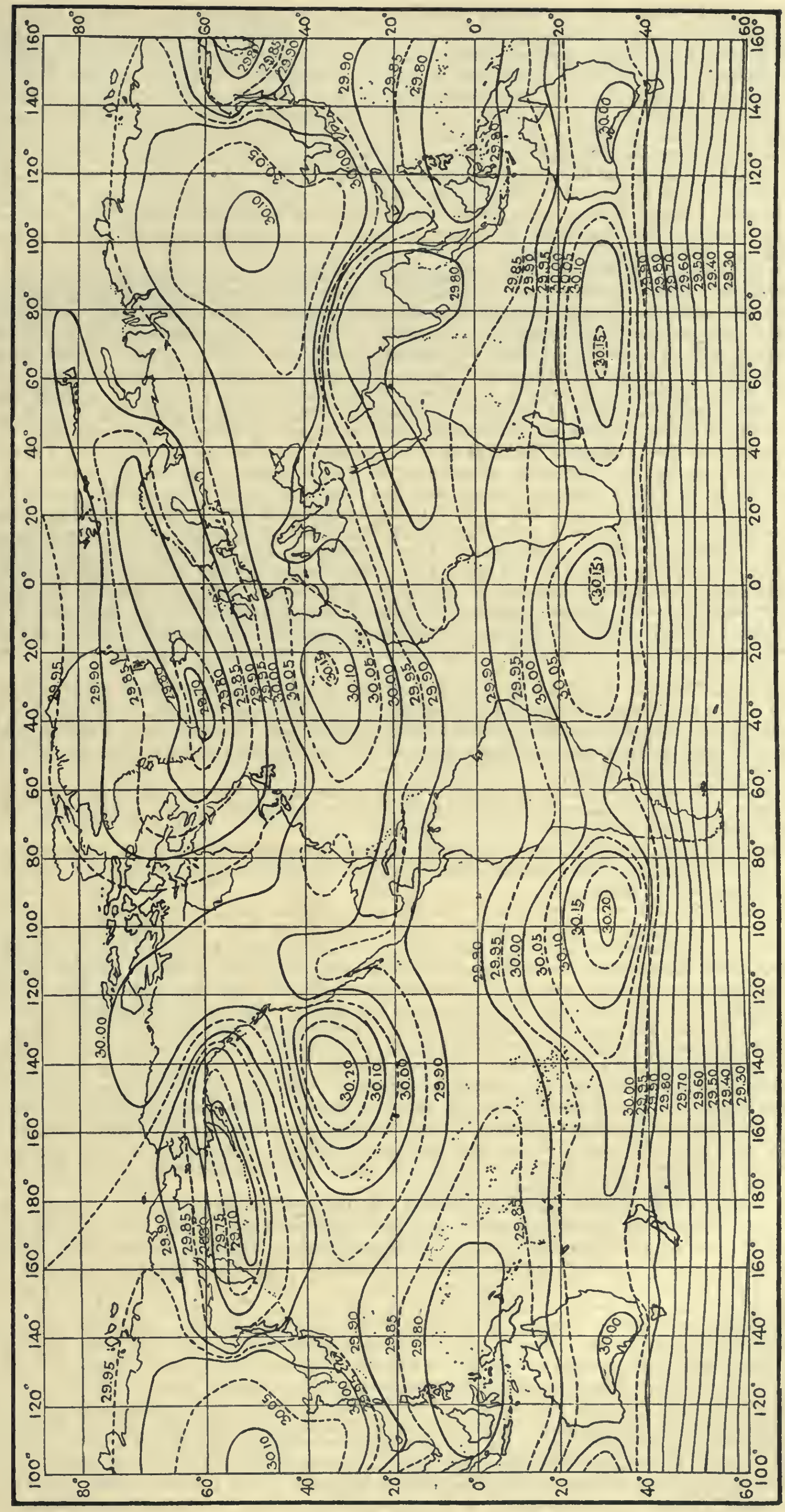


Fig. 59.

466. Seasonal Variations of Pressure.—As might be expected from its close relation to the temperature, the whole system of pressure distribution exhibits a tendency to follow the sun's motion in declination, the barometric equator occupying in July a position slightly to the northward of its position in January. In either hemisphere, moreover, the pressure over the land during the winter season is decidedly above the annual average, during the summer season decidedly below it; the extreme variations occurring in the case of continental Asia, where the mean monthly pressure ranges from 30.50 inches during January to 29.50 inches during July. Over the northern ocean, on the other hand, conditions are reversed, the summer pressures being here somewhat the higher. Thus, in January the Icelandic and the Aleutian minima increase in depth to 29.50 inches, while in July these minima fill up and are well-nigh obliterated, a fact which has much to do with the strength and frequency of the winter gales in high northern latitudes and the absence of these gales during the summer. Over the southern ocean, in keeping with its slight contrast between winter and summer temperatures, similar variations of pressure do not exist.

467. The Prevailing Winds.—As a result of the distribution of pressure just described, there is in either hemisphere a continual motion of the surface air away from the meteorological tropic—on one side towards the equator, on the other side towards the pole, the first constituting in each case the trade winds, the second the prevailing winds of higher latitudes. Upon a stationary earth the direction of this motion would be immediately from the region of high towards the region of low barometer, the moving air steadily following the barometric slope or gradient, increasing in force to a gale where these gradients are steep, decreasing to a light breeze where they are gentle, sinking to a calm where they are absent. The earth, however, is in rapid rotation, and this rotation gives rise to a force which exercises a material influence over all horizontal motions upon its surface, whatever their direction, serving constantly to divert them to the *right* in the northern hemisphere, to the *left* in the southern. The air set in motion by the difference of pressure is thus constantly turned aside from its natural course down the barometric gradient or slope, and the direction of the wind at any point, instead of being identical with that of the gradient at that point, is deflected by a certain amount, crossing the latter at an angle which in practice varies between 45° and 90° (4 to 8 compass points), the wind in the latter case blowing parallel to the isobars. As a consequence of this deflection the northerly winds which one would naturally expect to find on the equatorial slope of the belt of high pressure in the northern hemisphere become northeasterly,—the NE. trade; the southerly winds of the polar slope become southwesterly,—the prevailing westerly winds of northern latitudes. So, too, for the southern hemisphere, the southerly winds of the equatorial slope here becoming southeasterly,—the SE. trades; the northerly winds of the polar slope northwesterly,—the prevailing westerly winds of southern latitudes.

468. The relation here described as existing between the distribution of atmospheric pressure and the direction of the wind is of the greatest importance. It may be briefly stated as follows:

In the northern hemisphere stand with the back to the wind; in this position the region of high barometer lies on your right hand and somewhat behind you; the region of low barometer on your left hand and somewhat in front of you.

In the southern hemisphere stand with the back to the wind; in this position the region of high barometer lies on your left hand and somewhat behind you; the region of low barometer on your right hand and somewhat in front of you.

This relation holds absolutely, not only in the case of the general distribution of pressure and circulation of the atmosphere, but also in the case of the special conditions of high and low pressure which usually accompany severe gales.

469. The Trade Winds.—The *Trade Winds* blow from the tropical belts of high pressure towards the equatorial belt of low pressure—in the northern hemisphere from the northeast, in the southern hemisphere from the southeast. Over the eastern half of each of the great oceans they extend considerably farther from the line and their original direction inclines more towards the pole than in mid-ocean, where the latter is almost easterly. They are ordinarily looked upon as the most constant of winds, but while they may blow for days or even for weeks with slight variation in direction or strength, their uniformity should not be exaggerated. There are times when the trade winds weaken or shift. There are regions where their steady course is deformed, notably among the island groups of the South Pacific, where the trades during January and February are practically nonexistent. They attain their highest development in the South Atlantic and in the South Indian Ocean, and are everywhere fresher during the winter than during the summer season. They are rarely disturbed by cyclonic storms, the occurrence of the latter within the limits of the trade wind region being furthermore confined in point of time to the late summer and autumn months of the respective hemispheres, and in scene of action to the western portion of the several oceans. The South Atlantic Ocean alone, however, enjoys complete immunity from tropical cyclonic storms.

470. The Doldrums.—The equatorial girdle of low pressure occupies a position between the high-pressure belt of the northern and the similar belt of the southern hemisphere. Throughout the extent of this barometric trough the pressure, save for the slight diurnal oscillation, is practically uniform, and decided barometric gradients do not exist. Here, accordingly, the winds sink to stagnation, or rise at most only to the strength of fitful breezes, coming first from one point of the compass, then from another, with cloudy, rainy sky and frequent thunderstorms. The region throughout which these conditions prevail consists of a wedge-shaped area, the base of the wedge resting in the case of the Atlantic Ocean on the coast of Africa, and in the case of the Pacific Ocean on the coast of America, the axis extending westward. The position and extent of the belt vary somewhat with the season. Throughout February and March it is found immediately north of the equator and is of inappreciable width, vessels following the usual sailing routes frequently passing from trade to trade without interruption in both the Atlantic and the Pacific Oceans. In July and August it has migrated to the northward, the axis extending east and west along the parallel of 7° north, and the belt itself covering several degrees of latitude, even at its narrowest point. At this season of the year, also, the southeast trades blow with diminished freshness across the equator and well into the northern hemisphere, being here diverted, however, by the effect of the earth's rotation, into southerly and southwesterly winds, the so-called southwest monsoon of the African and Central American coasts.

471. The Horse Latitudes.—On the outer margin of the trades, corresponding vaguely with the summit of the tropical ridge of high pressure in either hemisphere, is a second region throughout which the barometric gradients are faint and undecided, and the prevailing winds correspondingly light and variable, the so-called *horse latitudes*, or calms of Cancer and of Capricorn. Unlike the doldrums, however, the weather is here clear and fresh, and the periods of stagnation are intermittent rather than continuous, showing none of the persistency which is so characteristic of the equatorial region. The explanation of this difference will become obvious as soon as we come to study the nature of the daily barometric changes of pressure in the respective regions, these in the one case being marked by the uniformity of the torrid zone, in the other sharing to a limited extent in the wide and rapid variations of the temperate.

472. The Prevailing Westerly Winds.—On the exterior or polar side of the tropical maxima the pressure again diminishes, the barometric gradients being now directed towards the pole; and the currents of air set in motion along these gradients, diverted to the right and left of their natural course by the earth's rotation, appear in the northern hemisphere as southwesterly winds, in the southern hemisphere as northwesterly—the prevailing westerly winds of the temperate zone.

Only in the southern hemisphere do these winds exhibit anything approaching the persistency of the trades, their course in the northern hemisphere being subject to frequent local interruption by periods of winds from the eastern semicircle. Thus the tabulated results show that throughout the portion of the North Atlantic included between the parallels 40°–50° North, and the meridians 10°–50° West, the winds from the western semicircle (South—NNW.) comprise about 74 per cent of the whole number of observations, the relative frequency being somewhat higher in winter, somewhat lower in summer. The average force, on the other hand, decreases from force 6 to force 4 Beaufort scale, with the change of season. Over the sea in the southern hemisphere such variations are not apparent; here the westerlies blow through the entire year with a steadiness little less than that of the trades themselves, and with a force which, though fitful, is very much greater, their boisterous nature giving the name of the "Roaring Forties" to the latitudes in which they are most frequently observed.

The explanation of this striking difference in the extra-tropical winds of the two halves of the globe is found in the distribution of atmospheric pressure, and in the variations which this latter undergoes in different parts of the world. In the landless southern hemisphere the atmospheric pressure after crossing the parallel of 30° South diminishes almost uniformly towards the pole, and is rarely disturbed by those large and irregular fluctuations which form so important a factor in the daily weather of the northern hemisphere. Here, accordingly, a system of polar gradients exists quite comparable in stability with the equatorial gradients which give rise to the trades; and the poleward movement of the air in obedience to these gradients, constantly diverted to the left by the effect of the earth's rotation, constitutes the steady westerly winds of the south temperate zone.

473. The Monsoon Winds.—The air over the land is warmer in summer and colder in winter than that over the adjacent oceans. During the former season the continents thus become the seat of areas of relatively low pressure; during the latter of relatively high. Pressure gradients, directed outward during the winter, inward during the summer, are thus established between the land and the sea, which exercise the greatest influence over the winds prevailing in the region adjacent to the coast. Thus, off the Atlantic seaboard of the United States southwesterly winds are most frequent in summer, northwesterly winds in winter; while on the Pacific coast the reverse is true, the wind here changing from northwest to southwest with the advance of the colder season.

The most striking illustration of winds of this class is presented by the *monsoons* (*Mausum*, season) of the China Sea and of the Indian Ocean. In January abnormally low temperatures and high pressure obtain over the Asiatic plateau, high temperatures and low pressure over Australia and the nearby portion of the Indian Ocean. As a result of the baric gradients thus established, the southern and eastern coast of the vast Asiatic continent and the seas adjacent thereto are swept by an outflowing current of air, which, diverted to the right of the gradient by the earth's rotation, appears as a northeast wind, covering the China Sea and the northern Indian Ocean. Upon entering the southern hemisphere, however, the same force which hitherto deflected the moving air to the right of the gradient now serves to deflect it to the left; and here, accordingly, we have the monsoon appearing as a northwest wind, covering the Indian Ocean as far south as 10°, the Arafura Sea, and the northern coast of Australia.

In July these conditions are precisely reversed. Asia is now the seat of high temperature and correspondingly low pressure, Australia of low temperature and high pressure, although the departure from the annual average is by no means so pronounced in the case of the latter as in that of the former. The baric gradients thus lead across the equator and are addressed toward the interior of the greater continent, giving rise to a system of winds whose direction is southeast in the southern hemisphere, southwest in the northern.

The northeast (winter) monsoon blows in the China Sea from October to April, the southwest (summer) monsoon from May to September. The former is marked by all the steadiness of the trades, often attaining the force of a moderate gale; the latter appears as a light breeze, unsteady in direction, and often sinking to a calm. Its prevalence is frequently interrupted by tropical cyclonic storms, locally known as *typhoons*, although the occurrence of these latter may extend well into the season of the winter monsoon.

474. Land and Sea Breezes.—Corresponding with the seasonal contrast of temperature and pressure over land and water, there is likewise a diurnal contrast which exercises a similar though more local effect. In summer particularly, the land over its whole area is warmer than the sea by day, colder than the sea by night, the variations of pressure thus established, although insignificant, sufficing to evoke a system of littoral breezes directed landward during the daytime, seaward during the night, which, in general, do not penetrate to a distance greater than 30 miles on and off shore, and extend but a few hundred feet into the depths of the atmosphere.

The sea breeze begins in the morning hours—from 9 to 11 o'clock—as the land warms. In the late afternoon it dies away. In the evening the land breeze springs up, and blows gently out to sea until

morning. In the tropics this process is repeated day after day with great regularity. In our own latitudes, the land and sea breezes are often masked by winds of cyclonic origin.

475. A single important effect of the seasonal variation of temperature and pressure over the land remains to be described. If there were no land areas to break the even water surface of the globe, the trades and westerlies of the terrestrial circulation would be developed in the fullest simplicity, with linear divisions along latitude circles between the several members—a condition nearly approached in the land-barren southern hemisphere during the entire year, and in the northern hemisphere during the winter season. In the summer season, however, the tropical belt of high pressure is broken where it crosses the warm land, and the air shouldered off from the continents accumulates over the adjacent oceans, particularly in the northern or land hemisphere. This tends to create over each of the oceans a circular or elliptical area of high pressure, from the center of which the baric gradients radiate in all directions, giving rise to an outflowing system of winds, which by the effect of the earth's rotation is converted into an outflowing spiral eddy or *anticyclonic whirl.* The sharp lines of demarcation which would otherwise exist between the several members of the general circulation are thus obliterated, the southwesterly winds of the middle northern latitudes becoming successively northwesterly, northerly, and northeasterly, as we approach the equator and round the area of high pressure by the east; the northeast trade becoming successively southeasterly, southerly, and southwesterly, as we recede from the equator and round this area by the west; similarly for the other hemisphere.

CHAPTER XIX.

CYCLONIC STORMS.

476. Variations of the Atmospheric Pressure.—The distribution of the atmospheric pressure previously described (Chap. XVIII) and the attendant circulation of the winds are those which become evident after the effects of many disturbing causes have been eliminated by the process of averaging, or embracing in the summation observations covering an extended period of time. The distribution of pressure and the system of winds which actually exist at a given instant will in general agree with these in its main features, but may differ from them materially in detail.

Confining our attention for the time being to the subject of atmospheric pressure, it may be said that this, at any given point on the earth's surface, is in a constant state of change, the mercury rarely becoming stationary, and then only for a few hours in succession. The variations which the pressure undergoes may be divided into two classes; viz, periodic, or those which are continuously in operation, repeating themselves within fixed intervals of time, long or short; and non-periodic or accidental, which occur irregularly, and are of varying duration and extent.

477. Periodic Variations.—Of the former class of changes the most important are the seasonal, which have been already to some extent described, and the diurnal. The latter consists of the daily occurrence of two barometric maxima, or points of highest pressure, with two intervening minima. Under ordinary circumstances, with the atmosphere free from disturbances, the barometer each day attains its first minimum about 4 a. m. As the day advances the pressure increases, and a maximum, or point of greatest pressure, is reached about 10 a. m. From this time the pressure diminishes, and a second minimum is reached about 4 p. m., after which the mercury again rises, reaching its second maximum about 10 p. m. The range of this diurnal oscillation is greatest at the equator, where it amounts to ten hundredths (0.10) of an inch. It diminishes with increased latitude, and near the poles it seems to vanish entirely. In middle latitudes it is much more apparent in summer than in winter.

478. Non-periodic Variations.—The equatorial slope of the tropical belt of high pressure which encircles the globe in either hemisphere is characterized by the marked uniformity of its meteorological conditions, the temperature, wind, and weather changes proper to any given season repeating themselves as day succeeds day with almost monotonous regularity. Here the diurnal oscillation of the barometer constitutes the main variation to which the atmospheric pressure is subjected. On the polar slope of these belts conditions the reverse of these obtain, the elements which go to make up the daily weather here passing from phase to phase without regularity, with the result that no two days are precisely alike; and as regards atmospheric pressure, it may be said that in marked contrast with the uniformity of the torrid zone, the barometer in the temperate zone is constantly subjected to non-periodic or accidental fluctuations of such extent that the periodic diurnal variation is scarcely apparent, the mercury at a given station frequently rising or falling several tenths of an inch in twenty-four hours.

479. Progressive Areas of High and Low Pressure.—The explanation of this rapid change of conditions is found in the approach and passage of extensive areas of alternately high and low pressure, which affect alike, although to a different degree, all the barometers coming within their scope. The general direction of motion of these areas is that of the prevailing winds; eastward, therefore, in the latitudes which are under consideration.

Taken in conjunction, these areas of high and low pressure exercise a controlling influence over the weather changes of the temperate zones. As the low area draws near, the sky becomes overclouded, the prevailing westerly wind falls away, and is succeeded by a wind from some easterly direction, faint at first, but increasing as the pressure continues to diminish; the lowest pressure having been reached, the wind again goes to the westward, the glass starts to rise, and the weather clears; all marking the eastward recession of the low area and the approach of the subsequent high.

The first stage in the development of the low is a slight diminution of the atmospheric pressure, amounting in general to not more than one or two hundredths of an inch, throughout an area covering a more or less extensive portion of the earth's surface, either land or water, but far more frequently over the former than over the latter. Shortly after the advent of this initiatory fall the decrease of pressure throughout some small region within the larger area assumes a more decided character, the mercury here standing at a lower level than elsewhere and reading successively higher as we go outward, the region thus becoming, as it were, the center of the whole barometric depression. A system of barometric gradients is by this means established, all directed radially inward, and in obedience to these gradients there is a movement of the surface air towards the center or point of lowest barometer. The air once in motion, however, the effect of the earth's rotation is brought into play precisely as in the case of the larger movements of the atmosphere, with the result that the several currents, instead of following the natural course along these gradients, are deflected from them, in the northern hemisphere to the right hand, in the southern hemisphere to the left, the extent of the deflection being from 4 to 8 compass points.

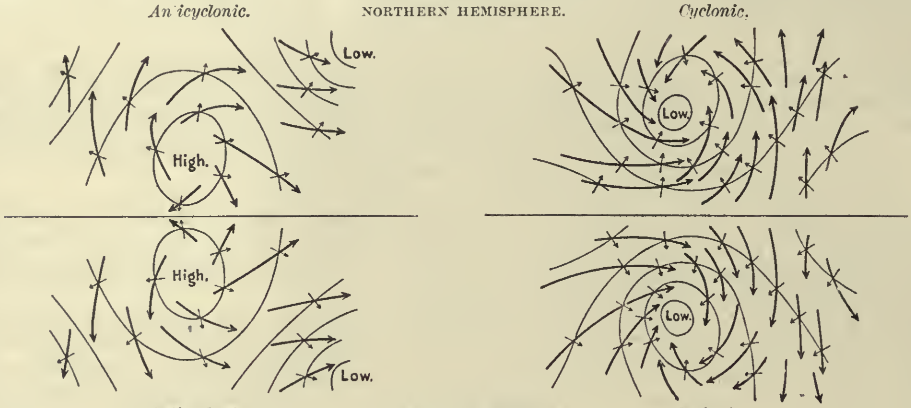
480. Cyclones and Cyclonic Circulations.—A central area of low barometer will thus be surrounded by a system of winds which constantly draw in towards the center but at the same time circulate about it, the whole forming an inflowing spiral; the direction of this circulation being in the southern hemisphere with the motion of the hands of a watch, in the northern hemisphere opposed to this

motion. Where the barometric gradients are steep, these winds are apt to be strong; where they are gentle, the winds are apt to be weak; where they are absent, as is the case at the center or bottom of the depression, calms are apt to prevail.

Around the center of the area of high pressure a similar system of wind will be found, but blowing in a contrary direction. Here the barometric gradients are directed radially outward, with the result that in place of the inflowing, we have an outflowing spiral, the circulatory motion being right handed or with the hands of a watch in the northern hemisphere, left handed or against the hands of a watch in the southern.

All of these features are shown in the accompanying diagrams (fig. 60), which exhibit the general character of cyclonic (around the low) and anticyclonic (around the high) circulations in the northern

Anticyclonic. NORTHERN HEMISPHERE. *Cyclonic.*



Anticyclonic. SOUTHERN HEMISPHERE. *Cyclonic.*

FIG. 60.

The light arrows show the direction of the gradients; the heavy arrows the direction of the winds.

and the southern hemisphere, respectively. The closed curves represent the isobars, or lines along which the barometric pressure is the same; the short arrows show the direction of the gradients, which are everywhere at right angles to the isobars; the long arrows give the direction of the winds, deflected by the earth's rotation to the right of the gradients in the northern hemisphere, to the left in the southern.

481. FEATURES OF CYCLONIC AND ANTICYCLONIC REGIONS.—Certain features of the two areas may here be contrasted. In the anticyclonic, the successive isobars are as a rule far apart, showing weak gradients and consequently light winds; the areas themselves are of relatively great extent, and their rate of progression is slow. During the summer they originate as extensions into higher latitudes of the margins of the tropical belts of high pressure; during the winter, as offshoots of the strong anticyclone which covers the land throughout that season. Their approach and presence is accompanied by polar or westerly winds, temperature below the seasonal average, fair weather, and clear skies. In the cyclonic area the successive isobars are crowded together, showing steep gradients and strong winds; they may appear either as trough-like extensions into the temperate zone of the polar belt of low pressure, in which case the easterly winds proper to their polar side are nonexistent, or (in lower latitudes) as independent areas, sometimes, indeed, as detached portions of the equatorial low-pressure belt, which move eastward and poleward across the temperate zone, and are ultimately merged into the great cyclonic area surrounding the pole. The progress of these independent areas is invariably attended by the strong and steadily shifting winds, foul weather, and other features which make up the ordinary storm at sea. In the trough-like depressions of higher latitudes these features may or may not be observed, their presence depending upon the depths of the barometric trough and the steepness of its slopes. In these, moreover, the cyclonic circulation is never completely developed, the storm winds having rather the character of right line gales, blowing from an equatorial or easterly direction until the axis of the trough is at hand, and as this passes shifting by the west at one bound to a polar direction.

482. CYCLONIC STORMS.—Strong winds are the result of steep barometric gradients. These may occur with cyclonic or with anticyclonic areas, the latter being exemplified in the case of the northers in the Gulf of Mexico and the northwesterly winter gales along the Atlantic coast of the United States, which are almost invariably accompanied by barometers above the average. They are, however, so much more frequent in the case of areas of low pressure and consequent cyclonic circulations, with their attendant foul weather characteristics, that the latter are generally known as cyclonic storms, i. e., storms in which the wind circulation is cyclonic.

Cyclonic storms may with convenience be divided into two classes; viz, tropical, or those which originate near but not on the equator; and extra-tropical, or those which first appear in higher latitudes.

483. TROPICAL CYCLONIC STORMS.—The occurrence of tropical cyclonic storms is confined to the summer and autumn months of the respective hemispheres, and to the western part of the several oceans, the North Atlantic, the North Pacific, the South Pacific, and the Indian Ocean. They are unknown in the South Atlantic Ocean.

The Arabian Sea and the Bay of Bengal are also visited by cyclonic storms, the season of their occurrence extending from May to October.

484. MOTION OF THE STORM CENTER.—In the case of tropical cyclonic storms there is always a tendency for the barometric depression, impelled by the general motion of the atmosphere in the

trade wind region, to follow a path which tends at once westward and away from the equator. This motion continues until the limits of the trades are reached, where the path ordinarily recurves, and the subsequent motion of the depression is eastward and towards the pole, the disturbance at the same time assuming the features of the extra-tropical cyclonic storm.

485. Rate of Progress of the Storm Center.—Within the tropics (in the northern hemisphere) the average velocity of the storm center along the track is about 17 miles per hour; in the latitudes of recurvature this drops to 8 miles per hour, the center at the time frequently becoming stationary; in higher latitudes it again increases, rising to 20 or even to 30 miles per hour.

In the southern hemisphere the average velocity of progress as far as determined is somewhat less than in the northern, but shows about the same relation in different parts of the track.

The general path of the tropical cyclonic storm in either hemisphere and the cyclonic circulation of the wind about the storm center are given in figures 61 and 62; that for the northern hemisphere applying to the West India hurricane; that for the southern hemisphere to the hurricanes of the South Pacific Ocean.

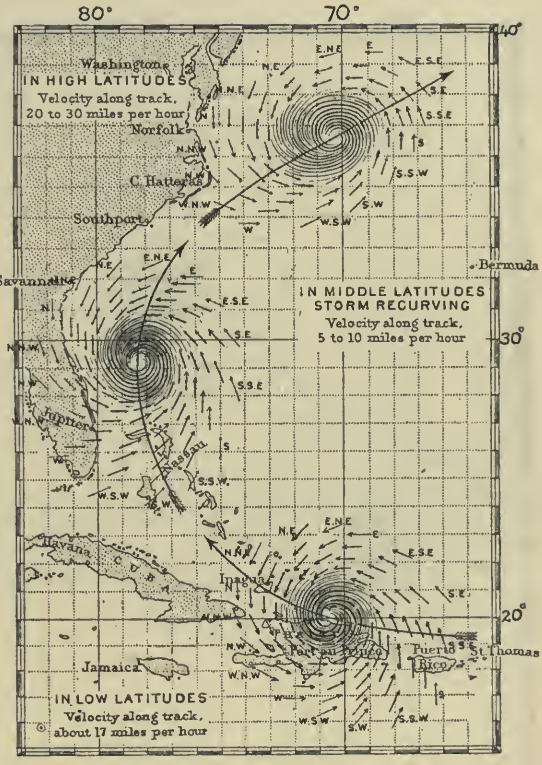


Fig. 61.

486. Character of Tropical Cyclonic Storms.—Within the tropics the storm area is small, the region covered by violent winds extending in general not more than 150 miles from the center. The barometric gradients are, however, exceedingly steep, instances having been recorded in which the difference of pressure for this distance amounted to 2 inches. In the typhoons of the North Pacific Ocean gradients of one inch in 60 miles are not infrequent. The successive isobars are almost circular. As a consequence of this distribution of pressure the winds on the slopes of the depression are frequently of great violence, and in the matter of direction they are more symmetrically disposed about the center than is the case with the larger and less regularly shaped depressions of higher latitudes. In these low latitudes the average values of the deflection of the wind from the barometric gradient is in the neighborhood of six compass points,—to the right in the northern hemisphere, to the left in the southern.

487. To Fix the Bearing of the Storm Center from the Vessel.—On this assumption, the following rules will enable an observer to fix the bearing of the storm center from his vessel:—

In the northern hemisphere, stand with the back to the wind; the storm center will bear six points to the observer's left.

In the southern hemisphere, stand with the back to the wind; the storm center will bear six points to the observer's right.

On the basis of these rules the tables hereafter given (art. 492) show the bearing of the center corresponding to a wind of any direction.

488. To Fix the Distance of the Storm Center from the Vessel.—The following table, taken from Piddington's "Sailor's Horn Book," may prove of some assistance in estimating the distance of the storm center from the vessel:

Average fall of the barometer per hour.	*Distance from the storm center.*
From 0.02 to 0.06 in.	From 250 to 150 miles.
From 0.06 to 0.08 in.	From 150 to 100 miles.
From 0.08 to 0.12 in.	From 100 to 80 miles.
From 0.12 to 0.15 in.	From 80 to 50 miles.

The table assumes that the vessel is hove-to in front of the storm, and that the latter is advancing directly toward it.

489. To Avoid the Center of the Storm.—In the immediate neighborhood of the center itself the winds attain full hurricane force, the sea is exceedingly turbulent, and there is danger of being struck aback. Every effort should therefore be made to avoid this region, either by running or by heaving-to; and if recourse is had to the latter maneuver, much depends upon the selection of the proper tack; this being in every case the tack which will cause the wind to draw aft with each successive shift.

A vessel hove-to in advance of a tropical cyclonic storm will experience a long heavy swell, a falling barometer with torrents of rain, and winds of steadily increasing force. The shifts of wind will depend upon the position of the vessel with respect to the path followed by the storm center. Immediately upon the path, the wind will hold steady in direction until the passage of the central calm, the "eye of the storm," after which the gale will renew itself, but from a direction opposite to that which it previ-

ously had. To the right of the path, or in the right-hand semicircle of the storm (the observer being supposed to face along the track), the wind, as the center advances and passes the vessel, will constantly shift to the right, the rate at which the successive shifts follow each other increasing with the proximity to the center; in this semicircle, then, in order that the wind shall draw aft with each shift, the vessel must be hove-to on the starboard tack; similarly, in the left-hand semicircle, the wind will constantly shift to the left, and here the vessel must be hove-to on the port tack.

These rules hold alike for both hemispheres and for cyclonic storms in all latitudes.

The above shifts of the wind are based upon the supposition that the vessel is lying-to. A vessel in rapid westerly motion may, in low latitudes, readily overtake the storm center, in which case the observed shifts will be just the reverse of those here described.

490. Dangerous and Navigable Semicircles.—Prior to recurving, the winds in that semicircle of the storm which is more remote from the equator (the right-hand semicircle in the northern hemisphere, the left-hand semicircle in the southern) are liable to be more severe than those of the opposite semicircle. A vessel hove-to in the semicircle adjacent to the equator has also the advantage of immunity from becoming involved in the actual center itself, inasmuch as there is a distinct tendency on the part of the latter to move away from the equator. For these reasons the more remote semicircle has been called the *dangerous;* the less remote, the *navigable.*

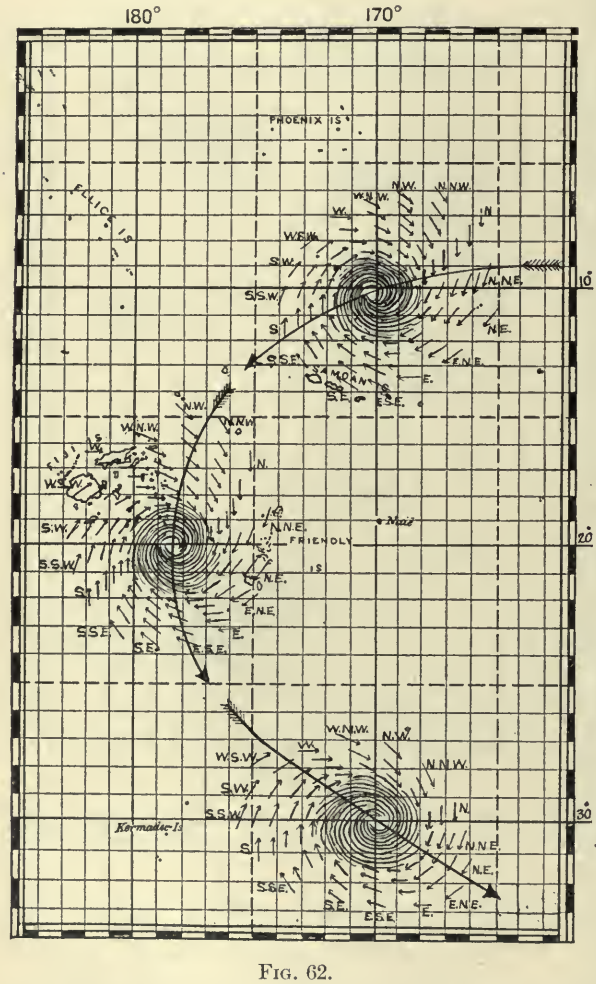


Fig. 62.

491. Maneuvering.—A vessel suspecting the dangerous proximity of a tropical cyclonic storm should lie-to for a time on the starboard tack to locate the center by observing shifts of the wind and the behavior of the barometer. If the former holds steady and increases in force, while the latter falls rapidly, say at a greater rate than 0.03 of an inch per hour, the vessel is probably on the track of the storm and in advance of the center. In this position the proper step (providing, of course, that sea room permits) is to run, keeping the wind, in the northern hemisphere, at all times well on the starboard quarter; in the southern hemisphere, well on the port; and thus constantly increasing the distance to the storm center. The same rule holds good if the observation places the vessel at but a scant distance within the forward quadrant of the dangerous semicircle. Here, too, the natural course will be to seek the navigable semicircle of the storm, even though such a course involves crossing the track in advance of the center, always exercising due caution to keep the wind from drawing too far aft.

The critical case is that of a vessel which finds herself in the forward quadrant of the dangerous semicircle and at a considerable distance from the track, for here the shifts of the wind are sluggish and the indications of the barometer are undecided, both causes conspiring to render the bearing of the center doubtful. If, upon heaving-to, the barometer becomes stationary, the position should be maintained until indications of a rise are apparent, upon which the course may be resumed with safety and held as long as the rise continues. If, however, the barometer falls, a steamer should make a run to the NNE. or NE. (southern hemisphere, SSE. or SE.), keeping the wind and sea a little on the port (southern hemisphere, starboard) bow, and using such speed as will at least keep the mercury stationary. Such a step will in general be attended with the assurance that the present weather conditions will in any case grow no worse. For a sailing vessel, unable to stand closer to the wind than six points, the last maneuver will be impossible, and driven to leeward by wind, sea, and current, she may be compelled to cross the track immediately in advance of the center, or may even become involved in the center itself. In this extremity the path of the storm center during the past twenty-four hours should be laid down on a diagram as accurately as the observations permit, and the line prolonged for some distance beyond the present position of the center. Having assumed an average rate of progress for the center, its probable position on the line should be frequently and carefully plotted. and the handling of the vessel should be in accordance with the diagram.

492. Summary of Rules.—The following summary comprises the rules for maneuvering in the *Northern Hemisphere,* so far as they may be made general:—

In the Right Semicircle: Haul by the wind on the starboard tack and carry sail as long as possible; if obliged to heave-to, do so on starboard tack.

In the Left Semicircle: Bring the wind on the starboard quarter, note course and keep it; if obliged to heave-to, do so on port tack.

In Front of Center: Bring wind two points on starboard quarter, note course and keep it; if obliged to heave-to, do so on port tack.

In Rear of Center: Run out with wind on starboard quarter; if obliged to heave-to, do so on starboard tack.

The application of these rules for the various directions of the wind is shown in the following table:—

Storm Table, Northern Hemisphere.

<table>
<tr><th>Direction of wind.</th><th>Direction of center.</th><th>If wind shifts towards the right.</th><th colspan="2">If wind shifts towards the left.</th><th colspan="2">If wind steady with falling barometer.</th><th colspan="2">If wind steady with rising barometer.</th></tr>
<tr><td>North.</td><td>ESE.</td><td rowspan="16">Haul by wind on starboard tack and carry sail as long as possible; if obliged to heave-to, do so on starboard tack.</td><td>Run SSW.</td><td rowspan="16">Hold course [a] as long as possible; if obliged to heave-to, do so on port tack.</td><td>Run SSW.</td><td rowspan="16">Hold course as long as possible; if obliged to heave-to, do so on port tack.</td><td>Run SSW.</td><td rowspan="16">Hold course [a] as long as possible; if obliged to heave-to, do so on starboard tack.</td></tr>
<tr><td>NNE.</td><td>SE.</td><td>Run SW.</td><td>Run SW.</td><td>Run SW.</td></tr>
<tr><td>NE.</td><td>SSE.</td><td>Run WSW.</td><td>Run WSW.</td><td>Run WSW.</td></tr>
<tr><td>ENE.</td><td>South.</td><td>Run West.</td><td>Run West.</td><td>Run West.</td></tr>
<tr><td>East.</td><td>SSW.</td><td>Run WNW.</td><td>Run WNW.</td><td>Run WNW.</td></tr>
<tr><td>ESE.</td><td>SW.</td><td>Run NW.</td><td>Run NW.</td><td>Run NW.</td></tr>
<tr><td>SE.</td><td>WSW.</td><td>Run NNW.</td><td>Run NNW.</td><td>Run NNW.</td></tr>
<tr><td>SSE.</td><td>West.</td><td>Run North.</td><td>Run North.</td><td>Run North.</td></tr>
<tr><td>South.</td><td>WNW.</td><td>Run NNE.</td><td>Run NNE.</td><td>Run NNE.</td></tr>
<tr><td>SSW.</td><td>NW.</td><td>Run NE.</td><td>Run NE.</td><td>Run NE.</td></tr>
<tr><td>SW.</td><td>NNW.</td><td>Run ENE.</td><td>Run ENE.</td><td>Run ENE.</td></tr>
<tr><td>WSW.</td><td>North.</td><td>Run East.</td><td>Run East.</td><td>Run East.</td></tr>
<tr><td>West.</td><td>NNE.</td><td>Run ESE.</td><td>Run ESE.</td><td>Run ESE.</td></tr>
<tr><td>WNW.</td><td>NE.</td><td>Run SE.</td><td>Run SE.</td><td>Run SE.</td></tr>
<tr><td>NW.</td><td>ENE.</td><td>Run SSE.</td><td>Run SSE.</td><td>Run SSE.</td></tr>
<tr><td>NNW.</td><td>East.</td><td>Run South.</td><td>Run South.</td><td>Run South.</td></tr>
</table>

[a] Courses given are for wind two points on starboard quarter, but it is preferable to take wind broad on quarter if possible.

Similarly, the following rules and table apply for the *Southern Hemisphere:*—

In the Right Semicircle: Bring the wind on the port quarter, note course and keep it; if obliged to heave-to, do so on starboard tack.

In the Left Semicircle: Haul by the wind on the port tack and carry sail as long as possible; if obliged to heave-to, do so on port tack.

In Front of Center: Bring wind two points on port quarter, note course and keep it; if obliged to heave-to, do so on starboard tack.

In Rear of Center: Run out with wind on port quarter; if obliged to heave-to, do so on port tack.

Storm Table, Southern Hemisphere.

<table>
<tr><th>Direction of wind.</th><th>Direction of center.</th><th colspan="2">If wind shifts towards the right.</th><th>If wind shifts towards the left.</th><th colspan="2">If wind steady with falling barometer.</th><th colspan="2">If wind steady with rising barometer.</th></tr>
<tr><td>North.</td><td>WSW.</td><td>Run SSE.</td><td rowspan="16">Hold course [a] as long as possible; if obliged to heave-to, do so on starboard tack.</td><td rowspan="16">Haul by wind on port tack and carry sail as long as possible; if obliged to heave-to, do so on port tack.</td><td>Run SSE.</td><td rowspan="16">Hold course as long as possible; if obliged to heave-to, do so on starboard tack.</td><td>Run SSE.</td><td rowspan="16">Hold course [a] as long as possible; if obliged to heave-to, do so on port tack.</td></tr>
<tr><td>NNE.</td><td>West.</td><td>Run South.</td><td>Run South.</td><td>Run South.</td></tr>
<tr><td>NE.</td><td>WNW.</td><td>Run SSW.</td><td>Run SSW.</td><td>Run SSW.</td></tr>
<tr><td>ENE.</td><td>NW.</td><td>Run SW.</td><td>Run SW.</td><td>Run SW.</td></tr>
<tr><td>East.</td><td>NNW.</td><td>Run WSW.</td><td>Run WSW.</td><td>Run WSW.</td></tr>
<tr><td>ESE.</td><td>North.</td><td>Run West.</td><td>Run West.</td><td>Run West.</td></tr>
<tr><td>SE.</td><td>NNE.</td><td>Run WNW.</td><td>Run WNW.</td><td>Run WNW.</td></tr>
<tr><td>SSE.</td><td>NE.</td><td>Run NW.</td><td>Run NW.</td><td>Run NW.</td></tr>
<tr><td>South.</td><td>ENE.</td><td>Run NNW.</td><td>Run NNW.</td><td>Run NNW.</td></tr>
<tr><td>SSW.</td><td>East.</td><td>Run North.</td><td>Run North.</td><td>Run North.</td></tr>
<tr><td>SW.</td><td>ESE.</td><td>Run NNE.</td><td>Run NNE.</td><td>Run NNE.</td></tr>
<tr><td>WSW.</td><td>SE.</td><td>Run NE.</td><td>Run NE.</td><td>Run NE.</td></tr>
<tr><td>West.</td><td>SSE.</td><td>Run ENE.</td><td>Run ENE.</td><td>Run ENE.</td></tr>
<tr><td>WNW.</td><td>South.</td><td>Run East.</td><td>Run East.</td><td>Run East.</td></tr>
<tr><td>NW.</td><td>SSW.</td><td>Run ESE.</td><td>Run ESE.</td><td>Run ESE.</td></tr>
<tr><td>NNW.</td><td>SW.</td><td>Run SE.</td><td>Run SE.</td><td>Run SE.</td></tr>
</table>

[a] Courses given are for wind two points on port quarter, but it is preferable to take wind broad on quarter, if possible.

493. Extra-Tropical Cyclonic Storms.—On turning to the cyclones of temperate latitudes, we find many features in which they resemble those of the torrid zone, but certain other features in which they differ. Their fundamental resemblance to tropical cyclones is seen in their incurving winds, forming an inflowing left-handed spiral about the center of low pressure in the northern hemisphere, an inflowing right-handed spiral in the southern. The intensity of these winds varies with the depth of the barometric depression. The depression itself, however, in place of covering a few miles, as is the case in the tropics, will frequently have a diameter of several hundred or even a thousand miles, and for some distance around the center the gradients will have a tolerably strong value. For this reason there is less concentration of violence close to the center, and the calm and clear central space, or "eye," is seldom sharply developed, although it is not uncommon to discover a gradual weakening or failing of the winds, and sometimes even an imperfect breaking away of the clouds as the central area passes over the observer. The form of tropical cyclones as defined by their isobaric lines is nearly circular. Extra-tropical cyclones are as a rule less symmetrical, and their isobars are often elongated into an oval form, the longer axis of the oval trending (in the northern hemisphere) between north and east—about, therefore, in the direction of progression. The steepest gradients, and consequently the strongest winds, are apt to be found on the equatorial and westerly sides of the depression.

Extra-tropical cyclones generally follow an easterly course, inclining somewhat towards the pole; but they occasionally turn to one side or the other, become stationary, or even move backward. The velocity of progression varies from 15 to 40 miles an hour. If they exist as independent barometric depressions, with strong upward gradients on all sides of the center, the cyclonic circulation will be complete, the wind shifting with the sun for an observer situated in the equatorial semicircle of the storm, against the sun for an observer situated in the polar semicircle.

494. Storms Along the Transatlantic Steamship Routes.—The storms which are so frequently met during the winter season along the steamship routes between America and Europe are not, as a rule, due to central barometric depressions, but to depressions having a trough or V shape, which extend southerly from the extensive permanent area of low pressure having its center in the vicinity of Iceland. They are not attended by complete cyclonic circulations, inasmuch as the polar gradients which would otherwise give rise to easterly winds on this polar side are lacking. Their approach is heralded by a gradual hauling of the wind to southward, which is later followed (at the time of passage of the central line of the trough) by a change to NW., accompanied by heavy rain squalls and a rapid increase in force. The general distribution of pressure and the surrounding winds are shown in figure 63.

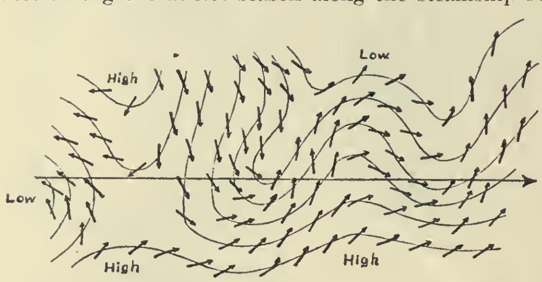


Fig. 63.

The changes in wind and pressure ensue much more rapidly in the case of a westward-bound vessel than in that of one eastward bound, the rate at which the observer and the depression approach each other being in the former case the sum of his own westward velocity and the eastward velocity of the trough, in the latter case, the difference of these velocities.

CHAPTER XX.

TIDES.

495. Definitions.—Tidal phenomena present themselves to the observer under two aspects—as alternate elevations and depressions of the sea, and as recurrent inflows and outflows of streams. The word *tide*, in common and general usage, is made to refer without distinction to both the vertical and horizontal motions of the sea, and confusion has sometimes arisen from this double application of the term; in its strict sense, this word may be used only with reference to the changes of elevation, while the recurrent streams are properly distinguished as *tidal currents*.

The tide rises until it reaches a maximum height called *high water* or *high tide*, and then falls to a minimum level called *low water* or *low tide;* that period at high or low water marking the transition between the tides, during which no vertical change can be detected, is called *stand.*

Of the tidal currents, that which arises from a movement of the water in a direction, generally speaking, from the sea toward the land, is called *flood*, and that arising from an opposite movement, *ebb;* the intermediate period between the currents, during which there is no horizontal motion, is distinguished as *slack*. *Set* and *drift* are terms applicable to the tidal currents, the first referring to the direction and the second to the velocity.

Care should be taken to avoid confusing the terms relating to tides with those which relate to tidal currents.

496. Cause.—The cause of the tides is the unequal attraction of the sun and moon upon different parts of the earth. These bodies attract the parts of the earth's surface which are nearer to them with greater force than they do its center, and attract its center more than they do its opposite surface; to restore equilibrium the waters take a spheroidal figure, whose longer axis lies in the direction of the attracting body. The mean force of the moon in raising the tides is two and a half times as great as that of the sun, for though the mass of the sun is vastly greater than the mass of the moon, the sun's distance is so great that it attracts the different parts of the earth with nearly equal force. Theory is not sufficiently advanced to render possible a prediction of tides or tidal changes from a mere knowledge of the positions of the sun and moon, but by theory, supplemented by observation of actual tidal conditions during a certain period of time, very accurate predictions may be arrived at.

497. Establishment.—High and low water occur, on the average of the twenty-eight days comprising a lunar month, at about the same intervals after the transit of the moon over the meridian. These nearly constant intervals, expressed in hours and minutes, are known respectively as the *high water lunitidal interval* and *low water lunitidal interval.*

The interval between the moon's meridian passage at any place and the time of the next succeeding high water, as observed on the days when the moon is at full or change, is called the *vulgar* (or *common*) *establishment* of that place, or, sometimes, simply the *establishment.* This interval is frequently spoken of as the *time of high water on full and change days* (abbreviated "H. W. F. & C."); for since, on such days, the moon's two transits (upper and lower) over the meridian occur about noon and midnight, the vulgar establishment then corresponds closely with the local times of high water. When more extended observations have been made, the average of all the high water lunitidal intervals for at least a lunar month is taken to obtain what is termed, in distinction to the vulgar establishment, the *corrected establishment* of the port, or *mean high water lunitidal interval.* In defining the tidal characteristics of a place some authorities give the corrected establishment, and others the vulgar establishment, or "high water, full and change;" calculations based upon the former will more accurately represent average conditions, though the two intervals seldom differ by a large amount.

Having determined the time of high water by applying the establishment to the time of moon's transit, the navigator may obtain the time of low water with a fair degree of approximation by adding or subtracting $6^h\ 13^m$ (one-fourth of a mean lunar day); but a closer result will be given by applying to the time of transit the *mean low water lunitidal interval*, which occupies the same relation to the time of low water as the mean high water lunitidal interval, or corrected establishment, does to the time of high water.

498. Range.—The *range* of the tide is the difference in height between low water and high water. This term is often applied to the difference existing under average conditions, and may in such a case be designated as the *mean range* or *mean rise and fall* to distinguish it from the *spring range* or *neap range*, which are the ranges at spring and neap tides, respectively.

499. Spring and Neap Tides.—At the times of new and full moon the relative positions of sun and moon are such that the high water produced by one of those bodies occurs at the same time as that produced by the other, and so also with the low waters; the tides then occurring, called *spring tides*, have a greater range than any others of the lunar month, and at such times the highest high tides as well as the lowest low tides are experienced, the tidal range being then at its maximum. At the first and third quarters of the moon the positions are such that the high tide due to one body occurs at the time of the low tide due to the other, so that the two actions are opposed; this causes the *neap tides*, which are those of minimum range, the high waters being lower and the low waters higher than at other periods of the month.

Since the horizontal motion of the water depends directly upon the rise and fall of the tides, it follows that the currents will be greatest at springs and least at neaps.

The effect of the moon's being at full or change is not felt at once in all parts of the world, and the greatest range of tides does not generally occur until one or two days thereafter; thus, on the Atlantic coast of North America, the highest tides are experienced one day, and on the Atlantic coast of Europe, two days afterward, though on the Pacific coast of North America they occur nearly at full and change.

500. The nearer the moon is to the earth the stronger is its attraction, and as it is nearest in perigee, the tides will be larger then on that account, and consequently less in apogee. For a like reason, the tides will be increased by the sun's action when the earth is near its perihelion, about the 1st of January, and decreased when near its aphelion, about the 1st of July.

501. The height of the tides at any place may undergo modification on account of strong prevailing winds or abnormal barometric conditions, a wind blowing off the shore or a high barometer tending to reduce the tides, and the reverse. The effect of atmospheric pressure is to create a difference of about 2 inches in the height of tide for every tenth of an inch of difference in the barometer.

502. PRIMING AND LAGGING.—The *tidal day* is the variable interval, averaging $24^h 50^m$, between two alternate high or low waters. The amount by which corresponding tides grow later day by day—that is, the amount by which the tidal day exceeds 24^h—is called the *daily retardation.* When the sun's tidal effect is such as to shorten the lunitidal intervals, thus reducing the length of the tidal day and causing the tides to occur earlier than usual, there is said to be a *priming* of the tide; when, from similar causes, the interval is lengthened, there is said to be a *lagging.*

503. TYPES OF TIDES.—The observed tide is not a simple wave; it is a compound of several elementary undulations, rising and falling from the same common plane, of which two can be distinguished and separated by a simple grouping of the data. These two waves are known as the *semi-diurnal* and the *diurnal* tides, because the first, if alone, would give two high and two low waters in a day, while the second would give but one high and one low water in an equivalent period of time. In nearly all ports these two tides coexist, but the proportion between them varies remarkably for different seas. The effect of the combination of these two types of tide is to produce a *diurnal inequality*, both in the height of two consecutive high or low waters, and in the intervals of time between their occurrence. The height of the diurnal wave may be regarded as reaching a maximum fortnightly, soon after the moon attains its extreme declination and is therefore near one of the tropics. The tides that then occur are denominated *tropic tides.*

In undertaking to investigate the tides of a port it is important to ascertain as early as possible the form of the tide; that is, whether it resembles the semi-diurnal, the diurnal, or the mixed type; because not only may this information be of scientific value, but the knowledge thus gained at the outset will enable the observer to fix upon the best method of keeping his record.

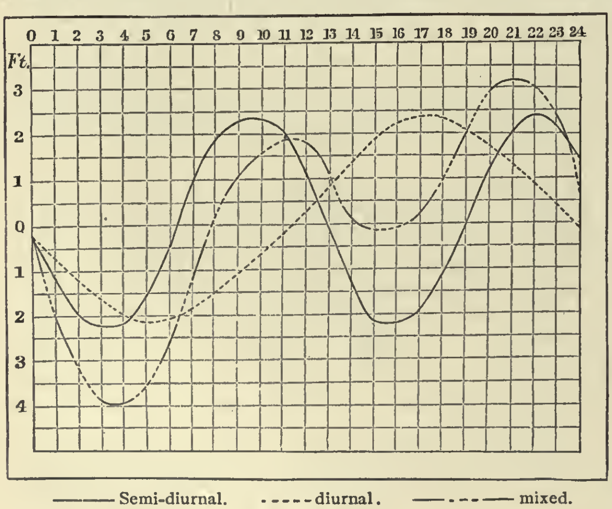


FIG. 64.

504. The type forms referred to are illustrated in the diagram in figure 64, where the waves are plotted in curves, using the times as abscissæ and the heights as ordinates. In this diagram, the curve traced in the full line is a tide-wave of the semi-diurnal type; that traced by the dotted line one of the diurnal; while the broken line is one of the mixed type, in this case the compound of the two others.

In order to determine the type to which the tide of any port belongs, it is usually only necessary to make hourly observations for a day or two at the date of the moon's maximum declination, and to repeat the series about a week later, when the moon crosses the equator. The reported irregularities of the rise and fall at any place should not deter persons from careful investigation. When analyzed, even the most complicated of tides are found to follow some general law.

505. TIDAL CURRENTS.—It should be clearly borne in mind by the navigator that the periods of flood and ebb currents do not necessarily coincide with those of rising and falling tides, and that, paradoxical though it may seem at first thought, the inward set of the surface current does not always cease when the water has attained its maximum height, nor the outward set when a minimum height has been reached. Under some circumstances it may occur that stand and slack will be simultaneous, while other conditions may produce a maximum current at stand, with a maximum rate of rise or fall at slack water.

The varying effects which will be produced according to local conditions may be considered by the comparison of two tidal basins, to one of which the tide-wave has access from the sea by a channel of ample capacity, while the other has an entrance that is narrow and constricted. In the first case, the process of filling or emptying the basin keeps pace with the change of level in the sea and is practically completed as soon as the height without becomes stationary; in this case slack and stand occur nearly at the same time, as do flood and rise and ebb and fall. In the second case, the limited capacity of the entrance will not permit the basin to fill or empty as rapidly as the tide changes its level without;

hence there is still a difference of level to produce a current when the vertical motion in either direction has ceased on the outside, and for a considerable time after motion in the reverse direction has been in progress; under extreme conditions it may even occur that a common level will not be established until mid-tide, and therefore the surface current at some places will ebb until three hours after low water and flow until three hours after high water.

Localities that partake of the nature of the first case are those upon open coasts and wide-mouthed bights. Examples of the latter class will be found in narrow bays and long channels.

TIMES OF HIGH AND LOW WATER.

506. Tide Tables.—The most expeditious, as well as most exact, method of ascertaining the times of high and low water and other features of the tides will be by reference to a *Tide Table,* and every navigator is recommended to provide himself with such a publication. The United States Coast and Geodetic Survey publishes annually, in advance, tables giving, for every day in the year, the predicted time and height of the tides at certain principal ports of the world, and from these, by a simple reduction, the times and heights at a multitude of other ports may readily be obtained; data for ascertaining the tidal currents in certain important regions are also provided. General tide tables are also published by the governments of other maritime nations, and special tables are to be had for many particular localities.

507. Where no tide tables are available, the method of calculation by applying the lunitidal interval to the time of the moon's meridian passage must be resorted to.

To do this, find first the time of the moon's meridian passage, upper or lower, as may be required. The Greenwich mean time of upper transit at Greenwich is given in the Nautical Almanac (page IV of the month); the corresponding time of lower transit is most easily found by taking the mean of the two adjacent upper transits; to the Greenwich time of Greenwich transit apply the correction for longitude given in Table 11 (using the daily variation of the moon's meridian passage shown in the Almanac), adding in west and subtracting in east longitude; the result is the local mean time of local transit. Add to this the high-water or low-water lunitidal interval of the port from Appendix IV, according as the time of high or low water may be required. The result is the time sought.

The astronomical date must be strictly adhered to, and in so doing it may be found necessary to employ the time of a lower transit, or the transit of a preceding day, to find the time of the tide in question.

Appendix IV contains, besides the geographical positions of all the more important positions in the world, a series of tidal data relating to many of those places. In such data are comprised the mean lunitidal intervals for high and low water; also, for places where the semi-diurnal type of tide prevails, the tidal range at spring and at neap tides, and for those where the tide is of the diurnal type, the tropic range. An alphabetical index is appended to this table.

The corrected establishment taken from the charts may be substituted for the high-water lunitidal interval of the table; or, with only slight variation in the results, the vulgar establishment (H. W. F. & C.) may be employed.

Example: Find the times of the high and low waters at the New York navy yard, occurring next after noon on April 22, 1879.

G. M. T. of Gr. transit,		$22^d\ 0^h\ 32^m.2$
Corr. for +74° Long. (Tab. 11),	+	10
L. M. T. of local transit,		22 0 42

Transit,	$22^d\ 0^h\ 42^m$
H. W. Lun. Int. (App. IV),	8 44
L. M. T., H. W.,	22 9 26 / April 22, 9.26 p. m.

Transit,	$22^d\ 0^h\ 42^m$
L. W. Lun. Int. (App. IV),	2 49
L. M. T., L. W.,	22 3 31 / April 22, 3.31 p. m.

Example: Find the time of high water at the Presidio, San Francisco, Cal., on the afternoon of May 7, 1879.

G. M. T. of Gr. transit,		$6^d\ 12^h\ 36^m.6$
Corr. for +122° Long. (Tab. 11),	+	22
L. M. T. of local transit,		6 12 59
H. W. Lun. Int. (App. IV),	+	11 43
L. M. T., H. W.,		7 0 42 / May 7, 12.42 p. m.

Example: Find the time of low water at Singapore on the night of May 28, 1879.

G. M. T. of Gr. transit,		$28^d\ 5^h\ 55^m.3$
Corr. for −104° Long. (Tab. 11),	−	13
L. M. T. of local transit,		28 5 42
L. W. Lun. Int. (App. IV),	+	4 02
L. M. T., L. W.,		28 9 44 / May 28, 9.44 p. m.

EXAMPLE: Find the time of morning high water and afternoon low water at Gibraltar on June 26, 1879.

G. M. T. of Gr. upper transit,	$25^d\ 4^h\ 40^m.1$
G. M. T. of Gr. upper transit,	26 5 27 .0
	2)51 10 07 .1
G. M. T. of Gr. lower transit,	25 17 04
Corr. for + 5° Long. (Tab. 11), +	01
L. M. T. of local lower trans.,	25 17 05

Transit,	$25^d\ 17^h\ 05^m$	Transit,	$25^d\ 17^h\ 05^m$
H. W. Lun. Int. (App. IV),	1 35	L. W. Lun. Int. (App. IV),	7 55
L. M. T., H. W.,	25 18 40 / June 26, 6.40 a. m.	L. M. T., L. W.,	26 1 00 / June 26, 1 p. m.

TIDAL OBSERVATIONS.

508. Since navigators will frequently have opportunity to observe tidal conditions, either in connection with a hydrographic survey or otherwise, at places where existing knowledge of the tides is incomplete, an understanding of the methods employed in tidal observations may be important.

509. TIDES.—For the proper study of tides, frequent and continuous observations are necessary; it will not suffice to observe the heights of the high and low waters only, even if they present themselves as distinct phases, but the whole tidal curve for each day should be developed by recording the height of water at intervals, which, preferably, should not exceed thirty minutes. Observations, to be complete, must cover a whole lunar month; or, if it be impracticable to observe the tides at night, the day tides of two lunar months may be substituted.

510. When made for the purposes of a hydrographic survey the tidal observations are used to correct the soundings, and care must be taken to make sure that the gauge is placed in a situation visited by the same form of tide as that which occurs at the place where soundings are being made. It will not answer, for instance, to correct the soundings upon an inlet-bar by tidal observations made within the lagoon with which this inlet communicates, because the range of the tide within the lagoon is less than upon the outside coast. A partial obstruction, like a bridge, or a natural contraction of the channel section, while it may not reduce the total range of the tide or materially affect the time of high or low tides, will alter the relative heights above and below at intermediate stages, so that the hydrographer must be careful to see that no such obstruction intervenes between his field of work and the gauge.

511. TIDAL CURRENTS.—Observations for tidal currents should be made with the same regularity as for tides; the intervals need not ordinarily be more frequent than once in every half hour. They should always be made at the same point or points, which should be far enough from shore to be representative of the conditions prevailing in the navigable waters. The ordinary log may be employed for measuring the current, but it is better to replace the chip by a pole weighted to float upright at a depth of about fifteen feet; the line should be a very light one, and buoyed at intervals by cork floats to keep it from sinking; the set of the current should be noted by a compass bearing of the direction of the pole at the end of the observation.

512. RECORD.—The record of observations should be kept clearly and in complete form. It should include a description of the locality of observation, the nature of gauge and of instruments used for measuring currents, and the exact position of both tidal and current stations, together with situation and height of bench mark. The time of making each observation should be shown, and data given for reduction to some standard time. In extended tidal observations the meteorological conditions should be carefully recorded, the instruments used for the observations being properly compared with standards.

513. There are frequently remarkable facts in reference to tides and currents to be obtained from persons having local knowledge; these should be examined and recorded. The date and circumstances of the highest and lowest tides ever known form important items of information.

514. PLANES OF REFERENCE.—The *plane of reference* is the plane to which soundings and tidal data are referred. One of the principal objects of observing tides when making a survey is to furnish the means for reducing the soundings to this plane. Four planes of reference are used; namely, mean low water, mean low water springs, mean lower low waters, and the harmonic or Indian tide plane.

Mean low water is a plane whose depression below mean sea level corresponds with half the mean semi-diurnal range, while the depression of *mean low-water springs* corresponds with half the mean range of spring tide; *mean lower low water* depends upon the diurnal inequality in high and low water; the *harmonic* or *Indian tide plane* was adopted as a convenient means of expressing something of an approximation to the level of low water of ordinary spring tides, but where there is a large diurnal inequality in low waters it falls considerably below the true mean of such tides.

As these planes may differ considerably, it is important to ascertain which plane of reference is adopted before making use of any chart or considering data concerning the tides.

515. The tides are subject to so many variations dependent upon the movements of the sun and moon, and to so many irregularities due to the action of winds and river outflows, that a very long series of observations would be necessary to fix any natural plane. In consideration of this, and keeping in view the possibilities of repetitions of the surveys or subsequent discoveries within the field of work, it is necessary to define the position of the plane of reference which has resulted from any series of observations. This is done by leveling from the tide gauge to a permanent *bench*, precisely as if the adopted plane were arbitrary.

516. BENCH MARK.—The plinth of a light-house, the water table of a substantial building, the base of a monument, and the like, are proper benches; and when these are not within reach, a mark

may be made on a rock not likely to be moved or started by the frost, or, if no rock naturally exists in the neighborhood, a block of stone buried below the reach of frost and plowshare should be the resort. When a bench is made on shore, it should be marked by a circle of 2 or 3 inches diameter with a cross in the center, indicating the reference point. The levelings between this point and the gauge should be be run over twice and the details recorded. A bench made upon a wharf or other perishable structure is of little value, but in the absence of permanent objects it is better than nothing. The marks should be cut in, if on stone, and if on wood, copper nails should be used. The bench must be sketched and carefully described, and its location marked on the hydrographic sheet, with a statement of the relative position of the plane of reference.

517. The leveling from the bench mark to the tide gauge may be done, when a leveling instrument is not available, by measuring the difference of height of a number of intermediate points by means of a long straight-edged board, held horizontal by the aid of a carpenter's spirit level, or even a plummet square, taking care to repeat each step with the level inverted end for end. A line of sight to the sea horizon, when it can be seen from the bench across the tide staff, will afford a level line of sufficient accuracy, especially when observed with the telescope. It may often be convenient to combine these methods.

518. Tide Gauges.—The *Staff Gauge* is the simplest device for measuring the heights of tides, and in perfectly sheltered localities it is the best. It consists of a vertical staff graduated upward in feet and tenths, and so placed that its zero shall lie below the lowest tides. The same gauge may also be used where the surface is rough, if a glass tube with a float inside is secured alongside of the staff, care being taken to practically close the lower end of the tube so as to exclude undulations; readings may also be made by noting the point midway between the crest and trough of the waves.

A staff gauge should always be erected for careful tidal observations, even where other classes of gauge are to be employed, as it furnishes a standard for comparison of absolute heights, and also serves to detect any defects in the mechanical details upon which all other gauges are to a greater or less extent dependent.

519. Where there is considerable swell, and where, from the situation of the gauge or the great range of the tide (making it inconvenient for the observer to see the figures in certain positions) the staff gauge can not be used, recourse must be had to the *Box Gauge.* This gauge consists of a vertical box, closed at the bottom, with a few small holes in the lower part which admit sufficient water to keep the level within equal to the mean level without, but which do not permit the admission of water with sufficient rapidity to be affected by the waves. Within the box is a copper float; in some cases this float carries a graduated vertical rod whose position with reference to a fixed point of the box affords a measure for the height of the water; in other gauges of this class the float is attached to a wire or cord which passes over pulleys and terminates in a counterpoise whose position on a vertical graduated scale shows the height of tide.

520. An *Automatic Gauge* requires a box and float such as has just been described. The motion of the float in rising and falling with the tide is communicated to a pencil which rests upon a moving sheet of paper; uniform motion is imparted to the paper by the revolution of a cylinder driven by clock-work; the motion of the pencil due to the tide is in a direction perpendicular to the direction of motion of the paper, and a curve is thus traced, of which one coordinate is time, and the other height. The paper, which is usually of sufficient length to contain a month's record, is paid out from one cylinder, passes over a second whereon it receives the record, and is rolled upon a third cylinder, which thus contains the completed tidal sheet.

This gauge, besides giving a perfectly continuous record, has the further merit of requiring but little of the observer's time. But its indications, both of time and heights, should be checked by occasional comparisons with the standard clock and the staff gauge, the readings of which should be noted by hand at appropriate points of the graphic record.

CHAPTER XXI.

OCEAN CURRENTS.

521. An *ocean current* is a progressive horizontal motion of the water occurring throughout a region of the ocean, as a result of which all bodies floating therein are carried with the stream.

The *set* of a current is the direction toward which it flows, and its *drift*, the velocity of the flow.

522. Cause.—The principal *cause* of ocean currents is the wind. Every breeze sets in motion, by its friction, the surface particles of the water over which it blows; this motion of the upper stratum is imparted to the stratum next beneath, and thus the general movement is communicated, each layer of particles acting upon the one below it, until a current is established. The direction, depth, strength, and permanence of such a current will depend upon the direction, steadiness, and force of the wind; all, however, subject to modification on account of extraneous causes, such as the intervention of land or shoals and the meeting of conflicting currents.

A minor cause in the generation of ocean currents is the difference in density of the sea water in different regions, as a result of which a set is produced from the more dense toward the less dense, in the effort to establish equilibrium of pressure; the difference of density may be due to temperature, the warmer water near the equator being less dense than the colder water of higher latitudes; or it may be created by a difference in the amount of contained saline matter, resulting from evaporation, freezing, or other causes. Another minor factor that may have influence upon ocean currents is the difference of pressure exerted by the atmosphere upon the water in different regions. But neither of the last-mentioned causes may be regarded as of great importance when compared with the influence, direct and indirect, of the wind.

523. Drift and Stream Currents.—Ocean currents may be divided into two classes: *Drift* and *Stream Currents.*

A *Drift Current* is one which arises from the effect of wind upon the surface water, impelling the particles to leeward. Such currents reach only to shallow depths, except in regions where caused by winds whose prevalence is almost unbroken, and where, in consequence, motion is communicated stratum by stratum, during a long series of years, until the influence is felt at great depths.

A *Stream Current* is one which arises when the water carried forward by a drift current encounters an obstacle which prevents a further flow in the direction which it has been following, and the particles are forced to acquire a new motion which takes such direction as may be imposed by the conditions existing in the locality.

Some currents are compounded of both drift and stream; for a stream already formed may pass through the region of a prevalent wind in such direction that it will receive an accelerating effect due to the wind.

524. Submarine Currents.—In any scientific investigation of the circulation of ocean waters it is necessary to take account of the submarine currents as well as those encountered upon the surface; but for the practical purposes of the navigator the surface currents alone are of interest.

525. Methods of Determination.—The methods of determining the existence of a current, with its set and drift, may be divided into three classes; namely, (*a*) by observations from a vessel occupying a stationary position not affected by the current; (*b*) by comparison of the position of a vessel under way as given by observation with that given by dead reckoning; and (*c*) by the drift of objects abandoned to the current in one locality and reappearing in another.

526. Of these methods, the first named, by observations from a vessel at anchor, is by far the most accurate and reliable, but being possible only under special circumstances is not often available. The most valuable information about ocean currents being that which pertains to conditions in the open sea, the great depths there existing usually preclude the possibility of anchoring a vessel; ships especially fitted for the purpose have at times, however, carried out current observations with excellent results; the most notable achievements in this direction are those of the survey of the Gulf Stream, made by United States naval officers acting under the Coast and Geodetic Survey, during which the vessel was anchored and observations were made in positions where the depth reached to upward of 2,000 fathoms.

527. The method of determining current from a comparison of positions obtained, respectively, by observation and by dead reckoning is the one upon which our knowledge must largely depend. This method is, however, always subject to some inaccuracy, and the results are frequently quite erroneous, for the so-called current is thus made to embrace not only the real set and drift, but also the errors of observation and dead reckoning. In the case of a modern steamer accurately steered and equipped with good instruments for determining the speed through the water as well as the position by astronomical observations, the current may be arrived at by this method with a fairly close degree of accuracy. It is not always possible, however, to keep an exact reckoning, and this is especially true in sailing vessels, where the conditions render it difficult to determine correctly the position by account; this source of error may be combined with faulty instrumental determinations, giving apparent currents differing widely from those that really exist.

528. Much useful knowledge regarding ocean currents has been derived from the observed drift of objects from one to another locality. This is true not only of the bottles thrown overboard from vessels with the particular object of determining the currents, but also of derelicts, drifting buoys, and pieces

of wreckage, which fulfill a similar mission. The deductions to be drawn from such drift are of a general nature only. The point of departure, point of arrival, and elapsed time are all that are positively known. The route followed and the set and drift of current at different points are not indicated, and in the case of objects floating otherwise than in a completely submerged condition account must be taken of the fact that the drift is influenced by the wind. But even this general information is of great value in researches as to ocean currents, and navigators who desire to aid in the work of investigation may do so by throwing overboard, from time to time, sealed bottles containing a statement of date and position at which they are launched.

529. Currents of the Atlantic Ocean.—A consideration of the currents of the Atlantic most conveniently begins with a description of the *Equatorial Currents*. The effect of the northeast and southeast trade winds is to form two great drift currents, setting in a westerly direction across the Atlantic from Africa toward the American continent, whose combined width covers at times upward of fifty degrees of latitude. These are distinguished as the *Northern* or *Southern Equatorial Currents*, according as they arise from the trade winds of the northern or southern hemisphere.

Of the two, the Southern Equatorial Current is the more extensive. It has its origin off the continent of Africa south of the Guinea coast, and begins its flow with a daily velocity that averages about 15 miles; it maintains a general set of west, the portion near the equator acquiring later, however, a northerly component, while the drift steadily increases until, on arriving off the South American coast, a rate of 60 miles is not uncommon. At Cape San Roque the current bifurcates, the main or equatorial branch flowing along the Guiana coast, while the other branch is deflected to the southward.

The Northern Equatorial Current originates to the northward of the Cape Verde Islands and sets across the ocean in a direction that averages due west; though parallel to the corresponding southern drift, its velocity is not so high.

530. Between the Northern and Southern Equatorial Currents is found the *Equatorial Counter Current*, which sets to the eastward, being apparently a flowing back, in the region of equatorial calms, of water carried westward by the trade drifts. The extent and strength of this current varies with the season, a maximum being attained in July or August, when its effect is apparent to ths westward of the fiftieth meridian of west longitude, while at its minimum, in November or December, its influence is but slight and prevails over a limited area only.

531. To the westward of the region of the Equatorial Counter Current the North and the South Equatorial Currents unite. A large part of the combined stream flows into the Caribbean Sea through the various passages between the Windward Islands, takes up a course first to the westward and then to the northward and westward, finally arriving off the extremity of the peninsula of Yucatan; from here some of the water follows the shore line of the Gulf of Mexico, while another portion passes directly toward the north Cuban coast; by the reuniting of these two branches in the Straits of Florida there is formed the most remarkable of all ocean currents—the Gulf Stream.

From that portion of the combined equatorial currents which fails to find entrance to the Caribbean Sea a current of moderate strength and volume takes its course along the north coasts of Porto Rico, Haiti, and Cuba, flows between the last-named island and the Bahamas, and enters the Gulf Stream off the Florida coast, thus adding its waters to those of the main branch of the equatorial current which have arrived at the same point by way of the Caribbean, the Yucatan Passage, and the Gulf.

532. The *Gulf Stream*, which has its origin, as has been described, in the Straits of Florida, and receives an accession from a branch of the Equatorial Current off the Bahamas, flows in a direction that averages true north as far as the parallel of 31°, then curves sharply to ENE. until reaching the latitude of 32°, when a direction a little to the north of NE. is assumed and maintained as far as Cape Hatteras; at this point its axis is about 40 miles, while its inner edge is in the neighborhood of 20 miles off the shore. Thus far in its flow the average position of the maximum current is from 11 to 20 miles outside the 100-fathom curve, disregarding the irregularities of the latter, and the width of the stream—about 40 miles—is nearly uniform. From off Hatteras the stream broadens rapidly and curves more to the eastward, seeking deeper water; its northern limit may be stated to be 60 to 80 miles off Nantucket Shoals and 120 to 150 miles to the southward of Nova Scotia, in which latter place it has expanded to a width of about 250 miles. Further on, its identity as the Gulf Stream is lost, but its general direction is preserved in a current to be described later.

The water of the Gulf Stream is of a deep indigo-blue color, and its junction with ordinary sea water may be plainly recognized; in moderate weather the edges of the stream are marked by ripples; in cool regions the evaporation from its surface, due to difference of temperature between air and water, is apparent to the eye; the stream carries with it a quantity of weed known as "gulf weed," which is familiar to all who have navigated its waters.

In its progress from the tropics to higher latitudes the transit is so rapid that time is not given for more than a partial cooling of the water, and it is therefore found that the Gulf Stream is very much warmer than the neighboring waters of the seas through which it flows. This warm water is, however, divided by bands of markedly cooler water which extend in a direction parallel to the axis and are usually found near the edges of the stream of warm water. The most abrupt change from warm to cold water occurs on the inshore side, where the name of the *Cold Wall* has been given to that band which has appeared to some oceanographers to form the northern and western boundary of the stream.

The investigations of Pillsbury tend to prove that the thermometer is only an approximate guide to the direction and velocity of the current. Though it indicates the limits of the stream in a general way, it must not be assumed that the greatest velocity of flow coincides with the highest temperature, nor that the northeasterly set will be lost when the thermometer shows a region of cold sea water.

The same authority has also demonstrated that in the vicinity of the land there is a marked variation in the velocity of current at different hours of the day, which may amount to upward of 2 knots, and which is due to the elevation and depression of the sea as a result of tidal influences, the maximum current being encountered at a period which averages about three hours after the moon's transit. Another effect noted is that at those times when the moon is near the equator tne current presents a narrow front with very high velocity in the axis of maximum strength, while at periods of great northerly or

southerly declination the front broadens, the current decreasing at the axis and increasing at the edges. These tidal effects are not, however, observed in the open sea.

The velocity of the Gulf Stream varies with the seasons, following the variation in the intensity of the trade winds, to which it largely owes its origin. The drift of the current under average conditions may be stated as follows:

Between Key West and Habana: Mean surface velocity in axis of maximum current, 2¼ knots; allowance to be made by a vessel crossing the entire width of the stream, 1.1 knots per hour.

Off Fowey Rocks: Mean surface velocity in axis, 3.5 knots; allowance in crossing, 2¼ knots per hour.

Off Cape Hatteras: Mean surface velocity in axis, upward of 2 knots; allowance in crossing the stream, 1½ knots per hour between the 100-fathom curve and a point 40 miles outside that curve.

533. After passing beyond the longitude of the easternmost portions of North America, it is generally regarded that the Gulf Stream, as such, ceases to exist; but by reason of the prevalence of westerly winds the direction of the set toward Europe is continued until the continental shores are approached, when the current divides, one branch going to the northeastward and entering the Arctic regions and the other running off toward the south and east in the direction of the African coast. These currents have received, respectively, the designations of the *Easterly, Northeast,* and *Southeast Drift Currents.*

534. The effect of the currents thus far described is to create a general circulation of the surface waters of the North Atlantic, in a direction coinciding with that of the hands of a watch, about the periphery of a huge ellipse, whose limits of latitude may be considered as 10° N. and 45° N., and which is bounded in longitude by the Eastern and Western continents. The central space thus inclosed, in which no well-marked currents are observed, and in the waters of which great quantities of the Sargasso or gulf weed are encountered, is known as the *Sargasso Sea.*

535. The Southeast Drift Current carries its waters to the northwest coast of Africa, whence they follow the general trend of the land from Cape Spartel to Cape Verde. From this point a large part of the current is deflected to the eastward close along the upper Guinea coast. The steam thus formed, greatly augmented at certain seasons by the prevailing monsoon and by the waters carried eastward with the Equatorial Counter Current, is called the *Guinea Current.* A remarkable characteristic of this current is the fact that its southern limit is only slightly removed from the northern edge of the west-moving Equatorial Current, the effect being that the two currents flow side by side in close proximity, but in diametrically opposite directions.

536. The *Arctic* or *Labrador Current* sets out of Davis Strait, flows southward down the coasts of Labrador and Newfoundland, and thence southwestward past Nova Scotia and the coast of the United States, being found inshore of the Gulf Stream. It brings with it the ice so frequently met at certain seasons off Newfoundland.

537. *Rennell's Current* is a temporary but extensive stream, which sets at times from the Bay of Biscay toward the west and northwest, across the entrance to the English Channel and to the westward of Cape Clear.

538. Of the two branches of the Southern Equatorial Current which are formed by its bifurcation off Cape San Roque, the northern one, setting along the coasts of northeastern Brazil and of Guiana and contributing to the formation of the Gulf Stream, has already been described; the other, known as the *Brazil Current,* flows to south and west, along the southeastern coast of Brazil, as far as the neighborhood of the island of Trinidad; here it divides, one part continuing down the coast and having some slight influence as far as the latitude of 45° S., and the other curving around toward east.

539. The last-mentioned branch of the Brazil Current is called the *Southern Connecting Current* and flows toward the African coast in about the latitude of Tristan d'Acunha. It then joins its waters with those of the general northerly current that sets out of the Antarctic region, forming a current which flows to the northward along the southwest African coast and eventually connects with the Southern Equatorial Current, thus completing the surface circulation of the South Atlantic.

540. There are two other currents whose effects are felt in the Atlantic, one originating in the Indian Ocean and flowing around the Cape of Good Hope, the other originating in the Pacific and flowing around Cape Horn. They will be described under the currents of the oceans in which they first appear.

541. Currents of the Pacific Ocean.—As in the Atlantic, the waters of the Pacific Ocean, in the region between the tropics, have a general drift toward the westward, due to the effect of the trade winds, the currents produced in the two hemispheres being denominated, respectively, the *Northern* and the *Southern Equatorial Currents.* These are separated, as also in the case of the Atlantic, by an east-setting stream, about 300 miles wide, whose mean position is a few degrees north of the equator, and which receives the name of the *Equatorial Counter Current.*

542. The major portion of the Northern Equatorial Current, after having passed the Mariana Islands, flows toward the eastern coast of Formosa in a WNW. direction, whence it is deflected northward, forming a current which is sometimes called the *Japan Stream,* but which more frequently receives its Japanese name of *Kuro Siwo,* or "black stream." This current, the waters of which are dark in color and contain a variety of seaweed similar to "gulf weed," carries the warm tropical water at a rapid rate to the northward and eastward along the coasts of Asia and its offlying islands, presenting many analogies to the Gulf Stream of the Atlantic.

The limits and volume of the Kuro Siwo vary according to the monsoon, being augmented during the season of southwesterly winds and diminished during the prevalence of those from northeast. The current sets to the north along the east coast of Formosa, and in about latitude 26° N. changes its course to northeast, arriving at the extreme southwestern point of Japan by a route to westward of the Meiacosima and Loo-choo islands. A branch makes off from the main stream to follow northward along the west coast of Japan, entering the Sea of Japan by the Korea Channel; but the principal current bends toward the east, flows through Van Diemen Strait and the passages between the Linschoten Isles, and runs parallel to the general trend of the south shores of the Japanese islands of Kiushu, Sikok, and Nipon, attaining its greatest velocity between Bungo and Kii channels, where its average drift is between 2 and 3 knots per hour. Continuing beyond the southeastern extremity of Nipon, the direction

of the stream becomes somewhat more northerly, and its width increases, with consequent loss of velocity. In the Kuro Siwo, as in the Gulf Stream, the temperature of the sea water is an approximate, though not an exact, guide as to the existence of the current.

543. Near 146° or 147° E. and north of the fortieth parallel the Kuro Siwo divides into two parts. One of these, called the *Kamchatka Current*, flows to the northeast in the direction of the Aleutian Islands, and its influence is felt to a high latitude. The second branch continues as the main stream, and maintains a general easterly direction to the 180th meridian, where it is merged into the north and northeast drift currents which are generally encountered in this region.

544. A cold counter current to the Kamchatka Current sets out of Bering Sea and flows to the south and west close to the shores of the Kuril Islands, Yezo and Nipon, sometimes, like the Labrador Current in the Atlantic, bringing with it quantities of Arctic ice. This is often called by its Japanese name of *Oya Siwo.*

545. On the Pacific coast of North America, from about 50° N. to the mouth of the Gulf of California, 23° N., a cold current, 200 or 300 miles wide, flows with a mean speed of three-quarters of a knot, being generally stronger near the land than at sea. It follows the trend of the land (nearly SSE.) as far as Point Concepcion (south of Monterey), when it begins to bend toward SSW., and then to WSW., off Capes San Blas and San Lucas, ultimately joining the great northern equatorial drift.

On the coast of Mexico, from Cape Corrientes (20° N.) to Cape Blanco (Gulf of Nicoya), there are alternate currents extending over a space of more than 300 miles in width, which appear to be produced by the prevailing winds. During the dry season—January, February, and March—the currents generally set toward southeast; during the rainy season—from May to October—especially in July, August, and September, the currents set to northwest, particularly from Cosas Island and the Gulf of Nicoya to the parallel of 15°.

546. The Southern Equatorial Current prevails between limits of latitude that may be approximately given as 4° N. and 10° S., in a broad region extending from the American continent almost to the one hundred and eightieth meridian, setting always to the west and with slowly increasing velocity. In the neighborhood of the Fiji Islands this current divides; one part, known as the *Rossel Current*, continues to the westward, following a route marked by the various passages between the islands, and later acquiring a northerly component and setting through Torres Strait and along the north coast of New Guinea; the other part, called the *Australia Current*, sets toward south and west, arriving off the east coast of Australia, along which it flows southward to about latitude 35° S., whence it bends toward southeast and east and is soon after lost in the currents due to the prevailing wind.

547. The general drift current that sets to the north out of the Antarctic regions is deflected until, upon gaining the regions to the southwest of Patagonia, it has acquired a nearly easterly set; in striking the shores of the South American continent it is divided into two branches.

The first, known as the *Cape Horn Current*, maintains the general easterly direction, and its influence is felt, where not modified by winds and tidal currents, throughout the vicinity of Cape Horn, and, in the Atlantic Ocean, off the Falkland Islands and eastern Patagonia.

The second branch flows northeast in the direction of Valdivia and Valparaiso, follows generally the direction of the coast lines of Chile and Peru (though at times setting directly toward the shore in such manner as to constitute a great danger to the navigator), and forms the important current which has been called variously the *Peruvian*, *Chilean*, or *Humboldt Current*, the last name having been given for the distinguished scientist who first noted its existence. The principal characteristic of the Peruvian Current is its relatively low temperature. The direction of the waters between Pisco and Payta is between north and northwest; near Cape Blanco the current leaves the coast of America and bears toward the Galapagos Islands, passing them on both the northern and southern sides; here it sets toward WNW. and west; beyond the meridian of the Galapagos it widens rapidly, and the current is lost in the equatorial current, near 108° W. As often happens in similar cases, the existence of a counter-current has been proved on different occasions; this sets toward the south, is very irregular, and extends only a little distance from shore.

548. Currents of the Indian Ocean.—In this ocean the currents to the north of the equator are very irregular; the periodical winds, the alternating breezes, and the changes of monsoon produce currents of a variable nature, their direction depending upon that of the wind which produces them, upon the form of neighboring coasts, or, at times, upon causes which can not be satisfactorily explained.

549. There is, in the Indian Ocean south of the equator, a regular *Equatorial Current* which, by reason of owing its source to the southeast trade winds, corresponds with the Southern Equatorial Currents of the Atlantic and Pacific. The limits of this west-moving current vary with the longitude as well as with the season. Upon reaching about the meridian of Rodriguez Island, a branch makes off toward the south and west, flowing past Mauritius, then to the south of Madagascar (on the meridian of which it is 480 miles broad), and thereafter, rapidly diminishing its breadth, forming part of the Agulhas Current a little to the south of Port Natal.

The main equatorial current continues westward until passing the north end of Madagascar, where, encountering the obstruction presented by the African continent, it divides, one branch following the coast in a northerly, the other in a southerly, direction. The former, in the season of the southwest monsoon, is merged into the general easterly and northeasterly drift that prevails throughout the ocean from the northern limit of the Equatorial Current on the south, as far as India and the adjacent Asiatic shores on the north; but during the northeast monsoon, when there exists in the northern regions of the Indian Ocean a westerly drift current analogous to the Northern Equatorial Currents produced in the Atlantic and Pacific by the northeast trades, there is formed an east-setting *Equatorial Counter Current*, which occupies a narrow area near the equator and is made up of the waters accumulated at the western continental boundary of the ocean by the drift currents of both hemispheres.

550. The southern branch of the Equatorial Current flows to the south and west down the Mozambique channel, and, being joined in the neighborhood of Port Natal by the stream which arrives from the open ocean, there is formed the warm *Agulhas Current*, which possesses many of the characteristics of the Gulf and Japan streams. This current skirts the east coast of South Africa and

attains considerable velocity over that part between Port Natal and Algoa Bay. During the summer months its effects are felt farther to the westward; during the winter it diminishes in force and extent. The meeting of the Agulhas Current with the cold water of higher latitudes is frequently denoted by a broken and confused sea.

Upon arriving at the southern side of the Agulhas Bank, the major part of the current is deflected to the south, and then curves toward east, flowing back into the Indian Ocean with diminished strength and temperature, on about the fortieth parallel of south latitude, where its influence is felt as far as the eightieth meridian. A small part of the stream which reaches Agulhas Bank continues across the southern edge of that bank, then turns to the northwest along the west coast of the continent until it is united with the waters of the Southern Connecting Current of the Atlantic.

551. Along the fortieth parallel of south latitude, between Africa and Australia, there is a general easterly set, due to the branch of the Agulhas current already described, to the continuation of the drift current from the Atlantic which passes to southward of the Cape of Good Hope, and to the westerly winds which largely prevail in this region. At Cape Leeuwin, the southwestern extremity of Australia, this east-setting current is divided into two branches; one, going north along the west coast of Australia, blends with the Equatorial current nearly in the latitude of the Tropic of Capricorn; the other preserves the direction of the original current and has the effect of producing an easterly set along the south coast of Australia.

552. As in the other oceans, a general northerly current is observed to set into the Indian Ocean from the Antarctic regions.

APPENDIX I.

EXTRACTS FROM THE AMERICAN EPHEMERIS AND NAUTICAL ALMANAC, FOR THE YEAR 1879, WHICH HAVE REFERENCE TO THE EXAMPLES FOR THAT YEAR GIVEN IN THIS WORK.

[Extracts: Page I.]

AT GREENWICH APPARENT NOON.

Day of the Week.	Day of the Month.	THE SUN'S Apparent Right Ascension.	Diff. for 1 hour.	Apparent Declination.	Diff. for 1 hour.	Semi-diameter.	Sidereal Time of the Semi-diameter passing the Meridian.	Equation of Time, *to be added to* / *subtracted from Apparent Time.*	Diff. for 1 hour.
		h. m. s.	s.	° ′ ″	″	′ ″	s.	m. s.	s.
				JANUARY.					
Sun.	19	20 4 60.17	10.626	S. 20 21 9.0	+31.54	16 17.58	69.72	10 56.68	0.769
Mon.	20	20 9 14.84	10.595	20 8 20.4	32.49	16 17.48	69.61	11 14.74	0.738
Tues.	21	20 13 28.75	10.564	S. 19 55 9.1	+33.43	16 17.38	69.51	11 32.05	0.706
				APRIL.					
Tues.	1	0 41 54.87	9.096	N. 4 30 43.2	+57.85	16 2.16	64.51	4 0.60	0.758
Wed.	2	0 45 33.24	9.100	4 53 49.1	57.64	16 1.89	64.53	3 42.46	0.754
Thur.	3	0 49 11.70	9.106	5 16 49.8	57.41	16 1.61	64.55	3 24.43	0.748
Sun.	13	1 25 47.34	9.205	9 0 54.1	54.40	15 58.86	64.89	0 35.02	0.649
Mon.	14	1 29 28.45	9.219	9 22 35.4	54.03	15 58.59	64.94	0 19.60	0.635
Tues.	15	1 33 9.91	9.234	9 44 7.5	53.64	15 58.31	64.99	0 4.54	0.620
Wed.	16	1 36 51.74	9.250	10 5 29.9	53.23	15 58.04	65.04	0 10.15	0.604
Thur.	17	1 40 33.95	9.268	10 26 42.3	52.80	15 57.77	65.09	0 24.46	0.587
Frid.	18	1 44 16.56	9.285	10 47 44.7	52.37	15 57.50	65.15	0 38.36	0.570
Sat.	19	1 47 59.58	9.302	11 8 36.4	51.92	15 57.24	65.21	0 51.85	0.553
Sun.	20	1 51 43.01	9.320	11 29 17.1	51.45	15 56.98	65.27	1 4.93	0.536
Mon.	21	1 55 26.87	9.337	N. 11 49 46.4	+50.97	15 56.72	65.33	1 17.60	0.518
				MAY.					
Mon.	5	2 48 30.72	9.626	N. 16 13 40.4	+42.86	15 53.36	66.37	3 25.18	0.229
Tues.	6	2 52 22.03	9.650	16 30 40.4	42.17	15 53.14	66.45	3 30.40	0.206
Sat.	10	3 7 53.03	9.747	17 35 53.8	39.33	15 52.25	66.78	3 45.58	0.109
Sun.	11	3 11 47.27	9.771	17 51 29.1	38.59	15 52.03	66.86	3 47.90	0.084
Thur.	15	3 27 30.07	9.871	18 50 48.5	35.52	15 51.20	67.19	3 51.32	0.014
Frid.	16	3 31 27.26	9.895	19 4 51.6	34.72	15 51.00	67.27	3 50.68	0.039
Sat.	17	3 35 25.03	9.919	19 18 35.5	33.91	15 50.80	67.35	3 49.47	0.062
Sun.	18	3 39 23.37	9.942	N. 19 31 59.8	+33.06	15 50.61	67.43	3 47.69	0.086

NOTE.—Mean Time of the Semidiameter passing may be found by substracting $0^s.18$ from the Sidereal Time.
+ prefixed to the hourly change of declination indicates that north declinations are increasing and south declinations are decreasing; − indicates that north declinations are decreasing and south declinations increasing.

[Extracts: Page I.]

AT GREENWICH APPARENT NOON—Continued.

Day of the Week.	Day of the Month.	THE SUN'S Apparent Right Ascension.	Diff. for 1 hour.	Apparent Declination.	Diff. for 1 hour.	Semi-diameter.	Sidereal Time of the Semi-diameter passing the Meridian.	Equation of Time, *to be subtracted from* / *added to Apparent Time.*	Diff. for 1 hour.
		h. m. s.	*s.*	° ′ ″	″	′ ″	*s.*	*m. s.*	*s.*
				JUNE.					
Sat.	7	5 0 33.74	10.312	N. 22 45 9.5	+14.64	15 47.63	68.70	1 28.86	0.455
Tues.	10	5 12 57.61	10.348	23 0 55.9	11.63	15 47.30	68.81	0 54.76	0.490
Wed.	11	5 17 6.09	10.358	23 5 22.9	10.62	15 47.20	68.84	0 42.87	0.500
Frid.	13	5 25 23.73	10.376	23 13 3.8	8.58	15 47.00	68.90	0 18.42	0.518
Sat.	14	5 29 32.85	10.383	23 16 17.4	7.55	15 46.91	68.92	0 5.89	0.525
Frid.	20	5 54 30.05	10.402	23 27 0.3	1.36	15 46.48	68.98	1 11.75	0.546
Sat.	21	5 58 39.75	10.402	23 27 20.5	+ 0.32	15 46.43	68.98	1 24.86	0.546
Wed.	25	6 15 18.00	10.389	23 24 33.1	− 3.78	15 46.27	68.94	2 16.72	0.532
Thur.	26	6 19 27.29	10.383	23 22 49.5	4.81	15 46.24	68.93	2 29.42	0.526
Frid.	27	6 23 36.42	10.376	N. 23 20 41.3	− 5.84	15 46.22	68.91	2 41.97	0.519
				JULY.					
Frid.	11	7 21 16.72	10.197	N. 22 8 29.2	−19.76	15 46.30	68.30	5 10.04	0.339
Sat.	12	7 25 21.24	10.179	22 0 23.2	20.71	15 46.33	68.24	5 17.99	0.321
Tues.	22	8 5 39.82	9.964	20 19 8.9	29.72	15 46.94	67.51	6 10.85	0.108
Wed.	23	8 9 38.68	9.939	20 7 5.2	30.57	15 47.03	67.43	6 13.15	0.083
Thur.	24	8 13 36.94	9.914	N. 19 54 41.3	−31.41	15 47.13	67.35	6 14.84	0.059
				SEPTEMBER.				*To be subtracted from Apparent Time.*	
Wed.	10	11 13 33.93	8.993	N. 4 59 24.2	−56.90	15 55.81	64.12	3 1.29	0.862
Thur.	11	11 17 9.68	8.988	N. 4 36 36.2	−57.10	15 56.06	64.10	3 22.03	0.867
				DECEMBER.					
Mon.	22	18 1 24.12	11.108	S. 23 27 17.3	+ 0.37	16 18.13	71.30	1 16.61	1.248
Tues.	23	18 5 50.72	11.107	S. 23 26 54.3	+ 1.56	16 18.18	71.30	0 46.64	1.246

NOTE.—Mean Time of the Semidiameter passing may be found by subtracting $0^s.18$ from the Sidereal Time.
+ prefixed to the hourly change of declination indicates that north declinations are increasing and south declinations are decreasing; − indicates that north declinations are decreasing and south declinations increasing.

[Extracts: Page II.]

AT GREENWICH MEAN NOON.

Day of the Week.	Day of the Month.	THE SUN'S Apparent Right Ascension.	THE SUN'S Diff. for 1 hour.	THE SUN'S Apparent Declination.	THE SUN'S Diff. for 1 hour.	Equation of Time, *to be subtracted from* / *added to Mean Time.*	Diff. for 1 hour.	Sidereal Time or Right Ascension of *Mean* Sun.
		h. m. s.	*s.*	° ′ ″	″	*m. s.*	*s.*	*h. m. s.*
				JANUARY.				
Frid.	10	19 26 16.08	10.866	S. 21 58 32.0	+ 22.35	7 43.42	1.010	19 18 32.66
Sat.	11	19 30 36.59	10.842	21 49 22.7	23.41	8 7.37	0.986	19 22 29.22
Mon.	20	20 9 12.84	10.593	20 8 26.6	32.48	11 14.60	0.738	19 57 58.24
Tues.	21	20 13 26.71	10.562	S. 19 55 15.6	+ 33.42	11 31.91	0.706	20 1 54.80
				APRIL.				
Tues.	1	0 41 54.27	9.098	N. 4 30 39.4	+ 57.86	4 0.65	0.758	0 37 53.62
Wed.	2	0 45 32.68	9.102	4 53 45.6	57.65	3 42.50	0.754	0 41 50.16
Tues.	8	1 7 26.22	9.146	7 10 20.3	56.08	1 56.74	0.709	1 5 29.48
Wed.	9	1 11 5.87	9.157	7 32 42.8	55.77	1 39.83	0.698	1 9 26.04
Tues.	15	1 33 9.91	9.236	9 44 7.4	53.65	0 4.54	0.620	1 33 5.37
Wed.	16	1 36 51.77	9.252	10 5 30.1	53.24	0 10.15	0.604	1 37 1.92
Thur.	17	1 40 34.02	9.269	10 26 42.8	52.81	0 24.46	0.587	1 40 58.48
Sun.	20	1 51 43.19	9.321	11 29 18.1	51.46	1 4.94	0.536	1 52 48.13
Mon.	21	1 55 27.08	9.338	11 49 47.6	50.98	1 17.61	0.518	1 56 44.69
Tues.	22	1 59 11.41	9.356	12 10 5.4	50.48	1 29.83	0.500	2 0 41.24
Wed.	23	2 2 56.19	9.375	12 30 11.2	49.97	1 41.61	0.481	2 4 37.80
Thur.	24	2 6 41.42	9.394	12 50 4.7	49.46	1 52.93	0.462	2 8 34.35
Frid.	25	2 10 27.11	9.414	13 9 45.4	48.92	2 3.80	0.442	2 12 30.91
Tues.	29	2 25 34.67	9.494	14 26 14.5	46.65	2 42.46	0.361	2 28 17.13
Wed.	30	2 29 22.79	9.515	N. 14 44 46.7	+ 46.04	2 50.89	0.340	2 32 13.68
				MAY.				
Frid.	9	3 4 0.01	9.723	N. 17 20 3.5	+ 40.06	3 42.68	0.134	3 7 42.69
Sat.	10	3 7 53.65	9.747	17 35 56.3	39.33	3 45.59	0.109	3 11 39.24
Sun.	11	3 11 47.89	9.771	17 51 31.6	38.59	3 47.91	0.084	3 15 35.80
Mon.	12	3 15 42.71	9.796	18 6 48.9	37.84	3 49.64	0.060	3 19 32.35
Frid.	16	3 31 27.90	9.895	19 4 53.8	34.72	3 50.68	0.039	3 35 18.58
Sat.	17	3 35 25.67	9.919	19 18 37.6	33.91	3 49.47	0.062	3 39 15.14
Sun.	18	3 39 24.01	9.942	19 32 1.8	33.09	3 47.68	0.086	3 43 11.69
Wed.	28	4 19 36.81	10.155	21 27 5.9	24.28	3 0.46	0.297	4 22 37.27
Thur.	29	4 23 40.75	10.173	21 36 37.4	23.34	2 53.08	0.315	4 26 33.83
Frid.	30	4 27 45.12	10.190	21 45 46.5	22.40	2 45.26	0.334	4 30 30.38
Sat.	31	4 31 49.91	10.207	N. 21 54 33.0	+ 21.45	2 37.03	0.351	4 34 26.94
				JUNE.		*To be added to* / *subtracted from Mean Time.*		
Sat.	7	5 0 34.00	10.311	N. 22 45 9.9	+ 14.64	1 28.85	0.455	5 2 2.85
Sun.	8	5 4 41.64	10.324	22 50 49.3	13.64	1 17.77	0.467	5 5 59.41
Wed.	11	5 17 6.22	10.357	23 5 23.0	10.62	0 42.86	0.500	5 17 49.08
Sat.	14	5 29 32.87	10.382	23 16 17.4	7.55	0 5.89	0.525	5 29 38.76
Sun.	15	5 33 42.11	10.388	23 19 6.4	+ 6.52	0 6.80	0.532	5 33 35.31
Wed.	25	6 15 17.60	10.388	23 24 33.2	− 3.78	2 16.70	0.532	6 13 0.90
Thur.	26	6 19 26.86	10.382	23 22 49.7	4.81	2 29.40	0.526	6 16 57.46
Frid.	27	6 23 35.96	10.375	N. 23 20 41.6	− 5.84	2 41.95	0.519	6 20 54.01

NOTE.—The Semidiameter for Mean Noon may be assumed the same as that for Apparent Noon. + prefixed to the hourly change of declination indicates that north declinations are increasing and south declinations are decreasing; − indicates that north declinations are decreasing and south declinations increasing.

Diff. for 1 hour. $+9^s.8565$.

[Extracts: Page II.]

AT GREENWICH MEAN NOON—Continued.

Day of the Week.	Day of the Month.	THE SUN'S Apparent Right Ascension.	Diff. for 1 hour.	Apparent Declination.	Diff. for 1 hour.	Equation of Time, *to be subtracted from Mean Time.*	Diff. for 1 hour.	Sidereal Time or Right Ascension of *Mean* Sun.
		h. m. s.	*s.*	° ′ ″	″	*m. s.*	*s.*	*h. m. s.*
				AUGUST.				
Tues.	5	9 0 27.45	9.610	N. 17 1 29.2	− 40.52	5 47.69	0.246	8 54 39.76
Wed.	6	9 4 17.82	9.586	N. 16 45 8.6	− 41.20	5 41.51	0.270	8 58 36.31
				SEPTEMBER.		*To be added to Mean Time.*		
Wed.	10	11 13 34.39	8.995	N. 4 59 21.3	− 56.91	3 1.33	0.862	11 16 35.72
Thur.	11	11 17 10.19	8.990	N. 4 36 32.9	− 57.12	3 22.07	0.867	11 20 32.26
				OCTOBER.				
Wed.	15	13 20 28.07	9.309	S. 8 29 16.2	− 55.65	14 7.02	0.548	13 34 35.08
Thur.	16	13 24 11.75	9.333	8 51 28.1	55.34	14 19.89	0.524	13 38 31.64
Frid.	17	13 27 56.01	9.357	9 13 32.4	55.02	14 32.18	0.500	13 42 28.19
Tues.	28	14 9 44.78	9.662	13 6 2.6	50.34	16 5.51	0.195	14 25 50.29
Wed.	29	14 13 37.03	9.693	S. 13 26 4.6	− 49.82	16 9.82	0.164	14 29 46.84
				NOVEMBER.				
Wed.	12	15 9 14.01	10.180	S. 17 41 18.4	− 40.77	15 44.60	0.323	15 24 58.61
Thur.	13	15 13 18.76	10.216	S. 17 57 27.6	− 39.99	15 36.41	0.359	15 28 55.17
				DECEMBER.				
Wed.	3	16 37 40.65	10.844	S. 22 6 24.6	− 21.30	10 5.66	0.987	16 47 46.31
Thur.	4	16 42 1.22	10.869	22 14 43.0	20.23	9 41.65	1.013	16 51 42.87
Mon.	8	16 59 29.19	10.960	22 43 35.6	15.83	7 59.91	1.104	17 7 29.10
Tues.	9	17 3 52.48	10.979	22 49 42.3	14.71	7 33.18	1.123	17 11 25.66
Wed.	10	17 8 16.23	10.998	22 55 21.9	13.58	7 5.99	1.142	17 15 22.22
Thur.	11	17 12 40.41	11.015	23 0 34.3	− 12.45	6 38.37	1.159	17 19 18.78
Mon.	22	18 1 24.34	11.104	23 27 17.3	+ 0.37	1 16.58	1.248	18 2 40.92
Tues.	23	18 5 50.85	11.103	23 26 54.3	1.55	0 46.63	1.246	18 6 37.48
Wed.	24	18 10 17.33	11.101	S. 23 26 2.9	+ 2.73	0 16.71	1.244	18 10 34.03

NOTE.—The Semidiameter for Mean Noon may be assumed the same as that for Apparent Noon. + prefixed to the hourly change of declination indicates that north declinations are increasing and south declinations are decreasing; − indicates that north declinations are decreasing and south declinations increasing.

Diff. for 1 hour. $+9^s.8565$

[Extracts: Page III.]

AT GREENWICH MEAN NOON.

Day of the Month.	Day of the Year.	THE SUN'S True LONGITUDE. λ	λ′	Diff. for 1 hour.	LATITUDE.	Logarithm of the Radius Vector of the Earth.	Diff. for 1 hour.	Mean time of Sidereal 0^h.
		° ′ ″	′ ″	″	″			h. m. s.
APRIL.								
21	111	30 60 16.5	59 47.4	146.27	+0.52	0.0023923	+48.8	21 59 38.53
22	112	31 58 46.1	58 16.9	146.19	+0.52	0.0025087	+48.3	21 55 42.62

[Extracts: Page IV.]

GREENWICH MEAN TIME.

Day of the Month.	THE MOON'S SEMIDIAMETER. Noon.	Midnight.	HORIZONTAL PARALLAX. Noon.	Diff. for 1 hour.	Midnight.	Diff. for 1 hour.	MERIDIAN PASSAGE.	Diff. for 1 hour.	AGE. Noon.
	′ ″	′ ″	′ ″	″	′ ″	″	h. m.	m.	d.
APRIL.									
16	15 4.7	15 0.6	55 13.6	−1.34	54 58.5	−1.19	21 3.8	1.71	24.6
17	14 57.0	14 53.8	54 45.1	1.04	54 33.5	0.90	21 44.3	1.67	25.6
18	14 51.1	14 48.9	54 23.5	0.76	54 15.2	0.63	22 24.6	1.68	26.6
19	14 47.0	14 45.6	54 8.4	0.50	54 3.1	0.38	23 5.4	1.73	27.6
20	14 44.5	14 43.7	53 59.1	0.27	53 56.5	−0.16	23 47.7	1.81	28.6
21	14 43.4	14 43.4	53 55.3	−0.05	53 55.3	+0.06	☌		29.6
22	14 43.8	14 44.6	53 56.7	+0.17	53 59.4	0.29	0 32.2	1.90	0.9
23	14 45.7	14 47.2	54 3.6	0.41	54 9.3	0.54	1 19.0	2.01	1.9
24	14 49.2	14 51.6	54 16.5	0.67	54 25.3	0.80	2 8.2	2.10	2.9
25	14 54.5	14 57.8	54 35.8	0.94	54 48.0	1.09	2 59.3	2.15	3.9
26	15 1.6	15 5.9	55 2.1	+1.24	55 17.9	+1.39	3 51.2	2.16	4.9
MAY.									
6	16 44.6	16 42.1	61 20.1	−0.53	61 11.3	−0.93	12 36.6	2.66	14.9
7	16 38.5	16 33.7	60 57.8	−1.29	60 40.2	−1.62	13 41.2	2.69	15.9
28	15 47.0	15 53.2	57 48.8	+1.86	58 11.4	+1.90	5 55.3	1.95	7.3
29	15 59.4	16 5.6	58 34.3	+1.90	58 57.1	+1.88	6 42.5	1.98	8.3
JUNE.									
25	15 49.8	15 54.3	57 59.1	1.37	58 15.5	1.36	4 40.1	1.94	5.7
26	15 58.7	16 3.0	58 31.7	1.34	58 47.6	1.30	5 27.0	1.98	6.7
27	16 7.2	16 11.1	59 3.0	1.25	59 17.5	1.17	6 15.6	2.08	7.7

[Extracts: Pages V–XII.]

GREENWICH MEAN TIME.

THE MOON'S RIGHT ASCENSION AND DECLINATION.

Hour.	Right Ascension.	Diff. for 1 m.	Declination.	Diff. for 1 m.
	h. m. s.	s.	° ′ ″	″
THURSDAY, APRIL 10.				
17	17 18 38.57	2.6448	S. 26 19 38.3	− 0.138
18	17 21 17.16	2.6414	26 19 41.1	+ 0.044
19	17 23 55.54	2.6379	S. 26 19 33.0	+ 0.225
WEDNESDAY, APRIL 16.				
4	22 12 47.08	1.8718	S. 8 12 37.4	+13.010
5	22 14 39.29	1.8685	7 59 36.1	13.032
6	22 16 31.30	1.8653	S. 7 46 33.5	+13.054
FRIDAY, APRIL 25.				
16	5 41 33.19	2.2558	N. 26 5 43.8	− 1.272
17	5 43 48.55	2.2562	26 4 23.5	1.405
18	5 46 3.93	2.2566	N. 26 2 55.2	− 1.537
TUESDAY, APRIL 29.				
11	9 2 56.23	2.1384	N. 15 27 3.6	−12.135
12	9 5 4.49	2.1369	15 14 52.7	12.227
13	9 7 12.66	2.1356	N. 15 2 36.3	−12.318

Hour.	Right Ascension.	Diff. for 1 m.	Declination.	Diff. for 1 m.
	h. m. s.	s.	° ′ ″	″
WEDNESDAY, MAY 28.				
6	10 19 4.23	2.0591	N. 7 4 18.5	−14.411
7	10 21 7.78	2.0592	6 49 52.4	14.459
8	10 23 11.34	2.0593	N. 6 35 23.4	−14.507
THURSDAY, JUNE 26.				
2	11 37 41.96	2.0743	S. 2 35 36.4	−15.135
3	11 39 46.49	2.0767	2 50 44.4	15.133
11	11 56 28.42	2.0989	S. 4 51 36.5	−15.069
MONDAY, DECEMBER 8.				
2	12 23 13.52	2.1615	S. 8 9 24.4	14.354
3	12 25 23.37	2.1668	8 23 44.9	14.328
4	12 27 33.54	2.1722	S. 8 38 3.8	14.302

[Extracts: Pages relating to Planets.]

GREENWICH MEAN TIME.

JUPITER.

April.

Day of Month.	Apparent Right Ascension. Noon.	Var. of R. A. for 1 Hour. Noon.	Apparent Declination. Noon.	Var. of Dec. for 1 Hour. Noon.	Meridian Passage.
	h. m. s.	s.	° ′ ″	″	h. m.
15	22 25 51.70	+1.834	—10 44 29.6	+10.10	20 50.0
16	22 26 35.54	1.819	10 40 28.0	10.03	20 46.8
17	22 27 19.02	1.804	10 36 28.1	9.96	20 43.6
18	22 28 2.14	+1.789	—10 32 30.0	+9.89	20 40.3

Day of the Month.	1st.	11th.	21st.	31st.
	″	″	″	″
Polar Semidiameter	16.4	16.7	17.1	17.5
Horizontal Parallax	1.5	1.6	1.6	1.6

September.

Day of Month.	Apparent Right Ascension. Noon.	Var. of R. A. for 1 Hour. Noon.	Apparent Declination. Noon.	Var. of Dec. for 1 Hour. Noon.	Meridian Passage.
	h. m. s.	s.	° ′ ″	″	h. m.
16	22 32 5.11	—1.134	—10 44 20.5	—6.58	10 49.8
17	22 31 38.03	—1.120	—10 46 57.2	—6.47	10 45.5

Day of Month.	1st.	11th.	21st.	31st.
	″	″	″	″
Polar Semidiameter	23.6	23.5	23.2	22.8
Horizontal Parallax	2.2	2.2	2.2	2.2

VENUS.

April.

Day of Month.	Apparent Right Ascension. Noon.	Var. of R. A. for 1 Hour. Noon.	Apparent Declination. Noon.	Var. of Dec. for 1 Hour. Noon.	Meridian Passage.
	h. m. s.	s.	° ′ ″	″	h. m.
24	4 19 14.43	+12.686	+22 40 33.2	+37.08	2 10.7
25	4 24 19.28	12.718	22 55 4.9	35.55	2 11.9
26	4 29 24.88	+12.748	+23 8 59.5	+34.00	2 13.0

Day of the month.	1st.	6th.	11th.	16th.	21st.	26th.
	″	″	″	″	″	″
Semidiameter	6.0	6.1	6.2	6.3	6.4	6.6
Hor. Parallax	6.2	6.3	6.4	6.5	6.7	6.8

MARS.

March.

Day of Month.	Apparent Right Ascension. Noon.	Var. of R. A. for 1 Hour. Noon.	Apparent Declination. Noon.	Var. of Dec. for 1 Hour. Noon.	Meridian Passage.
	h. m. s.	s.	° ′ ″	″	h. m.
17	20 5 56.83	+7.690	—21 13 58.1	+20.48	20 26.4
18	20 9 1.27	7.680	21 5 40.4	20.98	20 25.6
19	20 12 5.45	+7.669	—20 57 10.7	+21.48	20 24.7

NOTE.—North declinations are marked +, south declinations —.
+ prefixed to the hourly change of declination, indicates that north declinations are increasing and south declinations are decreasing; — indicates that north declinations are decreasing and south declinations increasing.

[Extracts: Pages relating to Fixed Stars.]

FIXED STARS.

MEAN PLACES FOR 1879.0. (Jan. 0 + d.016, Washington.)

Star's Name.	Magnitude.	Right Ascension.	An. Variation.	Declination.	An. Variation.
		h. m. s.	s.	° ′ ″	″
α Ursæ Min. (*Polaris*)*	2	1 14 24.861	+21.485	+88 39 49.92	+19.00
α Eridani (*Achernar*)	1	1 33 12.133	+ 2.233	−57 51 5.79	+18.40
α Tauri (*Aldebaran*)	1	4 28 58.716	+ 3.437	+16 15 53.35	+ 7.59
μ Geminorum	3	6 15 38.457	+ 3.633	+22 34 26.94	− 1.48
α Canis Maj. (*Sirius*)	1	6 39 48.935	+ 2.645	−16 33 4.30	− 4.68
α Virginis (*Spica*)	1	13 18 49.216	+ 3.154	−10 31 44.21	−18.90
α Bootis (*Arcturus*)	1	14 10 8.551	+ 2.735	+19 48 48.59	−18.87
α Scorpii (*Antares*)	1.2	16 21 59.432	+ 3.670	−26 9 41.94	− 8.34

* Circumpolar Star.

APPARENT PLACES FOR THE UPPER TRANSIT AT WASHINGTON.

α Ursæ Minoris. (*Polaris.*)			α Eridani. (*Achernar.*)			α Tauri. (*Aldebaran.*)		
Mean Solar Date.	Right Ascension.	Declination *North.*	Mean Solar Date.	Right Ascension.	Declination *South.*	Mean Solar Date.	Right Ascension.	Declination *North.*
	h. m. 1 13	° ′ +88 39		h. m. 1 33	° ′ −57 50		h. m. 4 28	° ′ +16 15
	s.	″		s.	″		s.	″
June 10.8	63.54	47.1	July 27.7	14.91 +.47	28.6 +0.5	Apr. 9.1	59.66 −.10	58.7 −0.2
11.8	64.35	47.0	Aug. 6.7	15.37 +.45	28.3 0.0	19.1	59.57 .07	58.6 −0.1
12.8	65.21	46.9				29.1	59.52 −.02	58.5 0.0

α Canis Majoris. (*Sirius.*)			α Virginis. (*Spica.*)			α Bootis. (*Arcturus.*)		
Mean Solar Date.	Right Ascension.	Declination *South.*	Mean Solar Date.	Right Ascension.	Declination *South.*	Mean Solar Date.	Right Ascension.	Declination *North.*
	h. m. 6 39	° ′ −16 32		h. m. 13 18	° ′ −10 31		h. m. 14 10	° ′ +19 48
	s.	″		s.	″		s. ″	″
(Dec. 30.5)	51.06 +.10	63.7 −2.5	Apr. 29.5	52.28 +.02	64.6 −0.1	May 9.4	11.71 +.02	32.1 +1.6
Jan. 9.5	51.14 +.05	66.1 −2.3	May 9.4	52.29 .00	64.7 0.0	19.4	11.71 −.01	33.7 +1.6
Apr. 9.2	50.09 −.18	76.2 +0.3	19.4	52.28 −.03	64.6 +0.1			
19.2	49.92 .16	75.8 0.6	29.4	52.24 .04	64.4 0.3			
29.2	49.77 .13	75.0 0.9	June 8.3	52.19 −.60	64.1 +0.4			
May 9.2	49.65 −.10	74.0 +1.1						

α Scorpii. (*Antares.*)		
Mean Solar Date.	Right Ascension.	Declination *South.*
	h. m. 16 21	° ′ −26 9
	s.	″
May 9.5	63.11 +.19	53.8 −0.5
19.5	63.28 .16	54.3 0.4
29.5	63.43 .12	54.7 0.4
June 8.5	63.53 .09	55.0 0.3
18.4	63.60 +.05	55.3 −0.3
July 28.3	63.49 −.10	56.0 0.0
Aug. 7.3	63.38 .13	55.9 +0.1
17.3	63.24 −.15	55.8 +0.2

APPENDIX II.

A COLLECTION OF FORMS FOR WORKING DEAD RECKONING AND VARIOUS ASTRONOMICAL SIGHTS, WITH NOTES EXPLAINING THEIR APPLICATION UNDER ALL CIRCUMSTANCES.

(The figures in parenthesis refer to the Notes following these forms.)

FORM FOR DAY'S WORK, DEAD RECKONING.

Time.	Compass Course.	Var.	Dev.	Lee-way.	Total error.	True Course.	Patent log.	Dist.	N.	S.	E.	W.	Diff.(1) Long.

	Latitude. ° ′		*Longitude.* ° ′	
Left at departure (or noon)	......	(2) N. *or* S.	......	(2) E. *or* W.
Run to......	......	N. *or* S.	......	E. *or* W.
By D. R. at......	......	N. *or* S.	......	E. *or* W.
Run to......	......	N. *or* S.	......	E. *or* W.
By D. R. at......	......	N. *or* S.	......	E. *or* W.

FORM FOR TIME SIGHT OF SUN'S LOWER LIMB (SUMNER LINE).

		h. m. s.
W. T.		....
C–W	+	....
Chro. t.		....
C. C.	±	....
(11) G. M. T.		....
(7) Eq. t.	±	....
G. A. T.		....

		° ′ ″
Obs. alt. ⊙		....
Corr.	±	....
h		....
		′ ″
(3) S. D.	+	....
(4) I. C.	+	....
	+	....
		′ ″
dip	−	....
$p.$ & $r.$	−	....
	−	....
		′ ″
Corr.	±	....

		° ′ ″	
(5) Dec.		....	N. *or* S.
		″	
H. D.	±	....	
		h.	
G. M. T.		....	
		′ ″	
Corr.	±	....	
		° ′ ″	
Dec.		....	N. *or* S.
		° ′ ″	
(6) p		....	

		m. s.
(5) Eq. t.		....
		s.
H. D.	±	....
		h.
G. M. T.		....
		s.
Corr.	±	....
		m. s.
Eq. t.		....

	° ′ ″		
h	....		
L_1	....	sec	....
p	....	cosec	....
	2)..........		
s_1	....	cos	....
s_1-h	....	sin	....
			2)..........
	h. m. s.		
G. A. T.	....		
L. A. T.$_1$	....	sin $\frac{1}{2}t_1$	....

(8) Long.$_1$ { h. m. s. .... / ° ′ ″ .... / .... } E. *or* W.

	° ′ ″		
(9) L_2	....	sec	....
		cosec	....
(10) s_2	....	cos	....
s_2-h	....	sin	....
			2)..........
	h. m. s.		
G. A. T.	....		
L. A. T.$_2$	....	sin $\frac{1}{2}t_2$	....

Long.$_2$ { h. m. s. .... / ° ′ ″ .... / .... } E. *or* W.

FORM FOR TIME SIGHT OF A STAR (SUMNER LINE).

		h. m. s.	
	W. T.	....	
	C–W	+	
	Chro. t.	....	
	C. C.	±	
(^{11})	G. M. T.	....	
	R. A. M. S.	+	
	Red. (Tab. 9)	+	
	G. S. T.	....	
	R. A. ✱	....	
(^{12})	H. A. from Gr.	....	E. *or* W.

		° ′ ″
	Obs. alt. ✱	....
	Corr.	± ....
	h	....
		′ ″
(^{4})	I. C.	+ ....
		′ ″
	dip	− ....
	ref.	− ....
		− ....
		′ ″
	Corr.	± ....

		h. m. s.	
	R. A.	....	
		° ′ ″	
	Dec.	....	N. *or* S.
		° ′ ″	
(^{6})	p	....	

		° ′ ″		
	h	....		
	L_1	....	sec	....
	p	....	cosec	....
		2)		
	s_1	....	cos	....
	$s_1 - h$	....	sin	....
		h. m. s.		2) ....
	Gr. H. A.	.... E. *or* W.		
(^{13})	H. A.$_1$	.... E. *or* W.	sin $\frac{1}{2} t_1$	....
(^{14})	Long.$_1$	h. m. s. .... ° ′ ″	E. *or* W.	

		° ′ ″		
(^{9})	L_2	....	sec	....
			cosec	....
(^{10})	s_2	....	cos	....
	$s_2 - h$	....	sin	....
		h. m. s.		2) ....
	Gr. H. A.	....		
	H. A.$_2$	....	sin $\frac{1}{2} t_2$	....
	Long.$_2$	h. m. s. .... ° ′ ″	E. *or* W.	

FORM FOR TIME SIGHT OF A PLANET (SUMNER LINE).

		h. m. s.	
	W. T.	....	
	C–W	+	
	Chro. t.	....	
	C. C.	±	
(^{11})	G. M. T.	....	
	R. A. M. S.	+	
	Red. (Tab.9)	+	
	G. S. T.	....	
	R. A. ✱	....	
(^{12})	H. A. from Gr.	....	E. *or* W.

		° ′ ″
	Obs. alt. ✱	....
	Corr.	± ....
	h	....
		′ ″
(^{15})	par.	+ ....
(^{4})	I. C.	+ ....
		+ ....
		′ ″
	dip	− ....
	ref.	− ....
		− ....
		′ ″
	Corr.	± ....

	h. m. s.
R. A.	....
	s.
H. D.	± ....
	h.
G. M. T.	....
	s.
Corr.	± ....
	h. m. s.
R. A.	....

		° ′ ″	
	Dec.	....	N. *or* S.
		″	
	H. D.	±	
		h.	
	G. M. T.	....	
		′ ″	
	Corr.	±	
		° ′ ″	
	Dec.	....	N. *or* S.
		° ′ ″	
(^{6})	p	....	

For the remainder of the work, by which the hour angles and thence the longitudes are found, employ the method given under "Form for Time Sight of a Star (Sumner Line)."

FORM FOR TIME SIGHT OF MOON'S LOWER LIMB (SUMNER LINE).

	h. m. s.
W. T.	....
C–W	+........
Chro. t.	....
C. C.	±........
(11) G. M. T.	....
R. A. M. S.	+........
Red. (Tab. 9)	+........
G. S. T.	....
R. A. ☾	....
(12) H.A. from Gr.	.... E. or W.

	° ′ ″
Obs. alt. ☾	....
	′ ″
(16) S. D.	+........
Aug.	+........
(4) I. C.	+........
	+........
	′ ″
dip	−........
	′ ″
1st corr.	±........
	° ′ ″
Approx. alt.	....
$p. \& r.$ (Tab. 24)	+........
h	....

	h. m. s.
(17) R. A.	....
	s.
M. D.	+........
	m.
No. min.	±........
	s.
Corr.	±........
	h. m. s.
R. A.	....

	° ′ ″
(17) Dec.	.... N. or S.
	″
M. D.	±........
	m.
No. min.	±........
	′ ″
Corr.	±........
	° ′ ″
Dec.	.... N. or S.
(6) p	....

For the remainder of the work, by which the hour angles and thence the longitudes are found, employ the method given under "Form for Time Sight of a Star (Sumner Line)."

FORM FOR MERIDIAN ALTITUDE OF SUN'S LOWER LIMB.

	° ′ ″
Obs. alt. ⨀	....
Corr.	± ....
h	....
	° ′ ″
(18) z	.... N. or S.
d	.... N. or S.
Lat.	.... N. or S.

	′ ″
(3) S. D.	+ ......
(4) I. C.	+ ......
	+ ......
	′ ″
dip	− ......
$p. \& r.$	− ......
	− ......
	′ ″
Corr.	± ......

	° ′ ″
(19) Dec.	.... N. or S.
	″
H. D.	± ....
	h.
Long.	± ....
	′ ″
Corr.	± ....
	° ′ ″
Dec.	.... N. or S.

FORM FOR MERIDIAN ALTITUDE OF A STAR.

	° ′ ″
Obs. alt. ✱	....
Corr.	± ....
h	....
(18) z	.... N. or S.
d	.... N. or S.
Lat.	.... N. or S.

	′ ″
(4) I. C.	+ ......
	′ ″
dip	− ......
ref.	− ......
	− ......
	′ ″
Corr.	± ......

	° ′ ″
Dec.	.... N. or S.

FORM FOR MERIDIAN ALTITUDE OF A PLANET.

	° ′ ″
Obs. alt. ✱	....
Corr.	± ....
h	....
	° ′ ″
(18) z	.... N. or S.
d	.... N. or S.
Lat.	.... N. or S.

	′ ″
(15) par.	+ ......
(4) I. C.	+ ......
	+ ......
	′ ″
dip	− ......
ref.	− ......
	− ......
	′ ″
Corr.	± ......

	h. m.
G. M. T., Gr. trans.	......
Corr. for Long.	± ......
L. M. T., local trans.	......
Long.	± ......
G. M. T., local trans.	......

	° ′ ″
Dec.	.... N. or S.
	″
H. D.	± ....
	h.
G. M. T.	....
	′ ″
Cor.	± ....
	° ′ ″
Dec.	.... N. or S.

FORM FOR MERIDIAN ALTITUDE OF MOON'S LOWER LIMB.

	° ′ ″	
h	....	
	° ′ ″	
(18) z	....	N. or S.
d	....	N. or S.
Lat.	....	N. or S.

	° ′ ″
Obs. alt. ☾	....
	′ ″
(16) S. D.	+ ....
Aug.	+ ....
(4) I. C.	+ ....
	+ ....
	′ ″
dip	− ....
	′ ″
1st corr	± ....
	° ′ ″
Approx. Alt.	....
$p.$ & $r.$ (Tab. 24)	+ ....
h	....

	h. m.
G. M. T., Gr. trans.	.....
Corr. for Long. (Tab. 11)	± .....
L. M. T., local trans.	.....
Long.	± .....
G. M. T., local trans.	.....

	° ′ ″	
(17) Dec.	....	N. or S.
	″	
M. D.	±	
	m.	
No. min.	±	
	′ ″	
Corr.	±	
	° ′ ″	
Dec.	....	N. or S.

ALTERNATIVE FORM FOR MERIDIAN ALTITUDE OF A BODY. (20)

	± 90° 00′ 00″	
(21) Dec.	±	
Corr.	±	
Constant	±	
Obs. alt.	±	
Lat.	....	N. or S.

Rules for signs.

Case I. Lat. & Dec. same name, Lat. greater	+ 90° + Dec. − Corr. − Alt.
Case II. Lat. & Dec. same name, Dec. greater	− 90° + Dec. + Corr. + Alt.
Case III. Lat. and Dec. opposite names	+ 90° − Dec. − Corr. − Alt.
Case IV. Lower transit	+ 90° − Dec. + Corr. + Alt.

FORM FOR LATITUDE SIGHTS OF SUN'S LOWER LIMB (SUMNER LINE).

	h. m. s.
W. T.	....
C–W	± ....
Chro. t.	....
C. C. ±	....
(11) G. M. T.	....
(7) Eq. t.	± ....
G. A. T.	....
Long.$_1$	± ....
L. A. T.$_1$	....
(22) t_1	h. m. s. .... ° ′ ″ ....
	h. m. s.
(23) Long.$_2$	± ....
L. A. T.$_2$	....
t_2	h. m. s. .... ° ′ ″ ....

	° ′ ″
Obs. alt. ☉	....
Corr.	± ....
h	....
	′ ″
(3) S. D.	+ ....
(4) I. C.	+ ....
	+ ....
	′ ″
dip	− ....
$p.$ & $r.$	− ....
	− ....
	′ ″
Corr.	± ....

	° ′ ″	
(5) Dec.	....	N. or S.
	″	
H. D.	±	
	h.	
G. M. T.	....	
	′ ″	
Corr.	±	
	° ′ ″	
Dec.	....	N. or S.

	m. s.
(5) Eq. t.	....
	s.
H. D.	± ....
	h.
G. M. T.	....
	s.
Corr.	± ....
	m. s.
Eq. t.	....

φ′ φ″ Method.

	° ′ ″		
t_1	....	sec	
d	....	tan	cosec .....
h	....		sin ....
(24) φ_1''	.... N. or S.	tan	sin ....
φ_1'	.... N. or S.		cos ....
Lat.$_1$	.... N. or S.		

	° ′ ″		
t_2	....	sec	
d	....	tan	cosec .....
h	....		sin ....
φ_2''	....	tan	sin ....
φ_2'	....		cos ....
Lat.$_2$	.... N. or S.		

Reduction to Meridian.

	″		
(25) a	....		
	° ′ ″		° ′ ″
h	....	h	....
(26) $a\,t_1{}^2$ ±	....	$a\,t_2{}^2$ ±	....
H_1	....	H_2	....
	° ′ ″		° ′ ″
(18) z_1	.... N. or S.	z_2	....
d	.... N. or S.	d	....
Lat.$_1$	.... N. or S.	Lat.$_2$	.... N. or S.

FORM FOR LATITUDE SIGHTS OF A STAR (SUMNER LINE).

		h. m. s.	
W. T.		....	
C–W	+	....	
Chro. t.		....	
C. C.	±	....	
(11) G. M. T.		....	
R. A. M. S.	+	....	
Red.(Tab.9)	+	....	
G. S. T.		....	
R. A.✱		....	
(12) H.A. from Gr.		....	E. *or* W.
(27) Long.$_1$		....	E. *or* W.
t_1		*h. m. s.* .... ° ′ ″	E. *or* W.
		h. m. s.	
(23) Long.$_2$		....	
t_2		*h. m. s.* .... ° ′ ″	

		° ′ ″
Obs. alt.✱		....
Corr.	±	....
h		....
		′ ″
(4) I. C.	+	....
		′ ″
dip	−	....
ref.	−	....
	−	....
		′ ″
Corr.	±	....

	h. m. s.	
R. A.	....	
	° ′ ″	
Dec.	....	N. *or* S.

For the remainder of the work, by which the latitudes are found from either the φ' φ'' formula or the reduction to the meridian, employ the methods given under "Form for Latitude Sights of Sun's Lower Limb (Sumner Line)."

FORM FOR LATITUDE SIGHTS OF A PLANET (SUMNER LINE).

		h. m. s.	
W. T.		....	
C–W	+	....	
Chro. t.		....	
C. C.	±	....	
(11) G. M. T.		....	
R. A. M. S.	+	....	
Red. (Tab. 9)	+	....	
G. S. T.		....	
R. A.✱		....	
(12) H. A. from Gr.		....	E. *or* W.
(27) Long.$_1$		....	E. *or* W.
t_1		*h. m. s.* .... ° ′ ″	E. *or* W.
		h. m. s.	
(23) Long.$_2$		....	
t_2		*h. m. s.* .... ° ′ ″	

		° ′ ″
Obs. alt. ✱		....
Corr.	±	....
h		....
		′ ″
(15) par.	+	....
(4) I. C.	+	....
	+	....
		′ ″
dip	−	....
ref.	−	....
	−	....
Corr.	±	....

		h. m. s.
R. A.		....
		s.
H. D.	±	....
		h.
G. M. T.		....
		s.
Corr.	±	....
		h. m. s.
R. A.		....

		° ′ ″	
Dec.		....	N. *or* S.
		″	
H. D.	±	....	
		h.	
G. M. T.		....	
		′ ″	
Corr.	±	....	
		° ′ ″	
Dec.		....	N. *or* S.

For the remainder of the work, by which the latitudes are found from either the φ' φ'' formula or the reduction to the meridian, employ the methods given under "Forms for Latitude Sights of Sun's Lower Limb (Sumner Line)."

FORM FOR LATITUDE SIGHTS OF MOON'S LOWER LIMB (SUMNER LINE).

	h. m. s.	
W. T.	....	
C–W	+..........	
Chro. t.	....	
C. C.	±..........	
(11) G. M. T.	....	
R. A. M. S.	+..........	
Red. (Tab. 9)	+..........	
G. S. T.	....	
R. A. ☾	....	
(12) H. A. from Gr.	....	E. or W.
(27) Long.$_1$	....	E. or W.
t_1	h. m. s. .... ° ′ ″	E. or W.
	h. m. s.	
Long.$_2$	....	E. or W
t_2	h. m. s. .... ° ′ ″	

	° ′ ″
Obs. alt. ☾	....
	′ ″
(16) S. D.	+........
Aug.	+........
(4) I. C.	+........
	+........
	′ ″
dip	−........
	′ ″
1st Corr.	±........
	° ′ ″
Approx. alt.	....
p. & r. (Tab. 24)	+........
	° ′ ″
h	......

	h. m. s.
(17) R. A.	....
	s.
M. D.	+........
	m.
No. min.	±........
	s.
Corr.	±........
	h. m. s.
R. A.	....

	° ′ ″	
(17) Dec.	....	N. or S.
	″	
M. D.	±.......	
	m.	
No. min.	±.......	
	′ ″	
Corr.	±.......	
	° ′ ″	
Dec.	....	N. or S.

For the remainder of the work, by which the latitudes are found from either the $\varphi' \varphi''$ formula or the reduction to the meridian, employ the methods given under "Forms for Latitude Sights of Sun's Lower Limb (Sumner Line)."

FORM FOR CHRONOMETER CORRECTION BY EQUAL ALTITUDES OF SUN.

	h. m. s.
W. T., A. M.	....
C–W	+..........
A. M. Chro. t.	....
P. M. Chro. t.	+..........
	2) ....
Mid. Chro. t.	....
Eq. eq. alt.	±..........
Chro. t. L. A. noon	....
(7) Eq. t.	±..........
Chro. t. L. M. noon	....
(29) Long.	±..........
(30) Chro. error on G. M. T.	±..........

	h. m. s.
W. T., P. M.	....
C–W	+..........
P. M. Chro. t.	....
A. M. Chro. t.	−..........
Elap. time	....
	m. s.
(28) Eq. t.	....
	s.
H. D.	±..........
	h.
Long.	±..........
	s.
Corr.	±..........
	m. s.
Eq. t.	....

	° ′ ″	
(28) Dec.	....	N. or S.
	″	
H. D. at merid.	±..........	
	h.	
Long.	±..........	
	′ ″	
Corr.	±..........	
	° ′ ″	
Dec.	....	N. or S.

	″
H. D. (prev. noon)	±..........
H. D. (foll. noon)	±..........
Diff. 24h	±..........
	″
Diff. 1h	±..........
	″
Diff. for long.	±..........
	″
H. D. at merid.	±..........

(31) Tab. 37		log A (±)....		log B (+)......
	″			
H. D.	±......	log (±)....		log (±)......
	° ′		° ′	
L	±......	tan (±)....	d ±......	tan (±)......
	s.			
1st pt.	±......	log (±)....		
2d pt.	±......			log (±)......
Eq. eq. alt.	±......			

FORM FOR FINDING THE TIME OF HIGH (OR LOW) WATER.

	d. h. m.
G. M. T. of Greenwich transit	....
(32) Corr. for Long. (Tab. 11)	±...........
L. M. T. of local transit	....
Lunitidal int. (App. IV)	+...........
L. M. T. of high (or low) water	....

NOTES RELATING TO THE FORMS.

1. It is not necessary to convert departure into difference of longitude for each course; it will suffice to make one conversion for the sum of all the departures used in bringing forward the position to any particular time.

2. In D. R. it will be found convenient to work Lat. and Long. in minutes and tenths, rather than in minutes and seconds.

3. If upper limb is observed, the correction for S. D. should be negative, instead of positive.

4. A positive I. C. has been assumed for illustration throughout the forms; if negative, it should be included with the *minus* terms of the correction.

5. For time sights and φ' φ'' sights, take Dec. and Eq. t. from Naut. Alm., p. II (G. M. noon).

6. To obtain p, subtract Dec. from 90° if of same name as Lat.; add to 90° if of opposite name.

7. Sign of Eq. t. that of application to *mean* time.

8. If G. A. T. is later than L. A. T., Long. is west; otherwise it is east.

9. If Lat. is exactly known, a second latitude need not be employed.

10. s_2 and s_2-h may be obtained by applying half the difference between L_1 and L_2, with proper sign, to s_1 and s_1-h, respectively.

11. The G. M. T. must represent the proper number of hours from noon, the beginning of the astronomical day; to obtain this it may be necessary to add 12^h to the Chro. t.

12. H. A. from Greenwich is the difference between G. S. T. and R. A., and should be marked W. if the former is greater; otherwise, E.

13. Local H. A. is marked E. or W., according as the body is east or west of the meridian at time of observation.

14. Subtract local hour angle from Greenwich hour angle to obtain longitude; that is, change name of local hour angle and combine algebraically.

15. The forms include a correction for the parallax of a planet, but in most cases this is small, and may be omitted. When used, take hor. par. from Naut. Alm. and reduce to observed altitude by Table 17. The semidiameter of a planet may be disregarded in sextant work if the *center* of the body is brought to the horizon line.

16. If upper limb is observed, the corrections for S. D. and Aug. should be negative, instead of positive.

17. R. A. and Dec. are to be picked out of Naut. Alm. for nearest hour of G. M. T., and to be corrected for the number of minutes and tenths.

18. Mark zenith distance N. or S. according as zenith is north or south of the body observed; mark Dec. according to its name, subtracting it from 180° for cases of lower transit; then, in combining the two for Lat., have regard to their names.

19. For meridian altitudes, take Dec. from Naut. Alm., p. I (G. A. noon).

20. This form enables "Constant" to be worked up before sight is taken, and gives latitude directly on completion of meridian observation. Longitude and altitude at transit must be known in advance with sufficient accuracy for correcting terms.

21. The details of obtaining Dec. at transit and correction for altitude are shown in the meridian altitude forms for each of the various bodies.

22. In an a. m. sight subtract L. A. T. from 24^h to obtain t; in a p. m. sight L. A. T. is equal to t.

23. If Long. is exactly known, a second longitude need not be employed.

24. Mark φ'' N. or S. according to name of Dec., and subtract it from 180° when body is nearer to lower than to upper transit; mark φ' N. or S. according as zenith is north or south of the body; then combine for Lat. having regard to the names.

25. Take a from Table 26 and at^2 from Table 27.

26. Add for upper, subtract for lower transits.

27. Subtract longitude from Greenwich hour angle to obtain local hour angle; that is, change name of longitude and combine algebraically.

28. For equal altitude sights, take Dec. and Eq. t. from Naut. Alm., p. I (G. A. noon).

29. Add longitude if east; subtract if west.

30. If *error* is +, the chronometer is fast, and the *correction* is subtractive; and the reverse.

31. Mark log A and log B as indicated in Table 37; mark N. Lat., N. Dec., and H. D. toward the north +, and the reverse. If, in combining the three logarithms for the respective parts of the equations, one or three of them should be *minus*, the sign of that part is *minus*; otherwise, *plus*.

32 Add for west, subtract for east longitude.

APPENDIX III.

EXPLANATION OF CERTAIN RULES AND PRINCIPLES OF MATHEMATICS OF USE IN THE SOLUTION OF PROBLEMS IN NAVIGATION.

DECIMAL FRACTIONS.

Fractions, or *Vulgar Fractions*, are expressions for any assignable part of a unit; they are usaually denoted by two numbers, placed one above the other, with a line between them; thus $\frac{1}{4}$ denotes the fraction one-fourth, or one part out of four of some whole quantity, considered as divisible into four equal parts. The lower number, 4, is called the *denominator* of the fraction, showing into how many parts the whole is divided; and the upper number, 1, is called the *numerator*, and shows how many of those equal parts are contained in the fraction. It is evident that if the numerator and denominator be varied in the same ratio the value of the fraction will remain unaltered; thus, if both the numerator and denominator of the fraction, $\frac{1}{4}$, be multiplied by 2, 3, 4, etc., the fractions arising will be $\frac{2}{8}$, $\frac{3}{12}$, $\frac{4}{16}$, etc., all of which are evidently equal to $\frac{1}{4}$.

A *Decimal Fraction* is a fraction whose denominator is always a unit with some number of ciphers annexed and the numerator any number whatever; as, $\frac{2}{10}$, $\frac{3}{100}$, $\frac{15}{1000}$, etc. And as the denominator of a decimal is always one of the numbers 10, 100, 1000, etc., the necessity for writing the denominator may be avoided by employing a point; thus, $\frac{3}{10}$ is written .3, and $\frac{14}{100}$ is written .14; the *mixed* number $3\frac{14}{100}$, consisting of a whole number and a fractional one, is written 3.14.

In setting down a decimal fraction the numerator must consist of as many places as there are ciphers in the denominator; and if it has not so many figures the defect must be supplied by placing ciphers before it; thus, $\frac{16}{100}=.16$, $\frac{16}{1000}=.016$, $\frac{16}{10000}=.0016$, etc. And as ciphers on the right-hand side of integers increase their value in a tenfold proportion, as 2, 20, 200, etc., so when set on the left hand of decimal fractions they decrease their value in a tenfold proportion, as .2, .02, .002, etc.; but ciphers set on the right hand of these fractions make no alteration in their value; thus, .2 is the same as .20 or .200.

The common arithmetical operations are performed the same way in decimals as they are in integers, regard being had only to the particular notation, to distinguish the integral from the fractional part of a sum.

Addition of Decimals.—Addition of decimals is performed exactly like that of whole numbers, placing the numbers of the same denomination under each other, in which case the separating decimal points will range straight in one column.

Examples.

	Miles.	Feet.	Inches.
Add:	26.7	1.26	272.3267
	32.15	2.31	.0134
	143.206	1.785	2.1576
	.003	2.0	31.4
Sum:	202.059	7.355	305.8977

Subtraction of Decimals.—Subtraction of decimals is performed in the same manner as in whole numbers, observing to set the figures of the same denomination and the separating points directly under each other.

Examples.

From:	31.267	36.75	1.254	1364.2
Take:	2.63	.026	.316	25.163
Difference:	28.637	36.724	.938	1339.037

Multiplication of Decimals.—Multiply the numbers together as if they were whole numbers, and point off as many decimals from the right hand as there are decimals in both factors together; and when it happens that there are not so many figures in the product as there must be decimals, then prefix such number of ciphers to the left hand as will supply the defect.

Example I.

Multiply 3.25 by 4.5.

```
          3.25
          4.5
         -----
          1.625
         13.00
Answer:  14.625
```

In one of the factors is one decimal, and in the other two; their sum, 3, is the number of decimals of the product.

Example II.

Multiply .17 by .06.

```
          .17
          .06
         -----
Answer:   .0102
```

In each of the factors are two decimals; the product ought therefore to contain 4; and, there being only three figures in the product, a cipher must be prefixed.

EXAMPLE III.

Multiply 0.5 by 0.7.

```
         0.5
         0.7
        ----
Answer:  0.35
```

EXAMPLE IV.

Multiply .18 by 24.

```
          .18
          24
         ----
          72
         36
         ----
Answer:  4.32
```

DIVISION OF DECIMALS.—Division of decimals is performed in the same manner as in whole numbers. The number of decimals in the quotient must be equal to the excess of the number of decimals of the dividend above those of the divisor; when the divisor contains more decimals than the dividend, ciphers must be affixed to the right hand of the latter to make the number equal or exceed that of the divisor.

EXAMPLE I.

Divide 14.625 by 3.25.

```
3.25 ) 14.625 ( 4.5
       1300
       ----
        1625
        1625
```

In this example there are two decimals in the divisor and three in the dividend; hence, there is one decimal in the quotient.

EXAMPLE II.

Divide 3.1 by .0062.

Previous to the division affix three ciphers to the right hand of 3.1, to make the number of decimals in the dividend equal the number in the divisor.

```
.0062 ) 3.1000 ( 500
        310
        ----
         000
```

EXAMPLE III.

Divide 17.256 by 1.16.

```
1.16 ) 17.25600 ( 14.875
       116
       ---
        565
        464
        ----
        1016
         928
         ----
          880
          812
          ----
           680
           580
           ---
           100
```

MULTIPLICATION OF DECIMALS BY CONTRACTION.—The operation of multiplication of decimal fractions may be very much abbreviated when it is not required to retain any figures beyond a certain order or place; this will constantly occur in reducing the elements taken from the Nautical Almanac from Greenwich noon to later or earlier instants of time.

In multiplying by this method, omit writing down that part of the operation which involves decimal places below the required order, but mental note should be made of the product of the first discarded figure by the multiplying figure, and the proper number of tens should be carried over to insure accuracy in the lowest decimal place sought.

EXAMPLE: Required the reduction for the sun's declination for $7^h.43$, the hourly difference being $58''.18$, where the product is required to the second decimal.

By ordinary method.	*By contraction.*
$58''.18$	$58''.18$
$7^h.43$	$7^h.43$
17454	1.74
23272	23.27
40726	407.26
$432''.2774$	$432.''27$

In the contracted method, for the multiplier .03 it is not necessary to record the product of any figures in the multiplicand below units; for the multiplier .4, none below tenths; but in each case observe the product of the left-hand one of the rejected figures and carry forward the number of tens.

REDUCTION OF DECIMALS.—To reduce a vulgar fraction to a decimal, add any number of ciphers to the numerator and divide it by the denominator; the quotient will be the decimal fraction. The decimal point must be so placed that there may be as many figures to the right hand of it as there were added ciphers to the numerator. If there are not so many figures in the quotient place ciphers to the left hand to make up the number.

EXAMPLE I.

Reduce $\frac{1}{50}$ to a decimal.

$$\begin{array}{r} 50)1.00 \\ \hline .02 \text{ Answer.} \end{array}$$

EXAMPLE II.

Reduce $\frac{3}{8}$ to a decimal.

$$\begin{array}{r} 8)3.000 \\ \hline .375 \text{ Answer.} \end{array}$$

EXAMPLE III.

Reduce 3 inches to the decimal of a foot.
Since 12 inches = 1 foot this fraction is $\frac{3}{12}$.

$$\begin{array}{r} 12)3.00 \\ \hline .25 \text{ Answer.} \end{array}$$

EXAMPLE IV.

Reduce 15 minutes to the decimal of an hour.
Since $60^m = 1^h$, this fraction is $\frac{15}{60}$.

$$\begin{array}{r} 60)15.00 \\ \hline .25 \text{ Answer.} \end{array}$$

EXAMPLE V.

Reduce $17^m\ 22^s$ to the decimal of an hour.

$$22^s = \frac{22^m}{60} = 0^m.37.$$

$$17^m.37 = \frac{17^h.37}{60} = 0^h.289 \text{ Answer.}$$

Any decimal may be reduced to lower denominations of the same quantity by multiplying it by the number representing the relation between the respective denominations.

EXAMPLE VI: Reduce 7.231 days to days, hours, minutes, and seconds.

$$\begin{array}{r} 0^d.231 \\ 24 \\ \hline 924 \\ 462 \\ \hline 5^h.544 \end{array} \qquad \begin{array}{r} 0^h.544 \\ 60 \\ \hline 32^m.640 \end{array} \qquad \begin{array}{r} 0^m.640 \\ 60 \\ \hline 38^s.400 \end{array} \qquad \text{Answer: } 7^d\ 5^h\ 32^m\ 38^s.4.$$

GEOMETRY.

Geometry is the science which treats of the description, properties, and relations of magnitudes, of which there are three kinds; viz, a *line*, which has only length without either breadth or thickness; a *surface*, comprehended by length and breadth; and a *solid*, which has length, breadth, and thickness.

A *point*, considered mathematically, has neither length, breadth, nor thickness; it denotes position simply.

A *line* has length without breadth or thickness.

A *surface* has length and breadth without thickness.

A *solid* has length, breadth, and thickness.

A *straight* or *right line* is the shortest distance between two points on a plane surface.

A *plane surface* is one in which, any two points being taken, the straight line between them lies wholly within that surface.

Parallel lines are such as are in the same plane and if extended indefinitely never meet.

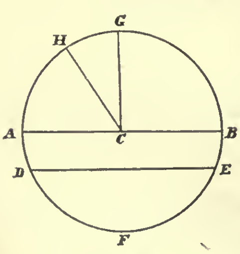


FIG. 65.

A *circle* is a plane figure bounded by a curve line of which every point is equally distant from a point within called the *center*. The bounding curve of the circle is called the *circumference*.

The *radius* of a circle, or *semi-diameter*, is a right line drawn from the center to the circumference, as AC (fig. 65); its length is that distance which is taken between the points of the compasses to describe the circle.

A *diameter* of a circle is a right line drawn through the center and terminated at both ends by the circumference, as ACB, its length being twice that of the radius. A diameter divides the circle and its circumference into two equal parts.

An *arc* of a circle is any portion of the circumference, as DFE.

The *chord* of an arc is a straight line joining the ends of the arc. It divides the circle into two unequal parts, called *segments*, and is a chord to them both; thus, DE is the chord of the arcs DFE and DGE.

A *semicircle*, or half circle, is a figure contained between a diameter and the arc terminated by that diameter, as AGB or AFB.

Any part of a circle contained between two radii and an arc is called a *sector*, as GCH.

A *quadrant* is half a semicircle, or one-fourth part of a whole circle, as CAG.

All circles are supposed to have their circumferences divided into 360 equal parts, called degrees; each degree is divided into 60 equal parts, called minutes; and each minute into 60 equal parts, called seconds; an arc is measured by the number of degrees, minutes, and seconds that it contains.

A *sphere* is a solid bounded by a surface of which every point is equally distant from a point within which, as in the circle, is called the *center*. Substituting *surface* for *circumference*, the definitions of the *radius* and *diameter*, as given for the circle, apply for the sphere.

An *angle* is the inclination of two intersecting lines, and is measured by the arc of a circle intercepted between the two lines that form the angle, the center of the circle being the point of intersection.

A *right angle* is one that is measured by a quadrant, or 90°. An *acute angle* is one which is less than a right angle. An *obtuse angle* is one which is greater than a right angle.

A *plane triangle* is a figure contained by three straight lines in the same plane.

When the three sides are equal, the triangle is called *equilateral;* when two of them are equal, it is called *isosceles.* When one of the angles is 90°, the triangle is said to be *right-angled.* When each angle is less than 90°, it is said to be *acute-angled.* When one is greater than 90°, it is said to be *obtuse-angled.* Triangles that are not right-angled are generally called *oblique-angled.*

A *quadrilateral* figure is one bounded by four sides. If the opposite sides are parallel, it is called a *parallelogram.* A parallelogram having all its sides equal and its angles right angles is called a *square.* When the angles are right angles and only the opposite sides equal, it is called a *rectangle.*

In a right-angled triangle the side opposite the right angle is called the *hypotenuse,* one of the other sides is called the *base*, and the third side is called the *perpendicular.* In any oblique-angled triangle, one side having been assumed as a base, the distance from the intersection of the other two sides to the base or the base extended, measured at right angles to the latter, is the perpendicular. In a parallelogram, one of the sides having been assumed as the base, the distance from its opposite side, measured at right angles to its direction, is the perpendicular. The term *altitude* is sometimes substituted for *perpendicular* in this sense.

Every section of a sphere made by a plane is a circle. A *great circle* of a sphere is a section of the surface made by a plane which passes through its center. A *small circle* is a section by a plane which intersects the sphere without passing through the center.

A great circle may be drawn through any two points on the surface of a sphere, and the arc of that circle lying between those points is shorter than any other distance between them that can be measured upon the surface. All great circles of a sphere have equal radii, and all bisect each other.

The extremities of that diameter of the sphere which is perpendicular to the plane of a circle are called the *poles* of that circle. In the case of a small circle the poles are named the *adjacent pole* and the *remote pole.* All circles of a sphere that are parallel have the same poles. All points in the circumference of a circle are equidistant from the poles. In the case of a great circle, the poles are 90° distant from every point of the circle.

Assuming any great circle as a *primary*, all great circles which pass through its poles are called its *secondaries.* All secondaries cut the primary at right angles.

Useful Formulæ Derived from Geometry.—In these formulæ the following abbreviations are adopted:

b, base of triangle or parallelogram.
h, perpendicular of triangle or parallelogram.
l, height of cylinder or cone.
π, ratio of diameter to circumference ($=3.141593$).
r, radius of sphere or circle.
d, diameter of sphere or circle.
A, major axis of ellipse.
a, minor axis of ellipse.
s, side of a cube.

Area of parallelogram $= b \times h$.
Area of triangle $= \frac{1}{2}\, b \times h$.
Area of any right-lined figure = sum of the areas of the triangles into which it is divided.
Sum of three angles of any triangle = 180°.
Circumference of circle $= 2\pi r$, or πd.

Area of circle $= \pi r^2$, or $\frac{\pi d^2}{4}$.

Angle subtended by arc equal to radius = 57°.29578.

Volume of sphere	$= \frac{\pi d^3}{6}$.
Surface of sphere	$= \pi d^2$, or $4\pi r^2$.
Area of ellipse	$= \frac{\pi A a}{4}$.
Volume of cube	$= s^3$.
Volume of cylinder	= Area of base $\times\, l$.
Volume of pyramid or cone	= Area of base $\times\, \frac{l}{3}$.

TRIGONOMETRIC FUNCTIONS.

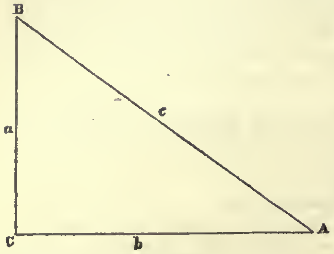


FIG. 66.

The *trigonometric functions* of the angle formed by any two lines are the *ratios* existing between the sides of a right triangle formed by letting fall a perpendicular from any point in one line upon the other line; no matter what point is chosen for the perpendicular nor which line, the ratios, and therefore the respective functions, will be the same for any given angle.

Let ABC (fig. 66) be a plane right triangle in which C is the right angle; A and B, the other angles; c, the hypotenuse; a and b the sides opposite the angles A and B, respectively. In considering the functions of the angle A, its opposite side, a, is regarded as the perpendicular and adjacent side, b, as the base; for the angle B, b is the perpendicular and a the base. Then the various ratios are designated as follows:

$\frac{a}{c}$, or $\frac{\text{perpendicular}}{\text{hypotenuse}}$, is called the *sine* of angle A, abbreviated sin A;

$\frac{b}{c}$, or $\frac{\text{base}}{\text{hypotenuse}}$, is called the *cosine* of angle A, abbreviated cos A;

$\frac{a}{b}$, or $\frac{\text{perpendicular}}{\text{base}}$, is called the *tangent* of the angle A, abbreviated tan A;

$\frac{b}{a}$, or $\frac{\text{base}}{\text{perpendicular}}$, is called the *cotangent* of the angle A, abbreviated cot A;

$\frac{c}{b}$, or $\frac{\text{hypotenuse}}{\text{base}}$, is called the *secant* of the angle A, abbreviated sec A;

$\frac{c}{a}$, or $\frac{\text{hypotenuse}}{\text{perpendicular}}$, is called the *cosecant* of the angle A, abbreviated cosec A;

1 — cosine A, is called the *versed sine* of A, abbreviated vers A.

1 — sine A, is called the *co-versed sine* of A, abbreviated covers A.

The following relations may be seen to exist between the various functions:

$$\frac{1}{\sin A} = 1 \div \frac{a}{c} = \frac{c}{a} = \text{cosec A};$$

$$\frac{1}{\cos A} = 1 \div \frac{b}{c} = \frac{c}{b} = \text{sec A};$$

$$\frac{1}{\tan A} = 1 \div \frac{a}{b} = \frac{b}{a} = \text{cot A};$$

$$\frac{\sin A}{\cos A} = \frac{a}{c} \div \frac{b}{c} = \frac{a}{b} = \text{tan A}.$$

Hence the cosecant is the reciprocal of the sine, the secant is the reciprocal of the cosine, the cotangent is the reciprocal of the tangent, and the tangent equals the sine divided by the cosine.

The *complement* of an angle is equal to 90° minus that angle, and thus in the triangle ABC the angle B is the complement of A. The *supplement* is equal to 180° minus the angle.

From the triangle ABC, regarding the angle B, we have:

$$\sin B = \frac{b}{c} = \cos A;$$

$$\tan B = \frac{b}{a} = \cot A;$$

$$\sec B = \frac{c}{a} = \text{cosec A}.$$

Hence it may be seen that the sine of an angle is the cosine of the complement of that angle; the tangent of an angle is the cotangent of its complement, and the secant of an angle is the cosecant of its complement.

The functions of angles vary in sign according to the quadrant in which the angles are located.

Let AA′ and BB′ (fig. 67) be two lines at right angles intersecting at the point O, and let that point be the center about which a radius revolves from an initial position OB, successively passing the points A, B′, A′. In considering the angle made by this radius at any position, P′, P″, P‴, P⁗, with the line OB, its position of origin, the functions will depend upon the ratios existing between the sides of a right triangle whose base, b, will always lie within BB,′ and whose perpendicular, a, will always be parallel to AA′, while its hypotenuse, c (of a constant length equal to that of the radius), will depend upon the position occupied by the radius. Now, if OB and OA be regarded as the positive directions of the base and perpendicular, respectively, and OB′ and OA′ as their negative directions, the sign of the hypotenuse being always positive, the sign of any function may be determined by the signs of the sides of the triangle upon which it depends.

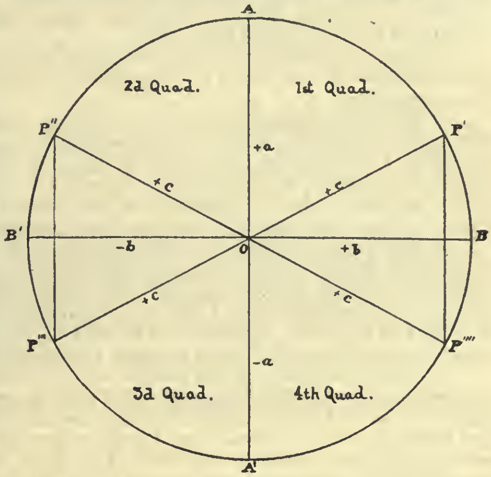


FIG. 67.

For example, the sine of the angle P″OB is $\frac{a}{c}$, and since a is positive the quantity has a positive value; its cosine is $\frac{b}{c}$, and as b is measured in a negative direction from O the cosine must therefore be negative.

In the first quadrant, between 0° and 90°, all quantities being positive, all functions will also be positive.

In the second quadrant, between 90° and 180°, sin A $\left(=\frac{a}{c}\right)$ is positive; cos A $\left(=\frac{b}{c}\right)$ has a negative value because b is negative; tan A $\left(=\frac{a}{b}\right)$ is also negative because of b. The cosecant, secant, and cotangent have, as in all cases, the same signs as the sine, cosine, and tangent, respectively, being the reciprocals of those quantities.

In the third quadrant, between 180° and 270°, sin A $\left(=\frac{a}{c}\right)$ and cos A $\left(=\frac{b}{c}\right)$ are both negative, because both a and b have negative values; tan A $\left(=\frac{a}{b}\right)$ is positive for the same reason.

In the fourth quadrant, between 270° and 360°, sin A $\left(=\frac{a}{c}\right)$ is negative, cos A $\left(=\frac{b}{c}\right)$ is positive, and tan A $\left(=\frac{a}{b}\right)$ is also negative.

From a consideration of the signs in the manner that has been indicated the following relations will appear:

$$\sin A = \sin (180° - A) = -\sin (180° + A) = -\sin (360° - A).$$
$$\cos A = -\cos (180° - A) = -\cos (180° + A) = \cos (360° - A).$$
$$\tan A = -\tan (180° - A) = \tan (180° + A) = -\tan (360° - A).$$
$$\sin A = \cos (90° - A) = -\cos (90° + A) = -\cos (270° - A) = \cos (270° + A).$$

Any similar relation may be deduced from the figure.

It is of great importance to have careful regard for the signs of the functions in all trigonometrical solutions.

LOGARITHMS.

In order to abbreviate the tedious operations of multiplication and division with large numbers, a series of numbers, called *Logarithms*, was invented by Lord Napier, by means of which the operation of multiplication may be performed by addition, and that of division by subtraction. Numbers may be involved to any power by simple multiplication and the root of any power extracted by simple division.

In Table 42 are given the logarithms of all numbers, from 1 to 9999; to each one must be prefixed an index, with a period or dot to separate it from the other part, as in decimal fractions; the numbers from 1 to 100 are given in that table with their indices; but from 100 to 9999 the index is left out for the sake of brevity; it may be supplied, however, by the general rule that the index of the logarithm of any

integer or mixed number is always one less than the number of integral places in the natural number. Thus, the index of the logarithm of any number (integral or mixed) between 10 and 100 is 1; from 100 to 1000 it is 2; from 1000 to 10000 it is 3, etc.; the method of finding the logarithms from this table will be evident from the rules that follow:

To find the logarithm of any number less than 100, enter the first page of the table, and opposite the given number will be found the logarithm with its index prefixed. Thus, opposite 71 is 1.85126, which is its logarithm.

To find the logarithm of any number between 100 and 1000, find the given number in the left-hand column of the table of logarithms, and immediately under 0 in the next column is a number, to which must be prefixed the number 2 as an index (because the number consists of three places of figures), and the required logarithm will be found. Thus, if the logarithm of 149 was required, this number being found in the left-hand column, against it, in the column marked 0 at the top (or bottom) is found 17319, prefixing to which the index 2, we have the logarithm of 149, 2.17319.

To find the logarithm of any number between 1000 and 10000, find the three left-hand figures of the given number in the left-hand column of the table of logarithms, opposite to which, in the column that is marked at the top (or bottom) with the fourth figure, is to be found the required logarithm, to which must be prefixed the index 3, because the number contains four places of figures. Thus, if the logarithm of 1495 was required, opposite to 149, and in the column marked 5 at the top (or bottom) is 17464, to which prefix the index 3, and we have the logarithm, 3.17464.

To find the logarithm of any number above 10000, find the first three figures of the given number in the left-hand column of the table, and the fourth figure at the top or bottom, and take out the corresponding logarithm as in the preceding rule; take also the difference between this logarithm and the next greater, and multiply it by the remaining figure or figures of the number whose logarithm is sought, pointing off as many decimal places in the product as there are figures in the multiplier. To facilitate the calculation of the proportional parts several small tables are placed in the margin, which give the correction corresponding to the difference, and to the *fifth* figure of the proposed number. Thus, if the logarithm of 14957 was required, opposite to 149, and under 5, is 17464; the difference between this and the next greater number, 17493, is 29; this multiplied by 7 (the last figure of the given number) gives 203; pointing off the right-hand figure gives 20.3 (or 20) to be added to 17464, which makes 17484; to this, prefixing the index 4, we have the logarithm sought, 4.17484. This correction, 20, may also be found by inspection in the small table in the margin, marked at the top 29; opposite to the *fifth* figure of the number, 7, in the left-hand column, is the corresponding correction, 20, in the right-hand column.

Again, if the logarithm of 1495738 was required, the logarithm corresponding to 149 at the left, and 5 at the top, is, as in the last example, 17464; the difference between this and the next greater is 29; multiplying this by 738 (the given number excluding the first four figures) gives 21402; crossing off the three right-hand figures of this product (because the number 738 consists of three figures), we have the correction 21 to be added to 17464; and the index to be prefixed is 6, because the given number consists of 7 places of figures; therefore the required logarithm is 6.17485. This correction, 21, may be found as above, by means of the marginal table marked at the top 29, taking at the side 7.38 (or $7\frac{1}{2}$ nearly), to which corresponds 21, as before.

To find the logarithm of any mixed decimal number, find the logarithm of the number, as if it were an integer, by the preceding rules, to which prefix the index of the integral part of the given number. Thus, if the logarithm of the mixed decimal 149.5738 was required, find the logarithm of 1495738, without noticing the decimal point; this, in the last example, was found to be 17485; to this prefix the index 2, corresponding to the integral part 149; the logarithm sought will therefore be 2.17485.

To find the logarithm of any decimal fraction less than unity, it must be observed that the index of the logarithm of any number less than unity is negative; but, to avoid the mixture of positive and negative quantities, it is common to borrow 10 in the index, which, in most cases, may afterwards be neglected in summing them with other indices; thus, instead of writing the index -1 it is written $+9$; instead of -2 we may write $+8$; and so on. In this way we may find the logarithm of any decimal fraction by the following rule: Find the logarithm of a fraction as if it were a whole number; see how many ciphers precede the first figure of the decimal fraction, subtract that number from 9, and the remainder will be the index of the given fraction. Thus the logarithm of 0.0391 is $8.59218-10$; the logarithm of 0.25 is $9.39794-10$; the logarithm of 0.0000025 is $4.39794-10$, etc. In most cases the writing of -10 after the logarithm may be dispensed with, as it will be quite apparent whether the logarithm has a positive or a negative index.

To find the number corresponding to any logarithm, seek in the column marked 0 at top and bottom the next smallest logarithm, neglecting the index; write down the number in the side column abreast which this is found and this will give the first three figures of the required number; carry the eye along the line until the next smallest logarithm to the given one is found, and the fourth figure of the required number will be at the top and bottom of the column in which this stands; take the difference between this next smallest logarithm and the next larger one in the table, and also the difference between the next smallest logarithm and the given one; entering the small marginal table which has for its heading the first-named difference and finding in the right-hand column of that table the last-named difference, there will appear abreast the latter, in the left-hand column, the fifth figure of the required number. Where it is desired to determine figures beyond the fifth for the corresponding number, the difference between the next lower logarithm and the given one may be divided by the difference between the next lower and next higher ones, and the quotient (disregarding the decimal point, but retaining any ciphers that may come between the decimal point and the significant figures) will be the fifth and succeeding figures of the number sought. Having found the figures of the corresponding number, point off from the left a number of figures which shall be one greater than the index number, and there place a decimal point. In this operation of placing the decimal point, proper account must be taken of the negative value of any index.

Thus, if the number corresponding to the logarithm 1.52634 were required, find 52634 in the column marked 0 at the top or bottom, and opposite to it is 336; now, the index being 1, the required number must consist of two integral places; therefore it is 33.6.

If the number corresponding to the logarithm 2.57345 were required, look in the column 0 and find in it, against the number 374, the logarithm 57287, and, guiding the eye along that line, find the given logarithm, 57345, in the column marked 5; therefore the mixed number sought is 3745, and since the index is 2, the integral part must consist of 3 places; therefore the number sought is 374.5. If the index be 1 the number will be 37.45, and if the index be 0 the number will be 3.745. If the index be 8, corresponding to a number less than unity, the number will be 0.03745.

Again, if the number corresponding to the logarithm 3.57811 were required, find, against 378 and under 5, the logarithm 57807, the difference between this and the next greater logarithm, 57818, being 11, and the difference between 57807 and the given number, 57811, being 4; in the marginal table headed 11, find in the right hand column the number 4, and abreast the latter appears the figure 4, which is the fifth figure of the required number; hence the figures are 37854; pointing off from the left $3+1=4$ places, the number is 3785.4.

If the given logarithm were 5.57811, since the index 5 requires that there shall be six places in the whole number, it is desirable to seek accuracy to the sixth figure. The logarithmic part being the same as in the example immediately preceding, it is found as before that the first four figures are 3785, the difference between the next lower and next greater logarithms is 11, and between the next lower logarithm and the given one is 4; divide 4 by 11 and the quotient is .36; drop the decimal point, annex and point off, and the number required is found to be 378536.

It may be remarked that in using five-place logarithm tables it is not generally to be expected that results will be exact beyond the fifth figure.

To show, at one view, the indices corresponding to mixed and decimal numbers, the following examples are given:

Mixed number.	*Logarithms.*	*Decimal number.*	*Logarithms.*
40943. 0	Log. 4. 61218	0. 40943	Log. 9. 61218 — 10
4094. 3	Log. 3. 61218	0. 040943	Log. 8. 61218 — 10
409. 43	Log. 2. 61218	0. 0040943	Log. 7. 61218 — 10
40. 943	Log. 1. 61218	0. 00040943	Log. 6. 61218 — 10
4. 0943	Log. 0. 61218	0. 000040943	Log. 5. 61218 — 10

To perform multiplication by logarithms, add the logarithms of the two numbers to be multiplied and the sum will be the logarithm of their product.

EXAMPLE I.

Multiply 25 by 35.

25	Log. 1. 39794
35	Log. 1. 54407
Product, 875	Log. 2. 94201

EXAMPLE II.

Multiply 22.4 by 1.8.

22. 4	Log. 1. 35025
1. 8	Log. 0. 25527
Product, 40. 32	Log. 1. 60552

EXAMPLE III.

Multiply 3.26 by 0.0025.

3. 26	Log. 0. 51322
0. 0025	Log. 7. 39794
Product, 0. 00815	Log. 7. 91116

EXAMPLE IV.

Multiply 0.25 by 0.003.

0. 25	Log. 9. 39794
0. 003	Log. 7. 47712
Product, 0. 00075	Log. 6. 87506

In the last example, the sum of the two logarithms is really 16.87506 — 20; this is the same as 6.87506 — 10, or, remembering that the quantity is less than unity, simply 6.87506.

To perform division by logarithms, from the logarithm of the dividend subtract the logarithm of the divisor; the remainder will be the logarithm of the quotient.

EXAMPLE I.

Divide 875 by 25.

875	Log. 2. 94201
25	Log. 1. 39794
Quotient, 35	Log. 1. 54407

EXAMPLE II.

Divide 40.32 by 22.4.

40. 32	Log. 1. 60552
22. 4	Log. 1. 35025
Quotient, 1.8	Log. 0. 25527

EXAMPLE III.

Divide 0.00815 by 0.0025.

0.00815	Log. 7. 91116
0.0025	Log. 7. 39794
Quotient, 3.26	Log. 0. 51322

EXAMPLE IV.

Divide 0.00075 by 0.025.

0.00075	Log. 6. 87506
0.025	Log. 8. 39794
Quotient, 0.03	Log. 8.47712

In Example III both the divisor and dividend are fractions less than unity, and the divisor is the lesser; consequently the quotient is greater than unity. In Example IV both fractions are less than unity; and, since the divisor is the greater, its logarithm is greater than that of the dividend; for this reason it is necessary to borrow 10 in the index before making the subtraction, that is, to regard the logarithm of .00075 as 16.87506 — 20; hence the quotient is less than unity.

The *arithmetical complement of a logarithm* is the difference between that logarithm and the logarithm of unity (10.00000—10, or 0.00000). It is therefore the logarithm of unity divided by that number which is the reciprocal of the number; and, since the effect of dividing by any number is the same as that of multiplying by its reciprocal, it follows that, in performing division by logarithms, we may either subtract the logarithm of the divisor or add the arithmetical complement of that logarithm. As the addition of a number of quantities can be performed in a single operation, while in subtraction the difference between only two quantities can be taken at a time, it is frequently a convenience to deal with the arithmetical complements rather than with the logarithms themselves.

EXAMPLE I.

Divide 875 by 25.

875		Log. 2.94201
25	Log. 1.39794	Colog. 8.60206
Quotient, 35		Log. 1.54407

EXAMPLE II.

Divide 0.00075 by 0.025.

0.00075		Log. 6.87506
0.025	Log. 8.39794	Colog. 1.60206
Quotient, 0.03		Log. 8.47712

EXAMPLE III.

Simplify the expression, $\dfrac{40.32 \times .00815}{22.4 \times .0025}$.

40.32		Log. 1.60552
.00815		Log. 7.91116
22.4	Log. 1.35025	Colog. 8.64975
.0025	Log. 7.39794	Colog. 2.60206
Result, 5.868		Log. 0.76849

To perform involution by logarithms, multiply the logarithm of the given number by the index of the power to which the quantity is to be raised; the product will be the logarithm of the power sought.

EXAMPLE I.

Required the square of 18.

18	Log. 1.25527
	2
Answer, 324	Log. 2.51054

EXAMPLE II.

Required the square of 6.4.

6.4	Log. 0.80618
	2
Answer, 40.96	Log. 1.61236

EXAMPLE III.

Required the cube of 13.

13	Log. 1.11394
	3
Answer, 2197	Log. 3.34182

EXAMPLE IV.

Required the cube of 0.25.

0.25	Log. 9.39794
	3
Answer, 0.015625	Log. 8.19382

In the last example, the full product of the multiplication of 9.39794—10 by 3 is 28.19382—30, which is equivalent to 8.19382—10.

To perform evolution by logarithms divide the logarithm of the number by the index of the power; the quotient will be the logarithm of the root sought. If the number whose root is to be extracted is a decimal fraction less than unity, increase the index of its logarithm by adding a number of tens which shall be less by one than the index of the power before making the division.

EXAMPLE I.

Required the square root of 324.

324	Log. 2) 2.51055
Answer, 18	Log. 1.25527

EXAMPLE II.

Required the cube root of 2197.

2197	Log. 3) 3.34183
Answer, 13	Log. 1.11394

EXAMPLE III.

Required the square root of 40.96.

40.96	Log. 2) 1.61236
Answer, 6.4	Log. 0.80618

EXAMPLE IV.

Required the cube root of 0.015625.

0.015625	Log. 8.19382
Add 20 to the index	3)28.19382
Answer, 0.25	Log. 9.39794

In the last example the logarithm 8.19382—10 was converted into its equivalent form of 28.19382—30, which, divided by 3, gives 9.39794—10.

To find the logarithm of any function of an angle, Table 44 must be employed. This table is so arranged that on every page there appear the logarithms of all the functions of a certain angle A, together with those of the angles 90°—A, 90°+A, and 180°—A; thus on each page may be found the logarithms of the functions of four different angles. The number of degrees in the respective angles are printed in bold-faced type, one in each corner of the page; the number of minutes corresponding appear in one column at the left of the page and another at the right; the names of the functions

to which the various logarithms correspond are printed at the top and bottom of the columns. The invariable rule must be to take the name of the function from the top or the bottom of the page, according as the number of degrees of the given angle is found at the top or bottom; and to take the minutes from the right or left hand column, according as the number of degrees is found at the right or left hand side of the page; or, more briefly, take names of functions and number of minutes, respectively, from the line and column nearest in position to the number of degrees.

Taking, as an example, the thirty-first page of the table, it will be found that 30° appears at the upper left-hand corner, 149° at the upper right-hand, 59° at the lower right-hand, and 120° at the lower left-hand corner. Suppose that it is desired to find the log. sine of 30° 10′; following the rule given, we find 10′ in the left-hand column and Sine at the top of the page, and abreast one and below the other is the required logarithm, 9.70115. But if the log. sine of 59° 10′ were sought, as 59° appears below and at the right of the page, the logarithm 9.93382 would be taken from the column marked Sine at the bottom and abreast 10′ on the right. It may also be seen that log. sin 30° 10′=log. cos 59° 50′=log. cos 120° 10′=log. sin 149° 50′=9.70115, the equality of the functions agreeing with trigonometrical deductions; (in this statement numerical values only are regarded, and not signs; the latter must, of course, be taken into account in all operations).

EXAMPLE I.

Required the log. sine, cosecant, tangent, cotangent, secant, and cosine of 28° 37′.

Log. sin	9.68029	Log. cot	10.26313
Log. cosec	10.31971	Log. sec	10.05658
Log. tan	9.73687	Log. cos	9.94342

EXAMPLE II.

Required the log. sine, cosecant, tangent, cotangent, secant, and cosine of 75° 42′.

Log. sin	9.98633	Log. cot	9.40636
Log. cosec	10.01367	Log. sec	10.60730
Log. tan	10.59364	Log. cos	9.39270

When the angle of which the logarithmic function is required is given to seconds, it becomes necessary to interpolate between the logarithms given for the even minutes next below and next above; this may be done either by computation or (except in a few cases) by inspection of the table.

To interpolate by computation, let n represent the number of seconds, D the difference between the logarithms of the next less and next greater even minute, and d the difference between the logarithm of the next less even minute and that of the required angle. Then,

$$d=\frac{n}{60}\times \mathrm{D}.$$

It should be noted when the number of seconds is 30, 20, 15, or some similar number, permitting the reduction of the fraction $\frac{n}{60}$ to a simple value, such as $\frac{1}{2}$, $\frac{1}{3}$, $\frac{1}{4}$, as the interpolation by this method may thus be made with greater facility.

Having obtained the difference of the logarithm from that of the next lower even minute, it must be applied in the proper direction—that is, if the function is such that its logarithm increases as the angle increases, the logarithmic difference must be added; but if it decreases, then that difference must be subtracted.

For example, let it be required to find the log. sin and log. cosec of 30° 10′ 19″. The log. sin of 30° 10′ is 9.70115; the difference between this logarithm and that of the sine of 30° 11′ (9.70137) is +22, which is D. Hence,

$$d=\frac{19}{60}\times(+22)=+7;$$

and the required logarithm is 9.70122. The log. cosec of 30° 10′ is 10.29885; the difference, D, between that and log. sin 30° 11′ (10.29863) is −22. In this case

$$d=\frac{19}{60}\times(-22)=-7;$$

therefore, log. cosec 30° 10′ 19″ = 10.29878.

The method of interpolating by inspection consists in entering that column marked "Diff." which is adjacent to the one from which the logarithmic function for the next lower minute is taken, and finding, abreast the number in the left-hand minute column which corresponds to the seconds, the required logarithmic difference; and the latter is to be added or subtracted according as the logarithms increase or decrease with an increased angle. Thus, if it be required to find log. sin 30° 10′ 19″, find as before log. sin 30° 10′ = 9.70115; then, in the adjacent column headed "Diff." and abreast the number of seconds, 19, in the left-hand minute column will be found 7, the logarithmic difference; add this, as the function is increasing, and we have the required logarithm 9.70122. If log. cosec 30° 10′ 19″ be sought, find log. cosec 30° 10′=10.29885; then in the adjacent difference column, which is the same as was used for the sines, find as before the logarithmic difference, 7; and since this function decreases as the angle increases, this must be subtracted; therefore, log. cosec 30° 10′ 19″ = 10.29878.

This method of interpolation by inspection is not available in that portion of the table where the logarithmic differences vary so rapidly that no values will apply alike to all the angles on the same page; on such pages the difference for one minute is given in a column headed "Diff. 1′," instead of the usual difference for each second; in this case, the interpolation must be made by computation, the given difference for one minute being D. In other parts of the table the interpolation by inspection may be liable to slight error because of the variation in logarithmic difference for different angles on the same page; but the tabulated values are sufficiently accurate for the usual calculations in navigation.

It will be evident that while the methods explained have contemplated entering the tables with a smaller angle and interpolating *ahead*, it would be equally correct to enter with a greater angle and interpolate *back* for the proper number of minutes, making the requisite change in the sign of the correction.

EXAMPLE I.

Required the log. sine, cosine, and tangent of 42° 57′ 06″.

	For 42° 57′	d	For 42° 57′ 06″.
Log. sin	9.83338	+ 1	9.83339
Log. cos	9.86448	− 1	9.86447
Log. tan	9.96890	+ 3	9.96893

EXAMPLE II.

Required the log. secant, cosecant, and cotangent of 175° 32′ 36″.

	For 175° 32′	d	For 175° 32′ 36″
Log. sec	10.00132	− 1	10.00131
Log. cosec	11.10858	+97	11.10955
Log. cot	11.10726	+98	11.10824

It should be observed that, for uniformity and convenience, all logarithms given in Table 44 have been increased by 10 in the index, and it is understood that −10 ought properly to be written after each; thus all logarithms under 10.00000 represent functions whose value is less than unity, and all over 10.00000 those greater than unity; for example, 11.10726 is the logarithm of a number in which the decimal point should be placed after the second figure from the left.

To find the angle corresponding to any logarithmic function, the process is the reverse of the one just described. Find, in the column marked with the name of the function, either at top or bottom, the two logarithms between which the given one falls; write down the degrees and minutes of the lesser of the two corresponding angles, which will be the degrees and minutes of the angle required. Call the difference between the two tabulated logarithms D, and the difference between the given logarithm and that which corresponds to the lesser angle, d; then if n represent the number of seconds, we have:

$$n = \frac{d}{D} \times 60.$$

Or, the same may be obtained by inspection (except where, as before explained, the differences for seconds are not tabulated) by finding, in the "Diff." column adjacent to that from which the logarithm was taken, the logarithmic difference, d, and noting the number of seconds abreast which it stands in the left-hand minute column.

Interpolation may be also made in the reverse direction from the next greater even minute.

Thus, if it be required to find the angle corresponding to log. sin 9.61400, we find log. sin 24° 16′, 9.61382, and log. sin 24° 17′, 9.61411; hence $D = 29$, and $d = 18$;

$$n = \frac{18}{29} \times 60 = 37;$$

and the angle is 24° 16′ 37″. Or, in adjacent column headed "Diff.," 18 would be found abreast 38, 39, or 40 (seconds) in the left-hand minute column—a correspondence sufficiently close for navigation work.

If the angle were known to be in the second quadrant, we find log. sin 155° 43′, 9.61411, and log. sin 155° 44′, 9.61382; here, $D = 29$, and $d = 11$;

$$n = \frac{11}{29} \times 60 = 23;$$

therefore, the angle is 155° 43′ 23″. Or, in adjacent "Diff." column find, abreast 11, 23 or 24 seconds.

EXAMPLE I.

Find angles less than 90° corresponding to log. cot 10.33621, log. sec 10.11579, and log. cos 8.70542.

		°	′	d	″
Log. cot	10.33621	24	45	8	15
Log. sec	10.11579	40	00	4	22
Log. cos	8.70542	87	05	116	28

EXAMPLE II.

Find angles in second quadrant corresponding to log. tan 10.15593, log. sin 8.87926, and log. cosec 10.04944.

		°	′	d	″
Log. tan	10.15593	124	55	19	42
Log. sin	8.87926	175	39	69	25
Log. cosec	10.04944	116	49	3	27

The Hour Columns in Table 44 give the measure in time corresponding to twice the angular distance given in arc. Thus, abreast the angle 13° 00′ stands in the P. M. column $1^h\ 44^m\ 00^s$, corresponding in time to $2 \times 13°\ 00'$, and in the A. M. column $10^h\ 16^m\ 00^s$, which is the same subtracted from 12^h. These columns are of use in working the various formulæ which involve functions of half the hour angle. Interpolation for values intermediate to those given in the tables is made on the same principle as for the angular measure; this operation may be performed by inspection by the use of the small tables at the bottom of each page, where n, the number of seconds of time, is given in bold-faced type, and d, the logarithmic difference for the respective columns, appears below.

EXAMPLE I.

Given $t = 1^h\ 48^m\ 44^s$, find log. cot $\frac{1}{2}\,t$.

For $1^h\ 48^m\ 40^s$,	log. cot. $\frac{1}{2}\,t$	10.61687
Diff. for 4^s, Col. B,	—	28
For $1^h\ 48^m\ 44^s$,	log. cot $\frac{1}{2}\,t$	10.61659

EXAMPLE II.

Given log. sin $\frac{1}{2}\,t$ 9.91394, find the Hour A. M. corresponding.

For 9.91389,		$4^h 39^m 12^s$
Diff. for 5, Col. C,	—	5
For 9.91394.		4 39 07

MISCELLANEOUS USEFUL DATA.

Earth's Polar radius=6,356,583.8 meters.	
Earth's Equatorial radius=6,378,206.4 meters.	
Earth's Compression$=\frac{1}{293.465}$.	
Earth's Eccentricity=0.0824846	log $\bar{8}$. 9163666.
Number of feet in one statute mile=5280	log 3. 7226339.
Number of feet in one nautical mile=6080.27	log 3. 7839229.
Sine of 1″=0.00000485	log 4. 6855749.
Sine of 1′=0.00029089	log 6. 4637261.
The Napierian base ε=2.7182818	log 0. 4342945.
The modulus of common logarithms=0.4342945	log 9. 6377843.
French meter in English feet, 3.2808333	log 0. 5159842.
French meter in English statute miles, 0.000621369	log 6. 7933496.
French meter in nautical miles, 0.000539593	log 6. 7320663.

1 pound Avoirdupois=7,000 grains Troy.
French gramme=0.00220606 Imperial pound Troy.
French kilogramme=0.0196969 English cwts.

Cubic inch of distilled water, in grains=252.458.	Bar. 30.00 in.; ther. 62° F.
Cubic foot of water, in ounces Troy=908.8488.	
Cubic foot of water, in pounds Troy=75.7374.	
Cubic foot of water, in ounces Avoirdupois=997.1366691.	
Cubic foot of water, in pounds Avoirdupois=62.3210606.	

Length of pendulum which vibrates second at Greenwich, 39.1393 inches.

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

The following table contains the latitude and longitude of a large number of places, together with lunitidal intervals and tidal ranges at the more important ones. It is arranged geographically and followed by an alphabetical index.

The geographical position generally relates to some specified exact location, and is based upon the best available authority. The tidal data relate to the waters adjacent to the point whose latitude and longitude are given, being abstracted from the Tide Tables published by the United States Coast and Geodetic Survey for the year 1903.

The high water and low water lunitidal intervals represent the mean intervals between the moon's transit and the time of next succeeding high and low waters throughout a lunar month. The spring and neap ranges are the differences in height between high water and low water at spring and at neap tides. For those places where the tide is chiefly of a diurnal type, and where there is usually but one high and one low water during a lunar day, the tidal values are bracketed; in such cases the lunitidal intervals are for the semi-diurnal part of the tide (which, however, is only appreciable for a few days when the moon is near the equator), and the range given in the column headed "Spg." does not, as in other cases, apply to the spring tide, but to the greatest periodic daily range, which usually occurs a day or two after the moon attains its extreme of declination, and is therefore near one of the tropics. As those places where the diurnal type predominates seldom experience large tidal effects, the general data furnished regarding such tides will suffice for the ordinary purpose of the navigator. The method of finding the time of high or low water from this table is illustrated in article 507, Chapter XX.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF NORTH AMERICA.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Labrador.	Salisbury Island: E. pt	63 27 00	76 30 00				
	Nottingham Island: S. pt	63 06 00	77 50 00	8 58	2 46	13.5	6.1
	Digges Island: W. extreme	62 37 00	78 08 00				
	Cape Wostenholme	62 35 00	77 33 00				
	Charles Island: E. pt	62 48 00	74 00 00				
	W. pt	62 50 00	75 20 00				
	Cape Weggs	62 30 00	74 03 00				
	Prince of Wales Sound: Center of ent	62 07 00	72 25 00				
	Cape of Hopes Advance	61 18 00	70 02 00				
	Akpatok Island: E. pt	60 10 00	67 05 00				
	Green Island: NE. pt	60 40 00	67 50 00				
	Button Islands: N. pt	60 52 00	64 40 00				
	Cape Chidleigh	60 33 00	64 12 00				
	Resolution Island: S. pt., Hutton h'dl'd	61 21 00	65 00 00				
	E. pt., C. Resolution	61 40 00	64 30 00				
	Black Head	60 00 00	64 28 00				
	Eclipse Harbor: E. side	59 48 00	64 07 15	8 00	1 48	5.0	2.0
	Nachvack Bay: Islands off entrance	59 07 00	63 20 00	7 00	0 48	5.2	2.1
	Saddle Island	57 35 00	61 20 00				
	Port Manvers: Entrance	57 00 00	62 07 00				
	Nain: Church	56 32 45	61 40 13	7 00	0 48	6.5	3.0
	Hopedale Harbor: Hill to E'd	55 27 04	60 12 34	5 30	11 43	6.9	3.2
	Aillick Harbor: Cape Mokkivik	55 13 33	59 08 01				
	Cape Harrison: N. extreme	54 55 50	57 56 40				
	Indian Harbor: Obs	54 26 55	57 12 40	6 10	12 23	7.0	3.2
	Outer Gannet Island: Summit	54 00 05	56 31 31				
	Gready Harbor	53 50 00	56 23 00				
	Cartwright Harbor: Caribou Castle	53 42 37	56 59 50				
	Indian Tickle: Summit	53 34 25	55 58 39	6 27	0 15	6.0	2.8
	Roundhill Island: Summit	53 26 00	55 35 48				
	Occasional Harbor: E. summit of Twin I.	52 40 07	55 44 29	6 38	0 26	5.0	2.3
	Cape St. Lewis: SE. pt	52 21 16	55 38 08	6 30	0 18	3.5	1.6
	Battle Islands: NE. extreme, SE. I	52 15 36	55 32 20				
	Table Head	52 06 00	55 41 00				
	Belle Isle: Light-house	51 53 00	55 22 10				
Newfoundland.	Cape Bauld: Light-house	51 38 48	55 25 12				
	Bell Island: S. end	50 42 10	55 35 30				
	Cape St. John: Gull Island light	49 59 54	55 21 33				
	Tilt Cove, Union Copper Mine	49 53 00	55 37 17				
	Funk Island: Summit	49 45 29	53 10 56				
	Offer Wadham: Light-house	49 35 40	53 45 00				
	Toulinguet Islands: Light-house	49 41 20	54 47 35				
	Seldom-come-by Harbor: Shiphill	49 36 50	54 12 00				
	Cape Freels: Gull I	49 15 20	53 25 12				
	Greenspond Island	49 04 20	53 37 45				
	Cape Bonavista: Light-house	48 42 01	53 04 42				
	Catalina Harbor: Green I. light-house	48 30 15	53 02 40				
	Bonaventure Head	48 16 55	53 23 35				
	Hearts Content: Light-house	47 53 10	53 23 20	7 23	1 11	4.1	1.9
	Baccalieu Island: Light-house	48 08 58	52 47 42				
	Harbor Grace: Light-house on beach	47 42 45	53 08 11	7 15	1 03	3.3	1.5
	Cape St. Francis: Light-house	47 48 30	52 47 20				
	St. Johns Harbor: Chain Rock Battery	47 34 02	52 40 54	7 12	1 01	3.3	1.5
	Cape Race: Light-house	46 39 24	53 04 30	6 50	0 38	6.5	3.0
	Cape Pine: Light-house	46 37 04	53 31 55				
	Trepassey Harbor: Shingle Neck	46 43 20	53 22 10	6 50	0 38	6.6	3.1
	Cape St. Mary: Light-house	46 49 34	54 11 42	8 20	2 08	7.2	3.3
	Little Placentia Harbor: W. side Coopers Cove	47 17 55	53 58 43				
	Burin Island: Light-house	47 00 26	55 08 49				
	Laun: Gr. Laun R. C. Church	46 56 30	55 32 00	8 05	1 53	7.0	3.2
	St. Pierre: U. S. Coast Survey Station	46 46 51	56 10 36	8 23	2 11	6.6	3.1
	Brunet Island: Mercers Hd. light-house	47 15 30	55 51 40	8 53	2 41	6.5	3.0
	Boar Islands: Burgeo I. light-house	47 35 13	57 36 52	8 22	2 10	6.2	2.9

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Newfoundland.	La Poile Bay: Gr. Espic Church	47 39 50	58 24 10	8 50	2 38	6.0	2.8
	Cape Ray: Light-house	47 37 00	59 18 00				
	Codroy Island: S. side Boat Harbor	47 52 30	59 23 40	8 50	2 32	4.3	2.1
	Cape St. George: Red I., SE. pt	48 33 48	59 13 10				
	Cow Head: NW. extreme	49 55 20	57 50 00	9 40	3 13	4.9	2.5
	Port Saunders: NE. point of entry	50 38 30	57 17 07				
	Rich Point: Light-house	50 41 39	57 24 20				
	Férolle Point: Cove Point, NE. extreme	51 02 10	57 02 40				
	Flower Cove: Capstan Pt	51 17 25	56 44 45				
	Green Island: 150 fms. from NE. end	51 24 10	56 33 40				
	Cape Norman: Light-house	51 38 00	55 53 52				
Labrador.	Chateau Bay: S. pt. Castle I	51 58 00	55 50 20				
	Amour Point: Light-house	51 27 35	56 51 05				
	Wood Island: S. pt	51 22 45	57 08 00				
	Greenly Island: Light-house	51 22 35	57 10 50				
	Bradore Bay: Obs. Spot, Jones Pt	51 27 30	57 14 12				
	Old Fort Island: Center	51 21 40	57 46 00				
	Great Mecatina Island: SE pt	50 47 30	58 51 00				
	Mecatina Harbor: S. point of Dead Cove	50 46 44	58 59 20				
	Little Mecatina I.: S. pt. C. McKinnon	50 31 40	59 20 00				
	St. Mary Reefs	50 14 00	59 45 00				
	South Makers Ledge	50 09 30	59 57 00				
R. and G. of St. Lawrence.	Cape Whittle	50 11 00	60 08 00				
	Natashquan Point: S. edge	50 06 00	61 44 00	1 25	6 45	4.0	2.0
	Clearwater Point: SW. extreme	50 12 27	63 27 03				
	Carousel Island: Light-house	50 05 40	66 22 44	1 43	7 05	8.1	6.0
	Point de Monts: Light-house	49 19 35	67 21 55	1 48	7 18	10.8	8.0
	Quebec: Mann's Bastion, Citadel	46 48 17	71 12 19	6 07	0 54	14.6	10.8
	Montreal: Cathedral	45 30 24	73 33 04				
	Father Point: Light-house	48 31 25	68 27 40	1 52	7 33	12.0	8.9
	Cape Chatte: Extreme	49 06 00	66 46 00	1 46	7 13	10.5	7.8
	Cape Magdalen: Light-house	49 15 40	65 19 30	1 33	6 50	6.4	4.7
	Cape Rosier: Light-house	48 51 37	64 12 00	1 25	6 40	5.5	4.1
	Cape Gaspé: Light-house	48 45 15	64 09 35				
	Anticosti Island: Heath Pt. light-house	49 05 20	61 42 30	1 20	6 35	3.6	1.8
	SW. pt. light-house	49 23 45	63 35 46	1 25	6 40	4.9	2.5
New Brunswick.	Bonaventure Island: E. pt	48 29 30	64 08 00				
	Leander Shoal	48 24 00	64 18 00				
	Macquereau Point	48 12 00	64 46 30	1 55	7 33	4.7	2.3
	Chaleur Bay: Carlisle	48 01 00	65 19 00	2 20	8 07	4.8	2.4
	Dalhousie I	48 04 24	66 22 10	3 10	9 10	8.1	4.1
	Miscou Island: NE. pt., Point Birch	48 01 00	64 29 00	2 00	8 25	4.0	2.0
	Miramichi Bay: Portage I., N. pt	47 14 00	65 02 00	4 16	10 59	2.3	1.2
	Point Escumenac: Light-house	47 05 00	64 47 33				
P. Edward I.	North Point: Light-house	47 03 46	63 59 19	4 20	11 00	2.4	1.2
	Richmond Harbor: Royalty Pt	46 34 00	63 43 00	5 15	11 55	1.8	0.9
	East Point: Light-house	46 27 15	61 58 05	8 17	2 20	1.4	0.7
	Charlottetown: Flag-staff on fort	46 13 55	63 07 23	11 07	4 23	6.4	3.2
Magdalen Is.	Gt. Bird Rock: Light-house	47 50 40	61 08 32				
	East Island: E. extreme	47 37 40	61 24 30				
	Entry Island: Light-house	47 16 30	61 41 20				
	Amherst Hbr.: N. side of entrance	47 14 23	61 49 38				
	Deadman Rock: W. pt	47 16 03	62 12 25				
	St. Paul Island: Light-house, NE. end	47 13 50	60 08 32	8 30	2 12	2.7	1.4
	Light-house, SW. end	47 11 20	60 09 50				
C. Breton I.	Cape North: Light-house	47 01 45	60 23 27	8 35	2 17	3.1	1.6
	St. Anns Harbor: E. pt. entrance	46 21 00	60 27 00	8 25	2 13	6.0	3.7
	Sydney Harbor: Light-house	46 12 25	60 12 50	8 10	2 05	5.0	3.1

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
C. Breton I.	Scatary Island: Light-house, NE. pt	46 02 15	59 40 25	......	......	......	......
	Louisburg: Light-house, NE. pt	45 54 34	59 59 26	7 45	1 35	5.0	3.1
	Madame Island: S. pt	45 28 00	61 03 00	7 55	1 47	5.0	3.1
	Port Hood: Just-au-corps I	46 00 00	61 36 00	9 05	2 47	3.5	1.8
	Sable Island: Light-house, E. end	43 58 14	59 46 08	......	......	......	......
Nova Scotia.	Pictou: Custom-house	45 40 50	62 42 10	9 34	3 13	3.9	2.0
	Cape St. George	45 52 00	61 52 00	9 20	3 00	2.8	1.4
	North Canso: Light-house, NW. entrance	45 41 42	61 29 10	9 26	3 10	3.1	1.6
	Arichat Harbor: R. C. Church steeple	45 30 48	61 01 47	7 55	1 47	5.0	3.1
	Cape Canso: Cranberry I., light-house	45 19 49	60 55 41	7 43	1 36	6.5	4.0
	White Head Island: Light-house	45 11 58	61 08 14	7 45	1 38	6.6	4.1
	Green Island: Light-house	45 06 15	61 32 40	......	......	......	......
	Wedge Island: Light-house	45 00 35	61 52 45	......	......	......	......
	Halifax: Dock-yard observatory	44 39 38	63 35 22	7 34	1 46	5.2	3.2
	Sambro Island: Light-house	44 26 10	63 33 30	......	......	......	......
	Margaret Bay: Shut-in I	44 34 00	63 54 00	7 32	1 30	7.1	4.4
	Tancook Island	44 29 00	64 06 00	......	......	......	......
	Lunenburg: Battery Pt. light	44 21 45	64 17 35	7 39	1 36	7.0	4.3
	Cape Le Havre: Black Rock	44 12 00	64 18 00	......	......	......	......
	Coffin Island: Light-house	44 02 00	64 37 30	......	......	......	......
	Little Hope Island: Light-house	43 48 30	64 47 15	......	......	......	......
	Shelburne Hbr.: Two lights, McNutts I.	43 37 15	65 15 45	......	......	......	......
	Cape Sable: Light-house	43 23 19	65 37 11	8 17	2 05	8.5	5.2
	Seal Island: Light-house	43 23 34	66 00 52	9 35	3 23	12.8	9.5
	Yarmouth: Cape Fourchu light	43 47 28	66 09 21	10 00	3 41	16.0	11.8
	Cape St. Mary	44 05 20	66 12 40	......	......	......	......
	Bryer Island: Light-house	44 14 57	66 23 38	10 29	4 36	20.8	15.4
	Annapolis Harbor: Prim Pt. light	44 41 34	65 47 20	10 49	4 41	27.5	20.4
	Haute Island: Light-house	45 14 55	65 00 45	11 07	5 27	33.0	24.4
	Cape Chignecto	45 19 00	64 57 00	......	......	......	......
	Burntcoat Head: Light-house	45 18 40	63 48 30	0 27	7 27	50.5	37.4
New Brunswick.	Cape Enragé: Light-house	45 35 34	64 46 55	......	......	......	......
	Cape Quaco: Light-house	45 19 30	65 32 00	11 21	5 56	30.0	22.2
	St. Johns: Partridge I. light	45 14 20	66 03 20	11 07	4 58	23.9	17.7
	Cape Lepreau: Light-house	45 03 40	66 27 40	11 04	5 26	24.5	18.2
	L'Etang Harbor: S. pt. tower	45 04 00	66 49 00	11 09	5 08	23.3	17.1
	St. Andrew: S. pt. light	45 04 06	67 02 52	11 00	5 00	24.9	18.2
	Campo Bello Island: Light-house, N. pt.	44 57 40	66 54 10	......	......	......	......
	Grand Manan Island: Light-house, NE. pt.	44 45 52	66 44 00	11 02	5 21	22.5	16.7
	Gannet Rock: Light-house, NE. pt	44 30 38	66 47 00	......	......	......	......
	Machias Island: Light-house	44 30 07	67 06 13	10 51	4 56	18.0	13.2
Maine.	Calais: Astronomical station	45 11 05	67 16 50	11 36	5 40	23.3	17.1
	Eastport: Cong. Church	44 54 15	66 59 14	11 09	5 05	20.9	15.2
	Quoddy Head: Light-house	44 48 55	66 57 04	......	......	......	......
	Machias: Town Hall	44 43 01	67 27 22	11 02	4 59	15.5	11.3
	Petit Manan Island: Light-house	44 22 03	67 51 51	......	......	......	......
	Bakers Island: Light-house	44 14 29	68 11 58	......	......	......	......
	Mount Desert Rock: Light-house	43 58 08	68 07 44	......	......	......	......
	Bangor: Thomas Hill	44 48 23	68 46 59	0 23	6 47	15.1	11.0
	Belfast: Methodist Church	44 25 29	69 00 19	11 35	5 22	11.7	8.6
	Rockland: Episcopal Church	44 06 06	69 06 52	11 09	4 55	11.0	8.1
	Matinicus Rock: Light-house	43 47 03	68 51 28	10 45	4 31	10.2	7.5
	Monhegan Island: Light-house	43 45 53	69 18 59	......	......	......	......
	Seguin Island: Light-house	43 42 26	69 45 32	......	......	......	......
	Bath: Winter St. Church	43 54 55	69 49 00	12 13	6 16	7.9	5.8
	Brunswick: College spire	43 54 29	69 57 44	......	......	......	......
	Augusta: Baptist Church	44 18 52	69 46 37	2 54	10 18	4.9	3.6
	Portland: Custom-house	43 39 28	70 15 18	11 06	4 51	10.1	7.3
	Portland Head light-house	43 37 23	70 12 30	......	......	......	......
	Cape Elizabeth: Light-house (west)	43 33 51	70 12 11	......	......	......	......
	Wood Island: Light-house	43 27 24	70 19 46	11 12	4 51	10.2	7.5
	Boon Island: Light-house	43 07 17	70 28 37	......	......	......	......

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
N. H.	Whale Back: Light-house	43 03 32	70 41 49	......	......	......	......
	Portsmouth: Navy-yard flagstaff	43 04 56	70 44 22	11 23	5 09	10.5	7.7
	Fort Constitution	43 04 16	70 42 34	......	......	......	......
	Hampton: Baptist Church	42 56 15	70 50 12	......	......	......	......
	Isles of Shoals: White I. light-house	42 58 02	70 37 25	11 19	4 58	10.0	7.3
Massachussts.	Newburyport: Academy	42 48 30	70 52 28	11 23	5 10	9.1	6.6
	Plum I. light-house	42 48 55	70 49 10	......	......	......	......
	Ipswich: Light-house (rear)	42 41 07	70 46 00	11 17	5 04	10.1	7.4
	Annisquam Harbor: Light-house	42 39 43	70 40 55	11 13	5 00	10.1	7.4
	Cape Ann: Thatchers I. light-house (N.)	42 38 21	70 34 31	......	......	......	......
	Gloucester: Universalist Church	42 36 46	70 39 59	......	......	......	......
	Ten-pound I. light-house	42 36 07	70 39 58	11 02	4 49	10.2	7.5
	Beverly: Hospital Pt. light-house	42 32 48	70 51 23	......	......	......	......
	Salem: Derbys Wharf light-house	42 31 00	70 53 03	11 16	5 03	10.6	7.7
	Marblehead: Light-house	42 30 20	70 50 03	11 09	4 57	10.6	7.7
	Cambridge: Harvard Observatory	42 22 48	71 07 43	......	......	......	......
	Boston: Navy-yard flagstaff	42 22 22	71 03 05	11 27	5 17	11.0	8.1
	State house	42 21 28	71 03 50	......	......	......	......
	Little Brewster I. light-house	42 19 41	70 53 26	11 09	4 56	10.9	8.0
	Minots Ledge: Light-house	42 16 11	70 45 35	......	......	......	......
	Plymouth: Pier head	41 58 44	70 39 12	......	......	......	......
	Gurnet light-house	42 00 12	70 36 04	11 23	5 11	10.8	7.9
	Barnstable: Light-house	41 43 20	70 16 52	11 36	5 25	11.6	8.5
	Cape Cod: Highlands light-house	42 02 23	70 03 40	......	......	......	......
	Chatham: Light-house (south)	41 40 17	69 57 01	12 11	5 57	4.6	3.4
	Monomoy Point: Light-house	41 33 34	69 59 39	12 00	5 48	4.3	3.1
	Nantucket: South Church	41 16 55	70 05 57	0 04	6 00	3.8	2.3
	Nantucket South shoal: Light ship	40 37 05	69 36 33	......	......	......	......
	Sankaty Head: Light-house	41 17 01	69 57 57	......	......	......	......
	Tarpaulin Cove: Light-house	41 28 08	70 45 29	7 51	1 51	2.8	1.7
	Vineyard Haven: W. Chop light-house	41 28 51	70 36 01	11 34	4 33	2.0	1.2
	Gay Head: Light-house	41 20 55	70 50 08	7 31	1 20	3.7	2.2
	Cuttyhunk: Light-house	41 24 52	70 57 01	7 36	0 59	4.3	2.6
	New Bedford: Baptist Church	41 38 10	70 55 36	7 57	1 18	5.2	3.1
Rhode Island.	Sakonnet Point: Light-house	41 26 30	71 13 30	7 40	1 05	4.5	2.6
	Beaver Tail: Light-house	41 26 58	71 24 00	7 40	1 09	4.7	2.8
	Newport: Flagstaff, torpedo station	41 29 07	71 19 40	7 48	1 00	4.4	2.6
	Bristol Ferry: Light-house	41 38 34	71 15 39	7 53	0 40	5.2	3.6
	Providence: Unitarian Church	41 49 26	71 24 19	8 12	0 57	5.4	3.4
	Point Judith: Light-house	41 21 40	71 28 55	7 32	1 17	3.8	2.3
	Block Island: Light-house (SE)	41 09 10	71 33 08	7 33	1 25	3.7	2.2
	Watch Hill Point: Light-house	41 18 14	71 51 32	8 49	2 38	3.2	2.1
Connecticut and New York.	Montauk Point: Light-house	41 04 16	71 51 27	8 20	2 03	2.3	1.5
	Stonington: Light-house	41 19 31	71 54 49	9 09	3 03	3.2	2.1
	New London: Groton Monument	41 21 16	72 04 47	9 26	3 32	2.9	1.9
	Little Gull Island: Light-house	41 12 23	72 06 26	9 26	3 04	3.0	2.0
	Gardners Island: Light-house, N. pt	41 08 29	72 08 44	9 40	3 35	2.5	1.7
	Plum Island: Light-house, W. pt	41 10 25	72 12 43	......	......	......	......
	Saybrook: Light-house, Lynde Pt	41 16 17	72 20 37	10 29	4 11	4.3	2.8
	New Haven: Yale College spire (middle)	41 18 28	72 55 45	11 08	4 54	7.0	4.9
	Bridgeport Harbor: Light-house	41 09 24	73 10 49	11 09	5 04	8.4	5.9
	Norwalk Island: Light-house	41 02 56	73 25 11	11 03	4 56	8.2	5.7
	Shinnecock Bay: Light-house	40 51 03	72 30 16	7 48	1 38	3.0	2.0
	Fire Island: Light-house	40 37 57	73 13 08	7 19	1 20	2.2	1.4
	Albany: Dudley Observatory	42 39 50	73 44 56	5 13	0 46	2.8	1.8
	New York: Navy-yard flagstaff	40 42 02	73 58 51	8 44	2 49	5.3	3.4
	City Hall	40 42 44	74 00 24	......	......	......	......
	Fort Wadsworth: Light-house	40 36 20	74 03 15	7 41	1 38	5.4	3.5

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
New Jersey, Delaware, Virginia, and Maryland.	Sandy Hook: Light-house (rear)	40 27 42	74 00 09	7 30	1 23	5.6	3.6
	Light-ship	40 28 15	73 50 09	......	......	......	......
	Navesink Highlands: N. light-house	40 23 48	73 59 10	......	......	......	......
	Barnegat Inlet: Light-house	39 45 52	74 06 24	7 50	1 43	2.7	1.7
	Tuckers Beach: Light-house	39 30 22	74 17 08	7 48	1 42	4.2	2.7
	Absecon Inlet: Light-house	39 21 59	74 24 52	9 59	3 57	4.7	3.0
	Five Fathom Bank: Light-ship	38 47 20	74 34 36	......	......	......	......
	Cape May: Light-house	38 55 59	74 57 39	8 16	1 47	5.6	3.6
	Philadelphia, Pa.: Statehouse	39 56 53	75 09 03	1 28	8 58	6.2	4.4
	Navy-yard flagstaff, League I	39 53 14	75 10 32	0 53	8 02	7.0	5.2
	Wilmington, Del.: Town hall	39 44 27	75 33 03	12 00	6 40	6.7	4.9
	Cape Henlopen: Light-house	38 46 42	75 05 03	8 17	1 50	5.4	3.5
	Assateague Island: Light-house	37 54 40	75 21 23	......	......	......	......
	Hog Island: Light-house	37 23 46	75 41 59	......	......	......	......
	Cape Charles: Light-house	37 07 22	75 54 24	8 03	2 19	3.0	2.0
	Baltimore: Washington Monument	39 17 48	76 36 59	6 34	0 44	1.4	1.0
	Annapolis: Naval Academy observatory	38 58 53	76 29 08	4 39	10 53	1.0	0.8
	Point Lookout: Light-house	38 02 19	76 19 20	0 31	6 52	1.7	1.1
	Washington, D. C.: Navy-yard flagstaff	38 52 30	76 59 45	7 42	1 56	3.5	2.5
	Naval Observatory	38 55 14	77 03 57	......	......	......	......
	Capitol dome	38 53 20	77 00 36	......	......	......	......
	Old Point Comfort: Light-house	37 00 06	76 18 24	8 44	2 17	3.0	2.0
	Norfolk: Navy-yard flagstaff	36 49 33	76 17 46	9 05	2 47	3.2	2.1
	Richmond, Va.: Capitol	37 32 16	77 26 04	4 30	11 55	4.3	2.8
	Cape Henry: Light-house	36 55 35	76 00 27	7 53	1 43	3.2	2.1
North Carolina.	Elizabeth City: Court-house	36 17 58	76 13 23	......	......	......	......
	Edenton: Court-house	36 03 24	76 36 31	......	......	......	......
	Currituck Beach: Light-house	36 22 36	75 49 51	7 37	1 26	3.4	2.2
	Bodie Island: Light-house	35 49 07	75 33 49	......	......	......	......
	Cape Hatteras: Light-house	35 15 17	75 31 16	......	......	......	......
	Ocracoke: Light-house	35 06 32	75 59 11	7 00	0 45	2.2	1.5
	Newbern, Episcopal spire	35 06 21	77 02 24	......	......	......	......
	Cape Lookout: Light-house	34 37 22	76 31 29	6 29	0 20	4.4	3.0
	Beaufort, N. C.: Court-house	34 43 05	76 39 48	7 21	1 08	3.3	2.3
	Frying-Pan Shoals: Light-ship	33 34 26	77 49 12	......	......	......	......
S. Carolina.	Georgetown: Episcopal Church	33 22 08	79 16 49	8 39	3 38	4.3	2.9
	Light-house, North I	33 13 21	79 10 55	......	......	......	......
	Cape Romain: Light-house	33 01 06	79 22 19	6 59	0 50	5.9	4.1
	Charleston: Light-house, Morris I	32 41 43	79 52 54	......	......	......	......
	St. Michael's Church	32 46 34	79 55 49	7 20	1 10	6.0	4.2
	Beaufort, S. C.: Episcopal Church	32 26 02	80 40 27	8 10	2 06	8.5	5.9
	Port Royal: Martins Industry light-ship	32 05 33	80 33 15	......	......	......	......
Georgia.	Tybee Island: Light-house	32 01 20	80 50 37	7 10	1 04	7.9	5.5
	Savannah: Exchange spire	32 04 52	81 05 26	8 13	3 07	7.6	5.3
	Sapelo Island: Light-house	31 23 28	81 17 01	7 30	1 24	8.4	5.8
	Darien: Winnowing House	31 21 54	81 25 39	7 40	1 44	7.5	5.2
	St. Simon: Light-house	31 08 02	81 23 30	7 30	1 27	7.5	5.3
	Brunswick: Academy	31 08 51	81 29 26	8 00	1 57	7.8	5.4
Florida.	Amelia Island: Light-house	30 40 23	81 26 26	......	......	......	......
	Fernandina: Astronomical station	30 40 18	81 27 47	7 39	1 31	6.9	4.8
	St. Johns River: Light-house	30 23 36	81 25 27	7 36	1 33	5.4	3.7
	Jacksonville: Methodist Church	30 19 43	81 39 14	......	......	......	......
	St. Augustine: Presbyterian Church	29 53 20	81 18 41	......	......	......	......
	Light-house	29 53 07	81 17 12	8 12	2 00	5.3	3.6
	Cape Canaveral: Light-house	28 27 37	80 32 30	8 00	1 52	5.9	4.0
	Jupiter Inlet: Light-house	26 56 54	80 04 48	8 00	2 00	1.8	1.2
	Fowey Rocks: Light-house	25 35 25	80 05 41	8 20	2 16	2.6	1.3
	Carysfort Reef: Light-house	25 13 17	80 12 40	8 21	2 08	2.7	1.4

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Florida.	Alligator Reef: Light-house	24 51 02	80 37 08	8 22	2 00	2.6	1.3
	Sombrero Key: Light-house	24 37 36	81 06 40	8 24	2 05	1.9	1.0
	Sand Key: Light-house	24 27 10	81 52 40	8 40	2 20	1.5	0.8
	Key West: Light-house	24 32 58	81 48 04	9 20	2 36	1.6	0.9
	Loggerhead Key: Light-house	24 38 04	82 55 42	9 44	3 21	1.4	0.8
	Sanibel Island: Light-house	26 27 11	82 00 43	12 17	6 10	2.3	1.2
	Gasparilla Island: Light-house	26 43 06	82 15 34	0 42	6 19	1.4	0.7
	Tampa Bay: Egmont Key light	27 36 04	82 45 40	11 32	5 07	1.8	0.9
	Cedar Keys: Ast. station, Depot Key	29 07 29	83 01 57	0 42	7 13	3.1	1.5
	Seahorse Key light	29 05 49	83 03 58				
	St. Marks: Fort St. Marks	30 09 03	84 12 42	2 00	8 30	2.6	1.2
	Apalachicola: Flag-staff	29 43 32	84 59 12	[12 10]	[5 35]	[2.5]	
	Cape St. George: Light-house	29 35 18	85 02 54				
	Cape San Blas: Light-house	29 40 00	85 21 30	[11 10]	[4 55]	[2.1]	
	Pensacola: Light-house	30 20 47	87 18 32				
	Navy-yard chimney	30 20 49	87 16 06	[11 28]	[4 20]	[1.7]	
Alabama, Mississippi, and Louisiana.	Sand Island: Light-house (front)	30 11 19	88 03 02				
	Mobile Point: Light-house	30 13 44	88 01 26	[11 25]	[3 09]	[1.5]	
	Mobile: Episcopal Church	30 41 26	88 02 28	[1 35]	[6 50]	[2.1]	
	Horn Island: Light-house	30 13 23	88 31 39	[12 00]	[5 40]	[2.0]	
	East Pascagoula: Coast-Survey station	30 20 42	88 32 45	[0 20]	[5 45]	[2.3]	
	Mississippi City: Coast-Survey station	30 22 54	89 01 57				
	Ship Island: Light-house	30 12 53	88 57 56				
	Cat Island: Light-house	30 13 57	89 09 41	[0 23]	[6 35]	[2.1]	
	Chandeleur: Light-house	30 02 58	88 52 19	[11 53]	[5 33]	[1.8]	
	Mouth Mississippi River: Pass a l'Outre light	29 11 30	89 02 28	[11 15]	[5 00]	[1.6]	
	S. Pass light (East Jetty)	28 59 28	89 08 08	[10 55]	[4 42]	[1.7]	
	SW. Pass light	28 58 22	89 23 30	[10 54]	[4 41]	[1.9]	
	New Orleans: United States Mint	29 57 46	90 03 28				
	Barataria Bay: Light-house	29 16 30	89 56 43	[11 00]	[4 47]	[2.1]	
	Timbalier Island: Light-house	29 02 49	90 21 25	[11 50]	[5 38]	[2.0]	
	Ship Shoal: Light-house	28 54 56	91 04 15	[0 18]	[6 33]	[2.2]	
	Southwest Reef: Light-house	29 23 36	91 30 14	[0 40]	[6 56]	[2.0]	
	Calcasieu Pass: Light-house	29 46 55	93 20 43	2 17	8 41	1.7	1.3
	Sabine Pass: Light-house	29 43 04	93 51 00	3 17	9 36	0.9	0.6
Texas.	Galveston: Cathedral, N. spire	29 18 17	94 47 26	[4 18]	[10 33]	[1.4]	
	Light-house, Bolivar Pt	29 22 05	94 46 00	[4 07]	[10 23]	[1.6]	
	Matagorda: Coast-Survey station	28 41 29	95 57 26				
	Light-house	28 20 18	96 25 28	[4 35]	[10 47]	[1.6]	
	Indianola: Coast-Survey station	28 32 28	96 31 01				
	Lavaca: Coast-Survey station	28 37 36	96 37 21				
	Aransas Pass: Light-house	27 51 53	97 03 23	[4 25]	[10 35]	[1.6]	
	Brazos Santiago: Light, S. end Padre I	26 04 16	97 10 00				
	Point Isabel: Light-house	26 04 36	97 12 28				
	Rio Grande del Norte: Obs. N. side of entrance	25 57 22	97 08 57	[1 55]	[8 03]	[1.4]	
Mexico.	San Fernando River: Entrance	25 23 40	97 21 25				
	Santander River: Entrance	23 46 20	97 46 55				
	Mount Mecate: Summit	22 38 40	98 04 55				
	Tampico: Light-house	22 15 50	97 49 55	[1 06]	[7 19]	[1.3]	
	Cape Roxo	21 35 00	97 22 00				
	Lobos Cay: Light-house	21 28 12	97 13 00				
	Tuspan Reefs: Middle islet	21 03 00	97 13 35				
	Mexico: National Observatory	19 26 01	99 06 39				
	Bernal Chico: Middle of islet	19 39 50	96 24 39				
	Zempoala Point: Extreme	19 27 26	96 20 22				
	Vera Cruz: San Juan d'Ulloa light	19 12 29	96 07 57	[2 49]	[8 38]	[2.4]	
	Sacrificios Island	19 10 10	96 05 30				
	Orizaba Mountain: 17,400 feet	19 04 00	97 15 55				
	Cofre de Perote Mount: 14,000 feet	19 29 30	97 07 30				
	Alvarado: E. side of entrance	18 49 00	95 44 48				
	Roca Partida: Summit	18 44 00	95 11 14				
	Tuxtla, volcano: Summit	18 29 00	95 08 00				
	Montepio: Landing place	18 40 00	95 05 12				

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Mexico.	Zapotitlan Point: Light-house	18 34 00	94 50 00				
	San Juan Point: Light-house	18 19 45	94 38 57				
	Coatzacoalcos: Light-house	18 08 56	94 24 46				
	Santa Ana Lagoon: Entrance	18 18 49	93 51 53				
	Tupilco River: Entrance	18 26 44	93 25 25				
	Tabasco River: Light-house	18 39 30	92 42 00				
	Carmen Island: NE. pt	18 47 08	91 30 50				
	Laguna de Terminos: Vigia tower, W. end Carmen I	18 38 44	91 50 17	[12 16]	[6 00]	[1.6]	
Yucatan.	Paypoton Mount: Summit	19 38 00	90 43 27				
	Lerma: Church	19 48 24	90 36 11				
	Campeche: Light-house	19 50 20	90 32 20	2 59	9 28	2.1	1.3
	Fort San José	19 51 36	90 30 51				
	Point Palmas	21 02 00	90 22 00				
	Sisal: Fort light	21 10 06	90 02 37	10 20	4 10	1.8	0.9
	Madagascar Reef: Center	21 26 30	90 18 27				
	Progreso: Light-house	21 17 00	89 39 30				
	Silan: Village	21 23 00	88 54 27				
	Lagartos: Village	21 36 30	88 10 27				
	Cape Catoche: Light-house	21 35 50	87 04 10	9 30	3 19	1.5	0.8
	Arcas Cays: Light-house	20 12 45	91 57 45	[12 06]	[5 50]	[1.6]	
	Obispo Shoal: 16-foot spot	20 29 00	92 13 27				
	New Bank: Center	20 32 00	91 52 27				
	Triangles, E. reef: Beacon	20 54 54	92 12 47	[12 00]	[5 45]	[1.6]	
	Triangles, W. reef: Cay at SW. end	20 58 00	92 18 57				
	Bajo Nuevo Reef: Center	21 50 00	92 04 26				
	Arenas Cays: NW. Cay	22 07 10	91 24 21				
	Alacran Reef: Perez Cay	22 23 36	89 41 45				
	Contoy Island: Light-house	21 33 00	86 48 00				
	Mugeres Island: Light-house	21 12 00	86 43 39	9 20	3 08	1.6	0.9
	Cancun Island: Nisuc Pt	21 03 00	86 46 45				
	Cozumel Island: N. pt. light-house	20 35 50	86 43 55	8 20	2 08	1.5	0.8
	S. pt. light-house	20 16 20	86 59 04				
	Ascension Bay: Allen Pt	19 46 55	87 28 27				
	Chinchorro Bank: Cayo Lobos light	18 23 20	87 23 40				
Belize.	Half-Moon Cay: Light-house	17 12 15	87 32 30				
	Mauger Cay, NW. end: Light-house	17 36 15	87 46 30				
	Glover Reef: SW. Cay	16 42 20	87 50 50				
	English Cay: Light-house	17 19 30	88 03 20				
	St. Georges Cay: Center	17 33 15	88 04 45				
	Sand-Fly Cays: Hut, S. end	16 57 50	88 06 05				
	South Water Cay: Center	16 48 50	88 05 36				
	Belize: Fort George light	17 29 20	88 11 20	8 00	1 50	1.5	0.8
	North Standing Creek: Entrance	16 57 40	88 13 48				
	Sittee Point: Cay	16 47 45	88 15 15				
	Cockscomb Mount: Summit, 4,000 feet	16 48 10	88 37 40				
	Placentia Point: Huts on point	16 30 54	88 22 13				
	Icacos Point: S. extreme	16 14 15	88 35 51				
	Sarstoon River: Entrance	15 54 00	88 56 20				
Guat.	Dulce River: Entrance, W. side	15 49 45	88 46 22	9 00	2 50	2.0	1.1
	Dulce Gulf: Fort St. Philip	15 38 00	89 01 36				
	Isabel	15 24 20	89 09 44				
Honduras.	Hospital Bight: Hut, N. pt. of entrance	15 52 20	88 33 22				
	Cape Three Points: NW. extreme	15 57 45	88 38 50				
	Seal Cays: S. Cay	16 08 00	88 20 15				
	Omoa: Entrance	15 47 11	88 04 31				
	Cape Triunfo: Bluff pt	15 48 45	87 27 46				
	Congrehoy Peak: Summit, 8,040 feet	15 38 00	86 55 00				
	Truxillo: Fort	15 55 45	85 59 18				
	Utilla Island: S. Cay	16 03 40	86 59 15				
	Hog Islands: Highest hill on W. islet	15 58 00	86 32 09				
	Roatan: Center of Coxen Cay	16 18 00	86 34 27	7 35	1 23	3.5	1.8
	Port Royal, NW. pt. of George Cay	16 24 20	86 18 41				
	Bonacca Island: Summit, 1,200 feet	16 28 00	85 55 00	8 50	2 38	1.5	0.8
	Misteriosa Bank: S. Point	18 44 00	84 02 00				
	Swan Islands: NW. pt. of W. I	17 24 30	83 56 27				

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Honduras.	Great Rock Head: Bluff extreme	15 53 00	85 27 10	......	......	......	......
	Cape Camaron	16 00 00	85 03 00	......	......	......	......
	Brewers Lagoon: E. side of entrance	15 51 50	84 38 33	......	......	......	......
	Patook River: E. side of entrance	15 48 50	84 17 10	......	......	......	......
	Carataska Lagoon: E. side of entrance	15 23 40	83 42 36	......	......	......	......
Nicaragua.	Cape Gracias-á-Dios: Light-house	15 00 00	83 10 00	10 20	4 07	2.0	1.1
	Caxones Reef: Great Hobby Islet	16 03 30	83 08 20	......	......	......	......
	Gorda Bank: Gorda Cay	15 52 00	82 23 27	......	......	......	......
	Farrall Rock: Center	15 51 00	82 18 07	......	......	......	......
	Half-Moon Cay: Center	15 08 50	82 42 08	......	......	......	......
	Alargate Reef: E. pt	15 07 00	82 20 00	......	......	......	......
Mosquito Coast.	Mosquito Cays: S. end	14 21 12	82 45 57	......	......	......	......
	Rosalind Bank: NW. extreme	16 54 00	80 51 27	......	......	......	......
	Serranilla Bank: Beacon Cay	15 47 45	79 50 53	4 00	10 13	2.0	1.1
	Serrana Bank: Little Cay	14 21 33	80 15 20	4 00	10 13	2.0	1.1
	Quita Sueño Bank: S. extreme of reef	14 08 00	81 08 21	......	......	......	......
	Spit at NW. end	14 30 00	81 07 21	......	......	......	......
	Roncador Cay: S. pt	13 34 30	80 05 05	......	......	......	......
	Old Providence: Isabel House	13 22 54	81 21 26	4 00	10 13	1.0	0.5
	St. Andrews Island: SW. cove, Entrance I.	12 31 40	81 43 06	......	......	......	......
	Courtown Cays: Middle Cay	12 24 00	81 27 53	......	......	......	......
	Albuquerque Bank: Smith Cay	12 10 00	81 49 54	......	......	......	......
	Brangmans Bluff: Extreme	14 03 00	83 21 27	......	......	......	......
	Pearl Cays: Colombilla Cay	12 22 35	83 23 10	1 50	8 03	2.0	1.1
	Pearl Cays Lagoon: Mosquito Pt	12 20 39	83 37 12	......	......	......	......
	Cookra Hill: Summit	12 15 30	83 45 57	......	......	......	......
	Bluefields: Schooner Pt	11 59 00	83 41 57	1 40	7 52	2.0	1.1
	Little Corn Island: Gun Pt	12 17 30	82 58 35	......	......	......	......
	Great Corn Island: Wells N. of Quin Bluff	12 09 17	83 03 35	1 35	7 47	2.0	1.1
	Greytown: Light-house	10 56 15	83 42 15	1 00	7 13	1.5	0.8
C. R.	Mount Cartago: Peak, 11,100 feet	10 01 30	83 47 27	......	......	......	......
	Port Limon: Grape Cay light	10 00 05	83 02 00	1 00	7 13	1.6	0.9
Colombia.	Carreta Point: Extreme	9 38 30	82 39 06	......	......	......	......
	Tirby Point: Extreme	9 25 45	82 21 47	......	......	......	......
	Columbus Island: Lime Pt	9 24 47	82 20 31	......	......	......	......
	Blanco Peak: Summit, 11,740 feet	9 16 30	83 03 27	......	......	......	......
	Shepherd Island: Hut on summit	9 14 22	82 20 33	......	......	......	......
	Cobbler Rock: Center	9 14 30	82 07 51	......	......	......	......
	Valiente Peak: Summit, 722 feet	9 10 30	81 55 02	......	......	......	......
	Escudo de Veragua: W. pt. of island	9 06 30	81 33 57	......	......	......	......

WEST COAST OF NORTH AMERICA.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
Alaska.	Point Barrow: Highest lat. of U. S	71 23 30	156 27 00	11 41	5 33	0.6	0.2
	Icy Cape: Extreme	70 16 00	161 47 30	......	......	......	......
	Cape Lisburne: 849 feet	68 52 00	166 06 00	......	......	......	......
	Cape Krusenstern: Extreme	67 09 00	163 34 00	......	......	......	......
	Chamisso Island: Summit	66 14 30	161 45 00	7 45	1 50	2.0	0.6
	Cape Espenberg: Extreme	66 32 00	163 36 00	......	......	......	......
	Diomede Island: Fairway Rock	65 35 30	168 40 00	......	......	......	......
	Cape Prince of Wales: W. pt	65 33 30	168 00 00	......	......	......	......
	Port Clarence: Point Spencer	65 16 40	166 46 30	6 10	1 10	1.1	0.9
	King Island: N. pt	65 00 00	168 02 00	......	......	......	......
	Cape Nome: Extreme	64 26 00	165 05 00	[2 05]	[8 25]	[2.1]	......
	St. Michael: Fort	63 26 00	162 02 30	[8 05]	[1 20]	[4.5]	......
	Stuart Island: W. pt	63 34 30	162 42 30	......	......	......	......
	Cape Romanzof: Extreme	61 40 00	166 15 00	......	......	......	......
	St. Lawrence Island: E. pt	63 16 00	168 41 00	......	......	......	......
	NW. pt	63 50 00	171 31 00	......	......	......	......
	St. Matthew Island: SE. pt	60 18 00	172 02 00	4 40	11 0	3.1	1.6
	Pinnacle Islet: Summit, 930 feet	60 13 00	172 36 00	......	......	......	......
	Nunivak Island: Cape Etolin	60 25 22	166 08 30	......	......	......	......
	Hagenmeister Island	58 48 31	160 50 00	......	......	......	......

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Alaska.	Cape Menchikof: Extreme	57 30 24	157 58 30	....	....	......	.....
	Port Moller	55 54 59	160 34 54	....	....	......	.....
	St. George Island: S. side	56 34 23	169 39 50	....	....	......	.....
Aleutian Islands.			Long. E.				
	Attu Island: Chichagof Harbor	52 56 01	173 12 24	3 35	9 48	5.7	2.9
	Kiska Island: Kiska Harbor, Ast. sta	51 59 04	177 30 00	3 30	9 43	5.2	2.7
	Amchitka Island: Constantine Harbor	51 23 39	179 12 06	....	....	......	.....
			Long. W.				
	Adakh Island: Bay of Islands	51 49 18	176 52 00	3 25	9 38	5.0	2.6
	Atka Island: Nazan Bay (church)	52 10 36	174 15 18	....	....	......	.....
	Pribilof Island: St. Paul I., village	57 07 19	170 17 52	4 17	10 29	2.7	1.4
	Unalaska Island: C. S. station, Iliuliuk	53 52 54	166 31 44	3 50	9 58	2.9	1.5
	Sannakh Reefs: S. edge	54 13 30	162 38 00	12 13	6 10	5.7	2.8
	Sannakh Island: NE. end	54 26 12	162 18 00	....	....	......	.....
	Unga Island	55 20 45	160 38 39	2 40	8 55	8.2	4.1
	Popof Island: Humboldt I	55 19 17	160 31 14	....	....	......	.....
	Nagai Island: Sanborn Harbor	55 07 36	159 56 06	....	....	......	.....
	Koniushi Island: NW. harbor	55 03 17	159 23 05	....	....	......	.....
	NE. harbor	54 58 25	159 22 18	....	....	......	.....
	Simeonof Island: Simeonof Harbor	54 55 30	159 15 03	2 20	8 33	7.5	3.8
Alaska.	Cape Strogonof: Extreme	56 48 00	158 46 00	....	....	......	.....
	Chignik Bay: Anchorage	56 19 20	158 24 24	....	....	......	.....
	Anowik Island: S. end	56 05 13	156 39 19	1 45	7 58	8.1	4.0
	Chiachi Islands	55 51 58	159 05 24	....	....	......	.....
	Light-House Rocks	55 45 24	157 27 04	....	....	......	.....
	Chirikof Island	55 48 22	155 42 51	....	....	......	.....
	Kodiak Island, St. Paul Harbor: Cove NW. of village	57 47 57	152 21 21	0 16	6 24	9.0	4.5
	Port Etches	60 20 43	146 37 38	0 50	7 05	10.1	5.1
	Middleton Island	59 27 22	146 18 45	....	....	......	.....
	Mount St. Elias: Summit	60 20 45	141 00 12	....	....	......	.....
	Yakutat Bay: Port Mulgrave	59 33 42	139 46 16	0 34	6 41	9.5	5.0
	Lituya Bay	58 36 57	137 40 06	....	....	......	.....
	Sitka: Middle of parade ground	57 02 52	135 19 31	0 06	6 17	9.9	5.2
	Juneau	58 18 00	134 24 00	0 45	6 56	18.6	9.7
	Wrangell: Ast. station	56 27 00	132 23 00	0 30	6 39	17.7	9.2
Queen Charlotte Is.	North Island: N. pt	54 15 00	132 56 20	....	....	......	.....
	Cape Knox: Extreme	54 10 30	132 57 50	....	....	......	.....
	Port Kuper: Sansum I	52 56 31	132 09 06	0 00	6 12	11.5	6.1
	Forsyth Point: Extreme	52 09 07	131 03 20	....	....	......	.....
	St. James Cape: S. extreme	51 54 00	131 01 26	....	....	......	.....
	Cumshewa Harbor: N. side of entrance	53 02 00	131 31 00	....	....	......	.....
	Skidegate Bay: Rock on bar	53 22 20	131 51 00	0 07	6 19	12.8	6.7
	Rose Spit Point: Extreme	54 13 00	131 34 00	....	....	......	.....
	Massett Harbor: Uttewas village	54 01 40	132 10 00	....	....	......	.....
	Cape Edenshaw: Extreme	54 04 30	132 20 56	....	....	......	.....
Vancouver Island.	Hecate Bay: Observatory Islet	49 15 22	125 55 43	12 15	6 08	10.0	5.8
	Stamp Harbor: Observatory Islet	49 13 46	124 50 07	0 45	7 20	12.4	7.1
	Island Harbor: Observatory Islet	48 54 41	125 16 54	....	....	......	.....
	Cape Beale: Light-house	48 47 23	125 13 14	12 20	6 15	9.9	5.7
	Refuge Cove: Village on W. side	49 20 50	126 16 06	....	....	......	.....
	Hesquiat Harbor: Boat Cove	49 27 31	126 24 53	12 05	5 56	10.3	5.9
	Estevan Point: S. extreme	49 22 07	126 31 58	....	....	......	.....
	Nootka Sound: Friendly Cove	49 35 31	126 36 58	12 05	5 55	9.8	5.6
	Port Langford: Colwood Islet	49 47 20	126 56 31	....	....	......	.....
	Esperanza Inlet: Observatory Rock	49 52 45	126 59 21	11 55	5 45	9.7	5.5
	Kyuquot Sound: Shingle Point	49 59 55	127 08 56	11 50	5 38	9.3	5.3
	Nasparti Inlet: Head Beach	50 11 21	127 37 24	11 47	5 34	9.3	5.3
	Cook Cape: Solander I	50 06 31	127 56 46	....	....	......	.....
	North Harbor: Observatory Rock	50 29 25	128 03 05	....	....	......	.....

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Vancouver I.	Koprino Harbor: Observatory Rock	50 30 00	127 51 42	......	......	.....	....
	Hecate Cove: Kitten Islet	50 32 26	127 35 44	......	......	.....	....
	Triangle Island: W. side	50 51 53	129 05 58	......	......	.....	....
	Cape Scott: Summit	50 46 41	128 26 11	......	......	.....	....
	Bull Harbor, Hope Island: N. pt. Indian I.	50 54 47	127 55 29	0 10	6 22	10.7	5.6
	Port Alexander: Islet in center	50 50 49	127 39 23	0 32	6 44	11.6	6.1
	Beaver Harbor: Shell Islet	50 42 36	127 24 33	0 30	6 42	11.5	6.0
	Cormorant I.: Yellow Bluff in Alert Bay	50 35 02	126 56 56	0 55	7 08	12.8	6.7
	Baynes Sound: Beak Pt	49 36 29	124 50 44	4 45	11 00	10.6	6.6
	Nanoose Harbor: Entrance Rock	49 15 43	124 07 32	4 52	11 18	10.2	6.4
	Nanaimo: Light-house	49 12 50	123 48 11	......	......	.....	....
	Benson's House	49 10 15	123 56 02	4 40	11 05	9.8	6.1
	Victoria: Light-house	48 25 26	123 23 28	[2 17]	[8 31]	[5.7]	....
	Esquimalt: Fisgard I. light	48 25 50	123 26 46	[2 00]	[8 14]	[5.8]	....
	Race Island: Light-house	48 17 53	123 31 47	......	......	.....	....
	Sooke Inlet: Secretary I	48 19 35	123 42 40	......	......	.....	....
	Port San Juan: Pinnacle Rock	48 33 30	124 27 37	......	......	.....	....
British Columbia.	Port Harvey: Tide Pole Islet	50 33 58	126 16 06	1 55	8 10	14.1	7.4
	Port Neville: Robber's Nob	50 31 09	126 03 47	2 30	8 47	16.0	8.3
	Knox Bay, Thurlow Island: Stream at head of bay	50 24 15	125 38 26	3 40	10 00	15.7	7.7
	Valdes Island: S. pt	50 02 42	125 14 34	4 45	10 15	7.2	4.8
	Howe Sound: Plumper Cove	49 24 39	123 28 46	5 38	11 58	9.0	5.6
	Atkinson Point: Light-house	49 19 42	123 15 54	5 20	11 35	7.8	4.9
	Vancouver, Burrard Inlet: Govt. Reserve, English Bay	49 16 18	123 11 26	5 28	12 01	8.2	5.0
	Fraser River: Garry Pt	49 07 04	123 11 27	5 11	11 23	7.0	4.4
	New Westminster: Military barracks	49 13 01	123 53 52	......	......	.....	....
	Point Roberts: Parallel station	49 00 00	123 04 52	......	......	.....	....
	Semiamoo Bay: Parallel station	49 00 00	122 44 56	4 59	11 10	7.1	4.6
Washington.	Admiralty Head: Light-house	48 09 19	122 40 34	......	......	.....	....
	Steilacoom: Methodist Church	47 10 20	122 35 51	4 46	11 04	11.0	7.2
	Seattle: C. S. ast. station	47 35 54	122 19 59	4 22	10 33	9.2	6.0
	Port Townsend: C. S. ast. station	48 06 56	122 44 58	3 47	9 32	6.2	4.0
	Smith Island: Light-house	48 19 07	122 50 36	3 40	9 28	5.6	3.7
	New Dungeness: Light-house	48 10 52	123 06 31	2 42	8 34	5.0	3.3
	Port Angeles: Ediz Hook light-house	48 08 24	123 24 07	2 10	8 23	5.3	3.4
	Cape Flattery: Light-house	48 23 30	124 44 06	0 08	6 16	7.1	4.1
	Cape Shoalwater: Light-house	46 43 00	124 04 25	......	......	.....	....
	Cape Disappointment: Light-house	46 16 29	124 03 11	12 22	6 19	7.7	4.5
	Kalama: Methodist Church	46 00 26	122 50 39	3 39	11 25	3.2	1.9
	Bremerton: Navy-yard flagstaff	47 33 24	122 37 33	4 27	10 35	9.4	6.1
	Tacoma: St. Luke Church	47 15 32	122 26 26	4 32	10 45	9.8	6.4
Oregon.	Astoria: Flagstaff	46 11 19	123 49 42	0 15	6 42	7.8	4.7
	Yaquina Head: Light-house	44 40 35	124 04 40	11 50	5 37	7.3	4.3
	Cape Arago, or Gregory: Light-house	43 20 36	124 22 31	11 55	5 49	6.0	3.5
	Cape Blanco: Light-house	42 50 22	124 33 30	......	......	.....	....
California.	Crescent City: Light-house	41 44 36	124 12 10	11 33	5 15	5.8	3.4
	Trinidad Head: Light-house	41 03 01	124 09 03	11 27	5 11	5.7	3.3
	Eureka: Methodist Church	40 48 11	124 09 41	11 57	5 45	5.7	3.3
	Humboldt: Light-house	40 41 37	124 16 26	11 33	5 19	5.3	3.1
	Cape Mendocino: Light-house	40 26 18	124 24 25	11 00	4 50	4.7	3.0
	Point Arena: Light-house	38 57 12	123 44 27	10 36	4 21	4.1	2.6
	Point Reyes: Light-house	37 59 39	123 01 24	11 23	5 08	5.1	3.2
	San Francisco: Coast Survey ast. station	37 47 55	122 24 32	12 07	5 34	5.1	3.2
	Presidio station	37 47 30	122 27 49	11 43	5 07	4.6	2.9
	Mare Island: Stone block, obs. station	38 05 53	122 16 24	1 05	7 15	5.6	3.7
	Benicia: Church	38 03 05	122 09 23	1 35	7 48	5.6	3.7
	Farallon Islet: Light-house	37 41 51	123 00 07	10 40	4 25	4.5	2.9
	Santa Clara: Catholic Church	37 20 49	121 56 26	......	......	.....	....
	Mount Hamilton: Obs. peak	37 21 03	121 36 40	......	......	.....	....
	San José: Spire	37 19 58	121 53 39	......	......	.....	....
	Pigeon Point: Light-house	37 10 49	122 23 39	......	......	.....	....

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
California.	Santa Cruz: Warehouse flagstaff	36 57 31	122 01 29	10 54	4 27	5.2	3.3
	Monterey: C. S. azimuth station	36 35 21	121 52 59	10 43	4 24	4.8	3.1
	Point Pinos: Light-house	36 37 55	121 56 02				
	Piedras Blancas: Light-house	35 39 50	121 17 06				
	Point Conception: Light-house	34 26 49	120 28 18				
	Santa Barbara: N. tower, Mission Church	34 26 10	119 42 42	9 37	3 15	4.8	2.2
	San Buenaventura: C. S. ast. station	34 15 46	119 15 56	9 53	3 21	4.9	2.2
	Pt. Fermin, San Pedro Bay: Light-house	33 42 14	118 17 41	9 36	3 13	5.5	2.5
	Los Angeles: Court-house	34 03 05	118 14 32				
	Point Loma: Light-house	32 39 48	117 14 37	9 29	3 07	5.2	2.3
	San Diego: C. S. ast. station	32 43 06	117 09 41	9 32	3 20	5.1	2.3
	Mexican Boundary: Obelisk	32 31 58	117 07 32				
	San Miguel Island: Seal Pt	34 04 19	120 21 55	9 23	3 02	4.9	2.2
	Santa Rosa Island: E. pt	33 56 30	119 58 29				
	Santa Cruz Island: NE. pt	34 03 12	119 33 51	9 29	3 06	4.9	2.2
	Anacapa Island: E. pt	34 00 25	119 23 04				
	Santa Barbara Island: Summit	33 28 16	119 02 29				
	San Nicolas Island: Summit	33 14 55	119 31 19	9 20	3 04	4.9	2.2
	Santa Catalina Island: Catalina Peak	33 23 09	118 24 05	9 28	3 08	5.1	2.3
Lower California.	Ensenada Harbor: Head of bay, close to beach	31 51 10	116 38 05	9 28	3 06	5.0	2.2
	San Tomas: NW. shore of cove	31 33 04	116 40 51				
	Colnett Bay: Head of bay	30 57 39	116 17 28	9 27	3 05	5.8	2.6
	San Martin Island: Hassler Cove	30 28 58	116 06 46				
	Port San Quentin: Sextant Pt	30 22 16	115 59 07	9 23	3 00	4.9	2.2
	San Geronimo Island: Bight at E. end	29 47 20	115 48 12				
	Canoas Point: High bluff	29 25 29	115 12 14				
	Guadeloupe: North pt	29 10 50	118 18 30				
	La Playa Maria: Mound on W. side	28 56 06	114 31 06	9 15	2 53	7.6	3.4
	Santa Rosalia Bay: Obs. spot, Cairn	28 40 16	114 14 15				
	Lagoon Head: Highest pt. of crater	28 14 26	114 06 21				
	Cerros Island: SE. extremity	28 03 52	115 11 32	9 05	2 42	7.8	3.5
	San Benito Island: Summit of W. island	28 18 08	115 36 10				
	San Bartolomé: N. side of entrance	27 39 35	114 54 27	9 00	2 37	8.2	2.8
	Asuncion Island: Summit of island	27 06 10	114 17 25				
	San Ignacio Point: Extreme	26 45 45	113 16 25				
	Abreojos Point: Extreme of rocky ledge	26 42 49	113 35 04	9 00	2 48	6.7	2.3
	San Domingo Point: Edge of cliff	26 18 56	112 41 44				
	San Juanico Point: Knoll	26 03 18	112 17 52	8 29	2 17	5.7	1.6
	Alijos Rocks: South Rock	24 58 00	115 51 54				
	Cape San Lazaro: Extreme	24 47 31	112 18 25				
	Magdalena Bay: Obs. spot (post) N. of Port Magdalena	24 38 23	112 08 54	8 25	2 12	5.5	1.5
	Cape Tosco: Extreme	24 18 12	111 42 54				
	El Conejo Point: Extreme	24 20 17	111 30 21				
	Todos Santos: Foot of hill, Lobos Pt	23 27 14	110 14 07				
	San Lucas: Steep sand beach, NW. pt. of bay	22 53 07	109 54 50				
	San José del Cabo: NE. side of entrance	23 03 35	109 40 43	8 36	2 20	4.5	1.2
	Arena Point: Extreme	23 32 48	109 28 57				
	Arena de la Ventana: Extreme	24 03 52	109 50 29				
	Pichilinque Bay: SE. pt. of San Juan, Nepomezeino I	24 15 31	110 20 34				
	La Paz: Obs. spot, El Mogote	24 10 10	110 20 41	9 40	3 34	5.4	1.3
	Lupona Point: Extreme	24 24 10	110 20 35				
	San Evaristo: 3 m. S. of S. Evaristo Hd	24 52 03	110 41 47				
	San Marcial Point: Extreme	25 29 23	111 01 43				
	Salinas Bay: Beach, NE. pt. of bay	25 59 37	111 06 53				
	Loreto: Cathedral	26 00 41	111 21 03				
	Pulpito Point: Summit	26 30 44	111 27 14				
	Muleje: Equipalito Pt	26 53 37	111 58 04				
	San Marcos Island: S. sand spit	27 10 21	112 05 39				
	Santa Maria Cove: Beach on NW. shore	27 26 06	112 19 56				
	San Carlos Point: Extreme	28 00 07	112 47 36				
	Santa Teresa Bay: Beach on N. side	28 25 04	112 51 59	11 50	5 47	11.2	2.6

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Lower California.	Las Animas: Low pt	28 47 40	113 12 48				
	Raza Island: Landing place, S. side	28 49 11	113 00 05				
	Angeles Bay: Bight on NW. shore	28 56 39	113 34 35				
	Remedios Bay: Beach on W. shore	29 13 52	113 40 00				
	Mejia Island: S. side	29 33 08	113 35 19				
	San Luis Island: SE. side	29 57 27	114 25 49				
	San Firmin: Beach, N. of bight	30 25 16	114 39 47				
	San Felipe Point: Peak, 1,000 feet	31 02 57	114 52 10				
	Philips Point: Beacon	31 46 10	114 43 31				
Mexico.	Georges Island: NE. shore	31 00 54	113 16 30				
	Cape Tepoca: Hill, 300 feet	30 16 05	112 53 26				
	Libertad Anchorage: Beach	29 54 12	112 45 04				
	Patos Island: SE. end	29 16 12	112 28 51				
	Tiburon Island: SE. end	28 45 55	112 21 46				
	Kino Point: 0.2 mile N. 88° W. of mound	28 45 28	111 58 37				
	San Pedro: N. side of bay	28 03 22	111 16 00				
	Guaymas: Light-house	27 50 28	110 54 28	11 30	5 26	5.0	1.2
	Ciaris Island: NW. part	26 58 59	109 57 17				
	Santa Barbara: NW. side of bay	26 41 09	109 40 48				
	Agiabampo: SE. side of entrance	26 16 35	109 17 30				
	Topolobampo: SE. end of Santa Maria I	25 33 56	109 10 23				
	Navachista: W. side of creek	25 23 06	108 49 00				
	Playa Colorado: N. side of entrance	25 11 42	108 23 37				
	Altata: N. side of entrance	24 38 52	107 59 37	10 07	3 59	5.8	1.4
	Mazatlan: Light-house	23 10 40	106 26 47	9 08	2 51	3.8	0.9
	Palenita Village: Boca Tecapan	22 30 26	105 44 25				
	San Blas: Custom-house	21 32 30	105 18 40	9 08	2 52	3.2	1.0
	Mariá Madre Island: SE. extreme	21 30 45	106 33 14				
	Mita Point: Extreme	20 45 50	105 33 37				
	Peñas Anchorage: Mouth of Rio Real	20 36 26	105 16 00				
	Cape Corrientes: Extreme	20 25 00	105 39 21				
	Perula Bay: Smooth Rock	19 34 48	105 08 54	9 07	2 53	2.5	1.1
	San Benedicto Island: S. extreme	19 17 15	110 49 22				
	Socorro Island: SE. part	18 42 57	110 56 53				
	Roca Partida: Summit	18 59 41	112 04 07				
	Clarion Island: S. end	18 20 55	114 44 17				
	Clipperton Island: Summit	10 17 00	109 13 00				
	Navidad Bay: W. end of sandy beach	19 13 25	104 43 26				
	Manzanilla Bay: Flagstaff, U. S. consulate	19 03 15	104 19 50	9 07	2 54	1.9	1.3
	Sacatula River: Beach, W. side of bay	17 58 21	102 07 06				
	Isla Grande: Tripod on NW. summit	17 40 15	101 40 25				
	Sihuatanejo Point: Tree on beach	17 37 50	101 33 23	8 50	2 38	2.0	0.9
	Morro Petatlan: Junction of stony and sandy beaches	17 31 28	101 27 14				
	Tequepa Harbor: Limekiln	17 16 13	101 04 32				
	Acapulco: Light-house	16 49 10	99 55 50				
	Maldonado: El Recordo Pt	16 19 37	98 35 05				
	Port Angeles: Light-house	15 39 09	96 30 43				
	Sacrificios Point: Highest pt. of cape	15 40 41	96 15 04				
	Port Guatulco: Cross	15 44 58	96 08 10				
	Morro Ayuca: Summit of N. edge of cape	15 52 17	95 46 43				
	Salina Cruz: Light-house	16 09 49	95 12 31				
Central America.	Champerico: Inshore end of iron wharf	14 17 44	91 55 36	2 50	9 02	8.5	4.6
	San José de Guatemala: Light-house	13 55 15	90 49 45	2 50	9 02	9.0	4.9
	Acajutla: Light-house	13 34 20	89 50 26	2 55	9 08	9.5	5.1
	Libertad: Light-house	13 28 49	89 19 25	3 05	9 18	10.0	5.4
	La Union: Light-house	13 20 00	87 51 00	3 15	9 28	10.5	5.7
	Chicarene Point: Extreme	13 17 09	87 47 06				
	Corinto: Light-house	12 27 54	87 12 31	2 55	9 08	10.5	5.7
	San Juan del Sur: Signal station	11 14 45	85 52 59	3 00	9 12	10.0	5.4
	Salinas Bay: Salinas Islet	11 03 10	85 43 38	2 50	9 02	9.5	5.1
	Port Culebra: Extremity of Mala Pt	10 36 46	85 42 46	2 45	8 58	9.0	4.9
	Ballena Bay: N. Estero Toussa	9 43 45	85 00 46				
	Parida Anchorage: S. pt. of Deer Id	8 10 13	82 14 32	3 15	9 28	10.5	5.7
	Port Nuevo: Entrada Pt	8 04 30	81 43 30				
	Bahia Honda: W. end of Centinela I	7 43 32	81 31 58	3 10	9 22	11.0	5.9
	Coiba (Quibo) Island: Observation pt	7 24 20	81 41 51				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF NORTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
C. America.	Cocos Island: Head of Chatham Bay	5 32 57	86 59 17	....	....	......	......
	Panama: NE. bastion, ast. station	8 57 12	79 32 05	3 00	9 14	16.0	8.7
	Taboga Island: Church	8 47 45	79 33 16	3 00	9 13	15.4	8.3
	Cape Mala: Extreme	7 27 40	79 59 25	3 10	9 22	13.0	7.0
	Malpelo Island: Summit	4 03 00	81 36 00	....	....	......	......

WEST INDIA ISLANDS.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
Bahama Islands.	Memory Rock: Center	26 56 53	79 06 54	7 40	1 28	3.2	1.7
	Bahama Island: W. pt	26 41 18	79 00 38	....	....	......	......
	Abaco Island: Light-house	25 51 30	77 10 45	....	....	......	......
	Little Guana Cay: Light-house	26 31 10	76 57 36	....	....	......	......
	Walker Cay: Highest part	27 15 42	78 23 48	....	....	......	......
	Great Isaac Cay: Light-house	26 02 00	79 06 00	....	....	......	......
	Gun Cay: Light-house	25 34 30	79 18 26	8 20	2 08	3.0	1.5
	Ginger Cay: Center	22 45 10	78 06 02	....	....	......	......
	Cay Lobos: Light-house	22 22 30	77 34 26	....	....	......	......
	St. Domingo Cay: Center	21 42 00	75 44 39	....	....	......	......
	Cay Verde: Hill at S. end	22 01 15	75 10 34	....	....	......	......
	Ragged Island: Gun Pt	22 14 02	75 45 17	....	....	......	......
	Nairn Cay: E. pt	22 20 44	75 28 20	....	....	......	......
	Nurse Channel Cay: Beacon	22 31 15	75 51 41	....	....	......	......
	Long Island: S. pt	22 51 00	74 51 54	....	....	......	......
	Great Emma Island: Beacon	23 32 15	75 46 24	....	....	......	......
	Clarence Harbor: Light-house	23 06 00	74 59 00	8 20	2 08	4.1	2.1
	Eleuthera Island: Light-house	25 00 00	76 13 00	7 00	0 48	4.0	2.1
	Royal Island: Eastern Pass	25 31 20	76 51 48	....	....	......	......
	Nassau: Light-house	25 05 37	77 21 58	7 20	1 08	4.0	2.1
	Andros Island: Light-house	24 43 45	77 46 45	7 40	1 28	3.0	1.5
	Great Stirrup Cay: Light-house	25 49 40	77 53 55	....	....	......	......
	Little Stirrup Cay: W. end	25 49 12	77 57 06	....	....	......	......
	San Salvador (Cat I.): Light-house	24 06 15	75 26 00	7 00	0 48	4.0	2.1
	Concepcion Island: W. bay	23 50 50	75 07 27	....	....	......	......
	Watlings Island: Hunchinbroke Rock	23 56 40	74 28 20	....	....	......	......
	Rum Cay: Harbor Pt	23 37 45	74 50 08	....	....	......	......
	Castle Island: Light-house	22 06 40	74 20 37	....	....	......	......
	Fortune Island: S. end	22 32 40	74 22 54	....	....	......	......
	Crooked Island: Moss flagstaff	22 47 30	74 20 21	....	....	......	......
	Bird Island: Light-house	22 51 00	74 22 48	....	....	......	......
	Samana Cay: W. pt	23 05 30	73 49 15	....	....	......	......
	Plana Cay: NW. pt	22 34 38	73 38 03	....	....	......	......
	Mariguana Island: SE. pt	22 16 30	72 47 03	7 20	1 08	3.0	1.5
	Hogsty Reef: NW. Cay	21 40 30	73 50 29	....	....	......	......
	Inagua Island: Light-house	20 56 00	73 40 17	7 50	1 38	3.5	1.8
	Little Inagua Island: NW. pt	21 30 40	73 42 33	....	....	......	......
	W. Caicos Cay: Hill, SE. end	21 37 30	72 28 18	....	....	......	......
	French Cay: W. pt	21 30 00	72 12 51	....	....	......	......
	Fort George Cay: Old magazine	21 54 00	72 07 14	....	....	......	......
	Caicos Island: Parsons Pt., S. islet	21 29 33	71 31 12	....	....	......	......
	Turk Island: Light-house	21 30 55	71 07 29	7 30	1 18	3.0	1.5
	Square Handkerchief Bank: NE. breaker	21 06 30	70 29 54	....	....	......	......
	Silver Bank: E. extreme	20 35 00	69 21 24	....	....	......	......
	Navidad Bank: Center of E. side	20 02 00	68 47 24	....	....	......	......
Cuba.	Cape Maysi: Light-house	20 15 10	74 09 41	5 40	11 53	2.8	1.6
	Port Baracoa: Light-house	20 21 40	74 29 34	....	....	......	......
	Port Cayo Moa: Carenero Pt	20 41 41	74 53 44	....	....	......	......
	Port Nipe: Roma Pt	20 47 14	75 33 18	....	....	......	......
	Lucrecia Point: Light-house	21 04 24	75 36 59	....	....	......	......
	Port Sama: E. side of entrance	21 09 00	75 47 18	....	....	......	......
	Peak of Sama: Summit, 885 feet	21 07 00	75 47 40	....	....	......	......
	Port Naranjo: E. side of entrance	21 07 30	75 52 18	....	....	......	......
	Jibara: Fort San Fernando	21 07 05	76 07 48	6 20	0 08	2.4	1.4
	Port Padre: Guinchos Pt	21 18 30	76 35 34	....	....	......	......
	Port Nuevitas: Light-house	21 38 54	77 05 32	7 00	0 48	2.2	1.2

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

WEST INDIA ISLANDS—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Cuba.	Maternillos Point: Light-house	21 40 02	77 08 04	......	......	......	......
	Cay Verde: NW. end	22 08 45	77 37 33	......	......	......	......
	Cay Confites: S. pt	22 11 14	77 39 23	......	......	......	......
	Paredon Grande Cay: Light-house	22 29 10	78 09 11	7 20	1 08	2.8	1.6
	Cay Sal: Light-house	23 56 30	80 27 51	......	......	......	......
	Bahia de Cadiz Cay: Light-house	23 12 34	80 29 26	......	......	......	......
	Piedras Cay: Light-house	23 14 10	81 07 20	......	......	......	......
	Matanzas: Summit of peak	23 01 54	81 43 18	8 30	2 18	2.2	1.2
	Habana: Morro light-house	23 09 21	82 21 30	8 18	1 56	1.3	0.7
	Transit pier, arsenal yard	23 08 03	82 21 17	......	......	......	......
	Cape San Antonio: Light-house	21 51 44	84 57 28	8 30	2 18	1.5	0.9
	San Felipe Cays: SW. pt	21 55 00	83 31 18	......	......	......	......
	Isle of Pines: Port Frances	21 35 30	83 09 13	......	......	......	......
	Piedras Cay: Light-house	21 57 45	81 07 18	......	......	......	......
	Cienfuegos: Colorados Pt. light	22 01 58	80 26 32	4 47	11 00	2.0	1.1
	Cape Cruz: Light-house	19 50 13	77 43 30	......	......	......	......
	Santiago de Cuba: Light-house	19 57 31	75 52 12	8 20	2 30	2.2	1.1
	Port Guantanamo: Fisherman Pt	19 54 39	75 09 27	7 50	2 00	2.6	1.3
	Cayman Brac: E. pt	19 45 15	79 46 07	......	......	......	......
	Little Cayman: W. pt	19 39 10	80 07 17	......	......	......	......
	Grand Cayman: Fort George, W. end	19 17 45	81 23 17	......	......	[1.3]	......
Jamaica.	Morant Point: Light-house	17 55 05	76 11 08	......	......	[1.1]	......
	Port Antonio: Folly Pt. Light	18 11 31	76 26 31	......	......	......	......
	Port Maria: NW. wharf	18 23 00	76 54 22	......	......	......	......
	St. Ann Bay: Long wharf	18 26 24	77 12 52	......	......	[1.2]	......
	Falmouth: Fort	18 30 34	77 39 52	......	......	......	......
	Montego Bay: Fort	18 29 25	77 56 16	......	......	......	......
	St. Lucia: Fort	18 27 45	78 10 52	......	......	......	......
	Savanna-la-Mar: Fort	18 12 20	78 08 54	......	......	......	......
	Kingston: Plum Pt. light	17 55 32	76 46 45	......	......	......	......
	Port Royal: Fort Charles, flagstaff	17 55 56	76 50 38	......	......	[1.1]	......
	Morant Cays: NE. Cay	17 26 30	75 58 20	......	......	......	......
	Pedro Bank: Portland Rock, E. end	17 06 20	77 26 28	......	......	......	......
	Baxo Nuevo: Sandy Cay	15 53 00	78 39 04	......	......	......	......
Haiti.	Samana Town: Fort	19 12 29	69 19 23	9 00	2 48	3.0	1.5
	Cape Cabron: Extreme	19 21 17	69 16 00	......	......	......	......
	Port Plata: Light-house	19 48 51	70 41 27	......	......	......	......
	Grange Point: W. end	19 54 45	71 39 03	......	......	......	......
	Manzanilla Point: Presidente Pt	19 45 34	71 47 20	6 50	0 39	5.5	2.9
	Cape Haitien: Town fountain	19 46 20	72 11 42	......	......	......	......
	Port Paix: Wharf	19 57 40	72 49 45	......	......	......	......
	Nicolas Mole: Fort George, flagstaff	19 49 15	73 23 07	......	......	......	......
	Gonaïves: Verreur Pt	19 25 42	72 42 52	......	......	......	......
	Gonave Island: W. pt	18 55 26	73 18 34	......	......	......	......
	Arcadius Islands: Light-house	18 48 13	72 39 05	......	......	......	......
	Port au Prince: Fort Islet light	18 33 54	72 22 01	......	......	[1.2]	......
	Petite Rivière Village: Sand beach in front of huts	18 37 15	74 23 55	......	......	......	......
	Jeremie: Fort	18 38 15	74 05 54	......	......	......	......
	Navassa Island: N. extreme	18 25 10	75 02 03	......	......	......	......
	Formigas Bank: Shoal spot	18 33 00	75 44 24	......	......	......	......
	Vache Island: Sand beach, near NW. pt.	18 06 00	73 43 40	......	......	......	......
	Jacmel: Wharf	18 13 30	72 34 30	......	......	[2.5]	......
	Beata Island: NW. pt	17 36 45	71 33 44	......	......	......	......
	Frayle Rock: Center	17 37 00	71 41 00	......	......	......	......
	Alta Vela: Summit	17 28 50	71 39 11	......	......	......	......
	Avarena Point: Extreme	18 07 00	70 59 18	......	......	......	......
	Salinas Point (Caldera): Extreme	18 12 00	70 35 18	......	......	......	......
	St. Domingo City: Light-house	18 27 54	69 52 59	......	......	[2.2]	......
	Point Espada: Extreme	18 19 43	68 27 34	......	......	......	......

MARITIME POSITIONS AND TIDAL DATA.

WEST INDIA ISLANDS—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Porto Rico.	Mona Island: Light-house	18 02 43	67 50 30				
	Mayaguez: Mouth of Mayaguez R	18 11 56	67 09 04	7 04	2 00	2.0	1.0
	Aguadilla Bay: Village	18 25 09	67 16 08				
	San Juan de Porto Rico: Morro light-house	18 28 56	66 07 28	8 21	2 20	1.3	0.9
	Cape San Juan: Light-house	18 23 05	65 36 31				
	Guanica: Meseta Pt	17 57 10	66 54 11			[1.0]	
	Culebrita Island: Light-house	18 18 44	65 13 34	[7 31]	[1 30]	[1.0]	
	Vieques (Crab) Island: Port Ferro light	18 05 20	65 25 26	[7 35]	[1 40]	[1.1]	
	St. Thomas: Fort Christian, SW. bastion	18 20 23	64 55 52	[7 11]	[0 58]	[1.2]	
	St. John Island: Ram Head	18 18 08	64 42 03				
	Tortola: Fort Burt	18 25 04	64 36 47				
	Virgin Gorda: Vixen Pt	18 30 39	64 21 48				
	Anegada: W. pt	18 45 11	64 24 58				
	E. extreme of reefs	18 36 30	64 10 45				
	Christiansted, Santa Cruz: SW. bastion of fort	17 45 09	64 42 16				
	Sombrero: Light-house	18 35 37	63 28 13				
	Dog Island: Center	18 16 42	63 16 00				
	Anguilla: Custom-house	18 13 06	63 04 39				
	St. Martin: Fort Marigot light	18 04 07	63 05 45				
	St. Bartholomew: Fort Oscar	17 53 58	62 51 30			[1.5]	
	Saba: Diamond Rock	17 39 10	63 15 16				
	St. Eustatius: Fort flagstaff	17 29 10	62 59 09				
	St. Christopher: Basseterre Church	17 18 12	62 43 14				
	Booby Island: Center	17 13 38	62 35 25				
	Nevis: Fort Charles	17 07 52	62 37 29				
	Barbuda: Flagstaff, Martello Tower	17 35 50	61 49 54				
	Antigua, English Harbor: Flagstaff, dockyard	17 00 00	61 46 07			[2.0]	
	Sandy Island: Light-house	17 06 54	61 55 11				
	Redonda Islet: Center	16 55 18	62 19 10				
	Montserrat: Plymouth Wharf	16 42 12	62 13 24				
	Guadeloupe, Basseterre: Light on mast	15 59 50	61 44 09				
	Port Louis: Light on mast	16 25 09	61 32 15				
	Gozier Islet: Light-house	16 11 57	61 29 40			[1.3]	
	Manroux Id.: Light-house	16 13 14	61 32 05				
	Point à Pitre: Jarry Mill	16 13 56	61 33 15				
	Desirade: E. pt	16 19 56	61 00 44				
	Petite Terre: Light-house	16 10 17	61 06 45				
	Marie Galante: Light-house	15 52 59	61 19 15				
	Saintes Islands: Tower on Chameau hill	15 51 32	61 35 55				
	Dominica, Prince Ruperts Bay: Sand beach W. of church	15 34 34	61 28 14	4 00	10 12	1.5	0.8
	Roseau: Flagstaff, Fort Young	15 17 27	61 23 52				
	Aves Island: Center	15 42 00	63 37 46				
	Martinique, Fort de France: Fort St. Louis light	14 35 44	61 04 30				
	St. Pierre: Ste. Marthe Battery	14 43 54	61 11 12				
	Caravelle Pen.: Light-house	14 46 13	60 53 20	3 50	10 02	1.1	0.6
	Cabrit Islet: Summit	14 23 23	60 52 33				
	St. Lucia, Port Castries: Light-house	14 01 54	61 00 48				
	Barbados, Bridgetown: Flagstaff, Rickett's Battery	13 05 42	59 37 19	2 50	9 02	3.0	1.5
	S. Point: Light-house	13 02 45	59 31 50				
	Ragged Point: Light-house	13 09 40	59 26 04				
	St. Vincent, Kingstown: Light-house	13 09 19	61 14 34	2 50	9 05	1.6	0.8
	Bequia Island, Admiralty Bay: Church	13 00 25	61 14 09				
	Grenada: St. George light-house	12 03 02	61 45 06	2 30	8 42	1.5	0.8
	Tobago, Rocky Bay: Light-house	11 10 08	60 42 38	3 50	10 02	2.1	1.1

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

WEST INDIA ISLANDS—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Testigos Islets: Center of Testigo Grande	11 25 02	63 05 48				
	Sola Island: Center	11 19 00	63 36 00				
	Pampatar, Margarita I.: San Carlos Castle	10 59 43	63 48 00				
	Tortugas Island: S. end of W. Tortugillo Islet	10 57 45	65 26 38				
	Orchila Island: S. side	11 47 57	66 12 31				
	Roques Islands: Pirate Cay	11 56 16	66 39 10				
	Bonaive Island: Light-house	12 02 06	68 14 10				
	Little Curaçao Island: Light-house	11 59 30	68 39 19				
	Curaçao Island: Fort Nassau	12 06 59	68 55 50				
	Light-house	12 06 17	68 56 16				
	Oruba Island: Light-house	12 31 05	70 02 34				

NORTH AND EAST COASTS OF SOUTH AMERICA.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
Colombia.	Chagres: San Lorenzo Castle	9 19 27	80 00 22				
	Toro Point: Light-house	9 22 39	79 57 16				
	Colon: Light-house	9 22 09	79 54 45	0 06	6 18	1.1	0.6
	Porto Bello: Ft. St. Geronimo	9 32 30	79 39 40				
	Caledonia Harbor: Scorpion Cay	8 54 52	77 42 25	11 30	5 17	1.5	0.8
	Carreto Port: Peak	8 47 00	77 38 00				
	Caribana Point: Extreme	8 37 30	76 52 55				
	Fuerte Island: N. extreme	9 24 00	76 10 45				
	Cispata Port: Zapote Pt	9 24 00	75 48 00				
	Cartagena: Light-house	10 25 50	75 32 50				
	Savanilla: Light-house	11 00 15	74 57 55				
	Magdalena River: NW. pt. of Gomez I	10 07 00	74 49 51				
	Santa Marta: Light-house	11 15 28	74 14 33				
	Rio de la Hacha: Light on church	11 33 30	72 54 50				
	Cape La Vela: Sand beach inside cape	12 12 34	72 09 42				
	Bahia Honda: E. pt., S. side	12 23 09	71 45 42				
Venezuela.	Espada Point: Extreme	12 04 00	71 07 55				
	Maracaibo: Zapara I. light	10 57 30	71 37 00	5 05	11 17	2.5	1.5
	Estangues Point: 500 ft. from extreme	11 48 56	70 17 21				
	Cape San Roman: Extreme	12 11 00	70 04 55				
	Marjes Islets: N. islet	12 29 15	70 57 00				
	Vela de Coro: Light-house	11 27 56	69 34 20				
	Tucacas Island: Ore house	10 47 00	68 19 55				
	St. Juan Bay: Cay	11 10 00	68 22 54				
	Puerto Cabello: Light-house	10 29 53	68 00 55				
	La Guaira: Light-house	10 36 57	66 56 06	6 00	12 12	2.8	1.7
	Cape Codera: Morro	10 35 00	66 06 15				
	Corsarios Bay: W. pt	10 34 06	66 04 13				
	Centinela Islet: Center	10 49 30	66 09 25				
	Barcelona: Morro	10 13 30	64 44 00				
	Cumana: Light-house	10 27 20	64 11 33				
	Escarseo Point: Extreme	10 40 00	64 17 55				
	Chacopata: Morro	10 42 00	63 50 25				
	Esmeralda Islet: Center	10 40 00	63 31 55				
	Carupano: Light-house	10 40 15	63 18 00				
	Pt. Herman Vasquez	10 42 00	63 14 00				
	Puerto Santo Bay: Sand spit S. of Morro	10 43 27	63 09 43				
	Tres Puntas Cape: Extreme	10 45 00	62 41 55				
	Unare Bay: Obs. spot, 200 yds. S. of Morro	10 44 19	62 44 29				
	Pena Point: Extreme	10 43 48	61 50 50				
	Pato Island: E. pt	10 38 15	61 51 18				
	Mocomoco Pt.: Extreme	8 39 25	60 10 15				
Trinidad.	Port of Spain: King's Wharf light	10 38 37	61 30 38	4 20	10 30	3.2	1.9
	Chacachacare Island: Rocks off SW. pt	10 40 03	61 45 54				
	Galera Point: NE. extreme, light-house	10 50 02	60 54 10				
	Icacos Point: Light-house	10 03 29	61 55 41				
	San Fernando: Pierhead	10 16 59	61 28 12				

MARITIME POSITIONS AND TIDAL DATA.

NORTH AND EAST COASTS OF SOUTH AMERICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Guiana.	Demerara: Georgetown light-house	6 49 20	58 11 30	4 18	9 50	8.6	3.9
	Nickerie River: Light-house	5 58 30	57 00 30				
	Paramaribo: Stone steps	5 49 30	55 08 48	5 50	12 00	9.5	4.3
	Maroni River: W. light-house	5 44 50	54 00 30				
	Salut Islands: Light-house	5 16 50	52 34 53				
	Enfant Perdu Islet: Light-house	5 02 40	52 21 11				
	Cayenne: Light-house	4 56 20	52 20 26	4 27	10 30	6.0	2.7
	Connétable Islet: Center	4 49 30	51 55 36				
	Carimare Mount: Summit	4 23 20	51 50 36				
Brazil.	Orange Cape: Extreme	4 20 45	51 27 46				
	Mayé Mountain: Summit	2 46 30	50 54 46				
	North Cape: Extreme	1 40 17	49 56 46				
		Lat. S.					
	Cape Magoari: Extreme	0 17 00	48 23 30				
	Para: Custom-house	1 26 59	48 30 01	11 50	5 37	11.0	5.2
	Atalaia Point: Light-house	0 35 03	47 20 54				
	Itacolomi Point: Light-house	2 10 11	44 25 56				
	Maranhão Island: Landing place	2 31 48	44 18 45	6 50	0 38	16.5	7.9
	Santa Anna Island: Light-house	2 16 22	43 37 30	5 35	11 47	13.1	6.2
	Tutoya: Entrance	2 41 55	42 18 02	5 05	11 17	11.7	5.6
	Paranahiba River: Amarção Village	2 53 20	41 40 35				
	Ceará: Light-house	3 42 05	38 28 25	5 25	11 37	8.2	3.9
	Jaguaribe River: Pilot station	4 25 35	37 44 55	5 50	12 00	8.0	3.8
	Caiçara: Village	5 03 15	36 02 52				
	Cape St. Roque: Extreme	5 29 15	35 15 52	4 05	10 17	8.8	4.2
	Rio Grande do Norte: Light-house	5 45 05	35 11 55				
	Natal: Cathedral	5 46 41	35 12 43				
	Parahiba River: Light-house at entrance	6 56 30	34 49 30				
	Parahiba: Cathedral	7 06 35	34 53 04				
	Olinda: Light-house	8 00 50	34 50 36				
	Pernambuco: Picao light-house	8 03 22	34 51 57	4 33	10 50	7.0	3.3
	Cape St. Augustine: Light-house	8 20 45	34 56 05				
	Tamandaré: Village	8 43 40	35 05 06				
	Maceio: Light-house	9 39 35	35 44 54	4 20	10 32	8.5	4.1
	San Francisco River: Light-house at entrance	10 30 30	36 21 51	4 17	10 29	7.8	3.7
	Cotinguiba River: Light-house at entrance	10 58 20	37 04 00				
	Vaza Barris River: Semaphore at entrance	11 09 45	37 12 36				
	Real River: Light-house	11 27 40	37 24 00				
	Conde: Village	12 12 05	37 45 46				
	Garcia d'Avila: Tower	12 33 40	38 02 16				
	Bahia: Santo Antonio light-house	13 00 37	38 32 06	4 10	10 22	7.6	3.6
	Itaparica: Fort on N. pt.	12 52 48	38 41 28				
	Morro de São Paulo: Light-house	13 22 37	38 54 38	3 50	10 00	6.0	2.9
	Camamu: Village	13 56 42	39 07 05	3 50	10 00	6.3	3.0
	Contas: Church	14 17 40	39 00 45				
	Ilheos: Church	14 47 40	39 03 25	3 35	9 47	6.4	3.1
	Olivença: Center of village	14 56 40	39 01 45				
	Una: Center of village	15 13 27	39 01 15				
	Comandatuba: Center of village	15 21 00	39 16 45				
	Santa Cruz: Church	16 17 20	39 02 05	3 25	9 37	6.0	2.9
	Porto Seguro: Matriz Church	16 25 38	39 04 15				
	Prado: River entrance	17 21 40	39 13 15				
	Alcobaça: Center of village	17 31 45	39 12 00				
	Caravellas: Center of village	17 43 30	39 14 36	3 10	9 23	6.4	3.1
	Abrolhos Island: Light-house	17 57 31	38 41 46	3 15	9 27	7.5	3.6
	Porto Alegre: Center of village	18 06 15	39 31 16				
	Espiritu Santo Bay: Light-house	20 19 23	40 16 36	2 50	9 00	4.0	1.9
	Guarapiri Islets: E. islet	20 38 25	40 23 46				
	Benevente: Village	20 49 00	40 40 45	2 40	8 52	5.0	2.4
	Itapemirim: Moscas Islet	20 57 35	40 46 35				
	São João da Barra: Light-house	21 38 40	41 02 21				
	Cape St. Thomé: Extreme	22 02 00	40 59 00				
	Macahé: Fort at entrance	22 23 45	41 47 35	2 20	8 30	9.2	4.4

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

NORTH AND EAST COASTS OF SOUTH AMERICA—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Brazil.	Santa Anna Island: Summit	22 26 00	41 43 15				
	Barra São João: Village	22 37 00	41 59 45				
	Busios: Church	22 46 00	41 54 05				
	Cape Frio: Light-house	23 00 42	42 00 00				
	Port Frio: Village	22 53 15	42 01 15	2 30	8 42	4.9	2.3
	Maricas Islands: S. islet	23 01 43	42 54 05				
	Rio de Janeiro: Fort Villegagnon Light	22 54 46	43 09 24	2 50	9 00	4.2	2.0
	Imperial Observatory	22 54 15	43 10 16				
	Raza Island: Light-house	23 03 40	43 08 45				
	Petropolis: Center of town	22 32 00	43 11 01				
	Cape Guaratiba: Summit	23 03 40	43 33 24				
	Marambaya Island: Summit of SW. end	23 04 20	43 59 26				
	Mangaratiba: Village	22 57 20	44 02 29				
	Palmas Bay: Beach at head of bay	23 09 20	44 08 24				
	Angra dos Reis: Landing-place	23 00 30	44 19 04				
	Ilha Grande: Light-house	23 09 50	44 05 45				
	Parati: Fort	23 12 20	44 42 04	1 35	7 47	5.3	2.5
	Ubatuba: Cathedral	23 25 55	45 04 04				
	Porcos Grande Islet: Summit	23 32 57	45 03 50				
	Busios Islets: Summit	23 45 15	45 00 39				
	St. Sebastian Island: Boi Pt. light	23 58 30	45 15 20				
	Villa Nova da Princessa: Center	23 47 20	45 21 04				
	Santos: Moela I. light-house	24 03 06	46 15 57				
	Quay	23 56 00	46 19 09	2 50	9 00	5.0	2.8
	Alcatrasses Island: Summit, 880 ft	24 06 30	45 40 49				
	Conceição: Church	24 10 32	46 47 44				
	Quemada Grande Island: Summit, 623 ft	24 28 45	46 41 04				
	Iguape: Quay	24 42 35	47 32 54				
	Bom Abrigo Islet: Light-house	25 06 40	47 51 50				
	Ilha do Mel: Light-house	25 30 55	48 19 53				
	Paranagua: Quay	25 31 20	48 31 03	2 55	9 05	6.4	3.1
	Antonina: Quay	25 26 30	48 43 14				
	Coral Islet: Center	25 44 10	48 23 14				
	Itacolomi Islet: Center	25 50 15	48 25 51				
	São Francisco: Center of town	26 14 17	48 39 29				
	Itapacaroya: Church	26 46 45	48 36 59				
	Cambria: Church	27 01 35	48 36 44				
	Arvoredo Island: Light-house	27 18 00	48 22 20				
	Anhatomirim: Light-house	27 25 30	48 34 25				
	St. Catharine Island: Rapa Pt	27 22 55	48 26 09	2 35	8 47	5.9	2.8
	Naufragados light	27 50 27	48 35 16				
	Nostra Senhora do Deserto: Quay	27 36 00	48 34 14				
	Coral Island: Summit, 230 feet	27 56 40	48 33 44				
	Cape St. Martha: Light-house	28 38 00	48 49 45				
	Torres Point: Extreme	29 20 20	49 43 39				
	Rio Grande do Sul: Light-house	32 06 40	52 07 44	4 00	10 12	1.8	0.9
Uruguay.	Castillos: Beuna Vista Hill, 184 feet	34 21 19	53 47 16	8 20	2 08	2.0	0.9
	Cape Santa Maria: Light-house	34 40 01	54 09 14				
	Lobos Island: Center	35 01 39	54 53 16				
	Maldonado: Light-house	34 58 15	54 57 10				
	Flores Island: Light-house	34 56 55	55 55 04				
	Montevideo: Cathedral, SE. tower	34 54 33	56 12 15	2 00	8 12	3.5	2.3
	Colonia: Light-house	34 28 20	57 52 27	6 30	0 00	4.0	2.7
Argentina.	Martin Garcia Island: Light-house	34 10 50	58 15 40				
	Buenos Ayres: Cupola of custom-house	34 36 30	58 22 14	6 43	12 15	2.1	1.4
	La Plata	34 54 30	57 54 15				
	Indio Point: Light-house	35 15 45	57 10 45				
	Piedras Point: Extreme	35 26 50	57 05 28				
	Cape San Antonio: Light-house	36 18 24	56 44 15	9 50	3 35	5.3	3.5
	Madanas Point: Light-house	36 53 00	56 38 54				
	Cape Corrientes: E. summit	38 05 30	57 30 01				
	Port Belgrano: Anchor-Stock Hill	38 57 00	61 59 15	6 00	0 00	15.8	8.2
	Argentina: Fort	38 43 50	62 15 27				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

NORTH AND EAST COASTS OF SOUTH AMERICA—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Argentina.	Labyrinth Head: Summit	39 26 30	62 03 22				
	Union Bay: Indian Head	39 57 30	62 07 46				
	San Blas Harbor: SW. end of Hog Islet	40 32 52	62 09 30				
	San Blas Bay: Summit of Rubia Pt	40 36 10	62 10 12				
	Rio Negro: Main Pt	41 02 00	62 45 11	10 50	4 38	14.7	7.7
	Bermeja Head: E. summit	41 11 00	63 08 16				
	Port San Antonio: Point Villarino	40 49 00	64 54 41	10 35	4 23	23.5	12.3
	San Antonio Sierra: Summit	41 41 10	65 12 29				
	Port San José: San Quiroga Pt	42 14 15	64 27 56				
	Delgado Point: SE. cliff	42 46 15	63 37 16				
	Cracker Bay: Anchorage	42 57 00	64 28 20				
	Port Madryn: Anchorage off cave bluff	42 45 40	64 59 00	7 05	0 52	13.2	6.9
	Chupat River: Entrance	43 20 45	65 03 36				
	Port St. Elena: St. Elena pen	44 30 40	65 22 10	3 50	10 03	16.8	8.8
	Leones Island: SE. summit	45 04 00	65 36 01				
	Melo Port: W. pt	45 03 00	65 52 30				
	Port Malaspina: S. pt	45 10 10	66 32 36				
	Cape Three Points: NE. pitch	47 06 20	65 51 46				
	Port Desire: Largest ruin	47 45 05	65 54 45	0 00	6 12	18.3	9.6
	Sea Bear Bay: Wells Pt	47 57 15	65 45 40				
	Port San Julian: Sholl Pt	49 15 20	67 42 30	10 35	4 23	29.5	15.4
	Port Santa Cruz: Mount at entrance	50 08 30	68 23 00	9 20	3 08	39.6	20.7
	Coy Inlet: Height S. side of entrance	50 58 27	69 09 47	9 00	2 47	40.0	20.9
	Gallegos River: Observation mound	51 33 21	69 00 31	8 40	2 28	45.6	23.9
	Cape Virgins: SE. extreme	52 18 35	68 22 12	8 18	2 06	38.7	20.2
	Cape San Diego: Extreme	54 40 35	65 05 53	4 20	10 33	9.9	5.2
	Staten Island, Cape St. John: Light-house, W. pt	54 43 24	63 47 00	4 19	10 32	7.8	6.0
	Port Cork: Observation mark, summit	54 45 16	64 03 00				
	Cape St. Bartholomew: Middle pt	54 53 45	64 45 45				
	Good Success Bay: S. end of beach	54 48 02	65 13 48				
Chile.	Lennox Cove: Bluff, N. end of beach	55 17 00	66 49 00				
	Goree Road: Guanaco Pt	55 19 00	67 10 00	3 50	10 03	6.7	5.2
	Wollaston Island: Middle Cove	55 35 30	67 19 00				
	Barneveldt Islands: Center	55 48 54	66 43 48				
	Cape Horn: South summit, 500 ft	55 58 41	67 16 15				
	Hermite Island: St. Martin Cove	55 51 20	67 34 00	4 07	10 02	4.8	3.8

WEST COAST OF SOUTH AMERICA.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
Chile.	False Cape Horn: S. extreme	55 43 15	68 04 40				
	Ildefonso Island: Highest summit	55 52 30	69 17 30				
	Diego Ramirez Island: Highest summit	56 28 50	68 41 30	3 50	10 03	5.0	3.9
	York Minster Rock: Summit, 800 ft	55 24 50	70 01 30				
	Cape Desolation: S. summit	54 45 40	71 36 10				
	Mount Skyring: Summit, 3,000 ft	54 24 48	72 10 20				
	Noir Island: SE. extreme	54 30 00	73 00 00	2 20	8 33	4.8	3.7
	Landfall Island: Summit of Cape Inman	53 18 30	74 18 15	1 50	8 03	4.7	3.7
	Cape Deseado: Peaked summit	52 55 30	74 36 30				
	Apostle Rocks: W. rocks	52 46 15	74 46 50				
	Cape Pillar: N. cliff	52 42 50	74 42 20	0 32	6 45	4.0	3.1
	Dungeness Point: Light-house	52 23 55	68 25 45	8 19	2 07	39.4	20.6
	Cape Espiritu Santo: NE. cliff	52 39 00	68 34 00	8 20	2 08	39.0	20.4
	Catharine Point: NE. extreme	52 32 00	68 45 20	8 24	2 12	30.0	15.7
	Cape Possession: Light-house	52 17 54	68 57 10	8 35	2 25	39.0	20.4
	Cape Orange: N. extreme	52 28 40	69 24 00				
	Delgada Point: Light-house	52 28 00	69 33 00	8 47	2 40	39.0	20.4
	Cape Gregory: Light-house	52 38 18	70 14 16	9 23	3 20	21.0	11.0
	Cape San Vicente: W. extreme	52 46 20	70 25 25				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF SOUTH AMERICA—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Chile.	Elizabeth Island: NE. bluff	52 49 18	70 37 51	10 24	4 24	8.0	4.2
	Sandy Point: Light-house	53 10 10	70 54 24	11 03	5 03	5.0	2.6
	Cape St. Valentine: Summit, at extreme	53 33 30	70 34 27				
	Port Famine: Observatory	53 38 12	70 58 31	11 58	5 58	6.0	3.1
	Cape San Isidro: Extreme	53 47 00	70 55 03	12 21	6 21	8.0	4.2
	Cape Froward: Summit of bluff	53 53 43	71 17 15	0 28	6 53	7.0	3.7
	Mount Pond: Summit	53 51 45	71 55 30				
	Port Gallant: Wigwam Pt	53 41 45	71 59 41	1 20	7 40	8.0	4.2
	Charles Island: White rock near NW. end	53 43 57	72 04 45				
	Rupert Island: Summit	53 42 00	72 10 42				
	Mussel Bay: Entrance	53 37 10	72 19 30				
	Tilly Bay: Sarah I	53 34 20	72 27 10				
	Borja Bay: Bluff on W. shore	53 31 45	72 34 15	1 54	8 11	5.5	2.9
	Cape Quad: Extreme	53 32 10	72 32 25				
	Barcelo Bay: Entrance	53 30 50	72 38 00				
	Swallow Bay: Shag I	53 30 05	72 47 30	1 53	8 08	5.0	3.9
	Cape Notch: Extreme	53 25 00	72 47 55				
	Playa Parda Cove: Summit of Shelter I	53 18 45	73 00 30	1 31	7 44	4.5	3.5
	Pollard Cove: Entrance	53 15 30	73 12 05				
	Port Angosto: Hay Pt	53 13 40	73 21 30	1 09	7 21	4.0	3.1
	St. Anne Island: Central summit	53 06 30	73 15 30				
	Half Port Bay: Point	53 11 40	73 17 45				
	Upright Port: Entrance	53 06 35	73 16 15				
	Port Tamar: Mouat Islet	52 55 46	73 44 28	0 55	7 07	6.0	4.6
	Port Churruca: Summit of Blanca Pen	53 01 00	73 59 33				
	Valentine Harbor: Observation mount	52 55 00	74 17 45				
	Cape Parker: W. summit	52 42 00	74 13 30				
	Mercy Harbor: Summit of Battle I	52 44 58	74 38 14				
	Mayne Harbor: Observation spot	51 18 29	74 04 00				
	Port Grappler: Observation spot	49 25 19	74 17 39				
	Port Riofrio: Vitalia I	49 12 40	74 23 27				
	Eden Harbor: Observation spot	49 07 30	74 25 10				
	Halt Bay: Observation islet	48 54 20	74 20 55				
	Westminster Hall Islet: E. summit	52 37 18	74 23 10				
	Evangelistas Island: Light-house	52 24 00	75 06 00	0 55	7 08	4.4	3.4
	Cape Victory: Extreme	52 16 10	74 55 00				
	Cape Isabel: W. extreme	51 51 50	75 13 20				
	Cape Santiago: Summit	50 42 00	75 27 45				
	Molyneux Sound: Romalo I	50 17 20	74 51 30				
	Cape Tres Puntas: Summit, 2,000 ft	50 02 00	75 22 00				
	Port Henry: Observation spot	50 00 18	75 13 20	0 30	6 45	4.5	3.5
	Mount Corso: SW. summit	49 48 00	75 34 00				
	Rock of Dundee: Summit	48 06 15	75 40 30				
	Santa Barbara Port: N. extreme obs. pt	48 02 20	75 28 20	0 15	6 30	5.3	4.1
	Guaineco Islands: Speedwell Bay, hill, NE. pt	47 39 30	75 10 00				
	Port Otway: Observation spot	46 49 31	75 18 20	0 10	6 25	5.3	4.1
	Cape Tres Montes: Extreme	46 58 57	75 25 30				
	Cape Raper: Rock close to cape	46 49 10	75 37 55				
	Christmas Cove: SE. extreme	46 35 00	75 31 30				
	Hellyer Rocks: Middle	46 04 00	75 12 00				
	Cape Taytao: W. extreme	45 53 20	75 06 00	0 00	6 13	4.4	3.4
	Socorro Island: S. extreme	44 55 50	75 08 45				
	Mayne Mountain: Summit, 2,080 ft	44 09 00	74 07 45				
	Port Low: Observation islet	43 48 30	73 59 35	12 20	6 10	6.2	4.8
	Huafo Island: S. extreme	43 41 50	74 42 00	12 10	6 00	6.1	3.1
	Port San Pedro: Cove on S. shore	43 19 35	73 41 50				
	Cape Quilan: SW. extreme	43 17 10	74 22 00				
	Corcovado Volcano: Summit, 7,510 ft	43 11 20	72 44 40				
	Minchinmadiva Volcano: S. summit, 8,000 feet	42 48 00	72 30 30				
	Castro: E. end of town	42 27 45	73 45 20	0 01	6 21	18.0	9.1

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF SOUTH AMERICA—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Dalcahue: Chapel	42 23 00	73 36 00				
	Oscuro head: Observation pt	42 04 00	73 25 00				
	Coman Inlet: Olvidada I	42 03 00	72 45 00				
	Port Calbuco: La Picuta	41 46 08	73 07 15	1 10	7 35	14.8	7.5
	San Carlos de Ancud: Light-house	41 46 40	73 52 54	0 04	6 20	5.9	3.0
	Condor Cove: Landing	40 46 19	73 51 00				
	Ranu Cove: Anchorage	40 43 18	73 49 50				
	Muilcalpue Cove: Landing place	40 35 52	73 45 00				
	Milagro Cove: Landing place	40 21 04	73 45 20				
	Laruehuapi Cove: Landing place	40 11 47	73 41 50	0 00	6 13	7.2	3.7
	Valdivia: Niebla Fort light	39 51 37	73 26 25	10 25	4 13	5.6	2.8
	Queule Bay: Choros Pt	39 23 00	73 14 00	10 18	4 05	4.9	2.5
	Mocha Island: Light-house	38 21 22	73 58 06	10 20	5 07	3.3	1.7
	Lebu River: Tucapel Head	37 35 20	73 39 55	10 15	4 02	4.9	2.5
	Yañez Port: Anchorage	37 22 30	73 40 00	10 10	3 55	5.3	2.7
	Lota: Light-house	37 05 20	73 11 13	10 05	3 50	4.9	2.5
	Santa Maria Island: Light-house	36 59 07	73 32 30	10 10	3 55	6.0	3.0
	Talcahuano: Fort Galvez	36 42 00	73 07 27	10 04	3 51	5.3	2.7
	Light on Quinquina I	36 36 45	73 02 49	10 05	3 53	5.0	2.5
	Llico: Village	34 46 02	72 06 12	9 57	3 48	4.1	2.1
	Port San Antonio: Village	33 34 13	71 38 00	9 44	3 34	4.0	2.0
	Aconcagua Mountain: Summit	33 38 30	69 56 30				
	Santiago: Observatory	33 26 42	70 41 32				
	Valparaiso: Playa Ancha Pt. light	33 01 08	71 38 52	9 37	3 26	3.9	2.0
	Site of Fort San Antonio	33 01 52	71 38 42				
	Quintero Point: Summit	32 46 00	71 32 56	9 35	3 25	4.1	2.1
	Pichidanque: SE. pt. of island	32 07 55	71 33 22	9 30	3 20	3.9	2.0
	Tablas Point: SW. extreme	31 51 45	71 34 51	9 26	3 16	4.2	2.1
	Chuapa River: S. entrance pt	31 39 30	71 35 20				
Chile.	Maitencillo Cove: N. head	31 17 05	71 39 21				
	Talinay Mount: Summit	30 50 45	71 39 00				
	Lengua de Vaca: Light-house	30 14 00	71 39 00				
	Port Tongoi: Obs. spot. W. of village	30 15 14	71 31 09	9 15	3 05	4.1	2.1
	Coquimbo: Tortuga Pt. light	29 56 15	71 21 00	8 58	2 48	4.9	2.5
	Smelting works, N. of town	29 56 24	71 21 53				
	N. islet	29 55 10	71 22 21				
	Pajaros Islets: Light-house	29 34 40	71 33 20				
	Choros Islands: SW. pt. of largest id	29 15 45	71 34 38				
	Chañaral Island: Light-house	29 00 50	71 36 40				
	Huasco: Light on mole	28 27 20	71 15 45	8 23	2 10	4.9	2.5
	Herradura de Carrizal: Landing place	28 05 45	71 12 48	8 50	2 38	4.9	2.5
	Port Carrizal: Middle Point	28 04 30	71 11 32				
	Matamoras Cove: Outer pt. S. side	27 54 10	71 09 38				
	Salado Bay: Summit of Cachos Pt	27 39 20	71 03 26				
	Copiapo: Landing place	27 20 00	70 58 45	8 21	2 08	5.0	2.5
	Caldera: Light-house	27 03 15	70 52 54	8 50	2 37	4.9	2.5
	Light on mole head	27 03 15	70 53 45				
	Cabeza de Vaca Point: Extreme	26 51 05	70 51 55				
	Flamenco: SE. corner of bay	26 34 30	70 44 25	9 00	2 47	5.0	2.5
	Chañaral Bay: Observation pt	26 20 00	70 37 25	9 05	2 52	4.9	2.5
	St. Felix I.: Peterborough Cathedral Rock	26 16 12	80 11 43				
	Pan de Azucar Island: Summit	26 09 15	70 43 57				
	Lavata: Cove near SW. pt	25 39 30	70 44 03	9 10	2 57	5.0	2.5
	San Pedro Point: Summit	25 31 00	70 41 18				
	Port Taltal: Light-house	25 25 20	70 34 10	9 20	3 07	4.9	2.5
	Grande Point: Outer summit	25 07 00	70 30 16	9 35	3 22	5.0	2.5
	Paposo Road: Huanillo Pt	25 05 25	70 29 50	9 30	3 17	4.9	2.5
	Reyes Head: Extreme pitch	24 34 30	70 36 29				
	Cobre Bay: Pt. W. of village	24 15 00	70 33 00				
	Jara Head: Summit	23 53 00	70 32 28				
	Antofagasta: Light-house	23 38 50	70 25 18	9 05	2 52	4.7	2.4
	Chimba Bay: E. pt. of large island	23 33 05	70 26 55				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF SOUTH AMERICA—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Chile.	Moreno Mountain: Summit	23 28 30	70 34 56				
	Constitution Cove: Shingle pt. of island	23 26 42	70 37 11				
	Mexillones Mount: Summit	23 06 30	70 31 39	9 35	3 22	3.9	2.0
	Port Cobija: Landing place	22 34 00	70 17 42	9 44	3 31	4.0	2.0
	Tocopilla: Extremity Point	22 06 00	70 13 40	8 55	2 42	4.8	2.4
	San Francisco Head: W. pitch	21 55 50	70 11 17				
	Loa River: Mouth	21 28 00	70 02 45				
	Lobos Point: Outward pitch	21 05 30	70 12 12	9 00	2 47	4.9	2.5
	Pabellon de Pica: Summit	20 57 40	70 10 26				
	Patache Point: Extreme	20 51 05	70 14 40				
	Iquique: Light-house	20 12 30	70 11 20	8 35	2 22	5.0	2.5
	Mexillon Bay: Landing place	19 05 01	70 10 30				
	Pisagua: Pichalo Pt., extreme	19 36 30	70 15 21	8 32	2 20	5.0	2.5
	Gorda Point: W. low extreme	19 19 00	70 17 50				
	Lobos Point: Summit	18 45 40	70 21 50				
	Arica: Iron church	18 28 43	70 20 00	7 49	1 37	5.6	2.8
	Schama Mount: Highest summit	17 58 35	70 52 31				
Peru.	Coles Point: Extreme	17 42 00	71 22 31				
	Ilo: Mouth of rivulet	17 37 00	71 20 01	7 55	1 43	5.3	2.7
	Port Mollendo: Light-house	17 01 00	72 02 53				
	Islay: Custom-house	17 00 00	72 07 16	7 39	1 27	6.2	3.1
	Quilca: W. head of cove	16 42 20	72 27 16				
	Pescadores Point: SW. extreme	16 23 50	73 16 41				
	Atico: E. cove	16 13 30	73 41 31				
	Chala Point: Extreme	15 48 00	74 27 16				
	Lomas: Flagstaff on pt	15 33 15	74 51 01				
	San Juan Port: Needle Hummock	15 20 56	75 09 36	6 47	0 35	3.9	2.0
	Nasca Point: Summit	14 57 00	75 30 46				
	Mesa de Doña Maria: Central summit	14 41 00	75 49 56				
	Carreta Mount: Summit	14 09 50	76 16 36				
	San Gullan Island: N. summit	13 50 00	76 27 31				
	Paraca Bay: N. extreme of W. pt	13 48 00	76 18 31				
	Pisco: Light-house	13 45 00	76 10 00	6 16	0 04	3.8	1.9
	Chincha Islands: Boat slip, E. side N. id	13 38 20	76 24 15				
	Frayles Point: Extreme	13 01 00	76 31 06				
	Asia Rock: Summit	12 48 00	76 38 11				
	Chilca Point: SW. pitch	12 31 00	76 48 56				
	Morro Solar: Summit	12 11 30	77 02 31				
	San Lorenzo Island: Light-house	12 04 03	77 15 44				
	Callao: Palominos Rock Light	12 08 15	77 14 45	5 47	12 00	3.5	1.8
	Pescadores Islands: Summit of largest	11 47 10	77 16 11				
	Pelado Island: Summit	11 27 10	77 50 04				
	Supé: W. end of village	10 49 45	77 43 42				
	Huarmey: W. end of sandy beach	10 06 15	78 10 02	5 08	11 21	2.1	1.1
	Colina Redonda: Summit	9 38 35	78 21 33				
	Samanco Bay: Cross Pt	9 15 30	78 30 03				
	Chimbote: Village, N. part	9 04 40	78 35 57	4 50	11 03	2.0	1.0
	Chao Islet: Center	8 46 30	78 45 16				
	Guanape Islands: Summit of highest	8 34 50	78 56 53				
	Huanchaco Point: SW. extreme	8 05 40	79 06 46				
	Malabrigo Bay: Rocks	7 42 40	79 26 00	4 19	10 32	2.1	1.1
	Pacasmayo: Light-house	7 23 40	79 33 15				
	Eten Head: Light-house	6 55 50	79 51 30	4 04	10 17	2.5	1.3
	Lambayeque: Beach opposite	6 46 00	79 57 55				
	Lobos de Afuera Island: Cove on E. side	6 46 45	80 42 54				
	Lobos de Tierra Island: Central summit	6 26 45	80 51 56				
	Aguja Point: W. cliff summit	5 55 30	81 09 19				
	Paita, Saddle: S. summit	5 12 00	81 05 36				
	Paita: Light-house	5 05 00	81 07 03	3 20	9 33	3.5	1.8
	Parinas Point: Extreme	4 40 50	81 17 01				
	Cape Blanco: Under middle of high cliff	4 16 40	81 12 01				
	Tumbez: Malpelo Pt	3 30 42	80 28 12				

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF SOUTH AMERICA—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Ecuador.	Guayaquil River: Light on Santa Clara I.	3 10 40	80 25 29	4 00	10 13	10.0	5.1
	Guayaquil, Concejo: S. pt. of city	2 12 24	79 52 19	7 00	1 00	11.0	5.6
	Puna: Mandinga Pt. light	2 44 30	79 53 45	......	......	......	......
	Point Santa Elena: Veintemilla light	2 12 00	80 59 00	3 00	9 13	7.9	4.0
	Plata Isle: E. pt	1 16 55	81 03 55	......	......	......	......
	Cape San Lorenzo: Marlingspike Rock	1 03 30	80 55 55	......	......	......	......
	Manta Bay: Light-house	0 56 50	80 42 50	3 10	9 23	7.5	3.8
	Caraques Bay: Punta Playa	0 35 25	80 25 24	......	......	......	......
	Cape Pasado: Extreme	0 21 30	80 30 37	3 15	9 28	9.9	5.0
		Lat. N.					
	Point Galera: N. extreme	0 50 10	80 05 40	......	......	......	......
	Cape San Francisco: SW. extreme	0 40 00	80 07 55	......	......	......	......
Colombia.	Esmeralda River: Light-house	1 03 30	79 42 00	......	......	......	......
	Mangles Point: S. pt. of creek entrance	1 36 00	79 03 30	......	......	......	......
	Tumaco: S. pt. of El Morro I	1 49 36	78 45 29	3 35	9 48	13.2	7.1
	Guascama Point: Extreme	2 37 10	78 24 24	......	......	......	......
	Gorgona Island: Watering Bay	2 58 10	78 11 16	......	......	......	......
	Buenaventura: Basan Pt	3 49 27	77 11 45	6 00	12 13	13.2	7.1
	Chirambiri Point: N. extreme	4 17 06	77 29 44	......	......	......	......
	Cape Corrientes: SW. extreme	5 28 46	77 33 28	3 40	9 53	13.1	7.0
	Cupica Bay: Entrance to Cupica River	6 41 19	77 30 31	3 30	9 43	13.3	7.2
	Cape Marzo: SE. extreme	6 49 45	77 40 55	......	......	......	......
	Isla del Rey: Extreme of Cocos Pt	8 12 30	78 54 40	3 00	9 13	15.7	8.5
	Darien Harbor: Graham Pt	8 28 50	78 05 35	......	......	......	......
	Flamenco Island: N. Pt	8 54 30	79 31 15	......	......	......	......
	Chepillo Island: Center	8 56 32	79 07 55	3 05	9 18	16.0	8.7
	Point Chamé: Extreme	8 39 00	79 41 45	3 30	9 42	15.0	8.1

ISLANDS IN THE ATLANTIC OCEAN.

Coast.	Place.	Lat.	Long.	H. W.	L. W.	Spg.	Neap.
	Færoe Islands, Strom Islet: Thorshaven Fort flagstaff	62 02 26	6 43 08	......	......	......	......
	Halderoig Islet: Halderoig Church	62 18 20	7 00 36	......	......	......	......
	Numken Rock	61 23 00	6 45 30	......	......	......	......
	Rockall Islet: Summit, 70 feet	57 35 52	13 42 21	......	......	......	......
Azores Islands.	Corvo Island: S. pt	39 40 07	31 08 00	......	......	......	......
	Flores Island: Santa Cruz Fort	39 27 00	31 08 49	......	......	......	......
	Fayal Channel: N. Magdalen Rock	38 32 09	28 34 00	......	......	......	......
	Fayal Island, Horta: Castle of Santa Cruz	38 31 45	28 37 39	11 30	5 18	3.9	1.8
	Caldera: summit 3,351 ft	38 34 30	28 44 00	......	......	......	......
	Pico Island: Summit	38 25 00	28 28 12	......	......	......	......
	St. George Island: Light-house	38 40 30	28 13 00	......	......	......	......
	Graciosa Island: Santo Fort light	39 05 24	28 00 45	......	......	......	......
	Terceira Island: Monte del Brazil, near Angra	38 38 20	27 13 45	0 20	6 32	4.4	2.0
	St. Michael Island: Custom-house, Ponta Delgada	37 44 16	25 40 40	......	......	......	......
	Pt. Arnel light	37 49 20	25 08 21	0 15	6 27	5.7	2.6
	Santa Maria Island: Villa do Porto light	36 56 00	25 10 00	......	......	......	......
	Formigas Islands: Highest rock	37 16 44	24 47 06	......	......	......	......
Madeira Is.	Porto Santo Island: Light-house	33 03 15	16 16 20	0 40	6 52	6.6	3.0
	Desertas: Chao I., Sail Rock	32 35 45	16 33 30	......	......	......	......
	Madeira Island: Funchal light	32 37 42	16 55 16	0 35	6 47	6.6	3.0
	Fora I. light-house	32 43 14	16 39 31	......	......	......	......
	Pico Ruivo, summit 6,056 ft	32 45 00	16 57 30	......	......	......	......
	Pargo (W.) Pt	32 48 07	17 16 05	......	......	......	......

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS IN THE ATLANTIC OCEAN—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Salvage Islands: Light-house, Gran Salvage I	30 08 00	15 54 00				
Canary Islands.	Alegranza Island: Delgada Pt. light	29 23 50	13 29 31				
	Lanzarote Island: Port Naos light	28 57 24	13 33 07	0 50	7 00	8.5	3.9
	Pechinguera Pt. light	28 50 56	13 52 05				
	Lobos Island: Martino Pt. light	28 45 25	13 49 13				
	Fuerta Ventura Island: Jandia Pt. light	28 03 00	14 31 35				
	Gran Canaria: Isleta Pt. light	28 10 42	15 25 11	0 40	6 50	9.3	4.3
	Palmas light	28 07 06	15 24 56				
	Teneriffe Island: Anga Pt. light	28 35 25	16 08 11				
	Santa Cruz, Br. consulate	28 28 12	16 15 09	1 15	7 27	7.8	3.6
	Summit of peak, 12,180 ft	28 16 35	16 38 02				
	Gomera Island: Port Gomera	28 08 00	17 05 55				
	Ferro Island: Port Hierro	27 46 30	17 54 22				
	Palma Island: Light, NE. pt	28 50 06	17 47 01	0 20	6 30	8.6	4.0
Cape Verde Islands.	San Antonio Island: Bull Pt. light	17 06 50	24 59 15				
	Summit, 7,400 ft	17 04 00	25 17 00				
	St. Vincent Island: Porto Grande light	16 54 36	25 01 12	5 50	12 00	3.3	1.5
	St. Lucia Island: N. pt	16 49 00	24 47 08				
	Raza Island: E. pt	16 38 00	24 38 08				
	St. Nicholas Island: Light-house	16 34 00	24 16 00				
	Sal Island: N. pt. light	16 50 50	22 54 55				
	S. pt	16 34 00	22 55 42	7 30	1 20	4.4	2.0
	Boavista Island: NW. pt	16 13 20	22 55 44				
	NE. pt	16 11 00	22 42 00				
	Light-house	16 09 10	22 57 20				
	Mayo Island: English Road	15 07 30	23 12 42				
	St. Jago Island: Reta Pt. light	15 18 06	23 47 06				
	Porto Praya, S. light	14 53 40	23 31 45	5 50	12 00	4.8	2.2
	Fogo Island: N. S. da Luz, village	14 53 00	24 30 38				
	Brava Island: Light-house	14 50 30	24 40 00				
Bermuda Is.	Ireland Island: Dock yard clock tower	32 19 22	64 49 35	7 04	0 52	4.0	2.6
	Bastion C	32 19 37	64 49 15				
	Hamilton Island: Gibbs Hill light	32 15 05	64 49 40				
	St. Davids Island: Light-house	32 21 40	64 38 40				
	St. Paul Rocks: Summit, 64 ft	0 55 30	29 22 28				
		Lat. S.					
	Rocas Reef: NW. sandy islet	3 51 30	33 49 29	5 05	11 18	10.0	4.6
	Fernando Noronha: The Pyramid	3 50 30	32 25 29	5 00	11 13	6.0	2.7
	Ascension Island: Fort Thornton	7 55 20	14 24 35	5 20	11 30	2.0	0.9
	St. Helena Island: Obs. Ladder Hill	15 55 00	5 43 03	3 00	9 10	2.8	1.3
	Martin Vaz Rocks: Largest islet	20 27 42	28 46 57	3 35	9 48	3.5	1.6
	Trinidad Island: SE. pt	20 30 32	29 14 56	3 40	9 53	4.0	1.8
	Inaccessible Island: Center	37 19 00	12 23 00				
	Tristan d'Acunha Islands: NW. pt	37 02 48	11 18 39	12 50	5 40	5.2	2.4
	Gough Island: Penguin Islet	40 19 11	9 56 11				
Falkland Islands.	Port Egmont: Observation spot	51 21 26	60 04 52	7 20	1 08	10.7	5.6
	Mare Harbor: Observation spot	51 04 11	58 30 56				
	Port Louis: Flagstaff, govt. house	51 32 20	58 08 04	5 31	11 27	4.3	2.2
	Port Stanley: Governor's house	51 41 10	57 51 30				
	Cape Pembroke: Light-house	51 40 40	57 41 48				
	South Georgia Island: N. cape	54 04 45	38 15 00				
	Shag Rocks: Center	53 48 00	43 25 00				
	Sandwich Islands: S. Thulé	59 34 00	27 45 00				
	Traverse I. volcano	55 57 00	26 33 00				

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS IN THE ATLANTIC OCEAN—Continued.

Coast.	Place.	Lat. S.	Long W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	New S. Orkney Is.: E. pt. Laurie I.	60 54 00	44 25 00	......	......	......	......
	E. summit Coronation I., 5,397 ft	60 46 00	45 53 00	......	......	......	......
	New S. Shetland Islands, Deception Island: Port Foster	62 55 36	60 35 00	......	......	......	......
			Long. E.				
	Bouvets Island (Circumcision): Center	54 16 00	6 14 00	......	......	......	......

ATLANTIC COAST OF EUROPE.

Coast.	Place.	Lat. N.	Long. W.	H. W.	L. W.	Spg.	Neap.
Great Britain.	Greenwich: Observatory	51 28 38	0 00 00	1 10	7 46	18.8	12.6
	Oxford: University Observatory	51 45 34	1 15 04	......	......	......	......
	Cambridge: Observatory	52 12 52	0 05 40	......	......	......	......
			Long. E.				
	North Foreland: Light-house	51 22 28	1 26 48	11 24	5 53	16.8	8.4
	South Foreland: Light-house	51 08 23	1 22 22	11 09	5 43	19.8	10.0
	Dungeness: Light-house	50 54 47	0 58 18	10 35	4 23	21.5	11.0
	Beachy Head: Light-house	50 44 15	0 13 00	11 10	4 58	19.8	10.1
			Long. W.				
	Southsea Castle: Light-house	50 46 35	1 05 15	......	......	......	......
	Portsmouth: Observatory	50 48 03	1 05 58	11 31	4 19	13.2	6.7
	Southampton: Royal Pier light	50 53 45	1 24 00	0 35	6 48	12.8	6.5
	Hurst Castle: W. light	50 42 07	1 33 04	11 05	4 53	12.2	6.2
	Needles Rocks: Old light-house	50 39 42	1 35 25	......	......	......	......
	St. Catharine: New light-house	50 34 30	1 17 47	......	......	......	......
	Portland: Notch Bill light	50 31 10	2 27 30	6 29	0 09	6.7	1.0
	Start Point: Light-house	50 13 18	3 38 28	5 25	11 38	14.9	6.8
	Plymouth: Breakwater light	50 20 02	4 09 27	5 20	11 33	15.3	7.0
	Eddystone: Light-house	50 10 49	4 15 53	......	......	......	......
	Falmouth: St. Anthony Pt. light	50 08 30	5 01 00	......	......	......	......
	Lizard Point: W. light-house	49 57 40	5 12 06	4 45	10 58	14.2	6.5
	Porthcurnow: SE. cor. telegraph co.'s sta.	50 02 44	5 39 18	......	......	......	......
	Lands End: Longships light-house	50 04 10	5 44 45	......	......	......	......
	Scilly Ilands: St. Agnes light-house	49 53 33	6 20 38	4 15	10 28	15.9	7.3
	Trevose Head: Light-house	50 33 00	5 01 55	......	......	......	......
	Bideford: High light-house	51 04 00	4 12 30	5 45	11 58	22.7	11.4
	Lundy Island: Light-house, N. pt	51 12 05	4 40 35	5 00	11 13	26.9	13.5
	Bristol: Cathedral	51 27 24	2 35 55	7 00	0 48	31.3	15.7
	Cardiff: Light-house, W. pier	51 27 48	3 09 42	6 45	0 33	36.2	18.1
	Swansea: Light-house, W. pier	51 36 50	3 56 00	5 45	11 58	27.1	13.6
	Caldy Island: Light-house	51 37 52	4 40 59	5 40	11 53	25.3	12.7
	St. Anns: Upper light-house	51 41 00	5 10 30	5 41	11 54	24.0	12.0
	Smalls Rocks: Light-house	51 43 15	5 40 15	5 40	11 53	20.9	10.5
	Aberystwith: Light-house	52 24 20	4 05 40	7 25	1 13	14.2	7.1
	Bardsey Island: Light-house	52 45 00	4 47 50	7 24	1 12	14.9	7.5
	South Stack: Light-house on rocks	53 18 30	4 42 00	......	......	......	......
	Holyhead: Light-house on old pier	53 18 54	4 37 01	10 00	3 48	15.8	7.9
	Skerries Rocks: Light-house, highest I.	53 25 15	4 36 20	......	......	......	......
	Bidstone: Light-house on hill	53 24 02	3 10 42	......	......	......	......
	Liverpool: Rock light	53 26 38	3 02 27	......	......	......	......
	Observatory	53 24 04	3 04 16	11 08	5 27	27.6	14.0
	Morecambe Bay: Fleetwood high light	53 55 03	3 00 20	11 00	4 48	27.4	13.9
	Calf of Man: Upper light-house	54 03 14	4 49 37	......	......	......	......
	Isle of Man: Ayre Pt. light-house	54 24 56	4 22 01	10 55	4 43	19.7	10.0
	St. Bees: Light-house	54 30 50	3 37 50	......	......	......	......
	White Haven: W. pier-head light	54 33 00	3 36 00	11 00	4 48	25.9	13.1
	Mull of Galloway: Light-house	54 38 10	4 51 20	11 05	4 53	14.8	8.9
	Ayr, Firth of Clyde: Light-house, N. side harbor	55 28 10	4 38 10	11 40	5 28	8.7	5.2
	Troon: Light-house, inner pier	55 32 55	4 41 00	......	......	......	......

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Great Britain.	Ardrossan: S. breakwater light	55 38 27	4 49 28	11 35	5 23	8.8	5.3
	Pladda Island: Light-house	55 26 00	5 07 09				
	Glasgow: Observatory	55 52 43	4 17 39	0 55	7 08	11.2	6.7
	Cantyre: Light-house	55 18 39	5 48 00	10 20	4 08	4.0	2.4
	Rhynns of Islay: Light-house	55 40 20	6 30 46				
	Oban: Light-house on N. pier	56 24 50	5 28 20	5 10	11 22	12.8	7.7
	Skerryvore Rocks: Light-house	56 19 22	7 06 32				
	Barra Head: Light-house	56 47 08	7 39 09	5 35	11 47	11.1	4.8
	Glas Island: Light-house, Scalpay I.	57 51 25	6 38 28				
	Stornoway: Arnish Pt. light	58 11 28	6 22 10	6 35	0 22	13.4	5.7
	Butt of Lewis: Light-house	58 30 40	6 16 01				
	Cape Wrath: Light-house	58 37 30	4 59 41				
	Dunnet Head: Light-house	58 40 16	3 22 25				
	Kirkwall (Orkneys): New pier-head light	58 59 15	2 57 33	9 57	3 44	9.8	4.2
	Startpoint (Orkneys): Light-house	59 16 45	2 22 25				
	North Ronaldsay: Light-house	59 23 24	2 22 45				
	Fair Isle Skroo: Light-house	59 33 00	1 36 30	10 50	4 37	5.0	2.2
	Sumburgh Head: Light-house	59 51 15	1 16 20	9 35	3 22	5.2	2.2
	Blackness (Shetland Is.): Light-house pier	60 08 02	1 16 02				
	Lerwick (Shetland Is.): Fort	60 09 22	1 08 41	10 20	4 17	6.0	2.6
	Hillswickness (Shetland Is.): S. extreme	60 27 20	1 29 50				
	Balta I. (Shetland Is.): Cairn on E. side	60 44 25	0 47 30	9 30	3 17	6.4	2.7
	Pentland Skerries: Upper light-house	58 41 22	2 55 25	10 00	3 47	9.8	4.2
	Tarbertness: Light-house	57 51 54	3 46 30				
	Buchanness: Light-house	57 28 15	1 46 22	0 24	6 36	11.2	6.1
	Aberdeen (Girdleness): Light-house	57 08 33	2 04 06	0 50	7 02	11.7	6.4
	Buddonness: Upper light-house	56 28 07	2 44 53	1 56	8 08	15.5	8.5
	Bell Rock: Light-house	56 26 03	2 23 06				
	May Island: Light-house	56 11 00	2 33 22				
	Inch Keith Rock: Light-house	56 02 09	3 08 05				
	Edinburgh: Observatory	55 57 23	3 10 54	1 58	8 11	16.5	8.9
	Berwick: Light-house	55 46 00	1 59 00	2 08	8 28	15.0	7.5
	Farn Island: NW. light-house	55 37 00	1 39 00				
	Coquet Island: Light-house	55 20 06	1 32 00				
	Tynemouth: Souter Point light-house	54 58 10	1 21 30				
	North Shields: Light-house	55 00 30	1 26 00	3 11	9 31	14.8	7.4
	Sunderland: N. pier light	54 55 07	1 21 30	3 12	9 32	14.5	7.3
	Hartlepool: Light-house	54 41 51	1 10 19	3 21	9 43	14.2	7.0
	Flamborough: New light-house	54 07 00	0 05 00	4 20	10 36	15.8	8.8
	Humber River: Killingholme middle light	53 39 00	0 12 00				
			Long. E.				
	Spurn Head: Upper light-house	53 34 45	0 07 10	5 16	11 29	18.5	10.2
	Lowestoft: Light-house	52 29 14	1 45 24	9 47	3 35	6.2	3.6
	Orfordness: N. light-house	52 05 00	1 34 30	11 05	4 53	7.8	4.5
	Harwich: Landguard Pt. light	51 56 05	1 19 10	11 56	5 44	11.2	6.6
			Long. W				
	Cape Clear: Old light-house	51 26 02	9 29 03	3 50	10 03	8.8	4.4
	Fastnet Rock: Light-house	51 23 18	9 36 25				
	Mount Gabriel: Ordnance survey station	51 33 24	9 32 44				
	Castlehaven: Light-house	51 31 00	9 10 20	4 10	10 23	10.6	5.3
	Mizen Hill: Ordnance survey station	51 27 41	9 48 19				
	Bantry Bay: Roancarrig light	51 39 10	9 44 49				
	Bull Rock: Light-house	51 35 30	10 18 03				
	Skelligs Rocks: Light-house	51 46 14	10 32 45				
	Valentia: Light-house	51 56 00	10 19 16	3 30	9 43	10.8	4.6
	Port Magee	51 53 08	10 23 17				
	Dingle Bay: Light at entrance	52 07 15	10 15 30	3 40	9 53	10.7	4.6
	Blasket Islands: Westernmost rock	52 04 30	10 40 00				
	Smerwick: Signal tower	52 13 46	10 21 40	3 40	9 53	10.7	4.6
	Tralee Bay: Light-house	52 16 14	9 52 53	3 50	10 03	12.3	5.3
	Beeves Rocks: Light-house	52 39 00	9 01 18				
	Limerick: Cathedral	52 40 04	8 37 23	6 00	0 13	18.7	8.0
	Shannon River: Loop Head light	52 33 38	9 55 54				

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Great Britain.	Eeragh Island: Light-house	53 08 55	9 51 30				
	Arran Island: Light-house	53 07 38	9 42 06	4 15	10 28	13.4	5.7
	Galway: Mutton I. light	53 15 13	9 03 10	4 19	10 19	15.1	6.4
	Golam Head: Tower	53 13 46	9 46 03				
	Slyne Head: N. light-house	53 23 58	10 14 01	4 16	10 29	13.2	5.7
	Clifden Bay: Gortrumnagh Hill	53 29 47	10 03 54				
	Tully Mountain: Ordnance survey station	53 35 00	10 00 15				
	Inishboffin: Lyon Head light	53 36 40	10 09 40	4 20	10 33	12.1	5.2
	Inishturk Island: Tower	53 42 27	10 06 41				
	Clew Bay: Inishgort light	53 49 34	9 40 12				
	Newport: Church	53 53 06	9 32 56				
	Clare Island: Light-house	53 49 30	9 59 00				
	Blacksod Point: Light-house	54 05 45	10 03 34				
	Eagle Island: W. light-house	54 17 00	10 05 31				
	Broadhaven: Guba Cashel light	54 16 00	9 53 00	4 50	11 03	10.4	4.5
	Dounpatrick Head: Ordnance survey station	54 19 36	9 20 41				
	Anghris Head: Ordnance survey station	54 16 33	8 46 02				
	Knocknarea: Tumulus	54 15 30	8 34 25				
	Sligo Bay: Black Rock light	54 18 00	8 37 00	5 10	11 23	11.4	5.3
	Knocklane: Ordnance survey station	54 20 50	8 40 14				
	Killybegs (Donegal Bay): St. Johns Pt. light	54 34 08	8 27 33	5 03	11 16	11.2	4.8
	Rathlin O'Birne Islet: Light-house	54 39 47	8 49 52				
	Aran Island: Rinrawros light	55 00 52	8 33 48				
	Bloody Foreland: Ordnance survey station	55 08 13	8 15 38				
	Tory Island: Light-house	55 16 26	8 15 00				
	Horn Head: Ordnance survey station	55 12 31	7 57 15				
	Melmore Head: Tower	55 15 14	7 47 12	5 28	11 41	11.6	5.3
	Fanad Point: Light-house	55 16 33	7 37 53				
	Glashedy Island: Ordnance survey station	55 19 07	7 23 51				
	Malin Head: Tower	55 22 50	7 22 22				
	Inishtrahull: Light-house	55 25 55	7 13 37				
	Inishowen Head: E. light-house	55 13 38	6 55 38				
	Moville: New Pier	55 10 20	7 02 20	6 55	0 43	7.5	3.4
	Londonderry: Cathedral	54 59 40	7 19 25	7 48	1 35	8.0	3.6
	Scalp Mountain: Ordnance survey station	55 05 23	7 21 51				
	Benbane Head: Summit	55 15 03	6 28 45				
	Rathlin Island: Altacarry light-house	55 18 05	6 10 45				
	Maiden Rocks: W. light-house	54 55 47	5 44 18	10 30	4 18	6.7	4.5
	Lough Larne: Farres Pt. light-house	54 51 07	5 47 21				
	Belfast Bay: Light, east side	54 40 20	5 49 30	10 42	4 06	9.3	6.3
	Mew Islands: Light-house	54 41 50	5 31 30				
	Donaghadee: Light-house	54 38 45	5 32 01	11 00	4 48	11.1	7.4
	South Rock: Light vessel	54 24 04	5 22 20				
	Dundrum Bay: St. John Pt. light	54 13 30	5 39 30				
	Carlingford Lough: Haulbowline Rk. lt.	54 01 10	6 04 45	10 45	4 33	15.8	9.2
	Drogheda: Light-house	53 43 00	6 15 00	10 45	4 33	11.6	6.8
	Rockabill: Light-house	53 35 47	6 00 20				
	Howth Peninsula: Bailey light	53 21 40	6 03 06	10 55	4 43	12.7	7.5
	Dublin: Observatory	53 23 13	6 20 30				
	N. wall light	53 20 47	6 13 33				
	Poolbeg: Light-house	53 20 30	6 09 00	11 00	4 48	13.0	7.6
	Kingstown: E. pier light	53 18 10	6 07 30	10 52	4 27	10.9	6.4
	Killiney Hill: Mapas obelisk	53 15 52	6 06 37				
	Bray Head: Ordnance survey station	53 10 39	6 04 55	10 30	4 18	11.8	6.9
	Wicklow: Upper light	52 57 54	6 00 08	10 10	3 58	8.7	5.1
	Tara Hill: Summit	52 41 55	6 13 01				
	Black Stairs Mountain: Ordnance survey station	52 32 55	6 48 17				
	Tory Hill: Ordnance survey station	52 20 53	7 07 31				
	Wexford: College	52 20 04	6 28 15	7 05	0 53	4.9	2.9
	Forth Mount: Ordnance survey station	52 18 57	6 33 41				
	Tuskar Rock: Light-house	52 12 09	6 12 35	5 30	11 43	8.8	5.1
	Great Saltee: S. end	52 06 41	6 37 15				
	Waterford: Hoop Pt. light	52 07 25	6 55 53	5 05	11 18	12.3	6.2

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Great Britain.	Waterford: Cathedral	52 15 33	7 06 24				
	Great Newton Head: Metal Man Tower	52 08 13	7 10 15				
	Dungarvan: Ballinacourty light	52 04 27	7 33 05	5 00	11 13	12.4	6.2
	Knockmealdown Mount: Ordnance survey station	52 13 39	7 54 54				
	Helvick Head: Ordnance survey station	52 03 00	7 32 39				
	Mine Head: Light-house	51 59 33	7 35 08				
	Youghal: Light-house	51 56 34	7 50 34	5 02	11 15	12.6	6.3
	Capel Island: Tower	51 52 54	7 51 10				
	Ballycottin: Light-house	51 49 30	7 59 00	4 40	10 53	11.8	5.9
	Cork Harbor: Haulbowline Coal Wharf	51 50 33	8 18 20				
	Queenstown: Roches Pt. light	51 47 33	8 15 14	4 33	10 59	11.6	5.8
	Kinsale: Light-house, S. pt	51 36 11	8 31 58	4 30	10 43	11.4	5.7
	Seven Heads: Tower	51 34 14	8 42 51	4 20	10 33	10.7	5.3
	Galley Head: Light on summit	51 31 50	8 57 10				
	Stag Rocks: Largest	51 28 05	9 13 27				
	Alderney Harbor: Old pier light	49 43 00	2 12 00	6 21	0 16	17.2	7.6
	St. Heliers: Light on Victoria Pier	49 10 29	2 06 44	6 09	0 00	31.2	13.6
			Long. E.				
Norway.	Vardo: Fortress	70 22 00	31 07 30	5 40	11 57	9.0	5.1
	Vadso: Light-house	70 04 00	29 45 00				
	North Cape: Extreme	71 11 00	25 40 00				
	Fruholm: Light-house	71 06 00	23 59 00				
	Hammerfest: Light-house	70 40 15	23 40 00	2 20	8 40	8.3	4.7
	Tromso: Observatory	69 39 12	18 57 00	1 35	7 48	7.8	4.4
	Hekkingen: Light-house	69 36 05	17 50 15				
	Andenes: Light-house	69 19 30	16 08 00	0 42	6 55	7.0	4.0
	Lodingen (Hjertholm): Light-house	68 24 40	16 02 30				
	Lofoten Island: Skraaven I. light	68 09 20	14 40 40				
	Glopen light	67 53 15	13 04 30				
	Gryto: Light-house	67 23 15	13 52 30				
	Stot: Light-house	66 56 35	13 28 50				
	Trænen: Soe Islet light	66 25 50	11 59 50	11 35	5 23	6.9	3.3
	Bronnosund: Light-house	65 28 40	12 13 30				
	Villa: Light-house	64 32 55	10 42 10				
	Halten Island: Light-house	64 10 25	9 24 50				
	Koppem	63 48 25	9 44 45				
	Agdenes: Light-house	63 38 45	9 45 20				
	Trondheim: Mumkholmen flagstaff	63 27 04	10 23 30	11 18	5 04	8.4	4.1
	Grip: Church	63 13 11	7 36 05				
	Christiansund: Storvaden	63 07 01	7 43 35	11 00	4 48	5.0	2.9
	Freikallen	63 03 04	7 46 04				
	Hestskjaer: Light-house	63 05 00	7 29 55				
	Stemshesten	62 58 49	7 12 32				
	Ærstenen: Light-house	62 48 20	6 36 10				
	Svinoen Islet	62 19 38	5 16 25				
	Hjœrringa Mountain: Summit	62 11 12	5 07 59				
	Hornelen Mountain: Summit	61 51 21	5 15 11				
	Batalden Island: Store	61 38 40	4 47 38				
	Kinnsund: Light-house	61 33 35	4 46 45				
	Alden	61 19 16	4 47 14				
	Helliso: Light-house	60 45 05	4 42 55				
	Bergen: Cathedral	60 23 37	5 20 15	10 15	3 55	4.1	2.1
	Lorstakken Mountain: Summit	60 21 39	5 19 35				
	Marstenen Islet: Light-house	60 07 50	5 01 00				
	Furen Islet	59 57 44	5 03 30				
	Ulsire: Light-house	59 18 20	4 52 35				
	Hvidingso: Light-house	59 03 10	5 24 20				
	Port Stavanger: Light-house	58 58 30	5 45 20	9 43	3 40	1.9	0.8
	Obristadbrœkke: Light-house	58 39 25	5 33 35				
	Synesvarde Mountain: Summit	58 36 56	5 49 08				
	Kompas Mountain: Summit	58 25 51	5 58 49				
	Lister: Light-house	58 06 25	6 34 20				
	Lindesnes: Light-house	57 58 55	7 03 10				
	Ryvingen Island: Light-house	57 58 00	7 29 50				
	Christianssand: Odderoen light	58 07 50	8 00 30	4 16	10 15	1.1	0.5

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Norway.	Okso: Light-house	58 04 15	8 03 30				
	Hamberg: Mill	58 15 02	8 31 36				
	Arendal Inlet: Inner Torungerne light	58 24 40	8 47 55	4 17	10 10	1.0	0.7
	Jomfruland: Light-house	58 51 50	9 36 15				
	Langotangen: Light-house	58 59 25	9 45 50				
	Langesund: Church	59 00 01	9 45 14				
	Frederiksværn: Lookout tower	58 59 34	10 03 28	4 34	10 00	1.3	1.0
	Svenor: Light-house	58 58 05	10 09 26				
	Fœrder Islet: Light-house	59 01 35	10 31 55				
	Fulehuk: Light-house	59 10 30	10 36 25				
	Basto: Light-house	59 23 10	10 32 45				
	Horten: Church	59 25 34	10 29 52				
	Holmestrand: Church	59 29 23	10 19 15				
	Drobak: Church	59 39 52	10 38 08				
	Oscarsberg: Fort flagstaff	59 40 21	10 36 55				
	Christiania: Observatory	59 54 44	10 43 35	5 22	10 37	1.2	0.9
	Stromtangen (Torgauten): Light-house	59 09 00	10 50 15				
	Fredriksten: Fort clock tower	59 07 08	11 24 09				
	Torbjornskjær: Light-house	58 59 45	10 47 20				
	Koster: Light-house	58 54 05	11 00 45				
Sweden.	Stromstad: Steeple	58 56 24	11 10 28				
	Nord Koster Islands: Light-house	58 54 12	11 00 36				
	Wadero Island: Light-house	58 32 45	11 02 16				
	Hollo Island: Light-house	58 20 12	11 13 24				
	Paternoster Rocks: Light-house	57 53 49	11 28 04				
	Gottenburg: Signal station	57 40 58	11 53 54				
	Nidingen Islet: Light-house	57 18 15	11 54 16				
	Warberg: Castle tower	57 06 26	12 14 32				
	Falkenberg: Church	56 54 08	12 29 48				
	Halmstad: Palace	56 40 21	12 51 38				
	Engelholm: Church	56 14 40	12 51 47				
	Kullen Point: Light-house	56 18 06	12 27 11				
	Helsingborg: Light-house	56 02 37	12 41 30				
	Landskrona: Light-house	55 52 00	12 49 48				
	Malmo: Light-house	55 36 47	12 59 49				
	Falsterbo: Light-house	55 23 00	12 49 02				
	Trelleborg: Light-house	55 22 00	13 09 20				
	Ystad: Light-house	55 25 42	13 49 38				
	Sandhammaren: Light-house	55 22 58	14 11 10				
	Hano Island: Light-house	56 00 54	14 50 57				
	Karlshamn: Light-house	56 10 04	14 52 02				
	Karlskrona: Stumholm Tower	56 09 45	15 36 05				
	Oland Island: Light on S. pt	56 11 50	16 24 04				
	Gottland Island: Hoburg light, S. pt	56 55 18	18 11 06				
	Ostergarns light	57 26 29	18 59 27				
	Faro Island: Holmadden light	57 57 24	19 22 36				
	Sparo Vestervik: Granso light	57 45 38	16 40 36				
	Haradsskar Islet: Light-house	58 08 52	16 59 22				
	Norrkopings Inlopp: Light-house	58 17 55	16 11 28				
	Landsort: Light-house	58 44 26	17 52 09				
	Stockholm: Observatory	59 20 35	18 03 30				
	Upsala: Observatory	59 51 31	17 37 39				
	Norrtelge: Inn	59 45 24	18 41 34				
	Soderarm: Light-house	59 45 15	19 24 34				
	Svartklubben: Light-house	60 10 35	18 49 49				
	Osthammar: Church	60 15 19	18 22 36				
	Oregrund: Clock tower	60 20 26	18 26 33				
	Djursten: Light-house	60 22 15	18 24 21				
	Forsmark: Church	60 22 26	18 09 49				
	Orskar Rock: Light-house	60 31 41	18 22 38				
	Gefle: Church	60 40 29	17 08 29				
	Eggegrund Islet: Light-house	60 43 48	17 33 50				
	Hamrange: Church	60 55 57	17 02 57				
	Soderhamn: Court-house	61 18 22	17 04 18				
	Enanger: Church	61 32 54	17 01 51				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Sweden.	Hudiksvalls: Court-house	61 43 57	17 07 37				
	Gnarp: Church	62 02 51	17 16 22				
	Sundsvall: Church	62 23 30	17 19 05				
	Lungo: Light-house	62 38 35	18 05 05				
	Skags Head: Light-house	63 11 55	19 02 50				
	Holmogadd: Light-house	63 35 34	20 45 35				
	Umea: Bredekar Light	63 39 33	20 18 35				
	Bjuroklubb: Light-house	64 28 50	21 34 45				
	Pitea	65 19 10	21 30 00				
	Rodkallen: Light-house	65 18 53	22 21 55				
	Maloren: Light-house	65 31 30	23 34 00				
Russia.	Tornea: Light-house	65 48 30	24 12 00				
	Uleaborg: Karlo I. light	65 02 20	24 34 00				
	Ulko Kalla Rock: Light-house	64 20 05	23 27 00				
	Norrsher Islet: Kvarken light	63 14 08	20 37 40				
	Kaske: Shelgrund I. light	62 20 06	21 11 24				
	Bierneborg: Sebsher light	61 28 29	21 22 34				
	Nuistad: Ensher light	60 43 10	21 01 00				
	Abo: Observatory	60 26 57	22 17 03				
	Aland Island: Shelsher light	60 24 45	19 34 00				
	Ekkere light	60 13 20	19 31 20				
	Logsher light	59 50 50	19 54 05				
	Bogsher: Beacon	59 31 11	20 25 50				
	Ute Islet: Light-house	59 46 30	21 22 00				
	Gange: Gange I. light	59 46 00	22 58 08				
	Rensher: Light-house	59 56 10	24 24 43				
	Helsingfors: Observatory	60 09 43	24 57 17				
	Soder Skars: Light-house	60 06 40	25 25 51				
	Kalboden Island: Light vessel	59 58 45	25 37 30				
	Rodsher Island: Light-house	59 58 08	26 41 05				
	Hogland Island: Lower light	60 00 40	27 01 40				
	Upper light	60 06 22	26 58 44				
	Sommer Island: Light-house	60 12 31	27 33 46				
	Vieborg Bay: Nelva I. light	60 14 43	27 58 36				
	Stirsudden: Light-house	60 11 05	29 03 01				
	Kronstadt: Light on Frederikstadt bastion	59 58 14	29 47 12				
	Cathedral	59 59 44	29 46 07				
	St. Petersburg: Observatory	59 56 30	30 19 22				
	Pulkowa: Observatory	59 46 19	30 19 40				
	Peterhof: Pier-head light	59 53 26	29 54 54				
	Oranienbaum: Light-house	59 55 40	29 46 38				
	Seskar Islet: Light-house	60 02 08	28 23 01				
	Narva: Light S. pt. of entrance	59 28 04	28 03 31				
	Stensher Rock: Light-house	59 49 10	26 23 00				
	Ekholm Islet: Light-house	59 41 06	25 48 58				
	Koksher: Light-house	59 42 00	25 02 37				
	Revel: Light N. end of W. mole	59 27 05	24 46 10				
	Cathedral	59 26 28	24 44 45				
	Nargen Island: Light-house	59 36 22	24 31 57				
	Surop: W. light	59 27 55	24 24 05				
	Baltic Port: Light-house	59 21 30	24 04 30				
	Odenskholm Island: Light-house	59 18 06	23 23 15				
	Takhkona Point: Light-house	59 05 25	22 36 15				
	Dago Island: Dagerort light	58 55 02	22 11 36				
	Filzand Island: Light-house	58 23 02	21 49 56				
	Svalferort Tzerel: Light-house	57 54 37	22 04 15				
	Kuino: Light-house	58 05 50	23 59 34				
	Pernau: Light at S. entrance	58 23 10	24 49 25				
	Riga: Light on Fort Kametskoi dike	57 03 28	24 00 59				
	Cathedral	56 56 36	24 08 25				
	Runo Island: Light-house	57 48 02	23 15 00				
	Domesnes: Light-house	57 48 10	22 39 15				
	Windau: Light on S. jetty	57 24 00	21 34 00				
	Libau: Light at entrance of port	56 31 01	20 59 40				

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Germany.	Memel: Light-house	55 43 45	21 06 06	......	......	.....	.....
	Heiligen Creutz: Church tower	54 53 47	20 01 25	......	......	.....	.....
	Brusterort: Light-house	54 57 40	19 59 06	......	......	.....	.....
	Pillau: Light-house	54 38 25	19 53 55	......	......	.....	.....
	Fischausen: City-hall tower	54 43 49	20 00 39	......	......	.....	.....
	Konigsberg: Observatory	54 42 51	20 29 44	......	......	.....	.....
	Tolkemit: Church tower	54 19 19	19 31 58	......	......	.....	.....
	Elbing: Church tower	54 09 44	19 23 58	......	......	.....	.....
	Tiegenort: Church tower	54 16 30	19 08 37	......	......	.....	.....
	Danzig: Observatory	54 21 18	18 39 46	......	......	.....	.....
	Neufahrwasser light	54 24 28	18 39 59	......	......	.....	.....
	Weichselmunde: Fortress tower	54 23 51	18 41 03	......	......	.....	.....
	Putziger Heisternest: Church tower	54 12 16	18 40 35	......	......	.....	.....
	Oxhoft: Light-house	54 33 09	18 33 46	......	......	.....	.....
	Hela: Light-house	54 36 06	18 49 04	......	......	.....	.....
	Rixhoft: Light-house	54 49 55	18 20 29	......	......	.....	.....
	Leba: Church tower	54 45 29	17 33 38	......	......	.....	.....
	Stopelmunde: Church	54 35 16	16 51 35	......	......	.....	.....
	Jershoft: Light-house	54 32 29	16 32 50	......	......	.....	.....
	Rugenwalde: St. Mary's Church	54 25 27	16 24 52	......	......	.....	.....
	Coslin: St. Mary's Church	54 11 28	16 11 05	......	......	.....	.....
	Funkenhagen: Light-house	54 14 40	15 52 39	......	......	.....	.....
	Colberg: St. Mary's Church	51 10 40	15 34 44	......	......	.....	.....
	Gross-Horst: Light-house	54 05 47	15 04 06	......	......	.....	.....
	Cammin: Cathedral tower	53 58 29	14 46 36	......	......	.....	.....
	Wollin: Church tower	53 50 41	14 37 12	......	......	.....	.....
	Stettin: N. Castle tower	53 25 41	14 33 52	......	......	.....	.....
	Swinemunde: Light-house	53 55 03	14 17 19	......	......	.....	.....
	Streckelsberg: Survey station near beacon	54 03 08	14 01 17	......	......	.....	.....
	Usedom: Church tower	53 52 17	13 55 26	......	......	.....	.....
	Lassau: Church tower	53 56 59	13 51 13	......	......	.....	.....
	Wolgast: Church tower	54 03 18	13 46 51	......	......	.....	.....
	Griefswald: St. Nicholas Church	54 05 49	13 22 53	......	......	.....	.....
	Griefswalder Oie: Light-house	54 15 02	13 55 42	......	......	.....	.....
	Granitz: Castle tower	54 22 56	13 37 54	......	......	.....	.....
	Bergen: Church tower	54 25 08	13 26 11	......	......	.....	.....
	Arkona: Light-house	54 40 53	13 26 12	......	......	.....	.....
	Stralsund: St. Mary's Church	54 18 42	13 05 30	......	......	.....	.....
	Darsserort: Light-house	54 28 28	12 30 23	......	......	.....	.....
	Wustrow: Church	54 20 47	12 24 02	......	......	.....	.....
	Ribnitz: Church tower	54 14 42	12 26 04	......	......	.....	.....
	Warnemunde: Church	54 10 42	12 05 19	......	......	.....	.....
	Rostock: St. Jacob's Church	54 05 27	12 08 10	......	......	.....	.....
	Diedrichshagen: Survey station	54 06 32	11 46 04	......	......	.....	.....
	Basdorf: Survey station	54 08 00	11 41 54	......	......	.....	.....
	Wismar: St. Nicholas Church	53 53 50	11 28 09	......	......	.....	.....
	Hohenschonberg: Survey station	53 58 54	11 05 54	......	......	.....	.....
	Travemunde: Light-house	53 57 44	10 52 59	......	......	.....	.....
	Burg: Church tower	54 26 16	11 11 59	......	......	.....	.....
	Marienleuchte: Light-house	54 29 43	11 14 29	......	......	.....	.....
	Petersdorf: Church tower	54 28 54	11 04 18	......	......	.....	.....
	Hessenstein: Flagstaff of lookout tower	54 19 47	10 32 59	......	......	.....	.....
	Schonberg: Church	54 23 52	10 22 24	......	......	.....	.....
	Bulk: Light-house	54 27 25	10 12 04	......	......	.....	.....
	Kiel: Observatory	54 20 30	10 08 56	......	......	.....	.....
	Eckemforde: Church	54 28 25	9 50 23	......	......	.....	.....
	Schleswig: Cathedral	54 30 55	9 34 23	......	......	.....	.....
	Kappeln: Church	54 39 48	9 56 13	......	......	.....	.....
	Flensberg: Church	54 47 05	9 26 20	......	......	.....	.....
	Duppel: Survey station	54 54 28	9 45 35	......	......	.....	.....
	Schleimunde: Light-house	54 40 23	10 02 23	......	......	.....	.....
	Augustenburg: Church	54 56 48	9 52 20	......	......	.....	.....
	Hugeberg: Survey station	54 58 05	9 58 41	......	......	.....	.....
	Apenrade: Church	55 02 46	9 25 18	......	......	.....	.....
	Skoorgaarde: Survey station	55 03 52	9 23 35	......	......	.....	.....
	Ballum: Church	55 05 31	8 39 41	......	......	.....	.....
	List: E. light-house	55 03 04	8 26 50	0 20	6 33	5.2	3.0

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range Spg.	Range Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Germany.	Keitum: Church	54 54 13	8 22 03				
	Fohr: St. Nicholas Church	54 41 51	8 33 13	1 35	7 47	7.8	4.5
	Galgenberg: Survey station	54 41 21	8 33 58				
	Husum: Church	54 28 43	9 03 21	2 10	8 23	10.8	6.2
	Tonning: Church	54 19 08	8 56 38	1 45	7 57	11.0	6.4
	Busum: Church	54 07 52	8 51 53	1 11	7 24	11.7	6.8
	Helgoland: Light-house	54 10 57	7 53 11	11 29	5 17	8.1	4.7
	Scharhorn: Beacon	53 57 15	8 24 35				
	Neuwerk: Light-house	53 55 01	8 29 58				
	Cuxhaven: Light-house	53 52 25	8 42 43	0 39	6 51	10.1	5.8
	Stade: Church steeple	53 36 12	9 28 48				
	Steinkirchen: Church	53 33 43	9 36 40	4 00	10 13	8.5	4.9
	Altona: Observatory	53 32 45	9 56 35				
	Hamburg: Observatory	53 33 07	9 58 25	5 00	11 12	6.1	3.5
	Berlin: Observatory	52 30 17	13 23 44				
	Harburg: Light-house	53 28 30	9 59 37				
	Hohe Weg: Light-house	53 42 50	8 14 48	0 25	6 38	10.1	5.7
	Langwarden: Church	53 36 20	8 18 30				
	Bremerhaven: New harbor light	53 32 52	8 34 25	0 54	7 07	10.4	5.8
	Minsener Sand: Light vessel	53 46 57	8 04 47	0 10	6 23	9.5	5.3
	Schillighorn: Light-house	53 42 21	8 01 43				
	Wilhelmshaven: Observatory	53 31 52	8 08 48	0 04	6 17	13.2	7.4
	Wangeroog: Light-house	53 47 25	7 54 09	11 27	5 15	8.0	4.5
	Spikeroog: Church	53 46 19	7 41 45				
	Langeoog: Belvedere	53 45 06	7 35 41				
	Balstrum: Church	53 43 46	7 22 03				
	Norderney: Light-house	53 42 39	7 13 58	11 05	4 53	7.3	4.1
	Juist: Church	53 40 45	6 59 53				
	Emden: City Hall tower	53 22 06	7 12 25	0 24	6 36	8.9	5.0
Denmark.	Falster: Gjedser light	54 33 50	11 58 03				
	Moen Island: Stege Church spire	54 59 03	12 17 16				
	Moen light, SE. pt	54 56 46	12 32 40				
	Prœste: Church spire	55 07 24	12 03 07				
	Kjorge: Church tower	55 29 44	12 07 36				
	Amager Island: Hollœnderby Ch. spire	55 35 45	12 38 24				
	Nordse Rase light	55 38 10	12 41 26				
	Copenhagen: New observatory	55 41 14	12 34 47	9 33	3 21	0.6	0.3
	Bornholm: Ronne light	55 05 40	14 42 00				
	Christianso Island: Great tower	55 19 19	15 11 39				
	Kronberg: High spire	56 02 20	12 32 02				
	Nakkehooed: Upper light	56 07 10	12 20 50				
	Hesselo Island: Light-house	56 11 50	11 42 50				
	Anholt Island: Light-house	56 44 16	11 39 15				
	Spodsbjerg: Light-house	55 58 36	11 51 36				
	Roeskilde: Cathedral	55 38 34	12 05 02				
	Nykjobing: Church tower	55 55 30	11 40 29				
	Oddensby: Church tower	55 57 52	11 24 06				
	Sejro Island: Sejro Point light	55 55 09	11 05 07				
	Kallundborg: Church	55 40 50	11 05 04				
	Omo Island: Church	55 09 48	11 09 32				
	Vordingborg: Waldemar's tower	55 00 26	11 54 59				
	Veiro Island: Light-house	55 02 19	11 22 23				
	Langeland Island: Fakkebjerg light	54 44 23	10 42 13				
	Æro Island: Church spire	54 51 14	10 24 11				
	Lyo Island: Church tower	55 02 34	10 09 16				
	Assens: Church tower	55 16 09	9 53 50				
	Baago Island: Light-house	55 17 44	9 48 09				
	Kolding: Castle tower	55 29 31	9 28 40				
	Bogense: Church spire	55 34 03	10 05 29				
	Nyborg: Church spire	55 18 41	10 47 47				
	Turo Island: Church spire	55 03 00	10 40 02				
	Svendborg: Frue Church	55 03 37	10 36 48				
	Endelave Island: Church tower	55 45 32	10 16 20				
	Samso Island: Koldby Church tower	55 48 02	10 33 37				
	Horsens: Frelser Church spire	55 51 44	9 51 19				

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Denmark.	Tuno Island: Light-house	55 56 58	10 26 51				
	Samsoe Island: Nordby Church tower	55 57 06	10 33 00				
	Aarhus: Cathedral spire	56 09 26	10 12 50				
	Hjelm Islet: Light-house	56 08 00	10 48 32				
	Fornæs: Light-house	56 26 36	10 57 40				
	Hals: Church tower	56 59 54	10 18 53				
	Aalborg: St. Rudolph's Church	57 02 54	9 55 22				
	Cape Skaw, or Skagen: Old light-house	57 43 46	10 36 38	5 46	11 58	1.0	0.5
	Hirtshals: Light-house	57 35 06	9 56 44	4 18	10 30	1.2	0.7
	Haustholm: Light-house	57 06 50	8 36 10				
	Boobjerg: Light-house	56 30 48	8 07 23				
	Ringkjobing: Church spire	56 05 27	8 14 52				
	Loune: Church tower	55 47 17	8 14 36	2 35	8 47	2.1	1.2
	Blaabjerg: Summit, 100 ft	55 44 50	8 14 43				
	Guldager: Church	55 31 52	8 24 12	2 35	8 47	4.5	2.6
	Fano Island: Nordby Church	55 26 26	8 24 03	2 34	8 46	4.7	2.7
	Mano Island: Church spire	55 16 11	8 32 38				
Holland.	Niewe Diep: Time-ball station	52 57 50	4 46 36	7 17	1 05	3.9	2.0
	Amsterdam: W. church tower	52 22 30	4 53 01				
	Utrecht: Observatory	52 05 10	5 07 50				
	Leyden: Observatory	52 09 20	4 29 03				
	The Hague: Church tower	52 04 40	4 18 30				
	Scheveningen: Light-house	52 06 16	4 15 10				
	Brielle: Light-house	51 54 29	4 10 45	2 50	9 02	4.8	2.5
	Rotterdam: Time-ball station	51 54 30	4 28 50	3 35	9 47	6.7	3.5
	Hellevoetsluis: Time-ball station	51 49 19	4 07 40	2 20	8 32	5.2	2.8
	Willemstadt: Light-house	51 41 48	4 26 26	3 20	9 32	9.8	5.2
	Goedereede: Light on church tower	51 49 08	3 58 35				
	Flushing: Time-ball station	51 26 33	3 35 48				
	Light, Westhaven bastion	51 26 24	3 34 32	0 44	6 56	14.7	7.8
Belgium.	Brussels: Observatory	50 51 11	4 22 18				
	Antwerp: Observatory	51 12 28	4 24 44	4 15	10 27	14.8	7.8
	Notre Dame Cathedral	51 13 17	4 24 12				
	Blankenberghe: Fort light-house	51 18 47	3 06 54	0 05	6 17	12.5	6.7
	Ostend: Light-house	51 14 13	2 55 51	0 02	6 32	16.1	8.4
	Church tower	51 13 50	2 55 22				
	Nieuport: Templars tower	51 07 53	2 45 34	0 10	6 22	15.7	8.4
France.	Paris: Observatory	48 50 11	2 20 14				
	Dunkerque: Tower	51 02 09	2 22 31	11 58	5 58	16.8	8.5
	Gravelines: Light on N. breakwater	51 00 18	2 06 34	11 59	6 16	19.0	9.6
	Calais: Light on old fort	50 57 45	1 51 07	11 39	6 13	21.0	10.7
	Cape Gris Nez: Light-house	50 52 10	1 35 02	11 17	5 51	21.5	11.0
	Boulogne, C. Alprech: Light-house	50 41 57	1 33 47	11 18	5 52	25.2	12.8
	Abbeville: Tower	50 07 05	1 49 56				
	Cayeux: Light-house	50 11 42	1 30 46				
	Dieppe: W. jetty light	49 56 06	1 05 01	10 54	5 48	27.3	13.3
	Ailly Point: Light-house	49 55 04	0 57 35				
	St. Valery en Caux: Light on W. breakwater	49 52 28	0 42 34	10 29	5 33	26.8	13.1
	Fécamp: N. jetty light	49 46 05	0 22 12	10 06	5 02	23.3	11.4
	Cape La Heve: S. light	49 30 04	0 04 08				
	Havre: S. jetty light	49 29 01	0 06 22	9 03	4 14	22.5	11.0
	Honfleur: Hospital jetty light	49 25 32	0 13 43				
			Long. W.				
	Caen: Church tower	49 11 14	0 21 10				
	Port Corseulles: W. jetty light	49 20 18	0 27 24				
	Point De Ver: Light-house	49 20 28	0 31 08				
	Cape La Hougue: Light-house	49 34 19	1 16 21	8 13	2 45	18.5	8.2
	Cape Barfleur: Light-house	49 41 50	1 15 56	8 14	2 37	17.0	7.5
	Cherbourg: Light, W. head of breakwater	49 40 29	1 43 44				
	Naval Observatory	49 38 54	1 38 08	7 30	1 44	17.6	7.8
	Cape La Hague: Light-house	49 43 22	1 57 15				
	Casquets Rocks: Light on NW. rock	49 43 17	2 22 41	6 20	0 15	15.5	6.9

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
France.	Port St. Peter, Guernsey: Light on Castle Coonet Breakwater	49 27 13	2 31 31	6 12	0 07	26.0	11.5
	Douvres Rocks: Light-house	49 06 28	2 48 49				
	Cape Carteret: Light-house	49 22 27	1 48 25	6 07	0 15	30.8	13.5
	Coutances: Cathedral tower	49 02 54	1 26 39				
	Granville: Light-house	48 50 07	1 36 46	5 50	0 09	36.7	16.0
	Chausey Is.: Light on SE. end of large id.	48 52 13	1 49 20	5 55	0 04	34.7	15.2
	St. Malo: Rochebourne light	48 40 18	1 58 41	5 43	0 04	36.0	15.7
	Cape Frehel: Light-house	48 41 05	2 19 08				
	Heau de Brehat: Light-house	48 54 33	3 05 11	5 35	12 00	30.4	13.3
	Morlaix, Ile Noire: Light-house	48 40 23	3 52 33	5 00	11 25	23.1	10.6
	De Bas Islet: Light-house	48 44 45	4 01 38	4 35	11 00	22.0	10.1
	Abervrach: Light on Vrach Islet	48 36 57	4 34 34	4 00	10 25	20.6	9.5
	Ushant: Stiff Point light	48 28 31	5 03 26	3 35	10 00	18.9	8.7
	Brest: Observatory	48 23 32	4 29 36	3 23	9 45	19.5	9.0
	Brest (approach): Quelern light	48 19 10	4 34 28				
	De Sein Islet: Light-house	48 02 40	4 52 03	3 25	9 53	17.2	7.9
	Bec du Raz: Light-house	48 02 28	4 45 25				
	Audierne: Pier-head light	48 00 47	4 32 50	3 04	9 31	11.1	5.1
	Penmarch Rocks: Light-house	47 47 52	4 22 30	3 05	9 34	13.3	6.1
	Glenan Islands: Light, Penfret I	47 43 17	3 57 15	3 00	9 27	13.0	6.0
	De Groix Island: Light-house	47 38 51	3 30 35				
	Lorient: Church-tower light	47 44 53	3 21 31	3 09	9 36	13.8	6.3
	Belle Isle: Light-house	47 18 42	3 13 38	3 25	9 50	16.6	7.7
	Port Haliguen: Light on N. jetty	47 29 10	3 06 09	3 35	9 58	16.9	7.9
	Haedic Island: Light-house	47 19 18	2 50 07	3 20	9 46	16.7	7.7
	Port Navalo: Light-house	47 32 53	2 55 08	3 45	10 08	16.6	7.7
	Vannes: St. Pierre Church	47 39 30	2 45 28	5 47	12 11	15.8	7.4
	Le Four Rock: Light-house	47 17 53	2 38 05				
	Croisic: End of breakwater	47 18 30	2 31 25	3 25	9 47	16.7	7.7
	Guerande: Steeple	47 19 44	2 25 48				
	Port St. Nazaire: Light-house	47 16 18	2 11 50	3 35	9 56	16.6	7.7
	Paimbœuf: Steeple	47 17 17	2 02 09	4 18	10 39	17.0	7.9
	Nantes: Cathedral	47 13 08	1 32 59	5 50	12 28	16.5	7.7
	Noir Moutier Island: Light-house	47 00 41	2 13 16	3 05	9 26	16.7	7.7
	Le Pilier Island: Light-house	47 02 35	2 21 37				
	D'Yeu Island: Light-house	46 43 04	2 22 56	3 18	9 40	14.7	6.8
	La Chaume: Light-house	46 29 38	1 47 45	3 20	9 44	12.7	5.9
	Point de Grouin du Cou: Light-house	46 20 41	1 27 49				
	Ré Island: Light, NW. pt	46 14 40	1 33 40				
	Rochelle: E. Quay light	46 09 25	1 08 57	3 27	9 22	16.6	7.7
	Aix Island: Light-house	46 00 36	1 10 40	3 27	9 22	16.6	7.7
	Rochefort: Hospital	45 56 37	0 57 50	3 45	9 55	16.7	7.7
	Oleron Island: Light NW. pt	46 02 49	1 24 37				
	Point de la Coubre: Light-house	45 41 39	1 15 16				
	Point Cordouan: Light-house	45 35 14	1 10 24	3 35	9 53	16.8	7.8
	Point de Grave: Light-house	45 34 10	1 04 27				
	Bordeaux: St. André	44 50 19	0 34 42	6 30	0 12	15.3	7.1
	Bayonne: Cathedral	43 29 29	1 28 43				
	Biarritz: Light-house	43 29 38	1 33 16				
	St. Jean de Luz: St. Barbe Point light	43 23 58	1 39 53	3 07	9 14	12.3	5.8
Spain and Portugal.	Fuenterrabia: Light on Cape Higuera	43 23 30	1 47 30				
	Port Pasages: Light at entrance	43 20 05	1 56 05				
	San Sebastian: Monte Igueldo light	43 19 22	2 01 40	2 55	9 05	11.7	5.5
	Bilbao: Light on Galea Castle	43 22 36	3 04 06	2 50	9 03	12.7	5.9
	Castro Urdiales: Santa Ana Castle light	43 24 20	3 16 10	2 50	9 03	11.8	5.5
	Santoña: Pescador Point light	43 28 36	3 28 06	2 55	9 07	12.3	5.7
	Santander: Cape Mayor light	43 29 30	3 47 40	3 05	9 18	14.8	6.9
	San Martin de la Arena: Light-house	43 26 50	4 01 00	3 00	9 14	11.7	5.5
	San Vincent de la Barquera: End of new mole	43 23 35	4 24 55	3 00	9 14	10.4	4.9
	Rivadesella: Mount Somos light	43 31 00	5 07 10				
	Gijon: Santa Catalina light	43 32 48	5 40 11	2 50	9 03	13.5	6.3
	Aviles: Light-house	43 38 05	5 56 00	2 45	8 58	12.0	4.9
	Rivadeo: Light-house	43 34 40	7 03 00	2 45	8 58	14.4	3.9
	Estaca Point: Light-house	43 47 20	7 42 00				

MARITIME POSITIONS AND TIDAL DATA.

ATLANTIC COAST OF EUROPE—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Spain and Portugal.	Port Cedeira: Light-house	43 39 00	8 05 30	2 43	8 56	14.8	6.1
	Ferrol: Old naval observatory	43 29 30	8 13 29	2 44	8 57	14.9	6.1
	Priorino Chico light	43 27 30	8 20 20				
	Coruña: Hercules Tower light	43 23 10	8 24 26	2 43	8 56	14.8	6.1
	Cape Finisterre: Light-house	42 52 45	9 15 28	2 42	8 55	10.0	4.6
	Vigo: Cres I. light	42 12 30	8 54 00				
	Oporto: Light, N. S. de Luz	41 09 10	8 40 35	2 25	8 38	10.0	4.3
	Cape Mondego: Light-house	40 10 47	8 54 15	2 20	8 35	7.0	3.0
	Berlanga Island: Light-house	39 24 49	9 30 29				
	Peniche: Light-house	39 21 00	9 22 30	2 05	8 15	7.8	3.4
	Cape Roca: Light-house	38 46 49	9 29 46				
	Lisbon: Royal Observatory	38 42 31	9 11 10	2 20	8 05	11.1	4.8
	Setubal: Light-house	38 29 15	8 56 00	2 10	8 20	11.6	5.0
	Cape St. Vincent: Light-house	37 01 20	8 58 00				
	Lagos: Church	37 07 48	8 39 53	1 55	8 08	13.0	5.6
	Cape Sta. Maria: Light-house	36 58 23	7 51 48				
	Ayamonte: Light-house	37 11 00	7 24 00				
	Huelva: Plaza at head of mole	37 15 08	6 57 12				
	San Lucar: Chipiona light	36 43 58	6 26 30	1 15	7 28	12.3	5.6
	Cadiz: Observatory of San Fernando	36 27 40	6 12 20				
	San Sebastian light	36 31 30	6 19 00	1 45	7 58	11.8	5.4
	Cape Trafalgar: Light-house	36 10 50	6 02 08				
	Tarifa: Light-house	35 59 53	5 36 31	1 32	7 52	5.6	2.6
	Algeciras: Verde I. light	36 07 19	5 26 12				
	Gibraltar: Dockyard flagstaff	36 07 10	5 21 17				
	Europa Pt. light	36 06 25	5 20 42	1 35	7 55	3.7	1.7

COASTS OF THE MEDITERRANEAN, ADRIATIC, AND BLACK SEAS.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
Spain.	Malaga: Light-house	36 42 39	4 24 38	2 15	8 35	2.9	1.5
	Almeria: Light-house	36 50 12	2 27 50				
	Cape de Gata: Light-house	36 42 57	2 11 12				
	Mazarron: Light-house	37 33 28	1 15 12				
	Cartagena: Arsenal gate	37 35 50	0 59 09				
	Escombrera light	37 33 22	0 57 58				
	Porman: Light-house	37 34 38	0 50 20				
	Santa Pola Bay: Light-house	38 12 30	0 30 12				
	Alicante: N. mole light	38 20 12	0 28 48				
	Villajoyose: Light-house	38 30 00	0 11 42				
	Benidonne: Tower	38 30 57	0 10 06				
	Altea: Light-house	38 33 30	0 04 02				
			Long. E.				
	Calpe: Church tower	38 38 36	0 02 52				
	Morayva: Tower	38 40 51	0 09 17				
	Jarea: Cape San Antonio light	38 48 06	0 12 02				
	Denia: Mole-head light	38 51 00	0 07 30				
			Long. W.				
	Cape Cullera: Light-house	39 12 15	0 13 37				
	Valencia: Light-house	39 28 05	0 19 48				
	Mole-end light	39 27 50	0 18 50	5 00	11 30	1.5	0.8
			Long. E.				
	Columbretes Islands: Light-house	39 53 57	0 41 19				
	Oropesa Cape: Light-house	40 04 53	0 08 56				
	Vinaroz: Mole-head light	40 27 48	0 28 48				
	Port Alfaques: Baña light	40 33 30	0 39 45				
	Cape Tortosa: Light-house	40 43 10	0 53 55				
	Tarragona: E. mole light	41 06 00	1 14 42				
	Barcelona: E. mole-head light	41 22 10	2 10 52				
	Palamos Bay: Molino Pt. light	41 50 04	3 08 28				
	Cadaques: Clock tower	42 16 15	3 17 10				
	Cape Creux: Light-house	42 19 10	3 18 55				
Fr.	Cape Bear: Light-house	42 30 59	3 07 30				
	Port Vendres: Fort Fanal light	42 31 18	3 06 50				

6583—06——15

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

COASTS OF THE MEDITERRANEAN, ADRIATIC, AND BLACK SEAS—Continued.

Coast.	Place.	Lat. N.	Long E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
France.	Port Nouvelle: S. jetty light	43 00 47	3 04 08				
	Cette: Light, St. Louis mole	43 23 50	3 42 08				
	Aigues Mortes: Espignette Pt. light	43 29 17	4 08 32				
	Planier Rock: Light-house	43 11 57	5 13 51				
	Marseille: Janet Cliff light	43 20 43	5 20 46	7 31	2 00	0.6	0.3
	New observatory	43 18 22	5 23 43				
	Ciotat: Berouard mole light	43 10 21	5 36 42				
	Toulon: St. Mandrien light	43 05 10	5 56 06	8 22	2 24	0.6	0.2
	Grand Riband Island: Light-house	43 01 01	6 08 39				
	Cannes: Light-house	43 32 51	7 00 54				
	Antibes: Garoupe light	43 33 51	7 08 02				
	Nice: Light-house	43 41 32	7 17 13				
	Ville Franche: Mole-head light	43 41 58	7 18 42				
	Cape Ferret light	43 40 30	7 19 41				
Bal. I.	Port Ibiza: Light-house	38 54 10	1 27 25				
	Cabrera Island: Light-house	39 06 34	2 57 20				
	Pi (Majorca): Light-house	39 33 00	2 37 00				
	Port Mahon (Minorca): Light-house	39 51 53	4 18 20				
Sardinia.	Cape Spartivento: Light-house	38 52 34	8 51 08				
	Cape Sandalo: Light on San Pietro I	39 08 44	8 13 29				
	Porte Conte: Cape Caccia light	40 33 50	8 10 00				
	Port Torres: Light-house	40 50 25	8 23 56				
	Cape Testa: Light-house	41 14 36	9 08 35				
	Razzoli Island: Light-house	41 18 24	9 20 21				
	Caprera Island: Galera Pt	41 14 15	9 29 40				
	Cape Figari: Signal station	40 59 52	9 39 07				
	Cape Tavolara: Light-house	40 54 55	9 44 22				
	Cape Bellavista: Light-house	39 55 45	9 43 25				
	Cape Carbonera: Cavoli I. light	39 05 15	9 32 35				
	Cagliari: Light on mole	39 12 35	9 07 20				
Corsica.	Bonifacio: Mount Pertusato light	41 22 10	9 11 15				
	Ajaccio: Light-house	41 52 50	8 35 45				
	Corti: Church tower	42 18 14	9 09 04				
	Calvi: Light-house	42 35 10	8 43 25				
	Cape Corso: Giraglia I. light	43 01 45	9 24 10				
	Bastia: Light-house	42 41 47	9 27 00				
	Porto Vecchio: Chiape Pt. light	41 35 45	9 22 05				
Italy.	Cape Melle: Light-house	43 57 17	8 10 22				
	Genoa: San Benigno light	44 24 15	8 54 19				
	Spezzia: Fort Santa Maria light	44 04 00	9 50 48				
	Florence: Observatory	43 46 04	11 15 22				
	Leghorn (Livorno): Light on S. end of curved breakwater	43 32 33	10 17 25				
	Capraia Island: Cape Ferrajone light	43 02 57	9 51 07				
	Elba Island, Porto Longone: Fort Forcado light	42 45 14	10 24 38				
	Pianosa Island: Light on battery, W. side of fort	42 35 06	10 05 50				
	Africa Rock: Light-house	42 21 28	10 03 54				
	Monte Christo Islet: Summit	42 20 15	10 18 39				
	Giglio Island, Cape Rosso: Light-house	42 19 13	10 55 24				
	Civita Vecchia: Light N. end of breakwater	42 05 38	11 46 50				
	Rome: Observatory	41 53 54	12 28 40				
	Gaeta: Orlando tower	41 12 27	13 35 15				
	Ponza Islet: Punto della Guardia light	40 52 38	12 57 17				
	Naples: Observatory	40 51 46	14 14 44				
	Light on elbow of mole	40 50 15	14 15 38	4 00	10 13	0.7	0.2
	Capri Island: Carena Pt. light	40 32 07	14 11 40				
	Lipari Island: Casa Bianca light	38 28 43	14 51 40				
	Ustica Island: NE. point light	38 42 40	13 12 00				
	Faro of Messina: Capo di Faro light	38 16 02	15 39 11				
	Milazzo: Light-house	38 16 10	15 13 42				
	Palermo: Observatory	38 06 44	13 21 16				
	Light on mole head	38 07 56	13 22 04				
	Trapani: Palumbo Rock light	38 00 39	12 29 50				

MARITIME POSITIONS AND TIDAL DATA.

COASTS OF THE MEDITERRANEAN, ADRIATIC, AND BLACK SEAS—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Italy.	Maritimo Island: Light on SW. pt	37 57 13	12 02 55				
	Marsala: W. mole light	37 47 10	12 25 59				
	Girgenti: Port Empedocle light	37 16 55	13 32 27				
	Gozo Island: Light on NW. pt	36 04 10	14 12 55				
	Malta Island, Valetta Harbor: Light-house	35 54 00	14 31 30	3 12	9 25	0.7	0.2
	Linosa Island: Landing Cove	35 51 50	12 52 09				
	Lampedusa Island: Carallo Bianco light	35 29 37	12 36 12				
	Cape Passaro: Light-house	36 41 03	15 07 45				
	Syracuse: Maniace Castle light	37 03 04	15 17 37				
	Augusta Port: Torre d'Avola light	37 12 39	15 13 20	3 00	9 13	0.9	0.3
	Catania: Sciari Biscari light	37 29 35	15 05 19				
	Cape Taormina: Semaphore	37 50 25	15 18 30				
	Messina: San Ranieri light	38 11 33	15 34 36				
	Cape Peloro: Light-house	38 16 02	15 39 11				
	Cape Spartivento: Light-house	37 55 29	16 03 31				
	Cape Colonna: Light-house	39 01 29	17 12 09				
	Cotrone: Mole-head light	39 04 38	17 08 07				
	Taranto: Cape St. Vito light	40 24 41	17 12 23				
	Gallipoli: St. Andrea light	40 02 48	17 56 55				
	Cape Sta. Maria di Leuca: Light-house	39 47 43	18 22 17				
	Cape Otranto: Light-house	40 06 23	18 31 25				
	Port Otranto: Castle	40 09 06	18 28 45				
	Brindisi: Light-house	40 39 36	17 59 37	3 30	9 43	1.8	0.5
	Bari: St. Catalolo light	41 08 19	16 50 52				
	Viesti: Light on St. Croce Rock	41 53 17	16 11 13				
	Manfredonia: Light-house	41 37 39	15 55 34				
	Tremiti Islands: Caprara I. light	42 08 14	15 31 36				
	Ancona: Monte Cappucini light	43 37 14	13 31 18				
	Malamocco: Rocchetta Mole light	45 20 30	12 19 09	10 15	4 45	3.3	0.9
	Venice: Site of tower of St. Mark	45 25 58	12 20 29				
Austria.	Grado: Church tower	45 41 06	13 22 54				
	Monfalcone: Church tower	45 48 33	13 32 10				
	Trieste: Observatory Nautical Academy	45 38 51	13 46 00				
	Theresa Mole light	45 38 54	13 45 14	9 20	3 50	2.0	0.6
	Capo d'Istria: Light-house	45 33 00	13 43 18				
	Isola: Light-house	45 32 34	13 39 32				
	Pirano: Light-house	45 31 54	13 33 48				
	Salvore Point: Light-house	45 29 24	13 29 30				
	Citta Nuova: Light-house	45 19 16	13 33 42				
	Parenzo: Cathedral tower	45 13 45	13 35 39				
	Rovigno: St. Eufemia light	45 05 00	13 38 00				
	Pola: N. cupola of observatory	44 51 49	13 50 46	9 00	3 25	3.4	0.9
	Promontore Point: Porer Rock light	44 45 30	13 53 36				
	Nera Point: Light-house	44 57 24	14 08 42				
	Fiume: Cathedral tower	45 19 36	14 26 41	8 15	2 35	1.2	0.3
	Porto Ré: Light-house	45 16 18	14 33 42				
	Veglia: Mole head	45 01 30	14 34 36				
	Prestenizza Point: Light-house	45 07 12	14 16 30				
	Cherso: Kimen Point light	44 57 36	14 23 30				
	Galiola Rock: Light-house	44 43 36	14 10 36				
	Unie Island: Netak Point light	44 37 20	14 14 06				
	Lussin Piccolo: Sta. Maria Church	44 31 49	14 28 06	8 10	2 25	1.1	0.3
	St. Pietro di Nembo Island: Health office	44 27 42	14 33 28				
	Gruizza Rock: Light-house	44 24 42	14 34 06				
	Zengg: Mole-head light	44 59 24	14 53 48				
	Terstenik Rock: Light-house	44 40 06	14 34 42				
	Carlobago: Light-house	44 31 30	15 04 24				
	Zara: Church tower	44 07 05	15 14 05				
	Bianche Point: Light-house	44 09 06	14 49 24				
	Zara Vecchia: Church tower	43 56 16	15 26 21				
	Port Tajer: Lestrice I. light	43 51 15	15 12 06				
	Lucrietta Island: Light-house	43 37 36	15 34 24				
	Sebenico: Mount Tartaro	43 45 08	15 58 07	6 10	0 20	1.0	0.3
	Rogosnizza Port: Mulo Rock light	43 31 00	15 55 00				
	Zirona Grande Island: St. George Church tower	43 27 00	16 08 51				
	Traní: Cathedral tower	43 31 02	16 15 09				

MARITIME POSITIONS AND TIDAL DATA.

COASTS OF THE MEDITERRANEAN, ADRIATIC, AND BLACK SEAS—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Austria.	Port Spalato: Cathedral tower	43 30 07	16 26 06				
	Solta I., Port Olivetto: St. Nicholas tower	43 23 50	16 11 10				
	Spalato Passage: Speo Pt. light	43 19 12	16 24 30				
	Makarska: Church tower	43 17 46	17 01 36				
	Pomo Rock: Center	43 05 28	15 27 30				
	St. Andrea Rock: Summit	43 01 43	15 45 29				
	Lissa Island: Hoste Rock light	43 04 30	16 12 28	4 00	10 30	2.4	0.7
	Pakonjidol Rock: Light-house	43 09 24	16 27 14				
	Lesina Island: Port Gelsa light	43 09 50	16 41 55				
	St. Giorgio Pt. light	43 07 30	17 12 00				
	Sabioncello Peninsula: Cape Gomena light	43 02 50	17 00 19				
	Sorelle Rocks: Light-house	42 57 42	17 12 44				
	Curzola Island: Porto Bema mole head	42 54 19	16 51 32				
	Porto Valle Grande, church tower	42 57 37	16 43 07				
	Lagostini Island: Glavat Rock light	42 45 54	17 08 54				
	Lagosta Island: St. George Chapel	42 45 05	16 51 45				
	Cazza Island: Light-house	42 45 05	16 29 29				
	Pelagosa Rock: Light-house	42 23 30	16 15 12				
	Meleda Island: Port Palazzo Ruin	42 47 06	17 22 51				
	Olipa Rock: Light-house	42 45 30	17 46 48				
	Pettini di Ragusa Rocks: Light-house	42 39 00	18 03 08				
	Bobara Rock: Summit	42 35 08	18 10 49				
	Molonta Peninsula: Summit	42 27 04	18 25 36				
	Ostro Point: Light-house	42 23 36	18 32 00				
	Cattaro: Health office	42 25 30	18 46 12				
	Budua: Mole-head light	42 16 42	18 50 36				
	Katic Rock: St. Domenica Chapel	42 11 43	18 56 25				
	Antivari: Pt. Valovica light	42 05 15	19 04 19				
	Dulcigno: W. windmill	41 55 47	19 12 29				
Turkey.	Cape Rodoni: Guard-house	41 35 10	19 27 15				
	Cape Pali: Guard-house	41 23 31	19 24 54				
	Durazzo: Light-house	41 18 40	19 27 14				
	Cape Laghi: Ruin	41 08 44	19 26 47				
	Skumbi River: Pyramid at mouth	41 02 12	19 26 30				
	Semeny River: Samana Pt. light	40 47 00	19 20 14				
	Vojazza River: Pyramid at mouth	40 36 14	19 19 14				
	Saseno Island: Light-house	40 30 12	19 16 15				
	Avlona: Light-house	40 25 30	19 27 55				
	Cape Linguelta: Extreme	40 25 17	19 17 45				
	Mount Cica: Pyramid	40 12 00	19 38 33				
	Port Palermo: Pyramid	40 02 57	19 47 53				
	Cape Kiefali: Pyramid	39 54 29	19 54 55				
	Fano Island: Pt. Kastri light	39 51 53	19 26 06				
	Port Pagonia: Ruin	39 39 27	20 07 12				
	Port Gomenitza: Well Dogana	39 29 50	20 17 09				
	Port Parga: Madonna I	39 16 32	20 24 55				
Greece.	Port St. Spiridione: Convent	39 39 54	19 43 09				
	Corfu: Light-house	39 37 05	19 56 30				
	Paxo Island: Madonna I. light	39 11 30	20 12 34				
	Prevesa; Fort Nuovo minaret	38 56 30	20 45 40				
	Port Drepano: Observation island	38 47 25	20 44 16				
	Port Vliko: Custom-house	38 40 40	20 42 44				
	Port Vathi: Lazaretto light	38 22 04	20 43 37				
	Port Argostoli: St. Theodoro light	38 11 36	20 29 30				
	Patras: Light-house	38 15 00	21 43 50	3 40	9 53	1.0	0.3
	Katakolo: Light-house	37 38 20	21 18 55				
	Zante: Mole light	37 47 10	20 55 26				
	Strovathi, or Strivali Island: Stamphani I. light	37 15 12	21 01 14				
	Proti Passage: Marathon Pt	37 03 38	21 34 35				
	Navarin: Light-house	36 54 10	21 40 29				
	Mothoni: Round tower	36 48 40	21 42 40				
	Koroni Anchorage: Mole light	36 47 50	21 58 00				
	Petalidi Bay: Petalidi Pt	36 57 20	21 56 42				
	Candia Island, Port Suda: Light-house	35 28 55	24 09 39				
	Megalo Kastron: Mole light	35 20 30	25 09 44				

MARITIME POSITIONS AND TIDAL DATA.

COASTS OF THE MEDITERRANEAN, ADRIATIC, AND BLACK SEAS—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Greece.	Kandeliusa Island: Light-house	36 29 40	26 59 25	......	......	......	......
	Stampali Island, Maltezana Port: Agios Ioanes	36 34 25	26 24 28	......	......	......	......
	Christiana Islands: N. pt	36 15 20	25 13 00	......	......	......	......
	Milo Island: Summit, Mt. St. Elias	36 40 27	24 23 15	......	......	......	......
	Siphano Island: Light-house	36 59 12	24 40 30	......	......	......	......
	Naxos Island, Naxia: Gate on Bacchus I.	37 06 32	25 23 00	......	......	......	......
	Paros Island, Port Trio: Trio Pt	37 00 01	25 14 21	......	......	......	......
	Port Naussa: St. Yanni Church	37 08 38	25 14 08	......	......	......	......
	Syra: Mole light	37 26 12	24 56 14	......	......	......	......
	Sermo Island: Amyno Pt	37 07 36	24 32 23	......	......	......	......
	Thermia Island: Ruins of Cythnus	37 25 55	24 23 35	......	......	......	......
	Jura Island: North pt	37 38 00	24 44 32	......	......	......	......
	Port St. Nikolo: Light-house	37 39 28	24 19 44	......	......	......	......
	St. Nikalao Island: Port Mandri	37 44 00	24 04 12	......	......	......	......
	Andros Island, Cape Fasse: Light-house	37 57 30	24 42 30	......	......	......	......
	Ieraka: Acropolis	36 47 05	23 05 40	......	......	......	......
	Port Kheli: Light-house	37 18 42	23 08 53	......	......	......	......
	Poros Island: Light-house	37 31 45	23 25 45	......	......	......	......
	Ægina: Light-house	37 44 30	23 25 30	......	......	......	......
	Piræus: Light-house	37 56 14	23 38 10	......	......	......	......
	Athens: Observatory	37 58 20	23 43 55	......	......	......	......
	Cape Colonna: Extreme	37 38 45	24 02 15	......	......	......	......
	Port Raphti: Statue I	37 52 48	24 03 00	......	......	......	......
	Petali Island: Trago I. peak	38 01 28	24 16 42	......	......	......	......
	Euripo Strait: Light-house	38 28 15	23 36 45	......	......	......	......
	Skiathos Island: Mount Stavros	39 10 48	23 27 07	......	......	......	......
	Salonika: S. bastion	40 37 28	22 58 00	......	......	......	......
	Port Baklar: Cape Xeros	40 32 40	26 45 00	......	......	......	......
	Lemnos Island: Kastro Castle	39 52 10	25 03 20	......	......	......	......
	Port Moudros: Sangrada Pt	39 50 52	25 14 14	......	......	......	......
	Strati Island: St. Strati Church	39 31 58	24 59 13	......	......	......	......
	Mityleni Island, Port Sigri: Light-house	39 12 35	25 50 00	......	......	......	......
	Mityleni: Light on Mityleni Pt	39 06 10	26 34 54	......	......	......	......
	Port Iero: Sidero Islet	39 03 20	26 31 39	......	......	......	......
	Psara Island: Fort	38 32 00	25 35 00	......	......	......	......
	Tchesmé: C. Kézil light	38 19 55	26 17 45	......	......	......	......
	Samos Island: Fonia Pt. light	37 41 24	26 58 42	......	......	......	......
	Port Isene: Tower	37 16 33	27 36 55	......	......	......	......
	Kos: Light-house	36 55 00	27 18 25	......	......	......	......
	Marmorice Harbor: Adassi Pt. light	36 48 00	28 18 00	......	......	......	......
	Makry Harbor: Kasil I	36 39 33	29 06 13	......	......	......	......
	Rhodes Port: Arab's Tower light	36 26 00	28 16 24	......	......	......	......
	Port Lindo: Tower	36 05 53	28 08 10	......	......	......	......
Turkey.	Dardanelles: Hellas Pt. light	40 02 30	26 10 54	......	......	......	......
	Gallipoli: Light-house	40 24 27	26 41 24	......	......	......	......
	Bosphorus: Tofana Pt. light	41 01 20	29 01 00	......	......	......	......
	Scutari: Leander Tower light	41 01 02	29 00 29	......	......	......	......
	Constantinople: Seraglio Pt. light	41 00 35	29 01 14	......	......	......	......
	St. Sophia Mosque	41 00 16	28 58 59	......	......	......	......
	Cape Kara Burnu: Light-house	41 21 15	28 42 14	......	......	......	......
Russia.	Yuiada Road: Fort Tersana	41 52 04	27 58 45	......	......	......	......
	Burghaz: Light-house	42 27 52	27 35 54	......	......	......	......
	Varna Bay: Light-house	43 10 00	27 58 35	......	......	......	......
	Kusterjeh: Cape Kusterjeh light	44 10 20	28 39 14	......	......	......	......
	Danube River: Salina light	45 09 47	29 41 14	......	......	......	......
	Fidonisi Island: Light-house	45 16 00	30 14 14	......	......	......	......
	Odessa: Observatory	46 28 36	30 45 34	......	......	......	......
	Dnieper Bay: Fort Nikolaeo light	46 34 27	31 33 36	......	......	......	......
	Sebastopol: E. light-house	44 36 55	33 36 26	......	......	......	......
	Balaklava Bay: Hospital	44 29 50	33 36 25	......	......	......	......
	Kertch: Light-house	45 21 03	36 28 30	......	......	......	......
	Berdiansk: Breakwater light	46 45 00	36 46 40	......	......	......	......
	Saukhoum: Light-house	42 58 00	40 55 10	......	......	......	......
	Batoum: Light-house	41 39 30	41 38 15	......	......	......	......

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

COASTS OF THE MEDITERRANEAN, ADRIATIC, AND BLACK SEAS—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Turkey.	Trebizond: Light-house	41 01 00	39 46 25				
	Sinope: Light-house	42 01 20	35 13 20				
	Bender Erekli: Light-house	41 18 03	31 25 49				
	Marmora Island: Light off E. pt	40 38 10	27 46 09				
	Artaki Bay: Zeitijn Adasi Islet	40 23 30	27 47 30				
	Tenedos Island: Ponente Pt. light	39 50 00	25 58 34				
	Port Ajano: Nikolo Rock	39 01 21	26 47 57				
	Port Ali-Agha: W. pt. of entrance	38 50 10	26 57 20				
	Smyrna: English consulate flag-staff	38 25 40	27 09 10	9 15	3 15	2.5	0.7
	Vourlah: Custom-house	38 21 48	26 47 00				
	Sighajik Harbor: Beacon on islet	38 12 21	26 47 32				
	Budrum: Light-house	37 02 00	27 27 05				
	Adalia: Light-house	36 52 00	30 45 34				
	Alexandretta: Light-house	36 35 30	36 10 20				
	Latakiyah: Light-house	35 30 30	35 46 30				
	Tripoli Roadstead: Bluff Islet light	34 29 25	35 44 24				
	Ruad Island: Light-house	34 52 00	35 51 00				
	Beirut: Light-house	33 54 10	35 28 25	9 45	3 35	1.2	0.3
	Saida (ancient Sidon): Light-house	33 34 20	35 21 30				
	Sûr (ancient Tyre): Light-house	33 16 30	35 14 40				
	Acre: Light-house	32 54 35	35 08 00				
	Haifa: Light-house	32 47 40	35 05 00				
Cyprus.	Famagusta: Light-house	35 07 10	33 57 22	9 40	3 30	1.4	0.4
	C. Gata: Light	34 33 45	33 01 30				
	Lamaka: Light-house	34 54 00	33 38 59				
Egypt.	Port Said: High light-house	31 15 41	32 18 45	9 40	3 30	1.0	0.3
	River Nile: Damietta Mouth	31 31 40	31 51 00				
	Rosetta Mouth light	31 29 30	30 19 10				
	Aboukir Bay: Nelson I. peak	31 21 23	30 06 00				
	Alexandria: Eunostos Pt. light	31 11 43	29 51 40	9 45	3 15	1.1	0.3
	Ben Ghazi: Castle	32 06 51	20 02 40	9 55	3 45	1.2	0.3
	Tripoli Harbor: Light-house	32 54 03	13 10 50	10 00	3 50	1.9	0.5
Tunis.	Sfax: Ras Tina light	34 39 01	10 41 17	3 35	9 57	4.2	1.1
	Mehediah: Sidi Jubber	35 30 24	11 05 15				
	Monastir: Burj el Kelb battery	35 45 24	10 50 42				
	Hammamet Bay: Castle flag-staff	36 23 20	10 37 10				
	Kalibia Road: Light-house	36 50 12	11 07 00				
	Cape Bon: Light-house	37 04 45	11 03 15				
	Tunis: Goletta light	36 48 19	10 18 31	3 33	9 55	3.0	0.8
Algeria.	Cape Farina: Extreme	37 10 42	10 17 30				
	Benzert: N. Jetty light	37 16 38	9 53 21				
	Galita Island: Monte Guardia	37 31 16	8 56 12				
	Bona: Fort Genois light	36 57 15	7 46 40				
	Stora: Singe I. light	36 54 29	6 53 11				
	Cape Bougaroni: Light-house	37 05 17	6 28 37				
	Cape Carbon: Light-house	36 46 41	5 06 22				
	Algier: Light-house near Admiralty	36 47 16	3 04 13	2 46	8 58	2.6	1.3
	Cape Tenez: Light-house	36 33 07	1 20 36				
			Long. W.				
	Oran: Mers el Kebir light	35 44 21	0 41 38				
	Habibas Island: Light-house	35 43 22	1 07 57				
Morocco.	Zafarin Islands: Light Isabel Segunda I.	35 11 05	2 25 45				
	Alboran Island: Light-house	35 58 00	3 03 29				
	Ceuta: Light-house	35 53 44	5 16 46	1 55	8 07	3.3	1.5
	Tangier: Casbah tower	35 47 00	5 48 31	1 30	7 40	8.0	3.7
	Cape Spartel: Light-house	35 47 14	5 55 41				

WEST COAST OF AFRICA.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
	El Araish: S. pt. of entrance	35 12 50	6 09 13				
	Sali: Fort	34 04 10	6 48 00	1 35	7 45	10.4	4.8
	Cape Dar el Beida: Light-house	33 36 00	7 33 00				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF AFRICA—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Cape Blanco, North: Extreme	33 08 00	8 35 05				
	Mogador Harbor: English consulate	31 30 30	9 43 30	1 05	7 17	10.9	5.0
	Cape Ghir: Extreme	30 38 00	9 50 00				
	Cape Noun: Extreme	28 45 00	11 02 00				
	Cape Juby: Extreme	27 56 00	12 56 00	11 55	5 43	8.5	3.9
	Cape Bojador: Extreme	26 07 57	14 29 00	11 50	5 38	7.3	3.4
	Penha Grande	25 07 06	14 50 44				
	Ouro River entrance: Dumford Pt	23 36 03	15 58 00				
	Pedra de Galha	22 12 37	16 48 11				
	Cape Blanco, South: Extreme	20 46 27	17 05 40	11 35	5 23	5.5	2.5
	Portendik: Village	18 18 45	16 02 00				
	St. Louis: Light-house	16 01 31	16 30 22				
	Almadie Point: Light-house	14 44 45	17 32 25				
	Cape Verde: Light-house	14 43 20	17 30 55				
	Port Dakar: Light-house	14 40 30	17 25 28				
	Cape Manoel: Light-house	14 38 55	17 26 47				
	Goree Island: Fort	14 39 55	17 24 30				
	Bird Island: Flagstaff	13 39 45	16 40 30				
	Bathurst: Flagstaff	13 28 00	16 35 00	9 00	2 50	5.9	2.7
	Carabane: Light-house	12 35 00	16 44 00				
	Nunez River: Sand I	10 36 37	14 42 00				
	Ponga River entrance: Observation pt	10 03 15	14 04 30	7 30	1 20	11.4	5.2
	Isles de Los: Light-house	9 30 30	13 44 00				
	Matacong Island: House	9 16 10	13 26 20				
	Scarcies River: W. end of Yellaboi I	8 57 05	13 18 25				
	Sierra Leone: Light on cape	8 30 00	13 18 30	7 40	1 30	11.6	5.3
	N. battery	8 29 57	13 14 30				
	Sherbro Island: N. island	7 40 36	13 04 30				
	Sherbro River: Manna Pt	7 22 45	12 31 55	5 50	12 00	10.4	4.8
	Gallinas River: W. elbow of Kamasoun I.	7 00 08	11 38 45				
	Cape Mount: W. peak	6 44 30	11 22 51				
	Cape Mesurado: Light-house	6 19 10	10 49 25				
	Monrovia: Light-house	6 19 00	10 50 00	5 40	11 54	6.0	2.5
	Marshall: Agent's house	6 08 06	10 22 45				
	Grand Bassa: Agent's house	5 54 08	10 04 05				
	Cestos: Factory	5 26 25	9 34 45				
	Sangwin River: Sangwin Pt	5 12 42	9 20 16				
	Sinon: Bloobarra Pt	4 59 15	9 02 05	4 50	11 05	4.8	2.0
	Cape Palmas: Light-house	4 22 10	7 44 15	4 30	10 43	4.3	1.8
	Tabou River: Tabou Pt	4 24 47	7 21 30				
	Axim Bay: Ft. St. Anthony	4 52 18	2 14 45				
	Cape Three Points: Light-house	4 45 00	2 05 45	4 00	10 13	4.7	1.9
	Dix Cove: Fort	4 47 45	1 56 40				
	Tacorady Bay: Tacorady Pt	4 53 00	1 45 00				
	Chama Bay: Dutch Fort	5 01 00	1 38 00				
	El Mina Bay: Ft. St. George	5 04 48	1 21 05				
	Cape Coast Castle: Light-house	5 06 20	1 13 50	4 20	10 32	6.0	2.5
	Accra: Light-house	5 31 50	0 11 30				
			Long. E.				
	Volta River entrance: Dolbens Pt	5 46 00	0 41 00	4 20	10 33	4.2	1.8
	Lagos River: Light-house	6 25 15	3 25 15	4 50	11 05	3.3	1.3
	Benin River entrance: N. pt	5 46 01	5 03 05				
	Brass River: Entrance (approx.)	4 16 40	6 15 00				
	Calebar River (New): Rough Corner	4 23 07	7 07 00				
	Opobo River: W. pt. beacon (approx.)	4 27 00	7 40 00				
	Quaebo River: Bluff Pt	4 30 40	7 59 00				
	Calebar River (Old): Townsend flagstaff (Dunketown)	4 56 24	8 20 46				
	Fernando Po Island: Light-house	3 46 10	8 47 05				
	San Bento River: Joho Pt. (approx.)	1 35 00	9 39 00				
	Princes Island: Diamond Rocks, center of largest	1 40 42	7 27 56				
	St. Thomas Island: Ft. San Sebastian light	0 20 30	6 42 45				
		Lat. S.					
	Anno Bon Island: Turtle Islet	1 24 18	5 38 12				
	Cape Lopez: Light-house	0 36 25	8 43 10				
	Mayumba Bay: Light-house	3 23 00	10 38 00	4 25	10 38	7.0	2.9

MARITIME POSITIONS AND TIDAL DATA.

WEST COAST OF AFRICA—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Loango Bay: Indian Pt. light	4 40 00	11 46 30	4 13	10 26	6.5	2.7
	Black Point Bay: Sandy Pt	4 49 00	11 45 00				
	Malemba Bay: Landing Cove	5 18 30	12 08 00				
	Kabenda Bay: Kabenda Pt. light	5 32 30	12 11 00				
	Congo River entrance: Shark Pt	6 04 36	12 15 00	4 10	10 25	6.0	2.5
	Margate Head: Summit	6 31 50	12 25 25				
	St. Paul de Loando: Flag staff, Ft. San Miguel	8 48 24	13 13 20	3 40	9 53	4.8	2.0
	Lobito Point: Extreme	12 20 00	13 32 00				
	Benguela: Telegraph office	12 34 43	13 23 45	3 30	9 43	5.5	2.3
	Elephant Bay: Friar Rocks	13 12 30	12 48 55				
	St. Mary Bay: Bay I	13 26 05	12 36 00				
	Little Fish Bay: Light-house	15 09 00	12 12 00				
	Port Alexander: Bateman Pt	15 47 30	11 52 40				
	Great Fish Bay: Tiger Pt	16 30 00	11 42 00	3 00	9 12	5.7	2.4
	Cape Frio: Extreme	18 23 00	11 57 12				
	Walfisch Bay: Light-house	22 57 00	14 30 00				
	Ichabo Island	26 17 00	14 57 20				
	Angra Pequena: Diaz Pt	26 37 52	15 07 02				
	Elizabeth Bay: S. pt. of Possession I	26 58 30	15 12 22	2 35	8 47	5.5	2.3
	Port Nolloth: Magistrate's house	29 15 12	16 52 02	2 25	8 38	5.3	2.2
	Hondeklip Bay	30 18 33	17 16 20				
	Roodewal Bay	30 33 07	17 27 30				
	Saldanha Bay: Constable Hill	33 07 51	18 01 21	2 20	8 33	5.1	2.1
	Table Bay: Robben I. light	33 48 52	18 22 33				
	Cape Town: Observatory	33 56 04	18 28 40	1 36	7 47	4.6	2.0
	Cape of Good Hope: Light-house	34 21 12	18 29 26				

EAST COAST OF AFRICA AND THE RED SEA.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
	Simons Bay: Light-house	34 10 45	18 27 30	2 35	8 48	5.2	2.2
	Cape Hangklip: Extreme	34 23 48	18 50 20				
	Quoin Point: Extreme	34 46 45	19 38 17				
	Cape Agulhas: Light-house	34 49 45	20 00 37	2 40	8 53	5.2	2.2
	Port Beaufort: Flag-staff	34 23 47	20 48 40				
	St. Blaize: Light-house	34 11 10	22 09 31	3 18	9 31	5.6	2.0
	Knysna Harbor: Fountain beacon	34 04 35	23 03 38				
	Plettenberg Bay: Summit of Seal Pt	34 06 15	23 24 23				
	St. Francis: Light-house	34 12 30	24 50 20				
	Cape Recife: Light-house	34 01 41	25 42 12				
	Port Elizabeth: Light-house	33 57 43	25 37 21	3 21	9 33	5.4	1.9
	Bird Islands: Light-house	33 50 27	26 17 13				
	Port Alfred: Signal staff	33 36 09	26 54 10				
	Waterloo Bay: Maitland Signal Hill	33 28 00	27 03 00				
	Madagascar Reef: Center	33 23 10	27 20 48				
	Cove Rock: Center	33 05 10	27 49 12				
	East London: Light-house	33 01 45	27 55 02	3 37	9 50	5.0	1.8
	Cape Morgan: Extreme	32 42 00	28 22 36				
	Hole-in-the-Wall	32 02 30	29 06 40				
	Rame Head: Extreme	31 48 15	29 21 15				
	Cape Hermes: Extreme	31 38 06	29 33 16				
	Waterfall Bluff	31 26 15	29 48 40				
	Port Natal (Durban): Light-house	29 52 40	31 03 50	3 58	10 11	5.6	1.6
	Dumford Point: Extreme	29 00 12	31 51 39				
	Cape St. Lucia: Extreme	28 32 30	32 27 39				
	Cape Vidal: Extreme	28 09 36	32 38 10				
	Delagoa Bay: Reuben Pt. light	25 58 49	32 35 52	5 10	11 22	11.9	3.4
	Cape Corrientes: Small rock	24 05 30	35 29 45				
	Innamban Bay: Barrow Hill light	23 45 30	35 31 41	4 30	10 42	11.0	3.2
	Cape St. Sebastian: Extreme	22 05 00	35 29 00				
	Bazaruto Island: N. pt. light	21 31 00	35 29 30				
	Chuluwan Island: Light-house	20 38 10	34 53 30				
	Sofala: Fort on N. side of entrance	20 10 42	34 46 00				
	Zambesi River: Kangoni Mouth	18 52 50	36 11 47	4 15	10 27	13.5	3.9
	Quillimane River: Light-house	18 01 24	36 58 30				
	Quillimane: Town	17 51 50	37 01 09				
	Mazemba River: Entrance	17 15 00	38 04 00				

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF AFRICA AND THE RED SEA—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Premeira Islands: Center of Casuarina I.	17 06 30	39 06 27	....	....	......	......
	Angoxa Islands: Center of Hurd I......	16 33 24	39 49 57	....	....	......	......
	Mafamale Island: Center.............	16 20 30	40 03 57	....	....	......	......
	Port Mokamba: Mokambo Pt	15 08 00	40 36 12	....	....	......	......
	Port Mozambique: St. George I. light...	15 02 12	40 48 45	....	....	......	......
	San Sebastian light..	15 00 45	40 45 06	4 00	10 12	11.8	3.4
	Cape Cabeceira: Light-house	14 58 20	40 45 10	....	....	......	......
	Port Conducia: Bar Pt..............	14 53 00	40 40 00	....	....	......	......
	Lurio Bay: Pando Pt	13 23 40	40 46 00	....	....	......	......
	Pemba Bay: N. pt. light	12 55 45	40 31 15	....	....	......	......
	Querimba Islands: Ibo I. light	12 19 30	40 40 09	....	....	......	......
	Numba Island: E. pt	11 09 18	40 43 21	....	....	......	......
	Cape Delgado: Light-house............	10 41 20	40 38 35	3 59	10 11	11.3	3.3
	Msimbati: Ras Matunda	10 19 22	40 26 34	....	....	......	......
	Mikindini Harbor: Kinizi..............	10 16 31	40 10 33	....	....	......	......
	Mgan Mwania: Madjori Rock	10 06 43	40 02 14	....	....	......	......
	Lindi River: Fort flagstaff	9 59 30	39 46 41	3 55	10 08	10.9	4.5
	Mchinga Bay: Observation spot	9 44 22	39 47 07	....	....	......	......
	Kiswere Harbor: Rustmigi............	9 25 36	39 39 31	....	....	......	......
	Kilwa Kisiwani: Fort................	8 57 15	39 30 42	....	....	......	......
	Mafia Island: Moresby Pt.............	7 38 10	39 54 42	....	....	......	......
	Dar-Es-Salaam: Flagstaff............	6 49 41	39 17 05	....	....	......	......
	Bagamoyo: French Mission	6 26 10	38 54 27	....	....	......	......
	Zanzibar: English consulate..........	6 09 43	39 11 08	4 05	10 17	14.5	6.0
	Tanga Bay: Light-house	5 00 35	39 10 20	....	....	......	......
	Mombasa: Light-house	4 04 30	39 41 13	....	....	......	......
	Port Melinda: Vasco de Gama's Pillar ..	3 12 48	40 11 21	4 00	10 13	12.1	5.0
	Lamo Bay: Lamo Castle	2 15 42	40 56 21	....	....	......	......
	Manda Roads: E. side of Manda Toto I .	2 13 35	40 59 40	....	....	......	......
	Port Durnford: Foot Pt.............	1 13 00	41 54 15	4 30	10 42	11.7	4.9
	Kisimayu Bay: S. pt. of Kisimayu I....	0 22 35	42 33 57	....	....	......	......
		Lat. N.					
	Brava: Well	1 06 48	44 03 27	4 15	10 27	7.5	3.1
	Meurka Anchorage: S. pt. of town......	1 42 06	44 53 49	....	....	......	......
	Magadoxa: Tower	2 01 48	45 24 39	....	....	......	......
	Murat Hill: Peak..................	2 30 00	46 07 00	....	....	......	......
	Ras Hafun: E. extreme of Africa.......	10 26 30	51 22 55	....	....	......	......
	Cape Guardafui: E. pt...............	11 50 30	51 16 45	6 00	12 12	6.1	2.5
	Kal Farun Islet: Center	12 26 00	52 09 35	....	....	......	......
	Abd-al-Kuri Island: NE. pt...........	12 11 15	52 25 35	....	....	......	......
	Socotra Island: Tamarida, mosque.......	12 39 00	53 59 31	7 05	1 17	7.5	3.1
	Ras Antareh: Extreme of rocky pt	11 27 30	49 35 40	....	....	......	......
	Máit Island: Center	11 13 00	47 17 00	....	....	......	......
	Port Berbera: Light-house	10 25 00	44 59 35	....	....	......	......
	Zeyla: Mosque	11 22 00	43 29 35	7 30	1 18	8.5	3.5
	Perim Island: Light-house	12 39 00	43 25 35	7 50	1 38	7.2	3.0
Red Sea.	Hanfelah Bay: Hanfelah Pt............	14 44 00	40 52 00	....	....	......	......
	Disei Island: Village Bay	15 28 10	39 45 30	....	....	......	......
	Massaua Harbor: N. pt. of entrance	15 37 12	39 27 23	0 45	6 57	4.0	1.7
	Khôr Nowarat: Shatireh Islet..........	18 15 12	38 19 30	....	....	......	......
	Suakin: Light-house................	19 07 00	37 19 09	2 10	8 22	1.7	0.7
	Makaua Island: S. pt	20 44 00	37 15 30	....	....	......	......
	St. Johns Island: Peak	23 36 20	36 10 15	....	....	......	......
	Dædalus Shoal: Light-house	24 56 30	35 51 00	....	....	......	......
	Kosair Anchorage: SW. angle of fort....	26 06 24	34 17 03	....	....	......	......
	Brothers Island: Light-house..........	26 18 50	34 50 45	6 40	0 28	2.0	0.8
	Safajah Island: N. summit	26 45 48	33 59 43	....	....	......	......
	Ashrafi Island: Light-house...........	27 47 21	33 42 28	....	....	......	......
	Ras Gharib: Light-house.............	28 20 52	33 06 31	10 35	4 23	1.5	0.6
	Zafarana: Light-house	29 06 29	32 39 43	10 40	4 28	5.5	2.3
	Suez: Newport Rock................	29 53 05	32 32 50	10 45	4 32	6.8	2.8
	Tôr: Ruined fort	28 13 47	33 36 56	....	....	......	......
	Sherm Yahar: Entrance	27 35 45	35 30 30	....	....	......	......
	Sherm Joobbah: Entrance	27 33 00	35 32 30	....	....	......	......
	Sherm Wej: Light-house.............	26 13 00	36 27 00	....	....	......	......
	Sherm Hassejy: Anchorage	24 38 35	37 17 45	....	....	......	......
	Yembó: Anchorage.................	24 05 15	38 02 45	....	....	......	......

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF AFRICA AND THE RED SEA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Red Sea.	Sherm Rabigh: Anchorage	22 43 50	39 00 30				
	Jiddah: Jezirah el Mifsaka I	21 28 00	39 10 38	3 30	9 42	2.0	0.8
	Lith: Agha Islet	20 09 00	40 12 00				
	Jelalil: Anchorage	19 55 30	40 30 00				
	Kunfidah: Islet	19 07 40	41 03 20				
	Khôr Nohud: Entrance	18 15 50	41 27 30				
	Farisan I. Anchorage: Jebel Mandhakh	16 50 15	41 58 15				
	Gizau: Fort	16 53 00	42 29 00				
	Loheiya: Hill Fort	15 42 00	42 38 45	1 15	7 27	2.9	1.2
	Kamarán Bay: Harbor	15 20 30	42 34 00				
	Hodeïda Road	14 47 00	42 56 00				
	Jebel Zukur Island: N. pt	14 03 53	42 45 28				
	Mokha: N. Fort	13 19 43	43 13 36	11 45	5 33	4.5	1.9

ISLANDS OF THE INDIAN OCEAN.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
Laccadive Islands.	Chitlac Islet: S. end	11 40 45	72 42 54				
	Betrapar Islet: N. Island	11 35 00	72 09 54				
	Kittan Islet: S. end	11 27 30	72 59 00	10 20	4 00	6.3	3.0
	Cardamum Islet: Center	11 13 00	72 44 00				
	Ameni Islet: N. end	11 06 00	72 41 00				
	Underut Islet: Center	10 47 00	73 40 00				
	Cabrut Islet: E. end	10 32 00	72 37 40				
	Seuheli Par: N. islet	10 06 00	72 15 10				
	Kalpeni Islet: S. end	10 03 00	73 35 54				
	Minikoi Island: Light-house	8 16 00	73 01 15	11 27	5 15	2.5	1.2
Maldive Islands.	Heawandu Island: S. end	6 55 00	72 55 54				
	Kee-lah Island: N. end	6 59 00	73 12 54				
	Mah Kundu Island: NE. extreme	6 25 00	72 41 54				
	Nar Foree Island	5 26 30	73 20 00				
	Hee-tah-doo Island	5 01 30	72 53 00				
	To-du Island: Center	4 25 45	72 57 24				
	Gafor Island: Center	4 44 00	73 28 00				
	Malé, or Kings Island: Flagstaff	4 10 15	73 30 24	0 20	6 25	2.9	1.4
	Pha-li-du Island: Northern end	3 41 00	73 24 54				
	Moluk Island: Center	2 57 00	73 34 24				
	Himmittee Island	3 16 00	72 48 00				
	Kimbeedso Island: S. end	2 10 30	73 03 00				
	Esdu Island: NE. pt	2 07 00	73 35 54				
	Wahdu Island: E. end	0 14 30	73 13 00				
		Lat. S.					
	Addu Atoll: Gung I	0 41 30	73 06 54				
	Amirante Islands: Ile des Roches, N. beach	5 40 56	53 41 03				
	African Islands	4 52 26	53 23 38				
	Seychelle Is., Platte I.: S. end	5 53 00	55 27 10				
	Port Victoria: End of Hodoul Jetty	4 37 15	55 27 23	4 22	10 35	4.3	1.2
	Bird Island: Tree	3 43 06	55 12 19				
	Chagos Archipelago, Peros Banhos: Diamond Islet	5 15 00	71 43 47				
	Diego Garcia: N. end of Middle I	7 13 37	72 23 50	1 30	7 43	5.8	1.7
	Cargados Carajos: Establishment I., flagstaff	16 25 12	59 46 40	1 50	8 03	4.0	1.2
	Rodriguez Island: Mathurina Bay, Point Venus	19 40 22	63 25 38	0 20	6 32	5.5	1.6
Mauritius I.	Flat Island: Light-house	19 52 36	57 39 14				
	Cannonier Point: Light-house	19 59 45	57 32 35				
	Port Louis: Martello tower, Ft. George	20 08 46	57 29 26	0 48	7 00	1.6	0.3
	Grand Port: Fouquet I. light	20 24 20	57 47 14				

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE INDIAN OCEAN—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Réunion Island: St. Denis light	20 51 38	55 26 59				
	Bel-Air light	20 53 11	55 36 18				
	St. Paul light	20 59 45	55 16 18				
	St. Pierre light	21 19 47	55 28 58	11 50	5 38	3.5	0.6
	Tromelin Island: N. end	15 51 37	54 28 46				
	Agalegas Island: NW. pt	10 21 30	56 32 00				
	Farquhar Islands: Hall's house	10 06 45	51 10 21				
	Alphonse Island: SE. part (Trees)	7 00 30	52 44 57				
	Coetivy Island: N. end	7 06 00	56 22 00				
Madagascar.	Cape St. Mary: S. extreme	25 39 10	45 06 50				
	Leven Island: Center	25 12 30	44 17 57				
	Port Machikora: Barracouta I	25 03 00	44 07 20				
	St. Augustine Bay: Nosi Vei I	23 38 25	43 38 20	5 40	11 52	9.8	2.9
	Murderers Bay: Center of Murder I	22 05 18	43 15 20				
	Cape St. Vincent: Extreme	21 54 24	43 20 21				
	Mourondava: Village	20 18 18	44 19 21				
	Tsmano: Village	19 49 30	44 31 30				
	Kovra Rythi Point: Extreme	17 53 00	44 02 20				
	Coffin Island: Nosi Vao	17 29 00	43 45 18				
	Cape St. Andrew: Extreme	16 12 10	44 29 05				
	Boyanna Bay: Barabata Pt	16 07 00	45 17 09				
	Cape Tauzon: Extreme	15 46 30	45 43 09				
	Majunga (Mojanga): Light-house	15 43 45	46 18 45	4 15	11 28	10.9	3.2
	Majamba Bay: W. pt	15 11 42	46 57 29				
	Narendri Bay: Moormora Pt	14 40 18	47 24 36				
	Port Radama: Pt. Blair	13 59 00	47 58 21				
	Radama Islands: N. pt. Nossuvee I	13 55 40	47 48 05				
	Baratoube Bay: Ambubuka Pt	13 27 15	47 59 30				
	Nosi Bé: Hellville jetty	13 23 38	48 17 34				
	Minow Islands: N. pt. Great I	12 49 30	48 38 57				
	Cape San Sebastian: Extreme	12 27 20	48 45 45				
	Port Liverpool: N. pt. of entrance	12 03 18	49 11 21				
	Cape Amber: NE. extreme	11 57 30	49 17 25				
	Port Lady Frances: Sunson Pt	12 23 20	49 35 56				
	Port Looké: Pt. Bathurst	12 44 02	49 45 06				
	Port Leven: S. pt. Nosi Hau I	12 49 00	49 54 00				
	Andrava Bay: Berry Head	12 56 48	49 56 25				
	Vohemar: Flagstaff	13 21 15	50 01 59				
	Cape East: Ugoncy I	15 15 48	50 31 21				
	Venangue Bé Bay: Entrance	15 54 50	50 16 05				
	Port Choiseul: Maran Seelzy Village	15 27 55	49 49 11	3 45	9 57	5.1	1.5
	Cape Bellone: Extreme	16 14 00	49 50 59				
	St. Marys Island: Light on Madame I	17 00 05	49 50 59				
	Port Tantang: Flagstaff	16 42 30	49 56 15				
	Fenerive Point: Flagstaff	17 23 16	49 32 04				
	Tamatave: Pt. Hastie	18 09 47	49 25 31	4 00	10 12	7.3	2.1
	Mahanuru: Town	19 55 00	48 52 10				
	Matatane: Village	21 58 10	48 14 50				
	Santa Lucia: N. end of town, Obs. Rock	24 46 25	47 10 34				
	Point Ytapere: Extreme	24 59 42	47 07 20				
	Ytapere Bay: N. pt	24 58 50	47 04 24				
	Fort Dauphin: Flagstaff	25 01 30	46 59 11	4 15	10 27	4.7	1.3
	Europa Island: Center	22 22 30	40 24 10				
	Bassas da India: E. pt	21 29 00	39 40 39				
	Geyser Reef: SE. extreme	12 26 30	46 32 35				
	Mayotta Island: Zaoudzi	12 47 02	45 16 27	4 00	10 13	11.9	2.0
	Johanna Island: Landing place, Pomoni Harbor	12 16 20	44 24 54				
	Mohilla Island: Numa Choa Harbor	12 25 00	43 47 00				
	Glorioso Islands: W. islet	11 34 48	47 24 09				
	Comoro Island: Islet in Mauroni Bay	11 40 44	43 19 15	4 45	10 58	10.0	1.7
	Assumption Island: Hummock	9 46 20	46 31 07				
	Aldabra Island: West I., E. side entrance	9 22 35	46 14 52				
	Cosmoledo Islands: Observation islet	9 41 20	47 32 25				

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE INDIAN OCEAN—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Prince Edwards Islands: Marion I., Obs. spot, NE. side	46 49 30	37 49 15				
Crozet Is.	Penguin Islands: Center of SW. islet	46 36 00	50 41 30				
Crozet Is.	Possession Island: NW. pt	46 22 00	51 30 15				
Crozet Is.	Twelve Islands: Summit NE. I	46 01 00	50 40 00				
Crozet Is.	Navire Bay	46 28 18	51 50 00				
Crozet Is.	Hog Island: Summit	46 10 40	50 35 00				
Crozet Is.	East Island: Center	46 26 00	52 13 00				
Kerguelen Is.	Christmas Harbor	48 40 00	69 04 00				
Kerguelen Is.	Blighs Cape	48 26 45	68 48 20				
Kerguelen Is.	Cape Bourbon	49 42 00	68 54 00				
Kerguelen Is.	Molloy, Port Royal Sound: U. S. Tr. of Venus Obs., 1874	49 21 22	70 04 31	0 14	6 36	4.6	1.3
Kerguelen Is.	Cape Challenger	49 41 00	70 15 00				
Kerguelen Is.	Balfour Rock	49 29 00	70 29 50				
	Heard Island: Cape Laurens, NW. end	53 02 45	73 15 30				
	Sealing station	53 13 00	73 52 00				
	McDonald Island, Summit	53 02 50	72 31 45				
	St. Pauls Island: Ninepin Rock	38 42 51	77 31 53	10 40	4 28	3.0	0.9
	Amsterdam Island: Summit, 2,750 feet	37 50 00	77 29 15	10 50	4 38	3.3	1.0
	Keeling or Cocos Islands: Direction I	12 06 22	96 53 02	5 20	11 32	5.1	1.5
	Christmas Island: Flying Fish Cove	10 25 19	105 45 57	7 10	1 00	4.5	1.3

SOUTH COAST OF ASIA.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
Arabia.	Aden: Telegraph station	12 47 16	44 59 07	7 49	1 41	4.9	2.0
Arabia.	Sughra: Sheik's house	13 22 00	45 40 50				
Arabia.	Mokatein: Black ruin	13 24 50	46 26 35				
Arabia.	Howaiyuh: Sheik's house	13 28 45	46 39 00				
Arabia.	Banderburum: SE. house of town	14 20 10	48 56 45				
Arabia.	Makalleh Bay: Flagstaff	14 31 15	49 07 35	8 20	2 07	6.8	2.8
Arabia.	Shahah Roads: Custom-house	14 43 50	49 35 05				
Arabia.	Sharmoh: Single house	14 49 00	49 57 05				
Arabia.	Kosair: High house	14 54 40	50 16 35				
Arabia.	Sihut: Center of town	15 12 00	51 10 30				
Arabia.	Ras Fartak: Extreme pt	15 38 00	52 14 20				
Arabia.	Damghot: Town	16 30 00	52 48 00				
Arabia.	Merbat: Town	16 59 00	54 43 29	8 50	2 38	7.0	2.9
Arabia.	Kuria Maria Is., Hullaniyeh I.: NE. bluff	17 32 45	56 03 05				
Arabia.	Ras Sherbedat: Point	17 53 15	56 20 35				
Arabia.	Cape Isolette: Islet	19 00 25	57 51 35				
Arabia.	Masirah Island: Point Abu-Rasas	20 10 00	58 38 35				
Arabia.	Point Ras Ye	20 31 30	58 58 35	9 45	3 32	9.6	4.4
Arabia.	Ras-al-Hed: Extreme pt	22 32 40	59 48 35	9 15	3 03	8.9	4.1
Arabia.	Maskat (Muscat): Maskat Pt	23 38 00	58 30 50	9 30	3 20	6.0	2.8
Arabia.	Deimaniyeh Islands: E. islet	23 52 00	58 08 00				
Arabia.	Sueik: Fort	23 51 30	57 26 00				
Arabia.	Sohar: SE. tower of town hall	24 21 50	56 46 12				
Arabia.	Khaur Fakan Bay: W. end of village	25 21 00	56 22 56				
Arabia.	Ras Musendom: N. end of island	26 24 13	56 32 22				
Arabia.	Great Quoin Islet: Center	26 30 00	56 31 29				
Arabia.	Sharjah: High tower with flagstaff	25 21 34	55 24 12				
Arabia.	Abu-Thabi: Fort flagstaff	24 29 02	54 22 14				
Arabia.	Al Beda'a Harbor: Nessah Pt., N. extreme	25 17 24	51 33 32				
Arabia.	Ras Rakkin: NW. pt	26 10 55	51 13 46				
Arabia.	Bahrain Harbor: Portuguese fort	26 13 56	50 32 17	5 15	11 30	6.4	3.7
Arabia.	Basrah: Custom-house flagstaff	30 32 00	47 51 23				
Arabia.	Kuweit Harbor: N. end of town	29 22 56	48 00 55	0 05	6 17	8.3	4.8
Persia.	Khárig Islet: Fort flagstaff	29 15 25	50 21 11				
Persia.	Abu Shahr: Residency flagstaff	28 59 07	50 50 35	7 12	1 13	2.6	1.5
Persia.	Shaikh Shu'aib Islet: E. end	26 47 40	53 23 36				
Persia.	Kais Islet: NE. pt	26 33 37	54 02 21	0 30	6 40	6.6	3.8

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

SOUTH COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Persia.	Básidúh: Chapel	26 39 12	55 16 47				
	Haujam Islet: Ruined mosque	26 40 49	55 54 25				
	Kasm: Fort	26 57 27	56 17 37	10 50	4 35	11.6	5.3
	Jashak Bay: Telegraph office	25 38 19	57 46 14	9 20	3 05	7.8	3.6
	Kub Kalat: High peak, 1,680 feet	25 29 45	59 40 32				
	Chahbar Bay: Telegraph office	25 16 43	60 37 40				
	Gwatar Bay: Islet	25 03 17	61 26 24				
Baluchistan.	Gwadar Bay: Telegraph office	25 07 19	62 19 42	9 20	3 05	8.1	3.7
	Pasni: Telegraph office	25 15 52	63 28 37				
	Ormarah: Telegraph office	25 11 55	64 37 02				
	Sunmiyani: Jam's house	25 25 19	66 35 39	8 50	2 35	8.1	3.8
	Cape Monze: Peak	24 50 03	66 39 58				
India.	Karachi: Manora light	24 47 37	66 58 06	10 15	4 00	7.3	3.4
	Observatory	24 49 50	67 01 33				
	Mandavi: Light-house	22 50 00	69 20 15				
	Beyt (Bet): Light-house	22 29 20	69 04 40	12 05	5 39	10.8	5.2
	Dwarka: Light-house	22 14 00	68 57 06				
	Temple spire	22 14 00	68 58 54				
	Porebander: Light-house	21 38 00	69 36 00				
	Mangarol: Light-house	21 06 00	70 06 32				
	Diu Head: Light-house	20 41 20	70 50 45				
	Kutpur: Light-house	21 02 21	71 49 35				
	Bhaunagar: Light-house	21 47 00	72 14 00	4 27	11 18	29.8	15.1
	Perim Island: Light-house	21 35 54	72 21 08				
	Cambay: Flagstaff	22 17 00	72 35 10				
	Surat River: Tapti light	21 05 20	72 38 40				
	Surat: Minaret Adrusah	21 12 19	72 49 27				
	Bassein: Center of town	19 20 10	72 48 44				
	Bombay: Observatory	18 53 45	72 48 56	11 26	5 08	12.0	4.9
	Kenery Island light	18 42 08	72 48 49				
	Bankot: Fort Victoria	17 58 00	73 02 40				
	Ratnagherry: Fort	16 59 30	73 15 56				
	Viziadrug: Fort flagstaff	16 33 26	73 19 39				
	Cape Ramas: W. bastion of fort	15 05 12	73 54 50				
	Goa: St. Denis Church	15 21 24	73 54 00				
	Agaada light	15 29 25	73 46 10	10 34	4 10	5.2	2.5
	Vingorla: Signal-station light	15 51 10	73 37 00				
	Vingorla Rocks: Light-house	15 53 20	73 27 15				
	Sedashigar Bay: Oyster Rock light	14 49 00	74 03 40	10 34	4 11	5.0	2.4
	Kumpta: Light-house	14 25 00	74 22 30				
	Hináwar: Monument	14 17 28	74 26 40				
	Kundapur: Light-house	13 38 15	74 39 50				
	Mangalore: Light-house	12 52 17	74 50 40	10 50	4 28	6.5	3.4
	Kannanur: Light-house	11 51 10	75 21 51				
	Tellicherri: Flagstaff	11 45 00	75 29 40				
	Mahé: Light-house	11 42 00	75 31 10				
	Calicut: Light-house	11 15 10	75 46 40	11 21	4 59	2.7	1.4
	Cochin: Light-house	9 58 00	76 14 40	11 33	5 06	2.1	1.0
	Alipee: Light-house	9 30 00	76 20 40				
	Quilon: Tongacherri Point light	8 53 20	76 34 00	0 18	6 16	2.5	1.3
	Trevandrum: Observatory	8 30 47	76 56 45				
	Cape Comorin: Light-house	8 04 00	77 32 35				
	Trichendore: Pagoda on pt	8 29 55	78 07 47				
	Tuticorin: Light-house	8 47 10	78 11 26	1 52	7 51	3.0	0.8
	Paumben Pass: Light-house	9 17 20	79 12 50	1 37	7 36	2.0	0.5
Ceylon.	Manaar: Center of town	8 59 00	79 53 52				
	Colombo: Light-house	6 55 40	79 50 40	1 55	7 49	2.0	0.4
	Dondra Head: Light-house	5 55 30	80 34 12				
	Point de Galle: Light-house	6 01 25	80 13 04	2 02	8 07	1.9	0.4
	Great Bassas Rocks: Light-house	6 10 10	81 28 15				
	Little Bassas Rocks: Light-house	6 25 00	81 44 00				
	Batticaloa: Light-house	7 45 00	81 41 00				
	Trincomali: Dock-yard flagstaff	8 33 30	81 13 42	8 10	1 44	2.0	0.5
India.	Calimere Point: Light-house	10 18 00	79 51 30				
	Negapatam: Light-house	10 45 28	79 50 47	8 37	2 37	2.1	0.9
	Pondicherri: Light-house	11 55 40	79 50 10				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

SOUTH COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
India.	Madras: Observatory	13 04 06	80 14 51				
	Light-house	13 05 15	80 17 00	8 41	2 26	3.1	1.2
	Pulicat: Light-house	13 25 15	80 19 12				
	Armeghon: Light-house	13 53 08	80 12 30				
	Kistna: Light-house	15 47 00	80 59 00				
	Masulipatam: Flagstaff	16 09 45	81 11 00				
	Coconada: Light-house	16 56 21	82 15 05	8 42	2 35	4.5	1.9
	Vizagapatam: Fort flagstaff	17 41 34	83 17 42	8 48	2 34	4.4	1.8
	Kalingapatam: Light-house	18 19 00	84 07 30				
	Gopalpur: Light-house	19 13 00	84 52 06				
	Gaujam: Fort	19 22 30	85 03 29				
	Juggernath: Great temple	19 48 17	85 49 09				
	False Point: Light-house	20 20 20	86 44 00	9 21	3 00	6.8	2.6
	Balasor River: Chandipur light	21 27 15	87 02 20				
	Saugor Island: Light-house	21 38 40	88 02 00				
	Diamond Harbor: Flagstaff	22 11 10	88 11 07				
	Calcutta: Ft. William semaphore	22 33 25	88 20 12	1 25	9 06	11.2	4.4
Burma.	Chittagong River: Light-house	22 11 00	91 49 00	1 02	7 56	13.1	5.6
	Akyab: Oyster Reef light	20 05 00	92 39 00				
	Old temple	20 08 53	92 52 40	9 40	3 28	7.6	3.0
	Ramree Island: S. pt	18 51 00	93 56 30				
	Chedubah Island: NW. peak	18 50 30	93 31 00				
	Cape Negrais: Extreme	16 01 30	94 13 16				
	Bassein River: Alguada Reef light	15 42 14	94 12 00				
	Bassein: Port Dalhousie	16 01 30	94 23 00	3 05	9 55	18.7	7.8
	Andaman Is.: Table Id., Light-house	14 12 30	93 22 30				
	Port Cornwallis, Rock in entrance	13 18 40	92 57 10	9 50	3 37	8.6	2.9
	Port Blair, Light-house	11 40 40	92 45 15	9 40	3 27	6.3	2.1
	Little Andaman Island, SE. pt	10 27 00	92 31 10				
	Krishna Shoal: Light vessel	15 37 26	95 37 32				
	Rangoon River: Grove Pt. light	16 30 01	96 23 00				
	Rangoon: Great Dagon pagoda	16 46 00	96 07 30	4 26	11 15	16.9	7.0
	Moulmein: Docks	16 26 00	97 38 00	3 07	10 49	11.7	5.0
	Moulmein River: Amherst Pt. light	16 04 45	97 33 05	2 12	8 49	19.2	7.4
	Double Island: Light-house	15 52 00	97 35 00				
	Tavoy River: Light-house	13 36 40	98 13 00	10 50	4 20	15.6	5.9
	Mergui: Court-house	12 26 15	98 35 59	10 40	4 10	18.0	6.9
	Tenasserim	12 06 00	99 03 00				
	St. Matthew Island: Hastings Harbor	10 05 05	98 10 15				
	Pak Chan River: Light-house	9 58 00	97 35 00				
Malaysia.	Tongka Harbor, Junkseylon Island: Light-house	7 50 00	98 25 30				
	Pulo Penang: Fort Cornwallis	5 24 45	100 21 44	11 50	5 40	8.8	3.8
	Dinding Channel: Hospital Rock	4 13 05	100 34 15				
	One Fathom Bank: Light-house	2 52 10	100 59 12	5 50	12 00	14.4	6.2
	Cape Rachado: Light-house	2 24 08	101 51 02				
	Malacca; Stat. St. Pauls Hill	2 11 30	102 15 00	7 20	1 08	10.5	4.5
	Singapore Strait: Coney Island light	1 09 57	103 44 47				
	Singapore: Fullerton Battery	1 17 11	103 51 15	10 18	4 02	7.6	3.2
	Singapore Strait: Pedra Branca light	1 19 57	104 24 08				
	Summit Bintang great hill, 1,253 feet	1 04 20	104 27 21				
	Rhio Straits, Pulo Sauh: Light-house	1 03 13	104 10 30				
	Terkolei: Light-house	0 57 10	104 19 52				
	Little Garras: Light-house	0 44 30	104 21 19	9 40	3 14	7.1	3.1
	Rhio, Bintang Island: Residency flagstaff	0 55 50	104 25 43				
	Pitong Island: Peak	0 36 52	104 04 42				
	Abang Besar Island: N. pt	0 36 30	104 11 31				
		Lat. S.					
	Linga Island: Flagstaff	0 12 34	104 36 14	6 00	12 13	11.5	4.9
	Singkep Island: Mountain summit	0 26 13	104 30 15				
	Menali Island: N. pt	0 57 51	105 38 20				
		Lat. N.					
	Nicobar Islands, Car Nicobar: N. pt	9 15 40	92 48 00				

MARITIME POSITIONS AND TIDAL DATA.

SOUTH COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Malaysia.	Nicobar Islands, Nancowry Harbor: Naval Pt	8 02 10	93 29 42	9 05	2 52	8.3	2.8
	Great Nicobar: W. pt. Galathea Bay	6 46 20	93 49 20	......	......	......	......
Sumatra.	Acheen (Acheh) Head: Pulo Bras light	5 45 00	95 04 33	......	......	......	......
	N. extreme	5 34 40	95 19 00	10 00	3 44	5.2	2.3
	Diamond Point: Light-house	5 15 58	97 30 11	11 50	5 34	8.7	3.7
		Lat. S.					
	Point Baru or Datu: Extreme	0 00 32	103 47 58	......	......	......	......
	Point Bon or Djabon: Extreme	1 00 55	104 21 30	......	......	......	......
	Moeara-Kompehi: Fort	1 23 13	103 59 14	......	......	......	......
	Djambi: Flagstaff of fort	1 35 33	103 36 41	......	......	......	......
	Palembang: Residency flagstaff	2 59 26	104 45 34	......	......	......	......
	Lampong Bay: Telok Betong light	5 27 00	105 15 58	......	......	......	......
	Blimbing Bay	5 55 02	104 32 36	5 40	11 52	2.6	0.7
	Kroë: Village	5 11 24	103 55 42	......	......	......	......
	Engano Island: Barioe anchorage	5 18 50	102 07 28	......	......	......	......
	Bintœan: River mouth	4 48 35	103 20 18	......	......	......	......
	Mega Island: N. pt	3 59 25	101 00 58	......	......	......	......
	Benkulen: Light-house	3 47 22	102 14 50	5 50	12 03	4.0	1.1
	Bantal: Village	2 44 54	101 17 25	......	......	......	......
	Indrapura Point: Extreme	2 10 35	100 50 06	......	......	......	......
	Pisang: Light-house	0 59 56	100 19 28	......	......	......	......
	Padang: Light-house	0 57 53	100 20 19	5 35	11 48	5.5	1.4
	Siberaet Island: Sigeb Pt	0 53 58	98 53 58	......	......	......	......
	Katiagam: Village	0 07 41	99 45 20	......	......	......	......
	Batoe Islands: N. point of Simoe Islet	0 03 13	98 05 55	......	......	......	......
	Summit of Tello	0 02 56	98 16 43	......	......	......	......
		Lat. N.					
	Ayer Bangis: Fort flagstaff	0 11 41	99 22 09	5 29	11 42	2.8	0.7
	Natal: Fort flagstaff	0 33 11	99 06 33	......	......	......	......
	Nias Island: Lagoendi Bay	0 34 47	97 43 43	......	......	......	......
	Sitoli	1 17 36	97 36 46	......	......	......	......
	Lapan	1 24 16	97 12 28	......	......	......	......
	Siboga: Flagstaff	1 44 24	98 46 08	......	......	......	......
	Singkel: Post-office	2 16 47	97 45 06	......	......	......	......
	Bangkaru Islands: Bay	2 02 32	97 06 53	......	......	......	......
	Simaloe Island: NW. pt	2 51 30	95 56 02	......	......	......	......
	Tampat Toewon; Flagstaff	3 14 59	97 10 13	......	......	......	......
	Analaboe	4 08 14	96 07 23	......	......	......	......
	Batve Toetong: Landing place	4 38 21	95 34 29	......	......	......	......

EAST COAST OF ASIA.

Coast.	Place.	Lat. S.	Long. E.	H. W.	L. W.	Spg.	Neap.
Banka Strait.	Java Head: First Pt. light	6 44 30	105 11 48	5 30	11 42	2.5	0.7
	Sunda Strait: Krakatoa I. peak	6 08 46	105 26 58	6 50	0 37	3.8	1.1
	North Watcher Island: Light-house	5 12 17	106 27 33	......	......	......	......
	Lucipara I.: Beacon	3 13 05	106 13 02	......	......	......	......
	Banka Island: Tobol Ali Fort	3 00 48	106 27 22	[9 05]	[2 52]	[10.1]	......
	Berikat, summit	2 34 18	106 50 36	......	......	......	......
	Nanka I.: Light-house	2 23 20	105 44 30	[6 50]	[0 38]	[9.3]	......
	Banka Island: Mintok light	2 04 03	105 09 45	......	......	......	......
	Blinyu	1 38 26	105 46 28	......	......	......	......
	Crassok Pt	1 29 00	106 57 30	......	......	......	......
Gaspar Strait.	Shoalwater Island: Light-house	3 19 10	107 12 42	[2 08]	[8 21]	[5.6]	......
	Pulo Lepar: Light-house	2 56 52	106 54 38	......	......	......	......
	Pulo Jelaka: Light-house	2 52 05	107 00 43	......	......	......	......
	Billiton Island: Tandjong Pandan flagstaff	2 44 40	107 38 46	......	......	......	......
	Langkuas I. light	2 32 12	107 37 15	[3 17]	[9 29]	[6.6]	......
	Gaspar Island: Peak	2 24 30	107 03 33	......	......	......	......

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Entrance China Sea.	Carimata Island: Sharp peak	1 33 24	108 55 13				
	Pulo Eu: Center	2 07 00	104 17 00				
	Pulo Aor: S. peak, 1,805 feet	2 26 30	104 34 06				
		Lat. N.					
	St. Barbe Island: Center of W. side	0 07 26	107 13 00				
	Direction Island: S. pt	0 14 19	108 01 47				
	Dato Island: Summit	0 06 37	108 37 05				
	St. Julian Island: Summit	0 55 00	106 45 00				
	Tambelan Island: S. pt	0 56 52	107 32 57				
	Tamban I. obs. station	1 00 27	106 24 10				
	Victory Island: S. pt	1 34 41	106 18 27				
	Anamba Islands: White rock	2 18 10	105 35 58				
	Pulo Repon	2 25 00	105 52 00				
	Pulo Domar	2 44 31	105 22 57				
	St. Pierre Rock: S. pt	1 51 42	108 38 55				
	Natuna Islands: Pyramidal rocks	4 03 00	107 21 40				
	Semione I	4 31 00	107 42 30				
Gulf of Siam.	Pulo Varella: Center	3 17 00	103 40 00				
	Pulo Brala: Center	4 53 00	103 38 00				
	Tringano River: N. pt	5 21 40	103 08 00	8 00	1 48	5.8	2.5
	Great Redang Harbor: Bukit Maria I	5 44 21	103 01 37				
	Kalantan: Entrance small river	6 11 53	102 20 47				
	Cape Patani: NE. pt	6 58 01	101 18 39				
	Singora: SW. pt. of Ticos I	7 13 54	100 36 12	8 20	2 08	2.8	1.2
	Koh Krah Islet: SE. pt	8 24 47	100 45 27				
	Bangkok: Old British factory	13 44 20	100 28 42	8 00	2 00	7.3	3.1
	Cape Liant: NW. rock of Koh Mesan	12 35 08	100 56 47				
Cochin China.	Chentabun River: Entrance, Bar I	12 27 43	102 04 19	10 00	3 50	4.5	2.1
	Koh Chang: Small island on W. side	12 01 20	102 15 47				
	Koh Kong: S. pt. of river entrance	11 33 00	102 57 14				
	Kusrovie Rock: Center	11 06 25	102 47 49				
	Koh Tang Rocks: SW. rock of group	10 21 20	102 56 34				
	Panjang Island: NW. corner of SW. bay	9 18 14	103 29 14				
	Obi Islands: Light-house	8 25 20	104 48 30				
	Saigon: Observatory	10 46 47	106 42 10	5 00	11 20	9.8	4.2
	Mitho: S. gate of citadel	10 21 16	106 20 38				
	Cape St. James: Light-house	10 19 51	107 04 55				
	Cape Padaran: Extreme	11 21 00	108 58 00				
	Cape Varella: Extreme	12 53 40	109 23 42				
	Quin Hon: Battery flagstaff	13 45 23	109 14 52				
China Sea.	Condore Islands: Light-house	8 40 06	106 41 42				
	Safatu Island: Summit	9 58 23	109 06 00				
	Ceicer de Mer Island: SW. hill	10 32 36	108 56 27				
	Natuna Islands: Murundum I., SE. pt	2 02 55	109 06 10				
	Low I	3 00 00	107 48 00				
Cochin China.	Canton Pulo: Light-house	15 23 34	109 05 35				
	Cham-Callao Islet: Watering place	15 57 10	108 32 47				
	Tourane Bay: Light-house	16 07 00	108 11 30				
	Hon-Mé: Summit	19 22 14	105 55 22				
	Nam-Dinh: Citadel tower	20 25 30	106 08 41				
	Hon Dau Island: Light-house	20 40 03	106 47 10	9 00	2 48	4.3	2.1
China.	Hai-Fong: Observation pagoda	20 51 44	106 41 08				
	Hai-Duong: Citadel tower	20 56 29	106 17 56				
	Ha-Noi: Citadel tower	21 01 57	105 48 40				
	Pak-Hoi: Custom-house flagstaff	21 29 00	109 06 00	5 00	11 12	14.0	6.6
	Hainan Island: Cape Bastion, extreme	18 09 00	109 35 00				
	Gaalong Bay, E. Brother	18 11 30	109 41 30				

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
China.	Hainan Island: Light-house	20 01 15	110 16 10				
	Paracel Islands: Triton I	15 46 30	111 14 30				
	Observation bank	16 36 00	111 40 30				
	Lincoln I	16 40 07	112 43 32				
	Woody I	16 49 55	112 20 44				
	Pratas Island: NE. part	20 42 03	116 43 07				
	Ty-fung-kyoh Island: Center	21 22 30	111 10 30				
	Tien-pak Harbor: Pauk Pyah Islet	21 24 15	111 15 25	11 50	5 37	8.2	3.8
	Song-yui Point: Extreme	21 31 00	111 38 30				
	Hui-lang-san Harbor: Mamechow Islet	21 34 00	111 46 43				
	Mandarins Cap: Summit, 200 ft	21 28 00	112 21 30				
	Macao: Fort Guia light	22 11 40	113 34 00	9 50	3 38	6.3	3.0
	Fort San Francisco	22 11 24	113 33 25				
	Canton: Dutch Folly light	23 06 35	113 16 30	2 00	8 00	5.1	2.4
	Raleigh Rock: Center	22 02 00	113 47 00				
	Gap Rock: Light-house	21 48 50	113 56 20				
	Hongkong: Cathedral	22 16 52	114 09 31				
	Wellington Battery	22 16 23	114 10 02	9 20	2 52	4.4	2.0
	Lema Island: Lema Head	22 03 40	114 19 25				
	Nine-pin Rock: Center	22 15 45	114 22 07				
	Tuni-ang Island: Summit	22 27 06	114 36 45				
	Single Island: E. summit	22 24 06	114 39 12				
	Mendoza Island: Summit	22 30 42	114 50 00				
	Pank Piah Rock: Summit	22 32 54	115 01 00				
	Pedra Blanca Rock: Summit, 130 ft	22 18 30	115 06 54				
	Chino Bay: Obs. spot	22 48 14	115 47 56				
	Cupchi Point: Hill	22 48 07	116 04 26				
	Breaker Point: Light-house	22 56 24	116 29 44				
	Cape of Good Hope: Light-house	23 14 00	116 47 00				
	Swatau: British consulate	23 20 43	116 40 22	2 50	9 00	7.5	3.5
	Lamock Island: Light-house	23 15 43	117 17 04				
	Brothers Islets: SE. Islet	23 32 30	117 42 00				
	Tong-sang Harbor: Fall Peak	23 47 15	117 36 48	11 20	5 08	12.0	7.6
	Chapel Island: Light-house	24 09 49	118 13 30				
	Amoy: Taitan I. light	24 23 16	118 10 00	0 05	6 13	15.5	9.9
	Dodd Island: Light-house	24 25 44	118 30 11				
	Chinchin Harbor: Pisai Islet	24 49 13	118 41 00				
	Pyramid Point: Extreme	24 52 12	118 58 00				
	Ockseu Island: Light-house	24 59 36	119 27 07				
	Sorrel Rock: Summit	25 02 18	119 10 36				
	Lamyit Island: High Cone Peak	25 12 00	119 35 00				
	Hungwha Channel: Sentry I	25 16 30	119 45 00				
	Turnabout Island: Light-house	25 26 10	119 56 07				
	East Dog Island: Light-house	25 58 10	119 59 02				
	Min River: Pagoda, Losing I	25 59 00	119 27 16	0 30	7 00	19.3	12.2
	Temple Pt	26 08 26	119 37 35	9 45	3 33	19.0	12.0
	Alligator Island: Summit	26 09 29	120 24 06				
	Tung-yung Islands: Peak, N. end	26 22 37	120 29 40				
	Coney Island: Summit	26 30 00	120 10 00				
	Double Peak Island: Highest peak	26 36 06	120 11 12				
	Pih-seang Island: Town I	26 42 30	120 22 42				
	Dangerous Rock: Summit	26 51 25	120 32 33				
	Tae Islands: Summit	26 58 52	120 42 34				
	Nam-quan Harbor: Bate I	27 09 20	120 25 50	9 50	3 38	17.2	10.9
	Ping-fong Island: Summit	27 09 42	120 32 42				
	Pih-quan Peak: Summit	27 19 18	120 27 14				
	Port Namki: E. horn	27 26 18	121 06 36				
	Pih-ki-shan Island: Summit	27 37 36	121 12 09				
	Pe-shan Islands: Summit, SW. end	28 05 07	121 30 04				
	Tung-chuh Island: Summit	28 43 45	121 55 21				
	Kweshan Islands: Patahecock	29 22 45	122 13 16				
	Nimrod Sound: Middle islet	29 34 20	121 43 15				
	Tong-ting Islet: Summit	29 51 53	122 35 24				
	Chin-hai: Citadel	29 57 08	121 43 06				
	Ning-po: Square I. light	29 59 21	121 45 22	1 00	7 12	8.8	4.6
	Chusan Islands: Ting-hai Harbor	30 04 30	122 03 47				

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
China.	Video Island: Summit	30 08 04	122 45 48				
	West Volcano Island: Light-house	30 20 50	121 51 25				
	Chapu: Battery	30 36 00	121 03 00				
	Gutzlaff Island: Light-house	30 48 37	122 10 12				
	Saddle Islands: N. Saddle light	30 51 41	122 40 17				
	West Barren Island: Summit	30 44 07	123 08 27				
	Shanghai: Eng. consulate flagstaff	31 14 42	121 28 55				
	Wusung: Light-house	31 23 18	121 29 36	0 12	8 06	9.1	4.8
	Shaweishan Island: Light-house	31 25 27	122 14 12				
	Pescadores Islands: Fisher I. light	23 32 53	119 28 05				
	Second pt. on N. side Makung Harbor	23 32 54	119 30 12				
Formosa I.	South Cape: Light-house	21 55 00	120 51 00				
	Takau: Saracen Head	22 36 14	120 15 54	9 45	3 32	4.0	1.7
	Port Heongsan	24 46 00	120 55 00				
	Tam-sui Harbor: White Fort	25 10 24	121 25 00	10 00	3 47	8.0	3.4
	Kelung Harbor: Light-house	25 09 12	121 44 28	10 15	4 03	3.0	1.3
	Soo (Sauo) Bay: Beach near village	24 35 28	121 49 20	6 00	12 13	5.8	2.5
	Botel Tobago Sima: S. extreme	22 01 40	121 39 45				
Borneo.	Tanjong Datu	2 05 15	109 39 07				
	Saráwak River: Po Pt. light	1 43 50	110 30 30	4 00	10 12	9.0	3.9
	Saráwak: Fort	1 33 55	109 20 40	5 20	11 35	14.1	6.1
	Cape Sirik: Light-house	2 45 20	111 21 20				
	Tanjong Barram	2 36 15	113 58 57				
	Bruni River: Light-house	5 02 00	115 03 00				
	Labuan I., Victoria Hbr.: Light-house	5 15 25	115 16 05	9 35	3 23	5.5	2.4
	Sandakhan Harbor: Light-house	5 50 10	118 07 20	12 00	5 50	5.2	2.2
	Unsang: Anchorage	5 16 30	119 16 00				
	Cape Kaniongan: E. pt. of Borneo	1 04 00	118 56 00				
		Lat. S.					
	Pamaroong I.: E. pt. delta River Koetei	0 45 00	117 37 00	[7 45]	[1 33]	[7.0]	
	Pulo Laut: S. pt. Koengit Islet	4 05 42	116 01 40				
	Selatan Point: Extreme of Sita Pt	4 10 40	114 42 18				
	Bandjermasin: Residency flagstaff	3 18 55	114 34 56				
	Sampit Bay: Bandaran Pt	3 16 00	113 08 00				
	Kottaringin Bay: Samadra I	2 54 00	111 24 00				
	Succadana: Town	1 14 00	109 58 00				
	Padang Tikar: Point	0 40 00	109 16 00	7 00	0 47	7.2	3.1
Celebes Island.	Port Laykan: SW. pt. of Celebes	5 36 00	119 26 00				
	Macassar: Fort light	5 08 09	119 23 55	4 40	10 55	3.9	2.9
	Palos Bay: Village at head	0 57 00	119 47 30				
		Lat. N.					
	Cape Rivers: NE. Cape, Slime Islet	1 20 00	120 43 30				
	Gorontalo: Light-house	0 29 41	123 03 08				
	Manado Bay: Light-house	1 31 00	124 50 00	6 00	12 15	4.3	3.1
	Bajuren Island: Summit	2 07 00	125 22 00				
	Tagulanda Island: Peak	2 22 00	125 24 30				
	Seao Island: Conical peak	2 44 00	125 26 00				
	Sauguir Island: S. pt. Cape Palumbatu	3 21 00	125 39 00				
	Taluat Island: Kabruang I., SE. pt	3 49 00	127 02 30				
	Cape Flesko: Extreme	0 27 00	124 26 00				
		Lat. S.					
	Cape Talabo: E. end	0 46 00	123 27 00				
	Wowoni Island: N. pt	3 58 00	123 00 00				
	Bouton Island: N. pt	4 23 30	123 04 00				
	E. pt	5 15 00	123 16 00				
	Fort	5 29 15	122 36 41				
	Cape Lassa: Extreme	5 35 00	120 29 00				
	Salayar Island: N. pt	5 47 00	120 30 00				
	S. pt	6 26 00	120 28 30				

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Java.	Anjer: Fourth pt. light	6 04 15	105 53 05	7 11	0 58	2.4	0.7
	Bantam: Flagstaff	6 01 20	106 08 20				
	Batavia: Observatory	6 07 40	106 48 37	[11 58]	[5 46]	[3.0]	
	Buitenzorg: Palace tower	6 35 45	106 49 11				
	Boompjeo Island: Racket I. light	5 56 15	108 22 37				
	Cheribon: Light-house	6 43 00	108 34 00				
	Tegal: Flagstaff	6 51 09	109 08 07				
	Pekalongan: Light W. of entrance	6 51 29	109 41 08				
	Samarang: Light-house	6 57 09	110 25 03	[6 00]	[12 13]	[4.0]	
	Rembang: Residency flagstaff	6 42 18	111 20 32				
	Surabaya: Time-ball station	7 12 10	112 43 58	12 07	5 54	4.9	1.7
	Pasuruan: Light-house	7 37 30	112 55 00	11 44	5 31	6.2	2.3
	Madura Island: Light-house	7 02 00	112 41 09				
	Soemenep flagstaff	7 02 30	113 53 45				
	Besuki: Light-house	7 43 25	113 41 10				
	Cape Sedano: NE. pt. of Java	7 49 00	114 26 53				
	Banjuwangi: Fort	8 12 30	114 22 55	10 00	3 45	7.8	2.6
	Bantenan: S. pt. of Java	8 47 00	114 25 13				
	Barung Island: S. pt	8 32 00	113 15 00				
	Kambangan Island: Light-house	7 46 30	109 02 12	8 33	2 21	5.2	1.8
	Cape Anjoe: Extreme	7 25 00	106 24 30				
Islands.	Karimon Djawa Island: Flagstaff	5 52 57	110 25 29				
	Rawean Island: Sangkapura flagstaff	5 51 18	112 39 10				
	Great Solombo Island: NW. pt	5 32 28	114 23 42				
	Arentes Island: S. pt	5 05 46	114 35 00				
	Bali Island: Bliling light-house	8 05 30	115 03 48				
	Peak, 11,326 ft	8 21 00	115 28 00				
	Badong Bay, Kotta village	8 42 30	115 08 47	10 50	4 38	8.7	3.0
	Lombok Island: Peak 12,379 ft	8 23 00	116 27 30				
	Ampenam light	8 34 15	116 04 09	7 50	1 37	5.8	2.0
	Sumbawa I.: Sumbawa village	8 32 00	117 20 33				
	Tambora Volcano, summit E. side of crater	8 12 30	117 57 00				
	Bima, flagstaff	8 27 00	118 43 55	0 00	6 12	5.7	2.0
	Postilion Islands: N. island	6 31 00	118 43 00				
	Maria Reigersbergen I	7 30 00	117 56 00				
	Ardassier Islands: S. id	7 35 00	117 22 00				
	Brill Reef: Light-house	6 05 50	118 56 50				
	Hegadis Island	6 07 00	122 40 00				
	Token Bessi I.: Wangi-Wingi, NW. pt.	5 15 00	123 32 00				
	Binongko, S. pt	6 17 00	123 59 00				
	Gunong Api: Volcano	6 43 00	126 43 30				
	Lucipari Islands: N. islet	5 28 30	127 30 00				
	Flores Island: Reo village	8 16 15	120 29 55				
	Ende village	8 50 55	121 38 40				
	Flores Head, extreme	8 04 45	122 52 00				
	Komba Island: Peak, S. part	7 48 00	123 31 00				
	Adenara Island: Summit, Mount Woka.	8 20 30	123 15 00				
	Lombata Island: Mount Lamararap	8 33 00	123 22 00				
	Pantar Island: S. peak of saddle on S. pt	8 34 00	124 06 00				
	Ornbay Island: Dololo anchorage	8 12 00	124 23 00				
	Timor Island: Deli, custom-house	8 34 00	125 33 57	0 45	6 58	5.7	2.0
	Atapopa	9 00 00	124 52 00				
	Koupang, Fort Concordia	10 09 54	123 33 57	10 50	4 37	8.5	2.9
	Rotti Island: W. pt	10 46 00	122 52 00				
	Saru Island: Seba Bay, on NW. side	10 29 00	121 46 00				
	Sandalwood Island: Nangamessie	9 35 03	120 14 30	11 20	5 07	16.5	5.6
	Wetta Island: Ilwaki road	7 53 00	126 22 00				
	Roma Island: W. pt	7 38 00	127 19 00				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Islands.	Moa Island: Buffalo Peak, 4,100 ft	8 12 00	128 01 00				
	Sermalta Island: NE. pt	8 14 00	129 00 00				
	Damma Island: Kulewatta Harbor, N. pt.	7 03 00	128 28 00				
	Nila Island: Center	6 44 00	129 29 00				
	Mano or Bird Island: NW. extremity	5 32 50	130 17 44				
	Timor Laut Island: Olilet, on E. coast	7 55 00	131 23 30				
	Vordate Island: S. pt	7 04 00	131 55 00				
	Mulu Island: N. pt	6 35 00	131 40 00				
	Arru Islands: S. island	7 10 00	134 24 00				
	N. pt	5 20 00	134 40 00				
	Great Ki Island: S. pt	5 56 00	132 54 00				
	Tello Islands: S. island, summit	5 20 00	131 58 00				
	Tehor Island: NE. pt	4 44 00	131 47 00				
	Matabella Islands: Kukur	4 33 00	131 50 00				
	Goram Islands: Goram Mosque	4 03 05	131 25 23				
	Banda Island: Mole	4 31 53	129 53 18	1 45	7 57	9.0	6.6
	Bouro Island, Kajeli: Fort Defense	3 22 48	127 06 18	1 20	7 32	4.2	3.1
	Ceram Island: Kawa	2 55 52	128 07 04				
	Amboina Island: Light-house	3 41 00	128 10 00	2 20	8 32	7.5	5.5
	Xulla Islands, Taliabo Island: NW. pt	1 44 00	122 20 00				
	Mangola Island: E. pt	1 48 12	126 21 19				
	Besi Island: E. pt	2 28 00	126 01 00				
	Oby Major Island: W. pt	1 30 00	127 18 00				
	Popa Island: Outer Extremity Bay	1 11 21	129 55 48				
	Mysole Island: Efbe Harbor	2 04 00	130 12 00				
		Lat. N.					
	Gebey Islands: NW. pt	0 02 02	129 17 30				
	Gillolo Island: Cape Tabo: E. extreme	0 11 00	128 52 00				
	Cape Salawag: NE. pt	1 26 00	128 37 00				
	Derrick Point: N. extreme	2 12 00	128 03 30				
	Molucca Is., Makkian I.: Fort Reeburgh	0 24 00	127 21 00				
	Ternate Island: Residency flagstaff	0 47 13	127 22 39	5 00	11 10	3.9	2.9
		Lat. S.					
	Batian Island: Church	0 38 03	127 28 21				
		Lat. N.					
	Meiaco-Sima Is., Kumi I: N. Beach	24 26 00	122 56 00				
	Broughton Bay: Landing place	24 21 30	124 17 40				
	Port Haddington: Hamilton pt	24 25 00	124 06 40				
	Tai-pin-san: Hirara, Karimata Anch	24 48 18	125 17 57	7 27	1 14	4.9	2.1
	Raleigh Rock: Summit, 270 ft	25 55 00	124 35 00				
	Ti-ao-usu Island: Summit, 600 ft	25 58 30	123 40 00				
	Hoa-pin-su Island: N. face	25 47 07	123 30 31				
	Loo Choo Islands, Great Loo Choo: Nafa-Kiang	26 12 25	127 40 10	6 30	0 15	5.8	2.5
	Yori-sima, 413 ft	27 02 00	128 25 24				
	Yerabu-sima peak, 687 ft	27 21 00	128 33 10				
	Kakirouma: Summit, 2,207 ft	27 44 00	128 59 00				
	Iwo-sima: Volcano, 541 ft	27 53 00	128 14 30				
	Oho-sima: N. extreme	28 31 40	129 42 30				
	Kikai-jima: Summit, 867 ft	28 18 00	129 59 00				

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Philippine Islands.	Balábac Island, Cape Melville: Light-house	7 49 25	117 00 00				
	Paláwan Island, Cape Bovliluyan: S. extreme	8 20 25	117 09 35				
	Victoria Peak, 5,680 ft.	9 22 30	118 17 30				
	Port Royalist: Tide Pole Pt. Light	9 43 43	118 43 03	[11 30]	[5 20]	[6.5]	
	Taytay Fort	10 50 00	119 31 10				
	Port Barton: Bubon Pt.	10 29 19	119 05 36				
	Kabuli I.: Summit, N. extreme	11 26 25	119 29 55				
	Cuyo Island: Obs. spot	10 51 26	121 00 25				
	Agutaya Islet: Summit of Mt. Aguade	11 09 09	120 56 26				
	Quiniluban Islet: Summit	11 25 47	120 45 38				
	Culion Island: Fort	11 53 53	120 00 48				
	Busuanga Island: Mt. Tundalara	12 02 09	120 12 56				
	Apo Islet: Summit	12 39 46	120 27 18				
	Caluya Island: Summit	11 54 28	121 30 24				
	Semerara Island: N. extremity	12 06 45	121 20 10				
	Mindoro Island: Mangarin Pt., SE. extremity	12 20 03	121 03 33				
	Sablayan Pt., Vantay	12 50 15	120 44 42				
	Monte Calavite	13 28 40	120 22 33				
	Escarceo Pt	13 31 35	120 59 17				
	Pt. Dumaly	13 06 05	121 29 20				
	Ylin Island	12 17 15	121 01 53				
	Lubang Island, Port Tulig	13 49 30	120 09 58				
	Luzon Island, Batangas: Ast. station	13 45 22	121 02 56				
	Balayan: Plaza Rizal	13 56 17	120 43 37	[11 07]	[4 50]	[4.9]	
	Loro Peak: Summit, 3,985 feet	14 12 20	120 38 10				
	Caballo I.: Light-house	14 21 48	120 36 40				
	Corregidor Island: Light-house	14 22 27	120 33 48	[10 22]	[3 56]	[4.4]	
	Cavite: Sangley Pt. light	14 29 50	120 54 40				
	Manila: Pasig light-house	14 35 49	120 57 19	10 44	[4 10]	[4.6]	
	Manila: Cathedral	14 35 31	120 58 06				
	Subig: Town	14 52 36	120 13 52	[9 42]	[4 33]	[3.8]	
	Capones Islet: Light-house	14 55 33	120 00 15				
	Iba: Ast. station	15 19 30	119 57 11				
	Port Masinloc: Bani Pt.	15 34 48	119 54 16				
	Santa Cruz: Plaza	15 45 43	119 54 00				
	Sual: Army Hospital	16 04 06	120 06 01	[10 20]	[3 33]	[2.4]	
	Silaqui Islet: Summit	16 27 15	119 56 10	[10 21]	[3 44]	[2.3]	
	Port San Fernando: Main street	16 37 15	120 18 25	[9 40]	[3 29]	[2.6]	
	Candon: Ast. station	17 11 43	120 26 14				
	Port Santiago: Remarkable tree S. of port	17 16 55	120 25 07				
	Vigan: Race track	17 33 56	120 22 51				
	Salomague Island: Port Salomague flagstaff	17 47 17	120 25 04				
	Currimao: Town	18 01 09	120 28 44				
	Capa Bojeador: Light-house	18 31 08	120 35 35				
	Mairaira Pt.: Semaphore	18 39 02	120 50 53				
	Aparri: Plaza	18 21 43	121 37 27	5 43	−0 02	3.2	1.9
	Port San Vicente: San Vicente Islet	18 28 32	122 04 14				
	Cape Engaño: Roña Islet	18 32 02	122 05 49				
	Camiguin I.: Summit	18 50 26	121 48 26	6 00	−0 12	5.0	2.7
	Fuga Island: W. summit	18 52 54	121 15 42				
	Dalupiri Island: Peak	19 03 03	121 11 28				
	Calayan Island: NE. pt	19 22 00	121 32 00				
	Babayan Claro Island: W. pt	19 30 00	121 52 00				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Philippine Islands.	Balingtang Islands	19 58 30	122 14 00	......	......	......	......
	Batan Island: Mount Irada	20 28 30	122 01 20	......	......	......	......
	Ibayat Island: Mount Santa Rosa	20 48 00	121 52 30	......	......	......	......
	Yami Island: Islet off SW. part	21 04 56	121 58 24	......	......	......	......
	Luzon Island, Port Dimasalasan: Entrance	17 20 17	122 19 20	......	......	......	......
	Polillo I.: Port Polillo	14 51 00	121 54 48	......	......	......	......
	Tabaco: Church belfry	13 21 33	123 43 53	6 08	0 00	5.2	2.8
	Cautanduanco Islands: N. islet	14 09 00	124 06 48	......	......	......	......
	Cautanduanco Islands: S. extreme	13 28 30	124 04 48	......	......	......	......
	Point Calaan: S. extreme	12 31 20	124 04 18	......	......	......	......
	Port Sorsogon, Tinacos Islet	12 52 20	123 49 22	......	......	......	......
	Masbate Island, Palanog: Pier	12 22 10	123 35 58	......	......	......	......
	Bugui Pt. light-house	12 36 00	123 14 36	......	......	......	......
	Camasusu I.: Summit	12 10 03	123 12 47	......	......	......	......
	Tintolo Point: Extreme	11 56 09	123 07 34	......	......	......	......
	Burias Island: Busainga	13 07 40	123 02 45	[4 30]	[10 20]	[5.5]	......
	Marinduque I.: Summit of Mount Catala	13 18 10	121 54 33	......	......	......	......
	Maestro de Campo Island, Port Concepcion: Point Fernandez	12 54 03	121 43 08	......	......	......	......
	Banton Island: Banton Mountain	12 56 56	122 04 48	......	......	......	......
	Tablas Island: Tablas Head	12 38 42	122 08 38	......	......	......	......
	Sanguilan Pt	12 33 44	121 58 32	......	......	......	......
	Carabao Island: W. pt	12 03 15	121 53 53	......	......	......	......
	Romblon Island: Sabang Pt. light	12 36 00	122 17 08	......	......	......	......
	Summit over port	12 35 33	122 16 26	......	......	......	......
	Sibuyan Island: Summit	12 24 55	122 33 23	......	......	......	......
	Samar Island, Guiuan: Pier	11 01 30	125 43 14	......	......	......	......
	Catbalogan: Fort	11 46 44	124 51 37	......	......	......	......
	Maripipi Island: Summit	11 47 30	124 18 15	......	......	......	......
	Leyte, Tacloban	11 15 08	124 59 56	6 53	1 25	1.5	1.1
	Ormoc: Ast. station	11 00 17	124 36 20	......	......	......	......
	Palompon: Church	11 02 37	124 22 07	......	......	......	......
	Maasin	10 07 39	124 50 15	11 47	4 50	2.8	2.0
	Bohol I., Lapiniu I.: Mount Basiao	10 03 22	124 32 35	......	......	......	......
	Cebu Island, Cebu: Plaza	10 17 30	123 54 18	......	......	......	......
	Siquiquor Island, Port Canoan: S. pt. of entrance	9 15 17	123 34 26	......	......	......	......
	Negros Island, Port Bunbonon: E. pt. of entrance	9 03 37	123 06 09	......	......	......	......
	Dumaguete: Town	9 18 25	123 18 43	......	......	......	......
	Volcano of Malaspina, 8,192 ft	10 24 35	123 07 05	......	......	......	......
	Bacalod: Town	10 40 21	122 55 42	......	......	......	......
	Guimaras I., Inampulugan I., SW. pt	10 26 38	122 40 20	......	......	......	......
	Panay Island, Iloilo: Fort	10 41 27	122 34 26	11 06	5 22	4.2	1.9
	San José	10 44 08	121 54 27	......	......	......	......
	Pan de Azucar	11 16 47	122 09 09	......	......	......	......
	Batbatan Island: Summit	11 28 20	121 52 36	......	......	......	......
	Pucio Point: Extreme	11 45 30	121 58 59	......	......	......	......
	Port Batan: Village	11 35 40	122 28 50	......	......	......	......
	Capiz: Town	11 35 06	122 45 03	......	......	......	......
	Siargao Island, Port Sapao: Semaphore	10 11 26	126 02 53	......	......	......	......
	Gibdo Island: Semaphore	9 53 00	125 31 17	......	......	......	......
	Bucas Island: E. pt. of Port Sibanga	9 41 34	125 58 22	......	......	......	......
	Mindanao Island: Surigao	9 47 53	125 28 30	[11 40]	[6 15]	[6.5]	......
	Cape St. Augustin	6 14 30	125 47 48	......	......	......	......
	Mindanao Island, Davao: Mole	7 01 22	125 34 35	6 00	−0 13	6.9	5.1
	Saranguni Islets: W. islet	5 22 30	125 13 48	......	......	......	......
	Basianang Bay: N. pt. of Donauang I.	6 28 50	123 57 37	......	......	......	......
	Polloc: Small hill back of town	7 21 15	124 11 42	......	......	......	......

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	*h. m.*	*h. m.*	*ft.*	*ft.*
Philippine Islands.	Mindanao Island, Santa Cruz Islands: SE. islet	6 52 15	122 04 00				
	Zamboanga: Fort	6 54 03	122 04 52	6 50	0 42	3.8	2.8
	Sibuco Bay: Hill S. of beach	7 18 05	122 03 18				
	Port Sta. Maria: Fort	7 45 41	122 04 58				
	Dapitan: Village	8 40 15	123 23 13	[10 48]	[4 50]	[5.1]	
	Misamis: Fort	8 08 29	123 50 44				
	Camiguin Island: Mount Camiguin	9 10 19	124 42 50				
	Sombrero Rock: Center	10 43 00	121 33 00				
	Piedra Blanca: Center	10 27 00	121 03 00				
	Cagayanes Islands: Rocky islet between two larger islands	9 35 30	121 23 30				
	San Miguel Isles: E. pt. of Manuk Manukan	7 43 00	118 27 00				
	Cagayan Jolo Island: Middle of W. coast	7 00 38	118 26 06				
	Omapui Island: NW. extreme	4 54 10	119 22 45				
	Sibutu Island: Hill on E. coast	4 49 30	119 48 00				
	Simonor Island: NW. pt	4 55 30	119 46 45				
	Bahaltolis Island: Sandakan Harbor	5 50 00	118 11 00				
	Bongao Island: S. pt	5 00 30	119 44 15				
	Keenapoussan Island: Center	5 13 00	120 40 45				
	Bubuan Island: Lagoon entrance	5 25 15	120 35 00				
	Cuad Basang Island: SW. pt	5 27 10	120 11 30				
	Siassi: Town	5 32 40	120 48 25	5 54	−0 18	8.6	6.4
	Bulipongpong Island: Center hill	5 41 30	120 49 45				
	Tapul Island: Center hill, 1,676 ft.	5 44 30	120 55 00				
	Jolo Islands: Maimbun Anchorage, dry bank	5 54 45	121 00 40				
	Dalrymple Harbor, Tulyan Islet	6 02 30	121 18 20				
	Jolo light-house	6 03 40	120 58 40	[9 38]	[3 10]	[5.0]	
	Doc Can Islet: W. extreme	5 52 30	119 55 55				
	Pangituran Island: SW. pt	6 15 15	120 29 30				
	Basilan Island: La Isabela	6 42 43	121 56 50				
China.	Wang-kia-tia Bay: Langwang temple	35 39 00	119 51 30				
	Kyauchau Bay: Yunuisan light	36 02 50	120 17 30	4 50	11 03	11.4	6.0
	Staunton Island: Landing place, N. side	36 45 29	122 16 48				
	Shantung Promontory: Light-house	37 24 00	122 42 00	4 00	10 12	6.8	5.0
	Weihaiwei: Light, S. side harbor	37 27 41	122 15 05	9 20	3 08	9.0	6.6
	Chifu: Light-house	37 34 10	121 31 09	10 25	4 13	8.1	6.0
	Fort flagstaff	37 32 51	121 21 27				
	Miautao Island: Peak of N. Island	38 23 37	120 55 00				
	Pei-ho: S. Taku Fort, S. Cavalier	38 58 16	117 42 48				
	Tientsin: Shore opp. NE. angle of wall	39 09 00	117 11 44	6 50	1 00	4.5	3.3
	Shaluitien Island: Light-house	38 56 00	118 31 00				
	Niuchwang: Lightship	40 35 00	122 00 00	4 30	10 50	11.7	8.7
	Hulu-shan Bay: N. side	39 30 46	121 18 03				
	Port Adams: Entry	39 16 00	121 35 59				
	Liao-ti-shan Promontory: SW. pt. light	38 43 17	121 08 26				
	Port Arthur: Obs. spot	38 47 50	121 15 54	10 05	3 53	7.5	5.5
	Ta-lien-wan Bay: Isthmus on S. Sanshan I	38 52 38	121 51 59				
	Round Island: Summit	38 40 00	122 11 30				
	Thornton Haven, Hai-yun-tan Island: Beach opposite Temple Point	39 04 00	123 10 34				
Korea.	Choda Island: S. pt	38 27 00	124 34 40				
	Sir James Hall Islands: N. island	37 58 00	124 34 30				
	Chemulpo: So Wolmi	37 27 40	126 36 27	4 19	10 31	28.8	11.6
	Marjoribanks Harbor: Manzoc Islet	36 26 45	126 28 00				
	Tas de foin Islet: Center	36 24 30	126 24 00				
	Guerin Island: Summit, 969 ft	36 07 00	126 01 09				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Korea.	Kokoun-tan Islands: Camp Islet	35 48 08	126 31 00				
	Barren Island: Center, 600 ft	35 21 00	125 58 00				
	Sea Rock: Center, 160 ft	34 42 00	126 19 45				
	Modeste Island: N. peak, 1,228 ft	34 42 30	125 16 00				
	Ross Island: Peak, 1,920 ft	34 06 00	125 07 00				
	Kuper Harbor: NE. extreme of Josling I.	34 17 20	126 35 28				
	Port Hamilton: W. pt. of Obs. Island	34 01 23	127 18 34	9 05	2 52	10.5	4.2
	Bate Islands: Summit Thornton Islet	33 57 00	126 18 00				
	Montravel Island: Center, 1,041 feet	33 59 00	126 55 00				
	Quelpart Island: Beaufort I., middle of W. side	33 29 40	126 58 25				
	Observation Island: Point of W. arm	34 39 00	128 14 00				
	Sentinel Island: Summit, 400 feet	34 33 00	128 40 00				
	Broughton Head: Extreme	34 48 00	128 44 00				
	Tsau-liang-hai Harbor: Light-house	35 07 15	129 02 10	7 35	1 23	7.0	3.0
Japan.	Tsu Sima: Observation rock	34 18 55	129 13 06	8 56	2 44	6.7	2.4
	Iki Sima: Summit, S. end of island	33 44 30	129 42 30				
	Oro No Sima: Summit, 277 ft	33 52 10	130 02 00				
	Kosime No Osima: Summit Wilson I	33 53 50	130 25 20				
	Yeboshi Sima: Light-house	33 41 30	129 58 50				
	Yobuko Harbor: Bluff opposite Nicoya	33 32 30	129 52 43	9 23	3 10	6.4	2.5
	Hirado No Seto: Taske light	33 23 31	129 33 21				
	Goto Island: Ose Saki light	32 36 45	128 36 10				
	Pallas Rocks: S. rock	32 13 12	128 04 39				
	Meiaco Sima: Ears Peak	32 03 00	128 25 00				
	Nagasaki: Transit Venus Station	32 43 21	129 52 25	7 54	1 41	8.4	3.5
	Kuchinotsu: Light-house	32 36 05	130 13 40				
	Kagoshima: Breakwater light	31 35 39	130 33 49	6 40	1 00	10.5	4.4
	Tsukarase Rocks: Summit, 96 ft	31 20 00	129 46 20				
	Uji Shima: High peak, 1,097 ft	31 12 00	129 29 00				
	Yamagawa Harbor: Spit N. of town	31 12 43	130 37 00	7 20	1 08	9.5	3.9
	Satano Misaki: Light-house	30 59 30	130 39 30				
Linschoten Is.	Kusakaki Jima: Ingersoll Rocks, 530 ft.	30 51 00	129 28 00				
	Kuro Sima: 2,160 ft	30 50 00	129 55 30				
	Iwo Shima: Peak, 2,469 ft	30 47 00	130 18 00				
	Yakuno Shima: Mount Matomi, 6,252 ft.	30 17 00	130 32 00				
	Firase Rocks: Highest, 92 ft	30 05 00	130 03 00				
	Kuchino Shima: Summit, 2,230 ft	29 59 00	129 56 00				
	Guaja Shima: Summit, 1,687 ft	29 54 00	129 33 00				
	Naka no Shima: Peak, 3,400 ft	29 52 00	129 52 30				
	Suwanose Jima: Volcano, 2,706 ft	29 38 00	129 42 00				
	Tokara Jima: Summit, 860 ft	29 08 00	129 13 30				
	Yoko Shima: Summit, 1,700 ft	28 47 30	129 01 30				
Japan.	Shimonoseki Strait: Meji Zaki, extreme.	33 57 46	130 57 50				
	Rokuren Island: Light-house	33 58 53	130 52 07	8 30	2 20	6.7	2.4
	Shirasu Reef: Light-house	33 59 11	130 47 36				
	Susaki: SW. battery	33 23 19	133 17 00	5 55	12 08	5.0	2.0
	Tomo Roads: Tamatsu Sima	34 22 37	133 23 23	11 16	5 04	10.2	4.5
	Port Okayama: Take Sima temple	34 35 58	133 59 24				
	Wusimado Pt.: Wusimado Peak, 548 ft.	34 37 27	134 09 21				
	Akashi-no-seto: Maico Fort	34 38 05	135 01 51				
	Hiogo: Wada Misaki light	34 39 20	135 10 56				
	Kobe: Light-house	34 41 18	135 11 34				
	Osaka: Fort Temposan light	34 39 45	135 26 00	7 30	1 25	4.7	2.0
	Sakai: Pier-head light	34 35 12	135 27 44				
	Osaki Bay: Tree Islet, S. pt	34 07 42	135 08 19				
	Yura No Uchi: Pier	33 57 34	135 07 21				
	Tanabe Bay: Fossil pt	33 41 14	135 23 04				
	Oö-sima Hbr.: Kashinosaki light, E. pt.	33 28 15	135 51 59				
	Uragami Harbor: Village pt	33 33 37	135 54 25				
	Owashi Bay: Hikimoto	34 06 10	136 14 35				
	Mura Harbor: Osima Islet	34 13 52	136 48 51	6 23	0 10	4.7	2.0

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Japan.	Matoya Harbor: Anori-saki light	34 21 57	136 54 09	5 52	12 04	4.3	1.7
	Omoi Saki: Light-house	34 35 52	138 13 49				
	Shimizu Bay: Mound on pt	35 00 51	138 31 19	5 52	12 04	3.9	1.6
	Mikomoto Island: Light-house	34 34 25	138 56 30				
	Simoda Harbor: Center I	34 39 49	138 57 30				
	Yokosuka Harbor: Eyi Yama pt	35 17 30	139 39 43				
	Yokohama: English Hatoba light	35 26 52	139 38 41	5 25	11 30	4.9	1.9
	Tokio: Naval Observatory	35 39 18	139 44 30				
	No Sima Saki: Light-house	34 54 17	139 53 24	5 04	11 17	3.7	1.4
	Vries Island (O Sima) Volcano: Summit, 2,512 ft	34 43 30	139 23 00				
	Kozu Shima Volcano: Summit, 2,000 ft	34 13 15	139 08 00				
	Mikake Jima: Summit, 2,690 ft	34 05 00	139 31 00				
	Redfield Rocks: S. rock	33 56 50	138 48 15				
	Mikura Jima: Summit	33 52 00	139 34 00				
	Broughton Rock: Summit, 60 ft	33 39 00	139 17 45				
	Fatsizio Island: Observation spot	33 04 24	139 50 24				
	Aoga Shima: Center	32 29 00	139 43 31				
	Bayonnaise Island: Summit, 26 ft	32 00 40	140 00 00				
	Smith Island: Summit, 250 ft	31 27 00	140 02 00				
	Ponafidin Island: Summit, 1,328 ft	30 28 26	140 14 02				
	Lots Wife Rock: Summit, 300 ft	29 46 28	140 19 40				
	Inaboye Saki: Light-house	35 42 13	140 52 22				
	Kinkwosan Island: Light-house	38 16 57	141 35 33				
	Kamaishi Harbor: SE. end of village	39 16 30	141 52 50				
	Yamada Harbor: Ko Sima, 90 ft	39 27 17	141 59 00	4 30	10 45	3.4	1.3
	Siriya Saki: Light-house	41 25 58	141 27 32				
	Toriwi Saki: Center of Low Islet off	41 33 34	140 56 36				
	Awomori: Light-house	40 50 00	140 44 40				
	Tatsupi Saki: N. side	41 16 17	140 22 37				
	Bittern Rocks: SW. rock	40 31 00	139 31 00				
	Tobi Shima: Takamori Yama	39 12 02	139 32 58				
	Awa Sima: NE. extreme	38 29 23	139 15 31				
	Sado Island: Ya Saki	38 19 55	138 27 09				
	Fushiki Harbor: Light-house	36 47 47	137 03 15				
	Cape Roigen: Extreme	37 28 00	137 22 00				
	Niigata: Buddhist temple	37 55 14	139 03 01				
	Mana Sima: Summit, 200 ft	37 35 00	136 54 00				
	Manao Harbor: Sorenjo Pt	37 02 37	136 58 24				
	Tsuruga: Town	35 40 24	136 01 22	2 30	8 42	0.6	0.4
	Oki Islands: N. pt	36 30 00	133 23 00				
	Taka Yama (Cape Louisa): Extreme	34 40 00	131 36 00	11 41	5 28	1.1	0.5
	Ai Sima: Summit, 300 ft	34 32 00	131 18 00				
	Mino Sima: Summit, 492 ft	34 48 00	131 09 00				
	Kado Sima: Tsuno Shima light	34 21 12	130 50 29				
	Hakodate: Light-ship	41 47 36	140 41 49	3 40	10 00	3.0	1.2
	Endermo Harbor: Bluff on E. side	42 19 54	140 59 33	3 32	9 45	3.5	1.5
	Okishi Bay: Light-house	42 56 52	144 52 38	3 41	9 53	3.0	1.4
	Noshiaf Saki: Light-house	43 22 56	145 49 10	3 48	10 00	3.1	1.4
	Nemuro: Benten Sima light	43 20 22	145 34 40	3 33	9 46	2.1	0.5
	Notsuke Anchorage: Village	43 33 11	145 18 00	4 50	11 05	3.7	1.8
	Noshiaf Misaki: Light-house	45 26 30	141 38 40				
	Risiri Islet: Peak, 5,713 ft	45 11 00	141 19 00				
Kuril Islands.	Kunashir Island: St. Anthonys Peak	44 20 00	146 15 00				
	Iturup Island: NE. pt	45 38 30	149 14 00				
	Urup Island: Cape Vanderlind	45 37 00	149 34 00				
	Broughton Island: Summit	46 42 30	150 28 30				
	Simusir Island: Prevost Peak	47 02 50	151 52 50				
	Ketoy Island: S. pt	47 17 30	152 24 00				
	Matana Island: Peak	48 06 00	153 12 30				
	Shiash-Kotan Island: Center	48 52 00	154 08 00				
	Kharim-Kotan Island: Peak	49 08 00	154 39 00				
	Oune-Kotan Island: SW. pt	49 19 00	154 44 00				
	Moukon rushi Island: Center	49 51 00	154 32 00				
	Poro musir Island: Fool's Peak	50 15 36	156 15 20				
	Soumshu Island: Center	50 46 00	156 26 00				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

EAST COAST OF ASIA—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Korea.	Cape Clonard: Extreme	36 05 45	129 33 30				
	Ping-hai Harbor	36 36 00	129 20 00				
	Liancourt Rocks: Summit, 410 ft	37 09 30	131 55 00				
	Matu Sima: Peak, 4,000 ft	37 30 00	130 53 00				
	Port Lazaref: S. 1½ miles from the S. end of Bontenef I	39 19 12	127 32 48				
Siberia.	Wawoda Rock: Summit, 12 ft	42 14 30	137 17 00				
	Expedition Bay: Light-house	42 38 05	130 48 45				
	Port Novogorod: Light-house	42 33 40	131 10 00				
	Vladivostok: Cape Galdobin light	43 05 13	131 53 56	2 45	9 00	1.9	0.8
	Cape Povorotnyi: Light-house	42 41 00	133 02 00				
	Port Olga: Light-house	43 22 00	135 15 00				
	St. Vladimir Bay: Orekhera Pt	43 53 40	135 27 19				
	Shelter Bay	44 30 00	136 02 00				
	Sybillo Bay	44 43 45	136 22 30				
	Pique Bay	44 46 15	136 27 15				
	Bullock Bay	45 05 00	136 44 00				
	Luké Point: Extreme	45 19 30	137 10 15				
	Cape Disappointment: Extreme	45 41 30	137 38 15				
	Cape Suffren: Extreme	47 20 00	138 58 00				
	Cape St. Nikolaia: Light-house	48 59 30	140 23 40	9 50	3 40	2.7	1.1
	De Kastri: Light-house	51 28 00	140 48 00	10 45	4 40	6.3	2.6
	Sakhalin I., Cape Notoro: Light-house	45 53 10	142 04 51				
	Cape Siretoku: Extreme	46 01 20	143 26 30				
	Cape Elizabeth: N. pt	54 24 30	142 46 30	11 20	5 08	4.2	1.7
	Nikolaevsk: Cathedral	53 08 05	140 42 58				
	Great Shantar Island: N. pt	55 11 00	137 40 00				
	Port Aian: Cape Vneshni	56 25 28	138 25 50	0 10	7 30	8.4	3.4
	St. Jona Island: Summit, 1,200 ft	56 22 30	143 15 45				
	Okhotsk: Battery	59 19 45	143 07 14				
	Cape Lopatka: Extreme	51 02 00	156 46 00	3 55	10 08	4.6	1.9
	Petropavlovsk: Rakof light	52 52 37	158 46 42	3 30	9 45	5.1	2.1
	Cape Shipunski: Extreme	53 04 30	160 04 00				
	Bering Island: Cape Khitroff	54 56 00	166 43 00				
	Mednoi, or Copper Island: SE. extreme	54 32 24	168 09 00				
	Cape Kamchatka: Extreme	56 10 00	163 24 00				
	Karajinski Island: S. pt	58 26 00	163 34 00				
	Cape Oliutorski: Extreme, 2,480 ft	59 55 00	170 22 00	6 00	12 15	4.5	1.8
	Cape Navarin: Extreme, 2,512 ft	62 14 30	179 04 30				
			Long. W.				
	St. Matthew Island: Cape Upright, SE. pt	60 18 00	172 04 00				
	St. Lawrence Island: N. pt	63 12 00	159 50 00				
	Cape Tchoukotskoi: Extreme	64 16 00	173 10 00				
	Port Providence: Emma Harbor	64 25 55	173 07 15				
	Cape Indian: Extreme	64 24 30	172 12 30				
	Arakam Island: Cape Kiguinin	64 46 00	172 07 00				
			Long. E.				
	Anadir River: Mouth	64 50 00	178 40 00				
			Long. W.				
	Cape Bering: Extreme	65 00 30	175 54 00				
	East Cape: Extreme	66 02 00	169 32 30				

ISLANDS OF THE PACIFIC.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
	Malpelo Island: Summit, 1,200 ft	4 03 00	81 36 00				
	Cocos Island: Head of Chatham Bay	5 32 57	86 59 17				
Galapagos.	Redondo Rock: Summit, 85 ft	0 13 30	91 03 00				
	Towers Island: W. cliff	0 20 00	89 58 43				
	Bindloe Island: S. summit	0 18 50	90 30 08				
	Abingdon Island: Summit, 1,950 ft	0 34 25	90 44 23				
	Wenman Island: Summit, 550 ft	1 22 55	91 49 43				

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE PACIFIC—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Galapagos Islands.	Albemarle Island: Iguana Cove	0 59 00	91 29 12	2 00	8 13	6.2	3.1
	Marlborough Island: Cape Hammond	0 31 00	91 36 00				
	James Island: Sugarloaf, 1,200 ft	0 15 20	90 52 53	2 45	8 58	5.2	2.6
	Jervis Island: Summit	0 25 00	90 43 30				
	Duncan Island: Center hill	0 36 30	90 41 00				
	Indefatigable Island: NW. bay	0 33 25	90 33 58	2 00	8 13	6.2	3.1
	Barrington Island: W. summit, 900 ft	0 50 30	90 06 13				
	Charles Island: Summit, 1,780 ft	1 19 00	90 28 13	2 10	8 23	6.0	3.0
	Fatu Huku or Hood Island: E. summit, 640 ft	1 25 00	89 40 08				
	Chatham Island: Mount Pitt, 800 ft	0 44 15	89 16 58	2 20	8 33	6.5	3.3
		Lat. N.					
	Christmas Island: N. pt. of Cook Islet	1 57 17	157 27 45	4 25	10 38	2.4	1.4
	Fanning Island: Flagstaff, entrance to English Hbr	3 51 26	159 21 50	6 00	12 15	2.4	1.4
	Washington Island	4 41 10	160 24 30				
	Palmyra Island	5 52 15	162 05 00	5 25	11 40	1.5	0.9
	Baker Islet: Center	0 13 30	176 32 39				
	Howland Islands: Center island	0 49 00	176 43 09	7 10	1 00	6.2	3.6
		Lat. S.	Long. E.				
Gilbert Islands.	Arorai or Hurds Island: S. pt	2 40 54	177 01 13				
	Tamana Island: Center	2 35 00	176 07 00				
	Onoatoa Island: Center	1 50 00	175 39 00				
	Taputeuea or Drummond Island: SE. pt.	1 29 14	175 12 20				
	Nukunau or Byron Island: SE. pt	1 23 42	176 31 33				
	Peru or Francis Island: NW. pt	1 17 14	175 57 09				
	Nonuti or Sydenham Island	0 36 00	174 24 00				
		Lat. N.					
	Aranuka or Henderville Island: W. pt. of W. island	0 11 10	173 32 40				
	Apamama or Hoppers Island: Entrance islet	0 20 54	173 51 14	4 30	10 45	4.7	2.7
	Maiana Island: S. pt	0 51 30	173 03 30				
	Tarawa Island: NE. pt	1 38 45	173 03 00				
	Apaiang Island: S. pt	1 44 15	173 07 00	4 45	11 00	4.7	2.7
	Maraki Island: N. pt	2 03 00	173 25 30				
	Taritari Island: S. pt	3 01 30	172 45 40				
Marshall Islands.	Ebon Atoll: Rube Pt	4 35 25	168 41 31	4 45	11 00	4.7	2.7
	Jaluit or Bonham Islands: Jarbor Pier.	5 55 07	169 39 31				
	Burrh Island: Port Rhin, N. pt. of entrance	6 14 00	171 46 00	5 00	11 15	5.0	2.8
	Majuro or Arrowsmith Islands: Anchorage Djarrit I	7 05 30	171 24 30				
	Arno Atoll: NE. pt	7 09 17	171 55 51				
	Odia Islands: S. islet	7 15 00	168 46 00				
	Namu Island: S. pt	8 14 00	168 03 00				
	Jabwat Island: Center	8 27 00	168 26 00				
	Aurh or Ibbetson Island: NE. end, anchorage	8 19 00	171 09 00				
	Maloclab Islands: NW. end Karen Islet.	8 54 21	170 49 00				
	Wotje or Romanzov Islands: Christmas Harbor	9 28 09	170 16 05				
	Litkieh Island: NW. pt	10 03 40	169 01 57				
	Ailuk Islands: Capeniur Islet	10 17 25	169 59 20	4 50	11 00	6.2	3.6
	Bigar Islet: Center	11 48 00	170 07 00				
	Kongelab or Pescadores Islands: Center of group	11 19 21	167 24 57				
	Rongerik or Radakala Islands: Observation spot	11 24 00	167 35 00				
	Ailinginae Island: Easternmost Islet	11 07 00	166 35 00				
	Bikini or Eschholtz Islands: W. extreme	11 40 00	166 24 25				
	Wottho or Schanz Island: Center	10 05 00	166 04 00				
	Eniwetok Islands: North or Engibi I	11 40 00	162 15 00				
	Ujelang or Providence Island: Center of atoll	9 39 00	161 08 30				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE PACIFIC—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Greenwich Island: Northern islet	1 04 00	154 47 55				
Caroline Islands.	Matelotas group: Easternmost of the S. islands	8 18 30	137 33 30				
	Yap Island: Light in Tomil Bay	9 29 00	138 04 00	7 15	1 00	3.4	1.9
	Eau Island: Center	9 52 30	139 42 00				
	Uluthi or Mackenzie Islands: Mogmog Islet	10 06 00	139 46 00				
	Feys or Tromelin Island: E. extreme	9 46 00	140 35 00				
	Sorol or Philip Island: Center	8 06 00	140 52 00				
	Eauripik or Kama Islands: E. islet	6 40 00	143 11 00				
	Oleai group: Raur Islet, N. pt	7 21 45	143 57 30				
	Ifalik or Wilson Islets: N. end	7 15 00	144 31 00				
	Faraulep Island: S. end	8 35 00	144 36 00				
	W. Faiu Islet: Center	8 03 00	146 50 00				
	Olimarao Islet: Center	7 43 30	145 55 45				
	Toass Island: Center	7 29 30	146 24 30				
	Satawal Island: Center	7 22 00	147 06 48				
	Coquille or Pikelot Island: Center	8 09 00	147 42 00				
	Suk or Polusuk Island: S. end	6 40 00	149 21 00				
	Los Martires: Ollap Islet, N. pt	7 38 00	149 27 30				
	Namonuito Islands: Magur Islet	8 59 45	150 14 30				
	Hall Island: Namuine Islet	8 25 30	151 49 15				
	Hogolu (Hogulu) Group: N. end of Tsis Islet	7 18 30	151 56 30				
	Namoluk Islands: NW. islet	5 55 00	153 13 30				
	Mortlock Islands: Lukanor, Port Chamisso	5 29 18	153 58 00				
	Nukuor or Monteverde Islands: E. pt	3 51 00	155 00 54				
	Oraluk or Bordelaise Island: Center	7 39 00	155 05 00				
	Ngatik or Valientes Islands: E. extreme	5 48 00	157 31 30				
	Ponapi Island: Jamestown Harbor	7 00 35	158 12 21	4 00	10 15	4.3	2.4
	Mokil or Duperrey Islands: Aoura, NE. pt	6 41 45	159 50 00				
	Pingelasp or MacAskill Islands: E. end of island	6 14 00	160 38 43				
	Ualan or Strong Island: Chabrol Harbor	5 20 06	163 00 45	6 00	12 15	3.5	2.0
Pelew Islands.	Angaur Island: SW. pt	6 53 55	134 05 24				
	Pililu Island: S. pt	7 02 00	133 18 03				
	Earakong or Akamokan Island: Center	7 08 00	134 27 00				
	Korror Islands: Korror Harbor, Malakal pier	7 19 00	134 32 30				
	Baubeltaub Island: Cape Artingal	7 40 30	134 39 30				
	Kyangle Islets: Center of largest	8 08 00	134 17 00				
	Warren Hastings Island: Center	4 20 00	132 21 00				
	Nevil or Lord North Island: Center	3 02 00	131 11 00				
	Sonserol Island: Approx	5 20 00	132 16 00				
Ladrone (or Mariana) Islands.	Guam Island: Fort Sta. Cruz, San Luis d'Apra	13 25 48	144 39 30	7 20	1 20	2.6	1.5
	Rota Island: Summit	14 07 30	145 13 04				
	Tinian Island: Sunharon village	14 59 22	145 36 20				
	Saipan Island: Magicienne Bay, landing	15 08 30	145 43 55				
	Tanapag Hbr., Garapag	15 17 10	145 42 50	7 00	0 50	2.0	1.1
	Anataxan Island: Center	16 20 00	145 39 00				
	Sariguan Island: Center	16 41 00	145 47 00				
	Guguan Island: Center	17 17 00	145 57 00				
	Alamaguan Island: Center	17 36 00	145 55 00				
	Pagan Island: SW. pt	18 04 00	145 52 00				
	Agrigan Island: SE. pt	18 46 20	145 41 45				
	Asuncion Island: Crater, 2,600 ft	19 45 00	145 30 00				
	Urracas Islands: Largest islet	20 00 00	145 21 00				
	Farralon de Pajaros: S. end	20 32 54	144 54 00				

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE PACIFIC—Continued.

Coast.	Place.	Lat. N.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	*h. m.*	*h. m.*	*ft.*	*ft.*
	Wake Island: Obs. spot	19 15 00	166 31 30				
	Gaspar Rico Reef: N. clump of rocks	14 41 00	168 54 28				
			Long. W.				
	Johnston or Cornwallis Islands: Flag-staff on W. island	16 44 48	169 32 24				
	Clipperton Island: Center	10 17 00	109 13 00				
Hawaiian Islands.	Hawaii Island: Hilo, Kanaha Pt. light	19 46 14	155 05 31	3 09	9 06	2.3	1.3
	Kawaihae light	20 03 00	155 48 00				
	Kealakeakua Bay light	19 28 00	155 55 00	2 20	8 10	1.6	0.9
	Kailua, stone church	19 38 26	156 00 15				
	Kahoolawe Island: Summit	20 33 39	156 35 04				
	Maui Island: Kanahena Pt. light	20 36 00	156 26 00				
	Lahaina light	20 52 00	156 35 00	3 32	9 58	2.2	1.2
	Molokai Island: Light-house	21 06 17	157 18 32	2 38	8 56	2.1	1.1
	Oahu Island: E. pt. Makapuu station	21 18 16	157 39 07				
	Diamond Head	21 15 08	157 48 44				
	Honolulu, Tr. of V. Obs	21 17 57	157 51 34				
	Honolulu, Reef light	21 17 55	157 51 54	3 46	9 59	1.5	0.8
	Kauai Island: Hanalei, Black Head	22 12 51	159 30 47				
	Waimea, stone church	21 57 17	159 40 08	4 00	10 20	2.0	1.1
	Bird Island: Center	23 05 50	161 58 17				
	Necker Island: Center	23 35 18	164 40 47				
	French Frigate Shoal: Islet (120 ft.)	23 46 00	166 17 57				
	Gardiner Island: Center	25 00 40	168 00 52				
	Maro Reef: NW. pt	25 31 00	170 39 20				
	Laysan Island: Light-house	25 48 00	171 44 00				
	Lisiansky Island: Light-house	26 00 00	173 57 00				
	Pearl and Hermes Reef: NE. extreme	27 56 30	175 46 00				
	Midway Islands: N. end Sand Islet	28 13 15	177 21 30	3 30	9 45	1.1	0.6
	Ocean Island: Sand Islet	28 24 45	178 27 45				
			Long. E.				
	Marcus Island: Center	24 14 00	154 00 00				
	Bonin Is., Parrys Group: N. rock	27 45 00	142 06 53				
	Kater Island: N. rock	27 31 00	142 11 53				
	Peel Island: Port Lloyd, observatory	27 05 37	142 11 23	6 10	0 00	2.4	1.4
	Volcano Is., San Alessandro or North Island: Center	25 14 00	141 11 00				
	Sulphur Island	24 48 00	141 13 00				
	San Augustine Island: Center	24 14 00	141 20 00				
	Rosario Island: Center, 148 ft	27 15 32	140 50 28				
	Douglass Rocks: Center	20 30 00	136 10 00				
	Borodino Islands: Center of N. island	25 59 38	131 19 30				
	Center of S. island	25 52 45	131 12 17				
	Rasa Island: Center	24 27 00	131 01 50				
		Lat. S.	Long. W.				
Marquesas Islands.	Fatu Hiva Island: S. pt	10 32 00	138 39 20				
	Motane Island: SSE. pt	10 01 40	138 48 30				
	Tahuata Island: Port Resolution, watering place	9 56 00	139 09 00	2 30	8 45	3.1	1.9
	Hiva-Oa Island: C. Balguerie	9 45 00	138 47 40				
	Fatu Huku Island: Center	9 27 30	138 55 10				
	Roa Poua Island: Obelisk Islet	9 29 30	140 04 45				
	Nuka-Hiva Island: Port Tai-o-hae light	8 55 13	140 04 00	3 50	10 05	3.5	2.1
	Hiaou Island: S. pt	8 03 30	140 44 00				
	Motu-ili Island: Summit, 130 ft	8 44 00	140 38 30				
	Ua-Huka or Ua-Una Island: N. pt	8 54 00	139 33 30				
	Fetouhouhou Island: NE. pt	7 55 00	140 34 40				
	Caroline Islands: Solar Eclipse Transit Pier	10 00 01	150 14 30	4 00	10 14	1.1	0.7
	Vostok Island: Center	10 06 00	152 23 00				
	Flint Island: S. extremity	11 25 23	151 48 34				

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE PACIFIC—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Malden Island: Flagstaff, W. side	4 03 00	155 01 00				
	Starbuck Island: Flagstaff, W. side	5 37 00	155 56 00				
	Penrhyn or Tongarewa Island: NNW. pt.	8 55 15	158 07 00	6 00	12 15	1.5	0.9
	Jarvis Island: Center	0 22 33	159 54 11				
	Reirson Island: Church	10 02 00	161 05 30				
	Humphrey Island: N. pt	10 20 30	161 01 12				
	Union or Tokelau Islands: Spot N. of Fakaofu or Bowditch Islet	9 23 02	171 14 46	6 00	12 13	2.4	1.4
	Union or Tokelau Islands: Nuku-nono, or SE. island, Duke of Clarence I	9 13 06	171 44 40				
	Union or Tokelau Islands: Clump on S. island, Oatafu or Duke of York I	8 39 40	172 28 10				
Phœnix Is.	Canton or Mary Island: N. pt	2 44 25	171 45 29				
Phœnix Is.	Enderbury Island: W. pt	3 08 30	171 10 00	5 00	11 15	4.6	2.7
Phœnix Is.	Phœnix Island, N. pt	3 42 28	170 42 37				
Phœnix Is.	Birneys Island: S. pt	3 34 15	171 32 07				
Phœnix Is.	Gardners Island: Center	4 37 42	174 40 18				
Phœnix Is.	McKean Island: Center	3 35 10	174 17 26				
Phœnix Is.	Hulls Island: W. pt	4 30 95	172 13 28				
			Long. E.				
Ellice Islands.	Mukulaelae or Mitchells Island: S. pt	9 18 00	179 50 00				
Ellice Islands.	Funafuti or Ellice Island: E. pt	8 25 19	179 07 25				
Ellice Islands.	Nukufetau or De Peysters Island: S. pt	8 04 02	178 28 51				
Ellice Islands.	Vaitupu Island: S. end	7 32 00	178 41 01				
Ellice Islands.	Nui or Netherland Island: S. pt	7 15 45	177 16 50				
Ellice Islands.	Nauomaga Island: Center	6 12 00	176 16 30				
Ellice Islands.	Niutao Island: Church	6 06 00	177 20 01				
Ellice Islands.	Nanomea Island: Center	5 39 00	176 06 15				
	Ocean or Paanopa Island: Center (appx)	0 52 00	169 35 00				
	Pleasant Island: Center	0 25 00	167 05 00				
	Indispensable Reefs: S. pt. of S. reef	12 50 15	160 26 00				
	Rennel Island: SE. extreme	11 52 15	160 40 15				
	W. end	11 33 45	159 55 00				
Solomon Islands.	San Christoval Island: Point Wangalaha	10 17 32	161 33 30	6 45	0 33	3.3	2.0
Solomon Islands.	Guadalcanar Island: Wanderer Bay, mouth of Boyd Creek	9 41 47	159 39 30				
Solomon Islands.	Florida Island: Mboli Harbor, Tree Islet.	9 01 30	160 27 20				
Solomon Islands.	Malaita Island: Village, Mary I., Port Adam	9 30 00	161 27 40				
Solomon Islands.	Stewart Islands: Largest islet	8 23 00	162 58 15				
Solomon Islands.	Isabel Island: N. side of Cockatoo Islet.	8 30 50	159 38 20	5 00	11 15	3.5	2.1
Solomon Islands.	Gizo or Shark Island: N. point village	8 05 40	156 50 15				
Solomon Islands.	Choiseul Island: Choiseul Bay entrance	6 42 40	156 23 16				
Solomon Islands.	Treasury Islands: Observation Islet	7 24 30	155 34 00				
Solomon Islands.	Bougainville Island: Hiisker Pt., Gazelle Harbor	6 35 00	155 05 00	12 00	5 47	2.7	1.6
Solomon Islands.	Buka Island: Cape North	5 00 00	154 35 00				
Solomon Islands.	Lord Howe Group: Center, small SW. islet	5 38 00	159 21 00				
Solomon Islands.	Center, small NE. islet	5 18 00	159 34 00				
Solomon Islands.	NW. pt. of Hammond I	5 18 00	159 17 00				
	New Britain, Blanche Bay: Matupi I. N. pt	4 14 12	152 11 35	9 00	2 45	2.1	1.3
	Duke of York Island: Makada Harbor, Spit Pt	4 06 25	152 06 15				

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE PACIFIC—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	*h. m.*	*h. m.*	*ft.*	*ft.*
	New Ireland: Carteret Harbor, Cocoanut I	4 41 26	152 42 25	....	....	......	......
	Katharine Haven	3 11 00	151 35 30	....	....	......	......
	Holz Haven, E. side	2 47 30	150 57 35	2 50	9 03	2.4	1.4
	New Hanover Island: Water Haven, creek mouth	2 33 43	150 04 33	....	....	......	......
	North Haven anchorage	2 26 30	149 55 36	2 30	8 43	2.4	1.4
	St. Matthias Island: SW. extreme	1 35 00	149 37 00	....	....	......	......
Admiralty Is.	Admiralty Island: Nares Harbor, obs. islet	1 55 10	146 40 56	....	....	......	......
	St. Andrew Island: Violet Islet, 60 ft	2 25 40	147 28 35	....	....	......	......
	Jesus Maria Island: SE. pt	2 22 00	147 55 00	....	....	......	......
	Commerson Island: Center of largest islet	0 45 00	145 17 00	....	....	......	......
	Anchorite Island: N. pt	0 53 15	145 33 04	....	....	......	......
	Hermit or Loaf Island: Pemé Islet	1 28 00	145 08 00	....	....	......	......
	Purdy Island: Mole Islet	2 51 00	146 15 00	....	....	......	......
New Guinea Island.	Point d'Urville: extreme	1 25 40	135 28 12	....	....	......	......
	Drei Cap Peninsula: Wass Islet	2 44 00	132 04 00	....	....	......	......
	Triton Bay: Fort Dubus, Dubus Haven	3 47 00	134 06 00	0 55	7 08	7.3	4.3
	Cape Walsche: Extreme	8 22 00	137 40 00	....	....	......	......
	Fly River: Free Islet, S. pt	8 41 00	143 36 04	....	....	......	......
	Port Moresby: N. end of Jane I	9 25 30	147 07 04	8 50	2 38	8.0	4.8
	Cape Rodney: Extreme	10 14 30	148 30 30	....	....	......	......
	South Cape: S. pt. Su Au I	10 43 35	150 14 20	9 15	3 00	8.1	4.8
	Hayter Island: W. end	10 37 00	150 40 34	8 25	2 12	5.8	3.4
	Cape Cretin: Cretin Islets	6 43 00	147 53 20	....	....	......	......
Louisiade Arch.	Trobriand Islands: NE. pt. Cape Denis	8 24 00	151 01 24	4 45	10 58	3.0	1.8
	Woodlark Islands: N. pt	9 03 30	152 47 00	7 05	0 53	4.2	2.5
	D'Entrecasteaux Is.: Ferguson I., SW. extreme	9 38 00	150 30 00	....	....	......	......
	Well Island, E. pt.	9 41 00	150 58 00	....	....	......	......
	Normanby I., obs. islet	9 43 53	150 44 43	....	....	......	......
	St. Aignan Island: Summit	10 42 00	152 42 04	....	....	......	......
	Renard Islands: W. pt	10 52 40	152 47 12	....	....	......	......
	Rossel Island: E. pt	11 23 25	154 08 00	....	....	......	......
	Adèle Island: S. extreme	11 29 10	154 25 14	....	....	......	......
Coral Sea Arch.	Coringa Islands: Chilcott Islet	16 50 00	149 58 00	....	....	......	......
	Herald Cays: NE. Cay	16 55 50	149 11 54	....	....	......	......
	Tregosse Islands; S. islet	17 43 00	150 42 04	....	....	......	......
	Lhou Reef: Observation Cay	17 07 20	152 06 20	....	....	......	......
	Mellish Reef: Cay beacon	17 24 39	155 52 24	....	....	......	......
	Bampton Island	19 08 00	158 40 00	....	....	......	......
	Renard Island: Center	19 14 00	159 00 00	....	....	......	......
	Wreck Reef: Bird Islet	22 10 30	155 28 24	....	....	......	......
	Cato Island: Center	23 15 02	155 33 04	....	....	......	......
Santa Cruz Is.	Duff or Wilson Group: N. island	9 48 00	166 53 15	....	....	......	......
	Matema or Swallow Group: Nimanu Islet	10 21 00	166 17 15	....	....	......	......
	Tinakula Island: Summit, 2,200 ft	10 23 30	165 47 30	....	....	......	......
	Nitendi Island: NE. pt., Cape Byron	10 40 00	166 00 30	....	....	......	......
	Tapua Island: Basilisk Harbor, S. pt. of entrance	11 17 30	166 32 14	....	....	......	......
	Vanikoro: Ocili village	11 40 24	166 57 45	4 50	11 05	3.8	2.3

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE PACIFIC—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
New Hebrides Islands.	Torres or Ababa Island: Hayter Bay, Middle I	13 15 00	166 33 00	....	....	......	......
	Vanua Lava Island: Port Patterson, Nusa Pt	13 48 00	167 30 31	6 40	0 30	3.8	2.3
	Santa Maria Island: Lasolara Anchorage	14 11 00	167 30 00	....	....	......	......
	Aurora Island: Laka-rere	14 58 00	168 02 00	....	....	......	......
	Mallicollo Island: Port Sandwich, pt. on E. side	16 26 00	167 47 15	4 38	10 50	3.8	1.9
	Vaté or Sandwich Island: Havannah Harbor, Matapou Bay flagstaff	17 44 58	168 18 50	5 15	11 27	3.0	1.8
	Erromango Island: Dillon Bay, Pt. Williams	18 47 30	168 58 00	....	....	......	......
	Tanna Island: Port Resolution, Mission	19 31 17	169 27 30	....	....	......	......
	Erronan or Futuna Island: NW. pt	19 31 20	170 11 15	....	....	......	......
	Aneityum Island: Port Anatom, Sand Islet	20 15 17	169 44 45	5 10	11 23	3.1	1.9
	Matthew Island: Peak, 465 feet	22 20 12	171 20 30	....	....	......	......
	Hunter Island: Peak, 974 feet	22 24 02	172 05 15	....	....	......	......
	Walpole Island: S. pt	22 38 07	168 56 45	....	....	......	......
	Mitre Island: Center	11 55 00	170 10 00	....	....	......	......
	Rotumah Island: Epipigi Peak	12 30 10	177 07 15	6 15	0 00	4.2	2.5
Fiji Islands.	Kandavu Island: N. rock Astrolabe Reef light	18 38 15	178 32 15	....	....	......	......
	Mt. Washington, N. peak	19 07 09	177 57 09	....	....	......	......
	N'galoa Harbor, outer beacon	19 05 30	178 10 24	6 40	0 25	4.0	2.4
	Vatu Lele Island: S. pt	18 36 00	177 38 00	....	....	......	......
	Ovalau Island: Levuka light-house	17 40 45	178 49 00	....	....	......	......
	Viti Levu Island: Summit of Malolo Islet	17 44 45	177 09 00	....	....	......	......
	Suva Harbor, low light	18 06 50	178 24 40	6 30	0 15	3.6	2.2
	Mbega or Mbengha Island: Swan Harbor, Leaven Pt	18 22 00	178 06 53	....	....	......	......
	Matuku Island: N. side of Matuku entrance	19 09 38	179 44 27	....	....	......	......
	Moala Island: Rocks off N. pt	18 32 49	179 56 25	....	....	......	......
	Ngau Island: Herald Bay, E. side	17 59 32	179 14 08	....	....	......	......
	Wakaya Island: Rocky Peak	17 37 11	178 59 29	....	....	......	......
	Makongai Island: Dilliendreti Peak	17 27 14	178 57 46	....	....	......	......
	Goro Island: NW. pt	17 15 21	179 20 44	....	....	......	......
	Vanua Levu Island: Mount Dana	16 42 01	178 54 15	....	....	......	......
	Nandi, observation islet	16 57 53	178 48 32	....	....	......	......
	Savu Savu Pt.; extreme	16 49 19	179 16 08	6 00	12 13	4.3	2.6
			Long. W.				
	NE. Pt	16 08 00	179 58 46	....	....	......	......
	Taoiuni Island: Somu-Somu town	16 46 00	179 51 00	....	....	......	......
	Thikombia Island: E. hummock	15 44 45	179 54 26	....	....	......	......
	Naitamba Island: Center	17 03 00	179 17 00	....	....	......	......
	Vatu Vara Island: N. end, summit	17 25 33	179 32 17	....	....	......	......
	Kanathea Island: S. pt	17 17 20	179 10 00	....	....	......	......
	Vanua Mbalavu Island: NW. pt	17 10 00	179 05 45	....	....	......	......
	Mango Island: Pier end	17 25 26	179 10 33	6 10	0 00	3.1	1.9
	Thithia Island: Highest peak	17 44 12	179 19 49	....	....	......	......
	Tuvutha Island: Peak	17 39 33	178 50 27	....	....	......	......
	Naian Island: Summit, 580 ft	17 59 00	179 04 00	....	....	......	......
	Lakemba Island: Kendi Pt	18 14 10	178 52 00	....	....	......	......
	Oneata Island: Summit of Loa I	18 25 46	178 27 04	....	....	......	......
	Mothe Island: Summit	18 38 56	178 30 54	....	....	......	......
	Mamuka Island: Center, 260 feet	18 46 00	178 44 00	....	....	......	......

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE PACIFIC—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Fiji Islands.	Kambara Island: Highest peak	18 56 15	178 59 05				
	Totoya Island: Black Rock Bay, W. side	18 58 57	179 52 58	6 35	0 20	3.5	2.1
	Fulanga Island: W. bluff	19 03 00	178 47 25				
	Ongea Levu Island: Center	19 04 00	178 33 25				
	Vatoa or Turtle Island: Hummock	19 49 11	178 13 38	6 10	0 00	3.1	1.9
	Ono Islands: Peak	20 39 10	178 43 27				
	Michaeloff Island: Center	21 00 09	178 44 03				
	Simonoff Island: Center	21 01 39	178 49 47				
	Fatuna or Horne Island: Mt. Schouten	14 14 20	178 06 45				
	Uea or Wallis Island: Fenua-fu Islet	13 23 35	176 11 47	6 40	0 28	4.4	2.7
	Niua-fu or Good Hope Island: NW. extreme	15 34 00	175 40 40				
	Keppel Island: Center	15 52 00	173 52 00				
	Boscawen Island: Center	15 58 00	173 52 00				
Samoan Is.	Savaii Island: Paluale village	13 45 00	172 17 00				
	Upulo Is.: Apia Harbor, obs. spot	13 48 56	171 44 56	6 25	0 13	3.1	1.9
	Tutuila Island: Pago-Pago, obs. pt	14 18 06	170 42 14	7 00	0 45	2.7	1.6
	Manua Island: Village, NW. side	14 19 00	169 32 00	6 00	12 13	4.6	2.7
	Rose Island: Center	14 32 00	168 09 00				
	Niue or Savage Island: S. pt	19 10 00	169 50 00				
	Danger, or Bernardo, Is.: Middle rock	10 52 47	165 51 30				
	Suwarrow or Souwaroff Island: Cocoanut Islet	13 14 30	163 04 10	3 10	9 23	2.4	1.4
	Palmerston Islands: W. islet	18 05 50	163 10 00				
	Scilly Islands: E. islet	16 28 00	154 30 00				
	Bellingshausen Island: Center	15 48 00	154 31 00				
	Mopelia (Lord Howe) Island: Center	16 52 00	154 00 00				
Society Islands.	Maitea Island: Summit	17 53 00	148 05 00				
	Tahiti Island: Light-house	17 29 10	149 29 00	12 00	5 48	1.0	0.6
	Tubuai-Manu or Maia-iti I.: NW. pass	17 36 39	150 36 56				
	Eimeo Island: Talu Hbr., Vincennes Pt.	17 29 23	149 50 30				
	Huaheine Island: Light-house	16 42 30	151 01 28				
	Ulietea Island: Regent Pt	16 50 00	151 27 21				
	Tahoa Island: Center	16 35 00	151 35 00				
	Bola-Bola Island: Otea-Vanua village	16 31 35	151 46 00	12 10	6 00	1.4	0.8
	Tubai or Motu-iti Island: N. pt. of reef	16 11 00	151 48 00				
	Marua or Maupili Island: Center	16 26 00	152 12 00				
Tuamotu Archipelago.	Ducie Island: NE. entrance	24 40 20	124 48 00				
	Pitcairn Island: Village	25 03 50	130 08 30				
	Henderson or Elizabeth Island: Center	24 21 20	128 19 00				
	Oeno Island: N. pt	24 01 20	130 41 00				
	Mangareva or Gambier Island: Flagstaff	23 07 36	134 57 54	1 50	8 03	2.4	1.4
	Marutea or Lord Hood Island: Center	21 31 30	135 33 05				
	Maria or Moerenhout Island: Center	22 01 00	136 10 15				
	Vahanga Island: W. pt	21 20 00	136 38 53				
	Morane or Cadmus Island: Center	23 07 50	137 06 15				
	Tureia or Carysfort Island: E. pt	20 46 20	138 27 45				
	Mururoa or Osnabrug Island: Obs. spot	21 50 00	138 56 30				
	Tematangi or Bligh Island: N. pt	21 38 00	140 38 45				
	Nukutipipi: SW. pt	20 43 00	143 03 15				
	Hereheretue or St. Paul Island: Center	19 53 17	144 57 00				
	Vanavana or Barrow Island: Center	20 46 07	139 08 45				
	Nukutavake or Queen Charlotte I.: N. pt	19 16 30	138 48 30				
	Reao or Clermont Tonnere Island: NW. point	18 29 00	136 26 30				
	Puka-ruha or Serles Island: NW. pt	18 16 00	137 03 30				
	Vahitahi Island: W. pt	18 43 30	138 53 15				
	Ahunui or Byam Martin Island: NW. pt	19 37 00	140 15 45				
	Pinaki or Whitsunday Island: E. pt	19 25 00	138 40 45				
	Tatakoto or Clerke Island: Flagstaff on western coast	17 19 30	138 26 26				

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE PACIFIC—Continued.

Coast.	Place.	Lat. S.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Tuamotu Archipelago.	Hao or La Harpe Island: NW. pass	18 05 20	140 59 30	2 40	8 55	2.4	1.4
	Paraoa or Glocester Island: Center	19 08 45	141 41 10	......	......	......	......
	Ravahere Island: S. pt	18 18 30	142 11 31	......	......	......	......
	Reitoru or Bird Island: N. beach	17 49 35	143 05 23	......	......	......	......
	Hikueru or Melville Island, E. pt	17 35 28	142 35 16	......	......	......	......
	Tauere Island: NW. pt	17 20 30	141 29 43	......	......	......	......
	Puka-puka Island: E. pt	14 49 00	138 46 45	......	......	......	......
	Napuka Island: W. pt	14 12 00	141 15 37	......	......	......	......
	Angatau or Araktcheff Island: W. pt	15 50 00	140 53 35	......	......	......	......
	Tukume or Wolkonsky Island: NW. pt.	15 44 20	142 08 40	......	......	......	......
	Tuanske Island: NW. pt	16 39 10	144 14 45	......	......	......	......
	Nihiru Island (Tuanake): SW. pt	16 44 29	142 53 34	......	......	......	......
	Anaa Island: Islet in N. pass	17 20 20	145 30 54	......	......	......	......
	Tepoto Island: N. pt	16 47 49	144 17 18	......	......	......	......
	Haraiki or Crocker Island: SW. pt	17 28 41	143 31 17	......	......	......	......
	Makemo or Phillips Island: W. pass	16 26 09	143 57 59	......	......	......	......
	Fakarana or Wittgenstein Island: SE. pass	16 31 00	145 22 45	......	......	......	......
	Taiaro or Kings I.: Middle of W. shore.	15 43 15	144 38 34	......	......	......	......
	Aratika Island: E. pt	15 30 00	145 24 45	......	......	......	......
	Toau or Elizabeth Island: Amyot Bay.	15 50 00	146 02 45	......	......	......	......
	Takapoto Island: S. pt	14 43 00	145 11 00	......	......	......	......
	Aheu Island: Lagoon Entrance	14 29 10	146 20 00	......	......	......	......
	Rangiroa Island: E. pt	15 14 30	147 11 00	4 30	10 43	2.1	1.3
	Makatea Island: W. pt	15 50 30	148 15 00	......	......	......	......
	Matahiva Island: W. pt	14 53 00	148 39 45	......	......	......	......
	Juan Fernandez Island: Fort S. Juan Batista	33 37 36	78 50 02	......	......	......	......
	Mas-afuera Island: Summit, 4,000 ft	33 46 00	80 46 00	......	......	......	......
	St. Ambrose Island: N. part creek	26 18 07	79 54 56	......	......	......	......
	St. Felix Island: Center	26 16 00	80 06 56	......	......	......	......
	Sala y Gomez: NW. pt	26 27 41	105 28 00	4 00	10 15	3.3	2.0
	Easter Island: Cooks Bay, mission	27 10 00	109 26 00	0 40	6 53	2.8	1.7
	Rapa or Oparo Island: Tauna Islet	27 35 46	144 17 20	0 10	6 25	2.4	1.4
	Bass Islets (Morotiri): SE. islet, 344 ft.	27 55 30	143 28 21	......	......	......	......
	Tubuai or Austral Is., Vavitoa I.: Center.	23 55 00	147 48 00	......	......	......	......
	Tubuai I.: Flag staff, N. side	23 21 45	149 35 35	3 00	9 13	2.4	1.4
	Rurutu I.: N. pt	22 29 00	151 23 41	......	......	......	......
	Rimitara I.: Center	22 45 00	152 55 00	......	......	......	......
Cook Islands.	Hull Island: NW. pt	21 47 00	154 51 00	......	......	......	......
	Mangaia Island: Center	21 49 00	157 56 00	......	......	......	......
	Rarotonga Island: NW. pt	21 11 35	159 47 00	6 00	12 15	2.7	1.7
	Mauki or Parry Island: Center	20 17 00	157 23 00	......	......	......	......
	Mitiero Island: Center	20 01 00	157 34 00	......	......	......	......
	Vatiu or Atiu Island: Center	20 04 00	158 08 00	......	......	......	......
	Hervey Islets: Center	19 18 00	158 54 00	......	......	......	......
	Aitutaki Island: Center	18 54 00	159 32 00	......	......	......	......
Tonga Is.	Vavau Island: Port Valdes, Sandy Pt	18 39 02	174 01 00	6 20	0 10	3.8	2.3
	Kao Island: Summit, 5,000 ft	19 41 35	174 59 50	......	......	......	......
	Tofua Island: Summit, 2,800 ft	19 45 00	175 03 00	......	......	......	......
	Tongatabu Island: Light-house	21 08 00	175 12 00	6 20	0 10	3.8	2.3
	Minerva Reefs, N. Minerva: NE. side	23 37 06	178 55 45	7 50	1 35	5.5	3.3
	S. Minerva: S. side of entrance	23 55 00	179 07 45	......	......	......	......
	Kermadec Is., Raoul or Sunday I.: Denham B. flag staff	29 15 30	177 55 40	6 00	12 13	3.3	2.7
	Macauley I.: Center	30 15 00	178 31 45	......	......	......	......
	Curtis I.: Center	30 35 00	178 37 00	......	......	......	......
	Conway Reef: Center	21 44 45	Long. E. 174 37 45	......	......	......	......

MARITIME POSITIONS AND TIDAL DATA.

ISLANDS OF THE PACIFIC—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int.		Range.	
				H. W.	L. W.	Spg.	Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Loyalty Is., Uvea or Halgan I.: Uvea Church	20 27 06	166 35 25				
	Lifu I.: Wreck Bay, NW. shore	20 46 00	167 02 30	6 30	0 18	4.2	2.5
	Mare or Britannia I.: S. pt.	21 42 00	168 00 00				
New Caledonia.	Port Kanala: Observatory	21 29 12	165 58 50				
	Port St. Vincent: Marceau I.	22 00 10	166 05 00	5 40	11 52	3.3	2.0
	Noumea: Light-house	22 16 22	166 25 52	8 25	2 13	3.1	1.9
	Balari Pass: Amedée I. light	22 28 44	166 28 51				
	Port Alcmene: Alcmene I.	22 42 30	167 27 55	7 55	1 45	3.6	2.2
	Norfolk Island: Inner end of jetty	29 03 45	167 58 06	7 30	1 17	4.7	3.9
	Elizabeth Reef: Center	29 56 00	159 04 30				
	Lord Howe Island: S. end of middle beach	31 31 38	159 05 58	8 20	2 08	5.4	3.3
	Balls Pyramid: Summit, 1,816 ft.	31 45 10	159 16 10				
	Macquarie Island: N. pt.	54 19 00	158 56 00				
	Auckland Is.: Port Ross, Terror Cove	50 32 15	166 13 20	11 50	5 38	3.2	2.6
	Campbell Island: S. harbor, Shoal Pt.	52 33 26	169 08 41	11 45	5 33	3.5	2.9
	Antipodes Island: Summit, 600 ft.	49 42 00	178 43 05	3 20	9 30	5.3	4.3
	Bounty Islands: Anchorage N. I., West Group	47 43 00	179 00 27				
			Long. W.				
	Chatham Island, Whare-Kauri Island: Port Waitangi, Pt. Hanson	43 57 24	176 32 15				
	Chatham Island, Whare-Kauri Island: Port Hutt, Gordon Pt	43 49 03	176 42 00	5 22	0 23	2.5	2.1

AUSTRALIA.

Coast.	Place.	Lat. S.	Long. E.	H. W.	L. W.	Spg.	Neap.
North Australia.	Groate Eylandt: SE. pt	14 16 00	136 58 00				
	Bickerton Island: Summit	13 45 00	136 15 00				
	Cape Arnheim: Extreme	12 14 00	137 00 00				
	Cape Wilberforce: E. extreme	11 53 00	136 34 00	8 00	1 48	9.8	5.8
	Cape Wessel: Extreme	10 59 00	136 46 00				
	Dale Point: Extreme	11 36 00	136 07 00				
	Cape Stewart: Extreme	11 57 00	134 45 00				
	Liverpool River: W. pt. entrance	11 54 00	134 12 00	6 17	0 05	12.0	7.1
	Cape Croker: Extreme	10 57 00	132 36 30				
	Port Essington: Government house	11 22 02	132 09 18				
	Melville Island: Cape Van Diemen	11 08 00	130 19 00				
	Bathurst Island: Cape Fourcróy	11 51 00	129 58 00				
	Adelaide River: E. entrance pt	12 13 20	131 16 30	5 15	11 27	16.8	9.9
	Port Darwin: Charles Pt. light	12 23 20	130 37 00	4 57	11 18	17.0	10.0
	Port Patterson: Quail Islet	12 30 58	130 27 00	3 50	10 00	16.7	9.9
	Port Keats: Tree Pt.	13 59 00	129 37 00	5 45	11 58	21.9	12.9
	Pearce Point: Extreme	14 25 50	129 20 42	6 45	0 27	23.0	13.6
	Victoria River: Water Valley	15 13 45	129 48 14				
Western Australia.	Cape Dussejour: Rock off cape	14 42 00	128 10 00				
	Cape Londonderry: Extreme	13 44 00	126 57 00				
	Cape Bougainville: Extreme	13 52 00	126 12 00				
	Cassini Island: S. pt	13 57 07	125 38 45				
	Cape Voltaire: Flat Hill	14 15 00	125 39 00				
	Barker Islets: Center	13 55 00	124 55 00				
	Montalivet Islands: W. islet	14 14 00	125 12 00				
	Maret Islets: N. islet	14 23 00	125 00 00				
	Colbert Islet: Center	14 51 00	124 42 00				
	Prince Regent River: Mount Trafalgar	15 16 36	125 07 00				
	Port Nelson: Careening beach	15 06 00	125 01 00				
	De Freycinet Islets: Beacon on summit.	14 59 20	124 32 11				
	Red Islet: Center	15 13 15	124 14 00				
	Cockell Islet: W. pt	15 46 00	124 04 00				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

AUSTRALIA—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Western Australia.	MacLeay Islets: Rock off N. end	15 52 00	123 45 00	......	......	......	......
	Port Usborne: S. pt	15 39 25	123 36 27	......	......	......	......
	Fitz Roy River: Escape Pt	17 24 25	123 39 47	......	......	......	......
	Cape L'Evêque: Extreme	16 23 00	122 55 45	......	......	......	......
	Lacepede Island: NW. islet	16 50 00	122 05 30	......	......	......	......
	Cape Baskerville: Extreme	17 09 00	122 15 00	......	......	......	......
	Cape Latouche Tréville: Extreme	18 29 00	121 54 00	......	......	......	......
	Turtle Isles: Center of N. isle	19 54 00	118 48 00	......	......	......	......
	Cape Lambert: Extreme	20 36 00	117 11 00	11 30	5 10	17.6	10.4
	Legendre Island: NW. extreme	20 19 00	116 45 00	......	......	......	......
	Rosemary Island: W. summit	20 27 00	116 30 00	......	......	......	......
	Enderby Island: Rocky Head	20 35 00	116 23 00	......	......	......	......
	Montebello Island: N. extreme of reef	20 16 45	115 22 00	......	......	......	......
	Barrow Island: N. pt	20 40 40	115 27 45	......	......	......	......
	Northwest Cape: Extreme	21 46 41	114 10 08	......	......	......	......
	Cape Cuvier: Extreme	24 00 00	113 21 00	......	......	......	......
	Cape Inscription: Extreme	25 29 19	112 57 09	......	......	......	......
	Houtman Rocks: N. islet	28 18 05	113 35 33	......	......	......	......
	Port Gregory	28 12 00	114 14 30	......	......	......	......
	Cape Leschenault: Extreme	31 18 00	115 30 00	......	......	......	......
	Rottnest Island: Light-house	32 00 20	115 30 12	......	......	......	......
	Perth (Fremantle): Arthur Head light	32 03 12	115 44 23	[10 16]	[3 43]	[2.1]	......
	Peel: Robert Pt	32 27 00	115 44 00	......	......	......	......
	Cape Naturaliste: Extreme	33 31 45	115 00 15	......	......	......	......
	Cape Leeuwin: Light-house	34 21 55	115 08 00	......	......	......	......
	D'Entrecasteaux Point: Extreme	34 52 00	116 01 00	......	......	......	......
	Nuyts Point: Extreme	35 05 00	116 38 00	......	......	......	......
	West Cape Howe: Extreme	35 09 00	117 40 00	......	......	......	......
	Eclipse Islets: Summit of largest	35 11 54	117 53 45	......	......	......	......
	King George Sound: Commissariat house near Albany jetty	35 02 20	117 54 04	[10 53]	[4 40]	[2.6]	......
	Bald Isle: Center	34 55 00	118 27 00	......	......	......	......
	Hood Point: Doubtful Isles	34 24 00	119 34 00	......	......	......	......
	Recherche Archipelago: Termination Isle	34 30 00	121 58 00	......	......	......	......
	Culver Point: Extreme	32 57 00	124 39 00	......	......	......	......
	Dover Point: Extreme	32 34 00	125 30 00	......	......	......	......
South Australia.	Fowler Point: Extreme	32 01 30	132 33 00	11 50	9 35	5.1	0.3
	Streaker Bay: Port Blanche	32 48 00	134 13 40	......	......	......	......
	Coffin Bay: Mount Dutton	34 29 29	135 24 56	0 35	6 55	5.5	0.3
	Cape Catastrophe: W. pt	35 00 15	135 56 09	......	......	......	......
	Neptune Isles: SE. islet	35 20 15	136 06 24	......	......	......	......
	Port Lincoln: English Church	34 43 22	135 51 03	......	......	......	......
	Franklin Harbor: Observation spot	33 44 08	136 57 22	......	......	......	......
	Port Augusta: Flagstaff	32 29 42	137 45 24	8 20	2 15	11.4	0.7
	Port Victoria: Wardang Island hut	34 28 25	137 22 21	......	......	......	......
	Cape Spencer: S. pt	35 18 21	136 53 30	......	......	......	......
	Investigator Strait: Troubridge light	35 07 31	137 49 39	......	......	......	......
	Port Wakefield: Light-house	34 12 00	138 09 00	4 31	10 45	10.2	0.6
	Port Adelaide: Wonga Shoal light	34 50 25	138 26 58	4 04	10 22	6.3	0.9
	Cape Jervis: Light-house	35 36 45	138 05 29	......	......	......	......
	Cape Borda: Light-house	35 45 30	136 34 39	......	......	......	......
	Cape Willoughby: Light-house	35 51 00	138 07 45	4 00	10 15	5.8	0.3
	Port Victor: Flagstaff	35 34 06	138 37 09	......	......	......	......
	Cape Jaffa: Margaret Brock light-house	36 57 00	139 39 39	......	......	......	......
	Cape Northumberland: Light-house	38 04 18	140 39 40	11 52	5 40	4.2	0.2
Victoria.	Cape Nelson: S. extreme	38 26 00	141 32 39	......	......	......	......
	Portland Bay: Lawrence Rock	38 24 39	141 40 02	0 20	6 35	2.7	2.1
	Port Fairy: Griffith Island summit	38 23 47	142 14 37	......	......	......	......
	Cape Otway: Light-house	38 51 45	143 30 39	......	......	......	......
	King Island: Cape Wickham light	39 35 38	143 57 03	......	......	......	......
	Port Phillip: Point Lonsdale light	38 18 00	144 37 00	10 43	4 30	2.5	1.9
	Geelong: Custom-house	38 08 52	144 21 47	2 02	8 20	3.0	2.3
	Melbourne: Observatory	37 49 53	144 58 35	2 19	8 41	1.9	1.5

MARITIME POSITIONS AND TIDAL DATA.

AUSTRALIA—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H.W.	Lun. Int. L.W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Victoria.	Cape Schanck: Light-house	38 29 42	144 52 51	-------	-------	-----	-----
	Port Western: Extreme of W. head	38 29 15	145 01 34	-------	-------	-----	-----
	Wilson Promontory: Light, SE. pt	39 08 00	146 25 16	-------	-------	-----	-----
	Kent Island: Deal Island light	39 29 45	147 18 39	-------	-------	-----	-----
	Flinders Is.: Strzelecki Peaks, SE. peak	40 11 45	148 04 00	-------	-------	-----	-----
	Goose Island: Light on S. end	40 18 40	147 47 39	10 38	4 25	8.1	6.2
	Banks Strait: Swan Island light	40 43 40	148 07 24	-------	-------	-----	-----
	Port Albert: Light-house	38 45 06	146 37 43	-------	-------	-----	-----
	Gabo Island: Light-house	37 34 15	149 55 10	8 40	2 27	4.5	3.4
	Cape Howe (east): Extreme	37 30 10	149 58 39	-------	-------	-----	-----
New South Wales.	Cape Green: SE. pt	37 15 40	150 03 04	-------	-------	-----	-----
	Twofold Bay: Lookout Pt. light	37 04 18	149 54 45	8 05	1 52	5.2	3.1
	Dromedary Mountain: Summit	36 18 30	150 01 34	-------	-------	-----	-----
	Montagu Island: Light-house	36 14 30	150 13 34	8 20	2 07	5.3	3.2
	Bateman Bay: Observation head	35 43 58	150 12 34	-------	-------	-----	-----
	Ulladulla: Inner end of pier	35 21 41	150 29 29	8 20	2 07	5.4	3.3
	Jervis Bay: Light-house	35 09 15	150 46 26	-------	-------	-----	-----
	Kiama Harbor: Outer extreme of S. head	34 40 25	150 52 19	-------	-------	-----	-----
	Wollongong: Summit of head	34 25 30	150 55 14	-------	-------	-----	-----
	Sydney: Observatory	33 51 41	151 12 23	8 40	2 27	4.2	2.5
	Port Jackson: Outer S. head light	33 51 30	151 18 15	-------	-------	-----	-----
	Broken Bay: Baranjo Head light	33 35 00	151 20 30	-------	-------	-----	-----
	Newcastle: Nobby Head light	32 55 15	151 48 19	8 35	2 23	4.7	2.8
	Port Stephens: Light-house	32 45 10	152 13 20	8 15	2 00	5.8	3.6
	Sugar Loaf Point: Light-house	32 26 20	152 33 40	-------	-------	-----	-----
	Port Macquarie: Entrance	31 25 30	152 55 19	9 00	2 46	4.1	2.4
	Solitary Islands: S. Isle light	30 12 00	153 17 00	-------	-------	-----	-----
	Clarence River: S. Head light	29 25 30	153 23 10	8 15	2 00	4.0	2.4
Queensland.	Richmond River: N. Head light	28 51 30	153 35 55	-------	-------	-----	-----
	Brisbane: Signal station	27 27 32	153 01 48	10 45	4 30	6.4	3.9
	Lookout Point: Extreme	27 26 20	153 33 50	-------	-------	-----	-----
	Cape Moreton: Light-house	27 02 10	153 28 04	-------	-------	-----	-----
	Double Island Point: Light-house	25 56 00	153 13 00	-------	-------	-----	-----
	Indian Head: Extreme	25 00 15	153 23 00	-------	-------	-----	-----
	Sandy Cape: Light-house	24 43 20	153 13 40	-------	-------	-----	-----
	Burnett River: S. Head light	24 45 00	152 25 00	-------	-------	-----	-----
	Lady Elliot Islet: Light-house	24 07 00	152 45 15	-------	-------	-----	-----
	Bustard Head: Light-house	24 01 20	151 41 04	-------	-------	-----	-----
	Rodd Bay: Spit end	24 01 20	151 37 15	-------	-------	-----	-----
	Port Curtis: Gatcombe Head light	23 53 00	151 23 50	-------	-------	-----	-----
	Cape Capricorn: Light-house	23 29 30	151 14 04	-------	-------	-----	-----
	Port Bowen: Observation rock	22 31 40	150 45 44	-------	-------	-----	-----
	Percy Isles: Pine I. light	21 39 00	150 14 00	-------	-------	-----	-----
	Northumberland Isles: Summit of Prudhoe I	21 19 15	149 43 30	-------	-------	-----	-----
	Cape Palmerston: N. extreme	21 32 00	149 31 04	-------	-------	-----	-----
	Cape Conway: SE. pt	20 32 20	148 58 00	-------	-------	-----	-----
	Port Molle: S. side of entrance	20 18 50	148 53 15	-------	-------	-----	-----
	Cumberland Island: Whitsunday I., summit on W. side	20 15 30	149 00 00	-------	-------	-----	-----
	Port Denison: Obs. pt., W. side of Stone Isle	20 00 50	148 16 54	10 05	3 53	9.0	5.4
	Gloucester Island: Summit near N. end	19 57 30	148 27 34	-------	-------	-----	-----
	Holborne Islet: Center	19 41 50	148 23 00	-------	-------	-----	-----
	Cape Bowling Green: Light-house	19 19 20	147 27 40	-------	-------	-----	-----
	Cape Cleveland: Light-house	19 11 25	147 01 10	-------	-------	-----	-----
	Palm Islands: SE. point of SE. island	18 45 30	146 42 50	-------	-------	-----	-----
	Rockingham Bay: Peak of Goold Isle	18 09 30	146 11 04	-------	-------	-----	-----
	Barnard Island: Light-house	17 40 40	146 11 00	-------	-------	-----	-----
	Frankland Island: High islet	17 09 45	146 02 30	-------	-------	-----	-----
	Cape Tribulation: Extreme	16 04 20	145 29 34	-------	-------	-----	-----
	Hope Island: S. islet	15 45 00	145 28 30	-------	-------	-----	-----
	Cook Mountain: Summit	15 29 45	145 17 30	8 55	2 43	7.5	4.5
	Cape Bedford: SE. extreme	15 16 30	145 23 15	-------	-------	-----	-----

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

AUSTRALIA—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	*h. m.*	*h. m.*	*ft.*	*ft.*
Queensland.	Murdock Point: Extreme	14 37 15	144 57 30	......	......	......	......
	Cape Melville: NE. extreme	14 10 00	144 32 34	......	......	......	......
	Flinders Island: N. extreme of N. island	14 07 45	144 15 19	......	......	......	......
	Claremont Point: Extreme	14 00 30	143 42 15	......	......	......	......
	Cape Sidmouth: Extreme	13 24 45	143 36 19	9 00	2 47	9.6	5.8
	Cape Direction: NE. extreme	12 51 00	143 34 00	......	......	......	......
	Cape Grenville: Extreme	11 58 15	143 15 15	......	......	......	......
	Sir Charles Hardy Island: N. extreme of SE. isle	11 55 00	143 29 00	......	......	......	......
	Bird Island: NW. isle	11 46 30	143 06 00	......	......	......	......
	Hannibal Isles: E. isle	11 36 30	142 56 19	......	......	......	......
	Cape York: Sextant Rock	10 41 30	142 32 24	1 00	7 10	8.0	4.7
	Mount Adolphus: Summit	10 37 45	142 39 20	......	......	......	......
	Travers Isles: Center	10 22 00	142 21 19	......	......	......	......
	Prince of Wales Island: Cape Cornwall, extreme	10 46 00	142 10 50	......	......	......	......
	Booby Island: Center	10 36 05	141 53 49	4 20	10 30	7.8	4.7
	Flinders River: Entrance	17 36 40	140 37 06	......	......	......	......
	Albert River: Kangaroo Pt	17 35 10	139 45 56	......	......	......	......
	Sweers Island: Inscription Pt	17 06 50	139 38 36	......	......	......	......

TASMANIA.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
	Cape Portland: NW. pt	40 44 15	147 56 09	......	......	......	......
	Port Dalrymple: Low Head light	41 03 25	146 47 54	11 10	5 00	9.0	6.9
	Port Sorrell: NW. entrance head	41 07 05	146 33 30	......	......	......	......
	Port Frederick: Entrance	41 10 00	146 24 30	......	......	......	......
	Leven River: W. entrance head	41 08 30	146 12 00	......	......	......	......
	Emu Bay: Blackman Pt	41 02 50	145 56 39	......	......	......	......
	Hunter Island: N. pt	40 23 40	144 47 45	......	......	......	......
	Cape Grim: Outer Doughboy Islet	40 40 10	144 39 44	......	......	......	......
	Albatross Islet: N. pt	40 22 00	144 39 19	......	......	......	......
	Arthur River: Entrance	41 04 00	144 44 00	......	......	......	......
	Pieman River: Rocks close to entrance	41 41 00	144 57 00	......	......	......	......
	Macquarie Harbor: Entrance Islet	42 11 37	145 12 34	7 20	1 07	2.7	2.1
	Cape Sorrell: Light-house	42 11 00	145 10 30	......	......	......	......
	Port Davey: Pollard Head	43 19 00	145 53 00	......	......	......	......
	Southwest Cape: Extreme pt	43 33 30	146 01 04	......	......	......	......
	Mewstone Rock: Center	43 44 30	146 22 04	......	......	......	......
	Cape Bruny: Light-house	43 29 40	147 08 49	......	......	......	......
	Bruny Island: Penguin Islet	43 21 00	147 23 40	......	......	......	......
	Hobart Town: Transit of Venus station	42 53 25	147 20 07	8 05	1 52	4.2	3.2
	Cape Pillar: Tasman Islet	43 14 00	148 02 00	......	......	......	......
	Cape Frederik Hendrik: Extreme	42 52 00	148 00 00	......	......	......	......
	Freycinet Peninsula: Summit	42 13 00	148 18 04	......	......	......	......
	St. Patrick Head: N. pt	41 34 00	148 19 30	......	......	......	......
	Eddystone Point: Extreme	40 59 40	148 20 50	......	......	......	......

NEW ZEALAND.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
North I.	Three Kings Islands: NE. extreme of NE. island	34 06 20	172 08 49	......	......	......	......
	North Cape: Cape Islet	34 25 07	173 03 34	......	......	......	......
	Parenga-renga Harbor: Kohan Pt	34 31 00	173 00 54	......	......	......	......
	Maunganui Harbor: White Pt	35 00 20	173 32 39	......	......	......	......
	Wangaroa Harbor: Peach Islet	35 01 44	173 45 48	7 40	1 30	6.4	4.5
	Bay of Islands: Motu Mea Islet	35 17 00	174 06 06	7 26	1 55	5.9	4.2

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

NEW ZEALAND—Continued.

Coast.	Place.	Lat. S.	Long. E.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
North Island.	Wangaruru Harbor: Grove Pt	35 23 48	174 21 24	7 15	1 05	6.5	4.6
	Wangari Harbor: Loot Pt	35 51 09	174 31 14	7 05	0 55	6.7	4.8
	Great Barrier Island: Needles Pt	36 01 15	175 25 34				
	Auckland Harbor: Light-house	36 50 06	174 51 00	7 20	1 10	10.8	7.7
	Coromandel Harbor: Tuhnia I	36 48 35	175 24 34	7 05	0 55	10.7	7.6
	Cape Colville: N. pt	36 28 20	175 21 04				
	Cuvier Island: Light-house	36 26 20	175 49 00				
	Tauranga Harbor: Mount Maunganui, 860 ft	37 36 25	176 10 14	7 05	0 55	6.1	4.4
	White Island: Summit, 863 ft	37 30 00	177 10 49				
	Cape Runaway: Extreme	37 30 45	177 59 34	8 10	2 00	6.6	4.7
	East Cape: Islet, 420 ft	37 40 00	178 35 09	8 00	1 50	6.8	5.8
	Tolaga Bay: Matu-heka Islet	38 20 50	178 20 14				
	Mahia Peninsula: S. extreme of Portland I	39 18 00	177 53 15				
	Ahuriri Harbor: Light-house	39 28 30	176 54 14	6 05	12 15	3.5	3.0
	Kidnappers Cape: Extreme	39 38 00	177 06 44				
	Cape Palliser: Light-house	41 36 45	175 18 45	4 40	10 50	5.7	4.9
	Port Nicholson: Pencarrow light	41 21 40	174 51 04				
	Wellington: Queen's Wharf light	41 17 17	174 47 25	4 52	10 54	3.6	3.1
	Mana-watu River: Light-house	40 27 10	175 14 40	9 40	3 30	6.3	5.4
	Wanganui River: N. head	39 57 00	174 59 44				
	Egmont Mountain: Summit, 8,270 ft	39 18 00	174 03 59				
	New Plymouth: Flag-staff	39 03 35	174 04 35	9 15	3 05	11.6	8.2
	Kawhia Harbor: S. head	38 04 50	174 48 04	9 10	3 00	11.9	8.5
	Aotea Harbor: S. head	37 59 35	174 50 04				
	Whaingaroa Harbor: S. entrance pt	37 46 22	174 52 19	9 08	2 55	12.3	8.7
	Manukau Harbor: Paratutai flag-staff	37 03 00	174 31 14	9 05	2 50	12.6	9.0
	Kaipara Harbor: Light-house	36 23 00	174 08 00	9 00	2 50	10.0	7.1
	Hokianga River: Flag-staff at entrance	35 32 05	173 21 59	8 40	2 30	9.2	6.5
South island.	Cape Campbell: Light-house	41 44 00	174 17 14	4 45	11 00	7.5	6.5
	Port Cooper: Lyttleton custom-house	43 46 40	172 44 17	3 45	10 00	7.4	5.8
	Akaroa Island: Light-house	43 54 00	173 00 20				
	Ashburton River: N. entrance pt	44 04 50	171 48 34				
	Waitangi River: N. entrance head	44 54 50	171 11 14				
	Otago Harbor: Taivoa Head light	45 46 55	170 44 02	3 31	9 39	5.6	4.4
	Molyneux Bay: Landing place	46 24 05	169 47 53				
	Nugget Point: Light-house	46 27 10	169 50 04				
	Bluff Harbor: Light-house	46 37 00	168 23 00	1 05	7 15	7.8	6.2
	Tewaewae Bay: Pahia Pt	46 20 40	167 42 19				
	Solander Islands: Summit, 1,100 ft	46 36 00	166 54 04				
	Preservation Inlet: Light-house	46 10 00	166 38 15	11 10	5 00	7.5	5.9
	West Cape: Extreme	45 54 50	166 25 49				
	Queenstown: U. S. Tr. of Venus station	45 02 07	168 40 06				
	Milford Sound: Freshwater Basin	44 40 20	167 54 45				
	Cascade Point: N. extreme	44 00 30	168 21 34				
	Grey River: Entrance	42 26 20	171 11 54	10 10	4 00	9.8	7.7
	Hokitika: Entrance light	42 42 20	170 59 30	10 20	4 10	9.5	7.5
	Cape Foulwind: Light-house	41 45 40	171 27 44				
	Cape Farewell: Extreme	40 29 50	172 41 04				
	Nelson: Bowlder Bank light	41 16 05	173 17 30	9 55	3 45	12.0	9.4
	D'Urville Island: Port Hardy	40 46 35	173 54 04	9 45	3 35	11.6	9.2
	Port Gore: Head of Melville Cove	41 01 55	174 11 22				
	Port Underwood: Flag Pt	41 20 28	174 08 24	6 00	12 15	7.6	6.6
Stewart I.	Port William: Howell's House	46 50 30	168 05 34				
	Paterson Inlet: Glory Cove	46 58 30	168 09 54	1 00	9 15	7.8	6.2
	Port Adventure: White Beach, S. end	47 03 52	168 10 57				
	Port Pegasus: Cove abreast Anchorage I	47 11 40	167 40 51	11 45	5 40	7.9	6.2
	Codfish Island: NW. extreme	46 45 45	167 36 49				
	Snares Islands: SW. islet	48 06 43	166 27 44				

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

THE ARCTIC REGIONS.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H.W.	Lun. Int. L.W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
	Cape Walsingham: Extreme	66 00 00	69 28 00				
	Mile Island: N. pt	64 04 00	77 50 00				
	Marble Island: E. end	62 33 00	91 06 00	4 00	10 15	12.0	5.1
	Cape Kendall: Extreme	63 42 00	87 15 00				
	Iglooik Island: E. pt	69 21 00	81 31 00	6 50	0 40	8.0	4.2
	Victoria Harbor: N. shore	70 09 17	91 30 33				
	Elizabeth Harbor: Entrance	70 38 14	92 10 56				
	Magnetic Pole, 1831	70 05 00	96 47 00				
	Port Neill: N. pt. of entrance	73 09 13	89 00 54				
	Port Bowen: N. cove	73 13 39	88 54 48				
	Batty Bay: S. pt. of entrance	73 13 00	91 08 00				
	Port Leopold: Whaler Pt	73 50 05	90 12 00	11 38	5 29	5.5	2.9
	Careys Islands	76 49 00	73 10 00				
	Discovery Harbor	81 04 40	64 45 00				
	Alert's Winter Quarters	82 27 00	61 18 00	10 35	4 20	2.6	1.0
	Cape Joseph Henry: N. extreme	82 40 00	63 38 00				
	Cape Hecla: N. extreme	82 54 00	64 45 00				
	Cape Columbia: Extreme	83 07 00	70 20 00				
	Melville Island: Winter Harbor	74 47 10	110 48 15	1 20	7 40	3.8	1.9
	North Cape	68 55 00	179 57 00				
			Long. E.				
	Liakhov Islands: E. pt. of New Siberia	75 10 00	150 30 00				
	Cape Tscheljuskin: E. pt	77 41 00	104 01 00				
	Nova Zembla: Vaigats I., N. pt	70 25 00	59 10 00				
	Cape Costin (Kostina)	70 55 00	53 01 50	10 00	3 50	7.0	4.0
	NE. pt., Cape Desire	76 58 00	65 40 00				
	Franz Josef Land: Wilczek I	79 55 00	58 45 00				
	Mezen: Epiphany Church	65 50 18	44 17 00				
	Morjovetz Island: Light-house	66 45 50	42 30 00				
	Archangel: Trinity Church	64 32 06	40 33 30	7 18	2 00	2.2	1.3
	Jighinsk Island: Light-house	65 12 17	36 51 30	5 05	11 30	3.8	2.1
	Onega: St. Michael's Church	63 53 36	38 08 30	9 02	3 10	9.1	5.2
	Salovetski: Light-house	65 07 00	35 37 00				
	Cape Sviatoi Nos: Light-house	68 08 51	39 48 54	9 05	2 55	13.9	7.8
	Bear Island	74 30 00	20 00 00				
	Spitzbergen Island: S. cape	76 35 00	17 23 00				
	Cloven Cliff	79 50 00	11 40 30				
	Danes I., Robbe Bay	79 42 00	11 07 00	0 14	6 25	5.3	3.0
Greenland.	(a)		Long. W.				
	Thank God Harbor	81 38 00	61 44 00	12 14	5 58	5.4	2.0
	Cape York: Extreme	75 55 00	65 30 00				
	Upernivik: Flagstaff	72 47 48	55 53 42	10 50	4 38	8.0	3.0
	Proven: Village	72 20 42	55 20 00				
	Omenak Island: Village	70 40 00	51 59 00				
	Godhavn: Village	69 14 04	53 24 07				
	Jacobshavn: Village	69 13 12	50 56 30				
	Claushavn: Village	69 07 30	50 55 30				
	Christianshaab: Village	68 49 06	51 00 00				
	Egedesmunde: Village	68 42 30	52 46 00				
	Whalefish Island: Boat Inlet	68 58 30	53 27 00	8 05	1 52	7.5	3.6
	Holsteinberg: Village	66 55 54	53 40 18	6 20	0 07	10.0	4.8
	Kangamint	65 48 42	53 23 00				
	Ny Sukkertop: Village	65 24 30	52 54 00				
	Godthaab: Flagstaff	64 10 36	51 45 48	6 40	0 27	12.5	6.0
	Sermelik Fjord: Kasuk Peak	63 29 12	51 10 48				
	Fiskernaes: Village	63 05 12	50 43 36				
	Jensen Nunatak: Peak	62 50 00	48 57 00				
	Ravn Storo: Peak	62 42 36	50 20 48				
	Frederikshaab: Church	61 59 36	49 44 00	6 12	0 00	9.0	3.6
	Kangarssuk Havn: Village	61 28 20	48 51 00				
	Arsuk: Pingo Beacon	61 10 24	48 26 00	6 15	0 03	12.0	4.8
	Kajartalik Island: Summit	61 09 42	48 30 42				
	Ivigtuk: House	61 12 12	48 10 30				
	Bangs Havn: Anchorage	60 47 30	47 52 00				
	Aurora Harbor	60 48 36	47 46 48				

[a] Cape Morris Jesup (the most northern known land), 83° 39′ N., 30° 40′ W. (approx.).

APPENDIX IV.

MARITIME POSITIONS AND TIDAL DATA.

THE ARCTIC REGIONS—Continued.

Coast.	Place.	Lat. N.	Long. W.	Lun. Int. H. W.	Lun. Int. L. W.	Range. Spg.	Range. Neap.
		° ′ ″	° ′ ″	h. m.	h. m.	ft.	ft.
Greenland.	Julianshaab: Village	60 43 07	46 01 00	4 56	11 09	7.0	2.8
	Neunortalik: Village	60 08 12	45 16 00	5 33	11 46	8.6	3.4
	Fredieriksthal: Village	60 00 00	44 40 00	2 55	9 10	9.4	3.8
	Cape Farewell: Staten Huk	59 49 00	44 01 42	4 00	10 13	7.5	3.0
	Aleuk Islands: Center	60 09 00	42 55 00	......	......	.....	.....
	Cape Tordenskjold: Extreme	61 25 00	42 15 00	......	......	.....	.....
	Cape Bille: Extreme	62 01 00	42 00 00	......	......	.....	.....
	Cape Juul: Extreme	63 14 00	40 50 00	......	......	.....	.....
	Cape Lowenorn: Extreme	64 30 00	39 30 00	......	......	.....	.....
	Dannesbrog Island: Beacon	65 18 00	38 30 00	......	......	.....	.....
	Ingolsfjeld	66 19 02	35 11 00	......	......	.....	.....
	Rigny Mount: Summit	69 00 12	26 10 24	......	......	.....	.....
	Pendulum Islands	74 40 00	18 17 00	11 05	4 53	6.7	3.9
	Cape Philipp Broke	74 55 00	17 33 00	11 10	4 58	3.7	2.1
	Cape Bismark: Extreme	76 47 00	18 40 00	......	......	.....	.....
	Jan Mayen Island: Mt. Beerenberg, 6,870 ft.	71 04 00	7 36 00	......	......	.....	.....
	Youngs Foreland, or Cape Northeast	71 08 00	7 26 00	......	......	.....	.....
	Mary Muss Bay	71 00 00	8 28 00	11 21	5 06	3.8	2.2
Iceland.	Langanaes Point	66 22 45	14 30 46	......	......	.....	.....
	Rissnaes Point	66 32 40	16 10 24	......	......	.....	.....
	Grimsey Norddranger: Tr. Station	66 33 42	17 57 36	......	......	.....	.....
	Skagataas Point	66 07 30	20 05 26	......	......	.....	.....
	North Cape: Kalfatindr	66 27 29	22 23 04	......	......	.....	.....
	Straumness Point	66 26 30	23 08 00	......	......	.....	.....
	Fugle or Staabierg Huk: Point	65 30 15	24 31 26	......	......	.....	.....
	Snaefells Yokul: Tr. Station	64 48 04	23 45 08	......	......	.....	.....
	Reykiavik: Observatory	64 08 40	21 55 00	5 10	11 25	14.5	8.4
	Cape Skagi: Light-house	64 04 09	22 39 04	......	......	.....	.....
	Reykianaes: Light-house	63 48 06	22 39 00	......	......	.....	.....
	Ingolfshofde: Tr. Station	63 48 19	16 36 13	......	......	.....	.....
	Papey Island: Tr. Station	64 35 42	14 08 31	......	......	.....	.....
	Reythur Fjeld: Tr. Station	64 55 27	13 41 10	......	......	.....	.....
	Balatangi: Light-house	65 16 14	13 32 22	......	......	.....	.....
	Dia Fjeld: Tr. Station	65 45 00	14 23 35	......	......	.....	.....

INDEX TO APPENDIX IV.

REGIONS AND COASTS.

REGIONS AND COASTS—continued.

PLACES.

PLACES—continued.

PLACES—continued.

PLACES—continued.

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PLACES—continued.

APPENDIX V.

LUNAR DISTANCES.

By reason of the comparative rapidity of motion of the moon relatively to the earth, it occurs that the angular distance, measured from the earth, between the moon and a body that occupies a fixed, or nearly fixed, position in the celestial sphere, is constantly changing. If, therefore, an observer accurately measures with a sextant the angle between the moon and one of the various celestial bodies for which the lunar distance is tabulated in the Nautical Almanac, this observed distance, reduced to true distance, affords a means for determining the absolute instant of time at which the observation was taken; and from this may be deduced the longitude and the chronometer error.

If it were practicable to obtain results with a close degree of accuracy by this method, it would be an invaluable aid to the navigator, eliminating all anxiety as to change of rate of the chronometer, and even rendering it possible to navigate a vessel without such an instrument. It is unfortunately the case, however, that the method does not afford results that may be regarded as reliable within small limits, since a very small error in the observed angle, which it may not be possible to avoid even though every care be taken, causes a large error in the deduced time. Navigators of the present day do not, therefore, employ the method of lunar distances except under extraordinary circumstances, such as when an accident to the chronometer occurs, or, on a very long voyage, when there is reason to suspect the correctness of the chronometer error as brought forward by the rate.

In order to facilitate the method of determining the longitude from lunar distances, there is published in the Nautical Almanac, for every third hour of Greenwich mean time, the angular distances of the center of the moon from the center of the sun, from the brightest planets and from certain bright fixed stars selected in the path of the moon. All the distances that can be observed on the same day are grouped together under that date, and the columns are read from left to right across both pages of the same opening. The letter W. or E. is affixed to the name of the sun, planet, or star to indicate that it is on the west or east side of the moon. An observer on the surface of the earth having measured a lunar distance, corrected it for instrumental errors and for the semidiameters of the objects, and cleared it from the effects of refraction and parallax, finds the *true* or *geocentric* distance. With this distance and the distances in the Nautical Almanac of the same bodies on the same day, the Greenwich mean time of the observation can be found, as will hereafter be described.

The unavoidable errors to which the observation of lunar distance is subject are diminished by making a number of measurements. Errors of the instrument may be diminished by measuring distances on opposite sides of the moon, when possible, and combining the results.

Before taking the observation, the Nautical Almanac must be examined to see from what objects the distances are computed. If the star or planet selected for observation is not recognized from its position relatively to other bodies in the heavens, it can easily be identified from the distance given in the Almanac; for the observer may set the sextant to the distance computed roughly for the estimated time at the meridian of Greenwich, and direct his sight to the east or west of the moon, according as the object is marked E. or W. in the Nautical Almanac, and, having found the reflected image of the moon upon the horizon glass, sweep the instrument to the right or left, and the image will pass over the star or planet sought, if above the horizon and the weather clear; the star or planet is always one of the brightest, and is situated nearly in the arc passing through the moon's center, perpendicular to the line connecting the two horns.

Although all the instruments used in these observations ought to be well adjusted, yet particular care should be taken of the sextant used in measuring the angular distance of the moon from the sun or star, since an error of 1′ in this distance will cause an error of nearly 30′ in the longitude deduced therefrom. When a great angular distance is to be measured it is absolutely necessary to use a telescope, and its parallelism with respect to the plane of the instrument must be carefully examined; but in measuring small distances the use of the telescope is not of such great importance, and a sight tube may then be used, taking care, however, that the eye and point of contact of the objects on the horizon glass be equally distant from the plane of the instrument. It is always conducive to accuracy to use a telescope, and, after a little practice, this is easily done.

While one person is observing the distance of the objects, two others should observe the altitudes. The chronometer should be under the eye of a fourth person appointed to note the time; the observer who takes the angular distance gives previous notice to the others to be ready with their altitudes by the time he has finished his observation, which, being done, the time, altitudes, and distance should be carefully noted; if other sets of observations are taken it must be done within the space of fifteen minutes, and the mean of all the observations should be worked as a single one.

When a ship is rolling considerably it is difficult to measure the distance of the objects, but when steady there is much less difficulty, especially in small distances, which are much more easily measured than large ones, and are not so liable to error from an ill adjustment of the telescope; an observer would therefore do well to choose those times for observation when the distance of the objects is less than 70° or 80°. But it must be observed that neither of the objects, if possible, ought to be at a less altitude than 10°, on account of the uncertainty of the refraction near the horizon, for the horizontal refraction varies from 33′ to 36′ 40″ by an alteration of 40° in the thermometer; this alteration might cause an error of 2° in the longitude with an observer who uses the mean refraction.

In measuring the distance of the moon from the sun we must bring the moon's round limb in contact with the nearer limb of the sun. In measuring the distance of the moon from a planet or fixed star the round limb must be brought in contact with the center of the star or planet, observing that, the semidiameter of the planet being only a few seconds, the center of it can be estimated sufficiently near for all the purposes of this observation.

In taking the altitude of the moon, the round limb, whether it be the upper or lower, must be brought to the horizon. In misty weather it is rather difficult to observe the altitude of the stars on account of their dimness. Sometimes they are so dim that they can not be seen through the telescope of a sextant, particularly if the mirrors are not well silvered. In this case the telescope must be laid aside and the altitude taken with a sight tube.

It has been assumed that there were observers enough to measure the altitudes when the distance was observed, but if that is not the case the altitudes may be estimated in a manner to be explained hereafter.

The method here given is that of Professor Chauvenet, and involves the use of the tables in this Appendix. The object of these tables is to give the true correction of a lunar distance in all cases when, with the apparent distance of the moon from the sun, a planet, or star, the apparent altitudes of the two objects have also been obtained by observation. They enable us readily to take into account: First, the parallax of the moon in the latitude of the observer, allowing for the spheroidal figure of the earth; second, the parallax of the sun or a planet; third, the true atmospheric refraction, allowing for the actual state of the air as shown by the barometer and thermometer; and, fourth, that effect of refraction which gives the apparent disks of the moon and sun an oval or elliptical figure.

The longitude deduced from a lunar observation, when no attention is paid to the spheroidal figure of the earth, to the barometer and thermometer, or to the elliptical figure of the disks, may in certain cases be in error a whole degree. It is true these extreme cases are rare in practice, but cases are common in which from such neglect the error in the longitude is 10′, 15′, or 20′, and it is absolutely necessary to get rid of such errors and to leave no other inaccuracy in the result than that which unavoidably follows from the observations.

THE OBSERVATION.—The record of a complete observation embraces:

1. The latitude and approximate longitude of the place of observation.
2. The approximate local time.
3. The time of observation as shown by a chronometer, and the error of the chronometer, or its difference from mean Greenwich time.
4. The apparent distance of the moon's bright limb from a star or planet, or from the nearer limb of the sun.
5. The apparent altitude of the moon's upper or lower limb above the sea horizon.
6. The apparent altitude of the star, planet, or lower limb of the sun above the sea horizon.
7. The height of the barometer and thermometer.
8. The height of the eye above the level of the sea.
9. The index correction of the sextant.

The index correction of the sextant may be supposed to be previously determined; but, since even in the best instruments it is not constant, its determination should be considered a necessary part of the observation.

The error of the chronometer alluded to is that which is obtained by applying the daily rate (multiplied by the proper number of days) to the error found before leaving port. The agreement or disagreement of the error thus found with that found by the lunar observation will be the test of the accuracy of the chronometer, subject, of course, to the accepted limits of accuracy of the observation itself.

PREPARATION OF THE DATA.—*Greenwich Date.*—Correct the chronometer time for its error from Greenwich time and deduce the Greenwich date, i. e., the Greenwich day and hour (mean time), reckoning the hours in succession from 0 to 24, beginning at noon.

Nautical Almanac.—With the Greenwich date enter the Almanac and take out the moon's semidiameter and horizontal parallax; if the sun is observed, take its semidiameter; in the case of a planet, take its horizontal parallax only.

Apparent Altitude of the Moon.—To the altitude given by the sextant apply the index correction of the instrument and subtract the dip of the horizon (Table 14).[a] If the lower limb is observed, add the semidiameter and augmentation (Table 18); if the upper limb is observed, subtract the augmented semidiameter. The result is the apparent altitude of the moon's center, denoted "☾'s *App. Alt.*"

Apparent Altitude of the Sun, Planet, or Star.—To the observed altitude apply the index correction of the sextant, and subtract the dip (Table 14); and if the sun is used, add its semidiameter when the lower limb is observed, or subtract it when the upper limb is observed. The result is the apparent altitude required, denoted by "☉'s or ✱'s *App. Alt.*"

Apparent Distance.—First, when the sun is used, to the observed distance (corrected for index error when necessary) add the moon's augmented semidiameter and the sun's semidiameter; second, when a planet or star is used, add the moon's augmented semidiameter if its nearer limb is observed, but subtract it if its farther limb is observed. The result is "*App. Dist.*"

Moon's Reduced Parallax and Refraction.—Enter Table 19 with the latitude of the place of observation and the moon's horizontal parallax, and take out the correction, which add to the horizontal parallax. Call the result the moon's reduced parallax, or "☾'s *Red. P.*"

Enter Table I with the moon's apparent altitude, and take out the mean reduced refraction, and apply to this mean refraction the corrections given in Tables 21 and 22, adding or subtracting these corrections according to the directions in the tables. The result is the moon's reduced refraction, or "☾'s *Red. R.*"

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[a] The tables designated by their numbers in Arabic notation are to be found in Part II. The tables contained in this Appendix, which are for exclusive use with lunar-distance observations, are denoted by Roman numbers.

Subtract the "☾'s Red. R." from the "☾'s Red. P." and mark the result as "☾'s *Red. P. and R.*"

Reduced Parallax and Refraction of Sun, Planet, or Star.[a]—With the apparent altitude of the sun, planet, or star, take from Table I the mean reduced refraction, which correct by Tables 21 and 22. If the sun is observed, subtract its horizontal parallax (which may always be taken at 8″.5) from its reduced refraction, and mark the result as "☉'s *Red. P. and R.*" If a planet is observed subtract its horizontal parallax, and mark the result as "✱'s *Red. P. and R.*" If a star is observed, its reduced refraction is at once the required "✱'s *Red. P. and R.*"

Computation of the True Distance.—Take from Tables II, III, IV, and V respectively the four logarithms A, B, C, D,[b] and place these logarithms each at the head of a column, marking the columns A, B, C, and D; then put the—

log of ☾'s Red. P. and R. (Table IX) in columns A and B.
log of ☉'s or ✱'s Red. P. and R. (Table IX) in columns C and D.
log sin ☾'s App. Alt. (Table 44) in columns A and D.
log sin ☉'s or ✱'s App. Alt. (Table 44) in columns B and C.
log cot App. Dist. (Table 44) in columns A and C.
log cosec App. Dist. (Table 44) in columns B and D.

The sum of the four logs in Col. A is the log (Table IX) of the *First Part of ☾'s Correction*, which is to be marked + when the app. dist. is less than 90°, but − when the app. dist. is greater than 90°.

The sum of the four logs in Col. B is the log (Table IX) of the *Second Part of ☾'s Correction*, which is always to be marked −.

The sum of the four logs in Col. C is the log (Table IX) of the *First Part of the ☉'s or ✱'s Correction*, which is to be marked − when the app. dist. is less than 90°, but + when the app. dist. is greater than 90°.

The sum of the four logs in Col. D is the log (Table IX) of the *Second part of the ☉'s or ✱'s Correction*, which is always to be marked +.

Combine the first and second parts of the ☾'s correction according to the signs prefixed; that is, take their *sum* if they have the *same* sign, but their *difference* if they have *different* signs, and prefix the sign of the greater to the result, which call "☾'s *whole correction.*"

In the same manner form the "☉'s or ✱'s *whole correction.*"

First Correction of Distance.—Combine the *☾'s whole corr.* and the *☉'s or ✱'s whole corr.*, according to their signs; the result is the *First Correction of Distance*, which is to be added to or subtracted from the apparent distance, according as its sign is + or −.

Second Correction of Distance.—Enter Table VI with the Apparent Distance and the First Correction of Distance, and take out the *Second Correction of Distance*, which is to be applied to the distance according to the directions in the side columns of the Table.

Correction for the Elliptical Figure of the Moon's Disk, or Contraction of the Moon's Semi-diameter.—Enter Table VII A with the ☾'s App. Alt. and ☾'s Red. P. and R., and take out the number. With this number and the ☾'s whole correction enter Table VII B and take out the required *contraction*, which is to be *added* to the app. dist. when the *farther* limb is observed, but *subtracted* when the *nearer* limb is observed.

Correction for the Elliptical Figure of the Sun's Disk, or Contraction of the Sun's Semi-diameter.—Enter Table VIII A with the ☉'s App. Alt. and ☉'s Red. P. and R., and take out the number. With this number and the ☉'s whole corr. enter Table VIII B and take out the required *contraction*, which is always to be *subtracted* from the distance (the *nearer* limb of the sun being always observed).

Correction for Compression, or for the Spheroidal Figure of the Earth.—Take from the Nautical Almanac for the Greenwich date the declinations of the bodies to the nearest whole degree. With the moon's declination and apparent distance, take from Table XI A the *first part of N*, and mark it with the sign in the table if the declination is *North;* but if the declination is *South*, change the sign from + to − or from − to +. With the sun's or star's declination and the apparent distance, take from Table XI B the *second part of N*, giving it the same sign as the declination. Take the *sum*, or *difference*, of the two parts, according as their signs are the *same* or *different*, and to the resulting number prefix the sign of the greater. The logarithm of this number of seconds, taken from Table IX, with its sign prefixed, is the required log N. To log N add the log sine of the latitude of the place of observation; the sum is the log (Table IX) of the required *correction for compression.* In north latitude *add* this correction if log N is +, or *subtract* it if log N is −; in south latitude *subtract* the correction when log N is +, and *add* it when log N is −.

All these corrections being applied to the Apparent Distance, the result is the *True Distance.*

To Find the Greenwich Time.—Find in the Nautical Almanac the two distances between which the true distance falls. Take out the first of these, together with the Prop. Log following it, and the hours of Greenwich time over it. Find the difference between the distance taken from the Almanac and the true distance, and to the log of this difference (Table IX) *add* the Prop. Log from the Almanac; the sum is the log (Table IX) of an interval of time to be added to the hours of Greenwich time taken from the Almanac. The result is the *approximate* Greenwich time.

To correct this Greenwich time, take the difference between the two Prop. Logs in the Almanac which stand against the two distances between which the true distance falls. With this difference and the interval of time just found enter Table X and take out the seconds, which are to be *added* to the approximate Greenwich time when the Prop. Logs are *decreasing*, but *subtracted* when the Prop. Logs are *increasing*. The result is the *true Greenwich time.*

By comparing with this the local mean time the longitude will be found; or, if testing the time shown by chronometer, the difference between the true Greenwich time and the time shown by the chronometer is the error of the chronometer as determined by the lunar observation.

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[a] The parallax of a star being zero, its "reduced parallax and refraction" become, of course, merely its "reduced refraction;" but as no mistake can arise from marking it as "✱'s Red. P. and R.," this designation has been retained in order to give simplicity and uniformity at once to the rules and the tables.

[b] No interpolation is necessary in taking out these logarithms.

Degree of Dependence.—If the error thus determined agrees with that deduced by means of the rate and original error, it may be accepted as a confirmation of the rate of the chronometer; if otherwise, more or less doubt is thrown upon the chronometer, according to the degree of accuracy of the lunar observation itself. An error of 10″ in the measurement of the distance produces about 20^s error in the Greenwich time; and since, even with the best observers, a single set of distances is subject to a possible error of 10″, it may be well to consider the chronometer as still to be trusted so long as it does not differ from the lunar by more than 20^s. Since, however, so much depends upon skill in measuring the distance, the observer can only form a correct judgment of the degree of dependence to be placed upon his own observations by repeated trials and a careful comparison of his several results.

Example: In Lat. 35° 30′ N., Long. 30° W., by account, at the local mean time, 1855, September 6, $18^h 8^m 0^s$, the observed distance of ⊙'s and ☾'s nearer limbs was 43° 52′ 10″; observed alt. ☾, 49° 32′ 50″; observed alt. ⊙, 5° 27′ 10″; barometer, $29^{in}.1$; thermometer, 75°; height of the eye above the sea, 20^{ft}; I. C., 0′ 00″; required the longitude.

Preparation of the Data.

L. M. T., Sept. 6,		$18^h 08^m$
Long., D. R.,	+	2 00
G. M. T., approx.,		20 08
Obs. Alt. ☾,		49° 32′ 50″
Dip, Table 14,	—	4 23
☾'s Aug. S. D.,	+	15 01
☾'s App. Alt.,		49 43 28
☾'s Red. R., Table I,		1′ 16″
Bar. $29^{in}.1$, Table 21,	—	3
Ther. 75°, Table 22,	—	4
☾'s Red. R.,		1 09
☾'s Red. P.,		54 23
☾'s Red. P. and R.,		53 14

☾'s S. D.,		14′ 50″.0
Aug. Table 18,	+	11 .2
☾'s Aug. S. D,		15 01 .2
Obs. Alt. ⊙,		5° 27′ 10″
Dip,	—	4 23
⊙'s S. D.,	+	15 55
⊙'s App. Alt.,		5 38 42
⊙'s Red R., Table I,		8′ 57″
Bar., Table 21,	—	16
Ther., Table 22,	—	28
⊙'s Red. R.,		8 13
⊙'s Par.,		8
⊙'s Red. P. and R.,		8 05

☾'s Par., N. A.,		54′ 19″.4
Aug., Table 19,	+	3 .6
☾'s Red. P.,		54 23 .0
Obs. Dist. ⊙| |☾,		43° 52′ 10″
☾'s Aug. S. D.,	+	15 01
⊙'s S. D.,	+	15 55
App. Dist.,		44 23 06
☾'s Dec., N. A.,		25° N.
⊙'s Dec., N. A.,		6° N.

Computation of the True Distance.

A.

log A, Table II,	0.0021
log ☾'s Red. P. and R.,	3.5043
log sin ☾'s App. Alt.,	9.8825
log cot App. Dist.,	0.0093
{log, Table IX,	3.3982
{1st Part ☾'s corr.,	+41′ 42″

B.

log B, Table III,	9.9951
log ☾'s Red. P. and R.,	3.5043
log sin ⊙'s App. Alt.,	8.9929
log cosec App. Dist.,	0.1552
{log, Table IX,	2.6475
{2d Part ☾'s corr.,	— 7′ 24″
☾'s whole corr.,	+34′ 18″

log N, Tabs. XI and IX,	(—) 0.845
log sin Lat., + 35° 30′,	(+) 9.764
{log, Table IX,	(—) 0.609
{Corr. for Compression,	— 4″

C.

log C, Table IV,	9.9949
log ⊙'s Red. P. and R.,	2.6857
log sin ⊙'s App. Alt.,	8.9929
log cot App. Dist.,	0.0093
{log, Table IX,	1.6828
{1st Part ⊙'s corr.,	—0′ 48″

D.

log D, Table V,	9.9992
log ⊙'s Red. P. and R.,	2.6857
log sin ☾'s App. Alt.,	9.8825
log cosec App. Dist.,	0.1552
{log, Table IX,	2.7226
{2d Part ⊙'s corr.,	+8′ 48″
⊙'s whole corr.,	+8′ 00″

App. Dist.,		44° 23′ 06″
1st Corr.,	+	42 18
2d Corr., Table VI,	—	16
Contraction of ☾'s S. D., Table VII,		0
Contraction of ⊙'s S. D., Table VIII,	—	20
Corr. for Comp.	—	4
True Distance,		45 04 44

Extract from Nautical Almanac, September, 1855.

GREENWICH MEAN TIME: LUNAR DISTANCES.

Day of the month.	Star's name and position.	Midnight.	P. L. of Diff.	XV^h.	P. L. of Diff.	XVIII^h.	P. L. of Diff.	XXI^h.	P. L. of Diff.
6	SUN E.	48° 46′ 55″	3422	47° 25′ 3″	3427	46° 3′ 17″	3433	44° 41′ 38″	3438

Computation of Greenwich Mean Time.

True Distance,	45° 04′ 44″		
Distance, N. A., at XVIII^h,	46 03 17	P. L., 0.3433	Diff. P. logs + 5
Difference,	58 33	log, Table IX, 3.5457	
Approximate interval,	2^h 09^m 04^s	log, Table IX, 3.8890	
Add—	18		
Approx. G. M. T.,	20 09 04		
Corr., Table X,	— 2		
True G. M. T.,	20 09 02		
L. M. T.,	18 08 00		
Longitude,	+ 2 01 02 = 30° 15′ 30″ W.		

EXAMPLE: In Lat. 55° 20′ S., Long. 120° 25′ W., by account, on August 29, 1855, at $9^h 40^m 00^s$ p. m., local mean time, the following distance and altitudes were found, being the mean of six observations corrected for index error. Observed distance of Fomalhaut and moon's farther limb, 46° 30′ 23″; observed alt. ☾, 6° 26′ 10″; observed alt. Fomalhaut, 52° 34′ 40″; barometer, 31^{in}; thermometer, 20°; height of the eye above the sea, 18^{ft}.

Preparation of the Data.

L. M. T., August 29,	9^h 40^m 00^s
Long. by D. R.,	+ 8 01 40
Approx. G. M. T.,	17 41 40
Obs. alt. ☾	6° 26′ 10″
Dip,	— 4 09
☾'s aug. S. D.,	+ 16 28
☾'s App. Alt.,	6 38 29
☾'s Red R., Table I,	7′ 48″
Bar., Table 21,	+ 16
Ther., Table 22,	+ 32
☾'s Red R.,	8 36
☾'s Red. P.,	60 20
☾'s Red. P. and R.,	51 44

☾'s S. D., Naut. Al.,	16′ 26″.3
Aug., Table 18,	+ 2 .0
☾'s aug S. D.,	16 28 .3
Obs. alt. ✳,	52° 34′ 40″
Dip,	— 4 09
✳'s App. Alt.,	52 30 31
✳'s Red. R., Table I,	1′ 13″
Bar., Table 21,	+ 2
Ther., Table 22,	+ 5
✳'s Red. R.,	1 20
✳'s Red P.,	0
✳'s Red. P. and R.,	1 20

☾'s Par., N. A.,	60′ 11″.8
Aug., Table 19,	+ 8 .3
☾' Red P.,	60 20 .1
Obs. Dist. ✳ ☾,	46° 30′ 23″
☾'s aug., S. D.,	— 16 28
App. Dist.,	46 13 55
☾'s Dec., N. A.,	4° N.
✳'s Dec., N. A.,	30° S.

Computation of the True Distance.

A.

log A, Table II,		0.0274
log ☾'s Red. P. and R.,		3.4919
log sin ☾'s App. Alt.,		9.0632
log cot App. Dist.,		9.9813
log, Table IX,		2.5638
1st Part ☾'s corr.,	+	6′ 06″

B.

log B, Table III,		0.0001
log ☾'s Red. P. and R.,		3.4919
log sin ✱'s App. Alt.,		9.8995
log cosec App. Dist.,		0.1414
log, Table IX,		3.5329
2d Part ☾'s corr.,	—	56′ 51″
☾'s whole corr.,	—	50 45
log N, Tabs. XI and IX,	(—)	1.230
log sin Lat., –55°,	(—)	9.913
log Table IX,	(+)	1.143
Corr. for Comp.,	+	14″

C.

log C, Table IV,		9.9999
log ✱'s Red. P. and R.,		1.9031
log sin ✱'s App. Alt.,		9.8995
log cot App. Dist.,		9.9813
log, Table IX,		1.7838
1st Part ✱'s corr.,	—	1′ 01″

D.

log D, Table V,		0.0267
log ✱'s Red. P. and R.,		1.9031
log sin ☾'s App. Alt.,		9.0632
log cosec App. Dist.,		0.1414
log, Table IX,		1.1344
2d Part ✱'s corr.,	+	0′ 14″
✱'s whole corr.,	—	0 47

App. Dist.,		46° 13′ 55″
1st corr.,	—	51 32
2d corr., Table VI,	—	22
Contraction of ☾'s S. D., Table VII,	+	17
Corr. for Comp.,	+	14
True Distance,		45 22 32

Extract from Nautical Almanac, August, 1855.

GREENWICH MEAN TIME: LUNAR DISTANCES.

Day of the month.	Star's name and position.	Midnight.	P. L. of Diff.	XV[h].	P. L. of Diff.	XVIII[h].	P. L. of Diff.	XXI[h].	P. L. of Diff.
29	Fomalhaut W.	42° 11′ 34″	2535	43° 51′ 59″	2527	45° 32′ 35″	2521	47° 13′ 19″	2516

Computation of Greenwich Mean Time.

True Distance,	45° 22′ 32″			
Dist., N. A., at XV[h],	43 51 59	P. L.,	0.2527	Diff. P. logs — 6
Difference,	1 30 33	log, Table IX,	3.7350	
Approx. interval,	2[h] 42[m] 01[s]	log, Table IX,	3.9877	
Add—	15			
Approx. G. M. T.,	17 42 01			
Corr., Table X,	+ 01			
True G. M. T.,	17 42 02			
L. M. T.,	9 40 00			
Long.,	+ 8 02 02 = 120° 30′ 30″ W.			

Method of Taking a Lunar Observation by One Observer.—Three observers are required to make the necessary observations for determining the longitude—one to measure the distance of the bodies, and the others to take the altitudes. In case of not having a sufficient number of instruments or observers to take the altitudes, the latter may be calculated, there being given the latitude of the place, the time, the right ascensions, and the declinations of the objects. These calculations are long, however, especially in the case of the moon, and a considerable degree of accuracy is required in finding from the Nautical Almanac the moon's right ascension and declination, which must be liable to some error on account of the uncertainty of the ship's longitude. The following method of obtaining those altitudes is far more simple, and sufficiently accurate. This method depends on the supposition that the altitudes increase or decrease uniformly.

Before measuring the distance of the bodies, take their altitudes, and note the times by a chronometer; then measure the distance and note the time (or measure a number of distances, and note the corresponding times, and take the means); after having measured the distances, again measure the altitudes, and note the times; then, from the two observed altitudes of either of the objects, the required altitude of that object may be found from the following formula, which is based upon simple proportion:

$$x = \frac{d \times e}{t},$$

where x = change of altitude, in minutes, between first altitude and time of measuring the lunar distance, being positive or negative according as body is rising or falling;
d = difference between first and second altitudes, in minutes;
e = time, in seconds, between first altitude and lunar observations; and
t = time in seconds, between first and second altitudes.

The change of altitude thus deduced, applied with proper sign to the first altitude, gives the altitude at time of observing the lunar distance.

Example: Suppose the distances and altitudes of the sun and moon were observed, as in the following table; it is required to find the altitudes at the time of measuring the mean distance.

	Times by chronometer.	*Lunar distance.*	*Times by chronometer.*	*Obs. alt. ☾'s L. L.*	*Times by chronometer.*	*Obs. alt. ☉'s L. L.*
	$2^h\ 03^m\ 20^s$	40° 00′ 00″	$2^h\ 02^m\ 00^s$	20° 46′	$2^h\ 02^m\ 30^s$	40° 20′
	2 04 20	40 00 30	2 06 10	21 20	2 07 00	39 12
	2 05 50	40 01 30				
			t, 4 10	d, 34	t, 4 30	d, 1 08
Mean,	2 04 30	40 00 40	250^s		270^s	68′

For ☾.

Time of lunar obs.,	$2^h\ 04^m\ 30^s$
Time of 1st alt.,	2 02 00
e,	2 30 = 150^s

$$x = + \frac{34 \times 150}{250} = + 20'.4 = + 20'\ 24''$$

First altitude,	20° 46′ 00″
x,	+ 20 24
Required altitude,	21 06 24

For ☉.

Time of lunar obs.,	$2^h\ 04^m\ 30^s$
Time of 1st alt.,	2 02 30
e,	2 00 = 120^s

$$x = - \frac{68 \times 120}{270} = - 30'.2 = - 30'\ 12''$$

First altitude,	40° 20′ 00″
x,	− 30 12
Required altitude,	39 49 48

To obtain the altitudes by calculation the following formulæ may be employed:

$$\tan A = \tan d \sec t;$$

$$\sin h = \frac{\cos (A - L) \sin d}{\sin A};$$

in which d is the declination; t, the hour angle; L, the latitude; h, the *true* altitude of the center of the object; A, an arc which has the same name or sign as the declination and is numerically in the same quadrant as t. In the solution, strict regard must be had for the signs.

Example: Required the apparent altitude of the sun's center on December 22, 1879, in Lat. 48° 23′ N., Long. 60° W., at $10^h\ 01^m\ 14^s$ a. m., app. time.

L. A. T., December 21,	$22^h\ 01^m\ 14^s$	t,	$1^h\ 58^m\ 46^s$
Long.,	+ 4 00 00	☉'s Dec.,	23° 27′ 16″ S.
G. A. T., December 22,	2 01 14		

t	29° 41′ 30″	sec 0.06113	
d	− 23 . 27 16	tan (−) 9.63735	sin (−) 9.59991
A	− 26 32 20	tan (−) 9.69848	cosec (−) 0.34989
L	+ 48 23 00		
A − L	− 74 55 20		cos (+) 9.41520
h	13 23 58		sin (+) 9.36500
ref.—par.	+ 3 50		
App. alt.	13 27 48		

APPENDIX V: TABLE I.

Mean Reduced Refraction for Lunars.

Barometer 30 inches. Fahrenheit's Thermometer 50°.

Apparent altitude.	Reduced refraction.	Diff. to 1′.	Apparent altitude.	Reduced refraction.	Apparent altitude.	Reduced refraction.	Apparent altitude.	Reduced refraction.
° ′	′ ″	″	° ′	′ ″	° ′	′ ″	° ′	′ ″
5 0	9 54.2	1.6	10 0	5 24.1	15 0	3 41.7	27 0	2 7.8
5	9 46.3	1.5	5	5 21.6	10	3 39.4	27 30	2 5.7
10	9 38.6	1.5	10	5 19.2	20	3 37.1	28 0	2 3.7
15	9 31.0	1.5	15	5 16.8	30	3 34.9	28 30	2 1.7
20	9 23.7	1.4	20	5 14.4	40	3 32.7	29 0	1 59.8
25	9 16.5	1.4	25	5 12.1	50	3 30.6	29 30	1 58.0
5 30	9 9.5	1.4	10 30	5 9.8	16 0	3 28.5	30 0	1 56.2
35	9 2.7	1.3	35	5 7.5	10	3 26.5	30 30	1 54.5
40	8 56.0	1.3	40	5 5.3	20	3 24.5	31 0	1 52.8
45	8 49.5	1.3	45	5 3.1	30	3 22.6	31 30	1 51.2
50	8 43.1	1.2	50	5 0.9	40	3 20.7	32 0	1 49.7
55	8 36.9	1.2	55	4 58.8	50	3 18.8	32 30	1 48.2
6 0	8 30.9	1.2	11 0	4 56.7	17 0	3 16.9	33 0	1 46.7
5	8 24.9	1.2	5	4 54.6	10	3 15.1	33 30	1 45.3
10	8 19.1	1.1	10	4 52.5	20	3 13.4	34 0	1 44.0
15	8 13.4	1.1	15	4 50.5	30	3 11.6	34 30	1 42.7
20	8 7.8	1.1	20	4 48.5	40	3 9.9	35 0	1 41.4
25	8 2.4	1.1	25	4 46.6	50	3 8.2	35 30	1 40.2
6 30	7 57.0	1.0	11 30	4 44.6	18 0	3 6.6	36 0	1 39.0
35	7 51.8	1.0	35	4 42.7	10	3 5.0	36 30	1 37.8
40	7 46.7	1.0	40	4 40.8	20	3 3.4	37 0	1 36.7
45	7 41.7	1.0	45	4 38.9	30	3 1.8	37 30	1 35.6
50	7 36.7	1.0	50	4 37.1	40	3 0.3	38 0	1 34.5
55	7 31.9	0.9	55	4 35.3	50	2 58.8	38 30	1 33.5
7 0	7 27.2	0.9	12 0	4 33.5	19 0	2 57.3	39 0	1 32.5
5	7 22.6	0.9	5	4 31.7	10	2 55.9	39 30	1 31.5
10	7 18.0	0.9	10	4 30.0	20	2 54.4	40 0	1 30.6
15	7 13.6	0.9	15	4 28.3	30	2 53.0	40 30	1 29.6
20	7 9.2	0.9	20	4 26.6	40	2 51.6	41 0	1 28.7
25	7 4.9	0.8	25	4 24.9	50	2 50.3	41 30	1 27.8
7 30	7 0.8	0.8	12 30	4 23.2	20 0	2 49.0	42 0	1 27.0
35	6 56.6	0.8	35	4 21.6	10	2 47.6	42 30	1 26.2
40	6 52.6	0.8	40	4 20.0	20	2 46.4	43 0	1 25.4
45	6 48.6	0.8	45	4 18.4	30	2 45.1	43 30	1 24.6
50	6 44.8	0.8	50	4 16.8	40	2 43.8	44 0	1 23.8
55	6 40.9	0.7	55	4 15.2	50	2 42.6	44 30	1 23.1
8 0	6 37.2	0.7	13 0	4 13.7	21 0	2 41.4	45 0	1 22.4
5	6 33.5	0.7	5	4 12.2	10	2 40.2	46 0	1 21.0
10	6 29.9	0.7	10	4 10.7	20	2 39.0	47 0	1 19.6
15	6 26.3	0.7	15	4 9.2	30	2 37.9	48 0	1 18.4
20	6 22.8	0.7	20	4 7.7	40	2 36.7	49 0	1 17.2
25	6 19.4	0.7	25	4 6.3	50	2 35.6	50 0	1 16.0
8 30	6 16.0	0.7	13 30	4 4.8	22 0	2 34.5	51 0	1 15.0
35	6 12.7	0.6	35	4 3.4	10	2 33.4	52 0	1 13.9
40	6 9.5	0.6	40	4 2.0	20	2 32.4	53 0	1 13.0
45	6 6.3	0.6	45	4 0.6	30	2 31.3	54 0	1 12.0
50	6 3.1	0.6	50	3 59.3	40	2 30.3	55 0	1 11.1
55	6 0.0	0.6	55	3 57.9	50	2 29.2	56 0	1 10.3
9 0	5 57.0	0.6	14 0	3 56.6	23 0	2 28.2	57 0	1 9.5
5	5 54.0	0.6	5	3 55.3	20	2 26.3	58 0	1 8.7
10	5 51.1	0.6	10	3 54.0	40	2 24.4	59 0	1 8.0
15	5 48.2	0.6	15	3 52.7	24 0	2 22.5	60 0	1 7.3
20	5 45.3	0.6	20	3 51.4	20	2 20.7	62 0	1 6.0
25	5 42.5	0.5	25	3 50.1	40	2 18.9	64 0	1 4.9
9 30	5 39.8	0.5	14 30	3 48.9	25 0	2 17.2	66 0	1 3.8
35	5 37.0	0.5	35	3 47.6	20	2 15.5	68 0	1 2.9
40	5 34.4	0.5	40	3 46.4	40	2 13.9	70 0	1 2.0
45	5 31.7	0.5	45	3 45.2	26 0	2 12.3	73 0	1 1.0
50	5 29.2	0.5	50	3 44.0	20	2 10.8	76 0	1 0.1
55	5 26.6	0.5	55	3 42.8	40	2 9.3	80 0	0 59.2
10 0	5 24.1		15 0	3 41.7	27 0	2 7.8	90 0	0 58.3

APPENDIX V: TABLE II.

Log. A, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	Reduced parallax and refraction of moon.														
	41′	42′	43′	44′	45′	46′	47′	48′	49′	50′	51′	52′	53′	54′	55′
5° 0′	.0288	0295	0301	0308	0315	0321	0328	0335	0341	0348	0355	0361	0368		
2	.0286	0293	0299	0306	0313	0319	0326	0333	0339	0346	0352	0359	0366		
4	.0284	0291	0297	0304	0311	0317	0324	0330	0337	0344	0350	0357	0363		
6	.0282	0289	0296	0302	0309	0315	0322	0328	0335	0341	0348	0354	0361		
8	.0281	0287	0294	0300	0307	0313	0320	0326	0333	0339	0346	0352	0359		
5 10	.0279	0285	0292	0298	0305	0311	0318	0324	0331	0337	0344	0350	0356		
12	.0277	0284	0290	0296	0303	0309	0316	0322	0329	0335	0341	0348	0354		
14	.0275	0282	0288	0295	0301	0307	0314	0320	0327	0333	0339	0346	0352		
16	.0274	0280	0286	0293	0299	0306	0312	0318	0325	0331	0337	0344	0350		
18	.0272	0278	0285	0291	0297	0304	0310	0316	0323	0329	0335	0341	0348		
5 20	.0270	0277	0283	0289	0296	0302	0308	0314	0321	0327	0333	0339	0346		
22	.0269	0275	0281	0288	0294	0300	0306	0313	0319	0325	0331	0337	0344		
24	.0267	0273	0280	0286	0292	0298	0304	0311	0317	0323	0329	0335	0341		
26	.0265	0272	0278	0284	0290	0296	0303	0309	0315	0321	0327	0333	0339	0346	
28	.0264	0270	0276	0282	0289	0295	0301	0307	0313	0319	0325	0331	0337	0344	
5 30	.0262	0268	0275	0281	0287	0293	0299	0305	0311	0317	0323	0329	0335	0342	
32	.0261	0267	0273	0279	0285	0291	0297	0303	0309	0315	0321	0327	0334	0340	
34	.0259	0265	0271	0277	0283	0290	0296	0302	0308	0314	0320	0326	0332	0338	
36	.0258	0264	0270	0276	0282	0288	0294	0300	0306	0312	0318	0324	0330	0336	
38		0262	0268	0274	0280	0286	0292	0298	0304	0310	0316	0322	0328	0334	
5 40		0261	0267	0273	0279	0285	0290	0296	0302	0308	0314	0320	0326	0332	
42		0259	0265	0271	0277	0283	0289	0295	0301	0306	0312	0318	0324	0330	
44		0258	0264	0270	0275	0281	0287	0293	0299	0305	0311	0316	0322	0328	
46		0256	0262	0268	0274	0280	0286	0291	0297	0303	0309	0315	0320	0326	
48		0255	0261	0267	0272	0278	0284	0290	0296	0301	0307	0313	0319	0324	
5 50		0253	0259	0265	0271	0277	0282	0288	0294	0300	0305	0311	0317	0323	
52		0252	0258	0264	0269	0275	0281	0287	0292	0298	0304	0309	0315	0321	
54		0251	0256	0262	0268	0274	0279	0285	0291	0296	0302	0308	0313	0319	
56		0249	0255	0261	0266	0272	0278	0283	0289	0295	0300	0306	0312	0317	
58		0248	0254	0259	0265	0271	0276	0282	0287	0293	0299	0304	0310	0316	
6 0		0247	0252	0258	0263	0269	0275	0280	0286	0291	0297	0303	0308	0314	
2		0245	0251	0256	0262	0268	0273	0279	0284	0290	0295	0301	0307	0312	
4		0244	0249	0255	0261	0266	0272	0277	0283	0288	0294	0299	0305	0310	
6		0243	0248	0254	0259	0265	0270	0276	0281	0287	0292	0298	0303	0309	
8		0241	0247	0252	0258	0263	0269	0274	0280	0285	0291	0296	0302	0307	
6 10		0240	0246	0251	0256	0262	0267	0273	0278	0284	0289	0295	0300	0306	
12		0239	0244	0250	0255	0261	0266	0271	0277	0282	0288	0293	0299	0304	
14		0237	0243	0248	0254	0259	0265	0270	0275	0281	0286	0292	0297	0302	
16		0236	0242	0247	0252	0258	0263	0269	0274	0279	0285	0290	0295	0301	
18		0235	0240	0246	0251	0257	0262	0267	0273	0278	0283	0289	0294	0299	
6 20		0234	0239	0245	0250	0255	0261	0266	0271	0276	0282	0287	0292	0298	
22		0233	0238	0243	0249	0254	0259	0264	0270	0275	0280	0286	0291	0296	
24		0231	0237	0242	0247	0253	0258	0263	0268	0274	0279	0284	0289	0295	
26			0236	0241	0246	0251	0257	0262	0267	0272	0277	0283	0288	0293	
28			0234	0240	0245	0250	0255	0260	0266	0271	0276	0281	0286	0292	0297
6 30			0233	0238	0244	0249	0254	0259	0264	0270	0275	0280	0285	0290	0295
32			0232	0237	0242	0248	0253	0258	0263	0268	0273	0278	0284	0289	0294
34			0231	0236	0241	0246	0251	0257	0262	0267	0272	0277	0282	0287	0292
36			0230	0235	0240	0245	0250	0255	0260	0266	0271	0276	0281	0286	0291
38			0229	0234	0239	0244	0249	0254	0259	0264	0269	0274	0279	0284	0290
6 40			0227	0232	0238	0243	0248	0253	0258	0263	0268	0273	0278	0283	0288
42			0226	0231	0236	0241	0246	0252	0257	0262	0267	0272	0277	0282	0287
44			0225	0230	0235	0240	0245	0250	0255	0260	0265	0270	0275	0280	0285
46			0224	0229	0234	0239	0244	0249	0254	0259	0264	0269	0274	0279	0284
48			0223	0228	0233	0238	0243	0248	0253	0258	0263	0268	0273	0278	0283
6 50			0222	0227	0232	0237	0242	0247	0252	0257	0262	0266	0271	0276	0281
52			0221	0226	0231	0236	0241	0246	0250	0255	0260	0265	0270	0275	0280
54			0220	0225	0230	0235	0239	0244	0249	0254	0259	0264	0269	0274	0279
56			0219	0224	0229	0233	0238	0243	0248	0253	0258	0263	0267	0272	0277
58			0218	0223	0227	0232	0237	0242	0247	0252	0257	0261	0266	0271	0276
7 0			0217	0222	0226	0231	.0236	0241	0246	0251	0255	0260	0265	0270	0275

Log. A, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	Reduced parallax and refraction of moon.													
	44′	45′	46′	47′	48′	49′	50′	51′	52′	53′	54′	55′	56′	57′
7° 0′	.0222	0226	0231	0236	0241	0246	0251	0255	0260	0265	0270	0275		
3	.0220	0225	0230	0234	0239	0244	0249	0254	0258	0263	0268	0273		
6	.0218	0223	0228	0233	0238	0242	0247	0252	0257	0261	0266	0271		
9	.0217	0222	0226	0231	0236	0241	0245	0250	0255	0260	0264	0269		
12	.0215	0220	0225	0230	0234	0239	0244	0248	0253	0258	0262	0267		
7 15	.0214	0219	0223	0228	0233	0237	0242	0247	0251	0256	0261	0265		
18	.0213	0217	0222	0226	0231	0236	0240	0245	0250	0254	0259	0263		
21	.0211	0216	0220	0225	0230	0234	0239	0243	0248	0253	0257	0262		
24	.0210	0214	0219	0223	0228	0233	0237	0242	0246	0251	0255	0260		
27	.0208	0213	0217	0222	0227	0231	0236	0240	0245	0249	0254	0258		
7 30	.0207	0211	0216	0220	0225	0230	0234	0239	0243	0248	0252	0257		
33	.0206	0210	0215	0219	0224	0228	0232	0237	0241	0246	0250	0255		
36	.0204	0209	0213	0218	0222	0227	0231	0235	0240	0244	0249	0253		
39	.0203	0207	0212	0216	0221	0225	0229	0234	0238	0243	0247	0252		
42	.0202	0206	0210	0215	0219	0224	0228	0232	0237	0241	0246	0250		
7 45	.0200	0205	0209	0213	0218	0222	0227	0231	0235	0240	0244	0248		
48	.0199	0203	0208	0212	0216	0221	0225	0229	0234	0238	0242	0247		
51	.0198	0202	0206	0211	0215	0219	0224	0228	0232	0237	0241	0245	0249	
54	.0196	0201	0205	0209	0214	0218	0222	0227	0231	0235	0239	0244	0248	
57	.0195	0200	0204	0208	0212	0217	0221	0225	0229	0234	0238	0242	0246	
8 0	.0194	0198	0203	0207	0211	0215	0219	0224	0228	0232	0236	0241	0245	
3	.0193	0197	0201	0206	0210	0214	0218	0222	0227	0231	0235	0239	0243	
6	.0192	0196	0200	0204	0208	0213	0217	0221	0225	0229	0233	0238	0242	
9		0195	0199	0203	0207	0211	0215	0220	0224	0228	0232	0236	0240	
12		0193	0198	0202	0206	0210	0214	0218	0222	0227	0231	0235	0239	
8 15		0192	0196	0201	0205	0209	0213	0217	0221	0225	0229	0233	0237	
18		0191	0195	0199	0203	0207	0212	0217	0220	0224	0228	0232	0236	
21		0190	0194	0198	0202	0206	0210	0214	0218	0222	0226	0231	0235	
24		0189	0193	0197	0201	0205	0209	0213	0217	0221	0225	0229	0233	
27		0188	0192	0196	0200	0204	0208	0212	0216	0220	0224	0228	0232	
8 30		0187	0191	0195	0199	0203	0207	0211	0215	0219	0223	0226	0230	
33		0186	0190	0193	0197	0201	0205	0209	0213	0217	0221	0225	0229	
36		0184	0188	0192	0196	0200	0204	0208	0212	0216	0220	0224	0228	
39		0183	0187	0191	0195	0199	0203	0207	0211	0215	0219	0223	0226	
42		0182	0186	0190	0194	0198	0202	0206	0210	0214	0217	0221	0225	
8 45		0181	0185	0189	0193	0197	0201	0205	0208	0212	0216	0220	0224	
48		0180	0184	0188	0192	0196	0200	0203	0207	0211	0215	0219	0223	
51		0179	0183	0187	0191	0195	0198	0202	0206	0210	0214	0218	0221	
54		0178	0182	0186	0190	0193	0197	0201	0205	0209	0212	0216	0220	
57		0177	0181	0185	0189	0192	0196	0200	0204	0208	0211	0215	0219	
9 0		0176	0180	0184	0188	0191	0195	0199	0203	0206	0210	0214	0218	
3		0175	0179	0183	0186	0190	0194	0198	0201	0205	0209	0213	0216	
6		0174	0178	0182	0185	0189	0193	0197	0200	0204	0208	0211	0215	
9		0173	0177	0181	0184	0188	0192	0196	0199	0203	0207	0210	0214	
12		0172	0176	0180	0183	0187	0191	0194	0198	0202	0206	0209	0213	
9 15		0171	0175	0179	0182	0186	0190	0193	0197	0201	0204	0208	0212	
18		0170	0174	0178	0181	0185	0189	0192	0196	0200	0203	0207	0211	
21		0170	0173	0177	0180	0184	0188	0191	0195	0199	0202	0206	0209	
24			0172	0176	0179	0183	0187	0190	0194	0198	0201	0205	0208	
27			0171	0175	0179	0182	0186	0189	0193	0196	0200	0204	0207	
9 30			0170	0174	0178	0181	0185	0188	0192	0195	0199	0203	0206	
33			0170	0173	0177	0180	0184	0187	0191	0194	0198	0201	0205	
36			0169	0172	0176	0179	0183	0186	0190	0193	0197	0200	0204	
39			0168	0171	0175	0178	0182	0185	0189	0192	0196	0199	0203	
42			0167	0170	0174	0177	0181	0184	0188	0191	0195	0198	0202	
9 45			0166	0169	0173	0176	0180	0183	0187	0190	0194	0197	0201	
48			0165	0169	0172	0176	0179	0182	0186	0189	0193	0196	0200	0203
51			0164	0168	0171	0175	0178	0182	0185	0188	0192	0195	0199	0202
54			0163	0167	0170	0174	0177	0181	0184	0187	0191	0194	0198	0201
57			0163	0166	0169	0173	0176	0180	0183	0186	0190	0193	0197	0200
10 0			0162	0165	0169	0172	0175	0179	0182	0186	0189	0192	0196	0199

APPENDIX V: TABLE II.

Log. A, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	Reduced parallax and refraction of moon. 46′	47′	48′	49′	50′	51′	52′	53′	54′	55′	56′	57′	58′
10° 0′	.0162	0165	0169	0172	0175	0179	0182	0186	0189	0192	0196	0199	
5	.0160	0164	0167	0171	0174	0177	0181	0184	0187	0191	0194	0197	
10	.0159	0162	0166	0169	0172	0176	0179	0182	0186	0189	0192	0196	
15	.0158	0161	0164	0168	0171	0174	0178	0181	0184	0187	0191	0194	
20	.0156	0160	0163	0166	0170	0173	0176	0179	0183	0186	0189	0192	
25	.0155	0158	0162	0165	0168	0171	0175	0178	0181	0184	0188	0191	
10 30	.0154	0157	0160	0164	0167	0170	0173	0177	0180	0183	0186	0189	
35	.0153	0156	0159	0162	0166	0169	0172	0175	0178	0181	0185	0188	
40	.0151	0155	0158	0161	0164	0167	0171	0174	0177	0180	0183	0186	
45	.0150	0153	0157	0160	0163	0166	0169	0172	0175	0179	0182	0185	
50	.0149	0152	0155	0158	0162	0165	0168	0171	0174	0177	0180	0183	
55	.0148	0151	0154	0157	0160	0163	0167	0170	0173	0176	0179	0182	
11 0	.0147	0150	0153	0156	0159	0162	0165	0168	0171	0174	0177	0181	
5	.0146	0149	0152	0155	0158	0161	0164	0167	0170	0173	0176	0179	
10		0148	0151	0154	0157	0160	0163	0166	0169	0172	0175	0178	
15		0146	0149	0152	0155	0158	0161	0164	0167	0170	0173	0176	
20		0145	0148	0151	0154	0157	0160	0163	0166	0169	0172	0175	
25		0144	0147	0150	0153	0156	0159	0162	0165	0168	0171	0174	
11 30		0143	0146	0149	0152	0155	0158	0161	0164	0167	0170	0172	
35		0142	0145	0148	0151	0154	0157	0160	0162	0165	0168	0171	
40		0141	0144	0147	0150	0153	0156	0158	0161	0164	0167	0170	
45		0140	0143	0146	0149	0151	0154	0157	0160	0163	0166	0169	
50		0139	0142	0145	0148	0150	0153	0156	0159	0162	0165	0167	
55		0138	0141	0144	0146	0149	0152	0155	0158	0161	0163	0166	
12 0		0137	0140	0143	0145	0148	0151	0154	0157	0159	0162	0165	
5		0136	0139	0142	0144	0147	0150	0153	0156	0158	0161	0164	
10		0135	0138	0141	0143	0146	0149	0152	0154	0157	0160	0163	
15		0134	0137	0140	0142	0145	0148	0151	0153	0156	0159	0162	
20		0133	0136	0139	0141	0144	0147	0150	0152	0155	0158	0160	
25		0132	0135	0138	0140	0143	0146	0148	0151	0154	0157	0159	
12 30		0131	0134	0137	0139	0142	0145	0147	0150	0153	0155	0158	
35		0130	0133	0136	0138	0141	0144	0146	0149	0152	0154	0157	
40		0129	0132	0135	0137	0140	0143	0145	0148	0151	0153	0156	
45		0129	0131	0134	0136	0139	0142	0144	0147	0150	0152	0155	0158
50		0128	0130	0133	0136	0138	0141	0143	0146	0149	0151	0154	0156
55		0127	0129	0132	0135	0137	0140	0142	0145	0148	0150	0153	0155
13 0		0126	0129	0131	0134	0136	0139	0141	0144	0147	0149	0152	0154
5		0125	0128	0130	0133	0135	0138	0141	0143	0146	0148	0151	0153
10		0124	0127	0129	0132	0135	0137	0140	0142	0145	0147	0150	0152
15		0123	0126	0129	0131	0134	0136	0139	0141	0144	0146	0149	0151
20		0123	0125	0128	0130	0133	0135	0138	0140	0143	0145	0148	0150
25		0122	0124	0127	0129	0132	0134	0137	0139	0142	0144	0147	0149
13 30		0121	0124	0126	0129	0131	0133	0136	0138	0141	0143	0146	0148
35		0120	0123	0125	0128	0130	0133	0135	0138	0140	0142	0145	0147
40		0120	0122	0124	0127	0129	0132	0134	0137	0139	0142	0144	0146
45			0121	0124	0126	0128	0131	0133	0136	0138	0141	0143	0145
50			0120	0123	0125	0128	0130	0132	0135	0137	0140	0142	0145
55			0120	0122	0124	0127	0129	0132	0134	0136	0139	0141	0144
14 0			0119	0121	0124	0126	0128	0131	0133	0136	0138	0140	0143
5			0118	0121	0123	0125	0128	0130	0132	0135	0137	0139	0142
10			0117	0120	0122	0124	0127	0129	0132	0134	0136	0139	0141
15			0117	0119	0121	0124	0126	0128	0131	0133	0135	0138	0140
20			0116	0118	0121	0123	0125	0128	0130	0132	0135	0137	0139
25			0115	0118	0120	0122	0124	0127	0129	0131	0134	0136	0138
14 30			0114	0117	0119	0121	0124	0126	0128	0131	0133	0135	0137
35			0114	0116	0118	0121	0123	0125	0128	0130	0132	0134	0137
40			0113	0115	0118	0120	0122	0124	0127	0129	0131	0134	0136
45			0112	0115	0117	0119	0121	0124	0126	0128	0130	0133	0135
50			0112	0114	0116	0118	0121	0123	0125	0127	0130	0132	0134
55			0111	0113	0116	0118	0120	0122	0124	0127	0129	0131	0133
15 0			0110	0113	0115	0117	0119	0121	0124	0126	0128	0130	0133

APPENDIX V: TABLE II.

Log. A, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	Reduced parallax and refraction of moon.											
	48′	49′	50′	51′	52′	53′	54′	55′	56′	57′	58′	59′
15° 0′	.0110	0113	0115	0117	0119	0121	0124	0126	0128	0130	0133	
10	.0109	0111	0113	0116	0118	0120	0122	0124	0127	0129	0131	
20	.0108	0110	0112	0114	0116	0119	0121	0123	0125	0127	0129	
30	.0107	0109	0111	0113	0115	0117	0119	0121	0124	0126	0128	
40	.0105	0107	0110	0112	0114	0116	0118	0120	0122	0124	0126	
50	.0104	0106	0108	0110	0112	0115	0117	0119	0121	0123	0125	
16 0	.0103	0105	0107	0109	0111	0113	0115	0117	0119	0121	0124	
10	.0102	0104	0106	0108	0110	0112	0114	0116	0118	0120	0122	
20	.0101	0103	0105	0107	0109	0111	0113	0115	0117	0119	0121	
30	.0100	0102	0103	0105	0107	0109	0111	0113	0115	0117	0119	
40	.0098	0100	0102	0104	0106	0108	0110	0112	0114	0116	0118	
50	.0097	0099	0101	0103	0105	0107	0109	0111	0113	0115	0117	
17 0	.0096	0098	0100	0102	0104	0106	0108	0110	0112	0114	0116	
10	.0095	0097	0099	0101	0103	0105	0107	0109	0110	0112	0114	
20	.0094	0096	0098	0100	0102	0104	0106	0107	0109	0111	0113	
30		0095	0097	0099	0101	0103	0104	0106	0108	0110	0112	
40		0094	0096	0098	0100	0101	0103	0105	0107	0109	0111	
50		0093	0095	0097	0099	0100	0102	0104	0106	0108	0109	
18 0		0092	0094	0096	0098	0099	0101	0103	0105	0107	0108	
10		0091	0093	0095	0097	0098	0100	0102	0104	0105	0107	0109
20		0090	0092	0094	0096	0097	0099	0101	0103	0104	0106	0108
30		0089	0091	0093	0095	0096	0098	0100	0102	0103	0105	0107
40		0088	0090	0092	0094	0095	0097	0099	0101	0102	0104	0106
50		0088	0089	0091	0093	0094	0096	0098	0099	0101	0103	0105
19 0		0087	0088	0090	0092	0093	0095	0097	0098	0100	0102	0104
10		0086	0087	0089	0091	0092	0094	0096	0098	0099	0101	0103
20		0085	0087	0088	0090	0092	0093	0095	0097	0098	0100	0102
30		0084	0086	0087	0089	0091	0092	0094	0096	0097	0099	0101
40		0083	0085	0087	0088	0090	0091	0093	0095	0096	0098	0100
50		0082	0084	0086	0087	0089	0090	0092	0094	0095	0097	0099
20 0		0082	0083	0085	0086	0088	0090	0091	0093	0094	0096	0098
10		0081	0082	0084	0086	0087	0089	0090	0092	0093	0095	0097
20		0080	0082	0083	0085	0086	0088	0089	0091	0093	0094	0096
30		0079	0081	0082	0084	0086	0087	0089	0090	0092	0093	0095
40		0079	0080	0082	0083	0085	0086	0088	0089	0091	0092	0094
50		0078	0079	0081	0082	0084	0085	0087	0088	0090	0091	0093
21 0		0077	0079	0080	0082	0083	0085	0086	0088	0089	0091	0092
10		0076	0078	0079	0081	0082	0084	0085	0087	0088	0090	0091
20		0076	0077	0079	0080	0082	0083	0085	0086	0087	0089	0090
30		0075	0076	0078	0079	0081	0082	0084	0085	0087	0088	0090
40		0074	0076	0077	0079	0080	0082	0083	0084	0086	0087	0089
50		0074	0075	0076	0078	0079	0081	0082	0084	0085	0086	0088
22 0		0073	0074	0076	0077	0079	0080	0081	0083	0084	0086	0087
10		0072	0074	0075	0076	0078	0079	0081	0082	0083	0085	0086
20		0072	0073	0074	0076	0077	0079	0080	0081	0083	0084	0086
30		0071	0072	0074	0075	0076	0078	0079	0081	0082	0083	0085
40		0070	0072	0073	0074	0076	0077	0079	0080	0081	0083	0084
50		0070	0071	0072	0074	0075	0076	0078	0079	0081	0082	0083
23 0		0069	0070	0072	0073	0074	0076	0077	0078	0080	0081	0082
10		0068	0070	0071	0072	0074	0075	0076	0078	0079	0080	0082
20		0068	0069	0070	0072	0073	0074	0076	0077	0078	0080	0081
30		0067	0069	0070	0071	0072	0074	0075	0076	0078	0079	0080
40		0067	0068	0069	0071	0072	0073	0074	0076	0077	0078	0080
50		0066	0067	0069	0070	0071	0073	0074	0075	0076	0078	0079
24 0			0067	0068	0069	0071	0072	0073	0074	0076	0077	0078
10			0066	0067	0069	0070	0071	0073	0074	0075	0076	0078
20			0066	0067	0068	0069	0071	0072	0073	0074	0076	0077
30			0065	0066	0068	0069	0070	0071	0072	0074	0075	0076
40			0065	0066	0067	0068	0069	0071	0072	0073	0074	0076
50			0064	0065	0066	0068	0069	0070	0071	0072	0074	0075
25 0			0063	0065	0066	0067	0068	0069	0071	0072	0073	0074

APPENDIX V: TABLE II.

Log. A, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	Reduced parallax and refraction of moon.										
	50′	51′	52′	53′	54′	55′	56′	57′	58′	59′	60′
25° 0′	.0063	0065	0066	0067	0068	0069	0071	0072	0073	0074	
20	.0062	0064	0065	0066	0067	0068	0069	0071	0072	0073	
40	.0061	0062	0064	0065	0066	0067	0068	0069	0071	0072	
26 0	.0060	0061	0063	0064	0065	0066	0067	0068	0069	0071	
20	.0059	0060	0062	0063	0064	0065	0066	0067	0068	0069	
40	.0058	0059	0061	0062	0063	0064	0065	0066	0067	0068	
27 0	.0057	0058	0060	0061	0062	0063	0064	0065	0066	0067	
20	.0056	0057	0059	0060	0061	0062	0063	0064	0065	0066	
40	.0055	0057	0058	0059	0060	0061	0062	0063	0064	0065	
28 0	.0055	0056	0057	0058	0059	0060	0061	0062	0063	0064	
20	.0054	0055	0056	0057	0058	0059	0060	0061	0062	0063	
40	.0053	0054	0055	0056	0057	0058	0059	0060	0061	0062	
29 0	.0052	0053	0054	0055	0056	0057	0058	0059	0060	0061	
20	.0051	0052	0053	0054	0055	0056	0057	0058	0059	0060	
40	.0050	0051	0052	0053	0054	0055	0056	0057	0058	0059	
30 0	.0050	0051	0051	0052	0053	0054	0055	0056	0057	0058	
20	.0049	0050	0051	0052	0052	0053	0054	0055	0056	0057	
40	.0048	0049	0050	0051	0052	0053	0053	0054	0055	0056	
31 0	.0047	0048	0049	0050	0051	0052	0053	0053	0054	0055	
20	.0047	0047	0048	0049	0050	0051	0052	0053	0054	0054	0055
40	.0046	0047	0048	0048	0049	0050	0051	0052	0053	0054	0054
32 0	.0045	0046	0047	0048	0048	0049	0050	0051	0052	0053	0054
20	.0044	0045	0046	0047	0048	0049	0049	0050	0051	0052	0053
40	.0044	0045	0045	0046	0047	0048	0049	0049	0050	0051	0052
33 0	.0043	0044	0045	0045	0046	0047	0048	0049	0049	0050	0051
20	.0042	0043	0044	0045	0046	0046	0047	0048	0049	0050	0050
40	.0042	0043	0043	0044	0045	0045	0046	0047	0048	0049	0050
34 0	.0041	0042	0043	0043	0044	0045	0046	0046	0047	0048	0049
20	.0040	0041	0042	0043	0043	0044	0045	0046	0047	0047	0048
40	.0040	0041	0041	0042	0043	0044	0044	0045	0046	0047	0047
35 0	.0039	0040	0041	0041	0042	0043	0044	0044	0045	0046	0047
20	.0039	0039	0040	0041	0042	0042	0043	0044	0044	0045	0046
40	.0038	0039	0039	0040	0041	0042	0042	0043	0044	0044	0045
36 0	.0037	0038	0039	0040	0040	0041	0042	0042	0043	0044	0044
20	.0037	0038	0038	0039	0040	0040	0041	0042	0042	0043	0044
40	.0036	0037	0038	0038	0039	0040	0040	0041	0042	0042	0043
37 0	.0036	0036	0037	0038	0038	0039	0040	0040	0041	0042	0042
20	.0035	0036	0037	0037	0038	0039	0039	0040	0040	0041	0042
40	.0035	0035	0036	0037	0037	0038	0039	0039	0040	0040	0041
38 0	.0034	0035	0035	0036	0037	0037	0038	0039	0039	0040	0040
20	.0034	0034	0035	0036	0036	0037	0037	0038	0039	0039	0040
40	.0033	0034	0034	0035	0036	0036	0037	0037	0038	0039	0039
39 0		0033	0034	0034	0035	0036	0036	0037	0037	0038	0039
20		0033	0033	0034	0035	0035	0036	0036	0037	0037	0038
40		0032	0033	0033	0034	0035	0035	0036	0036	0037	0037
40 0		0032	0032	0033	0033	0034	0035	0035	0036	0036	0037
20		0031	0032	0032	0033	0034	0034	0035	0035	0036	0036
40		0031	0031	0032	0032	0033	0034	0034	0035	0035	0036
41 0		0030	0031	0031	0032	0033	0033	0034	0034	0035	0035
20		0030	0030	0031	0031	0032	0033	0033	0034	0034	0035
40		0029	0030	0030	0031	0032	0032	0033	0033	0034	0034
42 0		0029	0029	0030	0031	0031	0032	0032	0033	0033	0034
20		0029	0029	0030	0030	0031	0031	0032	0032	0033	0033
40		0028	0029	0029	0030	0030	0031	0031	0032	0032	0033
43 0		0028	0028	0029	0029	0030	0030	0031	0031	0032	0032
20		0027	0028	0028	0029	0029	0030	0030	0031	0031	0032
40		0027	0027	0028	0028	0029	0029	0030	0030	0031	0031
44 0		0026	0027	0027	0028	0028	0029	0029	0030	0030	0031
20		0026	0026	0027	0027	0028	0028	0029	0029	0030	0030
40		0026	0026	0026	0027	0027	0028	0028	0029	0029	0030
45 0		0025	0026	0026	0027	0027	0027	0028	0028	0029	0029

Log. A, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	Reduced parallax and refraction of moon.								
	51′	52′	53′	54′	55′	56′	57′	58′	59′	60′
45° 0′	.0025	0026	0026	0027	0027	0027	0028	0028	0029	0029
30	.0025	0025	0025	0026	0026	0027	0027	0028	0028	0028
46 0	.0024	0024	0025	0025	0026	0026	0027	0027	0027	0028
30	.0023	0024	0024	0025	0025	0026	0026	0026	0027	0027
47 0	.0023	0023	0024	0024	0025	0025	0025	0026	0026	0026
30	.0022	0023	0023	0024	0024	0024	0025	0025	0025	0026
48 0	.0022	0022	0023	0023	0023	0024	0024	0024	0025	0025
30	.0021	0022	0022	0022	0023	0023	0024	0024	0024	0025
49 0	.0021	0021	0022	.0022	0022	0023	0023	0023	0024	0024
30	.0020	0021	0021	0021	0022	0022	0022	0023	0023	0023
50 0	.0020	0020	0020	0021	0021	0022	0022	0022	0023	0023
30	.0019	0020	0020	0020	0021	0021	0021	0022	0022	0022
51 0	.0019	0019	0020	0020	0020	0020	0021	0021	0021	0022
30	.0018	0019	0019	0019	0020	0020	0020	0021	0021	0021
52 0	.0018	0018	0019	0019	0019	0019	0020	0020	0020	0021
30	.0018	0018	0018	0018	0019	0019	0019	0020	0020	0020
53 0	.0017	0017	0018	0018	0018	0018	0019	0019	0019	0020
30	.0017	0017	0017	0017	0018	0018	0018	0019	0019	0019
54 0	.0016	0016	0017	0017	0017	0018	0018	0018	0018	0019
30	.0016	0016	0016	0017	0017	0017	0017	0018	0018	0018
55 0	.0015	0016	0016	0016	0016	0017	0017	0017	0017	0018
30	.0015	0015	0015	0016	0016	0016	0016	0017	0017	0017
56 0	.0015	0015	0015	0015	0016	0016	0016	0016	0017	0017
30	.0014	0014	0015	0015	0015	0015	0016	0016	0016	0016
57 0	.0014	0014	0014	0015	0015	0015	0015	0015	0016	0016
30	.0014	0014	0014	0014	0014	0015	0015	0015	0015	0015
58 0	.0013	0013	0014	0014	0014	0014	0014	0015	0015	0015
30	.0013	0013	0013	0013	0014	0014	0014	0014	0014	0015
59 0	.0012	0013	0013	0013	0013	0013	0014	0014	0014	0014
30	.0012	0012	0012	0013	0013	0013	0013	0013	0014	0014
60	.0012	0012	0012	0012	0013	0013	0013	0013	0013	0013
61	.0011	0011	0011	0012	0012	0012	0012	0012	0012	0013
62	.0011	0011	0011	0011	0011	0011	0011	0012	0012	0012
63	.0010	0010	0010	0010	0011	0011	0011	0011	0011	0011
64	.0009	0010	0010	0010	0010	0010	0010	0010	0010	0011
65	.0009	0009	0009	0009	0009	0009	0010	0010	0010	0010
66	.0008	0008	0009	0009	0009	0009	0009	0009	0009	0009
67	.0008	0008	0008	0008	0008	0008	0008	0009	0009	0009
68	.0007	0007	0008	0008	0008	0008	0008	0008	0008	0008
69	.0007	0007	0007	0007	0007	0007	0007	0008	0008	0008
70	.0007	0007	0007	0007	0007	0007	0007	0007	0007	0007
71	.0006	0006	0006	0006	0006	0006	0007	0007	0007	0007
72	.0006	0006	0006	0006	0006	0006	0006	0006	0006	0006
73	.0005	0005	0006	0006	0006	0006	0006	0006	0006	0006
74	.0005	0005	0005	0005	0005	0005	0005	0005	0005	0006
75	.0005	0005	0005	0005	0005	0005	0005	0005	0005	0005
76	.0004	0005	0005	0005	0005	0005	0005	0005	0005	0005
77	.0004	0004	0004	0004	0004	0004	0004	0004	0004	0004
78	.0004	0004	0004	0004	0004	0004	0004	0004	0004	0004
79	.0004	0004	0004	0004	0004	0004	0004	0004	0004	0004
80	.0004	0004	0004	0004	0004	0004	0004	0004	0004	0004
81	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003
82	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003
83	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003
84	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003
85	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003
86	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003
87	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003
88	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003
89	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003
90	.0003	0003	0003	0003	0003	0003	0003	0003	0003	0003

APPENDIX V: TABLE III.

Log. B, for computing the First Correction of the Lunar Distance.

App. alt. of sun or star.	Reduced refraction and parallax of sun or star. 0′ 0″	0′ 30″	1′ 0″	1′ 30″	2′ 0″	2′ 30″	3′ 0″	3′ 30″	4′ 0″	4′ 30″	5′ 0″	5′ 30″
5° 0′												
10												
20												
30												
40												
50												
6 0												
20												9. 9970
40												9. 9972
7 0											9. 9976	9. 9974
20											9. 9977	9. 9975
40										9. 9981	9. 9978	9. 9976
8 0										9. 9982	9. 9979	9. 9977
20										9. 9982	9. 9980	9. 9978
40										9. 9983	9. 9981	9. 9979
9 0									9. 9986	9. 9984	9. 9982	9. 9980
20									9. 9986	9. 9985	9. 9983	9. 9981
40									9. 9987	9. 9985	9. 9983	9. 9982
10								9. 9989	9. 9988	9. 9986	9. 9984	9. 9982
11							9. 9992	9. 9991	9. 9989	9. 9987	9. 9986	9. 9984
12							9. 9993	9. 9992	9. 9990	9. 9989	9. 9987	9. 9986
13						9. 9995	9. 9994	9. 9992	9. 9991	9. 9990	9. 9989	9. 9987
14						9. 9995	9. 9994	9. 9993	9. 9992	9. 9991	9. 9990	
15					9. 9997	9. 9996	9. 9995	9. 9994	9. 9993	9. 9992	9. 9991	
16					9. 9997	9. 9996	9. 9995	9. 9994	9. 9993	9. 9993		
18				9. 9999	9. 9998	9. 9997	9. 9996	9. 9995	9. 9995			
20			0. 0000	9. 9999	9. 9998	9. 9998	9. 9997	9. 9996	9. 9996			
25			0. 0000	0. 0000	9. 9999	9. 9999	9. 9998	9. 9998				
30		0. 0001	0. 0001	0. 0000	0. 0000	0. 0000	9. 9999					
50	0. 0001	0. 0001	0. 0001	0. 0001	0. 0001	0. 0001						
90	0. 0001	0. 0002	0. 0002	0. 0002								

App. alt. of sun or star.	Reduced refraction and parallax of sun or star. 6′ 0″	6′ 30″	7′ 0″	7′ 30″	8′ 0″	8′ 30″	9′ 0″	9′ 30″	10′ 0″	10′ 30″	11′ 0″	11′ 30″
5° 0′			9. 9951	9. 9947	9. 9944	9. 9940	9. 9937	9. 9933	9. 9929	9. 9926	9. 9922	9. 9919
10			9. 9953	9. 9949	9. 9946	9. 9942	9. 9939	9. 9935	9. 9932	9. 9928	9. 9925	9. 9921
20			9. 9954	9. 9951	9. 9948	9. 9944	9. 9941	9. 9937	9. 9934	9. 9931	9. 9927	9. 9924
30		9. 9959	9. 9956	9. 9952	9. 9949	9. 9946	9. 9943	9. 9939	9. 9936	9. 9933	9. 9929	
40		9. 9960	9. 9957	9. 9954	9. 9951	9. 9948	9. 9944	9. 9941	9. 9938	9. 9935	9. 9932	
50	9. 9965	9. 9962	9. 9958	9. 9955	9. 9952	9. 9949	9. 9946	9. 9943	9. 9940	9. 9937		
6 0	9. 9966	9. 9963	9. 9960	9. 9957	9. 9954	9. 9951	9. 9948	9. 9945	9. 9942	9. 9939		
20	9. 9968	9. 9965	9. 9962	9. 9959	9. 9956	9. 9954	9. 9951	9. 9948	9. 9945			
40	9. 9969	9. 9967	9. 9964	9. 9961	9. 9959	9. 9956	9. 9953	9. 9951	9. 9948			
7 0	9. 9971	9. 9968	9. 9966	9. 9963	9. 9961	9. 9958	9. 9956	9. 9953				
20	9. 9972	9. 9970	9. 9968	9. 9965	9. 9963	9. 9960	9. 9958					
40	9. 9974	9. 9971	9. 9969	9. 9967	9. 9965	9. 9962						
8 0	9. 9975	9. 9973	9. 9971	9. 9968	9. 9966	9. 9964						
20	9. 9976	9. 9974	9. 9972	9. 9970	9. 9968							
40	9. 9977	9. 9975	9. 9973	9. 9971								
9 0	9. 9978	9. 9976	9. 9974	9. 9972								
20	9. 9979	9. 9977	9. 9975									
40	9. 9980	9. 9978	9. 9976									
10	9. 9981	9. 9979	9. 9977									
11	9. 9983	9. 9981										
12	9. 9985											
13												
14												
15												
16												
18												
20												
25												
30												
50												
90												

APPENDIX V: TABLE IV.

Log. C, for computing the First Correction of the Lunar Distance.

App. alt. of sun or star.	Reduced refraction and parallax of sun or star.											
	0′ 0″	0′ 30″	1′ 0″	1′ 30″	2′ 0″	2′ 30″	3′ 0″	3′ 30″	4′ 0″	4′ 30″	5′ 0″	5′ 30″
5° 0′												
20												
40												
6 0												
20												9.9969
40												9.9970
7											9.9974	9.9972
8										9.9980	9.9978	9.9975
9									9.9984	9.9982	9.9980	9.9978
10								9.9988	9.9986	9.9984	9.9982	9.9981
11							9.9990	9.9989	9.9987	9.9986	9.9984	9.9982
12							9.9991	9.9990	9.9988	9.9987	9.9985	9.9984
13						9.9993	9.9992	9.9991	9.9989	9.9988	9.9987	9.9985
14						9.9994	9.9993	9.9991	9.9990	9.9989	9.9988	
15					9.9995	9.9994	9.9993	9.9992	9.9991	9.9990	9.9989	
16					9.9996	9.9995	9.9994	9.9993	9.9992	9.9990		
17					9.9996	9.9995	9.9994	9.9993	9.9992	9.9991		
18				9.9997	9.9996	9.9995	9.9994	9.9994	9.9993			
20			9.9998	9.9998	9.9997	9.9996	9.9995	9.9994	9.9993			
25			9.9999	9.9998	9.9998	9.9997	9.9996	9.9996				
30		0.0000	9.9999	9.9999	9.9998	9.9998	9.9997					
40		0.0000	9.9999	9.9999	9.9999	9.9999						
50	0.0000	0.0000	0.0000	9.9999	9.9999							
90	0.0000	0.0000	0.0000	0.0000								

App. alt. of sun or star.	Reduced refraction and parallax of sun or star.											
	6′ 0″	6′ 30″	7′ 0″	7′ 30″	8′ 0″	8′ 30″	9′ 0″	9′ 30″	10′ 0″	10′ 30″	11′ 0″	11′ 30″
5° 0′			9.9949	9.9946	9.9942	9.9938	9.9935	9.9931	9.9927	9.9924	9.9920	9.9916
20		9.9956	9.9953	9.9949	9.9946	9.9942	9.9939	9.9936	9.9932	9.9929	9.9925	9.9922
40	9.9962	9.9959	9.9955	9.9952	9.9949	9.9946	9.9943	9.9939	9.9936	9.9933	9.9930	
6 0	9.9964	9.9961	9.9958	9.9955	9.9952	9.9949	9.9946	9.9943	9.9940	9.9937		
20	9.9966	9.9963	9.9960	9.9957	9.9955	9.9952	9.9949	9.9946	9.9943			
40	9.9968	9.9965	9.9962	9.9960	9.9957	9.9954	9.9951	9.9949	9.9946			
7	9.9969	9.9967	9.9964	9.9962	9.9959	9.9956	9.9954	9.9951				
8	9.9973	9.9971	9.9969	9.9966	9.9964	9.9962	9.9960					
9	9.9976	9.9974	9.9972	9.9970	9.9968							
10	9.9979	9.9977	9.9975									
11	9.9981	9.9979										
12	9.9983											
13												
14												
15												
16												
17												
18												
20												
25												
30												
40												
50												
90												

APPENDIX V: TABLE V.

Log. D, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	Reduced parallax and refraction of moon.														
	41′	42′	43′	44′	45′	46′	47′	48′	49′	50′	51′	52′	53′	54′	55′
5° 0′	.0283	0290	0296	0303	0310	0316	0323	0329	0336	0343	0349	0356	0362	0369	
3	.0280	0287	0293	0300	0307	0313	0320	0326	0333	0339	0346	0352	0359	0365	
6	.0277	0284	0291	0297	0304	0310	0317	0323	0330	0336	0342	0349	0355	0362	
9	.0275	0281	0288	0294	0301	0307	0313	0320	0326	0333	0339	0345	0352	0358	
12	.0272	0279	0285	0291	0298	0304	0310	0317	0323	0330	0336	0342	0349	0355	
5 15	.0270	0276	0282	0289	0295	0301	0308	0314	0320	0326	0333	0339	0345	0351	
18	.0267	0273	0280	0286	0292	0298	0305	0311	0317	0323	0330	0336	0342	0348	
21	.0264	0271	0277	0283	0289	0296	0302	0308	0314	0320	0327	0333	0339	0345	
24	.0262	0268	0274	0281	0287	0293	0299	0305	0311	0317	0324	0330	0336	0342	
27	.0260	0266	0272	0278	0284	0290	0296	0302	0308	0314	0321	0327	0333	0339	
5 30	.0257	0263	0269	0275	0282	0288	0294	0300	0306	0312	0318	0324	0330	0336	
33	.0255	0261	0267	0273	0279	0285	0291	0297	0303	0309	0315	0321	0327	0333	
36	.0253	0259	0265	0271	0276	0282	0288	0294	0300	0306	0312	0318	0324	0330	
39		0256	0262	0268	0274	0280	0286	0292	0298	0303	0309	0315	0321	0327	
42		0254	0260	0266	0272	0277	0283	0289	0295	0301	0306	0312	0318	0324	
5 45		0252	0258	0263	0269	0275	0281	0287	0292	0298	0304	0310	0315	0321	
48		0250	0255	0261	0267	0273	0278	0284	0290	0295	0301	0307	0313	0318	
51		0247	0253	0259	0265	0270	0276	0282	0287	0293	0299	0304	0310	0316	
54		0245	0251	0257	0262	0268	0274	0279	0285	0290	0296	0302	0307	0313	
57		0243	0249	0254	0260	0266	0271	0277	0282	0288	0294	0299	0305	0310	
6 0		0241	0247	0252	0258	0263	0269	0275	0280	0286	0291	0297	0302	0308	
3		0239	0245	0250	0256	0261	0267	0272	0278	0283	0289	0294	0300	0305	
6		0237	0243	0248	0254	0259	0265	0270	0275	0281	0286	0292	0297	0302	
9		0235	0241	0246	0252	0257	0262	0268	0273	0279	0284	0289	0295	0300	
12		0233	0239	0244	0249	0255	0260	0266	0271	0276	0282	0287	0292	0298	
6 15		0231	0237	0242	0247	0253	0258	0263	0269	0274	0279	0285	0290	0295	
18		0230	0235	0240	0245	0251	0256	0261	0267	0272	0277	0282	0288	0293	
21		0228	0233	0238	0243	0249	0254	0259	0264	0270	0275	0280	0285	0290	
24		0226	0231	0236	0342	0247	0252	0257	0262	0267	0273	0278	0283	0288	
27			0229	0234	0240	0245	0250	0255	0260	0265	0271	0276	0281	0286	0291
6 30			0227	0233	0238	0243	0248	0253	0258	0263	0268	0274	0279	0284	0289
33			0226	0231	0236	0241	0246	0251	0256	0261	0266	0271	0276	0281	0287
36			0224	0229	0234	0239	0244	0249	0254	0259	0264	0269	0274	0279	0284
39			0222	0227	0232	0237	0242	0247	0252	0257	0262	0267	0272	0277	0282
42			0220	0225	0230	0235	0240	0245	0250	0255	0260	0265	0270	0275	0280
6 45			0219	0224	0229	0234	0239	0244	0248	0253	0258	0263	0268	0273	0278
48			0217	0222	0227	0232	0237	0242	0247	0251	0256	0261	0266	0271	0276
51			0216	0220	0225	0230	0235	0240	0245	0250	0254	0259	0264	0269	0274
54			0214	0219	0224	0228	0233	0238	0243	0248	0253	0257	0262	0267	0272
57			0212	0217	0222	0227	0232	0236	0241	0246	0251	0255	0260	0265	0270
7 0			0211	0216	0220	0225	0230	0235	0239	0244	0249	0254	0258	0263	0268
3			0209	0214	0219	0223	0228	0233	0238	0242	0247	0252	0256	0261	0266
6			0208	0212	0217	0222	0227	0231	0236	0241	0245	0250	0255	0259	0264
9				0211	0216	0220	0225	0230	0234	0239	0243	0248	0253	0257	0262
12				0209	0214	0219	0223	0228	0232	0237	0242	0246	0251	0255	0260
7 15				0208	0212	0217	0222	0226	0231	0235	0240	0245	0249	0254	0258
18				0206	0211	0216	0220	0225	0229	0234	0238	0243	0247	0252	0256
21				0205	0209	0214	0219	0223	0228	0232	0237	0241	0246	0250	0255
24				0204	0208	0213	0217	0222	0226	0230	0235	0239	0244	0248	0253
27				0202	0207	0211	0216	0220	0224	0229	0233	0238	0242	0247	0251
7 30				0201	0205	0210	0214	0218	0223	0227	0232	0236	0241	0245	0249
33				0199	0204	0208	0213	0217	0221	0226	0230	0234	0239	0243	0248
36				0198	0202	0207	0211	0215	0220	0224	0229	0233	0237	0242	0246
39				0197	0201	0205	0210	0214	0218	0223	0227	0231	0236	0240	0244
42				0195	0200	0204	0208	0213	0217	0221	0225	0230	0234	0238	0243
7 45				0194	0198	0203	0207	0211	0215	0220	0224	0228	0232	0237	0241
48				0193	0197	0201	0205	0210	0214	0218	0222	0227	0231	0235	0239
51				0191	0196	0200	0204	0208	0213	0217	0221	0225	0229	0234	0238
54				0190	0194	0198	0203	0207	0211	0215	0219	0224	0228	0232	0236
57				0189	0193	0197	0201	0206	0210	0214	0218	0222	0226	0230	0235
8 0				0188	0192	0196	0200	0204	0208	0212	0217	0221	0225	0229	0233

APPENDIX V: TABLE V.

Log. D, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	Reduced parallax and refraction of moon.													
	45′	46′	47′	48′	49′	50′	51′	52′	53′	54′	55′	56′	57′	58′
8° 0′	.0192	0196	0200	0204	0208	0212	0217	0221	0225	0229	0233	0237		
5	.0190	0194	0198	0202	0206	0210	0214	0218	0222	0227	0231	0235		
10	.0188	0192	0196	0200	0204	0208	0212	0216	0220	0224	0228	0232		
15	.0186	0190	0194	0198	0202	0206	0210	0214	0218	0222	0226	0230		
20	.0184	0188	0192	0196	0200	0204	0207	0211	0215	0219	0223	0227		
25	.0182	0186	0190	0194	0197	0201	0205	0209	0213	0217	0221	0225		
8 30	.0180	0184	0188	0192	0195	0199	0203	0207	0211	0215	0219	0223		
35	.0178	0182	0186	0190	0193	0197	0201	0205	0209	0213	0216	0220		
40	.0176	0180	0184	0188	0191	0195	0199	0203	0207	0210	0214	0218		
45	.0174	0178	0182	0186	0189	0193	0197	0201	0205	0208	0212	0216		
50	.0173	0176	0180	0184	0188	0191	0195	0199	0202	0206	0210	0214		
55	.0171	0175	0178	0182	0186	0189	0193	0197	0200	0204	0208	0212		
9 0	.0169	0173	0177	0180	0184	0188	0191	0195	0198	0202	0206	0209		
5	.0167	0171	0175	0178	0182	0186	0189	0193	0197	0200	0204	0207		
10	.0166	0169	0173	0177	0180	0184	0187	0191	0195	0198	0202	0205		
15	.0164	0168	0171	0175	0179	0182	0186	0189	0193	0196	0200	0203		
20	.0163	0166	0170	0173	0177	0180	0184	0187	0191	0194	0198	0201		
25	.0161	0165	0168	0172	0175	0179	0182	0186	0189	0193	0196	0199		
9 30		0163	0166	0170	0173	0177	0180	0184	0187	0191	0194	0198		
35		0161	0165	0168	0172	0175	0179	0182	0185	0189	0192	0196		
40		0160	0163	0167	0170	0174	0177	0180	0184	0187	0191	0194		
45		0158	0162	0165	0169	0172	0175	0179	0182	0185	0189	0192	0195	
50		0157	0160	0164	0167	0170	0174	0177	0180	0184	0187	0190	0194	
55		0156	0159	0162	0165	0169	0172	0175	0179	0182	0185	0189	0192	
10 0		0154	0157	0161	0164	0167	0171	0174	0177	0180	0184	0187	0190	
5		0153	0156	0159	0162	0166	0169	0172	0175	0179	0182	0185	0188	
10		0151	0155	0158	0161	0164	0167	0171	0174	0177	0180	0183	0187	
15		0150	0153	0156	0160	0163	0166	0169	0172	0175	0179	0182	0185	
20		0149	0152	0155	0158	0161	0164	0168	0171	0174	0177	0180	0183	
25		0147	0150	0154	0157	0160	0163	0166	0169	0172	0175	0179	0182	
10 30		0146	0149	0152	0155	0158	0162	0165	0168	0171	0174	0177	0180	
35		0145	0148	0151	0154	0157	0160	0163	0166	0169	0172	0175	0179	
40		0143	0147	0150	0153	0156	0159	0162	0165	0168	0171	0174	0177	
45		0142	0145	0148	0151	0154	0157	0160	0163	0166	0169	0172	0175	
50		0141	0144	0147	0150	0153	0156	0159	0162	0165	0168	0171	0174	
55		0140	0143	0146	0149	0152	0155	0158	0161	0164	0167	0170	0172	
11 0		0139	0142	0145	0147	0150	0153	0156	0159	0162	0165	0168	0171	
5		0137	0140	0143	0146	0149	0152	0155	0158	0161	0164	0167	0170	
10			0139	0142	0145	0148	0151	0154	0157	0159	0162	0165	0168	
15			0138	0141	0144	0147	0150	0152	0155	0158	0161	0164	0167	
20			0137	0140	0143	0145	0148	0151	0154	0157	0160	0163	0165	
25			0136	0139	0141	0144	0147	0150	0153	0156	0158	0161	0164	
11 30			0135	0137	0140	0143	0146	0149	0151	0154	0157	0160	0163	
35			0133	0136	0139	0142	0145	0147	0150	0153	0156	0159	0161	
40			0132	0135	0138	0141	0143	0146	0149	0152	0154	0157	0160	
45			0131	0134	0137	0140	0142	0145	0148	0150	0153	0156	0159	
50			0130	0133	0136	0138	0141	0144	0147	0149	0152	0155	0157	
55			0129	0132	0135	0137	0140	0143	0145	0148	0151	0153	0156	
12 0			0128	0131	0134	0136	0139	0142	0144	0147	0150	0152	0155	
5			0127	0130	0132	0135	0138	0140	0143	0146	0148	0151	0154	
10			0126	0129	0131	0134	0137	0139	0142	0145	0147	0150	0152	
15			0125	0128	0130	0133	0136	0138	0141	0143	0146	0149	0151	
20			0124	0127	0129	0132	0135	0137	0140	0142	0145	0147	0150	
25			0123	0126	0128	0131	0133	0136	0139	0141	0144	0146	0149	
12 30			0122	0125	0127	0130	0132	0135	0138	0140	0143	0145	0148	
35			0121	0124	0126	0129	0131	0134	0136	0139	0141	0144	0147	
40			0120	0123	0125	0128	0130	0133	0135	0138	0140	0143	0145	
45			0119	0122	0124	0127	0129	0132	0134	0137	0139	0142	0144	0147
50			0118	0121	0123	0126	0128	0131	0133	0136	0138	0141	0143	0146
55			0118	0120	0123	0125	0127	0130	0132	0135	0137	0140	0142	0145
13 0			0117	0119	0122	0124	0126	0129	0131	0134	0136	0139	0141	0143

APPENDIX V: TABLE V.

Log. D, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	47′	48′	49′	50′	51′	52′	53′	54′	55′	56′	57′	58′	59′
	Reduced parallax and refraction of moon.												
13° 0′	.0117	0119	0122	0124	0126	0129	0131	0134	0136	0139	0141	0143	
10	.0115	0117	0120	0122	0125	0127	0129	0132	0134	0137	0139	0141	
20	.0113	0116	0118	0120	0123	0125	0127	0130	0132	0134	0137	0139	
30	.0112	0114	0116	0119	0121	0123	0125	0128	0130	0132	0135	0137	
40		0112	0114	0117	0119	0121	0124	0126	0128	0131	0133	0135	
50		0111	0113	0115	0117	0120	0122	0124	0126	0129	0131	0133	
14 0		0109	0111	0113	0116	0118	0120	0122	0125	0127	0129	0131	
10		0107	0110	0112	0114	0116	0118	0121	0123	0125	0127	0129	
20		0106	0108	0110	0112	0114	0117	0119	0121	0123	0125	0127	
30		0104	0106	0109	0111	0113	0115	0117	0119	0121	0123	0126	
40		0103	0105	0107	0109	0111	0113	0115	0118	0120	0122	0124	
50		0101	0103	0106	0108	0110	0112	0114	0116	0118	0120	0122	
15 0		0100	0102	0104	0106	0108	0110	0112	0114	0116	0118	0120	
10		0099	0101	0103	0105	0107	0109	0111	0113	0115	0117	0119	
20		0097	0099	0101	0103	0105	0107	0109	0111	0113	0115	0117	
30		0096	0098	0100	0102	0104	0106	0108	0110	0112	0113	0115	
40		0094	0096	0098	0100	0102	0104	0106	0108	0110	0112	0114	
50		0093	0095	0097	0099	0101	0103	0105	0107	0108	0110	0112	
16 0		0092	0094	0096	0098	0099	0101	0103	0105	0107	0109	0111	
10		0091	0093	0094	0096	0098	0100	0102	0104	0106	0107	0109	
20		0089	0091	0093	0095	0097	0099	0100	0102	0104	0106	0108	
30		0088	0090	0092	0094	0096	0097	0099	0101	0103	0105	0106	
40		0087	0089	0091	0092	0094	0096	0098	0100	0101	0103	0105	
50		0086	0088	0089	0091	0093	0095	0096	0098	0100	0102	0104	
17 0		0085	0087	0088	0090	0092	0093	0095	0097	0099	0100	0102	
10		0084	0085	0087	0089	0091	0092	0094	0096	0097	0099	0101	
20		0083	0084	0086	0088	0089	0091	0093	0094	0096	0098	0099	
30			0083	0085	0086	0088	0090	0091	0093	0095	0096	0098	
40			0082	0084	0085	0087	0089	0090	0092	0094	0095	0097	
50			0081	0083	0084	0086	0087	0089	0091	0092	0094	0096	
18 0			0080	0082	0083	0085	0086	0088	0090	0091	0093	0094	
20			0078	0079	0081	0083	0084	0086	0087	0089	0090	0092	0093
40			0076	0077	0079	0080	0082	0083	0085	0087	0088	0090	0091
19 0			0074	0075	0077	0078	0080	0081	0083	0084	0086	0087	0089
20			0072	0073	0075	0076	0078	0079	0081	0082	0084	0085	0086
40			0070	0072	0073	0074	0076	0077	0079	0080	0081	0083	0084
20 0			0068	0070	0071	0073	0074	0075	0077	0078	0079	0081	0082
20			0067	0068	0069	0071	0072	0073	0075	0076	0077	0079	0080
40			0065	0066	0068	0069	0070	0072	0073	0074	0075	0077	0078
21 0			0063	0065	0066	0067	0068	0070	0071	0072	0074	0075	0076
20			0062	0063	0064	0065	0067	0068	0069	0070	0072	0073	0074
40			0060	0061	0063	0064	0065	0066	0067	0069	0070	0071	0072
22 0			0059	0060	0061	0062	0063	0065	0066	0067	0068	0069	0070
20			0057	0058	0059	0061	0062	0063	0064	0065	0066	0068	0069
40			0056	0057	0058	0059	0060	0061	0062	0064	0065	0066	0067
23 0			0054	0055	0057	0058	0059	0060	0061	0062	0063	0064	0065
20			0053	0054	0055	0056	0057	0058	0059	0060	0061	0063	0064
40			0052	0053	0054	0055	0056	0057	0058	0059	0060	0061	0062
24 0			0050	0051	0052	0053	0054	0055	0056	0057	0058	0059	0060
20				0050	0051	0052	0053	0054	0055	0056	0057	0058	0059
40				0049	0050	0051	0052	0053	0053	0054	0055	0056	0057
25 0				0047	0048	0049	0050	0051	0052	0053	0054	0055	0056
20				0046	0047	0048	0049	0050	0051	0052	0053	0053	0054
40				0045	0046	0047	0048	0049	0049	0050	0051	0052	0053
26 0				0044	0045	0046	0046	0047	0048	0049	0050	0051	0052
20				0043	0043	0044	0045	0046	0047	0048	0048	0049	0050
40				0041	0042	0043	0044	0045	0046	0046	0047	0048	0049
27 0				0040	0041	0042	0043	0044	0044	0045	0046	0047	0047
20				0039	0040	0041	0042	0042	0043	0044	0045	0045	0046
40				0038	0039	0040	0040	0041	0042	0043	0043	0044	0045
28 0				0037	0038	0039	0039	0040	0041	0042	0042	0043	0044

Log. D, for computing the First Correction of the Lunar Distance.

App. alt. of moon.	Reduced parallax and refraction of moon. 50′	51′	52′	53′	54′	55′	56′	57′	58′	59′	60′
28° 0′	0.0037	0.0038	0.0039	0.0039	0.0040	0.0041	0.0042	0.0042	0.0043	0.0044	
30	0.0036	0.0036	0.0037	0.0038	0.0038	0.0039	0.0040	0.0040	0.0041	0.0042	
29 0	0.0034	0.0035	0.0035	0.0036	0.0037	0.0037	0.0038	0.0039	0.0039	0.0040	
30	0.0033	0.0033	0.0034	0.0035	0.0035	0.0036	0.0036	0.0837	0.0038	0.0038	
30 0	0.0031	0.0032	0.0032	0.0033	0.0034	0.0034	0.0035	0.0035	0.0036	0.0037	
30	0.0030	0.0030	0.0031	0.0031	0.0032	0.0033	0.0033	0.0034	0.0034	0.0035	
31 0	0.0028	0.0029	0.0029	0.0030	0.0031	0.0031	0.0032	0.0032	0.0033	0.0033	
30	0.0027	0.0028	0.0028	0.0029	0.0029	0.0030	0.0030	0.0031	0.0031	0.0032	0.0032
32 0	0.0026	0.0026	0.0027	0.0027	0.0028	0.0028	0.0029	0.0029	0.0030	0.0030	0.0031
30	0.0024	0.0025	0.0025	0.0026	0.0026	0.0027	0.0027	0.0028	0.0028	0.0029	0.0029
33 0	0.0023	0.0024	0.0024	0.0025	0.0025	0.0025	0.0026	0.0026	0.0027	0.0027	0.0028
30	0.0022	0.0022	0.0023	0.0023	0.0024	0.0024	0.0025	0.0025	0.0025	0.0026	0.0026
34 0	0.0021	0.0021	0.0022	0.0022	0.0022	0.0023	0.0023	0.0024	0.0024	0.0024	0.0025
30	0.0020	0.0020	0.0020	0.0021	0.0021	0.0022	0.0022	0.0022	0.0023	0.0023	0.0023
35 0	0.0018	0.0019	0.0019	0.0020	0.0020	0.0020	0.0021	0.0021	0.0021	0.0022	0.0022
30	0.0017	0.0018	0.0018	0.0018	0.0019	0.0019	0.0019	0.0020	0.0020	0.0020	0.0021
36 0	0.0016	0.0017	0.0017	0.0017	0.0018	0.0018	0.0018	0.0019	0.0019	0.0019	0.0019
30	0.0015	0.0016	0.0016	0.0016	0.0016	0.0017	0.0017	0.0017	0.0018	0.0018	0.0018
37 0	0.0014	0.0014	0.0015	0.0015	0.0015	0.0016	0.0016	0.0016	0.0016	0.0017	0.0017
30	0.0013	0.0013	0.0014	0.0014	0.0014	0.0014	0.0015	0.0015	0.0015	0.0015	0.0016
38 0	0.0012	0.0012	0.0013	0.0013	0.0013	0.0013	0.0014	0.0014	0.0014	0.0014	0.0014
30	0.0011	0.0011	0.0012	0.0012	0.0012	0.0012	0.0012	0.0013	0.0013	0.0013	0.0013
39 0	0.0010	0.0010	0.0011	0.0011	0.0011	0.0011	0.0011	0.0012	0.0012	0.0012	0.0012
30		0.0009	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0011	0.0011	0.0011
40		0.0008	0.0009	0.0009	0.0009	0.0009	0.0009	0.0009	0.0010	0.0010	0.0010
41		0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0008	0.0008
42		0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0006
43		0.0003	0.0003	0.0003	0.0003	0.0003	0.0003	0.0003	0.0003	0.0003	0.0004
44		0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0002	0.0002	0.0002	0.0002
45		0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
46		9.9998	9.9998	9.9998	9.9998	9.9998	9.9998	9.9998	9.9998	9.9998	9.9998
47		9.9997	9.9997	9.9997	9.9997	9.9996	9.9996	9.9996	9.9996	9.9996	9.9996
48		9.9995	9.9995	9.9995	9.9995	9.9995	9.9995	9.9995	9.9995	9.9994	9.9994
49		9.9994	9.9994	9.9994	9.9993	9.9993	9.9993	9.9993	9.9993	9.9993	9.9993
50		9.9992	9.9992	9.9992	9.9992	9.9992	9.9992	9.9992	9.9991	9.9991	9.9991
51		9.9991	9.9991	9.9991	9.9991	9.9990	9.9990	9.9990	9.9990	9.9990	9.9990
52		9.9990	9.9990	9.9990	9.9989	9.9989	9.9989	9.9989	9.9989	9.9988	9.9988
53		9.9989	9.9988	9.9988	9.9988	9.9988	9.9988	9.9987	9.9987	9.9987	9.9987
54		9.9988	9.9987	9.9987	9.9987	9.9987	9.9986	9.9986	9.9986	9.9986	9.9985
55		9.9986	9.9986	9.9986	9.9986	9.9985	9.9985	9.9985	9.9984	9.9984	9.9984
56		9.9985	9.9985	9.9985	9.9984	9.9984	9.9984	9.9984	9.9983	9.9983	9.9983
57		9.9984	9.9984	9.9984	9.9983	9.9983	9.9983	9.9982	9.9982	9.9982	9.9981
58		9.9983	9.9983	9.9983	9.9982	9.9982	9.9982	9.9981	9.9981	9.9981	9.9980
59		9.9982	9.9982	9.9981	9.9981	9.9981	9.9980	9.9980	9.9980	9.9979	9.9979
60		9.9981	9.9981	9.9980	9.9980	9.9980	9.9979	9.9979	9.9979	9.9978	9.9978
61		9.9980	9.9980	9.9980	9.9979	9.9979	9.9978	9.9978	9.9978	9.9977	9.9977
62		9.9979	9.9979	9.9979	9.9978	9.9978	9.9977	9.9977	9.9977	9.9976	9.9976
63		9.9979	9.9978	9.9978	9.9977	9.9977	9.9976	9.9976	9.9976	9.9975	9.9975
64		9.9978	9.9977	9.9977	9.9976	9.9976	9.9976	9.9975	9.9975	9.9974	9.9974
65		9.9977	9.9977	9.9976	9.9976	9.9975	9.9975	9.9974	9.9974	9.9973	9.9972
66		9.9976	9.9976	9.9975	9.9975	9.9974	9.9974	9.9973	9.9973	9.9973	9.9972
67		9.9976	9.9975	9.9975	9.9974	9.9974	9.9973	9.9973	9.9972	9.9972	9.9971
68		9.9975	9.9974	9.9974	9.9973	9.9973	9.9972	9.9972	9.9971	9.9971	9.9970
69		9.9974	9.9974	9.9973	9.9973	9.9972	9.9972	9.9971	9.9971	9.9970	9.9970
70		9.9974	9.9973	9.9973	9.9972	9.9972	9.9971	9.9970	9.9970	9.9969	9.9969
72		9.9972	9.9972	9.9971	9.9971	9.9970	9.9970	9.9969	9.9969	9.9968	9.9968
74		9.9971	9.9971	9.9970	9.9970	9.9969	9.9969	9.9968	9.9968	9.9967	9.9966
76		9.9971	9.9970	9.9969	9.9969	9.9968	9.9968	9.9967	9.9966	9.9966	9.9965
78		9.9970	9.9969	9.9969	9.9968	9.9967	9.9967	9.9966	9.9966	9.9965	9.9964
80		9.9969	9.9969	9.9968	9.9967	9.9967	9.9966	9.9965	9.9965	9.9964	9.9964
90		9.9968	9.9967	9.9966	9.9966	9.9965	9.9964	9.9964	9.9963	9.9963	9.9962

APPENDIX V: TABLE VI.

Second Correction of the Lunar Distance.

Apparent distance.	First correction of distance. 3′	7′	10	12′	14′	16′	18′	20′	21′	22′	23′	24′	25′	26′	27′	28′	Apparent distance.
Sub.	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	Add.
15° 0′	0	2	3	5	6	8	11	13	14	16	17	19	20	22	24	26	
30	0	2	3	5	6	8	10	13	14	15	17	18	20	21	23	25	
16 0	0	1	3	4	6	8	10	12	13	15	16	18	19	21	22	24	
30	0	1	3	4	6	8	10	12	13	14	16	17	18	20	21	23	
17 0	0	1	3	4	6	7	9	11	13	14	15	16	18	19	21	22	
30	0	1	3	4	5	7	9	11	12	13	15	16	17	19	20	22	
18 0	0	1	3	4	5	7	9	11	12	13	14	15	17	18	20	21	
30	0	1	3	4	5	7	8	10	12	13	14	15	16	18	19	20	
19 0	0	1	3	4	5	6	8	10	11	12	13	15	16	17	18	20	
30	0	1	2	4	5	6	8	10	11	12	13	14	15	17	18	19	
20 0	0	1	2	3	5	6	8	10	11	12	13	14	15	16	17	19	
21	0	1	2	3	4	6	7	9	10	11	12	13	14	15	17	18	
22	0	1	2	3	4	6	7	9	10	10	11	12	14	15	16	17	
23	0	1	2	3	4	5	7	8	9	10	11	12	13	14	15	16	
24	0	1	2	3	4	5	6	8	9	9	10	11	12	13	14	15	
25	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	
26	0	1	2	3	4	5	6	7	8	9	9	10	11	12	13	14	
27	0	1	2	2	3	4	6	7	8	8	9	10	11	12	12	13	
28	0	1	2	2	3	4	5	7	7	8	9	9	10	11	12	13	
29	0	1	2	2	3	4	5	6	7	8	8	9	10	11	11	12	
30	0	1	2	2	3	4	5	6	7	7	8	9	9	10	11	12	
31	0	1	1	2	3	4	5	6	6	7	8	8	9	10	11	11	
32	0	1	1	2	3	4	5	6	6	7	7	8	9	9	10	11	
33	0	1	1	2	3	3	4	5	6	7	7	8	8	9	10	11	
34	0	1	1	2	3	3	4	5	6	6	7	7	8	9	9	10	
35	0	1	1	2	2	3	4	5	5	6	7	7	8	8	9	10	
36	0	1	1	2	2	3	4	5	5	6	6	7	8	8	9	9	
37	0	1	1	2	2	3	4	5	5	6	6	7	7	8	8	9	
38	0	1	1	2	2	3	4	4	5	5	6	6	7	8	8	9	
39	0	1	1	2	2	3	3	4	5	5	6	6	7	7	8	8	
40	0	1	1	2	2	3	3	4	5	5	6	6	7	7	8	8	140°
42	0	0	1	1	2	2	3	4	4	5	5	6	6	7	7	8	138
44	0	0	1	1	2	2	3	4	4	4	5	5	6	6	7	7	136
46	0	0	1	1	2	2	3	3	4	4	4	5	5	6	6	7	134
48	0	0	1	1	2	2	3	3	3	4	4	5	5	5	6	6	132
50	0	0	1	1	1	2	2	3	3	4	4	4	5	5	5	6	130
52	0	0	1	1	1	2	2	3	3	3	4	4	4	5	5	5	128
54	0	0	1	1	1	2	2	3	3	3	3	4	4	4	5	5	126
56	0	0	1	1	1	2	2	2	3	3	3	3	4	4	4	5	124
58	0	0	1	1	1	1	2	2	2	3	3	3	3	4	4	4	122
60	0	0	0	1	1	1	2	2	2	2	3	3	3	3	4	4	120
62	0	0	0	1	1	1	2	2	2	2	2	3	3	3	3	4	118
64	0	0	0	1	1	1	1	2	2	2	2	2	3	3	3	3	116
66	0	0	0	1	1	1	1	2	2	2	2	2	2	3	3	3	114
68	0	0	0	1	1	1	1	1	2	2	2	2	2	2	3	3	112
70	0	0	0	0	1	1	1	1	1	2	2	2	2	2	2	2	110
74	0	0	0	0	0	1	1	1	1	1	1	1	2	2	2	2	106
78	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	102
82	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	98
86	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94
90	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	90
Apparent distance.	3′	7′	10′	12′	14′	16′	18′	20′	21′	22′	23′	24′	25′	26′	27′	28′	Apparent distance.
	First correction of distance.																

Second Correction of the Lunar Distance.

Apparent distance.	First correction of distance.																Apparent distance.
	29′	30′	31′	32′	33′	34′	35′	36′	37′	38′	39′	40′	41′	42′	43′	44′	
Sub.	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	Add.
15° 0′	27	29	31	33	35	38	40	42	45	47	50	52	55	57	60	63	
30	26	28	30	32	34	36	39	41	43	45	48	50	53	56	58	61	
16 0	26	27	29	31	33	35	37	39	42	44	46	49	51	54	56	59	
30	25	27	28	30	32	34	36	38	40	43	45	47	50	52	54	57	
17 0	24	26	27	29	31	33	35	37	39	41	43	46	48	50	53	55	
30	23	25	27	28	30	32	34	36	38	40	42	44	47	49	51	54	
18 0	23	24	26	28	29	31	33	35	37	39	41	43	45	47	50	52	
30	22	23	25	27	28	30	32	34	36	38	40	42	44	46	48	50	
19 0	21	23	24	26	28	29	31	33	35	37	39	41	43	45	47	49	
30	21	22	24	25	27	28	30	32	34	36	37	39	41	43	46	48	
20	20	22	23	25	26	28	29	31	33	35	36	38	40	42	44	46	
21	19	20	22	23	25	26	28	29	31	33	35	36	38	40	42	44	
22	18	19	21	22	24	25	26	28	30	31	33	35	36	38	40	42	
23	17	19	20	21	22	24	25	27	28	30	31	33	35	36	38	40	
24	16	18	19	20	21	23	24	25	27	28	30	31	33	35	36	38	
25	16	17	18	19	20	22	23	24	26	27	28	30	31	33	35	36	
26	15	16	17	18	19	21	22	23	25	26	27	29	30	32	33	35	
27	14	15	16	18	19	20	21	22	23	25	26	27	29	30	32	33	
28	14	15	16	17	18	19	20	21	22	24	25	26	28	29	30	32	
29	13	14	15	16	17	18	19	20	22	23	24	25	26	28	29	30	
30	13	14	14	15	16	17	19	20	21	22	23	24	25	27	28	29	
31	12	13	14	15	16	17	18	19	20	21	22	23	24	26	27	28	
32	12	13	13	14	15	16	17	18	19	20	21	22	23	25	26	27	
33	11	12	13	14	15	16	16	17	18	19	20	22	23	24	25	26	
34	11	12	12	13	14	15	16	17	18	19	20	21	22	23	24	25	
35	10	11	12	13	14	14	15	16	17	18	19	20	21	22	23	24	
36	10	11	12	12	13	14	15	16	16	17	18	19	20	21	22	23	
37	10	10	11	12	13	13	14	15	16	17	18	19	19	20	21	22	
38	9	10	11	11	12	13	14	14	15	16	17	18	19	20	21	22	
39	9	10	10	11	12	12	13	14	15	16	16	17	18	19	20	21	
40	9	9	10	11	11	12	13	13	14	15	16	17	17	18	19	20	140°
42	8	9	9	10	11	11	12	13	13	14	15	16	16	17	18	19	138
44	8	8	9	9	10	10	11	12	12	13	14	14	15	16	17	17	136
46	7	8	8	9	9	10	10	11	12	12	13	13	14	15	16	16	134
48	7	7	8	8	9	9	10	10	11	11	12	13	13	14	15	15	132
50	6	7	7	8	8	8	9	9	10	11	11	12	12	13	14	14	130
52	6	6	7	7	7	8	8	9	9	10	10	11	11	12	13	13	128
54	5	6	6	6	7	7	8	8	9	9	10	10	11	11	12	12	126
56	5	5	6	6	6	7	7	8	8	9	9	9	10	10	11	11	124
58	5	5	5	6	6	6	7	7	7	8	8	9	9	10	10	11	122
60	4	5	5	5	5	6	6	7	7	7	8	8	8	9	9	10	120
62	4	4	4	5	5	5	6	6	6	7	7	7	8	8	9	9	118
64	4	4	4	4	5	5	5	6	6	6	6	7	7	8	8	8	116
66	3	4	4	4	4	4	5	5	5	6	6	6	7	7	7	8	114
68	3	3	3	4	4	4	4	5	5	5	5	6	6	6	7	7	112
70	3	3	3	3	3	4	4	4	4	5	5	5	5	6	6	6	110
74	2	2	2	3	3	3	3	3	3	4	4	4	4	4	5	5	106
78	2	2	2	2	2	2	2	2	3	3	3	3	3	3	3	4	102
82	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	98
86	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	94
90°	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	90°
Apparent distance.	29′	30	31′	32′	33′	34′	35′	36′	37′	38′	39′	40′	41′	42′	43′	44′	Apparent distance.
	First correction of distance.																

APPENDIX V: TABLE VI.

Second Correction of the Lunar Distance.

Apparent distance.	First correction of distance.																Apparent distance.
	45′	46′	47′	48′	49′	50′	51′	52′	53′	54′	55′	56′	57′	58′	59′	60′	
Sub.	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	Add.
15° 0′	66	69	72	75	78	81	85	88	91	95	99	102	106	110	113	117	
30	64	67	70	72	76	79	82	85	88	92	95	99	102	106	110	113	
16 0	62	64	67	70	73	76	79	82	85	89	92	95	99	102	106	110	
30	60	62	65	68	71	74	77	80	83	86	89	92	96	99	103	106	
17 0	58	60	63	66	69	71	74	77	80	83	86	90	93	96	99	103	
30	56	59	61	64	66	69	72	75	78	81	84	87	90	93	96	100	
18 0	54	57	59	62	64	67	70	73	75	78	81	84	87	90	94	97	
30	53	55	58	60	63	65	68	71	73	76	79	82	85	88	91	94	
19 0	51	54	56	58	61	63	66	69	71	74	77	79	82	85	88	91	
30	50	52	54	57	59	62	64	67	69	72	75	77	80	83	86	89	
20	49	51	53	55	58	60	62	65	67	70	73	75	78	81	83	86	
21	46	48	50	52	55	57	59	61	64	66	69	71	74	76	79	82	
22	44	46	48	50	52	54	56	58	61	63	65	68	70	73	75	78	
23	42	44	45	47	49	51	53	56	58	60	62	64	67	69	72	74	
24	40	41	43	45	47	49	51	53	55	57	59	61	64	66	68	71	
25	38	40	41	43	45	47	49	51	53	55	57	59	61	63	65	67	
26	36	38	40	41	43	45	47	48	50	52	54	56	58	60	62	64	
27	35	36	38	39	41	43	45	46	48	50	52	54	56	58	60	62	
28	33	35	36	38	39	41	43	44	46	48	50	51	53	55	57	59	
29	32	33	35	36	38	39	41	43	44	46	48	49	51	53	55	57	
30	31	32	33	35	36	38	39	41	42	44	46	47	49	51	53	54	
31	29	31	32	33	35	36	38	39	41	42	44	46	47	49	51	52	
32	28	30	31	32	34	35	36	38	39	41	42	44	45	47	49	50	
33	27	28	30	31	32	34	35	36	38	39	41	42	44	45	47	48	
34	26	27	29	30	31	32	34	35	36	38	39	41	42	44	45	47	
35	25	26	28	29	30	31	32	34	35	36	38	39	40	42	43	45	
36	24	25	27	28	29	30	31	32	34	35	36	38	39	40	42	43	
37	23	25	26	27	28	29	30	31	33	34	35	36	38	39	40	42	
38	23	24	25	26	27	28	29	30	31	33	34	35	36	38	39	40	
39	22	23	24	25	26	27	28	29	30	31	33	34	35	36	38	39	
40	21	22	23	24	25	26	27	28	29	30	31	33	34	35	36	37	140°
42	20	21	21	22	23	24	25	26	27	28	29	30	31	33	34	35	138
44	18	19	20	21	22	23	24	24	25	26	27	28	29	30	31	33	136
46	17	18	19	19	20	21	22	23	24	25	26	26	27	28	29	30	134
48	16	17	17	18	19	20	20	21	22	23	24	25	26	26	27	28	132
50	15	16	16	17	18	18	19	20	21	21	22	23	24	25	25	26	130
52	14	14	15	16	16	17	18	18	19	20	21	21	22	23	24	25	128
54	13	13	14	15	15	16	16	17	18	18	19	20	21	21	22	23	126
56	12	12	13	14	14	15	15	16	17	17	18	18	19	20	20	21	124
58	11	12	12	13	13	14	14	15	15	16	16	17	18	18	19	20	122
60	10	11	11	12	12	13	13	14	14	15	15	16	16	17	18	18	120
62	9	10	10	11	11	12	12	13	13	14	14	15	15	16	16	17	118
64	9	9	9	10	10	11	11	12	12	12	13	13	14	14	15	15	116
66	8	8	9	9	9	10	10	11	11	11	12	12	13	13	14	14	114
68	7	7	8	8	8	9	9	10	10	10	11	11	11	12	12	13	112
70	6	7	7	7	8	8	8	9	9	9	10	10	10	11	11	11	110
74	5	5	6	6	6	6	7	7	7	7	8	8	8	8	9	9	106
78	4	4	4	4	4	5	5	5	5	5	6	6	6	6	6	7	102
82	2	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	98
86	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	94
90°	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	90°
Apparent distance.	45′	46′	47′	48′	49′	50′	51′	52′	53′	54′	55′	56′	57′	58′	59′	60′	Apparent distance.
	First correction of distance.																

APPENDIX V: TABLE VII.

For finding the Correction of the Lunar Distance for the Contraction of the Moon's Semidiameter.

TABLE VII A.—GIVING THE ARGUMENT FOR TABLE VII B.

Red. P. and R. of moon.	Apparent altitude of moon.																						
	5°	5½°	6°	6½°	7°	7½°	8°	8½°	9°	9½°	10°	11°	12°	13°	14°	15°	16°	17°	18°	20°	25°	30°	40°	50°
41′	65	56																						
42	63	54	47	41																				
43	62	53	46	40	35																			
44	60	51	45	39	34	30	27																	
45	58	50	43	38	33	30	26	24	21	20														
46	57	49	42	37	33	29	26	23	21	19	17	15												
47	56	48	41	36	32	28	25	23	20	19	17	14	12	10										
48	54	46	40	35	31	28	25	22	20	18	17	14	12	10	9	8	7	6						
49	53	45	39	35	30	27	24	22	19	18	16	14	12	10	9	8	7	6	6	5	3			
50	52	44	38	34	30	26	24	21	19	17	16	13	11	10	9	8	7	6	5	5	3	3	2	
51	50	43	38	33	29	26	23	21	19	17	15	13	11	10	8	7	7	6	5	5	3	2	2	2
52	49	42	37	32	28	25	23	20	18	17	15	13	11	9	8	7	7	6	5	4	3	2	2	2
53	48	41	36	32	28	25	22	20	18	16	15	12	11	9	8	7	6	6	5	4	3	2	2	2
54	47	41	35	31	27	24	22	19	18	16	15	12	10	9	8	7	6	6	5	4	3	2	2	2
55			35	30	27	24	21	19	17	16	14	12	10	9	8	7	6	6	5	4	3	2	2	2
56					26	23	21	19	17	15	14	12	10	9	8	7	6	5	5	4	3	2	2	2
57								18	17	15	14	12	10	9	7	7	6	5	5	4	3	2	2	2
58											13	11	10	8	7	7	6	5	5	4	3	2	2	2
59														8	7	6	6	5	5	4	3	2	2	2
60																				4	3	2	2	2

TABLE VII B.—CONTRACTION OF MOON'S SEMI-DIAMETER.

Whole correction of moon.	Argument, number from Table VII A.																									
	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	44	48	52	56	60	64
′	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1
15	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	3	3	3
20	0	0	0	1	1	1	1	1	1	2	2	2	2	2	2	3	3	3	3	3	4	4	4	4	5	5
22	0	0	1	1	1	1	1	2	2	2	2	2	3	3	3	3	3	3	4	4	4	5	5	5	6	6
24	0	0	1	1	1	1	2	2	2	2	3	3	3	3	3	4	4	4	4	5	5	6	6	6	7	7
26	0	1	1	1	1	2	2	2	2	3	3	3	4	4	4	4	5	5	5	5	6	6	7	8	8	9
28	0	1	1	1	2	2	2	3	3	3	3	4	4	4	5	5	5	6	6	6	7	8	8	9	9	10
30	0	1	1	1	2	2	3	3	3	4	4	4	5	5	5	6	6	6	7	7	8	9	9	10	11	12
32	0	1	1	2	2	2	3	3	4	4	5	5	5	6	6	7	7	7	8	8	9	10	11	11	12	13
34	0	1	1	2	2	3	3	4	4	5	5	6	6	6	7	7	8	8	9	9	10	11	12	13	14	15
36	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	9	9	10	10	11	12	13	15	16	17
38	1	1	2	2	3	3	4	5	5	6	6	7	8	8	9	9	10	10	11	12	13	14	15	16	17	18
40	1	1	2	3	3	4	4	5	6	6	7	8	8	9	9	10	11	12	12	13	14	15	17	18	19	20
42	1	1	2	3	4	4	5	6	6	7	8	8	9	10	11	11	12	13	13	14	16	17	18	20	21	23
44	1	2	2	3	4	5	5	6	7	8	9	9	10	11	12	12	13	14	15	15	17	19	20	22	23	
45	1	2	2	3	4	5	6	6	7	8	9	10	11	11	12	13	14	15	15	16	18	19	21	23	24	
46	1	2	3	3	4	5	6	7	7	8	9	10	11	12	13	14	14	15	16	17	19	20	22	24		
47	1	2	3	4	4	5	6	7	8	9	10	11	11	12	13	14	15	16	17	18	19	21	23	25		
48	1	2	3	4	5	6	6	7	8	9	10	11	12	13	14	15	16	17	18	18	20	22	24	26		
49	1	2	3	4	5	6	7	8	9	10	11	12	12	13	14	15	16	17	18	19	21	23	25			
50	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	22	24	26			
51	1	2	3	4	5	6	7	8	9	10	11	12	14	15	16	17	18	19	20	21	23	25	27			
52	1	2	3	4	5	6	8	9	10	11	12	13	14	15	16	17	18	19	21	22	24	26				
53	1	2	3	4	6	7	8	9	10	11	12	13	15	16	17	18	19	20	21	22	25	27				
54		2	3	5	6	7	8	9	10	12	13	14	15	16	17	19	20	21	22	23	26					
55		2	4	5	6	7	8	10	11	12	13	15	16	17	18	19	21	22								
56		3	4	5	6	8	9	10	11	13	14	15	16													
57			4	5	7																					

When the *nearer* limb is observed, *substract* this correction; when the *farther*, *add*.

APPENDIX V: TABLE VIII.

For finding the Correction of the Lunar Distance for the Contraction of the Sun's Semidiameter.

TABLE VIII A.—GIVING THE ARGUMENT FOR TABLE VIII B.

Red. P. and R. of sun.	Apparent altitude of sun.																							
	5°	5½°	6°	6½°	7°	7½°	8°	8½°	9°	9½°	10°	11°	12°	13°	14°	15°	16°	17°	18°	20°	25°	30°	40°	50°
1′ 0″																							22	18
30																					30	34	24	29
2 0																			35	37	42	46	46	
30																	40	42	44	47	53	59		
3 0															44	46	49	51	53	57				
30													45	48	51	54	57	60	62	67				
4 0											45	49	52	55	59	62	65	68						
30									47	49	51	55	59	63	66	70								
5 0							47	50	52	54	57	61	66	70	74									
30					47	50	52	55	57	60	62	67	72											
6 0				49	52	55	57	60	63	66	68	74												
30			50	53	56	59	62	65	68	71	74													
7 0		51	54	58	61	64	67	70	74															
30		55	58	62	65	69	72	75																
8 0	55	59	62	66	70	73	77																	
30	59	63	66	70	74	78																		
9 0	62	66	70	74	79																			
30	66	70	74	79																				
10 0	69	74	78																					
30	73	77																						
11 0	76	81																						
30	80																							

TABLE VIII B.—CONTRACTION OF SUN'S SEMIDIAMETER.

Whole correction of sun.	Argument, number from Table VIII A.																							
	20	24	28	32	36	40	44	46	48	50	52	54	56	58	60	62	64	66	68	70	72	74	76	78
′ ″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″
0 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 0	1	1	1	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2 0			2	2	2	2	2	2	2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
30					3	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	1	1
3 0						4	4	4	3	3	3	3	3	3	3	3	3	2	2	2	2	2	2	2
30							5	5	5	4	4	4	4	4	4	4	3	3	3	3	3	3	3	3
4 0							7	6	6	6	6	5	5	5	5	5	5	4	4	4	4	4	4	4
20								7	7	7	7	6	6	6	6	5	5	5	5	5	5	5	4	4
40								9	8	8	8	7	7	7	7	6	6	6	6	6	5	5	5	5
5 0								10	9	9	9	8	8	8	8	7	7	7	7	6	6	6	6	6
20									11	10	10	9	9	9	9	8	8	8	8	7	7	7	7	7
40									12	12	11	11	10	10	10	9	9	9	9	8	8	8	8	7
6 0										13	12	12	12	11	11	10	10	10	10	9	9	9	9	8
20										14	14	13	13	12	12	12	11	11	11	10	10	10	10	9
40										16	15	15	14	14	13	13	13	12	12	11	11	11	11	10
7 0										18	17	16	16	15	15	14	14	13	13	13	12	12	12	11
20											19	18	17	17	16	16	15	15	14	14	13	13	13	12
40												20	19	18	18	17	17	16	16	15	15	14	14	14
8 0												21	21	20	19	19	18	17	17	16	16	16	15	15
20														22	21	20	20	19	18	18	17	17	16	16
40														23	23	22	21	20	20	19	19	18	18	17
9 0																24	23	22	21	21	20	20	19	19
20																	25	24	23	22	22	21	21	20
40																		25	25	24	23	23	22	22
10 0																			26	26	25	24	24	23
20																				28	27	26	25	25
40																					28	28	27	26
11 0																							29	28
20																								30

Subtract this correction from the distance.

Logarithms of Small Arcs in Space or Time.

Arc.	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
° ′ ″										
0^h 0^m 0^s		0.0000	0.3010	0.4771	0.6021	0.6990	0.7782	0.8451	0.9031	0.9542
0 10	1.0000	1.0414	1.0792	1.1139	1.1461	1.1761	1.2041	1.2304	1.2553	1.2788
0 20	1.3010	1.3222	1.3424	1.3617	1.3802	1.3979	1.4150	1.4314	1.4472	1.4624
0 30	1.4771	1.4914	1.5051	1.5185	1.5315	1.5441	1.5563	1.5682	1.5798	1.5911
0 40	1.6021	1.6128	1.6232	1.6335	1.6435	1.6532	1.6628	1.6721	1.6812	1.6902
0 50	1.6990	1.7076	1.7160	1.7243	1.7324	1.7404	1.7482	1.7559	1.7634	1.7709
0 1 0	1.7782	1.7853	1.7924	1.7993	1.8062	1.8129	1.8195	1.8261	1.8325	1.8388
1 10	1.8451	1.8513	1.8573	1.8633	1.8692	1.8751	1.8808	1.8865	1.8921	1.8976
1 20	1.9031	1.9085	1.9138	1.9191	1.9243	1.9294	1.9345	1.9395	1.9445	1.9494
1 30	1.9542	1.9589	1.9638	1.9685	1.9731	1.9777	1.9823	1.9868	1.9912	1.9956
1 40	2.0000	2.0043	2.0086	2.0128	2.0170	2.0212	2.0253	2.0294	2.0334	2.0374
1 50	2.0414	2.0453	2.0492	2.0531	2.0569	2.0607	2.0645	2.0682	2.0719	2.0755
0 2 0	2.0792	2.0828	2.0864	2.0899	2.0934	2.0969	2.1004	2.1038	2.1072	2.1106
2 10	2.1139	2.1173	2.1206	2.1239	2.1271	2.1303	2.1335	2.1367	2.1399	2.1430
2 20	2.1461	2.1492	2.1523	2.1553	2.1584	2.1614	2.1644	2.1673	2.1703	2.1732
2 30	2.1761	2.1790	2.1818	2.1847	2.1875	2.1903	2.1931	2.1959	2.1987	2.2014
2 40	2.2041	2.2068	2.2095	2.2122	2.2148	2.2175	2.2201	2.2227	2.2253	2.2279
2 50	2.2304	2.2330	2.2355	2.2380	2.2405	2.2430	2.2455	2.2480	2.2504	2.2529
0 3 0	2.2553	2.2577	2.2601	2.2625	2.2648	2.2672	2.2695	2.2718	2.2742	2.2765
3 10	2.2788	2.2810	2.2833	2.2856	2.2878	2.2900	2.2923	2.2945	2.2967	2.2989
3 20	2.3010	2.3032	2.3054	2.3075	2.3096	2.3118	2.3139	2.3160	2.3181	2.3201
3 30	2.3222	2.3243	2.3263	2.3284	2.3304	2.3324	2.3345	2.3365	2.3385	2.3404
3 40	2.3424	2.3444	2.3464	2.3483	2.3502	2.3522	2.3541	2.3560	2.3579	2.3598
3 50	2.3617	2.3636	2.3655	2.3674	2.3692	2.3711	2.3729	2.3747	2.3766	2.3784
0 4 0	2.3802	2.3820	2.3838	2.3856	2.3874	2.3892	2.3909	2.3927	2.3945	2.3962
4 10	2.3979	2.3997	2.4014	2.4031	2.4048	2.4065	2.4082	2.4099	2.4116	2.4133
4 20	2.4150	2.4166	2.4183	2.4200	2.4216	2.4232	2.4249	2.4265	2.4281	2.4298
4 30	2.4314	2.4330	2.4346	2.4362	2.4378	2.4393	2.4409	2.4425	2.4440	2.4456
4 40	2.4472	2.4487	2.4502	2.4518	2.4533	2.4548	2.4564	2.4579	2.4594	2.4609
4 50	2.4624	2.4639	2.4654	2.4669	2.4683	2.4698	2.4713	2.4728	2.4742	2.4757
0 5 0	2.4771	2.4786	2.4800	2.4814	2.4829	2.4843	2.4857	2.4871	2.4886	2.4900
5 10	2.4914	2.4928	2.4942	2.4955	2.4969	2.4983	2.4997	2.5011	2.5024	2.5038
5 20	2.5051	2.5065	2.5079	2.5092	2.5105	2.5119	2.5132	2.5145	2.5159	2.5172
5 30	2.5185	2.5198	2.5211	2.5224	2.5237	2.5250	2.5263	2.5276	2.5289	2.5302
5 40	2.5315	2.5328	2.5340	2.5353	2.5366	2.5378	2.5391	2.5403	2.5416	2.5428
5 50	2.5441	2.5453	2.5465	2.5478	2.5490	2.5502	2.5514	2.5527	2.5539	2.5551
0 6 0	2.5563	2.5575	2.5587	2.5599	2.5611	2.5623	2.5635	2.5647	2.5658	2.5670
6 10	2.5682	2.5694	2.5705	2.5717	2.5729	2.5740	2.5752	2.5763	2.5775	2.5786
6 20	2.5798	2.5809	2.5821	2.5832	2.5843	2.5855	2.5866	2.5877	2.5888	2.5899
6 30	2.5911	2.5922	2.5933	2.5944	2.5955	2.5966	2.5977	2.5988	2.5999	2.6010
6 40	2.6021	2.6031	2.6042	2.6053	2.6064	2.6075	2.6085	2.6096	2.6107	2.6117
6 50	2.6128	2.6138	2.6149	2.6160	2.6170	2.6180	2.6191	2.6201	2.6212	2.6222
0 7 0	2.6232	2.6243	2.6253	2.6263	2.6274	2.6284	2.6294	2.6304	2.6314	2.6325
7 10	2.6335	2.6345	2.6355	2.6365	2.6375	2.6385	2.6395	2.6405	2.6415	2.6425
7 20	2.6435	2.6444	2.6454	2.6464	2.6474	2.6484	2.6493	2.6503	2.6513	2.6522
7 30	2.6532	2.6542	2.6551	2.6561	2.6571	2.6580	2.6590	2.6599	2.6609	2.6618
7 40	2.6628	2.6637	2.6646	2.6656	2.6665	2.6675	2.6684	2.6693	2.6702	2.6712
7 50	2.6721	2.6730	2.6739	2.6749	2.6758	2.6767	2.6776	2.6785	2.6794	2.6803
0 8 0	2.6812	2.6821	2.6830	2.6839	2.6848	2.6857	2.6866	2.6875	2.6884	2.6893
8 10	2.6902	2.6911	2.6920	2.6928	2.6937	2.6946	2.6955	2.6964	2.6972	2.6981
8 20	2.6990	2.6998	2.7007	2.7016	2.7024	2.7033	2.7042	2.7050	2.7059	2.7067
8 30	2.7076	2.7084	2.7093	2.7101	2.7110	2.7118	2.7126	2.7135	2.7143	2.7152
8 40	2.7160	2.7168	2.7177	2.7185	2.7193	2.7202	2.7210	2.7218	2.7226	2.7235
8 50	2.7243	2.7251	2.7259	2.7267	2.7275	2.7284	2.7292	2.7300	2.7308	2.7316
0 9 0	2.7324	2.7332	2.7340	2.7348	2.7356	2.7364	2.7372	2.7380	2.7388	2.7396
9 10	2.7404	2.7412	2.7419	2.7427	2.7435	2.7443	2.7451	2.7459	2.7466	2.7474
9 20	2.7482	2.7490	2.7497	2.7505	2.7513	2.7520	2.7528	2.7536	2.7543	2.7551
9 30	2.7559	2.7566	2.7574	2.7582	2.7589	2.7597	2.7604	2.7612	2.7619	2.7627
9 40	2.7634	2.7642	2.7649	2.7657	2.7664	2.7672	2.7679	2.7686	2.7694	2.7701
9 50	2.7709	2.7716	2.7723	2.7731	2.7738	2.7745	2.7752	2.7760	2.7767	2.7774

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc. ° ′ ″	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
0h 10m 0s	2.7782	2.7789	2.7796	2.7803	2.7810	2.7818	2.7825	2.7832	2.7839	2.7846
10 10	2.7853	2.7860	2.7868	2.7875	2.7882	2.7889	2.7896	2.7903	2.7910	2.7917
10 20	2.7924	2.7931	2.7938	2.7945	2.7952	2.7959	2.7966	2.7973	2.7980	2.7987
10 30	2.7993	2.8000	2.8007	2.8014	2.8021	2.8028	2.8035	2.8041	2.8048	2.8055
10 40	2.8062	2.8069	2.8075	2.8082	2.8089	2.8096	2.8102	2.8109	2.8116	2.8122
10 50	2.8129	2.8136	2.8142	2.8149	2.8156	2.8162	2.8169	2.8176	2.8182	2.8189
0 11 0	2.8195	2.8202	2.8209	2.8215	2.8222	2.8228	2.8235	2.8241	2.8248	2.8254
11 10	2.8261	2.8267	2.8274	2.8280	2.8287	2.8293	2.8299	2.8306	2.8312	2.8319
11 20	2.8325	2.8331	2.8338	2.8344	2.8351	2.8357	2.8363	2.8370	2.8376	2.8382
11 30	2.8388	2.8395	2.8401	2.8407	2.8414	2.8420	2.8426	2.8432	2.8439	2.8445
11 40	2.8451	2.8457	2.8463	2.8470	2.8476	2.8482	2.8488	2.8494	2.8500	2.8506
11 50	2.8513	2.8519	2.8525	2.8531	2.8537	2.8543	2.8549	2.8555	2.8561	2.8567
0 12 0	2.8573	2.8579	2.8585	2.8591	2.8597	2.8603	2.8609	2.8615	2.8621	2.8627
12 10	2.8633	2.8639	2.8645	2.8651	2.8657	2.8663	2.8669	2.8675	2.8681	2.8686
12 20	2.8692	2.8698	2.8704	2.8710	2.8716	2.8722	2.8727	2.8733	2.8739	2.8745
12 30	2.8751	2.8756	2.8762	2.8768	2.8774	2.8779	2.8785	2.8791	2.8797	2.8802
12 40	2.8808	2.8814	2.8820	2.8825	2.8831	2.8837	2.8842	2.8848	2.8854	2.8859
12 50	2.8865	2.8871	2.8876	2.8882	2.8887	2.8893	2.8899	2.8904	2.8910	2.8915
0 13 0	2.8921	2.8927	2.8932	2.8938	2.8943	2.8949	2.8954	2.8960	2.8965	2.8971
13 10	2.8976	2.8982	2.8987	2.8993	2.8998	2.9004	2.9009	2.9015	2.9020	2.9025
13 20	2.9031	2.9036	2.9042	2.9047	2.9053	2.9058	2.9063	2.9069	2.9074	2.9079
13 30	2.9085	2.9090	2.9096	2.9101	2.9106	2.9112	2.9117	2.9122	2.9128	2.9133
13 40	2.9138	2.9143	2.9149	2.9154	2.9159	2.9165	2.9170	2.9175	2.9180	2.9186
13 50	2.9191	2.9196	2.9201	2.9206	2.9212	2.9217	2.9222	2.9227	2.9232	2.9238
0 14 0	2.9243	2.9248	2.9253	2.9258	2.9263	2.9269	2.9274	2.9279	2.9284	2.9289
14 10	2.9294	2.9299	2.9304	2.9309	2.9315	2.9320	2.9325	2.9330	2.9335	2.9340
14 20	2.9345	2.9350	2.9355	2.9360	2.9365	2.9370	2.9375	2.9380	2.9385	2.9390
14 30	2.9395	2.9400	2.9405	2.9410	2.9415	2.9420	2.9425	2.9430	2.9435	2.9440
14 40	2.9445	2.9450	2.9455	2.9460	2.9465	2.9469	2.9474	2.9479	2.9484	2.9489
14 50	2.9494	2.9499	2.9504	2.9509	2.9513	2.9518	2.9523	2.9528	2.9533	2.9538
0 15 0	2.9542	2.9547	2.9552	2.9557	2.9562	2.9566	2.9571	2.9576	2.9581	2.9586
15 10	2.9590	2.9595	2.9600	2.9605	2.9609	2.9614	2.9619	2.9624	2.9628	2.9633
15 20	2.9638	2.9643	2.9647	2.9652	2.9657	2.9661	2.9666	2.9671	2.9675	2.9680
15 30	2.9685	2.9689	2.9694	2.9699	2.9703	2.9708	2.9713	2.9717	2.9722	2.9727
15 40	2.9731	2.9736	2.9741	2.9745	2.9750	2.9754	2.9759	2.9763	2.9768	2.9773
15 50	2.9777	2.9782	2.9786	2.9791	2.9795	2.9800	2.9805	2.9809	2.9814	2.9818
0 16 0	2.9823	2.9827	2.9832	2.9836	2.9841	2.9845	2.9850	2.9854	2.9859	2.9863
16 10	2.9868	2.9872	2.9877	2.9881	2.9886	2.9890	2.9894	2.9899	2.9903	2.9908
16 20	2.9912	2.9917	2.9921	2.9926	2.9930	2.9934	2.9939	2.9943	2.9948	2.9952
16 30	2.9956	2.9961	2.9965	2.9969	2.9974	2.9978	2.9983	2.9987	2.9991	2.9996
16 40	3.0000	3.0004	3.0009	3.0013	3.0017	3.0022	3.0026	3.0030	3.0035	3.0039
16 50	3.0043	3.0048	3.0052	3.0056	3.0060	3.0065	3.0069	3.0073	3.0077	3.0082
0 17 0	3.0086	3.0090	3.0095	3.0099	3.0103	3.0107	3.0111	3.0116	3.0120	3.0124
17 10	3.0128	3.0133	3.0137	3.0141	3.0145	3.0149	3.0154	3.0158	3.0162	3.0166
17 20	3.0170	3.0175	3.0179	3.0183	3.0187	3.0191	3.0195	3.0199	3.0204	3.0208
17 30	3.0212	3.0216	3.0220	3.0224	3.0228	3.0233	3.0237	3.0241	3.0245	3.0249
17 40	3.0253	3.0257	3.0261	3.0265	3.0269	3.0273	3.0278	3.0282	3.0286	3.0290
17 50	3.0294	3.0298	3.0302	3.0306	3.0310	3.0314	3.0318	3.0322	3.0326	3.0330
0 18 0	3.0334	3.0338	3.0342	3.0346	3.0350	3.0354	3.0358	3.0362	3.0366	3.0370
18 10	3.0374	3.0378	3.0382	3.0386	3.0390	3.0394	3.0398	3.0402	3.0406	3.0410
18 20	3.0414	3.0418	3.0422	3.0426	3.0430	3.0434	3.0438	3.0441	3.0445	3.0449
18 30	3.0453	3.0457	3.0461	3.0465	3.0469	3.0473	3.0477	3.0481	3.0484	3.0488
18 40	3.0492	3.0496	3.0500	3.0504	3.0508	3.0512	3.0515	3.0519	3.0523	3.0527
18 50	3.0531	3.0535	3.0538	3.0542	3.0546	3.0550	3.0554	3.0558	3.0561	3.0565
0 19 0	3.0569	3.0573	3.0577	3.0580	3.0584	3.0588	3.0592	3.0596	3.0599	3.0603
19 10	3.0607	3.0611	3.0615	3.0618	3.0622	3.0626	3.0630	3.0633	3.0637	3.0641
19 20	3.0645	3.0648	3.0652	3.0656	3.0660	3.0663	3.0667	3.0671	3.0674	3.0678
19 30	3.0682	3.0686	3.0689	3.0693	3.0697	3.0700	3.0704	3.0708	3.0711	3.0715
19 40	3.0719	3.0722	3.0726	3.0730	3.0734	3.0737	3.0741	3.0745	3.0748	3.0752
19 50	3.0755	3.0759	3.0763	3.0766	3.0770	3.0774	3.0777	3.0781	3.0785	3.0788

Logarithms of Small Arcs in Space or Time.

Arc.			0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
°	′	″										
0h	20m	0s	3. 0792	3. 0795	3. 0799	3. 0803	3. 0806	3. 0810	3. 0813	3. 0817	3. 0821	3. 0824
	20	10	3. 0828	3. 0831	3. 0835	3. 0839	3. 0842	3. 0846	3. 0849	3. 0853	3. 0856	3. 0860
	20	20	3. 0864	3. 0867	3. 0871	3. 0874	3. 0878	3. 0881	3. 0885	3. 0888	3. 0892	3. 0896
	20	30	3. 0899	3. 0903	3. 0906	3. 0910	3. 0913	3. 0917	3. 0920	3. 0924	3. 0927	3. 0931
	20	40	3. 0934	3. 0938	3. 0941	3. 0945	3. 0948	3. 0952	3. 0955	3. 0959	3. 0962	3. 0966
	20	50	3. 0969	3. 0973	3. 0976	3. 0980	3. 0983	3. 0986	3. 0990	3. 0993	3. 0997	3. 1000
0	21	0	3. 1004	3. 1007	3. 1011	3. 1014	3. 1017	3. 1021	3. 1024	3. 1028	3. 1031	3. 1035
	21	10	3. 1038	3. 1041	3. 1045	3. 1048	3. 1052	3. 1055	3. 1059	3. 1062	3. 1065	3. 1069
	21	20	3. 1072	3. 1075	3. 1079	3. 1082	3. 1086	3. 1089	3. 1092	3. 1096	3. 1099	3. 1103
	21	30	3. 1106	3. 1109	3. 1113	3. 1116	3. 1119	3. 1123	3. 1126	3. 1129	3. 1133	3. 1136
	21	40	3. 1139	3. 1143	3. 1146	3. 1149	3. 1153	3. 1156	3. 1159	3. 1163	3. 1166	3. 1169
	21	50	3. 1173	3. 1176	3. 1179	3. 1183	3. 1186	3. 1189	3. 1193	3. 1196	3. 1199	3. 1202
0	22	0	3. 1206	3. 1209	3. 1212	3. 1216	3. 1219	3. 1222	3. 1225	3. 1229	3. 1232	3. 1235
	22	10	3. 1239	3. 1242	3. 1245	3. 1248	3. 1252	3. 1255	3. 1258	3. 1261	3. 1265	3. 1268
	22	20	3. 1271	3. 1274	3. 1278	3. 1281	3. 1284	3. 1287	3. 1290	3. 1294	3. 1297	3. 1300
	22	30	3. 1303	3. 1307	3. 1310	3. 1313	3. 1316	3. 1319	3. 1323	3. 1326	3. 1329	3. 1332
	22	40	3. 1335	3. 1339	3. 1342	3. 1345	3. 1348	3. 1351	3. 1355	3. 1358	3. 1361	3. 1364
	22	50	3. 1367	3. 1370	3. 1374	3. 1377	3. 1380	3. 1383	3. 1386	3. 1389	3. 1392	3. 1396
0	23	0	3. 1399	3. 1402	3. 1405	3. 1408	3. 1411	3. 1414	3. 1418	3. 1421	3. 1424	3. 1427
	23	10	3. 1430	3. 1433	3. 1436	3. 1440	3. 1443	3. 1446	3. 1449	3. 1452	3. 1455	3. 1458
	23	20	3. 1461	3. 1464	3. 1467	3. 1471	3. 1474	3. 1477	3. 1480	3. 1483	3. 1486	3. 1489
	23	30	3. 1492	3. 1495	3. 1498	3. 1501	3. 1504	3. 1508	3. 1511	3. 1514	3. 1517	3. 1520
	23	40	3. 1523	3. 1526	3. 1529	3. 1532	3. 1535	3. 1538	3. 1541	3. 1544	3. 1547	3. 1550
	23	50	3. 1553	3. 1556	3. 1559	3. 1562	3. 1565	3. 1569	3. 1572	3. 1575	3. 1578	3. 1581
0	24	0	3. 1584	3. 1587	3. 1590	3. 1593	3. 1596	3. 1599	3. 1602	3. 1605	3. 1608	3. 1611
	24	10	3. 1614	3. 1617	3. 1620	3. 1623	3. 1626	3. 1629	3. 1632	3. 1635	3. 1638	3. 1641
	24	20	3. 1644	3. 1647	3. 1649	3. 1652	3. 1655	3. 1658	3. 1661	3. 1664	3. 1667	3. 1670
	24	30	3. 1673	3. 1676	3. 1679	3. 1682	3. 1685	3. 1688	3. 1691	3. 1694	3. 1697	3. 1700
	24	40	3. 1703	3. 1706	3. 1708	3. 1711	3. 1714	3. 1717	3. 1720	3. 1723	3. 1726	3. 1729
	24	50	3. 1732	3. 1735	3. 1738	3. 1741	3. 1744	3. 1746	3. 1749	3. 1752	3. 1755	3. 1758
0	25	0	3. 1761	3. 1764	3. 1767	3. 1770	3. 1772	3. 1775	3. 1778	3. 1781	3. 1784	3. 1787
	25	10	3. 1790	3. 1793	3. 1796	3. 1798	3. 1801	3. 1804	3. 1807	3. 1810	3. 1813	3. 1816
	25	20	3. 1818	3. 1821	3. 1824	3. 1827	3. 1830	3. 1833	3. 1836	3. 1838	3. 1841	3. 1844
	25	30	3. 1847	3. 1850	3. 1853	3. 1855	3. 1858	3. 1861	3. 1864	3. 1867	3. 1870	3. 1872
	25	40	3. 1875	3. 1878	3. 1881	3. 1884	3. 1886	3. 1889	3. 1892	3. 1895	3. 1898	3. 1901
	25	50	3. 1903	3. 1906	3. 1909	3. 1912	3. 1915	3. 1917	3. 1920	3. 1923	3. 1926	3. 1928
0	26	0	3. 1931	3. 1934	3. 1937	3. 1940	3. 1942	3. 1945	3. 1948	3. 1951	3. 1953	3. 1956
	26	10	3. 1959	3. 1962	3. 1965	3. 1967	3. 1970	3. 1973	3. 1976	3. 1978	3. 1981	3. 1984
	26	20	3. 1987	3. 1989	3. 1992	3. 1995	3. 1998	3. 2000	3. 2003	3. 2006	3. 2009	3. 2011
	26	30	3. 2014	3. 2017	3. 2019	3. 2022	3. 2025	3. 2028	3. 2030	3. 2033	3. 2036	3. 2038
	26	40	3. 2041	3. 2044	3. 2047	3. 2049	3. 2052	3. 2055	3. 2057	3. 2060	3. 2063	3. 2066
	26	50	3. 2068	3. 2071	3. 2074	3. 2076	3. 2079	3. 2082	3. 2084	3. 2087	3. 2090	3. 2092
0	27	0	3. 2095	3. 2098	3. 2101	3. 2103	3. 2106	3. 2109	3. 2111	3. 2114	3. 2117	3. 2119
	27	10	3. 2122	3. 2125	3. 2127	3. 2130	3. 2133	3. 2135	3. 2138	3. 2140	3. 2143	3. 2146
	27	20	3. 2148	3. 2151	3. 2154	3. 2156	3. 2159	3. 2162	3. 2164	3. 2167	3. 2170	3. 2172
	27	30	3. 2175	3. 2177	3. 2180	3. 2183	3. 2185	3. 2188	3. 2191	3. 2193	3. 2196	3. 2198
	27	40	3. 2201	3. 2204	3. 2206	3. 2209	3. 2212	3. 2214	3. 2217	3. 2219	3. 2222	3. 2225
	27	50	3. 2227	3. 2230	3. 2232	3. 2235	3. 2238	3. 2240	3. 2243	3. 2245	3. 2248	3. 2250
0	28	0	3. 2253	3. 2256	3. 2258	3. 2261	3. 2263	3. 2266	3. 2269	3. 2271	3. 2274	3. 2276
	28	10	3. 2279	3. 2281	3. 2284	3. 2287	3. 2289	3. 2292	3. 2294	3. 2297	3. 2299	3. 2302
	28	20	3. 2304	3. 2307	3. 2310	3. 2312	3. 2315	3. 2317	3. 2320	3. 2322	3. 2325	3. 2327
	28	30	3. 2330	3. 2333	3. 2335	3. 2338	3. 2340	3. 2343	3. 2345	3. 2348	3. 2350	3. 2353
	28	40	3. 2355	3. 2358	3. 2360	3. 2363	3. 2365	3. 2368	3. 2370	3. 2373	3. 2375	3. 2378
	28	50	3. 2380	3. 2383	3. 2385	3. 2388	3. 2390	3. 2393	3. 2395	3. 2398	3. 2400	3. 2403
0	29	0	3. 2405	3. 2408	3. 2410	3. 2413	3. 2415	3. 2418	3. 2420	3. 2423	3. 2425	3. 2428
	29	10	3. 2430	3. 2433	3. 2435	3. 2438	3. 2440	3. 2443	3. 2445	3. 2448	3. 2450	3. 2453
	29	20	3. 2455	3. 2458	3. 2460	3. 2463	3. 2465	3. 2467	3. 2470	3. 2472	3. 2475	3. 2477
	29	30	3. 2480	3. 2482	3. 2485	3. 2487	3. 2490	3. 2492	3. 2494	3. 2497	3. 2499	3. 2502
	29	40	3. 2504	3. 2507	3. 2509	3. 2512	3. 2514	3. 2516	3. 2519	3. 2521	3. 2524	3. 2526
	29	50	3. 2529	3. 2531	3. 2533	3. 2536	3. 2538	3. 2541	3. 2543	3. 2545	3. 2548	3. 2550

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
° ′ ″										
0h 30m 0s	3.2553	3.2555	3.2558	3.2560	3.2562	3.2565	3.2567	3.2570	3.2572	3.2574
30 10	3.2577	3.2579	3.2582	3.2584	3.2586	3.2589	3.2591	3.2594	3.2596	3.2598
30 20	3.2601	3.2603	3.2605	3.2608	3.2610	3.2613	3.2615	3.2617	3.2620	3.2622
30 30	3.2625	3.2627	3.2629	3.2632	3.2634	3.2636	3.2639	3.2641	3.2643	3.2646
30 40	3.2648	3.2651	3.2653	3.2655	3.2658	3.2660	3.2662	3.2665	3.2667	3.2669
30 50	3.2672	3.2674	3.2676	3.2679	3.2681	3.2683	3.2686	3.2688	3.2690	3.2693
0 31 0	3.2695	3.2697	3.2700	3.2702	3.2704	3.2707	3.2709	3.2711	3.2714	3.2716
31 10	3.2718	3.2721	3.2723	3.2725	3.2728	3.2730	3.2732	3.2735	3.2737	3.2739
31 20	3.2742	3.2744	3.2746	3.2749	3.2751	3.2753	3.2755	3.2758	3.2760	3.2762
31 30	3.2765	3.2767	3.2769	3.2772	3.2774	3.2776	3.2778	3.2781	3.2783	3.2785
31 40	3.2788	3.2790	3.2792	3.2794	3.2797	3.2799	3.2801	3.2804	3.2806	3.2808
31 50	3.2810	3.2813	3.2815	3.2817	3.2819	3.2822	3.2824	3.2826	3.2828	3.2831
0 32 0	3.2833	3.2835	3.2838	3.2840	3.2842	3.2844	3.2847	3.2849	3.2851	3.2853
32 10	3.2856	3.2858	3.2860	3.2862	3.2865	3.2867	3.2869	3.2871	3.2874	3.2876
32 20	3.2878	3.2880	3.2882	3.2885	3.2887	3.2889	3.2891	3.2894	3.2896	3.2898
32 30	3.2900	3.2903	3.2905	3.2907	3.2909	3.2911	3.2914	3.2916	3.2918	3.2920
32 40	3.2923	3.2925	3.2927	3.2929	3.2931	3.2934	3.2936	3.2938	3.2940	3.2942
32 50	3.2945	3.2947	3.2949	3.2951	3.2953	3.2956	3.2958	3.2960	3.2962	3.2964
0 33 0	3.2967	3.2969	3.2971	3.2973	3.2975	3.2978	3.2980	3.2982	3.2984	3.2986
33 10	3.2989	3.2991	3.2993	3.2995	3.2997	3.2999	3.3002	3.3004	3.3006	3.3008
33 20	3.3010	3.3012	3.3015	3.3017	3.3019	3.3021	3.3023	3.3025	3.3028	3.3030
33 30	3.3032	3.3034	3.3036	3.3038	3.3041	3.3043	3.3045	3.3047	3.3049	3.3051
33 40	3.3054	3.3056	3.3058	3.3060	3.3062	3.3064	3.3066	3.3069	3.3071	3.3073
33 50	3.3075	3.3077	3.3079	3.3081	3.3084	3.3086	3.3088	3.3090	3.3092	3.3094
0 34 0	3.3096	3.3098	3.3101	3.3103	3.3105	3.3107	3.3109	3.3111	3.3113	3.3115
34 10	3.3118	3.3120	3.3122	3.3124	3.3126	3.3128	3.3130	3.3132	3.3134	3.3137
34 20	3.3139	3.3141	3.3143	3.3145	3.3147	3.3149	3.3151	3.3153	3.3156	3.3158
34 30	3.3160	3.3162	3.3164	3.3166	3.3168	3.3170	3.3172	3.3174	3.3176	3.3179
34 40	3.3181	3.3183	3.3185	3.3187	3.3189	3.3191	3.3193	3.3195	3.3197	3.3199
34 50	3.3201	3.3204	3.3206	3.3208	3.3210	3.3212	3.3214	3.3216	3.3218	3.3220
0 35 0	3.3222	3.3224	3.3226	3.3228	3.3230	3.3233	3.3235	3.3237	3.3239	3.3241
35 10	3.3243	3.3245	3.3247	3.3249	3.3251	3.3253	3.3255	3.3257	3.3259	3.3261
35 20	3.3263	3.3265	3.3267	3.3269	3.3272	3.3274	3.3276	3.3278	3.3280	3.3282
35 30	3.3284	3.3286	3.3288	3.3290	3.3292	3.3294	3.3296	3.3298	3.3300	3.3302
35 40	3.3304	3.3306	3.3308	3.3310	3.3312	3.3314	3.3316	3.3318	3.3320	3.3322
35 50	3.3324	3.3326	3.3328	3.3330	3.3332	3.3334	3.3336	3.3339	3.3341	3.3343
0 36 0	3.3345	3.3347	3.3349	3.3351	3.3353	3.3355	3.3357	3.3359	3.3361	3.3363
36 10	3.3365	3.3367	3.3369	3.3371	3.3373	3.3375	3.3377	3.3379	3.3381	3.3383
36 20	3.3385	3.3387	3.3389	3.3391	3.3393	3.3395	3.3397	3.3398	3.3400	3.3402
36 30	3.3404	3.3406	3.3408	3.3410	3.3412	3.3414	3.3416	3.3418	3.3420	3.3422
36 40	3.3424	3.3426	3.3428	3.3430	3.3432	3.3434	3.3436	3.3438	3.3440	3.3442
36 50	3.3444	3.3446	3.3448	3.3450	3.3452	3.3454	3.3456	3.3458	3.3460	3.3462
0 37 0	3.3464	3.3465	3.3467	3.3469	3.3471	3.3473	3.3475	3.3477	3.3479	3.3481
37 10	3.3483	3.3485	3.3487	3.3489	3.3491	3.3493	3.3495	3.3497	3.3499	3.3501
37 20	3.3502	3.3504	3.3506	3.3508	3.3510	3.3512	3.3514	3.3516	3.3518	3.3520
37 30	3.3522	3.3524	3.3526	3.3528	3.3530	3.3531	3.3533	3.3535	3.3537	3.3539
37 40	3.3541	3.3543	3.3545	3.3547	3.3549	3.3551	3.3553	3.3555	3.3556	3.3558
37 50	3.3560	3.3562	3.3564	3.3566	3.3568	3.3570	3.3572	3.3574	3.3576	3.3577
0 38 0	3.3579	3.3581	3.3583	3.3585	3.3587	3.3589	3.3591	3.3593	3.3595	3.3596
38 10	3.3598	3.3600	3.3602	3.3604	3.3606	3.3608	3.3610	3.3612	3.3614	3.3615
38 20	3.3617	3.3619	3.3621	3.3623	3.3625	3.3627	3.3629	3.3630	3.3632	3.3634
38 30	3.3636	3.3638	3.3640	3.3642	3.3644	3.3646	3.3647	3.3649	3.3651	3.3653
38 40	3.3655	3.3657	3.3659	3.3660	3.3662	3.3664	3.3666	3.3668	3.3670	3.3672
38 50	3.3674	3.3675	3.3677	3.3679	3.3681	3.3683	3.3685	3.3687	3.3688	3.3690
0 39 0	3.3692	3.3694	3.3696	3.3698	3.3700	3.3701	3.3703	3.3705	3.3707	3.3709
39 10	3.3711	3.3713	3.3714	3.3716	3.3718	3.3720	3.3722	3.3724	3.3725	3.3727
39 20	3.3729	3.3731	3.3733	3.3735	3.3736	3.3738	3.3740	3.3742	3.3744	3.3746
39 30	3.3747	3.3749	3.3751	3.3753	3.3755	3.3757	3.3758	3.3760	3.3762	3.3764
39 40	3.3766	3.3768	3.3769	3.3771	3.3773	3.3775	3.3777	3.3779	3.3780	3.3782
39 50	3.3784	3.3786	3.3788	3.3789	3.3791	3.3793	3.3795	3.3797	3.3798	3.3800

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.			0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
°	′	″										
0h	40m	0s	3.3802	3.3804	3.3806	3.3808	3.3809	3.3811	3.3813	3.3815	3.3817	3.3818
	40	10	3.3820	3.3822	3.3824	3.3826	3.3827	3.3829	3.3831	3.3833	3.3835	3.3836
	40	20	3.3838	3.3840	3.3842	3.3844	3.3845	3.3847	3.3849	3.3851	3.3852	3.3854
	40	30	3.3856	3.3858	3.3860	3.3861	3.3863	3.3865	3.3867	3.3869	3.3870	3.3872
	40	40	3.3874	3.3876	3.3877	3.3879	3.3881	3.3883	3.3885	3.3886	3.3888	3.3890
	40	50	3.3892	3.3893	3.3895	3.3897	3.3899	3.3901	3.3902	3.3904	3.3906	3.3908
0	41	0	3.3909	3.3911	3.3913	3.3915	3.3916	3.3918	3.3920	3.3922	3.3923	3.3925
	41	10	3.3927	3.3929	3.3930	3.3932	3.3934	3.3936	3.3938	3.3939	3.3941	3.3943
	41	20	3.3945	3.3946	3.3948	3.3950	3.3952	3.3953	3.3955	3.3957	3.3959	3.3960
	41	30	3.3962	3.3964	3.3965	3.3967	3.3969	3.3971	3.3972	3.3974	3.3976	3.3978
	41	40	3.3979	3.3981	3.3983	3.3985	3.3986	3.3988	3.3990	3.3992	3.3993	3.3995
	41	50	3.3997	3.3998	3.4000	3.4002	3.4004	3.4005	3.4007	3.4009	3.4011	3.4012
0	42	0	3.4014	3.4016	3.4017	3.4019	3.4021	3.4023	3.4024	3.4026	3.4028	3.4029
	42	10	3.4031	3.4033	3.4035	3.4036	3.4038	3.4040	3.4041	3.4043	3.4045	3.4047
	42	20	3.4048	3.4050	3.4052	3.4053	3.4055	3.4057	3.4059	3.4060	3.4062	3.4064
	42	30	3.4065	3.4067	3.4069	3.4071	3.4072	3.4074	3.4076	3.4077	3.4079	3.4081
	42	40	3.4082	3.4084	3.4086	3.4087	3.4089	3.4091	3.4093	3.4094	3.4096	3.4098
	42	50	3.4099	3.4101	3.4103	3.4104	3.4106	3.4108	3.4109	3.4111	3.4113	3.4115
0	43	0	3.4116	3.4118	3.4120	3.4121	3.4123	3.4125	3.4126	3.4128	3.4130	3.4131
	43	10	3.4133	3.4135	3.4136	3.4138	3.4140	3.4141	3.4143	3.4145	3.4146	3.4148
	43	20	3.4150	3.4151	3.4153	3.4155	3.4156	3.4158	3.4160	3.4161	3.4163	3.4165
	43	30	3.4166	3.4168	3.4170	3.4171	3.4173	3.4175	3.4176	3.4178	3.4180	3.4181
	43	40	3.4183	3.4185	3.4186	3.4188	3.4190	3.4191	3.4193	3.4195	3.4196	3.4198
	43	50	3.4200	3.4201	3.4203	3.4205	3.4206	3.4208	3.4209	3.4211	3.4213	3.4214
0	44	0	3.4216	3.4218	3.4219	3.4221	3.4223	3.4224	3.4226	3.4228	3.4229	3.4231
	44	10	3.4232	3.4234	3.4236	3.4237	3.4239	3.4241	3.4242	3.4244	3.4246	3.4247
	44	20	3.4249	3.4250	3.4252	3.4254	3.4255	3.4257	3.4259	3.4260	3.4262	3.4263
	44	30	3.4265	3.4267	3.4268	3.4270	3.4272	3.4273	3.4275	3.4276	3.4278	3.4280
	44	40	3.4281	3.4283	3.4285	3.4286	3.4288	3.4289	3.4291	3.4293	3.4294	3.4296
	44	50	3.4298	3.4299	3.4301	3.4302	3.4304	3.4306	3.4307	3.4309	3.4310	3.4312
0	45	0	3.4314	3.4315	3.4317	3.4318	3.4320	3.4322	3.4323	3.4325	3.4326	3.4328
	45	10	3.4330	3.4331	3.4333	3.4334	3.4336	3.4338	3.4339	3.4341	3.4342	3.4344
	45	20	3.4346	3.4347	3.4349	3.4350	3.4352	3.4354	3.4355	3.4357	3.4358	3.4360
	45	30	3.4362	3.4363	3.4365	3.4366	3.4368	3.4370	3.4371	3.4373	3.4374	3.4376
	45	40	3.4378	3.4379	3.4381	3.4382	3.4384	3.4385	3.4387	3.4389	3.4390	3.4392
	45	50	3.4393	3.4395	3.4396	3.4398	3.4400	3.4401	3.4403	3.4404	3.4406	3.4408
0	46	0	3.4409	3.4411	3.4412	3.4414	3.4415	3.4417	3.4419	3.4420	3.4422	3.4423
	46	10	3.4425	3.4426	3.4428	3.4429	3.4431	3.4433	3.4434	3.4436	3.4437	3.4439
	46	20	3.4440	3.4442	3.4444	3.4445	3.4447	3.4448	3.4450	3.4451	3.4453	3.4454
	46	30	3.4456	3.4458	3.4459	3.4461	3.4462	3.4464	3.4465	3.4467	3.4468	3.4470
	46	40	3.4472	3.4473	3.4475	3.4476	3.4478	3.4479	3.4481	3.4482	3.4484	3.4486
	46	50	3.4487	3.4489	3.4490	3.4492	3.4493	3.4495	3.4496	3.4498	3.4499	3.4501
0	47	0	3.4502	3.4504	3.4506	3.4507	3.4509	3.4510	3.4512	3.4513	3.4515	3.4516
	47	10	3.4518	3.4519	3.4521	3.4522	3.4524	3.4526	3.4527	3.4529	3.4530	3.4532
	47	20	3.4533	3.4535	3.4536	3.4538	3.4539	3.4541	3.4542	3.4544	3.4545	3.4547
	47	30	3.4548	3.4550	3.4551	3.4553	3.4555	3.4556	3.4558	3.4559	3.4561	3.4562
	47	40	3.4564	3.4565	3.4567	3.4568	3.4570	3.4571	3.4573	3.4574	3.4576	3.4577
	47	50	3.4579	3.4580	3.4582	3.4583	3.4585	3.4586	3.4588	3.4589	3.4591	3.4592
0	48	0	3.4594	3.4595	3.4597	3.4598	3.4600	3.4601	3.4603	3.4604	3.4606	3.4607
	48	10	3.4609	3.4610	3.4612	3.4613	3.4615	3.4616	3.4618	3.4619	3.4621	3.4622
	48	20	3.4624	3.4625	3.4627	3.4628	3.4630	3.4631	3.4633	3.4634	3.4636	3.4637
	48	30	3.4639	3.4640	3.4642	3.4643	3.4645	3.4646	3.4648	3.4649	3.4651	3.4652
	48	40	3.4654	3.4655	3.4657	3.4658	3.4660	3.4661	3.4663	3.4664	3.4666	3.4667
	48	50	3.4669	3.4670	3.4672	3.4673	3.4675	3.4676	3.4678	3.4679	3.4681	3.4682
0	49	0	3.4683	3.4685	3.4686	3.4688	3.4689	3.4691	3.4692	3.4694	3.4695	3.4697
	49	10	3.4698	3.4700	3.4701	3.4703	3.4704	3.4706	3.4707	3.4709	3.4710	3.4711
	49	20	3.4713	3.4714	3.4716	3.4717	3.4719	3.4720	3.4722	3.4723	3.4725	3.4726
	49	30	3.4728	3.4729	3.4730	3.4732	3.4733	3.4735	3.4736	3.4738	3.4739	3.4741
	49	40	3.4742	3.4744	3.4745	3.4747	3.4748	3.4749	3.4751	3.4752	3.4754	3.4755
	49	50	3.4757	3.4758	3.4760	3.4761	3.4763	3.4764	3.4765	3.4767	3.4768	3.4770

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc. ° ′ ″	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
0^h 50^m 0^s	3.4771	3.4773	3.4774	3.4776	3.4777	3.4778	3.4780	3.4781	3.4783	3.4784
50 10	3.4786	3.4787	3.4789	3.4790	3.4791	3.4793	3.4794	3.4796	3.4797	3.4799
50 20	3.4800	3.4802	3.4803	3.4804	3.4806	3.4807	3.4809	3.4810	3.4812	3.4813
50 30	3.4814	3.4816	3.4817	3.4819	3.4820	3.4822	3.4823	3.4824	3.4826	3.4827
50 40	3.4829	3.4830	3.4832	3.4833	3.4834	3.4836	3.4837	3.4839	3.4840	3.4842
50 50	3.4843	3.4844	3.4846	3.4847	3.4849	3.4850	3.4852	3.4853	3.4854	3.4856
0 51 0	3.4857	3.4859	3.4860	3.4861	3.4863	3.4864	3.4866	3.4667	3.4869	3.4870
51 10	3.4871	3.4873	3.4874	3.4876	3.4877	3.4878	3.4880	3.4881	3.4883	3.4884
51 20	3.4886	3.4887	3.4888	3.4890	3.4891	3.4893	3.4894	3.4895	3.4897	3.4898
51 30	3.4900	3.4901	3.4902	3.4904	3.4905	3.4907	3.4908	3.4909	3.4911	3.4912
51 40	3.4914	3.4915	3.4916	3.4918	3.4919	3.4921	3.4922	3.4923	3.4925	3.4926
51 50	3.4928	3.4929	3.4930	3.4932	3.4933	3.4935	3.4936	3.4937	3.4939	3.4940
0 52 0	3.4942	3.4943	3.4944	3.4946	3.4947	3.4949	3.4950	3.4951	3.4953	3.4954
52 10	3.4955	3.4957	3.4958	3.4960	3.4961	3.4962	3.4964	3.4965	3.4967	3.4968
52 20	3.4969	3.4971	3.4972	3.4973	3.4975	3.4976	3.4978	3.4979	3.4980	3.4982
52 30	3.4983	3.4984	3.4986	3.4987	3.4989	3.4990	3.4991	3.4993	3.4994	3.4995
52 40	3.4997	3.4998	3.5000	3.5001	3.5002	3.5004	3.5005	3.5006	3.5008	3.5009
52 50	3.5011	3.5012	3.5013	3.5015	3.5016	3.5017	3.5019	3.5020	3.5022	3.5023
0 53 0	3.5024	3.5026	3.5027	3.5028	3.5030	3.5031	3.5032	3.5034	3.5035	3.5037
53 10	3.5038	3.5039	3.5041	3.5042	3.5043	3.5045	3.5046	3.5047	3.5049	3.5050
53 20	3.5051	3.5053	3.5054	3.5056	3.5057	3.5058	3.5060	3.5061	3.5062	3.5064
53 30	3.5065	3.5066	3.5068	3.5069	3.5070	3.5072	3.5073	3.5075	3.5076	3.5077
53 40	3.5079	3.5080	3.5081	3.5083	3.5084	3.5085	3.5087	3.5088	3.5089	3.5091
53 50	3.5092	3.5093	3.5095	3.5096	3.5097	3.5099	3.5100	3.5101	3.5103	3.5104
0 54 0	3.5105	3.5107	3.5108	3.5109	3.5111	3.5112	3.5113	3.5115	5.5116	3.5117
54 10	3.5119	3.5120	3.5122	3.5123	3.5124	3.5126	3.5127	3.5128	3.5130	3.5131
54 20	3.5132	3.5134	3.5135	3.5136	3.5138	3.5139	3.5140	3.5141	3.5143	3.5144
54 30	3.5145	3.5147	3.5148	3.5149	3.5151	3.5152	3.5153	3.5155	3.5156	3.5157
54 40	3.5159	3.5160	3.5161	3.5163	3.5164	3.5165	3.5167	3.5168	3.5169	3.5171
54 50	3.5172	3.5173	3.5175	3.5176	3.5177	3.5179	3.5180	3.5181	3.5183	3.5184
0 55 0	3.5185	3.5186	3.5188	3.5189	3.5190	3.5192	3.5193	3.5194	3.5196	3.5197
55 10	3.5198	3.5200	3.5201	3.5202	3.5204	3.5205	3.5206	3.5207	3.5209	3.5210
55 20	3.5211	3.5213	3.5214	3.5215	3.5217	3.5218	3.5219	3.5221	3.5222	3.5223
55 30	3.5224	3.5226	3.5227	3.5228	3.5230	3.5231	3.5232	3.5234	3.5235	3.5236
55 40	3.5237	3.5239	3.5240	3.5241	3.5243	3.5244	3.5245	3.5247	3.5248	3.5249
55 50	3.5250	3.5252	3.5253	3.5254	3.5256	3.5257	3.5258	3.5260	3.5261	3.5262
0 56 0	3.5263	3.5265	3.5266	3.5267	3.5269	3.5270	3.5271	3.5272	3.5274	3.5275
56 10	3.5276	3.5278	3.5279	3.5280	3.5281	3.5283	3.5284	3.5285	3.5287	3.5288
56 20	3.5289	3.5290	3.5292	3.5293	3.5294	3.5296	3.5297	3.5298	3.5299	3.5301
56 30	3.5302	3.5303	3.5305	3.5306	3.5307	3.5308	3.5310	3.5311	3.5312	3.5314
56 40	3.5315	3.5316	3.5317	3.5319	3.5320	3.5321	3.5322	3.5324	3.5325	3.5326
56 50	3.5328	3.5329	3.5330	3.5331	3.5333	3.5334	3.5335	3.5336	3.5338	3.5339
0 57 0	3.5340	3.5342	3.5343	3.5344	3.5345	3.5347	3.5348	3.5349	3.5350	3.5352
57 10	3.5353	3.5354	3.5355	3.5357	3.5358	3.5359	3.5361	3.5362	3.5363	3.5364
57 20	3.5366	3.5367	3.5368	3.5369	3.5371	3.5372	3.5373	3.5374	3.5376	3.5377
57 30	3.5378	3.5379	3.5381	3.5382	3.5383	3.5384	3.5386	3.5387	3.5388	3.5390
57 40	3.5391	3.5392	3.5393	3.5395	3.5396	3.5397	3.5398	3.5400	3.5401	3.5402
57 50	3.5403	3.5405	3.5406	3.5407	3.5408	3.5410	3.5411	3.5412	3.5413	3.5415
0 58 0	3.5416	3.5417	3.5418	3.5420	3.5421	3.5422	3.5423	3.5425	3.5426	3.5427
58 10	3.5428	3.5429	3.5431	3.5432	3.5433	3.5434	3.5436	3.5437	3.5438	3.5439
58 20	3.5441	3.5442	3.5443	3.5444	3.5446	3.5447	3.5448	3.5449	3.5451	3.5452
58 30	3.5453	3.5454	3.5456	3.5457	3.5458	3.5459	3.5460	3.5462	3.5463	3.5464
58 40	3.5465	3.5467	3.5468	3.5469	3.5470	3.5472	3.5473	3.5474	3.5475	3.5477
58 50	3.5478	3.5479	3.5480	3.5481	3.5483	3.5484	3.5485	3.5486	3.5488	3.5489
0 59 0	3.5490	3.5491	3.5492	3.5494	3.5495	3.5496	3.5497	3.5499	3.5500	3.5501
59 10	3.5502	3.5504	3.5505	3.5506	3.5507	3.5508	3.5510	3.5511	3.5512	3.5513
59 20	3.5514	3.5516	3.5517	3.5518	3.5519	3.5521	3.5522	3.5523	3.5524	3.5525
59 30	3.5527	3.5528	3.5529	3.5530	3.5532	3.5533	3.5534	3.5535	3.5536	3.5538
59 40	3.5539	3.5540	3.5541	3.5542	3.5544	3.5545	3.5546	3.5547	3.5549	3.5550
59 50	3.5551	3.5552	3.5553	3.5555	3.5556	3.5557	3.5558	3.5559	3.5561	3.5562

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.			0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
°	′	″										
1h	0m	0s	3.5563	3.5564	3.5565	3.5567	3.5568	3.5569	3.5570	3.5571	3.5573	3.5574
	0	10	3.5575	3.5576	3.5577	3.5579	3.5580	3.5581	3.5582	3.5583	3.5585	3.5586
	0	20	3.5587	3.5588	3.5589	3.5591	3.5592	3.5593	3.5594	3.5595	3.5597	3.5598
	0	30	3.5599	3.5600	3.5601	3.5603	3.5604	3.5605	3.5606	3.5607	3.5609	3.5610
	0	40	3.5611	3.5612	3.5613	3.5615	3.5616	3.5617	3.5618	3.5619	3.5621	3.5622
	0	50	3.5623	3.5624	3.5625	3.5626	3.5628	3.5629	3.5630	3.5631	3.5632	3.5634
1	1	0	3.5635	3.5636	3.5637	3.5638	3.5640	3.5641	3.5642	3.5643	3.5644	3.5645
	1	10	3.5647	3.5648	3.5649	3.5650	3.5651	3.5653	3.5654	3.5655	3.5656	3.5657
	1	20	3.5658	3.5660	3.5661	3.5662	3.5663	3.5664	3.5666	3.5667	3.5668	3.5669
	1	30	3.5670	3.5671	3.5673	3.5674	3.5675	3.5676	3.5677	3.5678	3.5680	3.5681
	1	40	3.5682	3.5683	3.5684	3.5686	3.5687	3.5688	3.5689	3.5690	3.5691	3.5693
	1	50	3.5694	3.5695	3.5696	3.5697	3.5698	3.5700	3.5701	3.5702	3.5703	3.5704
1	2	0	3.5705	3.5707	3.5708	3.5709	3.5710	3.5711	3.5712	3.5714	3.5715	3.5716
	2	10	3.5717	3.5718	3.5719	3.5721	3.5722	3.5723	3.5724	3.5725	3.5726	3.5728
	2	20	3.5729	3.5730	3.5731	3.5732	3.5733	3.5735	3.5736	3.5737	3.5738	3.5739
	2	30	3.5740	3.5741	3.5742	3.5744	3.5745	3.5746	3.5747	3.5748	3.5750	3.5751
	2	40	3.5752	3.5753	3.5754	3.5755	3.5756	3.5758	3.5759	3.5760	3.5761	3.5762
	2	50	3.5763	3.5765	3.5766	3.5767	3.5768	3.5769	3.5770	3.5771	3.5773	3.5774
1	3	0	3.5775	3.5776	3.5777	3.5778	3.5780	3.5781	3.5782	3.5783	3.5784	3.5785
	3	10	3.5786	3.5788	3.5789	3.5790	3.5791	3.5792	3.5793	3.5794	3.5796	3.5797
	3	20	3.5798	3.5799	3.5800	3.5801	3.5802	3.5804	3.5805	3.5806	3.5807	3.5808
	3	30	3.5809	3.5810	3.5812	3.5813	3.5814	3.5815	3.5816	3.5817	3.5818	3.5819
	3	40	3.5821	3.5822	3.5823	3.5824	3.5825	3.5826	3.5827	3.5829	3.5830	3.5831
	3	50	3.5832	3.5833	3.5834	3.5835	3.5837	3.5838	3.5839	3.5840	3.5841	3.5842
1	4	0	3.5843	3.5844	3.5846	3.5847	3.5848	3.5849	3.5850	3.5851	3.5852	3.5853
	4	10	3.5855	3.5856	3.5857	3.5858	3.5859	3.5860	3.5861	3.5862	3.5864	3.5865
	4	20	3.5866	3.5867	3.5868	3.5869	3.5870	3.5871	3.5873	3.5874	3.5875	3.5876
	4	30	3.5877	3.5878	3.5879	3.5880	3.5882	3.5883	3.5884	3.5885	3.5886	3.5887
	4	40	3.5888	3.5889	3.5891	3.5892	3.5893	3.5894	3.5895	3.5896	3.5897	3.5898
	4	50	3.5899	3.5901	3.5902	3.5903	3.5904	3.5905	3.5906	3.5907	3.5908	3.5910
1	5	0	3.5911	3.5912	3.5913	3.5914	3.5915	3.5916	3.5917	3.5918	3.5920	3.5921
	5	10	3.5922	3.5923	3.5924	3.5925	3.5926	3.5927	3.5928	3.5930	3.5931	3.5932
	5	20	3.5933	3.5934	3.5935	3.5936	3.5937	3.5938	3.5940	3.5941	3.5942	3.5943
	5	30	3.5944	3.5945	3.5946	3.5947	3.5948	3.5949	3.5951	3.5952	3.5953	3.5954
	5	40	3.5955	3.5956	3.5957	3.5958	3.5959	3.5960	3.5962	3.5963	3.5964	3.5965
	5	50	3.5966	3.5967	3.5968	3.5969	3.5970	3.5971	3.5973	3.5974	3.5975	3.5976
1	6	0	3.5977	3.5978	3.5979	3.5980	3.5981	3.5982	3.5984	3.5985	3.5986	3.5987
	6	10	3.5988	3.5989	3.5990	3.5991	3.5992	3.5993	3.5994	3.5996	3.5997	3.5998
	6	20	3.5999	3.6000	3.6001	3.6002	3.6003	3.6004	3.6005	3.6006	3.6008	3.6009
	6	30	3.6010	3.6011	3.6012	3.6013	3.6014	3.6015	3.6016	3.6017	3.6018	3.6020
	6	40	3.6021	3.6022	3.6023	3.6024	3.6025	3.6026	3.6027	3.6028	3.6029	3.6030
	6	50	3.6031	3.6033	3.6034	3.6035	3.6036	3.6037	3.6038	3.6039	3.6040	3.6041
1	7	0	3.6042	3.6043	3.6044	3.6046	3.6047	3.6048	3.6049	3.6050	3.6051	3.6052
	7	10	3.6053	3.6054	3.6055	3.6056	3.6057	3.6058	3.6060	3.6061	3.6062	3.6063
	7	20	3.6064	3.6065	3.6066	3.6067	3.6068	3.6069	3.6070	3.6071	3.6072	3.6073
	7	30	3.6075	3.6076	3.6077	3.6078	3.6079	3.6080	3.6081	3.6082	3.6083	3.6084
	7	40	3.6085	3.6086	3.6087	3.6088	3.6090	3.6091	3.6092	3.6093	3.6094	3.6095
	7	50	3.6096	3.6097	3.6098	3.6099	3.6100	3.6101	3.6102	3.6103	3.6104	3.6106
1	8	0	3.6107	3.6108	3.6109	3.6110	3.6111	3.6112	3.6113	3.6114	3.6115	3.6116
	8	10	3.6117	3.6118	3.6119	3.6120	3.6121	3.6123	3.6124	3.6125	3.6126	3.6127
	8	20	3.6128	3.6129	3.6130	3.6131	3.6132	3.6133	3.6134	3.6135	3.6136	3.6137
	8	30	3.6138	3.6139	3.6141	3.6142	3.6143	3.6144	3.6145	3.6146	3.6147	3.6148
	8	40	3.6149	3.6150	3.6151	3.6152	3.6153	3.6154	3.6155	3.6156	3.6157	3.6158
	8	50	3.6160	3.6161	3.6162	3.6163	3.6164	3.6165	3.6166	3.6167	3.6168	3.6169
1	9	0	3.6170	3.6171	3.6172	3.6173	3.6174	3.6175	3.6176	3.6177	3.6178	3.6179
	9	10	3.6180	3.6182	3.6183	3.6184	3.6185	3.6186	3.6187	3.6188	3.6189	3.6190
	9	20	3.6191	3.6192	3.6193	3.6194	3.6195	3.6196	3.6197	3.6198	3.6199	3.6200
	9	30	3.6201	3.6202	3.6203	3.6204	3.6206	3.6207	3.6208	3.6209	3.6210	3.6211
	9	40	3.6212	3.6213	3.6214	3.6215	3.6216	3.6217	3.6218	3.6219	3.6220	3.6221
	9	50	3.6222	3.6223	3.6224	3.6225	3.6226	3.6227	3.6228	3.6229	3.6230	3.6231

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc. ° ′ ″	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
1h 10m 0s	3.6232	3.6234	3.6235	3.6236	3.6237	3.6238	3.6239	3.6240	3.6241	3.6242
10 10	3.6243	3.6244	3.6245	3.6246	3.6247	3.6248	3.6249	3.6250	3.6251	3.6252
10 20	3.6253	3.6254	3.6255	3.6256	3.6257	3.6258	3.6259	3.6260	3.6261	3.6262
10 30	3.6263	3.6264	3.6265	3.6266	3.6268	3.6269	3.6270	3.6271	3.6272	3.6273
10 40	3.6274	3.6275	3.6276	3.6277	3.6278	3.6279	3.6280	3.6281	3.6282	3.6283
10 50	3.6284	3.6285	3.6286	3.6287	3.6288	3.6289	3.6290	3.6291	3.6292	3.6293
1 11 0	3.6294	3.6295	3.6296	3.6297	3.6298	3.6299	3.6300	3.6301	3.6302	3.6303
11 10	3.6304	3.6305	3.6306	3.6307	3.6308	3.6309	3.6310	3.6311	3.6312	3.6313
11 20	3.6314	3.6315	3.6316	3.6317	3.6318	3.6320	3.6321	3.6322	3.6323	3.6324
11 30	3.6325	3.6326	3.6327	3.6328	3.6329	3.6330	3.6331	3.6332	3.6333	3.6334
11 40	3.6335	3.6336	3.6337	3.6338	3.6339	3.6340	3.6341	3.6342	3.6343	3.6344
11 50	3.6345	3.6346	3.6347	3.6348	3.6349	3.6350	3.6351	3.6352	3.6353	3.6354
1 12 0	3.6355	3.6356	3.6357	3.6358	3.6359	3.6360	3.6361	3.6362	3.6363	3.6364
12 10	3.6365	3.6366	3.6367	3.6368	3.6369	3.6370	3.6371	3.6372	3.6373	3.6374
12 20	3.6375	3.6376	3.6377	3.6378	3.6379	3.6380	3.6381	3.6382	3.6383	3.6384
12 30	3.6385	3.6386	3.6387	3.6388	3.6389	3.6390	3.6391	3.6392	3.6393	3.6394
12 40	3.6395	3.6396	3.6397	3.6398	3.6399	3.6400	3.6401	3.6402	3.6403	3.6404
12 50	3.6405	3.6406	3.6407	3.6408	3.6409	3.6410	3.6411	3.6412	3.6413	3.6414
1 13 0	3.6415	3.6416	3.6417	3.6418	3.6419	3.6420	3.6421	3.6422	3.6423	3.6424
13 10	3.6425	3.6426	3.6427	3.6428	3.6429	3.6430	3.6431	3.6432	3.6433	3.6434
13 20	3.6435	3.6436	3.6437	3.6437	3.6438	3.6439	3.6440	3.6441	3.6442	3.6443
13 30	3.6444	3.6445	3.6446	3.6447	3.6448	3.6449	3.6450	3.6451	3.6452	3.6453
13 40	3.6454	3.6455	3.6456	3.6457	3.6458	3.6459	3.6460	3.6461	3.6462	3.6463
13 50	3.6464	3.6465	3.6466	3.6467	3.6468	3.6469	3.6470	3.6471	3.6472	3.6473
1 14 0	3.6474	3.6475	3.6476	3.6477	3.6478	3.6479	3.6480	3.6481	3.6482	3.6483
14 10	3.6484	3.6485	3.6486	3.6487	3.6488	3.6488	3.6489	3.6490	3.6491	3.6492
14 20	3.6493	3.6494	3.6495	3.6496	3.6497	3.6498	3.6499	3.6500	3.6501	3.6502
14 30	3.6503	3.6504	3.6505	3.6506	3.6507	3.6508	3.6509	3.6510	3.6511	3.6512
14 40	3.6513	3.6514	3.6515	3.6516	3.6517	3.6518	3.6519	3.6520	3.6521	3.6521
14 50	3.6522	3.6523	3.6524	3.6525	3.6526	3.6527	3.6528	3.6529	3.6530	3.6531
1 15 0	3.6532	3.6533	3.6534	3.6535	3.6536	3.6537	3.6538	3.6539	3.6540	3.6541
15 10	3.6542	3.6543	3.6544	3.6545	3.6546	3.6547	3.6548	3.6549	3.6549	3.6550
15 20	3.6551	3.6552	3.6553	3.6554	3.6555	3.6556	3.6557	3.6558	3.6559	3.6560
15 30	3.6561	3.6562	3.6563	3.6564	3.6565	3.6566	3.6567	3.6568	3.6569	3.6570
15 40	3.6571	3.6572	3.6572	3.6573	3.6574	3.6575	3.6576	3.6577	3.6578	3.6579
15 50	3.6580	3.6581	3.6582	3.6583	3.6584	3.6585	3.6586	3.6587	3.6588	3.6589
1 16 0	3.6590	3.6591	3.6592	3.6593	3.6593	3.6594	3.6595	3.6596	3.6597	3.6598
16 10	3.6599	3.6600	3.6601	3.6602	3.6603	3.6604	3.6605	3.6606	3.6607	3.6608
16 20	3.6609	3.6610	3.6611	3.6611	3.6612	3.6613	3.6614	3.6615	3.6616	3.6617
16 30	3.6618	3.6619	3.6620	3.6621	3.6622	3.6623	3.6624	3.6625	3.6626	3.6627
16 40	3.6628	3.6629	3.6629	3.6630	3.6631	3.6632	3.6633	3.6634	3.6635	3.6636
16 50	3.6637	3.6638	3.6639	3.6640	3.6641	3.6642	3.6643	3.6644	3.6645	3.6645
1 17 0	3.6646	3.6647	3.6648	3.6649	3.6650	3.6651	3.6652	3.6653	3.6654	3.6655
17 10	3.6656	3.6657	3.6658	3.6659	3.6660	3.6660	3.6661	3.6662	3.6663	3.6664
17 20	3.6665	3.6666	3.6667	3.6668	3.6669	3.6670	3.6671	3.6672	3.6673	3.6674
17 30	3.6675	3.6675	3.6676	3.6677	3.6678	3.6679	3.6680	3.6681	3.6682	3.6683
17 40	3.6684	3.6685	3.6686	3.6687	3.6688	3.6689	3.6689	3.6690	3.6691	3.6692
17 50	3.6693	3.6694	3.6695	3.6696	3.6697	3.6698	3.6699	3.6700	3.6701	3.6702
1 18 0	3.6702	3.6703	3.6704	3.6705	3.6706	3.6707	3.6708	3.6709	3.6710	3.6711
18 10	3.6712	3.6713	3.6714	3.6715	3.6715	3.6716	3.6717	3.6718	3.6719	3.6720
18 20	3.6721	3.6722	3.6723	3.6724	3.6725	3.6726	3.6727	3.6727	3.6728	3.6729
18 30	3.6730	3.6731	3.6732	3.6733	3.6734	3.6735	3.6736	3.6737	3.6738	3.6738
18 40	3.6739	3.6740	3.6741	3.6742	3.6743	3.6744	3.6745	3.6746	3.6747	3.6748
18 50	3.6749	3.6750	3.6750	3.6751	3.6752	3.6753	3.6754	3.6755	3.6756	3.6757
1 19 0	3.6758	3.6759	3.6760	3.6761	3.6761	3.6762	3.6763	3.6764	3.6765	3.6766
19 10	3.6767	3.6768	3.6769	3.6770	3.6771	3.6772	3.6772	3.6773	3.6774	3.6775
19 20	3.6776	3.6777	3.6778	3.6779	3.6780	3.6781	3.6782	3.6782	3.6783	3.6784
19 30	3.6785	3.6786	3.6787	3.6788	3.6789	3.6790	3.6791	3.6792	3.6792	3.6793
19 40	3.6794	3.6795	3.6796	3.6797	3.6798	3.6799	3.6800	3.6801	3.6802	3.6802
19 50	3.6803	3.6804	3.6805	3.6806	3.6807	3.6808	3.6809	3.6810	3.6811	3.6812

Logarithms of Small Arcs in Space or Time.

Arc.	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
° ′ ″										
1^h 20^m 0^s	3.6812	3.6813	3.6814	3.6815	3.6816	3.6817	3.6818	3.6819	3.6820	3.6821
20 10	3.6821	3.6822	3.6823	3.6824	3.6825	3.6826	3.6827	3.6828	3.6829	3.6830
20 20	3.6830	3.6831	3.6832	3.6833	3.6834	3.6835	3.6836	3.6837	3.6838	3.6839
20 30	3.6839	3.6840	3.6841	3.6842	3.6843	3.6844	3.6845	3.6846	3.6847	3.6848
20 40	3.6848	3.6849	3.6850	3.6851	3.6852	3.6853	3.6854	3.6855	3.6856	3.6857
20 50	3.6857	3.6858	3.6859	3.6860	3.6861	3.6862	3.6863	3.6864	3.6865	3.6865
1 21 0	3.6866	3.6867	3.6868	3.6869	3.6870	3.6871	3.6872	3.6873	3.6874	3.6874
21 10	3.6875	3.6876	3.6877	3.6878	3.6879	3.6880	3.6881	3.6882	3.6882	3.6883
21 20	3.6884	3.6885	3.6886	3.6887	3.6888	3.6889	3.6890	3.6890	3.6891	3.6892
21 30	3.6893	3.6894	3.6895	3.6896	3.6897	3.6898	3.6898	3.6899	3.6900	3.6901
21 40	3.6902	3.6903	3.6904	3.6905	3.6906	3.6906	3.6907	3.6908	3.6909	3.6910
21 50	3.6911	3.6912	3.6913	3.6913	3.6914	3.6915	3.6916	3.6917	3.6918	3.6919
1 22 0	3.6920	3.6921	3.6921	3.6922	3.6923	3.6924	3.6925	3.6926	3.6927	3.6928
22 10	3.6928	3.6929	3.6930	3.6931	3.6932	3.6933	3.6934	3.6935	3.6936	3.6936
22 20	3.6937	3.6938	3.6939	3.6940	3.6941	3.6942	3.6943	3.6943	3.6944	3.6945
22 30	3.6946	3.6947	3.6948	3.6949	3.6950	3.6950	3.6951	3.6952	3.6953	3.6954
22 40	3.6955	3.6956	3.6957	3.6957	3.6958	3.6959	3.6960	3.6961	3.6962	3.6963
22 50	3.6964	3.6964	3.6965	3.6966	3.6967	3.6968	3.6969	3.6970	3.6971	3.6971
1 23 0	3.6972	3.6973	3.6974	3.6975	3.6976	3.6977	3.6978	3.6978	3.6979	3.6980
23 10	3.6981	3.6982	3.6983	3.6984	3.6984	3.6985	3.6986	3.6987	3.6988	3.6989
23 20	3.6990	3.6991	3.6991	3.6992	3.6993	3.6994	3.6995	3.6996	3.6997	3.6998
23 30	3.6998	3.6999	3.7000	3.7001	3.7002	3.7003	3.7004	3.7004	3.7005	3.7006
23 40	3.7007	3.7008	3.7009	3.7010	3.7010	3.7011	3.7012	3.7013	3.7014	3.7015
23 50	3.7016	3.7017	3.7017	3.7018	3.7019	3.7020	3.7021	3.7022	3.7023	3.7023
1 24 0	3.7024	3.7025	3.7026	3.7027	3.7028	3.7029	3.7029	3.7030	3.7031	3.7032
24 10	3.7033	3.7034	3.7035	3.7035	3.7036	3.7037	3.7038	3.7039	3.7040	3.7041
24 20	3.7042	3.7042	3.7043	3.7044	3.7045	3.7046	3.7047	3.7048	3.7048	3.7049
24 30	3.7050	3.7051	3.7052	3.7053	3.7054	3.7054	3.7055	3.7056	3.7057	3.7058
24 40	3.7059	3.7060	3.7060	3.7061	3.7062	3.7063	3.7064	3.7065	3.7065	3.7066
24 50	3.7067	3.7068	3.7069	3.7070	3.7071	3.7071	3.7072	3.7073	3.7074	3.7075
1 25 0	3.7076	3.7077	3.7077	3.7078	3.7079	3.7080	3.7081	3.7082	3.7083	3.7083
25 10	3.7084	3.7085	3.7086	3.7087	3.7088	3.7088	3.7089	3.7090	3.7091	3.7092
25 20	3.7093	3.7094	3.7094	3.7095	3.7096	3.7097	3.7098	3.7099	3.7099	3.7100
25 30	3.7101	3.7102	3.7103	3.7104	3.7105	3.7105	3.7106	3.7107	3.7108	3.7109
25 40	3.7110	3.7110	3.7111	3.7112	3.7113	3.7114	3.7115	3.7116	3.7116	3.7117
25 50	3.7118	3.7119	3.7120	3.7121	3.7121	3.7122	3.7123	3.7124	3.7125	3.7126
1 26 0	3.7126	3.7127	3.7128	3.7129	3.7130	3.7131	3.7132	3.7132	3.7133	3.7134
26 10	3.7135	3.7136	3.7137	3.7137	3.7138	3.7139	3.7140	3.7141	3.7142	3.7142
26 20	3.7143	3.7144	3.7145	3.7146	3.7147	3.7147	3.7148	3.7149	3.7150	3.7151
26 30	3.7152	3.7153	3.7153	3.7154	3.7155	3.7156	3.7157	3.7158	3.7159	3.7159
26 40	3.7160	3.7161	3.7162	3.7163	3.7163	3.7164	3.7165	3.7166	3.7167	3.7168
26 50	3.7168	3.7169	3.7170	3.7171	3.7172	3.7173	3.7173	3.7174	3.7175	3.7176
1 27 0	3.7177	3.7178	3.7178	3.7179	3.7180	3.7181	3.7182	3.7183	3.7183	3.7184
27 10	3.7185	3.7186	3.7187	3.7188	3.7188	3.7189	3.7190	3.7191	3.7192	3.7192
27 20	3.7193	3.7194	3.7195	3.7196	3.7197	3.7197	3.7198	3.7199	3.7200	3.7201
27 30	3.7202	3.7202	3.7203	3.7204	3.7205	3.7206	3.7207	3.7207	3.7208	3.7209
27 40	3.7210	3.7211	3.7212	3.7212	3.7213	3.7214	3.7215	3.7216	3.7216	3.7217
27 50	3.7218	3.7219	3.7220	3.7221	3.7221	3.7222	3.7223	3.7224	3.7225	3.7226
1 28 0	3.7226	3.7227	3.7228	3.7229	3.7230	3.7230	3.7231	3.7232	3.7233	3.7234
28 10	3.7235	3.7235	3.7236	3.7237	3.7238	3.7239	3.7239	3.7240	3.7241	3.7242
28 20	3.7243	3.7244	3.7244	3.7245	3.7246	3.7247	3.7248	3.7248	3.7249	3.7250
28 30	3.7251	3.7252	3.7253	3.7253	3.7254	3.7255	3.7256	3.7257	3.7257	3.7258
28 40	3.7259	3.7260	3.7261	3.7262	3.7262	3.7263	3.7264	3.7265	3.7266	3.7266
28 50	3.7267	3.7268	3.7269	3.7270	3.7271	3.7271	3.7272	3.7273	3.7274	3.7275
1 29 0	3.7275	3.7276	3.7277	3.7278	3.7279	3.7279	3.7280	3.7281	3.7282	3.7283
29 10	3.7284	3.7284	3.7285	3.7286	3.7287	3.7288	3.7288	3.7289	3.7290	3.7291
29 20	3.7292	3.7292	3.7293	3.7294	3.7295	3.7296	3.7297	3.7297	3.7298	3.7299
29 30	3.7300	3.7301	3.7301	3.7302	3.7303	3.7304	3.7305	3.7305	3.7306	3.7307
29 40	3.7308	3.7309	3.7309	3.7310	3.7311	3.7312	3.7313	3.7313	3.7314	3.7315
29 50	3.7316	3.7317	3.7317	3.7318	3.7319	3.7320	3.7321	3.7322	3.7322	3.7323

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
° ′ ″										
1h 30m 0s	3.7324	3.7325	3.7326	3.7326	3.7327	3.7328	3.7329	3.7330	3.7330	3.7331
30 10	3.7332	3.7333	3.7334	3.7334	3.7335	3.7336	3.7337	3.7338	3.7338	3.7339
30 20	3.7340	3.7341	3.7342	3.7342	3.7343	3.7344	3.7345	3.7346	3.7346	3.7347
30 30	3.7348	3.7349	3.7350	3.7350	3.7351	3.7352	3.7353	3.7354	3.7354	3.7355
30 40	3.7356	3.7357	3.7358	3.7358	3.7359	3.7360	3.7361	3.7362	3.7362	3.7363
30 50	3.7364	3.7365	3.7366	3.7366	3.7367	3.7368	3.7369	3.7370	3.7370	3.7371
1 31 0	3.7372	3.7373	3.7374	3.7374	3.7375	3.7376	3.7377	3.7377	3.7378	3.7379
31 10	3.7380	3.7381	3.7381	3.7382	3.7383	3.7384	3.7385	3.7385	3.7386	3.7387
31 20	3.7388	3.7389	3.7389	3.7390	3.7391	3.7392	3.7393	3.7393	3.7394	3.7395
31 30	3.7396	3.7397	3.7397	3.7398	3.7399	3.7400	3.7400	3.7401	3.7402	3.7403
31 40	3.7404	3.7404	3.7405	3.7406	3.7407	3.7408	3.7408	3.7409	3.7410	3.7411
31 50	3.7412	3.7412	3.7413	3.7414	3.7415	3.7415	3.7416	3.7417	3.7418	3.7419
1 32 0	3.7419	3.7420	3.7421	3.7422	3.7423	3.7423	3.7424	3.7425	3.7426	3.7426
32 10	3.7427	3.7428	3.7429	3.7430	3.7430	3.7431	3.7432	3.7433	3.7434	3.7434
32 20	3.7435	3.7436	3.7437	3.7437	3.7438	3.7439	3.7440	3.7441	3.7441	3.7442
32 30	3.7443	3.7444	3.7444	3.7445	3.7446	3.7447	3.7448	3.7448	3.7449	3.7450
32 40	3.7451	3.7452	3.7452	3.7453	3.7454	3.7455	3.7455	3.7456	3.7457	3.7458
32 50	3.7459	3.7459	3.7460	3.7461	3.7462	3.7462	3.7463	3.7464	3.7465	3.7466
1 33 0	3.7466	3.7467	3.7468	3.7469	3.7469	3.7470	3.7471	3.7472	3.7473	3.7473
33 10	3.7474	3.7475	3.7476	3.7476	3.7477	3.7478	3.7479	3.7480	3.7480	3.7481
33 20	3.7482	3.7483	3.7483	3.7484	3.7485	3.7486	3.7487	3.7487	3.7488	3.7489
33 30	3.7490	3.7490	3.7491	3.7492	3.7493	3.7493	3.7494	3.7495	3.7496	3.7497
33 40	3.7497	3.7498	3.7499	3.7500	3.7500	3.7501	3.7502	3.7503	3.7504	3.7504
33 50	3.7505	3.7506	3.7507	3.7507	3.7508	3.7509	3.7510	3.7510	3.7511	3.7512
1 34 0	3.7513	3.7514	3.7514	3.7515	3.7516	3.7517	3.7517	3.7518	3.7519	3.7520
34 10	3.7520	3.7521	3.7522	3.7523	3.7524	3.7524	3.7525	3.7526	3.7527	3.7527
34 20	3.7528	3.7529	3.7530	3.7530	3.7531	3.7532	3.7533	3.7534	3.7534	3.7535
34 30	3.7536	3.7537	3.7537	3.7538	3.7539	3.7540	3.7540	3.7541	3.7542	3.7543
34 40	3.7543	3.7544	3.7545	3.7546	3.7547	3.7547	3.7548	3.7549	3.7550	3.7550
34 50	3.7551	3.7552	3.7553	3.7553	3.7554	3.7555	3.7556	3.7556	3.7557	3.7558
1 35 0	3.7559	3.7560	3.7560	3.7561	3.7562	3.7563	3.7563	3.7564	3.7565	3.7566
35 10	3.7566	3.7567	3.7568	3.7569	3.7569	3.7570	3.7571	3.7572	3.7572	3.7573
35 20	3.7574	3.7575	3.7575	3.7576	3.7577	3.7578	3.7579	3.7579	3.7580	3.7581
35 30	3.7582	3.7582	3.7583	3.7584	3.7585	3.7585	3.7586	3.7587	3.7588	3.7588
35 40	3.7589	3.7590	3.7591	3.7591	3.7592	3.7593	3.7594	3.7594	3.7595	3.7596
35 50	3.7597	3.7597	3.7598	3.7599	3.7600	3.7600	3.7601	3.7602	3.7603	3.7603
1 36 0	3.7604	3.7605	3.7606	3.7606	3.7607	3.7608	3.7609	3.7609	3.7610	3.7611
36 10	3.7612	3.7613	3.7613	3.7614	3.7615	3.7616	3.7616	3.7617	3.7618	3.7619
36 20	3.7619	3.7620	3.7621	3.7622	3.7622	3.7623	3.7624	3.7625	3.7625	3.7626
36 30	3.7627	3.7628	3.7628	3.7629	3.7630	3.7631	3.7631	3.7632	3.7633	3.7634
36 40	3.7634	3.7635	3.7636	3.7637	3.7637	3.7638	3.7639	3.7640	3.7640	3.7641
36 50	3.7642	3.7643	3.7643	3.7644	3.7645	3.7645	3.7646	3.7647	3.7648	3.7648
1 37 0	3.7649	3.7650	3.7651	3.7651	3.7652	3.7653	3.7654	3.7654	3.7655	3.7656
37 10	3.7657	3.7657	3.7658	3.7659	3.7660	3.7660	3.7661	3.7662	3.7663	3.7663
37 20	3.7664	3.7665	3.7666	3.7666	3.7667	3.7668	3.7669	3.7669	3.7670	3.7671
37 30	3.7672	3.7672	3.7673	3.7674	3.7675	3.7675	3.7676	3.7677	3.7677	3.7678
37 40	3.7679	3.7680	3.7681	3.7681	3.7682	3.7683	3.7683	3.7684	3.7685	3.7686
37 50	3.7686	3.7687	3.7688	3.7689	3.7689	3.7690	3.7691	3.7692	3.7692	3.7693
1 38 0	3.7694	3.7695	3.7695	3.7696	3.7697	3.7697	3.7698	3.7699	3.7700	3.7700
38 10	3.7701	3.7702	3.7703	3.7703	3.7704	3.7705	3.7706	3.7706	3.7707	3.7708
38 20	3.7709	3.7709	3.7710	3.7711	3.7711	3.7712	3.7713	3.7714	3.7714	3.7715
38 30	3.7716	3.7717	3.7717	3.7718	3.7719	3.7720	3.7720	3.7721	3.7722	3.7722
38 40	3.7723	3.7724	3.7725	3.7725	3.7726	3.7727	3.7728	3.7728	3.7729	3.7730
38 50	3.7731	3.7731	3.7732	3.7733	3.7733	3.7734	3.7735	3.7736	3.7736	3.7737
1 39 0	3.7738	3.7739	3.7739	3.7740	3.7741	3.7742	3.7742	3.7743	3.7744	3.7744
39 10	3.7745	3.7746	3.7747	3.7747	3.7748	3.7749	3.7750	3.7750	3.7751	3.7752
39 20	3.7752	3.7753	3.7754	3.7755	3.7755	3.7756	3.7757	3.7758	3.7758	3.7759
39 30	3.7760	3.7760	3.7761	3.7762	3.7763	3.7763	3.7764	3.7765	3.7766	3.7766
39 40	3.7767	3.7768	3.7768	3.7769	3.7770	3.7771	3.7771	3.7772	3.7773	3.7774
39 50	3.7774	3.7775	3.7776	3.7776	3.7777	3.7778	3.7779	3.7779	3.7780	3.7781

Logarithms of Small Arcs in Space or Time.

Arc. °	′	″	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
1h	40m	0s	3.7782	3.7782	3.7783	3.7784	3.7784	3.7785	3.7786	3.7787	3.7787	3.7788
	40	10	3.7789	3.7789	3.7790	3.7791	3.7792	3.7792	3.7793	3.7794	3.7795	3.7795
	40	20	3.7796	3.7797	3.7797	3.7798	3.7799	3.7800	3.7800	3.7801	3.7802	3.7802
	40	30	3.7803	3.7804	3.7805	3.7805	3.7806	3.7807	3.7807	3.7808	3.7809	3.7810
	40	40	3.7810	3.7811	3.7812	3.7813	3.7813	3.7814	3.7815	3.7815	3.7816	3.7817
	40	50	3.7818	3.7818	3.7819	3.7820	3.7820	3.7821	3.7822	3.7823	3.7823	3.7824
1	41	0	3.7825	3.7825	3.7826	3.7827	3.7828	3.7828	3.7829	3.7830	3.7830	3.7831
	41	10	3.7832	3.7833	3.7833	3.7834	3.7835	3.7835	3.7836	3.7837	3.7838	3.7838
	41	20	3.7839	3.7840	3.7840	3.7841	3.7842	3.7843	3.7843	3.7844	3.7845	3.7845
	41	30	3.7846	3.7847	3.7848	3.7848	3.7849	3.7850	3.7850	3.7851	3.7852	3.7853
	41	40	3.7853	3.7854	3.7855	3.7855	3.7856	3.7857	3.7858	3.7858	3.7859	3.7860
	41	50	3.7860	3.7861	3.7862	3.7863	3.7863	3.7864	3.7865	3.7865	3.7866	3.7867
1	42	0	3.7868	3.7868	3.7869	3.7870	3.7870	3.7871	3.7872	3.7872	3.7873	3.7874
	42	10	3.7875	3.7875	3.7876	3.7877	3.7877	3.7878	3.7879	3.7880	3.7880	3.7881
	42	20	3.7882	3.7882	3.7883	3.7884	3.7885	3.7885	3.7886	3.7887	3.7887	3.7888
	42	30	3.7889	3.7889	3.7890	3.7891	3.7892	3.7892	3.7893	3.7894	3.7894	3.7895
	42	40	3.7896	3.7897	3.7897	3.7898	3.7899	3.7899	3.7900	3.7901	3.7901	3.7902
	42	50	3.7903	3.7904	3.7904	3.7905	3.7906	3.7906	3.7907	3.7908	3.7908	3.7909
1	43	0	3.7910	3.7911	3.7911	3.7912	3.7913	3.7913	3.7914	3.7915	3.7916	3.7916
	43	10	3.7917	3.7918	3.7918	3.7919	3.7920	3.7920	3.7921	3.7922	3.7923	3.7923
	43	20	3.7924	3.7925	3.7925	3.7926	3.7927	3.7927	3.7928	3.7929	3.7930	3.7930
	43	30	3.7931	3.7932	3.7932	3.7933	3.7934	3.7934	3.7935	3.7936	3.7937	3.7937
	43	40	3.7938	3.7939	3.7939	3.7940	3.7941	3.7941	3.7942	3.7943	3.7943	3.7944
	43	50	3.7945	3.7946	3.7946	3.7947	3.7948	3.7948	3.7949	3.7950	3.7950	3.7951
1	44	0	3.7952	3.7953	3.7953	3.7954	3.7955	3.7955	3.7956	3.7957	3.7957	3.7958
	44	10	3.7959	3.7959	3.7960	3.7961	3.7962	3.7962	3.7963	3.7964	3.7964	3.7965
	44	20	3.7966	3.7966	3.7967	3.7968	3.7969	3.7969	3.7970	3.7971	3.7971	3.7972
	44	30	3.7973	3.7973	3.7974	3.7975	3.7975	3.7976	3.7977	3.7978	3.7978	3.7979
	44	40	3.7980	3.7980	3.7981	3.7982	3.7982	3.7983	3.7984	3.7984	3.7985	3.7986
	44	50	3.7987	3.7987	3.7988	3.7989	3.7989	3.7990	3.7991	3.7991	3.7992	3.7993
1	45	0	3.7993	3.7994	3.7995	3.7995	3.7996	3.7997	3.7998	3.7998	3.7999	3.8000
	45	10	3.8000	3.8001	3.8002	3.8002	3.8003	3.8004	3.8004	3.8005	3.8006	3.8006
	45	20	3.8007	3.8008	3.8009	3.8009	3.8010	3.8011	3.8011	3.8012	3.8013	3.8013
	45	30	3.8014	3.8015	3.8015	3.8016	3.8017	3.8017	3.8018	3.8019	3.8020	3.8020
	45	40	3.8021	3.8022	3.8022	3.8023	3.8024	3.8024	3.8025	3.8026	3.8026	3.8027
	45	50	3.8028	3.8028	3.8029	3.8030	3.8030	3.8031	3.8032	3.8033	3.8033	3.8034
1	46	0	3.8035	3.8035	3.8036	3.8036	3.8037	3.8038	3.8039	3.8039	3.8040	3.8041
	46	10	3.8041	3.8042	3.8043	3.8043	3.8044	3.8045	3.8045	3.8046	3.8047	3.8048
	46	20	3.8048	3.8049	3.8050	3.8050	3.8051	3.8052	3.8052	3.8053	3.8054	3.8054
	46	30	3.8055	3.8056	3.8056	3.8057	3.8058	3.8058	3.8059	3.8060	3.8060	3.8061
	46	40	3.8062	3.8062	3.8063	3.8064	3.8065	3.8065	3.8066	3.8067	3.8067	3.8068
	46	50	3.8069	3.8069	3.8070	3.8071	3.8071	3.8072	3.8073	3.8073	3.8074	3.8075
1	47	0	3.8075	3.8076	3.8077	3.8077	3.8078	3.8079	3.8079	3.8080	3.8081	3.8081
	47	10	3.8082	3.8083	3.8083	3.8084	3.8085	3.8085	3.8086	3.8087	3.8088	3.8088
	47	20	3.8089	3.8090	3.8090	3.8091	3.8092	3.8092	3.8093	3.8094	3.8094	3.8095
	47	30	3.8096	3.8096	3.8097	3.8098	3.8098	3.8099	3.8099	3.8100	3.8101	3.8102
	47	40	3.8102	3.8103	3.8104	3.8104	3.8105	3.8106	3.8106	3.8107	3.8108	3.8108
	47	50	3.8109	3.8110	3.8110	3.8111	3.8112	3.8112	3.8113	3.8114	3.8114	3.8115
1	48	0	3.8116	3.8116	3.8117	3.8118	3.8118	3.8119	3.8120	3.8120	3.8121	3.8122
	48	10	3.8122	3.8123	3.8124	3.8124	3.8125	3.8126	3.8126	3.8127	3.8128	3.8128
	48	20	3.8129	3.8130	3.8130	3.8131	3.8132	3.8132	3.8133	3.8134	3.8134	3.8135
	48	30	3.8136	3.8136	3.8137	3.8138	3.8138	3.8139	3.8140	3.8140	3.8141	3.8142
	48	40	3.8142	3.8143	3.8144	3.8144	3.8145	3.8146	3.8146	3.8147	3.8148	3.8148
	48	50	3.8149	3.8150	3.8150	3.8151	3.8152	3.8152	3.8153	3.8154	3.8154	3.8155
1	49	0	3.8156	3.8156	3.8157	3.8158	3.8158	3.8159	3.8160	3.8160	3.8161	3.8162
	49	10	3.8162	3.8163	3.8164	3.8164	3.8165	3.8166	3.8166	3.8167	3.8168	3.8168
	49	20	3.8169	3.8170	3.8170	3.8171	3.8172	3.8172	3.8173	3.8174	3.8174	3.8175
	49	30	3.8176	3.8176	3.8177	3.8178	3.8178	3.8179	3.8180	3.8180	3.8181	3.8182
	49	40	3.8182	3.8183	3.8184	3.8184	3.8185	3.8185	3.8186	3.8187	3.8188	3.8188
	49	50	3.8189	3.8190	3.8190	3.8191	3.8191	3.8192	3.8193	3.8193	3.8194	3.8195

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
° ′ ″										
1ʰ 50ᵐ 0ˢ	3.8195	3.8196	3.8197	3.8197	3.8198	3.8199	3.8199	3.8200	3.8201	3.8201
50 10	3.8202	3.8203	3.8203	3.8204	3.8205	3.8205	3.8206	3.8207	3.8207	3.8208
50 20	3.8209	3.8209	3.8210	3.8211	3.8211	3.8212	3.8213	3.8213	3.8214	3.8214
50 30	3.8215	3.8216	3.8216	3.8217	3.8218	3.8218	3.8219	3.8220	3.8220	3.8221
50 40	3.8222	3.8222	3.8223	3.8224	3.8224	3.8225	3.8226	3.8226	3.8227	3.8228
50 50	3.8228	3.8229	3.8230	3.8230	3.8231	3.8231	3.8232	3.8233	3.8233	3.8234
1 51 0	3.8235	3.8235	3.8236	3.8237	3.8237	3.8238	3.8239	3.8239	3.8240	3.8241
51 10	3.8241	3.8242	3.8243	3.8243	3.8244	3.8245	3.8245	3.8246	3.8246	3.8247
51 20	3.8248	3.8248	3.8249	3.8250	3.8250	3.8251	3.8252	3.8252	3.8253	3.8254
51 30	3.8254	3.8255	3.8256	3.8256	3.8257	3.8258	3.8258	3.8259	3.8259	3.8260
51 40	3.8261	3.8261	3.8262	3.8263	3.8263	3.8264	3.8265	3.8265	3.8266	3.8267
51 50	3.8267	3.8268	3.8269	3.8269	3.8270	3.8270	3.8271	3.8272	3.8272	3.8273
1 52 0	3.8274	3.8274	3.8275	3.8276	3.8276	3.8277	3.8278	3.8278	3.8279	3.8280
52 10	3.8280	3.8281	3.8281	3.8282	3.8283	3.8283	3.8284	3.8285	3.8285	3.8286
52 20	3.8287	3.8287	3.8288	3.8289	3.8289	3.8290	3.8290	3.8291	3.8292	3.8292
52 30	3.8293	3.8294	3.8294	3.8295	3.8296	3.8296	3.8297	3.8298	3.8298	3.8299
52 40	3.8299	3.8300	3.8301	3.8301	3.8302	3.8303	3.8303	3.8304	3.8305	3.8305
52 50	3.8306	3.8307	3.8307	3.8308	3.8308	3.8309	3.8310	3.8310	3.8311	3.8312
1 53 0	3.8312	3.8313	3.8314	3.8314	3.8315	3.8315	3.8316	3.8317	3.8317	3.8318
53 10	3.8319	3.8319	3.8320	3.8321	3.8321	3.8322	3.8323	3.8323	3.8324	3.8324
53 20	3.8325	3.8326	3.8326	3.8327	3.8328	3.8328	3.8329	3.8330	3.8330	3.8331
53 30	3.8331	3.8332	3.8333	3.8333	3.8334	3.8335	3.8335	3.8336	3.8337	3.8337
53 40	3.8338	3.8338	3.8339	3.8340	3.8340	3.8341	3.8342	3.8342	3.8343	3.8344
53 50	3.8344	3.8345	3.8345	3.8346	3.8347	3.8347	3.8348	3.8349	3.8349	3.8350
1 54 0	3.8351	3.8351	3.8352	3.8352	3.8353	3.8354	3.8354	3.8355	3.8356	3.8356
54 10	3.8357	3.8358	3.8358	3.8359	3.8359	3.8360	3.8361	3.8361	3.8362	3.8363
54 20	3.8363	3.8364	3.8365	3.8365	3.8366	3.8366	3.8367	3.8368	3.8368	3.8369
54 30	3.8370	3.8370	3.8371	3.8371	3.8372	3.8373	3.8373	3.8374	3.8375	3.8375
54 40	3.8376	3.8377	3.8377	3.8378	3.8378	3.8379	3.8380	3.8380	3.8381	3.8382
54 50	3.8382	3.8383	3.8383	3.8384	3.8385	3.8385	3.8386	3.8387	3.8387	3.8388
1 55 0	3.8388	3.8389	3.8390	3.8390	3.8391	3.8392	3.8392	3.8393	3.8394	3.8394
55 10	3.8395	3.8395	3.8396	3.8397	3.8397	3.8398	3.8399	3.8399	3.8400	3.8400
55 20	3.8401	3.8402	3.8402	3.8403	3.8404	3.8404	3.8405	3.8405	3.8406	3.8407
55 30	3.8407	3.8408	3.8409	3.8409	3.8410	3.8410	3.8411	3.8412	3.8412	3.8413
55 40	3.8414	3.8414	3.8415	3.8415	3.8416	3.8417	3.8417	3.8418	3.8419	3.8419
55 50	3.8420	3.8420	3.8421	3.8422	3.8422	3.8423	3.8424	3.8424	3.8425	3.8425
1 56 0	3.8426	3.8427	3.8427	3.8428	3.8429	3.8429	3.8430	3.8430	3.8431	3.8432
56 10	3.8432	3.8433	3.8434	3.8434	3.8435	3.8435	3.8436	3.8437	3.8437	3.8438
56 20	3.8439	3.8439	3.8440	3.8440	3.8441	3.8442	3.8442	3.8443	3.8444	3.8444
56 30	3.8445	3.8445	3.8446	3.8447	3.8447	3.8448	3.8448	3.8449	3.8450	3.8450
56 40	3.8451	3.8452	3.8452	3.8453	3.8453	3.8454	3.8455	3.8455	3.8456	3.8457
56 50	3.8457	3.8458	3.8458	3.8459	3.8460	3.8460	3.8461	3.8462	3.8462	3.8463
1 57 0	3.8463	3.8464	3.8465	3.8465	3.8466	3.8466	3.8467	3.8468	3.8468	3.8469
57 10	3.8470	3.8470	3.8471	3.8471	3.8472	3.8473	3.8473	3.8474	3.8474	3.8475
57 20	3.8476	3.8476	3.8477	3.8478	3.8478	3.8479	3.8479	3.8480	3.8481	3.8481
57 30	3.8482	3.8483	3.8483	3.8484	3.8484	3.8485	3.8486	3.8486	3.8487	3.8487
57 40	3.8488	3.8489	3.8489	3.8490	3.8491	3.8491	3.8492	3.8492	3.8493	3.8494
57 50	3.8494	3.8495	3.8495	3.8496	3.8497	3.8497	3.8498	3.8499	3.8499	3.8500
1 58 0	3.8500	3.8501	3.8502	3.8502	3.8503	3.8503	3.8504	3.8505	3.8505	3.8506
58 10	3.8506	3.8507	3.8508	3.8508	3.8509	3.8510	3.8510	3.8511	3.8511	3.8512
58 20	3.8513	3.8513	3.8514	3.8514	3.8515	3.8516	3.8516	3.8517	3.8517	3.8518
58 30	3.8519	3.8519	3.8520	3.8521	3.8521	3.8522	3.8522	3.8523	3.8524	3.8524
58 40	3.8525	3.8525	3.8526	3.8527	3.8527	3.8528	3.8528	3.8529	3.8530	3.8530
58 50	3.8531	3.8532	3.8532	3.8533	3.8533	3.8534	3.8535	3.8535	3.8536	3.8536
1 59 0	3.8537	3.8538	3.8538	3.8539	3.8539	3.8540	3.8541	3.8541	3.8542	3.8542
59 10	3.8543	3.8544	3.8544	3.8545	3.8545	3.8546	3.8547	3.8547	3.8548	3.8549
59 20	3.8549	3.8550	3.8550	3.8551	3.8552	3.8552	3.8553	3.8553	3.8554	3.8555
59 30	3.8555	3.8556	3.8556	3.8557	3.8558	3.8558	3.8559	3.8559	3.8560	3.8561
59 40	3.8561	3.8562	3.8562	3.8563	3.8564	3.8564	3.8565	3.8565	3.8566	3.8567
59 50	3.8567	3.8568	3.8568	3.8569	3.8570	3.8570	3.8571	3.8572	3.8572	3.8573

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.			0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
°	′	″										
2^h	0^m	0^s	3.8573	3.8574	3.8575	3.8575	3.8576	3.8576	3.8577	3.8578	3.8578	3.8579
	0	10	3.8579	3.8580	3.8581	3.8581	3.8582	3.8582	3.8583	3.8584	3.8584	3.8585
	0	20	3.8585	3.8586	3.8587	3.8587	3.8588	3.8588	3.8589	3.8590	3.8590	3.8591
	0	30	3.8591	3.8592	3.8593	3.8593	3.8594	3.8594	3.8595	3.8596	3.8596	3.8597
	0	40	3.8597	3.8598	3.8599	3.8599	3.8600	3.8600	3.8601	3.8602	3.8602	3.8603
	0	50	3.8603	3.8604	3.8605	3.8605	3.8606	3.8606	3.8607	3.8608	3.8608	3.8609
2	1	0	3.8609	3.8610	3.8611	3.8611	3.8612	3.8612	3.8613	3.8614	3.8614	3.8615
	1	10	3.8615	3.8616	3.8617	3.8617	3.8618	3.8618	3.8619	3.8620	3.8620	3.8621
	1	20	3.8621	3.8622	3.8623	3.8623	3.8624	3.8624	3.8625	3.8625	3.8626	3.8627
	1	30	3.8627	3.8628	3.8628	3.8629	3.8630	3.8630	3.8631	3.8631	3.8632	3.8633
	1	40	3.8633	3.8634	3.8634	3.8635	3.8636	3.8636	3.8637	3.8637	3.8638	3.8639
	1	50	3.8639	3.8640	3.8640	3.8641	3.8642	3.8642	3.8643	3.8643	3.8644	3.8645
2	2	0	3.8645	3.8646	3.8646	3.8647	3.8647	3.8648	3.8649	3.8649	3.8650	3.8650
	2	10	3.8651	3.8652	3.8652	3.8653	3.8653	3.8654	3.8655	3.8655	3.8656	3.8656
	2	20	3.8657	3.8658	3.8658	3.8659	3.8659	3.8660	3.8661	3.8661	3.8662	3.8662
	2	30	3.8663	3.8663	3.8664	3.8665	3.8665	3.8666	3.8666	3.8667	3.8668	3.8668
	2	40	3.8669	3.8669	3.8670	3.8671	3.8671	3.8672	3.8672	3.8673	3.8673	3.8674
	2	50	3.8675	3.8675	3.8676	3.8676	3.8677	3.8678	3.8678	3.8679	3.8679	3.8680
2	3	0	3.8681	3.8681	3.8682	3.8682	3.8683	3.8684	3.8684	3.8685	3.8685	3.8686
	3	10	3.8686	3.8687	3.8688	3.8688	3.8689	3.8689	3.8690	3.8691	3.8691	3.8692
	3	20	3.8692	3.8693	3.8693	3.8694	3.8695	3.8695	3.8696	3.8696	3.8697	3.8698
	3	30	3.8698	3.8699	3.8699	3.8700	3.8701	3.8701	3.8702	3.8702	3.8703	3.8703
	3	40	3.8704	3.8705	3.8705	3.8706	3.8706	3.8707	3.8708	3.8708	3.8709	3.8709
	3	50	3.8710	3.8710	3.8711	3.8712	3.8712	3.8713	3.8713	3.8714	3.8715	3.8715
2	4	0	3.8716	3.8716	3.8717	3.8717	3.8718	3.8719	3.8719	3.8720	3.8720	3.8721
	4	10	3.8722	3.8722	3.8723	3.8723	3.8724	3.8724	3.8725	3.8726	3.8726	3.8727
	4	20	3.8727	3.8728	3.8729	3.8729	3.8730	3.8730	3.8731	3.8731	3.8732	3.8733
	4	30	3.8733	3.8734	3.8734	3.8735	3.8736	3.8736	3.8737	3.8737	3.8738	3.8738
	4	40	3.8739	3.8740	3.8740	3.8741	3.8741	3.8742	3.8742	3.8743	3.8744	3.8744
	4	50	3.8745	3.8745	3.8746	3.8747	3.8747	3.8748	3.8748	3.8749	3.8749	3.8750
2	5	0	3.8751	3.8751	3.8752	3.8752	3.8753	3.8754	3.8754	3.8755	3.8755	3.8756
	5	10	3.8756	3.8757	3.8758	3.8758	3.8759	3.8759	3.8760	3.8760	3.8761	3.8762
	5	20	3.8762	3.8763	3.8763	3.8764	3.8764	3.8765	3.8766	3.8766	3.8767	3.8767
	5	30	3.8768	3.8769	3.8769	3.8770	3.8770	3.8771	3.8771	3.8772	3.8773	3.8773
	5	40	3.8774	3.8774	3.8775	3.8775	3.8776	3.8777	3.8777	3.8778	3.8778	3.8779
	5	50	3.8779	3.8780	3.8781	3.8781	3.8782	3.8782	3.8783	3.8783	3.8784	3.8785
2	6	0	3.8785	3.8786	3.8786	3.8787	3.8788	3.8788	3.8789	3.8789	3.8790	3.8790
	6	10	3.8791	3.8792	3.8792	3.8793	3.8793	3.8794	3.8794	3.8795	3.8796	3.8796
	6	20	3.8797	3.8797	3.8798	3.8798	3.8799	3.8800	3.8800	3.8801	3.8801	3.8802
	6	30	3.8802	3.8803	3.8804	3.8804	3.8805	3.8805	3.8806	3.8806	3.8807	3.8808
	6	40	3.8808	3.8809	3.8809	3.8810	3.8810	3.8811	3.8812	3.8812	3.8813	3.8813
	6	50	3.8814	3.8814	3.8815	3.8816	3.8816	3.8817	3.8817	3.8818	3.8818	3.8819
2	7	0	3.8820	3.8820	3.8821	3.8821	3.8822	3.8822	3.8823	3.8824	3.8824	3.8825
	7	10	3.8825	3.8826	3.8826	3.8827	3.8828	3.8828	3.8829	3.8829	3.8830	3.8830
	7	20	3.8831	3.8832	3.8832	3.8833	3.8833	3.8834	3.8834	3.8835	3.8835	3.8836
	7	30	3.8837	3.8837	3.8838	3.8838	3.8839	3.8839	3.8840	3.8841	3.8841	3.8842
	7	40	3.8842	3.8843	3.8843	3.8844	3.8845	3.8845	3.8846	3.8846	3.8847	3.8847
	7	50	3.8848	3.8849	3.8849	3.8850	3.8850	3.8851	3.8851	3.8852	3.8852	3.8853
2	8	0	3.8854	3.8854	3.8855	3.8855	3.8856	3.8856	3.8857	3.8858	3.8858	3.8859
	8	10	3.8859	3.8860	3.8860	3.8861	3.8862	3.8862	3.8863	3.8863	3.8864	3.8864
	8	20	3.8865	3.8865	3.8866	3.8867	3.8867	3.8868	3.8868	3.8869	3.8869	3.8870
	8	30	3.8871	3.8871	3.8872	3.8872	3.8873	3.8873	3.8874	3.8874	3.8875	3.8876
	8	40	3.8876	3.8877	3.8877	3.8878	3.8878	3.8879	3.8880	3.8880	3.8881	3.8881
	8	50	3.8882	3.8882	3.8883	3.8883	3.8884	3.8885	3.8885	3.8886	3.8886	3.8887
2	9	0	3.8887	3.8888	3.8889	3.8889	3.8890	3.8890	3.8891	3.8891	3.8892	3.8892
	9	10	3.8893	3.8894	3.8894	3.8895	3.8895	3.8896	3.8896	3.8897	3.8897	3.8898
	9	20	3.8899	3.8899	3.8900	3.8900	3.8901	3.8901	3.8902	3.8903	3.8903	3.8904
	9	30	3.8904	3.8905	3.8905	3.8906	3.8906	3.8907	3.8908	3.8908	3.8909	3.8909
	9	40	3.8910	3.8910	3.8911	3.8911	3.8912	3.8912	3.8913	3.8914	3.8914	3.8915
	9	50	3.8915	3.8916	3.8916	3.8917	3.8918	3.8918	3.8919	3.8919	3.8920	3.8920

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.			0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
°	′	″										
2h	10m	0s	3.8921	3.8922	3.8922	3.8923	3.8923	3.8924	3.8924	3.8925	3.8925	3.8926
	10	10	3.8927	3.8927	3.8928	3.8928	3.8929	3.8929	3.8930	3.8930	3.8931	3.8932
	10	20	3.8932	3.8933	3.8933	3.8934	3.8934	3.8935	3.8935	3.8936	3.8937	3.8937
	10	30	3.8938	3.8938	3.8939	3.8939	3.8940	3.8940	3.8941	3.8941	3.8942	3.8943
	10	40	3.8943	3.8944	3.8944	3.8945	3.8945	3.8946	3.8946	3.8947	3.8948	3.8948
	10	50	3.8949	3.8949	3.8950	3.8950	3.8951	3.8951	3.8952	3.8953	3.8953	3.8954
2	11	0	3.8954	3.8955	3.8955	3.8956	3.8956	3.8957	3.8958	3.8958	3.8959	3.8959
	11	10	3.8960	3.8960	3.8961	3.8961	3.8962	3.8963	3.8963	3.8964	3.8964	3.8965
	11	20	3.8965	3.8966	3.8966	3.8967	3.8967	3.8968	3.8969	3.8969	3.8970	3.8970
	11	30	3.8971	3.8971	3.8972	3.8972	3.8973	3.8974	3.8974	3.8975	3.8975	3.8976
	11	40	3.8976	3.8977	3.8977	3.8978	3.8978	3.8979	3.8980	3.8980	3.8981	3.8981
	11	50	3.8982	3.8982	3.8983	3.8983	3.8984	3.8985	3.8985	3.8986	3.8986	3.8987
2	12	0	3.8987	3.8988	3.8988	3.8989	3.8989	3.8990	3.8991	3.8991	3.8992	3.8992
	12	10	3.8993	3.8993	3.8994	3.8994	3.8995	3.8995	3.8996	3.8997	3.8997	3.8998
	12	20	3.8998	3.8999	3.8999	3.9000	3.9000	3.9001	3.9001	3.9002	3.9003	3.9003
	12	30	3.9004	3.9004	3.9005	3.9005	3.9006	3.9006	3.9007	3.9007	3.9008	3.9009
	12	40	3.9009	3.9010	3.9010	3.9011	3.9011	3.9012	3.9012	3.9013	3.9013	3.9014
	12	50	3.9015	3.9015	3.9016	3.9016	3.9017	3.9017	3.9018	3.9018	3.9019	3.9019
2	13	0	3.9020	3.9021	3.9021	3.9022	3.9022	3.9023	3.9023	3.9024	3.9024	3.9025
	13	10	3.9025	3.9026	3.9027	3.9027	3.9028	3.9028	3.9029	3.9029	3.9030	3.9030
	13	20	3.9031	3.9031	3.9032	3.9033	3.9033	3.9034	3.9034	3.9035	3.9035	3.9036
	13	30	3.9036	3.9037	3.9037	3.9038	3.9038	3.9039	3.9040	3.9040	3.9041	3.9041
	13	40	3.9042	3.9042	3.9043	3.9043	3.9044	3.9044	3.9045	3.9046	3.9046	3.9047
	13	50	3.9047	3.9048	3.9048	3.9049	3.9049	3.9050	3.9050	3.9051	3.9051	3.9052
2	14	0	3.9053	3.9053	3.9054	3.9054	3.9055	3.9055	3.9056	3.9056	3.9057	3.9057
	14	10	3.9058	3.9058	3.9059	3.9060	3.9060	3.9061	3.9061	3.9062	3.9062	3.9063
	14	20	3.9063	3.9064	3.9064	3.9065	3.9066	3.9066	3.9067	3.9067	3.9068	3.9068
	14	30	3.9069	3.9069	3.9070	3.9070	3.9071	3.9071	3.9072	3.9073	3.9073	3.9074
	14	40	3.9074	3.9075	3.9075	3.9076	3.9076	3.9077	3.9077	3.9078	3.9078	3.9079
	14	50	3.9079	3.9080	3.9081	3.9081	3.9082	3.9082	3.9083	3.9083	3.9084	3.9084
2	15	0	3.9085	3.9085	3.9086	3.9086	3.9087	3.9088	3.9088	3.9089	3.9089	3.9090
	15	10	3.9090	3.9091	3.9091	3.9092	3.9092	3.9093	3.9093	3.9094	3.9094	3.9095
	15	20	3.9096	3.9096	3.9097	3.9097	3.9098	3.9098	3.9099	3.9099	3.9100	3.9100
	15	30	3.9101	3.9101	3.9102	3.9103	3.9103	3.9104	3.9104	3.9105	3.9105	3.9106
	15	40	3.9106	3.9107	3.9107	3.9108	3.9108	3.9109	3.9109	3.9110	3.9111	3.9111
	15	50	3.9112	3.9112	3.9113	3.9113	3.9114	3.9114	3.9115	3.9115	3.9116	3.9116
2	16	0	3.9117	3.9117	3.9118	3.9118	3.9119	3.9120	3.9120	3.9121	3.9121	3.9122
	16	10	3.9122	3.9123	3.9123	3.9124	3.9124	3.9125	3.9125	3.9126	3.9126	3.9127
	16	20	3.9128	3.9128	3.9129	3.9129	3.9130	3.9130	3.9131	3.9131	3.9132	3.9132
	16	30	3.9133	3.9133	3.9134	3.9134	3.9135	3.9135	3.9136	3.9137	3.9137	3.9138
	16	40	3.9138	3.9139	3.9139	3.9140	3.9140	3.9141	3.9141	3.9142	3.9142	3.9143
	16	50	3.9143	3.9144	3.9144	3.9145	3.9146	3.9146	3.9147	3.9147	3.9148	3.9148
2	17	0	3.9149	3.9149	3.9150	3.9150	3.9151	3.9151	3.9152	3.9152	3.9153	3.9153
	17	10	3.9154	3.9155	3.9155	3.9156	3.9156	3.9157	3.9157	3.9158	3.9158	3.9159
	17	20	3.9159	3.9160	3.9160	3.9161	3.9161	3.9162	3.9162	3.9163	3.9163	3.9164
	17	30	3.9165	3.9165	3.9166	3.9166	3.9167	3.9167	3.9168	3.9168	3.9169	3.9169
	17	40	3.9170	3.9170	3.9171	3.9171	3.9172	3.9172	3.9173	3.9173	3.9174	3.9175
	17	50	3.9175	3.9176	3.9176	3.9177	3.9177	3.9178	3.9178	3.9179	3.9179	3.9180
2	18	0	3.9180	3.9181	3.9181	3.9182	3.9182	3.9183	3.9183	3.9184	3.9184	3.9185
	18	10	3.9186	3.9186	3.9187	3.9187	3.9188	3.9188	3.9189	3.9189	3.9190	3.9190
	18	20	3.9191	3.9191	3.9192	3.9192	3.9193	3.9193	3.9194	3.9194	3.9195	3.9195
	18	30	3.9196	3.9197	3.9197	3.9198	3.9198	3.9199	3.9199	3.9200	3.9200	3.9201
	18	40	3.9201	3.9202	3.9202	3.9203	3.9203	3.9204	3.9204	3.9205	3.9205	3.9206
	18	50	3.9206	3.9207	3.9207	3.9208	3.9209	3.9209	3.9210	3.9210	3.9211	3.9211
2	19	0	3.9212	3.9212	3.9213	3.9213	3.9214	3.9214	3.9215	3.9215	3.9216	3.9216
	19	10	3.9217	3.9217	3.9218	3.9218	3.9219	3.9219	3.9220	3.9221	3.9221	3.9222
	19	20	3.9222	3.9223	3.9223	3.9224	3.9224	3.9225	3.9225	3.9226	3.9226	3.9227
	19	30	3.9227	3.9228	3.9228	3.9229	3.9229	3.9230	3.9230	3.9231	3.9231	3.9232
	19	40	3.9232	3.9233	3.9233	3.9234	3.9235	3.9235	3.9236	3.9236	3.9237	3.9237
	19	50	3.9238	3.9238	3.9239	3.9239	3.9240	3.9240	3.9241	3.9241	3.9242	3.9242

Logarithms of Small Arcs in Space or Time.

Arc.			0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
°	′	″										
2^h	20^m	0^s	3.9243	3.9243	3.9244	3.9244	3.9245	3.9245	3.9246	3.9246	3.9247	3.9247
	20	10	3.9248	3.9248	3.9249	3.9250	3.9250	3.9251	3.9251	3.9252	3.9252	3.9253
	20	20	3.9253	3.9254	3.9254	3.9255	3.9255	3.9256	3.9256	3.9257	3.9257	3.9258
	20	30	3.9258	3.9259	3.9259	3.9260	3.9260	3.9261	3.9261	3.9262	3.9262	3.9263
	20	40	3.9263	3.9264	3.9264	3.9265	3.9265	3.9266	3.9267	3.9267	3.9268	3.9268
	20	50	3.9269	3.9269	3.9270	3.9270	3.9271	3.9271	3.9272	3.9272	3.9273	3.9273
2	21	0	3.9274	3.9274	3.9275	3.9275	3.9276	3.9276	3.9277	3.9277	3.9278	3.9278
	21	10	3.9279	3.9279	3.9280	3.9280	3.9281	3.9281	3.9282	3.9282	3.9283	3.9283
	21	20	3.9284	3.9284	3.9285	3.9285	3.9286	3.9287	3.9287	3.9288	3.9288	3.9289
	21	30	3.9289	3.9290	3.9290	3.9291	3.9291	3.9292	3.9292	3.9293	3.9293	3.9294
	21	40	3.9294	3.9295	3.9295	3.9296	3.9296	3.9297	3.9297	3.9298	3.9298	3.9299
	21	50	3.9299	3.9300	3.9300	3.9301	3.9301	3.9302	3.9302	3.9303	3.9303	3.9304
2	22	0	3.9304	3.9305	3.9305	3.9306	3.9306	3.9307	3.9307	3.9308	3.9308	3.9309
	22	10	3.9309	3.9310	3.9311	3.9311	3.9312	3.9312	3.9313	3.9313	3.9314	3.9314
	22	20	3.9315	3.9315	3.9316	3.9316	3.9317	3.9317	3.9318	3.9318	3.9319	3.9319
	22	30	3.9320	3.9320	3.9321	3.9321	3.9322	3.9322	3.9323	3.9323	3.9324	3.9324
	22	40	3.9325	3.9325	3.9326	3.9326	3.9327	3.9327	3.9328	3.9328	3.9329	3.9329
	22	50	3.9330	3.9330	3.9331	3.9331	3.9332	3.9332	3.9333	3.9333	3.9334	3.9334
2	23	0	3.9335	3.9335	3.9336	3.9336	3.9337	3.9337	3.9338	3.9338	3.9339	3.9339
	23	10	3.9340	3.9340	3.9341	3.9341	3.9342	3.9342	3.9343	3.9343	3.9344	3.9344
	23	20	3.9345	3.9345	3.9346	3.9346	3.9347	3.9348	3.9348	3.9349	3.9349	3.9350
	23	30	3.9350	3.9351	3.9351	3.9352	3.9352	3.9353	3.9353	3.9354	3.9354	3.9355
	23	40	3.9355	3.9356	3.9356	3.9357	3.9357	3.9358	3.9358	3.9359	3.9359	3.9360
	23	50	3.9360	3.9361	3.9361	3.9362	3.9362	3.9363	3.9363	3.9364	3.9364	3.9365
2	24	0	3.9365	3.9366	3.9366	3.9367	3.9367	3.9368	3.9368	3.9369	3.9369	3.9370
	24	10	3.9370	3.9371	3.9371	3.9372	3.9372	3.9373	3.9373	3.9374	3.9374	3.9375
	24	20	3.9375	3.9376	3.9376	3.9377	3.9377	3.9378	3.9378	3.9379	3.9379	3.9380
	24	30	3.9380	3.9381	3.9381	3.9382	3.9382	3.9383	3.9383	3.9384	3.9384	3.9385
	24	40	3.9385	3.9386	3.9386	3.9387	3.9387	3.9388	3.9388	3.9389	3.9389	3.9390
	24	50	3.9390	3.9391	3.9391	3.9392	3.9392	3.9393	3.9393	3.9394	3.9394	3.9395
2	25	0	3.9395	3.9396	3.9396	3.9397	3.9397	3.9398	3.9398	3.9399	3.9399	3.9400
	25	10	3.9400	3.9401	3.9401	3.9402	3.9402	3.9403	3.9403	3.9404	3.9404	3.9405
	25	20	3.9405	3.9406	3.9406	3.9407	3.9407	3.9408	3.9408	3.9409	3.9409	3.9410
	25	30	3.9410	3.9411	3.9411	3.9412	3.9412	3.9413	3.9413	3.9414	3.9414	3.9415
	25	40	3.9415	3.9416	3.9416	3.9417	3.9417	3.9418	3.9418	3.9419	3.9419	3.9420
	25	50	3.9420	3.9421	3.9421	3.9422	3.9422	3.9423	3.9423	3.9424	3.9424	3.9425
2	26	0	3.9425	3.9426	3.9426	3.9427	3.9427	3.9428	3.9428	3.9429	3.9429	3.9430
	26	10	3.9430	3.9430	3.9431	3.9431	3.9432	3.9432	3.9433	3.9433	3.9434	3.9434
	26	20	3.9435	3.9435	3.9436	3.9436	3.9437	3.9437	3.9438	3.9438	3.9439	3.9439
	26	30	3.9440	3.9440	3.9441	3.9441	3.9442	3.9442	3.9443	3.9443	3.9444	3.9444
	26	40	3.9445	3.9445	3.9446	3.9446	3.9447	3.9447	3.9448	3.9448	3.9449	3.9449
	26	50	3.9450	3.9450	3.9451	3.9451	3.9452	3.9452	3.9453	3.9453	3.9454	3.9454
2	27	0	3.9455	3.9455	3.9456	3.9456	3.9457	3.9457	3.9458	3.9458	3.9459	3.9459
	27	10	3.9460	3.9460	3.9461	3.9461	3.9462	3.9462	3.9463	3.9463	3.9464	3.9464
	27	20	3.9465	3.9465	3.9466	3.9466	3.9466	3.9467	3.9467	3.9468	3.9468	3.9469
	27	30	3.9469	3.9470	3.9470	3.9471	3.9471	3.9472	3.9472	3.9473	3.9473	3.9474
	27	40	3.9474	3.9475	3.9475	3.9476	3.9476	3.9477	3.9477	3.9478	3.9478	3.9479
	27	50	3.9479	3.9480	3.9480	3.9481	3.9481	3.9482	3.9482	3.9483	3.9483	3.9484
2	28	0	3.9484	3.9485	3.9485	3.9486	3.9486	3.9487	3.9487	3.9488	3.9488	3.9489
	28	10	3.9489	3.9490	3.9490	3.9490	3.9491	3.9491	3.9492	3.9492	3.9493	3.9493
	28	20	3.9494	3.9494	3.9495	3.9495	3.9496	3.9496	3.9497	3.9497	3.9498	3.9498
	28	30	3.9499	3.9499	3.9500	3.9500	3.9501	3.9501	3.9502	3.9502	3.9503	3.9503
	28	40	3.9504	3.9504	3.9505	3.9505	3.9506	3.9506	3.9507	3.9507	3.9508	3.9508
	28	50	3.9509	3.9509	3.9509	3.9510	3.9510	3.9511	3.9511	3.9512	3.9512	3.9513
2	29	0	3.9513	3.9514	3.9514	3.9515	3.9515	3.9516	3.9516	3.9517	3.9517	3.9518
	29	10	3.9518	3.9519	3.9519	3.9520	3.9520	3.9521	3.9521	3.9522	3.9522	3.9523
	29	20	3.9523	3.9524	3.9524	3.9525	3.9525	3.9526	3.9526	3.9526	3.9527	3.9527
	29	30	3.9528	3.9528	3.9529	3.9529	3.9530	3.9530	3.9531	3.9531	3.9532	3.9532
	29	40	3.9533	3.9533	3.9534	3.9534	3.9535	3.9435	3.9536	3.9536	3.9537	3.9537
	29	50	3.9538	3.9538	3.9539	3.9539	3.9540	3.9540	3.9540	3.9541	3.9541	3.9542

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
° ′ ″										
2^h 30^m 0^s	3.9542	3.9543	3.9543	3.9544	3.9544	3.9545	3.9545	3.9546	3.9546	3.9547
30 10	3.9547	3.9548	3.9548	3.9549	3.9549	3.9550	3.9550	3.9551	3.9551	3.9552
30 20	3.9552	3.9553	3.9553	3.9554	3.9554	3.9554	3.9555	3.9555	3.9556	3.9556
30 30	3.9557	3.9557	3.9558	3.9558	3.9559	3.9559	3.9560	3.9560	3.9561	3.9561
30 40	3.9562	3.9562	3.9563	3.9563	3.9564	3.9564	3.9565	3.9565	3.9566	3.9566
30 50	3.9566	3.9567	3.9567	3.9568	3.9568	3.9569	3.9569	3.9570	3.9570	3.9571
2 31 0	3.9571	3.9572	3.9572	3.9573	3.9573	3.9574	3.9574	3.9575	3.9575	3.9576
31 10	3.9576	3.9577	3.9577	3.9578	3.9578	3.9578	3.9579	3.9579	3.9580	3.9580
31 20	3.9581	3.9581	3.9582	3.9582	3.9583	3.9583	3.9584	3.9584	3.9585	3.9585
31 30	3.9586	3.9586	3.9587	3.9587	3.9588	3.9588	3.9589	3.9589	3.9589	3.9590
31 40	3.9590	3.9591	3.9591	3.9592	3.9592	3.9593	3.9593	3.9594	3.9594	3.9595
31 50	3.9595	3.9596	3.9596	3.9597	3.9597	3.9598	3.9598	3.9599	3.9599	3.9599
2 32 0	3.9600	3.9600	3.9601	3.9601	3.9602	3.9602	3.9603	3.9603	3.9604	3.9604
32 10	3.9605	3.9605	3.9606	3.9606	3.9607	3.9607	3.9608	3.9608	3.9609	3.9609
32 20	3.9609	3.9610	3.9610	3.9611	3.9611	3.9612	3.9612	3.9613	3.9613	3.9614
32 30	3.9614	3.9615	3.9615	3.9616	3.9616	3.9617	3.9617	3.9618	3.9618	3.9618
32 40	3.9619	3.9619	3.9620	3.9620	3.9621	3.9621	3.9622	3.9622	3.9623	3.9623
32 50	3.9624	3.9624	3.9625	3.9625	3.9626	3.9626	3.9627	3.9627	3.9627	3.9628
2 33 0	3.9628	3.9629	3.9629	3.9630	3.9630	3.9631	3.9631	3.9632	3.9632	3.9633
33 10	3.9633	3.9634	3.9634	3.9634	3.9635	3.9635	3.9636	3.9636	3.9637	3.9637
33 20	3.9638	3.9638	3.9639	3.9639	3.9640	3.9640	3.9641	3.9641	3.9642	3.9642
33 30	3.9642	3.9643	3.9643	3.9644	3.9644	3.9645	3.9645	3.9646	3.9646	3.9647
33 40	3.9647	3.9648	3.9648	3.9649	3.9649	3.9650	3.9650	3.9651	3.9651	3.9652
33 50	3.9652	3.9653	3.9653	3.9653	3.9654	3.9654	3.9655	3.9655	3.9656	3.9656
2 34 0	3.9657	3.9657	3.9658	3.9658	3.9658	3.9659	3.9659	3.9660	3.9660	3.9661
34 10	3.9661	3.9662	3.9662	3.9663	3.9663	3.9664	3.9664	3.9665	3.9665	3.9665
34 20	3.9666	3.9666	3.9667	3.9667	3.9668	3.9668	3.9669	3.9669	3.9670	3.9670
34 30	3.9671	3.9671	3.9672	3.9672	3.9672	3.9673	3.9673	3.9674	3.9674	3.9675
34 40	3.9675	3.9676	3.9676	3.9677	3.9677	3.9678	3.9678	3.9679	3.9679	3.9680
34 50	3.9680	3.9681	3.9681	3.9682	3.9682	3.9682	3.9683	3.9683	3.9684	3.9684
2 35 0	3.9685	3.9685	3.9686	3.9686	3.9687	3.9687	3.9688	3.9688	3.9689	3.9689
35 10	3.9689	3.9690	3.9690	3.9691	3.9691	3.9692	3.9692	3.9693	3.9693	3.9694
35 20	3.9694	3.9695	3.9695	3.9696	3.9696	3.9696	3.9697	3.9697	3.9698	3.9698
35 30	3.9699	3.9699	3.9700	3.9700	3.9701	3.9701	3.9702	3.9702	3.9703	3.9703
35 40	3.9703	3.9704	3.9704	3.9705	3.9705	3.9706	3.9706	3.9707	3.9707	3.9708
35 50	3.9708	3.9709	3.9709	3.9710	3.9710	3.9710	3.9711	3.9711	3.9712	3.9712
2 36 0	3.9713	3.9713	3.9714	3.9714	3.9715	3.9715	3.9716	3.9716	3.9716	3.9717
36 10	3.9717	3.9718	3.9718	3.9719	3.9719	3.9720	3.9720	3.9721	3.9721	3.9722
36 20	3.9722	3.9722	3.9723	3.9723	3.9724	3.9724	3.9725	3.9725	3.9726	3.9726
36 30	3.9727	3.9727	3.9728	3.9728	3.9729	3.9729	3.9729	3.9730	3.9730	3.9731
36 40	3.9731	3.9732	3.9732	3.9733	3.9733	3.9734	3.9734	3.9735	3.9735	3.9735
36 50	3.9736	3.9736	3.9737	3.9737	3.9738	3.9738	3.9739	3.9739	3.9740	3.9740
2 37 0	3.9741	3.9741	3.9741	3.9742	3.9742	3.9743	3.9743	3.9744	3.9744	3.9745
37 10	3.9745	3.9746	3.9746	3.9746	3.9747	3.9747	3.9748	3.9748	3.9749	3.9749
37 20	3.9750	3.9750	3.9751	3.9751	3.9752	3.9752	3.9752	3.9753	3.9753	3.9754
37 30	3.9754	3.9755	3.9755	3.9756	3.9756	3.9757	3.9757	3.9758	3.9758	3.9758
37 40	3.9759	3.9759	3.9760	3.9760	3.9761	3.9761	3.9762	3.9762	3.9763	3.9763
37 50	3.9763	3.9764	3.9764	3.9765	3.9765	3.9766	3.9766	3.9767	3.9767	3.9768
2 38 0	3.9768	3.9769	3.9769	3.9769	3.9770	3.9770	3.9771	3.9771	3.9772	3.9772
38 10	3.9773	3.9773	3.9774	3.9774	3.9774	3.9775	3.9775	3.9776	3.9776	3.9777
38 20	3.9777	3.9778	3.9778	3.9779	3.9779	3.9779	3.9780	3.9780	3.9781	3.9781
38 30	3.9782	3.9782	3.9783	3.9783	3.9784	3.9784	3.9785	3.9785	3.9785	3.9786
38 40	3.9786	3.9787	3.9787	3.9788	3.9788	3.9789	3.9789	3.9790	3.9790	3.9790
38 50	3.9791	3.9791	3.9792	3.9792	3.9793	3.9793	3.9794	3.9794	3.9795	3.9795
2 39 0	3.9795	3.9796	3.9796	3.9797	3.9797	3.9798	3.9798	3.9799	3.9799	3.9800
39 10	3.9800	3.9800	3.9801	3.9801	3.9802	3.9802	3.9803	3.9803	3.9804	3.9804
39 20	3.9805	3.9805	3.9805	3.9806	3.9806	3.9807	3.9807	3.9808	3.9808	3.9809
39 30	3.9809	3.9810	3.9810	3.9810	3.9811	3.9811	3.9812	3.9812	3.9813	3.9813
39 40	3.9814	3.9814	3.9815	3.9815	3.9815	3.9816	3.9816	3.9817	3.9817	3.9818
39 50	3.9818	3.9819	3.9819	3.9819	3.9820	3.9820	3.9821	3.9821	3.9822	3.9822

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.			0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
°	′	″										
2h	40m	0s	3.9823	3.9823	3.9824	3.9824	3.9825	3.9825	3.9825	3.9826	3.9826	3.9827
	40	10	3.9827	3.9828	3.9828	3.9829	3.9829	3.9829	3.9830	3.9830	3.9831	3.9831
	40	20	3.9832	3.9832	3.9833	3.9833	3.9834	3.9834	3.9834	3.9835	3.9835	3.9836
	40	30	3.9836	3.9837	3.9837	3.9838	3.9838	3.9839	3.9839	3.9839	3.9840	3.9840
	40	40	3.9841	3.9841	3.9842	3.9842	3.9843	3.9843	3.9843	3.9844	3.9844	3.9845
	40	50	3.9845	3.9846	3.9846	3.9847	3.9847	3.9848	3.9848	3.9848	3.9849	3.9849
2	41	0	3.9850	3.9850	3.9851	3.9851	3.9852	3.9852	3.9852	3.9853	3.9853	3.9854
	41	10	3.9854	3.9855	3.9855	3.9856	3.9856	3.9857	3.9857	3.9857	3.9858	3.9858
	41	20	3.9859	3.9859	3.9860	3.9860	3.9861	3.9861	3.9861	3.9862	3.9862	3.9863
	41	30	3.9863	3.9864	3.9864	3.9865	3.9865	3.9865	3.9866	3.9866	3.9867	3.9867
	41	40	3.9868	3.9868	3.9869	3.9869	3.9870	3.9870	3.9870	3.9871	3.9871	3.9872
	41	50	3.9872	3.9873	3.9873	3.9874	3.9874	3.9874	3.9875	3.9875	3.9876	3.9876
2	42	0	3.9877	3.9877	3.9878	3.9878	3.9878	3.9879	3.9879	3.9880	3.9880	3.9881
	42	10	3.9881	3.9882	3.9882	3.9882	3.9883	3.9883	3.9884	3.9884	3.9885	3.9885
	42	20	3.9886	3.9886	3.9886	3.9887	3.9887	3.9888	3.9888	3.9889	3.9889	3.9890
	42	30	3.9890	3.9890	3.9891	3.9891	3.9892	3.9892	3.9893	3.9893	3.9894	3.9894
	42	40	3.9894	3.9895	3.9895	3.9896	3.9896	3.9897	3.9897	3.9898	3.9898	3.9898
	42	50	3.9899	3.9899	3.9900	3.9900	3.9901	3.9901	3.9902	3.9902	3.9903	3.9903
2	43	0	3.9903	3.9904	3.9904	3.9905	3.9905	3.9906	3.9906	3.9906	3.9907	3.9907
	43	10	3.9908	3.9908	3.9909	3.9909	3.9910	3.9910	3.9910	3.9911	3.9911	3.9912
	43	20	3.9912	3.9913	3.9913	3.9914	3.9914	3.9914	3.9915	3.9915	3.9916	3.9916
	43	30	3.9917	3.9917	3.9918	3.9918	3.9918	3.9919	3.9919	3.9920	3.9920	3.9921
	43	40	3.9921	3.9922	3.9922	3.9922	3.9923	3.9923	3.9924	3.9924	3.9925	3.9925
	43	50	3.9926	3.9926	3.9926	3.9927	3.9927	3.9928	3.9928	3.9929	3.9929	3.9930
2	44	0	3.9930	3.9930	3.9931	3.9931	3.9932	3.9932	3.9933	3.9933	3.9933	3.9934
	44	10	3.9934	3.9935	3.9935	3.9936	3.9936	3.9937	3.9937	3.9937	3.9938	3.9938
	44	20	3.9939	3.9939	3.9940	3.9940	3.9941	3.9941	3.9941	3.9942	3.9942	3.9943
	44	30	3.9943	3.9944	3.9944	3.9944	3.9945	3.9945	3.9946	3.9946	3.9947	3.9947
	44	40	3.9948	3.9948	3.9948	3.9949	3.9949	3.9950	3.9950	3.9951	3.9951	3.9952
	44	50	3.9952	3.9952	3.9953	3.9953	3.9954	3.9954	3.9955	3.9955	3.9955	3.9956
2	45	0	3.9956	3.9957	3.9957	3.9958	3.9958	3.9959	3.9959	3.9959	3.9960	3.9960
	45	10	3.9961	3.9961	3.9962	3.9962	3.9962	3.9963	3.9963	3.9964	3.9964	3.9965
	45	20	3.9965	3.9966	3.9966	3.9966	3.9967	3.9967	3.9968	3.9968	3.9969	3.9969
	45	30	3.9969	3.9970	3.9970	3.9971	3.9971	3.9972	3.9972	3.9973	3.9973	3.9973
	45	40	3.9974	3.9974	3.9975	3.9975	3.9976	3.9976	3.9976	3.9977	3.9977	3.9978
	45	50	3.9978	3.9979	3.9979	3.9980	3.9980	3.9980	3.9981	3.9981	3.9982	3.9982
2	46	0	3.9983	3.9983	3.9983	3.9984	3.9984	3.9985	3.9985	3.9986	3.9986	3.9987
	46	10	3.9987	3.9987	3.9988	3.9988	3.9989	3.9989	3.9990	3.9990	3.9990	3.9991
	46	20	3.9991	3.9992	3.9992	3.9993	3.9993	3.9993	3.9994	3.9994	3.9995	3.9995
	46	30	3.9996	3.9996	3.9997	3.9997	3.9997	3.9998	3.9998	3.9999	3.9999	4.0000
	46	40	4.0000	4.0000	4.0001	4.0001	4.0002	4.0002	4.0003	4.0003	4.0003	4.0004
	46	50	4.0004	4.0005	4.0005	4.0006	4.0006	4.0007	4.0007	4.0007	4.0008	4.0008
2	47	0	4.0009	4.0009	4.0010	4.0010	4.0010	4.0011	4.0011	4.0012	4.0012	4.0013
	47	10	4.0013	4.0013	4.0014	4.0014	4.0015	4.0015	4.0016	4.0016	4.0016	4.0017
	47	20	4.0017	4.0018	4.0018	4.0019	4.0019	4.0019	4.0020	4.0020	4.0021	4.0021
	47	30	4.0022	4.0022	4.0023	4.0023	4.0023	4.0024	4.0024	4.0025	4.0025	4.0026
	47	40	4.0026	4.0026	4.0027	4.0027	4.0028	4.0028	4.0029	4.0029	4.0029	4.0030
	47	50	4.0030	4.0031	4.0031	4.0032	4.0032	4.0032	4.0033	4.0033	4.0034	4.0034
2	48	0	4.0035	4.0035	4.0035	4.0036	4.0036	4.0037	4.0037	4.0038	4.0038	4.0038
	48	10	4.0039	4.0039	4.0040	4.0040	4.0041	4.0041	4.0041	4.0042	4.0042	4.0043
	48	20	4.0043	4.0044	4.0044	4.0045	4.0045	4.0045	4.0046	4.0046	4.0047	4.0047
	48	30	4.0048	4.0048	4.0048	4.0049	4.0049	4.0050	4.0050	4.0051	4.0051	4.0051
	48	40	4.0052	4.0052	4.0053	4.0053	4.0054	4.0054	4.0054	4.0055	4.0055	4.0056
	48	50	4.0056	4.0057	4.0057	4.0057	4.0058	4.0058	4.0059	4.0059	4.0060	4.0060
2	49	0	4.0060	4.0061	4.0061	4.0062	4.0062	4.0063	4.0063	4.0063	4.0064	4.0064
	49	10	4.0065	4.0065	4.0066	4.0066	4.0066	4.0067	4.0067	4.0068	4.0068	4.0069
	49	20	4.0069	4.0069	4.0070	4.0070	4.0071	4.0071	4.0072	4.0072	4.0072	4.0073
	49	30	4.0073	4.0074	4.0074	4.0074	4.0075	4.0075	4.0076	4.0076	4.0077	4.0077
	49	40	4.0077	4.0078	4.0078	4.0079	4.0079	4.0080	4.0080	4.0080	4.0081	4.0081
	49	50	4.0082	4.0082	4.0083	4.0083	4.0083	4.0084	4.0084	4.0085	4.0085	4.0086

APPENDIX V: TABLE IX.

Logarithms of Small Arcs in Space or Time.

Arc.	0″	1″	2″	3″	4″	5″	6″	7″	8″	9″
° ′ ″										
2h 50m 0s	4.0086	4.0086	4.0087	4.0087	4.0088	4.0088	4.0089	4.0089	4.0089	4.0090
50 10	4.0090	4.0091	4.0091	4.0092	4.0092	4.0092	4.0093	4.0093	4.0094	4.0094
50 20	4.0095	4.0095	4.0095	4.0096	4.0096	4.0097	4.0097	4.0097	4.0098	4.0098
50 30	4.0099	4.0099	4.0100	4.0100	4.0100	4.0101	4.0101	4.0102	4.0102	4.0103
50 40	4.0103	4.0103	4.0104	4.0104	4.0105	4.0105	4.0106	4.0106	4.0106	4.0107
50 50	4.0107	4.0108	4.0108	4.0109	4.0109	4.0109	4.0110	4.0110	4.0111	4.0111
2 51 0	4.0111	4.0112	4.0112	4.0113	4.0113	4.0114	4.0114	4.0114	4.0115	4.0115
51 10	4.0116	4.0116	4.0117	4.0117	4.0117	4.0118	4.0118	4.0119	4.0119	4.0120
51 20	4.0120	4.0120	4.0121	4.0121	4.0122	4.0122	4.0122	4.0123	4.0123	4.0124
51 30	4.0124	4.0125	4.0125	4.0125	4.0126	4.0126	4.0127	4.0127	4.0128	4.0128
51 40	4.0128	4.0129	4.0129	4.0130	4.0130	4.0130	4.0131	4.0131	4.0132	4.0132
51 50	4.0133	4.0133	4.0133	4.0134	4.0134	4.0135	4.0135	4.0136	4.0136	4.0136
2 52 0	4.0137	4.0137	4.0138	4.0138	4.0138	4.0139	4.0139	4.0140	4.0140	4.0141
52 10	4.0141	4.0141	4.0142	4.0142	4.0143	4.0143	4.0144	4.0144	4.0144	4.0145
52 20	4.0145	4.0146	4.0146	4.0146	4.0147	4.0147	4.0148	4.0148	4.0149	4.0149
52 30	4.0149	4.0150	4.0150	4.0151	4.0151	4.0152	4.0152	4.0153	4.0153	4.0153
52 40	4.0154	4.0154	4.0154	4.0155	4.0155	4.0156	4.0156	4.0157	4.0157	4.0157
52 50	4.0158	4.0158	4.0159	4.0159	4.0159	4.0160	4.0160	4.0161	4.0161	4.0162
2 53 0	4.0162	4.0162	4.0163	4.0163	4.0164	4.0164	4.0164	4.0165	4.0165	4.0166
53 10	4.0166	4.0167	4.0167	4.0167	4.0168	4.0168	4.0169	4.0169	4.0169	4.0170
53 20	4.0170	4.0171	4.0171	4.0172	4.0172	4.0172	4.0173	4.0173	4.0174	4.0174
53 30	4.0175	4.0175	4.0175	4.0176	4.0176	4.0177	4.0177	4.0177	4.0178	4.0178
53 40	4.0179	4.0179	4.0180	4.0180	4.0180	4.0181	4.0181	4.0182	4.0182	4.0182
53 50	4.0183	4.0183	4.0184	4.0184	4.0185	4.0185	4.0185	4.0186	4.0186	4.0187
2 54 0	4.0187	4.0187	4.0188	4.0188	4.0189	4.0189	4.0190	4.0190	4.0190	4.0191
54 10	4.0191	4.0192	4.0192	4.0192	4.0193	4.0193	4.0194	4.0194	4.0194	4.0195
54 20	4.0195	4.0196	4.0196	4.0197	4.0197	4.0197	4.0198	4.0198	4.0199	4.0199
54 30	4.0199	4.0200	4.0200	4.0201	4.0201	4.0202	4.0202	4.0202	4.0203	4.0203
54 40	4.0204	4.0204	4.0204	4.0205	4.0205	4.0206	4.0206	4.0207	4.0207	4.0207
54 50	4.0208	4.0208	4.0209	4.0209	4.0209	4.0210	4.0210	4.0211	4.0211	4.0211
2 55 0	4.0212	4.0212	4.0213	4.0213	4.0214	4.0214	4.0214	4.0215	4.0215	4.0216
55 10	4.0216	4.0216	4.0217	4.0217	4.0218	4.0218	4.0219	4.0219	4.0219	4.0220
55 20	4.0220	4.0221	4.0221	4.0221	4.0222	4.0222	4.0223	4.0223	4.0223	4.0224
55 30	4.0224	4.0225	4.0225	4.0225	4.0226	4.0226	4.0227	4.0227	4.0228	4.0228
55 40	4.0228	4.0229	4.0229	4.0230	4.0230	4.0230	4.0231	4.0231	4.0232	4.0232
55 50	4.0233	4.0233	4.0233	4.0234	4.0234	4.0235	4.0235	4.0235	4.0236	4.0236
2 56 0	4.0237	4.0237	4.0237	4.0238	4.0238	4.0239	4.0239	4.0240	4.0240	4.0240
56 10	4.0241	4.0241	4.0242	4.0242	4.0242	4.0243	4.0243	4.0244	4.0244	4.0244
56 20	4.0245	4.0245	4.0246	4.0246	4.0246	4.0247	4.0247	4.0248	4.0248	4.0249
56 30	4.0249	4.0249	4.0250	4.0250	4.0251	4.0251	4.0251	4.0252	4.0252	4.0253
56 40	4.0253	4.0253	4.0254	4.0254	4.0255	4.0255	4.0256	4.0256	4.0256	4.0257
56 50	4.0257	4.0258	4.0258	4.0258	4.0259	4.0259	4.0260	4.0260	4.0260	4.0261
2 57 0	4.0261	4.0262	4.0262	4.0262	4.0263	4.0263	4.0264	4.0264	4.0265	4.0265
57 10	4.0265	4.0266	4.0266	4.0267	4.0267	4.0267	4.0268	4.0268	4.0269	4.0269
57 20	4.0269	4.0270	4.0270	4.0271	4.0271	4.0271	4.0272	4.0272	4.0273	4.0273
57 30	4.0273	4.0274	4.0274	4.0275	4.0275	4.0276	4.0276	4.0276	4.0277	4.0277
57 40	4.0278	4.0278	4.0278	4.0279	4.0279	4.0280	4.0280	4.0280	4.0281	4.0281
57 50	4.0282	4.0282	4.0282	4.0283	4.0283	4.0284	4.0284	4.0284	4.0285	4.0285
2 58 0	4.0286	4.0286	4.0287	4.0287	4.0287	4.0288	4.0288	4.0289	4.0289	4.0289
58 10	4.0290	4.0290	4.0291	4.0291	4.0291	4.0292	4.0292	4.0293	4.0293	4.0293
58 20	4.0294	4.0294	4.0295	4.0295	4.0295	4.0296	4.0296	4.0297	4.0297	4.0297
58 30	4.0298	4.0298	4.0299	4.0299	4.0300	4.0300	4.0300	4.0301	4.0301	4.0302
58 40	4.0302	4.0302	4.0303	4.0303	4.0304	4.0304	4.0304	4.0305	4.0305	4.0306
58 50	4.0306	4.0306	4.0307	4.0307	4.0308	4.0308	4.0308	4.0309	4.0309	4.0310
2 59 0	4.0310	4.0310	4.0311	4.0311	4.0312	4.0312	4.0312	4.0313	4.0313	4.0314
59 10	4.0314	4.0314	4.0315	4.0315	4.0316	4.0316	4.0317	4.0317	4.0317	4.0318
59 20	4.0318	4.0319	4.0319	4.0319	4.0320	4.0320	4.0321	4.0321	4.0321	4.0322
59 30	4.0322	4.0323	4.0323	4.0323	4.0324	4.0324	4.0325	4.0325	4.0325	4.0326
59 40	4.0326	4.0327	4.0327	4.0327	4.0328	4.0328	4.0329	4.0329	4.0329	4.0330
59 50	4.0330	4.0331	4.0331	4.0331	4.0332	4.0332	4.0333	4.0333	4.0333	4.0334

APPENDIX V: TABLE X.

Table showing the correction required, on account of Second Differences of the Moon's Motion, in Finding the Greenwich Time corresponding to a Corrected Lunar Distance.

Approximate interval.		Difference of the proportional logarithms in the Ephemeris.																	
		2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
h. m.	*h. m.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*
0 0	3 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0 10	2 50	0	0	0	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2
0 20	2 40	0	1	1	1	1	2	2	2	2	2	3	3	3	3	4	4	4	4
0 30	2 30	0	1	1	2	2	2	2	3	3	3	4	4	5	5	5	6	6	6
0 40	2 20	0	1	1	2	2	3	3	3	4	4	5	5	6	6	6	7	7	8
0 50	2 10	1	1	2	2	3	3	4	4	5	5	5	6	6	7	7	8	8	9
1 0	2 0	1	1	2	2	3	3	4	4	5	6	6	7	7	8	8	9	9	10
1 10	1 50	1	1	2	2	3	4	4	5	5	6	6	7	8	8	9	9	10	11
1 20	1 40	1	1	2	3	3	4	4	5	6	6	7	7	8	9	9	10	10	11
1 30	1 30	1	1	2	3	3	4	4	5	6	6	7	8	8	9	9	10	11	11

		Difference of the proportional logarithms in the Ephemeris.																
		38	40	42	44	46	48	50	52	54	56	58	60	62	64	66	68	70
h. m.	*h. m.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*
0 0	3 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0 10	2 50	2	3	3	3	3	3	3	3	4	4	4	4	4	4	4	4	5
0 20	2 40	5	5	5	5	6	6	6	6	7	7	7	7	8	8	8	8	9
0 30	2 30	7	7	7	8	8	8	9	9	9	10	10	10	11	11	12	12	12
0 40	2 20	8	9	9	10	10	10	11	11	12	12	13	13	13	14	14	15	15
0 50	2 10	9	10	10	11	12	12	13	13	14	14	15	15	16	16	16	17	17
1 0	2 0	10	11	12	12	13	13	14	14	15	16	16	17	17	18	18	19	19
1 10	1 50	11	12	12	13	14	14	15	15	16	17	17	18	18	19	19	20	21
1 20	1 40	12	12	13	14	14	15	15	16	17	17	18	19	19	20	20	21	21
1 30	1 30	12	12	13	14	14	15	16	16	17	18	18	19	19	20	21	21	22

		Difference of the proportional logarithms in the Ephemeris.																
		72	74	76	78	80	82	84	86	88	90	92	94	96	98	100	102	104
h. m.	*h. m.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*
0 0	3 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0 10	2 50	5	5	5	5	5	5	6	6	6	6	6	6	6	6	7	7	7
0 20	2 40	9	9	9	10	10	10	10	11	11	11	11	12	12	12	12	13	13
0 30	2 30	13	13	13	14	14	14	14	15	15	16	16	16	17	17	17	18	18
0 40	2 20	16	16	16	17	17	18	18	19	19	19	20	20	21	21	22	22	22
0 50	2 10	18	19	19	20	20	21	21	22	22	22	23	23	24	24	25	26	26
1 0	2 0	20	21	21	22	22	23	23	24	24	25	25	26	27	27	38	28	29
1 10	1 50	21	22	22	23	24	24	25	25	26	27	27	28	28	29	30	30	31
1 20	1 40	22	23	23	24	25	25	26	26	27	28	28	29	29	30	31	31	32
1 30	1 30	23	23	24	24	25	25	26	27	27	28	29	29	30	31	31	32	32

		Difference of the proportional logarithms in the Ephemeris.																
		106	108	110	112	114	116	118	120	122	124	126	128	130	132	134	136	138
h. m.	*h. m.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*	*s.*
0 0	3 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0 10	2 50	7	7	7	7	7	8	8	8	8	8	8	8	8	9	9	9	9
0 20	2 40	13	13	14	14	14	14	15	15	15	15	15	16	16	16	16	17	17
0 30	2 30	18	19	19	19	20	20	20	21	21	21	22	22	22	23	23	24	24
0 40	2 20	23	23	24	24	25	25	25	26	26	27	27	28	28	28	29	29	30
0 50	2 10	26	27	27	28	29	29	29	30	30	31	31	32	32	33	33	34	34
1 0	2 0	29	30	30	31	31	32	33	33	34	34	35	35	36	37	37	38	38
1 10	1 50	31	32	32	33	34	34	35	35	36	37	37	38	38	39	40	40	41
1 20	1 40	33	33	34	34	35	35	36	37	38	38	39	39	40	41	41	42	42
1 30	1 30	33	34	34	35	35	36	36	37	38	39	39	40	40	41	42	42	43

The correction is to be *added* to the approximate Greenwich time when the proportional logarithms in the Ephemeris are *decreasing*, and *subtracted* when they are *increasing*.

APPENDIX V: TABLE XI.

For finding the value of N for Correcting Lunar Distances for the Compression of the Earth.

Table XI A, giving 1st part of N.

App. dist.	Moon's declination. 0°	3°	6°	9°	12°	15°	18°	21°	24°	27°	30°
°	″	″	″	″	″	″	″	″	″	″	″
20	−0	3	6	10	13	16	19	22	25	28	31
22	0	3	6	9	12	14	17	20	23	25	28
24	0	3	5	8	11	13	16	18	21	23	25
26	0	2	5	7	10	12	14	17	19	21	23
28	0	2	4	7	9	11	13	15	17	19	21
30	−0	2	4	6	8	10	12	14	16	18	20
32	0	2	4	6	8	9	11	13	15	16	18
34	0	2	4	5	7	9	10	12	14	15	17
36	0	2	3	5	7	8	10	11	13	14	16
38	0	2	3	5	6	8	9	10	12	13	14
40	−0	1	3	4	6	7	8	10	11	12	13
42	0	1	3	4	5	7	8	9	10	11	13
44	0	1	2	4	5	6	7	8	10	11	12
46	0	1	2	3	5	6	7	8	9	10	11
48	0	1	2	3	4	5	6	7	8	9	10
50	−0	1	2	3	4	5	6	7	8	9	10
52	0	1	2	3	4	5	5	6	7	8	9
54	0	1	2	3	3	4	5	6	7	7	8
56	0	1	2	2	3	4	5	5	6	7	8
58	0	1	1	2	3	4	4	5	6	6	7
60	−0	1	1	2	3	3	4	5	5	6	7
62	0	1	1	2	3	3	4	4	5	5	6
64	0	1	1	2	2	3	3	4	4	5	6
66	0	1	1	2	2	3	3	4	4	5	5
68	0	0	1	1	2	2	3	3	4	4	5
70	−0	0	1	1	2	2	3	3	3	4	4
72	0	0	1	1	2	2	2	3	3	3	4
74	0	0	1	1	1	2	2	2	3	3	3
76	0	0	1	1	1	1	2	2	2	3	3
78	0	0	0	1	1	1	1	2	2	2	2
80	−0	0	0	1	1	1	1	1	2	2	2
82	0	0	0	0	1	1	1	1	1	1	2
84	0	0	0	0	0	1	1	1	1	1	1
86	0	0	0	0	0	0	0	1	1	1	1
88	0	0	0	0	0	0	0	0	0	0	0
90	−0	0	0	0	0	0	0	0	0	0	0
92	+0	0	0	0	0	0	0	0	0	0	0
94	0	0	0	0	0	0	0	1	1	1	1
96	0	0	0	0	0	1	1	1	1	1	1
98	0	0	0	0	1	1	1	1	1	1	2
100	+0	0	0	1	1	1	1	1	2	2	2
102	0	0	0	1	1	1	1	2	2	2	2
104	0	0	1	1	1	1	2	2	2	3	3
106	0	0	1	1	1	2	2	2	3	3	3
108	0	0	1	1	2	2	2	3	3	3	4
110	+0	0	1	1	2	2	3	3	3	4	4
112	0	0	1	1	2	2	3	3	4	4	5
114	0	1	1	2	2	3	3	4	4	5	5
116	0	1	1	2	2	3	3	4	4	5	6
118	0	1	1	2	3	3	4	4	5	5	6
120	+0	1	1	2	3	3	4	5	5	6	7
122	0	1	1	2	3	4	4	5	6	6	7
124	0	1	2	2	3	4	5	5	6	7	8
126	0	1	2	3	3	4	5	6	7	7	8
128	0	1	2	3	4	5	5	6	7	8	9
130	+0	1	2	3	4	5	6	7	8	9	10

Table XI B, giving 2d part of N.

App. dist.	Other body's declination. 0°	3°	6°	9°	12°	15°	18°	21°	24°	27°	30°
°	″	″	″	″	″	″	″	″	″	″	″
20	+0	3	7	10	14	17	20	24	27	30	33
22	0	3	6	9	13	16	19	22	25	27	30
24	0	3	6	9	12	14	17	20	23	25	28
26	0	3	5	8	11	13	16	18	21	23	26
28	0	3	5	8	10	12	15	17	20	22	24
30	+0	2	5	7	9	12	14	16	18	21	23
32	0	2	4	7	9	11	13	15	17	19	21
34	0	2	4	6	8	11	13	15	16	18	20
36	0	2	4	6	8	10	12	14	16	17	19
38	0	2	4	6	8	10	11	13	15	17	18
40	+0	2	4	6	7	9	11	13	14	16	18
42	0	2	4	5	7	9	10	12	14	15	17
44	0	2	3	5	7	8	10	12	13	15	16
46	0	2	3	5	6	8	10	11	13	14	16
48	0	2	3	5	6	8	9	11	12	14	15
50	+0	2	3	5	6	8	9	11	12	13	15
52	0	2	3	4	6	7	9	10	12	13	14
54	0	1	3	4	6	7	9	10	11	13	14
56	0	1	3	4	6	7	8	10	11	12	14
58	0	1	3	4	6	7	8	10	11	12	13
60	+0	1	3	4	5	7	8	9	11	12	13
62	0	1	3	4	5	7	8	9	10	12	13
64	0	1	3	4	5	7	8	9	10	11	13
66	0	1	3	4	5	6	8	9	10	11	12
68	0	1	3	4	5	6	8	9	10	11	12
70	+0	1	3	4	5	6	7	9	10	11	12
72	0	1	2	4	5	6	7	9	10	11	12
74	0	1	2	4	5	6	7	8	10	11	12
76	0	1	2	4	5	6	7	8	9	11	12
78	0	1	2	4	5	6	7	8	9	11	12
80	+0	1	2	4	5	6	7	8	9	10	11
82	0	1	2	4	5	6	7	8	9	10	11
84	0	1	2	4	5	6	7	8	9	10	11
86	0	1	2	4	5	6	7	8	9	10	11
88	0	1	2	4	5	6	7	8	9	10	11
90	+0	1	2	4	5	6	7	8	9	10	11
92	0	1	2	4	5	6	7	8	9	10	11
94	0	1	2	4	5	6	7	8	9	10	11
96	0	1	2	4	5	6	7	8	9	10	11
98	0	1	2	4	5	6	7	8	9	10	11
100	+0	1	2	4	5	6	7	8	9	10	11
102	0	1	2	4	5	6	7	8	9	11	12
104	0	1	2	4	5	6	7	8	9	11	12
106	0	1	2	4	5	6	7	8	10	11	12
108	0	1	2	4	5	6	7	9	10	11	12
110	+0	1	3	4	5	6	7	9	10	11	12
112	0	1	3	4	5	6	8	9	10	11	12
114	0	1	3	4	5	6	8	9	10	11	12
116	0	1	3	4	5	7	8	9	10	11	13
118	0	1	3	4	5	7	8	9	10	12	13
120	+0	1	3	4	5	7	8	9	11	12	13
122	0	1	3	4	6	7	8	10	11	12	13
124	0	1	3	4	6	7	8	10	11	12	14
126	0	1	3	4	6	7	9	10	11	13	14
128	0	2	3	4	6	7	9	10	12	13	14
130	+0	2	3	5	6	8	9	11	12	13	15

The signs in the 0° column apply to all the numbers in the same line, and are to be used when the declination is *North*. When the declination is *South* change the sign + to − and − to +.

INDEX TO PART I.

PART II.

TABLES.

CONTENTS OF PART II.

EXPLANATION OF THE TABLES.

TABLES 1, 2: TRAVERSE TABLES.

Tables 1 and 2 were originally calculated by the natural sines taken from the fourth edition of Sherwin's Logarithms, which were previously examined, by differences; when the proof sheets of the first edition were examined the numbers were again calculated by the natural sines in the second edition of Hutton's Logarithms; and if any difference was found, the numbers were calculated a third time by Taylor's Logarithms.

The first table contains the difference of latitude and departure corresponding to distances not exceeding 300 miles, and for courses to every quarter point of the compass. Table 2 is of the same nature, but for courses consisting of whole degrees; it was originally of the same extent as Table 1, but has been extended to include distances up to 600 miles. The manner of using these tables is particularly explained under the different problems of Plane, Middle Latitude, and Mercator Sailing in Chapter V.

The tables may be employed in the solution of any right triangle.

TABLE 3: MERIDIONAL PARTS.

This table contains the meridional parts, or increased latitudes, for every degree and minute to 80°, calculated by the following formula:

$$m = \frac{a}{M} \log \tan \left(45° + \frac{L}{2}\right) - a \left(e^2 \sin L + \tfrac{1}{3} e^4 \sin^3 L + \tfrac{1}{5} e^6 \sin^5 L + \;.\;.\;.\;.\;\right),$$

in which

the Equatorial radius $a = \frac{10800'}{\pi} = 3437'.74677$ (log 3.5362739);

M, the modulus of common logarithms $= 0.4342945$;

$\frac{1}{M} = 2.3025851$ (log 0.3622157);

C, the *compression* or meridional eccentricity of the earth

according to Clarke (1880) $= \frac{1}{293.465} = 0.003407562$ (log 7.5324437);

$e = \sqrt{2c - c^2} = 0.0824846$ (log 8.9163666);

from which

$\frac{a}{M} = 7915'.7044558$ (log 3.8984895);

$ae^2 = 23'.38871$ (log 1.3690072);

$\frac{1}{3}ae^4 = 0'.053042$ (log 8.7246192);

$\frac{1}{5}ae^6 = 0'.000216523$ (log 6.3355038).

The results are tabulated to one decimal place, which is sufficient for the ordinary problems of navigation.

The practical application of this table is illustrated in Chapters II and V, in articles treating of the Mercator Chart and Mercator Sailing.

TABLE 4: LENGTH OF DEGREES OF LATITUDE AND LONGITUDE.

This table gives the length of a degree in both latitude and longitude at each parallel of latitude on the earth's surface, in nautical and statute miles and in meters, based upon Clarke's value (1866) of the earth's compression, $\frac{1}{299.15}$. In the case of latitude, the length relates to an arc of which the given degree is the center.

TABLES 5A, 5B: DISTANCE BY TWO BEARINGS.

These tables have been calculated to facilitate the operation of finding the distance from an object by two bearings from a given distance run and course. In Table 5A the arguments are given in points, in Table 5B in degrees; the first column contains the multiplier of the distance run to give the distance of observed object at second bearing; the second, at time of passing abeam.

The method is explained in article 143, Chapter IV.

TABLE 6: DISTANCE OF VISIBILITY OF OBJECTS.

This table contains the distances, in nautical and statute miles, at which any object is visible at sea. It is calculated by the formulæ:

$$d = 1.15\sqrt{x}, \text{ and } d' = 1.32\sqrt{x},$$

in which d is the distance in nautical miles, d' the distance in statute miles, and x the height of the eye or the object in feet.

To find the distance of visibility of an object, the distance given by the table corresponding to its height should be added to that corresponding to the height of the observer's eye.

Example: Required the distance of visibility of an object 420 feet high, the observer being at an elevation of 15 feet.

Dist. corresponding to 420 feet,	23.5 naut. miles.
Dist. corresponding to 15 feet,	4.4 naut. miles.
Dist. of visibility,	27.9 naut. miles.

TABLE 7: CONVERSION OF ARC AND TIME.

In the first column of each pair in this table are contained angular measures expressed in arc (degrees, minutes, or seconds), and in the second column the corresponding angles expressed in time (hours, minutes, or seconds). As will be seen from the headings of columns, the time corresponding to degrees (°) is given in hours and minutes; to minutes of arc (′), in minutes and seconds of time; and to seconds of arc (″), in seconds and sixtieths of a second of time.

The table will be especially convenient in dealing with longitude and hour angle. The method of its employment is best illustrated by examples.

Example I.

Required the time corresponding to 50° 31′ 21″.

$$\begin{array}{rrrcrrr} 50^\circ & 00' & 00'' & = & 3^h & 20^m & 00^s \\ & 31 & 00 & = & & 2 & 04 \\ & & 21 & = & & & 1\tfrac{24}{60} \\ \hline 50 & 31 & 21 & = & 3 & 22 & 05.4 \end{array}$$

Example II.

Required the arc corresponding to $6^h\ 33^m\ 26^s.5$.

$$\begin{array}{rrrcrrr} 6^h & 32^m & 00^s & = & 98^\circ & 00' & 00'' \\ & 1 & 24 & = & & 21 & 00 \\ & & 2\tfrac{30}{60} & = & & & 37.5 \\ \hline 6 & 33 & 26.5 & = & 98 & 21 & 37.5 \end{array}$$

TABLES 8 AND 9: SIDEREAL AND MEAN SOLAR TIMES.

These tables give, respectively, the reductions necessary to convert intervals of sidereal time into those of mean solar time, and intervals of mean solar into those of sidereal time. The reduction for any interval is found by entering with the number of hours at the top and the number of minutes at the side, adding the reduction for seconds as given in the margin.

The relations between mean solar and sidereal time intervals, and the methods of conversion of these times, are given in articles 289–291, Chapter IX.

TABLE 10: SUN'S RISING AND SETTING.

This table gives the local mean time of the sun's visible rising and setting—that is, of the appearance and disappearance of the sun's upper limb in the unobstructed horizon of a person whose eye is 15 feet above the level of the earth's surface, the atmospheric conditions being normal.

The local apparent times of rising and setting were determined from the formula for a time sight, the altitude employed being −0° 56′ 08″, made up of the following terms: Refraction, − 36′ 29″; semidiameter, − 16′ 00″; dip, − 3′ 48″; and parallax, + 9″.

To ascertain the time of rising or setting for any given date and place, enter the table with the latitude and declination, interpolating if the degrees are not even. In the line R will be found the time of rising; in the line S, the time of setting. Be careful to choose the page in which the latitude is of the correct name, and in which the "approximate date" corresponds, nearly or exactly, with the given date.

This table is computed with the intention that, if accuracy is desired, it will be entered with the declination as an argument—not the date—as it is impossible to construct any table based upon dates whose application shall be general to all years. But as a given degree of declination will, in the majority of years, fall upon the date given in the table as the "approximate date," and as, when it does not do so, it can never be more than one day removed therefrom, it will answer, where a slight inaccuracy may be admitted, to enter the table with the date as an argument, thus avoiding the necessity of ascertaining the declination.

Example: Find the local mean time of sunset at Rio de Janeiro, Brazil (lat. 22° 54′ S., long. 43° 10′ W.), on January 1, 1903 (dec. 23° 04′ S.).

Exact method.

Lat. 22°, Dec. 23°	$6^h\ 48^m$
Corr. for + 54′ lat	+ 02
Corr. for + 04′ dec	00
L. M. T. sunset	6 50

Approximate method.

Lat. 22°, January 2	$6^h\ 48^m$
Corr. for + 54′ lat	+ 02
Corr. for 1 day	− 01
L. M. T. sunset	6 49

TABLE 11: REDUCTION FOR MOON'S TRANSIT.

This table was calculated by proportioning the daily variation of the time of the moon's passing the meridian.

The numbers taken from the table are to be added to the Greenwich time of moon's transit in west longitude, but subtracted in east longitude.

TABLE 12: REDUCTIONS FOR NAUTICAL ALMANAC.

This is a table of proportional parts for finding the variation of the sun's right ascension or declination, or of the equation of time, in any number of minutes of time, the horary motion being given at the top of the page in seconds, and the number of minutes of time in the side column; also for finding the variation of the moon's declination or right ascension in any number of seconds of time, the motion in one minute being given at the top, and the numbers in the side column being taken for seconds.

TABLE 13: CHANGE OF SUN'S RIGHT ASCENSION.

This is a table that may be employed for finding the change of the sun's right ascension for any given number of hours, the hourly change, as taken from the Nautical Almanac, being given in the marginal columns.

TABLE 14: DIP OF SEA HORIZON.

This table contains the dip of the sea horizon, calculated by the formula:

$$D = 58''.8 \sqrt{F},$$

in which F = height of the eye above the level of the sea in feet.

It is explained in article 300, Chapter X.

TABLE 15: DIP SHORT OF HORIZON.

This table contains the dip for various distances and heights, calculated by the formula:

$$D = \frac{3}{7} d + 0.56514 \times \frac{h}{d},$$

in which D represents the dip in miles or minutes, d, the distance of the land in sea miles, and h, the height of the eye of the observer in feet.

TABLE 16: PARALLAX OF SUN.

This table contains the sun's parallax in altitude calculated by the formula:

$$\text{par.} = \sin z \times 8''.75,$$

in which z = apparent zenith distance, the sun's horizontal parallax being $8''.75$.

It is explained in article 304, Chapter X.

TABLE 17: PARALLAX OF PLANET.

Parallax in altitude of a planet is found by entering at the top with the planet's horizontal parallax, and at the side with the altitude.

TABLE 18: AUGMENTATION OF MOON'S SEMIDIAMETER.

This table gives the augmentation of the moon's semidiameter calculated by the formula:

$$x = c\, s^2 \sin h + \tfrac{1}{2} c^2 s^3 \sin^2 h + \tfrac{1}{2} c^2 s^3,$$

where h = moon's apparent altitude;
s = moon's horizontal semidiameter;
x = augmentation of semidiameter for altitude h; and
$\log c = 5.25021$.

TABLE 19: AUGMENTATION OF MOON'S HORIZONTAL PARALLAX.

This table contains the augmentation of the moon's horizontal parallax, or the correction to reduce the moon's equatorial horizontal parallax to that point of the earth's axis which lies in the vertical of the observer in any given latitude; it is computed by the formulæ:

$$\triangle \pi = \pi (b - 1), \qquad b = \frac{1}{\sqrt{(1 - e^2 \sin^2 L)}},$$

where π = equatorial horizontal parallax;
L = latitude;
e = eccentricity of the meridian; $\log e^2 = 7.81602$; and
$\triangle \pi$ = augmentation of the horizontal parallax for the latitude L.

TABLE 20A: MEAN REFRACTION.

This table gives the refraction, reduced from Bessel's tables, for a mean atmospheric condition in which the barometer is 30.00 inches, and thermometer 50° Fahr.

TABLE 20B: MEAN REFRACTION AND PARALLAX OF SUN.

This table contains the correction to be applied to the sun's apparent altitude for mean refraction and parallax, being a combination of the quantities for the altitudes given in Tables 16 and 20A.

TABLES 21, 22: CORRECTIONS OF REFRACTION FOR BAROMETER AND THERMOMETER.

These are deduced from Bessel's tables. The method of their employment will be evident.

TABLE 23: MEAN REFRACTION AND MEAN PARALLAX OF MOON.

This table contains the correction of the moon's altitude for refraction and parallax corresponding to the mean refraction (Table 20A), and a horizontal parallax of the mean value of 57′ 30″.

TABLE 24: MEAN REFRACTION AND PARALLAX OF MOON.

This table contains the correction to be applied to the moon's apparent altitude for each minute of horizontal parallax, and for every 10′ of altitude from 5°, with height of barometer 30.00 inches, and thermometer 50° Fahr.

For seconds of parallax, enter the table abreast the approximate correction and find the seconds of horizontal parallax, the tens of seconds at the side and the units at the top. Under the latter and opposite the former will be the seconds to add to the correction.

For minutes of altitude, take the seconds from the extreme right of the page, and apply them as there directed.

TABLE 25: CHANGE OF ALTITUDE DUE TO CHANGE OF DECLINATION.

This table gives the variation of the altitude of any heavenly body arising from a change of 100″ in the declination. It is useful for finding the equation of equal altitudes by the approximate method explained in article 324, Chapter XI, and for other purposes.

If the change move the body toward the elevated pole, apply the correction to the altitude with the signs in the table; otherwise change the signs.

TABLE 26: CHANGE OF ALTITUDE IN ONE MINUTE FROM MERIDIAN.

This table gives the variation of the altitude of any heavenly body, for one minute of time from meridian passage, for latitudes up to 60°, declinations to 63°, and altitudes between 6° and 86°. It is based upon the method set forth in article 334, Chapter XII, and the values may be computed by the formula:

$$a=\frac{1''.9635 \cos \mathrm{L} \cos d}{\sin (\mathrm{L}-d)}.$$

where a = variation of altitude in one minute from meridian,

L = latitude, and

d = declination—positive for same name and negative for opposite name to latitude at upper transit, and negative for same name at lower transit.

The limits of the table take in all values of latitude, declination, and altitude which are likely to be required. In its employment, care must be taken to enter the table at a place where the declination is appropriately named (of the same or opposite name to the latitude); it should also be noted that at the bottom of the last three pages values are given for the variation of a body at *lower* transit, which can only be observed when the declination and latitude are of the same name, and in which case the reduction to the meridian is subtractive; the limitations in this case are stated at the *foot* of the page, and apply to all values below the heavy rules.

TABLE 27: CHANGE OF ALTITUDE IN GIVEN TIME FROM MERIDIAN.

This table gives the product of the variation in altitude in one minute of a heavenly body near the meridian, by the square of the number of minutes. Values are given for every half minute between $0^m\ 30^s$ and $26^m\ 0^s$, and for all variations likely to be employed in the method of "reduction to the meridian."

The formula for computing is:

$$\text{Red.} = a \times t^2,$$

where a = variation in one minute (Table 26), and

t = number of minutes (in units and tenths) from time of meridian passage.

The table is entered in the column of the nearest interval of time from meridian, and the value taken out corrresponding to the value of a found from Table 26. The units and tenths are picked out separately and combined, each being corrected by interpolation for intermediate intervals of time.

The result is the amount to be applied to the observed altitude to reduce it to the meridian altitude, which is always to be added for upper transits and subtracted for lower.

TABLE 28, A, B, C, D: LATITUDE BY POLARIS.

The formula on which these tables are based is:

$$L = h - p\cos t + \tfrac{1}{2}p^2 \sin 1'' \sin^2 t \tan h$$
$$- \tfrac{1}{3}p^3 \sin^2 1'' \cos t \sin^2 t + \tfrac{1}{8}p^4 \sin^3 1'' \sin^4 t \tan^3 h;$$

in which

L = the latitude of the place;
h = the true altitude;
p = the polar distance; and
t = the hour angle of the star.

Table A contains for the declination 88° 48′, or $p_0 = 1° 12' = 4320''$, the *first correction*,

$$A = -p_0 \cos t - \tfrac{1}{3}p^3_0 \sin^2 1'' \cos t \sin^2 t;$$

Argument, *the hour angle of the star*, or 24^h — the hour angle.

Table B contains the *second correction*,

$$B = \tfrac{1}{2}p^2_0 \sin 1'' \sin^2 t \tan h + \tfrac{1}{8}p^4_0 \sin^3 1'' \sin^4 t \tan^3 h;$$

Arguments, *the true altitude of the star* and the *hour angle*, or 24^h — *the hour angle*. This correction is always *additive*.

Table C contains the *third correction*,

$$C = \tfrac{1}{2}(p^2 - p^2_0) \sin 1'' \sin^2 t \tan h;$$

Arguments, *B* and *the declination of the star* from 88° 47′ 20″ to 88° 49′ 20″.

Table D contains the *fourth correction*,

$$-(p - p_0)\cos t - \tfrac{1}{3}(p^3 - p^3_0) \sin^2 1'' \cos t \sin^2 t;$$

Arguments, *A and the declination of the star* from 88° 47′ 20″ to 88° 49′ 20″.

The method of employing this table is illustrated in article 341, Chapter XII.

TABLES 29, 30, 31: CONVERSION TABLES.

These are self-explanatory.

TABLE 32: TRUE FORCE AND DIRECTION OF WIND.

This table enables an observer on board of a moving vessel to determine the true force and direction of the wind from its apparent force and direction. Enter the table with the apparent direction of the wind (number of points on the bow) and force (Beaufort scale) as arguments, and pick out the direction relatively to the ship's head and the force corresponding to the known speed of the ship.

EXAMPLE: A vessel steaming SE. at a speed of 15 knots appears to have a wind blowing from three points on the starboard bow with a force of 6, Beaufort scale. What is the true direction and force?

In the column headed 3 (meaning three points on bow, apparent direction) and in the line 6 (apparent force, Beaufort scale), we find abreast 15 (knots, speed of vessel) that the true direction is 5 points on starboard bow, *i. e.*, S. by W., and true force 4.

TABLE 33: VERTICAL ANGLES.

This table gives the distance of an object of known height by the vertical angle that it subtends at the position of the observer. It was computed by the formula:

$$\tan \alpha = \frac{h}{d},$$

where α = the vertical angle;
h = the height of the observed object in feet; and
d = the distance of the object, also converted into feet.

The employment of this method of finding distance is explained in article 139, chapter IV.

TABLE 34: HORIZON ANGLES.

This shows the distance in yards corresponding to any observed angle between an object and the sea horizon beyond, the observer being at a known height.

The method of use is explained in article 139, chapter IV.

TABLE 35: SPEED TABLE.

This table shows the rate of speed, in nautical miles per hour, of a vessel which traverses a measured mile in any given number of minutes and seconds. It is entered with the number of minutes at the top and the number of seconds at the side; under one and abreast the other is the number of knots of speed.

TABLE 36: LOCAL AND STANDARD TIMES.

This table contains the reduction to be applied to the local time to obtain the corresponding time at any other meridian whose time is adopted as a standard. The results are given to the nearest minute of time only, being intended for the reduction of such approximate quantities as the time of high water or time of sunset. More exact reductions, when required, may be made by Table 7.

TABLE 37: LOGARITHMS FOR EQUAL ALTITUDE SIGHTS.

Logarithms of A and B, for computing the Equation of Equal Altitudes, are calculated by the formulae:

$$A=\frac{E}{1800 \sin \frac{1}{2} E}, \qquad B=\frac{E}{1800 \tan \frac{1}{2} E},$$

where E in the numerator is the elapsed time in minutes, and E in the denominator the elapsed time expressed in arc.

If we put

L = latitude of the place of observation, + north, — south,
d = declination of the sun, + north, — south,
n = hourly change of declination, + north, — south,
C = correction to reduce the middle chronometer time to chronometer time of apparent noon, algebraically additive,
C′ = the same for midnight,

we have

$$C = -A\,n \tan L + B\,n \tan d;$$
$$C' = A\,n \tan L + B\,n \tan d.$$

This is Chauvenet's table to aid the solution of the problem of Equal Altitudes, and is explained in article 322 and following articles, Chapter XI.

TABLE 38: EFFECT UPON LONGITUDE OF ERROR IN LATITUDE.

Table 38 shows, approximately, the error in longitude in miles and tenths of a mile, occasioned by an error of one mile in the latitude.

Thus, when the sun's altitude is 30°, the latitude 30°, and the polar distance 100°, the error is eight-tenths of a mile.

The effect of an *increase* of latitude is as follows:

$$\begin{matrix}\text{In } \textit{West} \text{ longitude,} \\ \text{the body being}\end{matrix} \left\{\begin{matrix}\text{East}\\ \text{West}\end{matrix}\right\} \begin{matrix}\text{of meridian, the}\\ \text{longitude is}\end{matrix} \left\{\begin{matrix}\text{decreased}\\ \text{increased}\end{matrix}\right\}, \begin{matrix}\text{except where marked}\\ \text{by *, when it is}\end{matrix} \left\{\begin{matrix}\text{increased}\\ \text{decreased}\end{matrix}\right\}.$$

$$\begin{matrix}\text{In } \textit{East} \text{ longitude,} \\ \text{the body being}\end{matrix} \left\{\begin{matrix}\text{East}\\ \text{West}\end{matrix}\right\} \begin{matrix}\text{of meridian, the}\\ \text{longitude is}\end{matrix} \left\{\begin{matrix}\text{increased}\\ \text{decreased}\end{matrix}\right\}, \begin{matrix}\text{except where marked}\\ \text{by *, when it is}\end{matrix} \left\{\begin{matrix}\text{decreased}\\ \text{increased}\end{matrix}\right\}.$$

A *decrease* of latitude has the contrary effect.

The direction of error may readily be seen by drawing the Sumner line in a direction at right angles to the approximate bearing of the body.

TABLE 39: AMPLITUDES.

This table contains amplitudes of heavenly bodies, at rising and setting, for various latitudes and declinations, computed by the formula:

$$\sin \text{amp.} = \sec \text{Lat.} \times \sin \text{dec.}$$

It is entered with the declination at the top and the latitude at the side.

Its use is explained in article 358, Chapter XIV.

TABLE 40: CORRECTION FOR AMPLITUDES.

This table gives a correction to be applied to the observed amplitude to counteract the vertical displacement due to refraction, parallax, and dip, when the body is observed with its center in the visible horizon.

The correction is to be applied for the sun, a planet, or a star, as follows:

$$\left.\begin{matrix}\text{At Rising in N. Lat.}\\ \text{Setting in S. Lat.}\end{matrix}\right\} \text{apply the correction to the right.}$$

$$\left.\begin{matrix}\text{At Rising in S. Lat.}\\ \text{Setting in N. Lat.}\end{matrix}\right\} \text{apply the correction to the left.}$$

For the moon, apply *half* the correction in the *contrary* manner.

TABLE 41: NATURAL SINES AND COSINES.

This table contains the natural sine and cosine for every minute of the quadrant, and is to be entered at the top or bottom with the degrees, and at the side marked M., with the minutes; the corresponding numbers will be the natural sine and cosine, respectively, observing that if the degrees are found at the top, the name sine, cosine, and M. must also be found at the top, and the contrary if the degrees are found at the bottom. It should be understood that all numbers given in the table should be divided by 100,000—that is, pointed off to contain five decimal places. Thus, .43366 is the natural sine of 25° 42′, or the cosine of 64° 18′.

In the outer columns of the margin are given tables of proportional parts, for the purpose of finding, approximately, by inspection, the proportional part corresponding to any number of seconds in the proposed angle, the seconds being found in the marginal column marked M., and the correction in the adjoining column. Thus, if we suppose that it were required to find the natural sine corresponding to 25° 42′ 19″, the difference of the sines of 25° 42′ and 25° 43′ is 26, being the same as at the top of the left-hand column of the table; and in this column, and opposite 19 in the column M., is the correction 8. *Adding* this to the above number .43366, because the numbers are *increasing*, we get .43374 for the sine of 25° 42′ 19″. In like manner, we find the cosine of the same angle to be .90108 − 4 = .90104, using the right-hand columns, and *subtracting* because the numbers are *decreasing;* observing, however, that the number 14 at the top of this column varies 1 from the difference between the cosines of 25° 42′ and 25° 43′, which is only 13; so that the table may give in some cases a unit too much between the angles 25° 42′ and 25° 43′; but this is, in general, of but little importance, and when accuracy is required, the usual method of proportional parts is to be resorted to, using the actual tabular difference.

TABLE 42: LOGARITHMS OF NUMBERS.

This table, containing the common logarithms of numbers, was compared with Sherwin's, Hutton's, and Taylor's logarithms; its use is explained in an article on Logarithms in Appendix III.

TABLE 43: LOGARITHMS OF TRIGONOMETRIC FUNCTIONS, QUARTER POINTS.

This table contains the logarithms of the sines, tangents, etc., corresponding to points and quarter points of the compass. This was compared with Sherwin's, Hutton's, and Taylor's logarithms.

TABLE 44: LOGARITHMS OF TRIGONOMETRIC FUNCTIONS, DEGREES.

This table contains the common logarithms of the sines, tangents, secants, etc. It was compared with Sherwin's, Hutton's, and Taylor's tables. Two additional columns are given in this table, which are very convenient in finding the time from an altitude of the sun; also, three columns of proportional parts for seconds of space, and a small table at the bottom of each page for finding the proportional parts for seconds of time. The degrees are marked to 180°, which saves the trouble of subtracting the given angle from 180° when it exceeds 90°.

The use of this table is fully explained in Appendix III in an article on Logarithms.

TABLE 1.

Difference of Latitude and Departure for ¼ Point.

N. ¼ E. | N. ¼ W. | S. ¼ E. | S. ¼ W.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.0	61	60.9	3.0	121	120.9	5.9	181	180.8	8.9	241	240.7	11.8
2	2.0	0.1	62	61.9	3.0	22	121.9	6.0	82	181.8	8.9	42	241.7	11.9
3	3.0	0.1	63	62.9	3.1	23	122.9	6.0	83	182.8	9.0	43	242.7	11.9
4	4.0	0.2	64	63.9	3.1	24	123.9	6.1	84	183.8	9.0	44	243.7	12.0
5	5.0	0.2	65	64.9	3.2	25	124.8	6.1	85	184.8	9.1	45	244.7	12.0
6	6.0	0.3	66	65.9	3.2	26	125.8	6.2	86	185.8	9.1	46	245.7	12.1
7	7.0	0.3	67	66.9	3.3	27	126.8	6.2	87	186.8	9.2	47	246.7	12.1
8	8.0	0.4	68	67.9	3.3	28	127.8	6.3	88	187.8	9.2	48	247.7	12.2
9	9.0	0.4	69	68.9	3.4	29	128.8	6.3	89	188.8	9.3	49	248.7	12.2
10	10.0	0.5	70	69.9	3.4	30	129.8	6.4	90	189.8	9.3	50	249.7	12.3
11	11.0	0.5	71	70.9	3.5	131	130.8	6.4	191	190.8	9.4	251	250.7	12.3
12	12.0	0.6	72	71.9	3.5	32	131.8	6.5	92	191.8	9.4	52	251.7	12.4
13	13.0	0.6	73	72.9	3.6	33	132.8	6.5	93	192.8	9.5	53	252.7	12.4
14	14.0	0.7	74	73.9	3.6	34	133.8	6.6	94	193.8	9.5	54	253.7	12.5
15	15.0	0.7	75	74.9	3.7	35	134.8	6.6	95	194.8	9.6	55	254.7	12.5
16	16.0	0.8	76	75.9	3.7	36	135.8	6.7	96	195.8	9.6	56	255.7	12.6
17	17.0	0.8	77	76.9	3.8	37	136.8	6.7	97	196.8	9.7	57	256.7	12.6
18	18.0	0.9	78	77.9	3.8	38	137.8	6.8	98	197.8	9.7	58	257.7	12.7
19	19.0	0.9	79	78.9	3.9	39	138.8	6.8	99	198.8	9.8	59	258.7	12.7
20	20.0	1.0	80	79.9	3.9	40	139.8	6.9	200	199.8	9.8	60	259.7	12.8
21	21.0	1.0	81	80.9	4.0	141	140.8	6.9	201	200.8	9.9	261	260.7	12.8
22	22.0	1.1	82	81.9	4.0	42	141.8	7.0	02	201.8	9.9	62	261.7	12.9
23	23.0	1.1	83	82.9	4.1	43	142.8	7.0	03	202.8	10.0	63	262.7	12.9
24	24.0	1.2	84	83.9	4.1	44	143.8	7.1	04	203.8	10.0	64	263.7	13.0
25	25.0	1.2	85	84.9	4.2	45	144.8	7.1	05	204.8	10.1	65	264.7	13.0
26	26.0	1.3	86	85.9	4.2	46	145.8	7.2	06	205.8	10.1	66	265.7	13.1
27	27.0	1.3	87	86.9	4.3	47	146.8	7.2	07	206.8	10.2	67	266.7	13.1
28	28.0	1.4	88	87.9	4.3	48	147.8	7.3	08	207.7	10.2	68	267.7	13.2
29	29.0	1.4	89	88.9	4.4	49	148.8	7.3	09	208.7	10.3	69	268.7	13.2
30	30.0	1.5	90	89.9	4.4	50	149.8	7.4	10	209.7	10.3	70	269.7	13.2
31	31.0	1.5	91	90.9	4.5	151	150.8	7.4	211	210.7	10.4	271	270.7	13.3
32	32.0	1.6	92	91.9	4.5	52	151.8	7.5	12	211.7	10.4	72	271.7	13.3
33	33.0	1.6	93	92.9	4.6	53	152.8	7.5	13	212.7	10.5	73	272.7	13.4
34	34.0	1.7	94	93.9	4.6	54	153.8	7.6	14	213.7	10.5	74	273.7	13.4
35	35.0	1.7	95	94.9	4.7	55	154.8	7.6	15	214.7	10.5	75	274.7	13.5
36	36.0	1.8	96	95.9	4.7	56	155.8	7.7	16	215.7	10.6	76	275.7	13.5
37	37.0	1.8	97	96.9	4.8	57	156.8	7.7	17	216.7	10.6	77	276.7	13.6
38	38.0	1.9	98	97.9	4.8	58	157.8	7.8	18	217.7	10.7	78	277.7	13.6
39	39.0	1.9	99	98.9	4.9	59	158.8	7.8	19	218.7	10.7	79	278.7	13.7
40	40.0	2.0	100	99.9	4.9	60	159.8	7.9	20	219.7	10.8	80	279.7	13.7
41	41.0	2.0	101	100.9	5.0	161	160.8	7.9	221	220.7	10.8	281	280.7	13.8
42	41.9	2.1	02	101.9	5.0	62	161.8	7.9	22	221.7	10.9	82	281.7	13.8
43	42.9	2.1	03	102.9	5.1	63	162.8	8.0	23	222.7	10.9	83	282.7	13.9
44	43.9	2.2	04	103.9	5.1	64	163.8	8.0	24	223.7	11.0	84	283.7	13.9
45	44.9	2.2	05	104.9	5.2	65	164.8	8.1	25	224.7	11.0	85	284.7	14.0
46	45.9	2.3	06	105.9	5.2	66	165.8	8.1	26	225.7	11.1	86	285.7	14.0
47	46.9	2.3	07	106.9	5.3	67	166.8	8.2	27	226.7	11.1	87	286.7	14.1
48	47.9	2.4	08	107.9	5.3	68	167.8	8.2	28	227.7	11.2	88	287.7	14.1
49	48.9	2.4	09	108.9	5.3	69	168.8	8.3	29	228.7	11.2	89	288.7	14.2
50	49.9	2.5	10	109.9	5.4	70	169.8	8.3	30	229.7	11.3	90	289.7	14.2
51	50.9	2.5	111	110.9	5.4	171	170.8	8.4	231	230.7	11.3	291	290.6	14.3
52	51.9	2.6	12	111.9	5.5	72	171.8	8.4	32	231.7	11.4	92	291.6	14.3
53	52.9	2.6	13	112.9	5.5	73	172.8	8.5	33	232.7	11.4	93	292.6	14.4
54	53.9	2.6	14	113.9	5.6	74	173.8	8.5	34	233.7	11.5	94	293.6	14.4
55	54.9	2.7	15	114.9	5.6	75	174.8	8.6	35	234.7	11.5	95	294.6	14.5
56	55.9	2.7	16	115.9	5.7	76	175.8	8.6	36	235.7	11.6	96	295.6	14.5
57	56.9	2.8	17	116.9	5.7	77	176.8	8.7	37	236.7	11.6	97	296.6	14.6
58	57.9	2.8	18	117.9	5.8	78	177.8	8.7	38	237.7	11.7	98	297.6	14.6
59	58.9	2.9	19	118.9	5.8	79	178.8	8.8	39	238.7	11.7	99	298.6	14.7
60	59.9	2.9	20	119.9	5.9	80	179.8	8.8	40	239.7	11.8	300	299.6	14.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

E. ¼ N. | E. ¼ S. | W. ¼ N. | W. ¼ S. | [For 7¾ Points.

TABLE 1.

Difference of Latitude and Departure for ½ Point.

N. ½ E. N. ½ W. S. ½ E. S. ½ W.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.1	61	60.7	6.0	121	120.4	11.9	181	180.1	17.7	241	239.8	23.6
2	2.0	0.2	62	61.7	6.1	22	121.4	12.0	82	181.1	17.8	42	240.8	23.7
3	3.0	0.3	63	62.7	6.2	23	122.4	12.1	83	182.1	17.9	43	241.8	23.8
4	4.0	0.4	64	63.7	6.3	24	123.4	12.2	84	183.1	18.0	44	242.8	23.9
5	5.0	0.5	65	64.7	6.4	25	124.4	12.3	85	184.1	18.1	45	243.8	24.0
6	6.0	0.6	66	65.7	6.5	26	125.4	12.4	86	185.1	18.2	46	244.8	24.1
7	7.0	0.7	67	66.7	6.6	27	126.4	12.4	87	186.1	18.3	47	245.8	24.2
8	8.0	0.8	68	67.7	6.7	28	127.4	12.5	88	187.1	18.4	48	246.8	24.3
9	9.0	0.9	69	68.7	6.8	29	128.4	12.6	89	188.1	18.5	49	247.8	24.4
10	10.0	1.0	70	69.7	6.9	30	129.4	12.7	90	189.1	18.6	50	248.8	24.5
11	10.9	1.1	71	70.7	7.0	131	130.4	12.8	191	190.1	18.7	251	249.8	24.6
12	11.9	1.2	72	71.7	7.1	32	131.4	12.9	92	191.1	18.8	52	250.8	24.7
13	12.9	1.3	73	72.6	7.2	33	132.4	13.0	93	192.1	18.9	53	251.8	24.8
14	13.9	1.4	74	73.6	7.3	34	133.4	13.1	94	193.1	19.0	54	252.8	24.9
15	14.9	1.5	75	74.6	7.4	35	134.3	13.2	95	194.1	19.1	55	253.8	25.0
16	15.9	1.6	76	75.6	7.4	36	135.3	13.3	96	195.1	19.2	56	254.8	25.1
17	16.9	1.7	77	76.6	7.5	37	136.3	13.4	97	196.1	19.3	57	255.8	25.2
18	17.9	1.8	78	77.6	7.6	38	137.3	13.5	98	197.0	19.4	58	256.8	25.3
19	18.9	1.9	79	78.6	7.7	39	138.3	13.6	99	198.0	19.5	59	257.8	25.4
20	19.9	2.0	80	79.6	7.8	40	139.3	13.7	200	199.0	19.6	60	258.7	25.5
21	20.9	2.1	81	80.6	7.9	141	140.3	13.8	201	200.0	19.7	261	259.7	25.6
22	21.9	2.2	82	81.6	8.0	42	141.3	13.9	02	201.0	19.8	62	260.7	25.7
23	22.9	2.3	83	82.6	8.1	43	142.3	14.0	03	202.0	19.9	63	261.7	25.8
24	23.9	2.4	84	83.6	8.2	44	143.3	14.1	04	203.0	20.0	64	262.7	25.9
25	24.9	2.5	85	84.6	8.3	45	144.3	14.2	05	204.0	20.1	65	263.7	26.0
26	25.9	2.5	86	85.6	8.4	46	145.3	14.3	06	205.0	20.2	66	264.7	26.1
27	26.9	2.6	87	86.6	8.5	47	146.3	14.4	07	206.0	20.3	67	265.7	26.2
28	27.9	2.7	88	87.6	8.6	48	147.3	14.5	08	207.0	20.4	68	266.7	26.3
29	28.9	2.8	89	88.6	8.7	49	148.3	14.6	09	208.0	20.5	69	267.7	26.4
30	29.9	2.9	90	89.6	8.8	50	149.3	14.7	10	209.0	20.6	70	268.7	26.5
31	30.9	3.0	91	90.6	8.9	151	150.3	14.8	211	210.0	20.7	271	269.7	26.6
32	31.8	3.1	92	91.6	9.0	52	151.3	14.9	12	211.0	20.8	72	270.7	26.7
33	32.8	3.2	93	92.6	9.1	53	152.3	15.0	13	212.0	20.9	73	271.7	26.8
34	33.8	3.3	94	93.5	9.2	54	153.3	15.1	14	213.0	21.0	74	272.7	26.9
35	34.8	3.4	95	94.5	9.3	55	154.3	15.2	15	214.0	21.1	75	273.7	27.0
36	35.8	3.5	96	95.5	9.4	56	155.2	15.3	16	215.0	21.2	76	274.7	27.1
37	36.8	3.6	97	96.5	9.5	57	156.2	15.4	17	216.0	21.3	77	275.7	27.2
38	37.8	3.7	98	97.5	9.6	58	157.2	15.5	18	217.0	21.4	78	276.7	27.2
39	38.8	3.8	99	98.5	9.7	59	158.2	15.6	19	217.9	21.5	79	277.7	27.3
40	39.8	3.9	100	99.5	9.8	60	159.2	15.7	20	218.9	21.6	80	278.7	27.4
41	40.8	4.0	101	100.5	9.9	161	160.2	15.8	221	219.9	21.7	281	279.6	27.5
42	41.8	4.1	02	101.5	10.0	62	161.2	15.9	22	220.9	21.8	82	280.6	27.6
43	42.8	4.2	03	102.5	10.1	63	162.2	16.0	23	221.9	21.9	83	281.6	27.7
44	43.8	4.3	04	103.5	10.2	64	163.2	16.1	24	222.9	22.0	84	282.6	27.8
45	44.8	4.4	05	104.5	10.3	65	164.2	16.2	25	223.9	22.1	85	283.6	27.9
46	45.8	4.5	06	105.5	10.4	66	165.2	16.3	26	224.9	22.2	86	284.6	28.0
47	46.8	4.6	07	106.5	10.5	67	166.2	16.4	27	225.9	22.2	87	285.6	28.1
48	47.8	4.7	08	107.5	10.6	68	167.2	16.5	28	226.9	22.3	88	286.6	28.2
49	48.8	4.8	09	108.5	10.7	69	168.2	16.6	29	227.9	22.4	89	287.6	28.3
50	49.8	4.9	10	109.5	10.8	70	169.2	16.7	30	228.9	22.5	90	288.6	28.4
51	50.8	5.0	111	110.5	10.9	171	170.2	16.8	231	229.9	22.6	291	289.6	28.5
52	51.7	5.1	12	111.5	11.0	72	171.2	16.9	32	230.9	22.7	92	290.6	28.6
53	52.7	5.2	13	112.5	11.1	73	172.2	17.0	33	231.9	22.8	93	291.6	28.7
54	53.7	5.3	14	113.5	11.2	74	173.2	17.1	34	232.9	22.9	94	292.6	28.8
55	54.7	5.4	15	114.4	11.3	75	174.2	17.2	35	233.9	23.0	95	293.6	28.9
56	55.7	5.5	16	115.4	11.4	76	175.2	17.3	36	234.9	23.1	96	294.6	29.0
57	56.7	5.6	17	116.4	11.5	77	176.1	17.3	37	235.9	23.2	97	295.6	29.1
58	57.7	5.7	18	117.4	11.6	78	177.1	17.4	38	236.9	23.3	98	296.6	29.2
59	58.7	5.8	19	118.4	11.7	79	178.1	17.5	39	237.8	23.4	99	297.6	29.3
60	59.7	5.9	20	119.4	11.8	80	179.1	17.6	40	238.8	23.5	300	298.6	29.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

E. ½ N. E. ½ S. W. ½ N. W ½ S. [For 7½ Points.

TABLE 1.

Difference of Latitude and Departure for ¾ Point.

N. ¾ E. N. ¾ W. S. ¾ E. S. ¾ W.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.1	61	60.3	9.0	121	119.7	17.8	181	179.0	26.6	241	238.4	35.4
2	2.0	0.3	62	61.3	9.1	22	120.7	17.9	82	180.0	26.7	42	239.4	35.5
3	3.0	0.4	63	62.3	9.2	23	121.7	18.0	83	181.0	26.9	43	240.4	35.7
4	4.0	0.6	64	63.3	9.4	24	122.7	18.2	84	182.0	27.0	44	241.4	35.8
5	4.9	0.7	65	64.3	9.5	25	123.6	18.3	85	183.0	27.1	45	242.3	35.9
6	5.9	0.9	66	65.3	9.7	26	124.6	18.5	86	184.0	27.3	46	243.3	36.1
7	6.9	1.0	67	66.3	9.8	27	125.6	18.6	87	185.0	27.4	47	244.3	36.2
8	7.9	1.2	68	67.3	10.0	28	126.6	18.8	88	186.0	27.6	48	245.3	36.4
9	8.9	1.3	69	68.3	10.1	29	127.6	18.9	89	187.0	27.7	49	246.3	36.5
10	9.9	1.5	70	69.2	10.3	30	128.6	19.1	90	187.9	27.9	50	247.3	36.7
11	10.9	1.6	71	70.2	10.4	131	129.6	19.2	191	188.9	28.0	251	248.3	36.8
12	11.9	1.8	72	71.2	10.6	32	130.6	19.4	92	189.9	28.2	52	249.3	37.0
13	12.9	1.9	73	72.2	10.7	33	131.6	19.5	93	190.9	28.3	53	250.3	37.1
14	13.8	2.1	74	73.2	10.9	34	132.5	19.7	94	191.9	28.5	54	251.3	37.3
15	14.8	2.2	75	74.2	11.0	35	133.5	19.8	95	192.9	28.6	55	252.2	37.4
16	15.8	2.3	76	75.2	11.2	36	134.5	20.0	96	193.9	28.8	56	253.2	37.6
17	16.8	2.5	77	76.2	11.3	37	135.5	20.1	97	194.9	28.9	57	254.2	37.7
18	17.8	2.6	78	77.2	11.4	38	136.5	20.2	98	195.9	29.1	58	255.2	37.9
19	18.8	2.8	79	78.1	11.6	39	137.5	20.4	99	196.8	29.2	59	256.2	38.0
20	19.8	2.9	80	79.1	11.7	40	138.5	20.5	200	197.8	29.3	60	257.2	38.1
21	20.8	3.1	81	80.1	11.9	141	139.5	20.7	201	198.8	29.5	261	258.2	38.3
22	21.8	3.2	82	81.1	12.0	42	140.5	20.8	02	199.8	29.6	62	259.2	38.4
23	22.8	3.4	83	82.1	12.2	43	141.5	21.0	03	200.8	29.8	63	260.2	38.6
24	23.7	3.5	84	83.1	12.3	44	142.4	21.1	04	201.8	29.9	64	261.1	38.7
25	24.7	3.7	85	84.1	12.5	45	143.4	21.3	05	202.8	30.1	65	262.1	38.9
26	25.7	3.8	86	85.1	12.6	46	144.4	21.4	06	203.8	30.2	66	263.1	39.0
27	26.7	4.0	87	86.1	12.8	47	145.4	21.6	07	204.8	30.4	67	264.1	39.2
28	27.7	4.1	88	87.0	12.9	48	146.4	21.7	08	205.7	30.5	68	265.1	39.3
29	28.7	4.3	89	88.0	13.1	49	147.4	21.9	09	206.7	30.7	69	266.1	39.5
30	29.7	4.4	90	89.0	13.2	50	148.4	22.0	10	207.7	30.8	70	267.1	39.6
31	30.7	4.5	91	90.0	13.4	151	149.4	22.2	211	208.7	31.0	271	268.1	39.8
32	31.7	4.7	92	91.0	13.5	52	150.4	22.3	12	209.7	31.1	72	269.1	39.9
33	32.6	4.8	93	92.0	13.6	53	151.3	22.4	13	210.7	31.3	73	270.0	40.1
34	33.6	5.0	94	93.0	13.8	54	152.3	22.6	14	211.7	31.4	74	271.0	40.2
35	34.6	5.1	95	94.0	13.9	55	153.3	22.7	15	212.7	31.5	75	272.0	40.4
36	35.6	5.3	96	95.0	14.1	56	154.3	22.9	16	213.7	31.7	76	273.0	40.5
37	36.6	5.4	97	96.0	14.2	57	155.3	23.0	17	214.7	31.8	77	274.0	40.6
38	37.6	5.6	98	96.9	14.4	58	156.3	23.2	18	215.6	32.0	78	275.0	40.8
39	38.6	5.7	99	97.9	14.5	59	157.3	23.3	19	216.6	32.1	79	276.0	40.9
40	39.6	5.9	100	98.9	14.7	60	158.3	23.5	20	217.6	32.3	80	277.0	41.1
41	40.6	6.0	101	99.9	14.8	161	159.3	23.6	221	218.6	32.4	281	278.0	41.2
42	41.5	6.2	02	100.9	15.0	62	160.2	23.8	22	219.6	32.6	82	278.9	41.4
43	42.5	6.3	03	101.9	15.1	63	161.2	23.9	23	220.6	32.7	83	279.9	41.5
44	43.5	6.5	04	102.9	15.3	64	162.2	24.1	24	221.6	32.9	84	280.9	41.7
45	44.5	6.6	05	103.9	15.4	65	163.2	24.2	25	222.6	33.0	85	281.9	41.8
46	45.5	6.7	06	104.9	15.6	66	164.2	24.4	26	223.6	33.2	86	282.9	42.0
47	46.5	6.9	07	105.8	15.7	67	165.2	24.5	27	224.5	33.3	87	283.9	42.1
48	47.5	7.0	08	106.8	15.8	68	166.2	24.7	28	225.5	33.5	88	284.9	42.3
49	48.5	7.2	09	107.8	16.0	69	167.2	24.8	29	226.5	33.6	89	285.9	42.4
50	49.5	7.3	10	108.8	16.1	70	168.2	24.9	30	227.5	33.7	90	286.9	42.6
51	50.4	7.5	111	109.8	16.3	171	169.1	25.1	231	228.5	33.9	291	287.9	42.7
52	51.4	7.6	12	110.8	16.4	72	170.1	25.2	32	229.5	34.0	92	288.8	42.8
53	52.4	7.8	13	111.8	16.6	73	171.1	25.4	33	230.5	34.2	93	289.8	43.0
54	53.4	7.9	14	112.8	16.7	74	172.1	25.5	34	231.5	34.3	94	290.8	43.1
55	54.4	8.1	15	113.8	16.9	75	173.1	25.7	35	232.5	34.5	95	291.8	43.3
56	55.4	8.2	16	114.7	17.0	76	174.1	25.8	36	233.4	34.6	96	292.8	43.4
57	56.4	8.4	17	115.7	17.2	77	175.1	26.0	37	234.4	34.8	97	293.8	43.6
58	57.4	8.5	18	116.7	17.3	78	176.1	26.1	38	235.4	34.9	98	294.8	43.7
59	58.4	8.7	19	117.7	17.5	79	177.1	26.3	39	236.4	35.1	99	295.8	43.9
60	59.4	8.8	20	118.7	17.6	80	178.1	26.4	40	237.4	35.2	300	296.8	44.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

E. ¾ N. E. ¾ S. W. ¾ N. W. ¾ S. [For 7¼ Points.

TABLE 1.

Difference of Latitude and Departure for 1 Point.

N. by E.			N. by W.			S. by E.			S. by W.					
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.2	61	59.8	11.9	121	118.7	23.6	181	177.5	35.3	241	236.4	47.0
2	2.0	0.4	62	60.8	12.1	22	119.7	23.8	82	178.5	35.5	42	237.4	47.2
3	2.9	0.6	63	61.8	12.3	23	120.6	24.0	83	179.5	35.7	43	238.3	47.4
4	3.9	0.8	64	62.8	12.5	24	121.6	24.2	84	180.5	35.9	44	239.3	47.6
5	4.9	1.0	65	63.8	12.7	25	122.6	24.4	85	181.4	36.1	45	240.3	47.8
6	5.9	1.2	66	64.7	12.9	26	123.6	24.6	86	182.4	36.3	46	241.3	48.0
7	6.9	1.4	67	65.7	13.1	27	124.6	24.8	87	183.4	36.5	47	242.3	48.2
8	7.8	1.6	68	66.7	13.3	28	125.5	25.0	88	184.4	36.7	48	243.2	48.4
9	8.8	1.8	69	67.7	13.5	29	126.5	25.2	89	185.4	36.9	49	244.2	48.6
10	9.8	2.0	70	68.7	13.7	30	127.5	25.4	90	186.3	37.1	50	245.2	48.8
11	10.8	2.1	71	69.6	13.9	131	128.5	25.6	191	187.3	37.3	251	246.2	49.0
12	11.8	2.3	72	70.6	14.0	32	129.5	25.8	92	188.3	37.5	52	247.2	49.2
13	12.8	2.5	73	71.6	14.2	33	130.4	25.9	93	189.3	37.7	53	248.1	49.4
14	13.7	2.7	74	72.6	14.4	34	131.4	26.1	94	190.3	37.8	54	249.1	49.6
15	14.7	2.9	75	73.6	14.6	35	132.4	26.3	95	191.3	38.0	55	250.1	49.7
16	15.7	3.1	76	74.5	14.8	36	133.4	26.5	96	192.2	38.2	56	251.1	49.9
17	16.7	3.3	77	75.5	15.0	37	134.4	26.7	97	193.2	38.4	57	252.1	50.1
18	17.7	3.5	78	76.5	15.2	38	135.3	26.9	98	194.2	38.6	58	253.0	50.3
19	18.6	3.7	79	77.5	15.4	39	136.3	27.1	99	195.2	38.8	59	254.0	50.5
20	19.6	3.9	80	78.5	15.6	40	137.3	27.3	200	196.2	39.0	60	255.0	50.7
21	20.6	4.1	81	79.4	15.8	141	138.3	27.5	201	197.1	39.2	261	256.0	50.9
22	21.6	4.3	82	80.4	16.0	42	139.3	27.7	02	198.1	39.4	62	257.0	51.1
23	22.6	4.5	83	81.4	16.2	43	140.3	27.9	03	199.1	39.6	63	257.9	51.3
24	23.5	4.7	84	82.4	16.4	44	141.2	28.1	04	200.1	39.8	64	258.9	51.5
25	24.5	4.9	85	83.4	16.6	45	142.2	28.3	05	201.1	40.0	65	259.9	51.7
26	25.5	5.1	86	84.3	16.8	46	143.2	28.5	06	202.0	40.2	66	260.9	51.9
27	26.5	5.3	87	85.3	17.0	47	144.2	28.7	07	203.0	40.4	67	261.9	52.1
28	27.5	5.5	88	86.3	17.2	48	145.2	28.9	08	204.0	40.6	68	262.9	52.3
29	28.4	5.7	89	87.3	17.4	49	146.1	29.1	09	205.0	40.8	69	263.8	52.5
30	29.4	5.9	90	88.3	17.6	50	147.1	29.3	10	206.0	41.0	70	264.8	52.7
31	30.4	6.0	91	89.3	17.8	151	148.1	29.5	211	206.9	41.2	271	265.8	52.9
32	31.4	6.2	92	90.2	17.9	52	149.1	29.7	12	207.9	41.4	72	266.8	53.1
33	32.4	6.4	93	91.2	18.1	53	150.1	29.8	13	208.9	41.6	73	267.8	53.3
34	33.3	6.6	94	92.2	18.3	54	151.0	30.0	14	209.9	41.7	74	268.7	53.5
35	34.3	6.8	95	93.2	18.5	55	152.0	30.2	15	210.9	41.9	75	269.7	53.6
36	35.3	7.0	96	94.2	18.7	56	153.0	30.4	16	211.8	42.1	76	270.7	53.8
37	36.3	7.2	97	95.1	18.9	57	154.0	30.6	17	212.8	42.3	77	271.7	54.0
38	37.3	7.4	98	96.1	19.1	58	155.0	30.8	18	213.8	42.5	78	272.7	54.2
39	38.3	7.6	99	97.1	19.3	59	155.9	31.0	19	214.8	42.7	79	273.6	54.4
40	39.2	7.8	100	98.1	19.5	60	156.9	31.2	20	215.8	42.9	80	274.6	54.6
41	40.2	8.0	101	99.1	19.7	161	157.9	31.4	221	216.8	43.1	281	275.6	54.8
42	41.2	8.2	02	100.0	19.9	62	158.9	31.6	22	217.7	43.3	82	276.6	55.0
43	42.2	8.4	03	101.0	20.1	63	159.9	31.8	23	218.7	43.5	83	277.6	55.2
44	43.2	8.6	04	102.0	20.3	64	160.8	32.0	24	219.7	43.7	84	278.5	55.4
45	44.1	8.8	05	103.0	20.5	65	161.8	32.2	25	220.7	43.9	85	279.5	55.6
46	45.1	9.0	06	104.0	20.7	66	162.8	32.4	26	221.7	44.1	86	280.5	55.8
47	46.1	9.2	07	104.9	20.9	67	163.8	32.6	27	222.6	44.3	87	281.5	56.0
48	47.1	9.4	08	105.9	21.1	68	164.8	32.8	28	223.6	44.5	88	282.5	56.2
49	48.1	9.6	09	106.9	21.3	69	165.8	33.0	29	224.6	44.7	89	283.4	56.4
50	49.0	9.8	10	107.9	21.5	70	166.7	33.2	30	225.6	44.9	90	284.4	56.6
51	50.0	9.9	111	108.9	21.7	171	167.7	33.4	231	226.6	45.1	291	285.4	56.8
52	51.0	10.1	12	109.8	21.9	72	168.7	33.6	32	227.5	45.3	92	286.4	57.0
53	52.0	10.3	13	110.8	22.0	73	169.7	33.8	33	228.5	45.5	93	287.4	57.2
54	53.0	10.5	14	111.8	22.2	74	170.7	33.9	34	229.5	45.7	94	288.4	57.4
55	53.9	10.7	15	112.8	22.4	75	171.6	34.1	35	230.5	45.8	95	289.3	57.6
56	54.9	10.9	16	113.8	22.6	76	172.6	34.3	36	231.5	46.0	96	290.3	57.7
57	55.9	11.1	17	114.8	22.8	77	173.6	34.5	37	232.4	46.2	97	291.3	57.9
58	56.9	11.3	18	115.7	23.0	78	174.6	34.7	38	233.4	46.4	98	292.3	58.1
59	57.9	11.5	19	116.7	23.2	79	175.6	34.9	39	234.4	46.6	99	293.3	58.3
60	58.8	11.7	20	117.7	23.4	80	176.5	35.1	40	235.4	46.8	300	294.2	58.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
E. by N.			E. by S.			W. by N.			W. by S.			[For 7 points.		

TABLE 1.

Difference of Latitude and Departure for 1¼ Points.

N. by E. ¼ E. N. by W. ¼ W. S. by E. ¼ E. S. by W. ¼ W.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.2	61	59.2	14.8	121	117.4	29.4	181	175.6	44.0	241	233.8	58.6
2	1.9	0.5	62	60.1	15.1	22	118.3	29.6	82	176.5	44.2	42	234.7	58.8
3	2.9	0.7	63	61.1	15.3	23	119.3	29.9	83	177.5	44.5	43	235.7	59.0
4	3.9	1.0	64	62.1	15.6	24	120.3	30.1	84	178.5	44.7	44	236.7	59.3
5	4.9	1.2	65	63.1	15.8	25	121.3	30.4	85	179.5	45.0	45	237.7	59.5
6	5.8	1.5	66	64.0	16.0	26	122.2	30.6	86	180.4	45.2	46	238.6	59.8
7	6.8	1.7	67	65.0	16.3	27	123.2	30.9	87	181.4	45.4	47	239.6	60.0
8	7.8	1.9	68	66.0	16.5	28	124.2	31.1	88	182.4	45.7	48	240.6	60.3
9	8.7	2.2	69	66.9	16.8	29	125.1	31.3	89	183.3	45.9	49	241.5	60.5
10	9.7	2.4	70	67.9	17.0	30	126.1	31.6	90	184.3	46.2	50	242.5	60.7
11	10.7	2.7	71	68.9	17.3	131	127.1	31.8	191	185.3	46.4	251	243.5	61.0
12	11.6	2.9	72	69.8	17.5	32	128.0	32.1	92	186.2	46.7	52	244.4	61.2
13	12.6	3.2	73	70.8	17.7	33	129.0	32.3	93	187.2	46.9	53	245.4	61.5
14	13.6	3.4	74	71.8	18.0	34	130.0	32.6	94	188.2	47.1	54	246.4	61.7
15	14.6	3.6	75	72.8	18.2	35	131.0	32.8	95	189.2	47.4	55	247.4	62.0
16	15.5	3.9	76	73.7	18.5	36	131.9	33.0	96	190.1	47.6	56	248.3	62.2
17	16.5	4.1	77	74.7	18.7	37	132.9	33.3	97	191.1	47.9	57	249.3	62.4
18	17.5	4.4	78	75.7	19.0	38	133.9	33.5	98	192.1	48.1	58	250.3	62.7
19	18.4	4.6	79	76.6	19.2	39	134.8	33.8	99	193.0	48.4	59	251.2	62.9
20	19.4	4.9	80	77.6	19.4	40	135.8	34.0	200	194.0	48.6	60	252.2	63.2
21	20.4	5.1	81	78.6	19.7	141	136.8	34.3	201	195.0	48.8	261	253.2	63.4
22	21.3	5.3	82	79.5	19.9	42	137.7	34.5	02	195.9	49.1	62	254.1	63.7
23	22.3	5.6	83	80.5	20.2	43	138.7	34.7	03	196.9	49.3	63	255.1	63.9
24	23.3	5.8	84	81.5	20.4	44	139.7	35.0	04	197.9	49.6	64	256.1	64.1
25	24.3	6.1	85	82.5	20.7	45	140.7	35.2	05	198.9	49.8	65	257.1	64.4
26	25.2	6.3	86	83.4	20.9	46	141.6	35.5	06	199.8	50.1	66	258.0	64.6
27	26.2	6.6	87	84.4	21.1	47	142.6	35.7	07	200.8	50.3	67	259.0	64.9
28	27.2	6.8	88	85.4	21.4	48	143.6	36.0	08	201.8	50.5	68	260.0	65.1
29	28.1	7.0	89	86.3	21.6	49	144.5	36.2	09	202.7	50.8	69	260.9	65.4
30	29.1	7.3	90	87.3	21.9	50	145.5	36.4	10	203.7	51.0	70	261.9	65.6
31	30.1	7.5	91	88.3	22.1	151	146.5	36.7	211	204.7	51.3	271	262.9	65.8
32	31.0	7.8	92	89.2	22.4	52	147.4	36.9	12	205.6	51.5	72	263.8	66.1
33	32.0	8.0	93	90.2	22.6	53	148.4	37.2	13	206.6	51.8	73	264.8	66.3
34	33.0	8.3	94	91.2	22.8	54	149.4	37.4	14	207.6	52.0	74	265.8	66.6
35	34.0	8.5	95	92.2	23.1	55	150.4	37.7	15	208.6	52.2	75	266.8	66.8
36	34.9	8.7	96	93.1	23.3	56	151.3	37.9	16	209.5	52.5	76	267.7	67.1
37	35.9	9.0	97	94.1	23.6	57	152.3	38.1	17	210.5	52.7	77	268.7	67.3
38	36.9	9.2	98	95.1	23.8	58	153.3	38.4	18	211.5	53.0	78	269.7	67.5
39	37.8	9.5	99	96.0	24.1	59	154.2	38.6	19	212.4	53.2	79	270.6	67.8
40	38.8	9.7	100	97.0	24.3	60	155.2	38.9	20	213.4	53.5	80	271.6	68.0
41	39.8	10.0	101	98.0	24.5	161	156.2	39.1	221	214.4	53.7	281	272.6	68.3
42	40.7	10.2	02	98.9	24.8	62	157.1	39.4	22	215.3	53.9	82	273.5	68.5
43	41.7	10.4	03	99.9	25.0	63	158.1	39.6	23	216.3	54.2	83	274.5	68.8
44	42.7	10.7	04	100.9	25.3	64	159.1	39.8	24	217.3	54.4	84	275.5	69.0
45	43.7	10.9	05	101.9	25.5	65	160.1	40.1	25	218.3	54.7	85	277.5	69.2
46	44.6	11.2	06	102.8	25.8	66	161.0	40.3	26	219.2	54.9	86	277.4	69.5
47	45.6	11.4	07	103.8	26.0	67	162.0	40.6	27	220.2	55.2	87	278.4	69.7
48	46.6	11.7	08	104.8	26.2	68	163.0	40.8	28	221.2	55.4	88	279.4	70.0
49	47.5	11.9	09	105.7	26.5	69	163.9	41.1	29	222.1	55.6	89	280.3	70.2
50	48.5	12.1	10	106.7	26.7	70	164.9	41.3	30	223.1	55.9	90	281.3	70.5
51	49.5	12.4	111	107.7	27.0	171	165.9	41.5	231	224.1	56.1	291	282.3	70.7
52	50.4	12.6	12	108.6	27.2	72	166.8	41.8	32	225.0	56.4	92	283.2	71.0
53	51.4	12.9	13	109.6	27.5	73	167.8	42.0	33	226.0	56.6	93	284.2	71.2
54	52.4	13.1	14	110.6	27.7	74	168.8	42.3	34	227.0	56.9	94	285.2	71.4
55	53.4	13.4	15	111.6	27.9	75	169.8	42.5	35	228.0	57.1	95	286.2	71.7
56	54.3	13.6	16	112.5	28.2	76	170.7	42.8	36	228.9	57.3	96	287.1	71.9
57	55.3	13.8	17	113.5	28.4	77	171.7	43.0	37	229.9	57.6	97	288.1	72.2
58	56.3	14.1	18	114.5	28.7	78	172.7	43.3	38	230.9	57.8	98	289.1	72.4
59	57.2	14.3	19	115.4	28.9	79	173.6	43.5	39	231.8	58.1	99	290.9	72.7
60	58.2	14.6	20	116.4	29.2	80	174.6	43.7	40	232.8	58.3	300	291.0	72.9
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

ENE. ¾ E. ESE. ¾ E. WNW. ¾ W. WSW. ¾ W. [For 6¾ Points.

Difference of Latitude and Departure for 1½ Points.

N. by E. ½ E. N. by W. ½ W. S. by E. ½ E. S. by W. ½ W.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.3	61	58.4	17.7	121	115.8	35.1	181	173.2	52.5	241	230.6	70.0
2	1.9	0.6	62	59.3	18.0	22	116.7	35.4	82	174.2	52.8	42	231.6	70.2
3	2.9	0.9	63	60.3	18.3	23	117.7	35.7	83	175.1	53.1	43	232.5	70.5
4	3.8	1.2	64	61.2	18.6	24	118.7	36.0	84	176.1	53.4	44	233.5	70.8
5	4.8	1.5	65	62.2	18.9	25	119.6	36.3	85	177.0	53.7	45	234.5	71.1
6	5.7	1.7	66	63.2	19.2	26	120.6	36.6	86	178.0	54.0	46	235.4	71.4
7	6.7	2.0	67	64.1	19.4	27	121.5	36.9	87	178.9	54.3	47	236.4	71.7
8	7.7	2.3	68	65.1	19.7	28	122.5	37.2	88	179.9	54.6	48	237.3	72.0
9	8.6	2.6	69	66.0	20.0	29	123.4	37.4	89	180.9	54.9	49	238.3	72.3
10	9.6	2.9	70	67.0	20.3	30	124.4	37.7	90	181.8	55.2	50	239.2	72.6
11	10.5	3.2	71	67.9	20.6	131	125.4	38.0	191	182.8	55.4	251	240.2	72.9
12	11.5	3.5	72	68.9	20.9	32	126.3	38.3	92	183.7	55.7	52	241.1	73.2
13	12.4	3.8	73	69.9	21.2	33	127.3	38.6	93	184.7	56.0	53	242.1	73.4
14	13.4	4.1	74	70.8	21.5	34	128.2	38.9	94	185.6	56.3	54	243.1	73.7
15	14.4	4.4	75	71.8	21.8	35	129.2	39.2	95	186.6	56.6	55	244.0	74.0
16	15.3	4.6	76	72.7	22.1	36	130.1	39.5	96	187.6	56.9	56	245.0	74.3
17	16.3	4.9	77	73.7	22.4	37	131.1	39.8	97	188.5	57.2	57	245.9	74.6
18	17.2	5.2	78	74.6	22.6	38	132.1	40.1	98	189.5	57.5	58	246.9	74.9
19	18.2	5.5	79	75.6	22.9	39	133.0	40.3	99	190.4	57.8	59	247.8	75.2
20	19.1	5.8	80	76.6	23.2	40	134.0	40.6	200	191.4	58.1	60	248.8	75.5
21	20.1	6.1	81	77.5	23.5	141	134.9	40.9	201	192.3	58.3	261	249.8	75.8
22	21.1	6.4	82	78.5	23.8	42	135.9	41.2	02	193.3	58.6	62	250.7	76.1
23	22.0	6.7	83	79.4	24.1	43	136.8	41.5	03	194.3	58.9	63	251.7	76.3
24	23.0	7.0	84	80.4	24.4	44	137.8	41.8	04	195.2	59.2	64	252.6	76.6
25	23.9	7.3	85	81.3	24.7	45	138.8	42.1	05	196.2	59.5	65	253.6	76.9
26	24.9	7.5	86	82.3	25.0	46	139.7	42.4	06	197.1	59.8	66	254.5	77.2
27	25.8	7.8	87	83.3	25.3	47	140.7	42.7	07	198.1	60.1	67	255.5	77.5
28	26.8	8.1	88	84.2	25.5	48	141.6	43.0	08	199.0	60.4	68	256.5	77.8
29	27.8	8.4	89	85.2	25.8	49	142.6	43.3	09	200.0	60.7	69	257.4	78.1
30	28.7	8.7	90	86.1	26.1	50	143.5	43.5	10	201.0	61.0	70	258.4	78.4
31	29.7	9.0	91	87.1	26.4	151	144.5	43.8	211	201.9	61.3	271	259.3	78.7
32	30.6	9.3	92	88.0	26.7	52	145.5	44.1	12	202.9	61.5	72	260.3	79.0
33	31.6	9.6	93	89.0	27.0	53	146.4	44.4	13	203.8	61.8	73	261.2	79.2
34	32.5	9.9	94	90.0	27.3	54	147.4	44.7	14	204.8	62.1	74	262.2	79.5
35	33.5	10.2	95	90.9	27.6	55	148.3	45.0	15	205.7	62.4	75	263.2	79.8
36	34.4	10.5	96	91.9	27.9	56	149.3	45.3	16	206.7	62.7	76	264.1	80.1
37	35.4	10.7	97	92.8	28.2	57	150.2	45.6	17	207.7	63.0	77	265.1	80.4
38	36.4	11.0	98	93.8	28.4	58	151.2	45.9	18	208.6	63.3	78	266.0	80.7
39	37.3	11.3	99	94.7	28.7	59	152.2	46.2	19	209.6	63.6	79	267.0	81.0
40	38.3	11.6	100	95.7	29.0	60	153.1	46.4	20	210.5	63.9	80	267.9	81.3
41	39.2	11.9	101	96.7	29.3	161	154.1	46.7	221	211.5	64.2	281	268.9	81.6
42	40.2	12.2	02	97.6	29.6	62	155.0	47.0	22	212.4	64.4	82	269.9	81.9
43	41.1	12.5	03	98.6	29.9	63	156.0	47.3	23	213.4	64.7	83	270.8	82.2
44	42.1	12.8	04	99.5	30.2	64	156.9	47.6	24	214.4	65.0	84	271.8	82.4
45	43.1	13.1	05	100.5	30.5	65	157.9	47.9	25	215.3	65.3	85	272.7	82.7
46	44.0	13.4	06	101.4	30.8	66	158.9	48.2	26	216.3	65.6	86	273.7	83.0
47	45.0	13.6	07	102.4	31.1	67	159.8	48.5	27	217.2	65.9	87	274.6	83.3
48	45.9	13.9	08	103.3	31.4	68	160.8	48.8	28	218.2	66.2	88	275.6	83.6
49	46.9	14.2	09	104.3	31.6	69	161.7	49.1	29	219.1	66.5	89	276.6	83.9
50	47.8	14.5	10	105.3	31.9	70	162.7	49.3	30	220.1	66.8	90	277.5	84.2
51	48.8	14.8	111	106.2	32.2	171	163.6	49.6	231	221.1	67.1	291	278.5	84.5
52	49.8	15.1	12	107.2	32.5	72	164.6	49.9	32	222.0	67.3	92	279.4	84.8
53	50.7	15.4	13	108.1	32.8	73	165.6	50.2	33	223.0	67.6	93	280.4	85.1
54	51.7	15.7	14	109.1	33.1	74	166.5	50.5	34	223.9	67.9	94	281.3	85.3
55	52.6	16.0	15	110.0	33.4	75	167.5	50.8	35	224.9	68.2	95	282.3	85.6
56	53.6	16.3	16	111.0	33.7	76	168.4	51.1	36	225.8	68.5	96	283.3	85.9
57	54.5	16.5	17	112.0	34.0	77	169.4	51.4	37	226.8	68.8	97	284.2	86.2
58	55.5	16.8	18	112.9	34.3	78	170.3	51.7	38	227.8	69.1	98	285.2	86.5
59	56.5	17.1	19	113.9	34.5	79	171.3	52.0	39	228.7	69.4	99	286.1	86.8
60	57.4	17.4	20	114.8	34.8	80	172.2	52.3	40	229.7	69.7	300	287.1	87.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

ENE. ½ E. ESE. ½ E. WNW. ½ W. WSW. ½ W. [For 6½ Points.

TABLE 1.

Difference of Latitude and Departure for 1¾ Points.

N. by E. ¾ E. N. by W. ¾ W. S. by E. ¾ E. S. by W. ¾ W.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.3	61	57.4	20.6	121	113.9	40.8	181	170.4	61.0	241	226.9	81.2
2	1.9	0.7	62	58.4	20.9	22	114.9	41.1	82	171.4	61.3	42	227.9	81.5
3	2.8	1.0	63	59.3	21.2	23	115.8	41.4	83	172.3	61.7	43	228.8	81.9
4	3.8	1.3	64	60.3	21.6	24	116.8	41.8	84	173.2	62.0	44	229.7	82.2
5	4.7	1.7	65	61.2	21.9	25	117.7	42.1	85	174.2	62.3	45	230.7	82.5
6	5.6	2.0	66	62.1	22.2	26	118.6	42.4	86	175.1	62.7	46	231.6	82.9
7	6.6	2.4	67	63.1	22.6	27	119.6	42.8	87	176.1	63.0	47	232.6	83.2
8	7.5	2.7	68	64.0	22.9	28	120.5	43.1	88	177.0	63.3	48	233.5	83.5
9	8.5	3.0	69	65.0	23.2	29	121.5	43.5	89	178.0	63.7	49	234.4	83.9
10	9.4	3.4	70	65.9	23.6	30	122.4	43.8	90	178.9	64.0	50	235.4	84.2
11	10.4	3.7	71	66.8	23.9	131	123.3	44.1	191	179.8	64.3	251	236.3	84.6
12	11.3	4.0	72	67.8	24.3	32	124.3	44.5	92	180.8	64.7	52	237.3	84.9
13	12.2	4.4	73	68.7	24.6	33	125.2	44.8	93	181.7	65.0	53	238.2	85.2
14	13.2	4.7	74	69.7	24.9	34	126.2	45.1	94	182.7	65.4	54	239.2	85.6
15	14.1	5.1	75	70.6	25.3	35	127.1	45.5	95	183.6	65.7	55	240.1	85.9
16	15.1	5.4	76	71.6	25.6	36	128.0	45.8	96	184.5	66.0	56	241.0	86.2
17	16.0	5.7	77	72.5	25.9	37	129.0	46.2	97	185.5	66.4	57	242.0	86.6
18	16.9	6.1	78	73.4	26.3	38	129.9	46.5	98	186.4	66.7	58	242.9	86.9
19	17.9	6.4	79	74.4	26.6	39	130.9	46.8	99	187.4	67.0	59	243.9	87.3
20	18.8	6.7	80	75.3	27.0	40	131.8	47.2	200	188.3	67.4	60	244.8	87.6
21	19.8	7.1	81	76.3	27.3	141	132.8	47.5	201	189.3	67.7	261	245.7	87.9
22	20.7	7.4	82	77.2	27.6	42	133.7	47.8	02	190.2	68.1	62	246.7	88.3
23	21.7	7.7	83	78.1	28.0	43	134.6	48.2	03	191.1	68.4	63	247.6	88.6
24	22.6	8.1	84	79.1	28.3	44	135.6	48.5	04	192.1	68.7	64	248.6	88.9
25	23.5	8.4	85	80.0	28.6	45	136.5	48.8	05	193.0	69.1	65	249.5	89.3
26	24.5	8.8	86	81.0	29.0	46	137.5	49.2	06	194.0	69.4	66	250.5	89.6
27	25.4	9.1	87	81.9	29.3	47	138.4	49.5	07	194.9	69.7	67	251.4	89.9
28	26.4	9.4	88	82.9	29.6	48	139.3	49.9	08	195.8	70.1	68	252.3	90.3
29	27.3	9.8	89	83.8	30.0	49	140.3	50.2	09	196.8	70.4	69	253.3	90.6
30	28.2	10.1	90	84.7	30.3	50	141.2	50.5	10	197.7	70.7	70	254.2	91.0
31	29.2	10.4	91	85.7	30.7	151	142.2	50.9	211	198.7	71.1	271	255.2	91.3
32	30.1	10.8	92	86.6	31.0	52	143.1	51.2	12	199.6	71.4	72	256.1	91.6
33	31.1	11.1	93	87.6	31.3	53	144.1	51.5	13	200.5	71.8	73	257.0	92.0
34	32.0	11.5	94	88.5	31.7	54	145.0	51.9	14	201.5	72.1	74	258.0	92.3
35	33.0	11.8	95	89.4	32.0	55	145.9	52.2	15	202.4	72.4	75	258.9	92.6
36	33.9	12.1	96	90.4	32.3	56	146.9	52.6	16	203.4	72.8	76	259.9	93.0
37	34.8	12.5	97	91.3	32.7	57	147.8	52.9	17	204.3	73.1	77	260.8	93.3
38	35.8	12.8	98	92.3	33.0	58	148.8	53.2	18	205.3	73.4	78	261.7	93.7
39	36.7	13.1	99	93.2	33.4	59	149.7	53.6	19	206.2	73.8	79	262.7	94.0
40	37.7	13.5	100	94.2	33.7	60	150.6	53.9	20	207.1	74.1	80	263.6	94.3
41	38.6	13.8	101	95.1	34.0	161	151.6	54.2	221	208.1	74.5	281	264.6	94.7
42	39.5	14.1	02	96.0	34.4	62	152.5	54.6	22	209.0	74.8	82	265.5	95.0
43	40.5	14.5	03	97.0	34.7	63	153.5	54.9	23	210.0	75.1	83	266.5	95.3
44	41.4	14.8	04	97.9	35.0	64	154.4	55.2	24	210.9	75.5	84	267.4	95.7
45	42.4	15.2	05	98.9	35.4	65	155.4	55.6	25	211.8	75.8	85	268.3	96.0
46	43.3	15.5	06	99.8	35.7	66	156.3	55.9	26	212.8	76.1	86	269.3	96.4
47	44.3	15.8	07	100.7	36.0	67	157.2	56.3	27	213.7	76.5	87	270.2	96.7
48	45.2	16.2	08	101.7	36.4	68	158.2	56.6	28	214.7	76.8	88	271.2	97.0
49	46.1	16.5	09	102.6	36.7	69	159.1	56.9	29	215.6	77.1	89	272.1	97.4
50	47.1	16.8	10	103.6	37.1	70	160.1	57.3	30	216.6	77.5	90	273.0	97.7
51	48.0	17.2	111	104.5	37.4	171	161.0	57.6	231	217.5	77.8	291	274.0	98.0
52	49.0	17.5	12	105.5	37.7	72	161.9	57.9	32	218.4	78.2	92	274.9	98.4
53	49.9	17.9	13	106.4	38.1	73	162.9	58.3	33	219.4	78.5	93	275.9	98.7
54	50.8	18.2	14	107.3	38.4	74	163.8	58.6	34	220.3	78.8	94	276.8	99.0
55	51.8	18.5	15	108.3	38.7	75	164.8	59.0	35	221.3	79.2	95	277.8	99.4
56	52.7	18.9	16	109.2	39.1	76	165.7	59.3	36	222.2	79.5	96	278.7	99.7
57	53.7	19.2	17	110.2	39.4	77	166.7	59.6	37	223.1	79.8	97	279.6	100.1
58	54.6	19.5	18	111.1	39.8	78	167.6	60.0	38	224.1	80.2	98	280.6	100.4
59	55.6	19.9	19	112.0	40.1	79	168.5	60.3	39	225.0	80.5	99	281.5	100.7
60	56.5	20.2	20	113.0	40.4	80	169.5	60.6	40	226.0	80.9	300	282.5	101.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

ENE. ¼ E. ESE. ¼ E. WNW. ¼ W. WSW. ¼ W. [For 6¼ Points.

Difference of Latitude and Departure for 2 Points.

NNE. NNW. SSE. SSW.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.4	61	56.4	23.3	121	111.8	46.3	181	167.2	69.3	241	222.7	92.2
2	1.8	0.8	62	57.3	23.7	22	112.7	46.7	82	168.1	69.6	42	223.6	92.6
3	2.8	1.1	63	58.2	24.1	23	113.6	47.1	83	169.1	70.0	43	224.5	93.0
4	3.7	1.5	64	59.1	24.5	24	114.6	47.5	84	170.0	70.4	44	225.4	93.4
5	4.6	1.9	65	60.1	24.9	25	115.5	47.8	85	170.9	70.8	45	226.4	93.8
6	5.5	2.3	66	61.0	25.3	26	116.4	48.2	86	171.8	71.2	46	227.3	94.1
7	6.5	2.7	67	61.9	25.6	27	117.3	48.6	87	172.8	71.6	47	228.2	94.5
8	7.4	3.1	68	62.8	26.0	28	118.3	49.0	88	173.7	71.9	48	229.1	94.9
9	8.3	3.4	69	63.7	26.4	29	119.2	49.4	89	174.6	72.3	49	230.0	95.3
10	9.2	3.8	70	64.7	26.8	30	120.1	49.7	90	175.5	72.7	50	231.0	95.7
11	10.2	4.2	71	65.6	27.2	131	121.0	50.1	191	176.5	73.1	251	231.9	96.1
12	11.1	4.6	72	66.5	27.6	32	122.0	50.5	92	177.4	73.5	52	232.8	96.4
13	12.0	5.0	73	67.4	27.9	33	122.9	50.9	93	178.3	73.9	53	233.7	96.8
14	12.9	5.4	74	68.4	28.3	34	123.8	51.3	94	179.2	74.2	54	234.7	97.2
15	13.9	5.7	75	69.3	28.7	35	124.7	51.7	95	180.2	74.6	55	235.6	97.6
16	14.8	6.1	76	70.2	29.1	36	125.6	52.0	96	181.1	75.0	56	236.5	98.0
17	15.7	6.5	77	71.1	29.5	37	126.6	52.4	97	182.0	75.4	57	237.4	98.3
18	16.6	6.9	78	72.1	29.8	38	127.5	52.8	98	182.9	75.8	58	238.4	98.7
19	17.6	7.3	79	73.0	30.2	39	128.4	53.2	99	183.9	76.2	59	239.3	99.1
20	18.5	7.7	80	73.9	30.6	40	129.3	53.6	200	184.8	76.5	60	240.2	99.5
21	19.4	8.0	81	74.8	31.0	141	130.3	54.0	201	185.7	76.9	261	241.1	99.9
22	20.3	8.4	82	75.8	31.4	42	131.2	54.3	02	186.6	77.3	62	242.1	100.3
23	21.2	8.8	83	76.7	31.8	43	132.1	54.7	03	187.5	77.7	63	243.0	100.6
24	22.2	9.2	84	77.6	32.1	44	133.0	55.1	04	188.5	78.1	64	243.9	101.0
25	23.1	9.6	85	78.5	32.5	45	134.0	55.5	05	189.4	78.5	65	244.8	101.4
26	24.0	9.9	86	79.5	32.9	46	134.9	55.9	06	190.3	78.8	66	245.8	101.8
27	24.9	10.3	87	80.4	33.3	47	135.8	56.3	07	191.2	79.2	67	246.7	102.2
28	25.9	10.7	88	81.3	33.7	48	136.7	56.6	08	192.2	79.6	68	247.6	102.6
29	26.8	11.1	89	82.2	34.1	49	137.7	57.0	09	193.1	80.0	69	248.5	102.9
30	27.7	11.5	90	83.1	34.4	50	138.6	57.4	10	194.0	80.4	70	249.4	103.3
31	28.6	11.9	91	84.1	34.8	151	139.5	57.8	211	194.9	80.7	271	250.4	103.7
32	29.6	12.2	92	85.0	35.2	52	140.4	58.2	12	195.9	81.1	72	251.3	104.1
33	30.5	12.6	93	85.9	35.6	53	141.4	58.6	13	196.8	81.5	73	252.2	104.5
34	31.4	13.0	94	86.8	36.0	54	142.3	58.9	14	197.7	81.9	74	253.1	104.9
35	32.3	13.4	95	87.8	36.4	55	143.2	59.3	15	198.6	82.3	75	254.1	105.2
36	33.3	13.8	96	88.7	36.7	56	144.1	59.7	16	199.6	82.7	76	255.0	105.6
37	34.2	14.2	97	89.6	37.1	57	145.0	60.1	17	200.5	83.0	77	255.9	106.0
38	35.1	14.5	98	90.5	37.5	58	146.0	60.5	18	201.4	83.4	78	256.8	106.4
39	36.0	14.9	99	91.5	37.9	59	146.9	60.8	19	202.3	83.8	79	257.8	106.8
40	37.0	15.3	100	92.4	38.3	60	147.8	61.2	20	203.3	84.2	80	258.7	107.2
41	37.9	15.7	101	93.3	38.7	161	148.7	61.6	221	204.2	84.6	281	259.6	107.5
42	38.8	16.1	02	94.2	39.0	62	149.7	62.0	22	205.1	85.0	82	260.5	107.9
43	39.7	16.5	03	95.2	39.4	63	150.6	62.4	23	206.0	85.3	83	261.5	108.3
44	40.7	16.8	04	96.1	39.8	64	151.5	62.8	24	206.9	85.7	84	262.4	108.7
45	41.6	17.2	05	97.0	40.2	65	152.4	63.1	25	207.9	86.1	85	263.3	109.1
46	42.5	17.6	06	97.9	40.6	66	153.4	63.5	26	208.8	86.5	86	264.2	109.4
47	43.4	18.0	07	98.9	40.9	67	154.3	63.9	27	209.7	86.9	87	265.2	109.8
48	44.3	18.4	08	99.8	41.3	68	155.2	64.3	28	210.6	87.3	88	266.1	110.2
49	45.3	18.8	09	100.7	41.7	69	156.1	64.7	29	211.6	87.6	89	267.0	110.6
50	46.2	19.1	10	101.6	42.1	70	157.1	65.1	30	212.5	88.0	90	267.9	111.0
51	47.1	19.5	111	102.6	42.5	171	158.0	65.4	231	213.4	88.4	291	268.8	111.4
52	48.0	19.9	12	103.5	42.9	72	158.9	65.8	32	214.3	88.8	92	269.8	111.7
53	49.0	20.3	13	104.4	43.2	73	159.8	66.2	33	215.3	89.2	93	270.7	112.1
54	49.9	20.7	14	105.3	43.6	74	160.8	66.6	34	216.2	89.5	94	271.6	112.5
55	50.8	21.0	15	106.2	44.0	75	161.7	67.0	35	217.1	89.9	95	272.5	112.9
56	51.7	21.4	16	107.2	44.4	76	162.6	67.4	36	218.0	90.3	96	273.5	113.3
57	52.7	21.8	17	108.1	44.8	77	163.5	67.7	37	219.0	90.7	97	274.4	113.7
58	53.6	22.2	18	109.0	45.2	78	164.5	68.1	38	219.9	91.1	98	275.3	114.0
59	54.5	22.6	19	109.9	45.5	79	165.4	68.5	39	220.8	91.5	99	276.2	114.4
60	55.4	23.0	20	110.9	45.9	80	166.3	68.9	40	221.7	91.8	300	277.2	114.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat,	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

ENE. ESE. WNW WSW [For 6 Points.

TABLE 1.

Difference of Latitude and Departure for 2¼ Points.

NNE. ¼ E. NNW. ¼ W. SSE. ¼ E. SSW. ¼ W.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.4	61	55.1	26.1	121	109.4	51.7	181	163.6	77.4	241	217.9	103.0
2	1.8	0.9	62	56.0	26.5	22	110.3	52.2	82	164.5	77.8	42	218.8	103.5
3	2.7	1.3	63	57.0	26.9	23	111.2	52.6	83	165.4	78.2	43	219.7	103.9
4	3.6	1.7	64	57.9	27.4	24	112.1	53.0	84	166.3	78.7	44	220.6	104.3
5	4.5	2.1	65	58.8	27.8	25	113.0	53.4	85	167.2	79.1	45	221.5	104.8
6	5.4	2.6	66	59.7	28.2	26	113.9	53.9	86	168.1	79.5	46	222.4	105.2
7	6.3	3.0	67	60.6	28.6	27	114.8	54.3	87	169.0	80.0	47	223.3	105.6
8	7.2	3.4	68	61.5	29.1	28	115.7	54.7	88	169.9	80.4	48	224.2	106.0
9	8.1	3.8	69	62.4	29.5	29	116.6	55.2	89	170.9	80.8	49	225.1	106.5
10	9.0	4.3	70	63.3	29.9	30	117.5	55.6	90	171.8	81.2	50	226.0	106.9
11	9.9	4.7	71	64.2	30.4	131	118.4	56.0	191	172.7	81.7	251	226.9	107.3
12	10.8	5.1	72	65.1	30.8	32	119.3	56.4	92	173.6	82.1	52	227.8	107.7
13	11.8	5.6	73	66.0	31.2	33	120.2	56.9	93	174.5	82.5	53	228.7	108.2
14	12.7	6.0	74	66.9	31.6	34	121.1	57.3	94	175.4	82.9	54	229.6	108.6
15	13.6	6.4	75	67.8	32.1	35	122.0	57.7	95	176.3	83.4	55	230.5	109.0
16	14.5	6.8	76	68.7	32.5	36	122.9	58.1	96	177.2	83.8	56	231.4	109.5
17	15.4	7.3	77	69.6	32.9	37	123.8	58.6	97	178.1	84.2	57	232.3	109.9
18	16.3	7.7	78	70.5	33.3	38	124.8	59.0	98	179.0	84.7	58	233.2	110.3
19	17.2	8.1	79	71.4	33.8	39	125.7	59.4	99	179.9	85.1	59	234.1	110.7
20	18.1	8.6	80	72.3	34.2	40	126.6	59.9	200	180.8	85.5	60	235.0	111.2
21	19.0	9.0	81	73.2	34.6	141	127.5	60.3	201	181.7	85.9	261	235.9	111.6
22	19.9	9.4	82	74.1	35.1	42	128.4	60.7	02	182.6	86.4	62	236.8	112.0
23	20.8	9.8	83	75.0	35.5	43	129.3	61.1	03	183.5	86.8	63	237.7	112.4
24	21.7	10.3	84	75.9	35.9	44	130.2	61.6	04	184.4	87.2	64	238.7	112.9
25	22.6	10.7	85	76.8	36.3	45	131.1	62.0	05	185.3	87.6	65	239.6	113.3
26	23.5	11.1	86	77.7	36.8	46	132.0	62.4	06	186.2	88.1	66	240.5	113.7
27	24.4	11.5	87	78.6	37.2	47	132.9	62.9	07	187.1	88.5	67	241.4	114.2
28	25.3	12.0	88	79.6	37.6	48	133.8	63.3	08	188.0	88.9	68	242.3	114.6
29	26.2	12.4	89	80.5	38.1	49	134.7	63.7	09	188.9	89.4	69	243.2	115.0
30	27.1	12.8	90	81.4	38.5	50	135.6	64.1	10	189.8	89.8	70	244.1	115.4
31	28.0	13.3	91	82.3	38.9	151	136.5	64.6	211	190.7	90.2	271	245.0	115.9
32	28.9	13.7	92	83.2	39.3	52	137.4	65.0	12	191.6	90.6	72	245.9	116.3
33	29.8	14.1	93	84.1	39.8	53	138.3	65.4	13	192.5	91.1	73	246.8	116.7
34	30.7	14.5	94	85.0	40.2	54	139.2	65.8	14	193.5	91.5	74	247.7	117.2
35	31.6	15.0	95	85.9	40.6	55	140.1	66.3	15	194.4	91.9	75	248.6	117.6
36	32.5	15.4	96	86.8	41.0	56	141.0	66.7	16	195.3	92.4	76	249.5	118.0
37	33.4	15.8	97	87.7	41.5	57	141.9	67.1	17	196.2	92.8	77	250.4	118.4
38	34.4	16.2	98	88.6	41.9	58	142.8	67.6	18	197.1	93.2	78	251.3	118.9
39	35.3	16.7	99	89.5	42.3	59	143.7	68.0	19	198.0	93.6	79	252.2	119.3
40	36.2	17.1	100	90.4	42.8	60	144.6	68.4	20	198.9	94.1	80	253.1	119.7
41	37.1	17.5	101	91.3	43.2	161	145.5	68.8	221	199.8	94.5	281	254.0	120.1
42	38.0	18.0	02	92.2	43.6	62	146.4	69.3	22	200.7	94.9	82	254.9	120.6
43	38.9	18.4	03	93.1	44.0	63	147.4	69.7	23	201.6	95.3	83	255.8	121.0
44	39.8	18.8	04	94.0	44.5	64	148.3	70.1	24	202.5	95.8	84	256.7	121.4
45	40.7	19.2	05	94.9	44.9	65	149.2	70.5	25	203.4	96.2	85	257.6	121.9
46	41.6	19.7	06	95.8	45.3	66	150.1	71.0	26	204.3	96.6	86	258.5	122.3
47	42.5	20.1	07	96.7	45.7	67	151.0	71.4	27	205.2	97.1	87	259.4	122.7
48	43.4	20.5	08	97.6	46.2	68	151.9	71.8	28	206.1	97.5	88	260.3	123.1
49	44.3	21.0	09	98.5	46.6	69	152.8	72.3	29	207.0	97.9	89	261.3	123.6
50	45.2	21.4	10	99.4	47.0	70	153.7	72.7	30	207.9	98.3	90	262.2	124.0
51	46.1	21.8	111	100.3	47.5	171	154.6	73.1	231	208.8	98.8	291	263.1	124.4
52	47.0	22.2	12	101.2	47.9	72	155.5	73.5	32	209.7	99.2	92	264.0	124.8
53	47.9	22.7	13	102.2	48.3	73	156.4	74.0	33	210.6	99.6	93	264.9	125.3
54	48.8	23.1	14	103.1	48.7	74	157.3	74.4	34	211.5	100.0	94	265.8	125.7
55	49.7	23.5	15	104.0	49.2	75	158.2	74.8	35	212.4	100.5	95	266.7	126.1
56	50.6	23.9	16	104.9	49.6	76	159.1	75.2	36	213.3	100.9	96	267.6	126.6
57	51.5	24.4	17	105.8	50.0	77	160.0	75.7	37	214.2	101.3	97	268.5	127.0
58	52.4	24.8	18	106.7	50.5	78	160.9	76.1	38	215.1	101.8	98	269.4	127.4
59	53.3	25.2	19	107.6	50.9	79	161.8	76.5	39	216.1	102.2	99	270.3	127.8
60	54.2	25.7	20	108.5	51.3	80	162.7	77.0	40	217.0	102.6	300	271.2	128.3
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

NE. by E. ¾ E. SE. by E. ¾ E. NW. by W. ¾ W. SW. by W. ¾ W. [For 5¾ Points.

TABLE 1.

Difference of Latitude and Departure for 2½ Points.

NNE. ½ E. NNW. ½ W. SSE. ½ E. SSW. ½ W.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.5	61	53.8	28.8	121	106.7	57.0	181	159.6	85.3	241	212.5	113.6
2	1.8	0.9	62	54.7	29.2	22	107.6	57.5	82	160.5	85.8	42	213.4	114.1
3	2.6	1.4	63	55.6	29.7	23	108.5	58.0	83	161.4	86.3	43	214.3	114.5
4	3.5	1.9	64	56.4	30.2	24	109.4	58.5	84	162.3	86.7	44	215.2	115.0
5	4.4	2.4	65	57.3	30.6	25	110.2	58.9	85	163.2	87.2	45	216.1	115.5
6	5.3	2.8	66	58.2	31.1	26	111.1	59.4	86	164.0	87.7	46	217.0	116.0
7	6.2	3.3	67	59.1	31.6	27	112.0	59.9	87	164.9	88.2	47	217.8	116.4
8	7.1	3.8	68	60.0	32.1	28	112.9	60.3	88	165.8	88.6	48	218.7	116.9
9	7.9	4.2	69	60.9	32.5	29	113.8	60.8	89	166.7	89.1	49	219.6	117.4
10	8.8	4.7	70	61.7	33.0	30	114.6	61.3	90	167.6	89.6	50	220.5	117.8
11	9.7	5.2	71	62.6	33.5	131	115.5	61.8	191	168.4	90.0	251	221.4	118.3
12	10.6	5.7	72	63.5	33.9	32	116.4	62.2	92	169.3	90.5	52	222.2	118.8
13	11.5	6.1	73	64.4	34.4	33	117.3	62.7	93	170.2	91.0	53	223.1	119.3
14	12.3	6.6	74	65.3	34.9	34	118.2	63.2	94	171.1	91.5	54	224.0	119.7
15	13.2	7.1	75	66.1	35.4	35	119.1	63.6	95	172.0	91.9	55	224.9	120.2
16	14.1	7.5	76	67.0	35.8	36	119.9	64.1	96	172.9	92.4	56	225.8	120.7
17	15.0	8.0	77	67.9	36.3	37	120.8	64.6	97	173.7	92.9	57	226.7	121.1
18	15.9	8.5	78	68.8	36.8	38	121.7	65.1	98	174.6	93.3	58	227.5	121.6
19	16.8	9.0	79	69.7	37.2	39	122.6	65.5	99	175.5	93.8	59	228.4	122.1
20	17.6	9.4	80	70.6	37.7	40	123.5	66.0	200	176.4	94.3	60	229.3	122.6
21	18.5	9.9	81	71.4	38.2	141	124.4	66.5	201	177.3	94.8	261	330.2	123.0
22	19.4	10.4	82	72.3	38.7	42	125.2	66.9	02	178.1	95.2	62	231.1	123.5
23	20.3	10.8	83	73.2	39.1	43	126.1	67.4	03	179.0	95.7	63	231.9	124.0
24	21.2	11.3	84	74.1	39.6	44	127.0	67.9	04	179.9	96.2	64	232.8	124.4
25	22.0	11.8	85	75.0	40.1	45	127.9	68.4	05	180.8	96.6	65	233.7	124.9
26	22.9	12.3	86	75.8	40.5	46	128.8	68.8	06	181.7	97.1	66	234.6	125.4
27	23.8	12.7	87	76.7	41.0	47	129.6	69.3	07	182.6	97.6	67	235.5	125.9
28	24.7	13.2	88	77.6	41.5	48	130.5	69.8	08	183.4	98.1	68	236.4	126.3
29	25.6	13.7	89	78.5	42.0	49	131.4	70.2	09	184.3	98.5	69	237.2	126.8
30	26.5	14.1	90	79.4	42.4	50	132.3	70.7	10	185.2	99.0	70	238.1	127.3
31	27.3	14.6	91	80.3	42.9	151	133.2	71.2	211	186.1	99.5	271	239.0	127.7
32	28.2	15.1	92	81.1	43.4	52	134.1	71.7	12	187.0	99.9	72	239.9	128.2
33	29.1	15.6	93	82.0	43.8	53	134.9	72.1	13	187.8	100.4	73	240.8	128.7
34	30.0	16.0	94	82.9	44.3	54	135.8	72.6	14	188.7	100.9	74	241.6	129.2
35	30.9	16.5	95	83.8	44.8	55	136.7	73.1	15	189.6	101.4	75	242.5	129.6
36	31.7	17.0	96	84.7	45.3	56	137.6	73.5	16	190.5	101.8	76	243.4	130.1
37	32.6	17.4	97	85.5	45.7	57	138.5	74.0	17	191.4	102.3	77	244.3	130.6
38	33.5	17.9	98	86.4	46.2	58	139.3	74.5	18	192.3	102.8	78	245.2	131.0
39	34.4	18.4	99	87.3	46.7	59	140.2	75.0	19	193.1	103.2	79	246.1	131.5
40	35.3	18.9	100	88.2	47.1	60	141.1	75.4	20	194.0	103.7	80	246.9	132.0
41	36.2	19.3	101	89.1	47.6	161	142.0	75.9	221	194.9	104.2	281	247.8	132.5
42	37.0	19.8	02	90.0	48.1	62	142.9	76.4	22	195.8	104.7	82	248.7	132.9
43	37.9	20.3	03	90.8	48.6	63	143.8	76.8	23	196.7	105.1	83	249.6	133.4
44	38.8	20.7	04	91.7	49.0	64	144.6	77.3	24	197.6	105.6	84	250.5	133.9
45	39.7	21.2	05	92.6	49.5	65	145.5	77.8	25	198.4	106.1	85	251.3	134.3
46	40.6	21.7	06	93.5	50.0	66	146.4	78.3	26	199.3	106.5	86	252.2	134.8
47	41.5	22.2	07	94.4	50.4	67	147.3	78.7	27	200.2	107.0	87	253.1	135.3
48	42.3	22.6	08	95.2	50.9	68	148.2	79.2	28	201.1	107.5	88	254.0	135.8
49	43.2	23.1	09	96.1	51.4	69	149.0	79.7	29	202.0	107.9	89	254.9	136.2
50	44.1	23.6	10	97.0	51.9	70	149.9	80.1	30	202.8	108.4	90	255.8	136.7
51	45.0	24.0	111	97.9	52.3	171	150.8	80.6	231	203.7	108.9	291	256.6	137.2
52	45.9	24.5	12	98.8	52.8	72	151.7	81.1	32	204.6	109.4	92	257.5	137.6
53	46.7	25.0	13	99.7	53.3	73	152.6	81.6	33	205.5	109.8	93	258.4	138.1
54	47.6	25.5	14	100.5	53.7	74	153.5	82.0	34	206.4	110.3	94	259.3	138.6
55	48.5	25.9	15	101.4	54.2	75	154.3	82.5	35	207.3	110.8	95	260.2	139.1
56	49.4	26.4	16	102.3	54.7	76	155.2	83.0	36	208.1	111.2	96	261.0	139.5
57	50.3	26.9	17	103.2	55.2	77	156.1	83.4	37	209.0	111.7	97	261.9	140.0
58	51.2	27.3	18	104.1	55.6	78	157.0	83.9	38	209.9	112.2	98	262.8	140.5
59	52.0	27.8	19	104.9	56.1	79	157.9	84.4	39	210.8	112.7	99	263.7	140.9
60	52.9	28.3	20	105.8	56.6	80	158.7	84.9	40	211.7	113.1	300	264.6	141.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

NE. by E. ½ E. SE. by E. ½ E. NW. by W. ½ W. SW. by W. ½ W. [For 5½ Points.

TABLE 1.

Difference of Latitude and Departure for 2¾ Points.

NNE. ¾ E. NNW. ¾ W. SSE. ¾ E. SSW. ¾ W.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.5	61	52.3	31.4	121	103.8	62.2	181	155.2	93.1	241	206.7	123.9
2	1.7	1.0	62	53.2	31.9	22	104.6	62.7	82	156.1	93.6	42	207.6	124.4
3	2.6	1.5	63	54.0	32.4	23	105.5	63.2	83	157.0	94.1	43	208.4	124.9
4	3.4	2.1	64	54.9	32.9	24	106.4	63.7	84	157.8	94.6	44	209.3	125.4
5	4.3	2.6	65	55.8	33.4	25	107.2	64.3	85	158.7	95.1	45	210.1	126.0
6	5.1	3.1	66	56.6	33.9	26	108.1	64.8	86	159.5	95.6	46	211.0	126.5
7	6.0	3.6	67	57.5	34.4	27	108.9	65.3	87	160.4	96.1	47	211.9	127.0
8	6.9	4.1	68	58.3	35.0	28	109.8	65.8	88	161.3	96.7	48	212.7	127.5
9	7.7	4.6	69	59.2	35.5	29	110.6	66.3	89	162.1	97.2	49	213.6	128.0
10	8.6	5.1	70	60.0	36.0	30	111.5	66.8	90	163.0	97.7	50	214.4	128.5
11	9.4	5.7	71	60.9	36.5	131	112.4	67.3	191	163.8	98.2	251	215.3	129.0
12	10.3	6.2	72	61.8	37.0	32	113.2	67.9	92	164.7	98.7	52	216.1	129.6
13	11.2	6.7	73	62.6	37.5	33	114.1	68.4	93	165.5	99.2	53	217.0	130.1
14	12.0	7.2	74	63.5	38.0	34	114.9	68.9	94	166.4	99.7	54	217.9	130.6
15	12.9	7.7	75	64.3	38.6	35	115.8	69.4	95	167.3	100.3	55	218.7	131.1
16	13.7	8.2	76	65.2	39.1	36	116.7	69.9	96	168.1	100.8	56	219.6	131.6
17	14.6	8.7	77	66.0	39.6	37	117.5	70.4	97	169.0	101.3	57	220.4	132.1
18	15.4	9.3	78	66.9	40.1	38	118.4	70.9	98	169.8	101.8	58	221.3	132.6
19	16.3	9.8	79	67.8	40.6	39	119.2	71.5	99	170.7	102.3	59	222.2	133.2
20	17.2	10.3	80	68.6	41.1	40	120.1	72.0	200	171.5	102.8	60	223.0	133.7
21	18.0	10.8	81	69.5	41.6	141	120.9	72.5	201	172.4	103.3	261	223.9	134.2
22	18.9	11.3	82	70.3	42.2	42	121.8	73.0	02	173.3	103.8	62	224.7	134.7
23	19.7	11.8	83	71.2	42.7	43	122.7	73.5	03	174.1	104.4	63	225.6	135.2
24	20.6	12.3	84	72.0	43.2	44	123.5	74.0	04	175.0	104.9	64	226.4	135.7
25	21.4	12.9	85	72.9	43.7	45	124.4	74.5	05	175.8	105.4	65	227.3	136.2
26	22.3	13.4	86	73.8	44.2	46	125.2	75.1	06	176.7	105.9	66	228.2	136.8
27	23.2	13.9	87	74.6	44.7	47	126.1	75.6	07	177.5	106.4	67	229.0	137.3
28	24.0	14.4	88	75.5	45.2	48	126.9	76.1	08	178.4	106.9	68	229.9	137.8
29	24.9	14.9	89	76.3	45.8	49	127.8	76.6	09	179.3	107.4	69	230.7	138.3
30	25.7	15.4	90	77.2	46.3	50	128.7	77.1	10	180.1	108.0	70	231.6	138.8
31	26.6	15.9	91	78.1	46.8	151	129.5	77.6	211	181.0	108.5	271	232.4	139.3
32	27.4	16.5	92	78.9	47.3	52	130.4	78.1	12	181.8	109.0	72	233.3	139.8
33	28.3	17.0	93	79.8	47.8	53	131.2	78.7	13	182.7	109.5	73	234.2	140.4
34	29.2	17.5	94	80.6	48.3	54	132.1	79.2	14	183.6	110.0	74	235.0	140.9
35	30.0	18.0	95	81.5	48.8	55	132.9	79.7	15	184.4	110.5	75	235.9	141.4
36	30.9	18.5	96	82.3	49.4	56	133.8	80.2	16	185.3	111.0	76	236.7	141.9
37	31.7	19.0	97	83.2	49.9	57	134.7	80.7	17	186.1	111.6	77	237.6	142.4
38	32.6	19.5	98	84.1	50.4	58	135.5	81.2	18	187.0	112.1	78	238.4	142.9
39	33.5	20.1	99	84.9	50.9	59	136.4	81.7	19	187.8	112.6	79	239.3	143.4
40	34.3	20.6	100	85.8	51.4	60	137.2	82.3	20	188.7	113.1	80	240.2	143.9
41	35.2	21.1	101	86.6	51.9	161	138.1	82.8	221	189.6	113.6	281	241.0	144.5
42	36.0	21.6	02	87.5	52.4	62	139.0	83.3	22	190.4	114.1	82	241.9	145.0
43	36.9	22.1	03	88.3	53.0	63	139.8	83.8	23	191.3	114.6	83	242.7	145.5
44	37.7	22.6	04	89.2	53.5	64	140.7	84.3	24	192.1	115.2	84	243.6	146.0
45	38.6	23.1	05	90.1	54.0	65	141.5	84.8	25	193.0	115.7	85	244.5	146.5
46	39.5	23.6	06	90.9	54.5	66	142.4	85.3	26	193.8	116.2	86	245.3	147.0
47	40.3	24.2	07	91.8	55.0	67	143.2	85.9	27	194.7	116.7	87	246.2	147.5
48	41.2	24.7	08	92.6	55.5	68	144.1	86.4	28	195.6	117.2	88	247.0	148.1
49	42.0	25.2	09	93.5	56.0	69	145.0	86.9	29	196.4	117.7	89	247.9	148.6
50	42.9	25.7	10	94.4	56.6	70	145.8	87.4	30	197.3	118.2	90	248.7	149.1
51	43.7	26.2	111	95.2	57.1	171	146.7	87.9	231	198.1	118.8	291	249.6	149.6
52	44.6	26.7	12	96.1	57.6	72	147.5	88.4	32	199.0	119.3	92	250.5	150.1
53	45.5	27.2	13	96.9	58.1	73	148.4	88.9	33	199.9	119.8	93	251.3	150.6
54	46.3	27.8	14	97.8	58.6	74	149.2	89.5	34	200.7	120.3	94	252.2	151.1
55	47.2	28.3	15	98.6	59.1	75	150.1	90.0	35	201.6	120.8	95	253.0	151.7
56	48.0	28.8	16	99.5	59.6	76	151.0	90.5	36	202.4	121.3	96	253.9	152.2
57	48.9	29.3	17	100.4	60.2	77	151.8	91.0	37	203.3	121.8	97	254.7	152.7
58	49.7	29.8	18	101.2	60.7	78	152.7	91.5	38	204.1	122.4	98	255.6	153.2
59	50.6	30.3	19	102.1	61.2	79	153.5	92.0	39	205.0	122.9	99	256.5	153.7
60	51.5	30.8	20	102.9	61.7	80	154.4	92.5	40	205.9	123.4	300	257.3	154.2
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

NE. by E. ¼ E. SE. by E. ¼ E. NW. by W. ¼ W. SW. by W. ¼ W. [For 5¼ Points.

TABLE 1.

Difference of Latitude and Departure for 3 Points.

NE. by N. NW. by N. SE. by S. SW. by S.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	50.7	33.9	121	100.6	67.2	181	150.5	100.6	241	200.4	133.9
2	1.7	1.1	62	51.6	34.4	22	101.4	67.8	82	151.3	101.1	42	201.2	134.4
3	2.5	1.7	63	52.4	35.0	23	102.3	68.3	83	152.2	101.7	43	202.0	135.0
4	3.3	2.2	64	53.2	35.6	24	103.1	68.9	84	153.0	102.2	44	202.9	135.6
5	4.2	2.8	65	54.0	36.1	25	103.9	69.4	85	153.8	102.8	45	203.7	136.1
6	5.0	3.3	66	54.9	36.7	26	104.8	70.0	86	154.7	103.3	46	204.5	136.7
7	5.8	3.9	67	55.7	37.2	27	105.6	70.6	87	155.5	103.9	47	205 4	137.2
8	6.7	4.4	68	56.5	37.8	28	106.4	71.1	88	156.3	104.4	48	206.2	137.8
9	7.5	5.0	69	57.4	38.3	29	107.3	71.7	89	157.1	105.0	49	207.0	138.3
10	8.3	5.6	70	58.2	38.9	30	108.1	72.2	90	158.0	105.6	50	207.9	138.9
11	9.1	6.1	71	59.0	39.4	131	108.9	72.8	191	158.8	106.1	251	208.7	139.4
12	10.0	6.7	72	59.9	40.0	32	109.8	73.3	92	159.6	106.7	52	209.5	140.0
13	10.8	7.2	73	60.7	40.6	33	110.6	73.9	93	160.5	107.2	53	210.4	140.6
14	11.6	7.8	74	61.5	41.1	34	111.4	74.4	94	161.3	107.8	54	211.2	141.1
15	12.5	8.3	75	62.4	41.7	35	112.2	75.0	95	162.1	108.3	55	212.0	141.7
16	13.3	8.9	76	63.2	42.2	36	113.1	75.6	96	163.0	108.9	56	212.9	142.2
17	14.1	9.4	77	64.0	42.8	37	113.9	76.1	97	163.8	109.4	57	213.7	142.8
18	15.0	10.0	78	64.9	43.3	38	114.7	76.7	98	164.6	110.0	58	214.5	143.3
19	15.8	10.6	79	65.7	43.9	39	115.6	77.2	99	165.5	110.6	59	215.4	143.9
20	16.6	11.1	80	66.5	44.4	40	116.4	77.8	200	166.3	111.1	60	216.2	144.4
21	17.5	11.7	81	67.3	45.0	141	117.2	78.3	201	167.1	111.7	261	217.0	145.0
22	18.3	12.2	82	68.2	45.6	42	118.1	78.9	02	168.0	112.2	62	217.8	145.6
23	19.1	12.8	83	69.0	46.1	43	118.9	79.4	03	168.8	112.8	63	218.7	146.1
24	20.0	13.3	84	69.8	46.7	44	119.7	80.0	04	169.6	113.3	64	219.5	146.7
25	20.8	13.9	85	70.7	47.2	45	120.6	80.6	05	170.5	113.9	65	220.3	147.2
26	21.6	14.4	86	71.5	47.8	46	121.4	81.1	06	171.3	114.4	66	221.2	147.8
27	22.4	15.0	87	72.3	48.3	47	122.2	81.7	07	172.1	115.0	67	222.0	148.3
28	23.3	15.6	88	73.2	48.9	48	123.1	82.2	08	172.9	115.6	68	222.8	148.9
29	24.1	16.1	89	74.0	49.4	49	123.9	82.8	09	173.8	116.1	69	223.7	149.4
30	24.9	16.7	90	74.8	50.0	50	124.7	83.3	10	174.6	116.7	70	224.5	150.0
31	25.8	17.2	91	75.7	50.6	151	125.6	83.9	211	175.4	117.2	271	225.3	150.6
32	26.6	17.8	92	76.5	51.1	52	126.4	84.4	12	176.3	117.8	72	226.2	151.1
33	27.4	18.3	93	77.3	51.7	53	127.2	85.0	13	177.1	118.3	73	227.0	151.7
34	28.3	18.9	94	78.2	52.2	54	128.0	85.6	14	177.9	118.9	74	227.8	152.2
35	29.1	19.4	95	79.0	52.8	55	128.9	86.1	15	178.8	119.4	75	228.7	152.8
36	29.9	20.0	96	79.8	53.3	56	129.7	86.7	16	179.6	120.0	76	229.5	153.3
37	30.8	20.6	97	80.7	53.9	57	130.5	87.2	17	180.4	120.6	77	230.3	153.9
38	31.6	21.1	98	81.5	54.4	58	131.4	87.8	18	181.3	121.1	78	231.1	154.4
39	32.4	21.7	99	82.3	55.0	59	132.2	88.3	19	182.1	121.7	79	232.0	155.0
40	33.3	22.2	100	83.1	55.6	60	133.0	88.9	20	182.9	122.2	80	232.8	155.6
41	34.1	22.8	101	84.0	56.1	161	133.9	89.4	221	183.8	122.8	281	233.6	156.1
42	34.9	23.3	02	84.8	56.7	62	134.7	90.0	22	184.6	123.3	82	234.5	156.7
43	35.8	23.9	03	85.6	57.2	63	135.5	90.6	23	185.4	123.9	83	235.3	157.2
44	36.6	24.4	04	86.5	57.8	64	136.4	91.1	24	186.2	124.4	84	236.1	157.8
45	37.4	25.0	05	87.3	58.3	65	137.2	91.7	25	187.1	125.0	85	237.0	158.3
46	38.2	25.6	06	88.1	58.9	66	138.0	92.2	26	187.9	125.6	86	237.8	158.9
47	39.1	26.1	07	89.0	59.4	67	138.9	92.8	27	188.7	126.1	87	238.6	159.4
48	39.9	26.7	08	89.8	60.0	68	139.7	93.3	28	189.6	126.7	88	239.5	160.0
49	40.7	27.2	09	90.6	60.6	69	140.5	93.9	29	190.4	127.2	89	240.3	160.6
50	41.6	27.8	10	91.5	61.1	70	141.3	94.4	30	191.2	127.8	90	241.1	161.1
51	42.4	28.3	111	92.3	61.7	171	142.2	95.0	231	192.1	128.3	291	242.0	161.7
52	43.2	28.9	12	93.1	62.2	72	143.0	95.6	32	192.9	128.9	92	242.8	162.2
53	44.1	29.4	13	94.0	62.8	73	143.8	96.1	33	193.7	129.4	93	243.6	162.8
54	44.9	30.0	14	94.8	63.3	74	144.7	96.7	34	194.6	130.0	94	244.5	163.3
55	45.7	30.6	15	95.6	63.9	75	145.5	97.2	35	195.4	130.6	95	245.3	163.9
56	46.6	31.1	16	96.5	64.4	76	146.3	97.8	36	196.2	131.1	96	246.1	164.4
57	47.4	31.7	17	97.3	65.0	77	147.2	98.3	37	197.1	131.7	97	246.9	165.0
58	48.2	32.2	18	98.1	65.6	78	148.0	98.9	38	197.9	132.2	98	247.8	165.6
59	49.1	32.8	19	98.9	66.1	79	148.8	99.4	39	198.7	132.8	99	248.6	166.1
60	49.9	33.3	20	99.8	66.7	80	149.7	100.0	40	199.6	133.3	300	249.4	166.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

NE. by E. SE. by E. NW. by W. SW. by W. [For 5 Points.

TABLE 1.

Difference of Latitude and Departure for 3¼ Points.

NE. ¾ N.			NW. ¾ N.			SE. ¾ S.			SW. ¾ S.					
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	49.0	36.3	121	97.2	72.1	181	145.4	107.8	241	193.6	143.6
2	1.6	1.2	62	49.8	36.9	22	98.0	72.7	82	146.2	108.4	42	194.4	144.2
3	2.4	1.8	63	50.6	37.5	23	98.8	73.3	83	147.0	109.0	43	195.2	144.8
4	3.2	2.4	64	51.4	38.1	24	99.6	73.9	84	147.8	109.6	44	196.0	145.4
5	4.0	3.0	65	52.2	38.7	25	100.4	74.5	85	148.6	110.2	45	196.8	145.9
6	4.8	3.6	66	53.0	39.3	26	101.2	75.1	86	149.4	110.8	46	197.6	146.5
7	5.6	4.2	67	53.8	39.9	27	102.0	75.7	87	150.2	111.4	47	198.4	147.1
8	6.4	4.8	68	54.6	40.5	28	102.8	76.2	88	151.0	112.0	48	199.2	147.7
9	7.2	5.4	69	55.4	41.1	29	103.6	76.8	89	151.8	112.6	49	200.0	148.3
10	8.0	6.0	70	56.2	41.7	30	104.4	77.4	90	152.6	113.2	50	200.8	148.9
11	8.8	6.6	71	57.0	42.3	131	105.2	78.0	191	153.4	113.8	251	201.6	149.5
12	9.6	7.1	72	57.8	42.9	32	106.0	78.6	92	154.2	114.4	52	202.4	150.1
13	10.4	7.7	73	58.6	43.5	33	106.8	79.2	93	155.0	115.0	53	203.2	150.7
14	11.2	8.3	74	59.4	44.1	34	107.6	79.8	94	155.8	115.6	54	204.0	151.3
15	12.0	8.9	75	60.2	44.7	35	108.4	80.4	95	156.6	116.2	55	204.8	151.9
16	12.9	9.5	76	61.0	45.3	36	109.2	81.0	96	157.4	116.8	56	205.6	152.5
17	13.7	10.1	77	61.8	45.9	37	110.0	81.6	97	158.2	117.4	57	206.4	153.1
18	14.5	10.7	78	62.7	46.5	38	110.8	82.2	98	159.0	117.9	58	207.2	153.7
19	15.3	11.3	79	63.5	47.1	39	111.6	82.8	99	159.8	118.5	59	208.0	154.3
20	16.1	11.9	80	64.3	47.7	40	112.4	83.4	200	160.6	119.1	60	208.8	154.9
21	16.9	12.5	81	65.1	48.3	141	113.3	84.0	201	161.4	119.7	261	209.6	155.5
22	17.7	13.1	82	65.9	48.8	42	114.1	84.6	02	162.2	120.3	62	210.4	156.1
23	18.5	13.7	83	66.7	49.4	43	114.9	85.2	03	163.1	120.9	63	211.2	156.7
24	19.3	14.3	84	67.5	50.0	44	115.7	85.8	04	163.9	121.5	64	212.0	157.3
25	20.1	14.9	85	68.3	50.6	45	116.5	86.4	05	164.7	122.1	65	212.8	157.9
26	20.9	15.5	86	69.1	51.2	46	117.3	87.0	06	165.5	122.7	66	213.7	158.5
27	21.7	16.1	87	69.9	51.8	47	118.1	87.6	07	166.3	123.3	67	214.5	159.1
28	22.5	16.7	88	70.7	52.4	48	118.9	88.2	08	167.1	123.9	68	215.3	159.6
29	23.3	17.3	89	71.5	53.0	49	119.7	88.8	09	167.9	124.5	69	216.1	160.2
30	24.1	17.9	90	72.3	53.6	50	120.5	89.4	10	168.7	125.1	70	216.9	160.8
31	24.9	18.5	91	73.1	54.2	151	121.3	90.0	211	169.5	125.7	271	217.7	161.4
32	25.7	19.1	92	73.9	54.8	52	122.1	90.5	12	170.3	126.3	72	218.5	162.0
33	26.5	19.7	93	74.7	55.4	53	122.9	91.1	13	171.1	126.9	73	219.3	162.6
34	27.3	20.3	94	75.5	56.0	54	123.7	91.7	14	171.9	127.5	74	220.1	163.2
35	28.1	20.8	95	76.3	56.6	55	124.5	92.3	15	172.7	128.1	75	220.9	163.8
36	28.9	21.4	96	77.1	57.2	56	125.3	92.9	16	173.5	128.7	76	221.7	164.4
37	29.7	22.0	97	77.9	57.8	57	126.1	93.5	17	174.3	129.3	77	222.5	165.0
38	30.5	22.6	98	78.7	58.4	58	126.9	94.1	18	175.1	129.9	78	223.3	165.6
39	31.3	23.2	99	79.5	59.0	59	127.7	94.7	19	175.9	130.5	79	224.1	166.2
40	32.1	23.8	100	80.3	59.6	60	128.5	95.3	20	176.7	131.1	80	224.9	166.8
41	32.9	24.4	101	81.1	60.2	161	129.3	95.9	221	177.5	131.6	281	225.7	167.4
42	33.7	25.0	02	81.9	60.8	62	130.1	96.5	22	178.3	132.2	82	226.5	168.0
43	34.5	25.6	03	82.7	61.4	63	130.9	97.1	23	179.1	132.8	83	227.3	168.6
44	35.3	26.2	04	83.5	62.0	64	131.7	97.7	24	179.9	133.4	84	228.1	169.2
45	36.1	26.8	05	84.3	62.5	65	132.5	98.3	25	180.7	134.0	85	228.9	169.8
46	36.9	27.4	06	85.1	63.1	66	133.3	98.9	26	181.5	134.6	86	229.7	170.4
47	37.8	28.0	07	85.9	63.7	67	134.1	99.5	27	182.3	135.2	87	230.5	171.0
48	38.6	28.6	08	86.7	64.3	68	134.9	100.1	28	183.1	135.8	88	231.3	171.6
49	39.4	29.2	09	87.5	64.9	69	135.7	100.7	29	183.9	136.4	89	232.1	172.2
50	40.2	29.8	10	88.4	65.5	70	136.5	101.3	30	184.7	137.0	90	232.9	172.8
51	41.0	30.4	111	89.2	66.1	171	137.3	101.9	231	185.5	137.6	291	233.7	173.3
52	41.8	31.0	12	90.0	66.7	72	138.2	102.5	32	186.3	138.2	92	234.5	173.9
53	42.6	31.6	13	90.8	67.3	73	139.0	103.1	33	187.1	138.8	93	235.3	174.5
54	43.4	32.2	14	91.6	67.9	74	139.8	103.7	34	188.0	139.4	94	236.1	175.1
55	44.2	32.8	15	92.4	68.5	75	140.6	104.2	35	188.8	140.0	95	236.9	175.7
56	45.0	33.4	16	93.2	69.1	76	141.4	104.8	36	189.6	140.6	96	237.7	176.3
57	45.8	34.0	17	94.0	69.7	77	142.2	105.4	37	190.4	141.2	97	238.6	176.9
58	46.6	34.6	18	94.8	70.3	78	143.0	106.0	38	191.2	141.8	98	239.4	177.5
59	47.4	35.1	19	95.6	70.9	79	143.8	106.6	39	192.0	142.4	99	240.2	178.1
60	48.2	35.7	20	96.4	71.5	80	144.6	107.2	40	192.8	143.0	300	241.0	178.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
NE. ¾ E.			SE. ¾ E.			NW. ¾ W.			SW. ¾ W.			[For 4¾ Points.		

TABLE 1.

Difference of Latitude and Departure for 3½ Points.

NE. ½ N. NW. ½ N. SE. ½ S. SW. ½ S.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	47.2	38.7	121	93.5	76.8	181	139.9	114.8	241	186.3	152.9
2	1.5	1.3	62	47.9	39.3	22	94.3	77.4	82	140.7	115.5	42	187.1	153.5
3	2.3	1.9	63	48.7	40.0	23	95.1	78.0	83	141.5	116.1	43	187.8	154.2
4	3.1	2.5	64	49.5	40.6	24	95.9	78.7	84	142.2	116.7	44	188.6	154.8
5	3.9	3.2	65	50.2	41.2	25	96.6	79.3	85	143.0	117.4	45	189.4	155.4
6	4.6	3.8	66	51.0	41.9	26	97.4	79.9	86	143.8	118.0	46	190.2	156.1
7	5.4	4.4	67	51.8	42.5	27	98.2	80.6	87	144.6	118.6	47	190.9	156.7
8	6.2	5.1	68	52.6	43.1	28	98.9	81.2	88	145.3	119.3	48	191.7	157.3
9	7.0	5.7	69	53.3	43.8	29	99.7	81.8	89	146.1	119.9	49	192.5	158.0
10	7.7	6.3	70	54.1	44.4	30	100.5	82.5	90	146.9	120.5	50	193.3	158.6
11	8.5	7.0	71	54.9	45.0	131	101.3	83.1	191	147.6	121.2	251	194.0	159.2
12	9.3	7.6	72	55.7	45.7	32	102.0	83.7	92	148.4	121.8	52	194.8	159.9
13	10.0	8.2	73	56.4	46.3	33	102.8	84.4	93	149.2	122.4	53	195.6	160.5
14	10.8	8.9	74	57.2	46.9	34	103.6	85.0	94	150.0	123.1	54	196.3	161.1
15	11.6	9.5	75	58.0	47.6	35	104.4	85.6	95	150.7	123.7	55	197.1	161.8
16	12.4	10.2	76	58.7	48.2	36	105.1	86.3	96	151.5	124.3	56	197.9	162.4
17	13.1	10.8	77	59.5	48.8	37	105.9	86.9	97	152.3	125.0	57	198.7	163.0
18	13.9	11.4	78	60.3	49.5	38	106.7	87.5	98	153.1	125.6	58	199.4	163.7
19	14.7	12.1	79	61.1	50.1	39	107.4	88.2	99	153.8	126.2	59	200.2	164.3
20	15.5	12.7	80	61.8	50.8	40	108.2	88.8	200	154.6	126.9	60	201.0	164.9
21	16.2	13.3	81	62.6	51.4	141	109.0	89.4	201	155.4	127.5	261	201.8	165.6
22	17.0	14.0	82	63.4	52.0	42	109.8	90.1	02	156.1	128.1	62	202.5	166.2
23	17.8	14.6	83	64.2	52.7	43	110.5	90.7	03	156.9	128.8	63	203.3	166.8
24	18.6	15.2	84	64.9	53.3	44	111.3	91.4	04	157.7	129.4	64	204.1	167.5
25	19.3	15.9	85	65.7	53.9	45	112.1	92.0	05	158.5	130.1	65	204.8	168.1
26	20.1	16.5	86	66.5	54.6	46	112.9	92.6	06	159.2	130.7	66	205.6	168.7
27	20.9	17.1	87	67.3	55.2	47	113.6	93.3	07	160.0	131.3	67	206.4	169.4
28	21.6	17.8	88	68.0	55.8	48	114.4	93.9	08	160.8	132.0	68	207.2	170.0
29	22.4	18.4	89	68.8	56.5	49	115.2	94.5	09	161.6	132.6	69	207.9	170.7
30	23.2	19.0	90	69.6	57.1	50	116.0	95.2	10	162.3	133.2	70	208.7	171.3
31	24.0	19.7	91	70.3	57.7	151	116.7	95.8	211	163.1	133.9	271	209.5	171.9
32	24.7	20.3	92	71.1	58.4	52	117.5	96.4	12	163.9	134.5	72	210.3	172.6
33	25.5	20.9	93	71.9	59.0	53	118.3	97.1	13	164.7	135.1	73	211.0	173.2
34	26.3	21.6	94	72.7	59.6	54	119.0	97.7	14	165.4	135.8	74	211.8	173.8
35	27.1	22.2	95	73.4	60.3	55	119.8	98.3	15	166.2	136.4	75	212.6	174.5
36	27.8	22.8	96	74.2	60.9	56	120.6	99.0	16	167.0	137.0	76	213.4	175.1
37	28.6	23.5	97	75.0	61.5	57	121.4	99.6	17	167.7	137.7	77	214.1	175.7
38	29.4	24.1	98	75.8	62.2	58	122.1	100.2	18	168.5	138.3	78	214.9	176.4
39	30.1	24.7	99	76.5	62.8	59	122.9	100.9	19	169.3	138.9	79	215.7	177.0
40	30.9	25.4	100	77.3	63.4	60	123.7	101.5	20	170.1	139.6	80	216.4	177.6
41	31.7	26.0	101	78.1	64.1	161	124.5	102.1	221	170.8	140.2	281	217.2	178.3
42	32.5	26.6	02	78.8	64.7	62	125.2	102.8	22	171.6	140.8	82	218.0	178.9
43	33.2	27.3	03	79.6	65.3	63	126.0	103.4	23	172.4	141.5	83	218.8	179.5
44	34.0	27.9	04	80.4	66.0	64	126.8	104.0	24	173.2	142.1	84	219.5	180.2
45	34.8	28.5	05	81.2	66.6	65	127.5	104.7	25	173.9	142.7	85	220.3	180.8
46	35.6	29.2	06	81.9	67.2	66	128.3	105.3	26	174.7	143.4	86	221.1	181.4
47	36.3	29.8	07	82.7	67.9	67	129.1	105.9	27	175.5	144.0	87	221.9	182.1
48	37.1	30.5	08	83.5	68.5	68	129.9	106.6	28	176.2	144.6	88	222.6	182.7
49	37.9	31.1	09	84.3	69.1	69	130.6	107.2	29	177.0	145.3	89	223.4	183.3
50	38.7	31.7	10	85.0	69.8	70	131.4	107.8	30	177.8	145.9	90	224.2	184.0
51	39.4	32.4	111	85.8	70.4	171	132.2	108.5	231	178.6	146.5	291	224.9	184.6
52	40.2	33.0	12	86.6	71.1	72	133.0	109.1	32	179.3	147.2	92	225.7	185.2
53	41.0	33.6	13	87.4	71.7	73	133.7	109.8	33	180.1	147.8	93	226.5	185.9
54	41.7	34.3	14	88.1	72.3	74	134.5	110.4	34	180.9	148.4	94	227.3	186.5
55	42.5	34.9	15	88.9	73.0	75	135.3	111.0	35	181.7	149.1	95	228.0	187.1
56	43.3	35.5	16	89.7	73.6	76	136.0	111.7	36	182.4	149.7	96	228.8	187.8
57	44.1	36.2	17	90.4	74.2	77	136.8	112.3	37	183.2	150.4	97	229.6	188.4
58	44.8	36.8	18	91.2	74.9	78	137.6	112.9	38	184.0	151.0	98	230.4	189.0
59	45.6	37.4	19	92.0	75.5	79	138.4	113.6	39	184.7	151.6	99	231.1	189.7
60	46.4	38.1	20	92.8	76.1	80	139.1	114.2	40	185.5	152.3	300	231.9	190.3
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

NE. ½ E. SE. ½ E. NW. ½ W. SW. ½ W. [For 4½ Points.

TABLE 1.

Difference of Latitude and Departure for 3¾ Points.

NE. ¾ N.			NW. ¾ N.						SE. ¾ S.			SW. ¾ S.		
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.7	0.7	61	45.2	41.0	121	89.7	81.3	181	134.1	121.6	241	178.6	161.8
2	1.5	1.3	62	45.9	41.6	22	90.4	81.9	82	134.9	122.2	42	179.3	162.5
3	2.2	2.0	63	46.7	42.3	23	91.1	82.6	83	135.6	122.9	43	180.1	163.2
4	3.0	2.7	64	47.4	43.0	24	91.9	83.3	84	136.3	123.6	44	180.8	163.9
5	3.7	3.4	65	48.2	43.7	25	92.6	83.9	85	137.1	124.2	45	181.5	164.5
6	4.4	4.0	66	48.9	44.3	26	93.4	84.6	86	137.8	124.9	46	182.3	165.2
7	5.2	4.7	67	49.6	45.0	27	94.1	85.3	87	138.6	125.6	47	183.0	165.9
8	5.9	5.4	68	50.4	45.7	28	94.8	86.0	88	139.3	126.3	48	183.8	166.5
9	6.7	6.0	69	51.1	46.3	29	95.6	86.6	89	140.0	126.9	49	184.5	167.2
10	7.4	6.7	70	51.9	47.0	30	96.3	87.3	90	140.8	127.6	50	185.2	167.9
11	8.2	7.4	71	52.6	47.7	131	97.1	88.0	191	141.5	128.3	251	186.0	168.6
12	8.9	8.1	72	53.3	48.4	32	97.8	88.6	92	142.8	128.9	52	186.7	169.2
13	9.6	8.7	73	54.1	49.0	33	98.5	89.3	93	143.0	129.6	53	187.5	169.9
14	10.4	9.4	74	54.8	49.7	34	99.3	90.0	94	143.7	130.3	54	188.2	170.6
15	11.1	10.1	75	55.6	50.4	35	100.0	90.7	95	144.5	131.0	55	188.9	171.2
16	11.9	10.7	76	56.3	51.0	36	100.8	91.3	96	145.2	131.6	56	189.7	171.9
17	12.6	11.4	77	57.1	51.7	37	101.5	92.0	97	146.0	132.3	57	190.4	172.6
18	13.3	12.1	78	57.8	52.4	38	102.3	92.7	98	146.7	133.0	58	191.2	173.3
19	14.1	12.8	79	58.5	53.1	39	103.0	93.3	99	147.4	133.6	59	191.9	173.9
20	14.8	13.4	80	59.3	53.7	40	103.7	94.0	200	148.2	134.3	60	192.6	174.6
21	15.6	14.1	81	60.0	54.4	141	104.5	94.7	201	148.9	135.0	261	193.4	175.3
22	16.3	14.8	82	60.8	55.1	42	105.2	95.4	02	149.7	135.7	62	194.1	175.9
23	17.0	15.4	83	61.5	55.7	43	106.0	96.0	03	150.4	136.3	63	194.9	176.6
24	17.8	16.1	84	62.2	56.4	44	106.7	96.7	04	151.2	137.0	64	195.6	177.3
25	18.5	16.8	85	63.0	57.1	45	107.4	97.4	05	151.9	137.7	65	196.4	178.0
26	19.3	17.5	86	63.7	57.8	46	108.2	98.0	06	152.6	138.3	66	197.1	178.6
27	20.0	18.1	87	64.5	58.4	47	108.9	98.7	07	153.4	139.0	67	197.8	179.3
28	20.7	18.8	88	65.2	59.1	48	109.7	99.4	08	154.1	139.7	68	198.6	180.0
29	21.5	19.5	89	65.9	59.8	49	110.4	100.1	09	154.9	140.4	69	199.3	180.6
30	22.2	20.1	90	66.7	60.4	50	111.1	100.7	10	155.6	141.0	70	200.1	181.3
31	23.0	20.8	91	67.4	61.1	151	111.9	101.4	211	156.3	141.7	271	200.8	182.0
32	23.7	21.5	92	68.2	61.8	52	112.6	102.1	12	157.1	142.4	72	201.5	182.7
33	24.5	22.2	93	68.9	62.5	53	113.4	102.7	13	157.8	143.0	73	202.3	183.3
34	25.2	22.8	94	69.6	63.1	54	114.1	103.4	14	158.6	143.7	74	203.0	184.0
35	25.9	23.5	95	70.4	63.8	55	114.8	104.1	15	159.3	144.4	75	203.8	184.7
36	26.7	24.2	96	71.1	64.5	56	115.6	104.8	16	160.0	145.1	76	204.5	185.4
37	27.4	24.8	97	71.9	65.1	57	116.3	105.4	17	160.8	145.7	77	205.2	186.0
38	28.2	25.5	98	72.6	65.8	58	117.1	106.1	18	161.5	146.4	78	206.0	186.7
39	28.9	26.2	99	73.4	66.5	59	117.8	106.8	19	162.3	147.1	79	206.7	187.4
40	29.6	26.9	100	74.1	67.2	60	118.6	107.4	20	163.0	147.7	80	207.5	188.0
41	30.4	27.5	101	74.8	67.8	161	119.3	108.1	221	163.8	148.4	281	208.2	188.7
42	31.1	28.2	02	75.6	68.5	62	120.0	108.8	22	164.5	149.1	82	208.9	189.4
43	31.9	28.9	03	76.3	69.2	63	120.8	109.5	23	165.2	149.8	83	209.7	190.1
44	32.6	29.5	04	77.1	69.8	64	121.5	110.1	24	166.0	150.4	84	210.4	190.7
45	33.3	30.2	05	77.8	70.5	65	122.3	110.8	25	166.7	151.1	85	211.2	191.4
46	34.1	30.9	06	78.5	71.2	66	123.0	111.5	26	167.5	151.8	86	211.9	192.1
47	34.8	31.6	07	79.3	71.9	67	123.7	112.2	27	168.2	152.4	87	212.7	192.7
48	35.6	32.2	08	80.0	72.5	68	124.5	112.8	28	168.9	153.1	88	213.4	193.4
49	36.3	32.9	09	80.8	73.2	69	125.2	113.5	29	169.7	153.8	89	214.1	194.1
50	37.0	33.6	10	81.5	73.9	70	126.0	114.2	30	170.4	154.5	90	214.9	194.8
51	37.8	34.2	111	82.2	74.5	171	126.7	114.8	231	171.2	155.1	291	215.6	195.4
52	38.5	34.9	12	83.0	75.2	72	127.4	115.5	32	171.9	155.8	92	216.4	196.1
53	39.3	35.6	13	83.7	75.9	73	128.2	116.2	33	172.6	156.5	93	217.1	196.8
54	40.0	36.3	14	84.5	76.6	74	128.9	116.9	34	173.4	157.1	94	217.8	197.4
55	40.8	36.9	15	85.2	77.2	75	129.7	117.5	35	174.1	157.8	95	218.6	198.1
56	41.5	37.6	16	86.0	77.9	76	130.4	118.2	36	174.9	158.5	96	219.3	198.8
57	42.2	38.3	17	86.7	78.6	77	131.1	118.9	37	175.6	159.2	97	220.1	199.5
58	43.0	39.0	18	87.4	79.2	78	131.9	119.5	38	176.3	159.8	98	220.8	200.1
59	43.7	39.6	19	88.2	79.9	79	132.6	120.2	39	177.1	160.5	99	221.5	200.8
60	44.5	40.3	20	88.9	80.6	80	133.4	120.9	40	177.8	161.2	300	222.3	201.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
NE. ¼ E.			SE. ¼ E.			NW. ¼ W.			SW. ¼ W.			[For 4¼ Points.		

TABLE 1.

Difference of Latitude and Departure for 4 Points.

NE. NW. SE. SW.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.7	0.7	61	43.1	43.1	121	85.6	85.6	181	128.0	128.0	241	170.4	170.4
2	1.4	1.4	62	43.8	43.8	22	86.3	86.3	82	128.7	128.7	42	171.1	171.1
3	2.1	2.1	63	44.5	44.5	23	87.0	87.0	83	129.4	129.4	43	171.8	171.8
4	2.8	2.8	64	45.3	45.3	24	87.7	87.7	84	130.1	130.1	44	172.5	172.5
5	3.5	3.5	65	46.0	46.0	25	88.4	88.4	85	130.8	130.8	45	173.2	173.2
6	4.2	4.2	66	46.7	46.7	26	89.1	89.1	86	131.5	131.5	46	173.9	173.9
7	4.9	4.9	67	47.4	47.4	27	89.8	89.8	87	132.2	132.2	47	174.7	174.7
8	5.7	5.7	68	48.1	48.1	28	90.5	90.5	88	132.9	132.9	48	175.4	175.4
9	6.4	6.4	69	48.8	48.8	29	91.2	91.2	89	133.6	133.6	49	176.1	176.1
10	7.1	7.1	70	49.5	49.5	30	91.9	91.9	90	134.4	134.4	50	176.8	176.8
11	7.8	7.8	71	50.2	50.2	131	92.6	92.6	191	135.1	135.1	251	177.5	177.5
12	8.5	8.5	72	50.9	50.9	32	93.3	93.3	92	135.8	135.8	52	178.2	178.2
13	9.2	9.2	73	51.6	51.6	33	94.0	94.0	93	136.5	136.5	53	178.9	178.9
14	9.9	9.9	74	52.3	52.3	34	94.8	94.8	94	137.2	137.2	54	179.6	179.6
15	10.6	10.6	75	53.0	53.0	35	95.5	95.5	95	137.9	137.9	55	180.3	180.3
16	11.3	11.3	76	53.7	53.7	36	96.2	96.2	96	138.6	138.6	56	181.0	181.0
17	12.0	12.0	77	54.4	54.4	37	96.9	96.9	97	139.3	139.3	57	181.7	181.7
18	12.7	12.7	78	55.2	55.2	38	97.6	97.6	98	140.0	140.0	58	182.4	182.4
19	13.4	13.4	79	55.9	55.9	39	98.3	98.3	99	140.7	140.7	59	183.1	183.1
20	14.1	14.1	80	56.6	56.6	40	99.0	99.0	200	141.4	141.4	60	183.8	183.8
21	14.8	14.8	81	57.3	57.3	141	99.7	99.7	201	142.1	142.1	261	184.6	184.6
22	15.6	15.6	82	58.0	58.0	42	100.4	100.4	02	142.8	142.8	62	185.3	185.3
23	16.3	16.3	83	58.7	58.7	43	101.1	101.1	03	143.5	143.5	63	186.0	186.0
24	17.0	17.0	84	59.4	59.4	44	101.8	101.8	04	144.2	144.2	64	186.7	186.7
25	17.7	17.7	85	60.1	60.1	45	102.5	102.5	05	145.0	145.0	65	187.4	187.4
26	18.4	18.4	86	60.8	60.8	46	103.2	103.2	06	145.7	145.7	66	188.1	188.1
27	19.1	19.1	87	61.5	61.5	47	103.9	103.9	07	146.4	146.4	67	188.8	188.8
28	19.8	19.8	88	62.2	62.2	48	104.7	104.7	08	147.1	147.1	68	189.5	189.5
29	20.5	20.5	89	62.9	62.9	49	105.4	105.4	09	147.8	147.8	69	190.2	190.2
30	21.2	21.2	90	63.6	63.6	50	106.1	106.1	10	148.5	148.5	70	190.9	190.9
31	21.9	21.9	91	64.3	64.3	151	106.8	106.8	211	149.2	149.2	271	191.6	191.6
32	22.6	22.6	92	65.1	65.1	52	107.5	107.5	12	149.9	149.9	72	192.3	192.3
33	23.3	23.3	93	65.8	65.8	53	108.2	108.2	13	150.6	150.6	73	193.0	193.0
34	24.0	24.0	94	66.5	66.5	54	108.9	108.9	14	151.3	151.3	74	193.7	193.7
35	24.7	24.7	95	67.2	67.2	55	109.6	109.6	15	152.0	152.0	75	194.5	194.5
36	25.5	25.5	96	67.9	67.9	56	110.3	110.3	16	152.7	152.7	76	195.2	195.2
37	26.2	26.2	97	68.6	68.6	57	111.0	111.0	17	153.4	153.4	77	195.9	195.9
38	26.9	26.9	98	69.3	69.3	58	111.7	111.7	18	154.1	154.1	78	196.6	196.6
39	27.6	27.6	99	70.0	70.0	59	112.4	112.4	19	154.9	154.9	79	197.3	197.3
40	28.3	28.3	100	70.7	70.7	60	113.1	113.1	20	155.6	155.6	80	198.0	198.0
41	29.0	29.0	101	71.4	71.4	161	113.8	113.8	221	156.3	156.3	281	198.7	198.7
42	29.7	29.7	02	72.1	72.1	62	114.6	114.6	22	157.0	157.0	82	199.4	199.4
43	30.4	30.4	03	72.8	72.8	63	115.3	115.3	23	157.7	157.7	83	200.1	200.1
44	31.1	31.1	04	73.5	73.5	64	116.0	116.0	24	158.4	158.4	84	200.8	200.8
45	31.8	31.8	05	74.2	74.2	65	116.7	116.7	25	159.1	159.1	85	201.5	201.5
46	32.5	32.5	06	75.0	75.0	66	117.4	117.4	26	159.8	159.8	86	202.2	202.2
47	33.2	33.2	07	75.7	75.7	67	118.1	118.1	27	160.5	160.5	87	202.9	202.9
48	33.9	33.9	08	76.4	76.4	68	118.8	118.8	28	161.2	161.2	88	203.6	203.6
49	34.6	34.6	09	77.1	77.1	69	119.5	119.5	29	161.9	161.9	89	204.4	204.4
50	35.4	35.4	10	77.8	77.8	70	120.2	120.2	30	162.6	162.6	90	205.1	205.1
51	36.1	36.1	111	78.5	78.5	171	120.9	120.9	231	163.3	163.3	291	205.8	205.8
52	36.8	36.8	12	79.2	79.2	72	121.6	121.6	32	164.0	164.0	92	206.5	206.5
53	37.5	37.5	13	79.9	79.9	73	122.3	122.3	33	164.8	164.8	93	207.2	207.2
54	38.2	38.2	14	80.6	80.6	74	123.0	123.0	34	165.5	165.5	94	207.9	207.9
55	38.9	38.9	15	81.3	81.3	75	123.7	123.7	35	166.2	166.2	95	208.6	208.6
56	39.6	39.6	16	82.0	82.0	76	124.5	124.5	36	166.9	166.9	96	209.3	209.3
57	40.3	40.3	17	82.7	82.7	77	125.2	125.2	37	167.6	167.6	97	210.0	210.0
58	41.0	41.0	18	83.4	83.4	78	125.9	125.9	38	168.3	168.3	98	210.7	210.7
59	41.7	41.7	19	84.1	84.1	79	126.6	126.6	39	169.0	169.0	99	211.4	211.4
60	42.4	42.4	20	84.9	84.9	80	127.3	127.3	40	169.7	169.7	300	212.1	212.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

NE. NW. SE. SW. [For 4 Points.

TABLE 2.

Difference of Latitude and Departure for 1° (179°, 181°, 359°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.0	61	61.0	1.1	121	121.0	2.1	181	181.0	3.2	241	241.0	4.2
2	2.0	0.0	62	62.0	1.1	22	122.0	2.1	82	182.0	3.2	42	242.0	4.2
3	3.0	0.1	63	63.0	1.1	23	123.0	2.1	83	183.0	3.2	43	243.0	4.2
4	4.0	0.1	64	64.0	1.1	24	124.0	2.2	84	184.0	3.2	44	244.0	4.3
5	5.0	0.1	65	65.0	1.1	25	125.0	2.2	85	185.0	3.2	45	245.0	4.3
6	6.0	0.1	66	66.0	1.2	26	126.0	2.2	86	186.0	3.2	46	246.0	4.3
7	7.0	0.1	67	67.0	1.2	27	127.0	2.2	87	187.0	3.3	47	247.0	4.3
8	8.0	0.1	68	68.0	1.2	28	128.0	2.2	88	188.0	3.3	48	248.0	4.3
9	9.0	0.2	69	69.0	1.2	29	129.0	2.3	89	189.0	3.3	49	249.0	4.3
10	10.0	0.2	70	70.0	1.2	30	130.0	2.3	90	190.0	3.3	50	250.0	4.4
11	11.0	0.2	71	71.0	1.2	131	131.0	2.3	191	191.0	3.3	251	251.0	4.4
12	12.0	0.2	72	72.0	1.3	32	132.0	2.3	92	192.0	3.4	52	252.0	4.4
13	13.0	0.2	73	73.0	1.3	33	133.0	2.3	93	193.0	3.4	53	253.0	4.4
14	14.0	0.2	74	74.0	1.3	34	134.0	2.3	94	194.0	3.4	54	254.0	4.4
15	15.0	0.3	75	75.0	1.3	35	135.0	2.4	95	195.0	3.4	55	255.0	4.5
16	16.0	0.3	76	76.0	1.3	36	136.0	2.4	96	196.0	3.4	56	256.0	4.5
17	17.0	0.3	77	77.0	1.3	37	137.0	2.4	97	197.0	3.4	57	257.0	4.5
18	18.0	0.3	78	78.0	1.4	38	138.0	2.4	98	198.0	3.5	58	258.0	4.5
19	19.0	0.3	79	79.0	1.4	39	139.0	2.4	99	199.0	3.5	59	259.0	4.5
20	20.0	0.3	80	80.0	1.4	40	140.0	2.4	200	200.0	3.5	60	260.0	4.5
21	21.0	0.4	81	81.0	1.4	141	141.0	2.5	201	201.0	3.5	261	261.0	4.6
22	22.0	0.4	82	82.0	1.4	42	142.0	2.5	02	202.0	3.5	62	262.0	4.6
23	23.0	0.4	83	83.0	1.4	43	143.0	2.5	03	203.0	3.5	63	263.0	4.6
24	24.0	0.4	84	84.0	1.5	44	144.0	2.5	04	204.0	3.6	64	264.0	4.6
25	25.0	0.4	85	85.0	1.5	45	145.0	2.5	05	205.0	3.6	65	265.0	4.6
26	26.0	0.5	86	86.0	1.5	46	146.0	2.5	06	206.0	3.6	66	266.0	4.6
27	27.0	0.5	87	87.0	1.5	47	147.0	2.6	07	207.0	3.6	67	267.0	4.7
28	28.0	0.5	88	88.0	1.5	48	148.0	2.6	08	208.0	3.6	68	268.0	4.7
29	29.0	0.5	89	89.0	1.6	49	149.0	2.6	09	209.0	3.6	69	269.0	4.7
30	30.0	0.5	90	90.0	1.6	50	150.0	2.6	10	210.0	3.7	70	270.0	4.7
31	31.0	0.5	91	91.0	1.6	151	151.0	2.6	211	211.0	3.7	271	271.0	4.7
32	32.0	0.6	92	92.0	1.6	52	152.0	2.7	12	212.0	3.7	72	272.0	4.7
33	33.0	0.6	93	93.0	1.6	53	153.0	2.7	13	213.0	3.7	73	273.0	4.8
34	34.0	0.6	94	94.0	1.6	54	154.0	2.7	14	214.0	3.7	74	274.0	4.8
35	35.0	0.6	95	95.0	1.7	55	155.0	2.7	15	215.0	3.8	75	275.0	4.8
36	36.0	0.6	96	96.0	1.7	56	156.0	2.7	16	216.0	3.8	76	276.0	4.8
37	37.0	0.6	97	97.0	1.7	57	157.0	2.7	17	217.0	3.8	77	277.0	4.8
38	38.0	0.7	98	98.0	1.7	58	158.0	2.8	18	218.0	3.8	78	278.0	4.9
39	39.0	0.7	99	99.0	1.7	59	159.0	2.8	19	219.0	3.8	79	279.0	4.9
40	40.0	0.7	100	100.0	1.7	60	160.0	2.8	20	220.0	3.8	80	280.0	4.9
41	41.0	0.7	101	101.0	1.8	161	161.0	2.8	221	221.0	3.9	281	281.0	4.9
42	42.0	0.7	02	102.0	1.8	62	162.0	2.8	22	222.0	3.9	82	282.0	4.9
43	43.0	0.8	03	103.0	1.8	63	163.0	2.8	23	223.0	3.9	83	283.0	4.9
44	44.0	0.8	04	104.0	1.8	64	164.0	2.9	24	224.0	3.9	84	284.0	5.0
45	45.0	0.8	05	105.0	1.8	65	165.0	2.9	25	225.0	3.9	85	285.0	5.0
46	46.0	0.8	06	106.0	1.8	66	166.0	2.9	26	226.0	3.9	86	286.0	5.0
47	47.0	0.8	07	107.0	1.9	67	167.0	2.9	27	227.0	4.0	87	287.0	5.0
48	48.0	0.8	08	108.0	1.9	68	168.0	2.9	28	228.0	4.0	88	288.0	5.0
49	49.0	0.9	09	109.0	1.9	69	169.0	2.9	29	229.0	4.0	89	289.0	5.0
50	50.0	0.9	10	110.0	1.9	70	170.0	3.0	30	230.0	4.0	90	290.0	5.1
51	51.0	0.9	111	111.0	1.9	171	171.0	3.0	231	231.0	4.0	291	291.0	5.1
52	52.0	0.9	12	112.0	2.0	72	172.0	3.0	32	232.0	4.0	92	292.0	5.1
53	53.0	0.9	13	113.0	2.0	73	173.0	3.0	33	233.0	4.1	93	293.0	5.1
54	54.0	0.9	14	114.0	2.0	74	174.0	3.0	34	234.0	4.1	94	294.0	5.1
55	55.0	1.0	15	115.0	2.0	75	175.0	3.1	35	235.0	4.1	95	295.0	5.1
56	56.0	1.0	16	116.0	2.0	76	176.0	3.1	36	236.0	4.1	96	296.0	5.2
57	57.0	1.0	17	117.0	2.0	77	177.0	3.1	37	237.0	4.1	97	297.0	5.2
58	58.0	1.0	18	118.0	2.1	78	178.0	3.1	38	238.0	4.2	98	298.0	5.2
59	59.0	1.0	19	119.0	2.1	79	179.0	3.1	39	239.0	4.2	99	299.0	5.2
60	60.0	1.0	20	120.0	2.1	80	180.0	3.1	40	240.0	4.2	300	300.0	5.2
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

89° (91°, 269°, 271°).

TABLE 2.

Difference of Latitude and Departure for 1° (179°, 181°, 359°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	301.0	5.3	361	360.9	6.3	421	420.9	7.3	481	480.9	8.4	541	540.9	9.5
02	302.0	5.3	62	361.9	6.3	22	421.9	7.4	82	481.9	8.4	42	541.9	9.5
03	303.0	5.3	63	362.9	6.3	23	422.9	7.4	83	482.9	8.5	43	542.9	9.5
04	304.0	5.3	64	363.9	6.4	24	423.9	7.4	84	483.9	8.5	44	543.9	9.5
05	305.0	5.3	65	364.9	6.4	25	424.9	7.4	85	484.9	8.5	45	544.9	9.5
06	306.0	5.3	66	365.9	6.4	26	425.9	7.4	86	485.9	8.5	46	545.9	9.5
07	307.0	5.4	67	366.9	6.4	27	426.9	7.4	87	486.9	8.5	47	546.9	9.6
08	308.0	5.4	68	367.9	6.4	28	427.9	7.5	88	487.9	8.6	48	547.9	9.6
09	309.0	5.4	69	368.9	6.4	29	428.9	7.5	89	488.9	8.6	49	548.9	9.6
10	310.0	5.4	70	369.9	6.5	30	429.9	7.5	90	489.9	8.6	50	549.9	9.6
311	311.0	5.4	371	370.9	6.5	431	430.9	7.5	491	490.9	8.6	551	550.9	9.6
12	312.0	5.4	72	371.9	6.5	32	431.9	7.5	92	491.9	8.6	52	551.9	9.6
13	313.0	5.5	73	372.9	6.5	33	432.9	7.5	93	492.9	8.7	53	552.9	9.7
14	314.0	5.5	74	373.9	6.5	34	433.9	7.6	94	493.9	8.7	54	553.9	9.7
15	315.0	5.5	75	374.9	6.5	35	434.9	7.6	95	494.9	8.7	55	554.9	9.7
16	316.0	5.5	76	375.9	6.6	36	435.9	7.6	96	495.9	8.7	56	555.9	9.7
17	317.0	5.5	77	376.9	6.6	37	436.9	7.6	97	496.9	8.7	57	556.9	9.7
18	318.0	5.5	78	377.9	6.6	38	437.9	7.6	98	497.9	8.7	58	557.9	9.7
19	319.0	5.6	79	378.9	6.6	39	438.9	7.7	99	498.9	8.8	59	558.9	9.8
20	320.0	5.6	80	379.9	6.6	40	439.9	7.7	500	499.9	8.8	60	559.9	9.8
321	321.0	5.6	381	380.9	6.7	441	440.9	7.7	501	500.9	8.8	561	560.9	9.8
22	322.0	5.6	82	381.9	6.7	42	441.9	7.7	02	501.9	8.8	62	561.9	9.8
23	323.0	5.6	83	382.9	6.7	43	442.9	7.7	03	502.9	8.8	63	562.9	9.8
24	324.0	5.6	84	383.9	6.7	44	443.9	7.7	04	503.9	8.8	64	563.9	9.8
25	325.0	5.7	85	384.9	6.7	45	444.9	7.8	05	504.9	8.8	65	564.9	9.9
26	326.0	5.7	86	385.9	6.7	46	445.9	7.8	06	505.9	8.9	66	565.9	9.9
27	327.0	5.7	87	386.9	6.8	47	446.9	7.8	07	506.9	8.9	67	566.9	9.9
28	328.0	5.7	88	387.9	6.8	48	447.9	7.8	08	507.9	8.9	68	567.9	9.9
29	329.0	5.7	89	388.9	6.8	49	448.9	7.8	09	508.9	8.9	69	568.9	9.9
30	330.0	5.8	90	389.9	6.8	50	449.9	7.8	10	509.9	8.9	70	569.9	9.9
331	331.0	5.8	391	390.9	6.8	451	450.9	7.9	511	510.9	9.0	571	570.9	10.0
32	332.0	5.8	92	391.9	6.8	52	451.9	7.9	12	511.9	9.0	72	571.9	10.0
33	333.0	5.8	93	392.9	6.9	53	452.9	7.9	13	512.9	9.0	73	572.9	10.0
34	333.9	5.8	94	393.9	6.9	54	453.9	7.9	14	513.9	9.0	74	573.9	10.0
35	334.9	5.8	95	394.9	6.9	55	454.9	7.9	15	514.9	9.0	75	574.9	10.0
36	335.9	5.9	96	395.9	6.9	56	455.9	8.0	16	515.9	9.0	76	575.9	10.0
37	336.9	5.9	97	396.9	6.9	57	456.9	8.0	17	516.9	9.1	77	576.9	10.1
38	337.9	5.9	98	397.9	6.9	58	457.9	8.0	18	517.9	9.1	78	577.9	10.1
39	338.9	5.9	99	398.9	7.0	59	458.9	8.0	19	518.9	9.1	79	578.9	10.1
40	339.9	5.9	400	399.9	7.0	60	459.9	8.0	20	519.9	9.1	80	579.9	10.1
341	340.9	6.0	401	400.9	7.0	461	460.9	8.0	521	520.9	9.1	581	580.9	10.1
42	341.9	6.0	02	401.9	7.0	62	461.9	8.1	22	521.9	9.1	82	581.9	10.1
43	342.9	6.0	03	402.9	7.0	63	462.9	8.1	23	522.9	9.2	83	582.9	10.2
44	343.9	6.0	04	403.9	7.1	64	463.9	8.1	24	523.9	9.2	84	583.9	10.2
45	344.9	6.0	05	404.9	7.1	65	464.9	8.1	25	524.9	9.2	85	584.9	10.2
46	345.9	6.0	06	405.9	7.1	66	465.9	8.1	26	525.9	9.2	86	585.9	10.2
47	346.9	6.1	07	406.9	7.1	67	466.9	8.1	27	526.9	9.2	87	586.9	10.2
48	347.9	6.1	08	407.9	7.1	68	467.9	8.2	28	527.9	9.2	88	587.9	10.2
49	348.9	6.1	09	408.9	7.1	69	468.9	8.2	29	528.9	9.3	89	588.9	10.3
50	349.9	6.1	10	409.9	7.2	70	469.9	8.2	30	529.9	9.3	90	589.9	10.3
351	350.9	6.1	411	410.9	7.2	471	470.9	8.2	531	530.9	9.3	591	590.9	10.3
52	351.9	6.1	12	411.9	7.2	72	471.9	8.2	32	531.9	9.3	92	591.9	10.3
53	352.9	6.2	13	412.9	7.2	73	472.9	8.2	33	532.9	9.3	93	592.9	10.3
54	353.9	6.2	14	413.9	7.2	74	473.9	8.3	34	533.9	9.3	94	593.9	10.3
55	354.9	6.2	15	414.9	7.2	75	474.9	8.3	35	534.9	9.4	95	594.9	10.4
56	355.9	6.2	16	415.9	7.3	76	475.9	8.3	36	535.9	9.4	96	595.9	10.4
57	356.9	6.2	17	416.9	7.3	77	476.9	8.3	37	536.9	9.4	97	596.9	10.4
58	357.9	6.2	18	417.9	7.3	78	477.9	8.3	38	537.9	9.4	98	597.9	10.4
59	358.9	6.3	19	418.9	7.3	79	478.9	8.4	39	538.9	9.4	99	598.9	10.4
60	359.9	6.3	20	419.9	7.3	80	479.9	8.4	40	539.9	9.4	600	599.9	10.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

89° (91°, 269°, 271°).

TABLE 2.

Difference of Latitude and Departure for 2° (178°, 182°, 358°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.0	61	61.0	2.1	121	120.9	4.2	181	180.9	6.3	241	240.9	8.4
2	2.0	0.1	62	62.0	2.2	22	121.9	4.3	82	181.9	6.4	42	241.9	8.4
3	3.0	0.1	63	63.0	2.2	23	122.9	4.3	83	182.9	6.4	43	242.9	8.5
4	4.0	0.1	64	64.0	2.2	24	123.9	4.3	84	183.9	6.4	44	243.9	8.5
5	5.0	0.2	65	65.0	2.3	25	124.9	4.4	85	184.9	6.5	45	244.9	8.6
6	6.0	0.2	66	66.0	2.3	26	125.9	4.4	86	185.9	6.5	46	245.9	8.6
7	7.0	0.2	67	67.0	2.3	27	126.9	4.4	87	186.9	6.5	47	246.8	8.6
8	8.0	0.3	68	68.0	2.4	28	127.9	4.5	88	187.9	6.6	48	247.8	8.7
9	9.0	0.3	69	69.0	2.4	29	128.9	4.5	89	188.9	6.6	49	248.8	8.7
10	10.0	0.3	70	70.0	2.4	30	129.9	4.5	90	189.9	6.6	50	249.8	8.7
11	11.0	0.4	71	71.0	2.5	131	130.9	4.6	191	190.9	6.7	251	250.8	8.8
12	12.0	0.4	72	72.0	2.5	32	131.9	4.6	92	191.9	6.7	52	251.8	8.8
13	13.0	0.5	73	73.0	2.5	33	132.9	4.6	93	192.9	6.7	53	252.8	8.8
14	14.0	0.5	74	74.0	2.6	34	133.9	4.7	94	193.9	6.8	54	253.8	8.9
15	15.0	0.5	75	75.0	2.6	35	134.9	4.7	95	194.9	6.8	55	254.8	8.9
16	16.0	0.6	76	76.0	2.7	36	135.9	4.7	96	195.9	6.8	56	255.8	8.9
17	17.0	0.6	77	77.0	2.7	37	136.9	4.8	97	196.9	6.9	57	256.8	9.0
18	18.0	0.6	78	78.0	2.7	38	137.9	4.8	98	197.9	6.9	58	257.8	9.0
19	19.0	0.7	79	79.0	2.8	39	138.9	4.9	99	198.9	6.9	59	258.8	9.0
20	20.0	0.7	80	80.0	2.8	40	139.9	4.9	200	199.9	7.0	60	259.8	9.1
21	21.0	0.7	81	81.0	2.8	141	140.9	4.9	201	200.9	7.0	261	260.8	9.1
22	22.0	0.8	82	82.0	2.9	42	141.9	5.0	02	201.9	7.0	62	261.8	9.1
23	23.0	0.8	83	82.9	2.9	43	142.9	5.0	03	202.9	7.1	63	262.8	9.2
24	24.0	0.8	84	83.9	2.9	44	143.9	5.0	04	203.9	7.1	64	263.8	9.2
25	25.0	0.9	85	84.9	3.0	45	144.9	5.1	05	204.9	7.2	65	264.8	9.2
26	26.0	0.9	86	85.9	3.0	46	145.9	5.1	06	205.9	7.2	66	265.8	9.3
27	27.0	0.9	87	86.9	3.0	47	146.9	5.1	07	206.9	7.2	67	266.8	9.3
28	28.0	1.0	88	87.9	3.1	48	147.9	5.2	08	207.9	7.3	68	267.8	9.4
29	29.0	1.0	89	88.9	3.1	49	148.9	5.2	09	208.9	7.3	69	268.8	9.4
30	30.0	1.0	90	89.9	3.1	50	149.9	5.2	10	209.9	7.3	70	269.8	9.4
31	31.0	1.1	91	90.9	3.2	151	150.9	5.3	211	210.9	7.4	271	270.8	9.5
32	32.0	1.1	92	91.9	3.2	52	151.9	5.3	12	211.9	7.4	72	271.8	9.5
33	33.0	1.2	93	92.9	3.2	53	152.9	5.3	13	212.9	7.4	73	272.8	9.5
34	34.0	1.2	94	93.9	3.3	54	153.9	5.4	14	213.9	7.5	74	273.8	9.6
35	35.0	1.2	95	94.9	3.3	55	154.9	5.4	15	214.9	7.5	75	274.8	9.6
36	36.0	1.3	96	95.9	3.4	56	155.9	5.4	16	215.9	7.5	76	275.8	9.6
37	37.0	1.3	97	96.9	3.4	57	156.9	5.5	17	216.9	7.6	77	276.8	9.7
38	38.0	1.3	98	97.9	3.4	58	157.9	5.5	18	217.9	7.6	78	277.8	9.7
39	39.0	1.4	99	98.9	3.5	59	158.9	5.5	19	218.9	7.6	79	278.8	9.7
40	40.0	1.4	100	99.9	3.5	60	159.9	5.6	20	219.9	7.7	80	279.8	9.8
41	41.0	1.4	101	100.9	3.5	161	160.9	5.6	221	220.9	7.7	281	280.8	9.8
42	42.0	1.5	02	101.9	3.6	62	161.9	5.7	22	221.9	7.7	82	281.8	9.8
43	43.0	1.5	03	102.9	3.6	63	162.9	5.7	23	222.9	7.8	83	282.8	9.9
44	44.0	1.5	04	103.9	3.6	64	163.9	5.7	24	223.9	7.8	84	283.8	9.9
45	45.0	1.6	05	104.9	3.7	65	164.9	5.8	25	224.9	7.9	85	284.8	9.9
46	46.0	1.6	06	105.9	3.7	66	165.9	5.8	26	225.9	7.9	86	285.8	10.0
47	47.0	1.6	07	106.9	3.7	67	166.9	5.8	27	226.9	7.9	87	286.8	10.0
48	48.0	1.7	08	107.9	3.8	68	167.9	5.9	28	227.9	8.0	88	287.8	10.1
49	49.0	1.7	09	108.9	3.8	69	168.9	5.9	29	228.9	8.0	89	288.8	10.1
50	50.0	1.7	10	109.9	3.8	70	169.9	5.9	30	229.9	8.0	90	289.8	10.1
51	51.0	1.8	111	110.9	3.9	171	170.9	6.0	231	230.9	8.1	291	290.8	10.2
52	52.0	1.8	12	111.9	3.9	72	171.9	6.0	32	231.9	8.1	92	291.8	10.2
53	53.0	1.8	13	112.9	3.9	73	172.9	6.0	33	232.9	8.1	93	292.8	10.2
54	54.0	1.9	14	113.9	4.0	74	173.9	6.1	34	233.9	8.2	94	293.8	10.3
55	55.0	1.9	15	114.9	4.0	75	174.9	6.1	35	234.9	8.2	95	294.8	10.3
56	56.0	2.0	16	115.9	4.0	76	175.9	6.1	36	235.9	8.2	96	295.8	10.3
57	57.0	2.0	17	116.9	4.1	77	176.9	6.2	37	236.9	8.3	97	296.8	10.4
58	58.0	2.0	18	117.9	4.1	78	177.9	6.2	38	237.9	8.3	98	297.8	10.4
59	59.0	2.1	19	118.9	4.2	79	178.9	6.2	39	238.9	8.3	99	298.8	10.4
60	60.0	2.1	20	119.9	4.2	80	179.9	6.3	40	239.9	8.4	300	299.8	10.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

88° (92°, 268°, 272°).

TABLE 2.

Difference of Latitude and Departure for 2° (178°, 182°, 358°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	300.8	10.5	361	360.8	12.6	421	420.8	14.7	481	480.7	16.8	541	540.7	18.9
02	301.8	10.5	62	361.8	12.6	22	421.8	14.7	82	481.7	16.8	42	541.7	18.9
03	302.8	10.6	63	362.8	12.7	23	422.8	14.7	83	482.7	16.8	43	542.7	18.9
04	303.8	10.6	64	363.8	12.7	24	423.8	14.8	84	483.7	16.9	44	543.7	19.0
05	304.8	10.6	65	364.8	12.7	25	424.8	14.8	85	484.7	16.9	45	544.7	19.0
06	305.8	10.7	66	365.8	12.8	26	425.7	14.9	86	485.7	16.9	46	545.7	19.0
07	306.8	10.7	67	366.8	12.8	27	426.7	14.9	87	486.7	17.0	47	546.7	19.1
08	307.8	10.7	68	367.8	12.8	28	427.7	14.9	88	487.7	17.0	48	547.7	19.1
09	308.8	10.8	69	368.8	12.9	29	428.7	15.0	89	488.7	17.0	49	548.7	19.1
10	309.8	10.8	70	369.8	12.9	30	429.7	15.0	90	489.7	17.1	50	549.7	19.2
311	310.8	10.8	371	370.8	12.9	431	430.7	15.0	491	490.7	17.1	551	550.7	19.2
12	311.8	10.9	72	371.8	13.0	32	431.7	15.1	92	491.7	17.1	52	551.7	19.2
13	312.8	10.9	73	372.8	13.0	33	432.7	15.1	93	492.7	17.2	53	552.7	19.3
14	313.8	10.9	74	373.8	13.0	34	433.7	15.1	94	493.7	17.2	54	553.7	19.3
15	314.8	11.0	75	374.8	13.1	35	434.7	15.2	95	494.7	17.2	55	554.7	19.3
16	315.8	11.0	76	375.8	13.1	36	435.7	15.2	96	495.7	17.3	56	555.7	19.4
17	316.8	11.0	77	376.8	13.1	37	436.7	15.2	97	496.7	17.3	57	556.7	19.4
18	317.8	11.1	78	377.8	13.2	38	437.7	15.3	98	497.7	17.3	58	557.7	19.4
19	318.8	11.1	79	378.8	13.2	39	438.7	15.3	99	498.7	17.4	59	558.7	19.5
20	319.8	11.2	80	379.8	13.2	40	439.7	15.3	500	499.7	17.4	60	559.7	19.5
321	320.8	11.2	381	380.8	13.3	441	440.7	15.4	501	500.7	17.5	561	560.7	19.5
22	321.8	11.2	82	381.8	13.3	42	441.7	15.4	02	501.7	17.5	62	561.7	19.6
23	322.8	11.3	83	382.8	13.3	43	442.7	15.4	03	502.7	17.5	63	562.7	19.6
24	323.8	11.3	84	383.8	13.4	44	443.7	15.5	04	503.7	17.6	64	563.7	19.6
25	324.8	11.3	85	384.8	13.4	45	444.7	15.5	05	504.7	17.6	65	564.7	19.7
26	325.8	11.4	86	385.8	13.5	46	445.7	15.6	06	505.7	17.6	66	565.7	19.7
27	326.8	11.4	87	386.8	13.5	47	446.7	15.6	07	506.7	17.7	67	566.7	19.7
28	327.8	11.4	88	387.8	13.5	48	447.7	15.6	08	507.7	17.7	68	567.7	19.8
29	328.8	11.5	89	388.8	13.6	49	448.7	15.7	09	508.7	17.7	69	568.7	19.8
30	329.8	11.5	90	389.8	13.6	50	449.7	15.7	10	509.7	17.8	70	569.7	19.9
331	330.8	11.5	391	390.8	13.6	451	450.7	15.7	511	510.7	17.8	571	570.7	19.9
32	331.8	11.6	92	391.8	13.7	52	451.7	15.8	12	511.7	17.8	72	571.7	19.9
33	332.8	11.6	93	392.8	13.7	53	452.7	15.8	13	512.7	17.9	73	572.7	20.0
34	333.8	11.6	94	393.8	13.7	54	453.7	15.8	14	513.7	17.9	74	573.6	20.0
35	334.8	11.7	95	394.8	13.8	55	454.7	15.9	15	514.7	17.9	75	574.6	20.0
36	335.8	11.7	96	395.8	13.8	56	455.7	15.9	16	515.7	18.0	76	575.6	20.1
37	336.8	11.7	97	396.8	13.8	57	456.7	15.9	17	516.7	18.0	77	576.6	20.1
38	337.8	11.8	98	397.8	13.9	58	457.7	16.0	18	517.7	18.1	78	577.6	20.1
39	338.8	11.8	99	398.8	13.9	59	458.7	16.0	19	518.7	18.1	79	578.6	20.2
40	339.8	11.9	400	399.8	13.9	60	459.7	16.0	20	519.7	18.1	80	579.6	20.2
341	340.8	11.9	401	400.8	14.0	461	460.7	16.1	521	520.7	18.2	581	580.6	20.2
42	341.8	11.9	02	401.8	14.0	62	461.7	16.1	22	521.7	18.2	82	581.6	20.3
43	342.8	12.0	03	402.8	14.0	63	462.7	16.1	23	522.7	18.2	83	582.6	20.3
44	343.8	12.0	04	403.8	14.1	64	463.7	16.2	24	523.7	18.3	84	583.6	20.3
45	344.8	12.0	05	404.8	14.1	65	464.7	16.2	25	524.7	18.3	85	584.6	20.4
46	345.8	12.1	06	405.8	14.2	66	465.7	16.2	26	525.7	18.4	86	585.6	20.4
47	346.8	12.1	07	406.8	14.2	67	466.7	16.3	27	526.7	18.4	87	586.6	20.4
48	347.8	12.1	08	407.8	14.2	68	467.7	16.3	28	527.7	18.4	88	587.6	20.5
49	348.8	12.2	09	408.8	14.3	69	468.7	16.4	29	528.7	18.5	89	588.6	20.5
50	349.8	12.2	10	409.8	14.3	70	469.7	16.4	30	529.7	18.5	90	589.6	20.5
351	350.8	12.2	411	410.8	14.3	471	470.7	16.4	531	530.7	18.5	591	590.6	20.6
52	351.8	12.3	12	411.8	14.4	72	471.7	16.5	32	531.7	18.6	92	591.6	20.6
53	352.8	12.3	13	412.8	14.4	73	472.7	16.5	33	532.7	18.6	93	592.6	20.6
54	353.8	12.3	14	413.8	14.4	74	473.7	16.5	34	533.7	18.6	94	593.6	20.7
55	354.8	12.4	15	414.8	14.5	75	474.7	16.6	35	534.7	18.7	95	594.6	20.7
56	355.8	12.4	16	415.8	14.5	76	475.7	16.6	36	535.7	18.7	96	595.6	20.7
57	356.8	12.4	17	416.8	14.5	77	476.7	16.6	37	536.7	18.7	97	596.6	20.8
58	357.8	12.5	18	417.8	14.6	78	477.7	16.7	38	537.7	18.8	98	597.6	20.8
59	358.8	12.5	19	418.8	14.6	79	478.7	16.7	39	538.7	18.8	99	598.6	20.8
60	359.8	12.5	20	419.8	14.6	80	479.7	16.7	40	539.7	18.8	600	599.6	20.9
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

88° (92°, 268°, 272°).

TABLE 2.

Difference of Latitude and Departure for 3° (177°, 183°, 357°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.1	61	60.9	3.2	121	120.8	6.3	181	180.8	9.5	241	240.7	12.6
2	2.0	0.1	62	61.9	3.2	22	121.8	6.4	82	181.8	9.5	42	241.7	12.7
3	3.0	0.2	63	62.9	3.3	23	122.8	6.4	83	182.7	9.6	43	242.7	12.7
4	4.0	0.2	64	63.9	3.3	24	123.8	6.5	84	183.7	9.6	44	243.7	12.8
5	5.0	0.3	65	64.9	3.4	25	124.8	6.5	85	184.7	9.7	45	244.7	12.8
6	6.0	0.3	66	65.9	3.5	26	125.8	6.6	86	185.7	9.7	46	245.7	12.9
7	7.0	0.4	67	66.9	3.5	27	126.8	6.6	87	186.7	9.8	47	246.7	12.9
8	8.0	0.4	68	67.9	3.6	28	127.8	6.7	88	187.7	9.8	48	247.7	13.0
9	9.0	0.5	69	68.9	3.6	29	128.8	6.8	89	188.7	9.9	49	248.7	13.0
10	10.0	0.5	70	69.9	3.7	30	129.8	6.8	90	189.7	9.9	50	249.7	13.1
11	11.0	0.6	71	70.9	3.7	131	130.8	6.9	191	190.7	10.0	251	250.7	13.1
12	12.0	0.6	72	71.9	3.8	32	131.8	6.9	92	191.7	10.0	52	251.7	13.2
13	13.0	0.7	73	72.9	3.8	33	132.8	7.0	93	192.7	10.1	53	252.7	13.2
14	14.0	0.7	74	73.9	3.9	34	133.8	7.0	94	193.7	10.2	54	253.7	13.3
15	15.0	0.8	75	74.9	3.9	35	134.8	7.1	95	194.7	10.2	55	254.7	13.3
16	16.0	0.8	76	75.9	4.0	36	135.8	7.1	96	195.7	10.3	56	255.6	13.4
17	17.0	0.9	77	76.9	4.0	37	136.8	7.2	97	196.7	10.3	57	256.6	13.5
18	18.0	0.9	78	77.9	4.1	38	137.8	7.2	98	197.7	10.4	58	257.6	13.5
19	19.0	1.0	79	78.9	4.1	39	138.8	7.3	99	198.7	10.4	59	258.6	13.6
20	20.0	1.0	80	79.9	4.2	40	139.8	7.3	200	199.7	10.5	60	259.6	13.6
21	21.0	1.1	81	80.9	4.2	141	140.8	7.4	201	200.7	10.5	261	260.6	13.7
22	22.0	1.2	82	81.9	4.3	42	141.8	7.4	02	201.7	10.6	62	261.6	13.7
23	23.0	1.2	83	82.9	4.3	43	142.8	7.5	03	202.7	10.6	63	262.6	13.8
24	24.0	1.3	84	83.9	4.4	44	143.8	7.5	04	203.7	10.7	64	263.6	13.8
25	25.0	1.3	85	84.9	4.4	45	144.8	7.6	05	204.7	10.7	65	264.6	13.9
26	26.0	1.4	86	85.9	4.5	46	145.8	7.6	06	205.7	10.8	66	265.6	13.9
27	27.0	1.4	87	86.9	4.6	47	146.8	7.7	07	206.7	10.8	67	266.6	14.0
28	28.0	1.5	88	87.9	4.6	48	147.8	7.7	08	207.7	10.9	68	267.6	14.0
29	29.0	1.5	89	88.9	4.7	49	148.8	7.8	09	208.7	10.9	69	268.6	14.1
30	30.0	1.6	90	89.9	4.7	50	149.8	7.9	10	209.7	11.0	70	269.6	14.1
31	31.0	1.6	91	90.9	4.8	151	150.8	7.9	211	210.7	11.0	271	270.6	14.2
32	32.0	1.7	92	91.9	4.8	52	151.8	8.0	12	211.7	11.1	72	271.6	14.2
33	33.0	1.7	93	92.9	4.9	53	152.8	8.0	13	212.7	11.1	73	272.6	14.3
34	34.0	1.8	94	93.9	4.9	54	153.8	8.1	14	213.7	11.2	74	273.6	14.3
35	35.0	1.8	95	94.9	5.0	55	154.8	8.1	15	214.7	11.3	75	274.6	14.4
36	36.0	1.9	96	95.9	5.0	56	155.8	8.2	16	215.7	11.3	76	275.6	14.4
37	36.9	1.9	97	96.9	5.1	57	156.8	8.2	17	216.7	11.4	77	276.6	14.5
38	37.9	2.0	98	97.9	5.1	58	157.8	8.3	18	217.7	11.4	78	277.6	14.5
39	38.9	2.0	99	98.9	5.2	59	158.8	8.3	19	218.7	11.5	79	278.6	14.6
40	39.9	2.1	100	99.9	5.2	60	159.8	8.4	20	219.7	11.5	80	279.6	14.7
41	40.9	2.1	101	100.9	5.3	161	160.8	8.4	221	220.7	11.6	281	280.6	14.7
42	41.9	2.2	02	101.9	5.3	62	161.8	8.5	22	221.7	11.6	82	281.6	14.8
43	42.9	2.3	03	102.9	5.4	63	162.8	8.5	23	222.7	11.7	83	282.6	14.8
44	43.9	2.3	04	103.9	5.4	64	163.8	8.6	24	223.7	11.7	84	283.6	14.9
45	44.9	2.4	05	104.9	5.5	65	164.8	8.6	25	224.7	11.8	85	284.6	14.9
46	45.9	2.4	06	105.9	5.5	66	165.8	8.7	26	225.7	11.8	86	285.6	15.0
47	46.9	2.5	07	106.9	5.6	67	166.8	8.7	27	226.7	11.9	87	286.6	15.0
48	47.9	2.5	08	107.9	5.7	68	167.8	8.8	28	227.7	11.9	88	287.6	15.1
49	48.9	2.6	09	108.9	5.7	69	168.8	8.8	29	228.7	12.0	89	288.6	15.1
50	49.9	2.6	10	109.8	5.8	70	169.8	8.9	30	229.7	12.0	90	289.6	15.2
51	50.9	2.7	111	110.8	5.8	171	170.8	8.9	231	230.7	12.1	291	290.6	15.2
52	51.9	2.7	12	111.8	5.9	72	171.8	9.0	32	231.7	12.1	92	291.6	15.3
53	52.9	2.8	13	112.8	5.9	73	172.8	9.1	33	232.7	12.2	93	292.6	15.3
54	53.9	2.8	14	113.8	6.0	74	173.8	9.1	34	233.7	12.2	94	293.6	15.4
55	54.9	2.9	15	114.8	6.0	75	174.8	9.2	35	234.7	12.3	95	294.6	15.4
56	55.9	2.9	16	115.8	6.1	76	175.8	9.2	36	235.7	12.4	96	295.6	15.5
57	56.9	3.0	17	116.8	6.1	77	176.8	9.3	37	236.7	12.4	97	296.6	15.5
58	57.9	3.0	18	117.8	6.2	78	177.8	9.3	38	237.7	12.5	98	297.6	15.6
59	58.9	3.1	19	118.8	6.2	79	178.8	9.4	39	238.7	12.5	99	298.6	15.6
60	59.9	3.1	20	119.8	6.3	80	179.8	9.4	40	239.7	12.6	300	299.6	15.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

87° (93°, 267°, 273°).

TABLE 2.

Difference of Latitude and Departure for 3° (177°, 183°, 357°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	300.6	15.7	361	360.5	18.9	421	420.4	22.0	481	480.3	25.2	541	540.2	28.3
02	301.6	15.8	62	361.5	19.0	22	421.4	22.1	82	481.3	25.2	42	541.2	28.4
03	302.6	15.9	63	362.5	19.0	23	422.4	22.2	83	482.3	25.3	43	542.2	28.4
04	303.5	15.9	64	363.5	19.1	24	423.4	22.2	84	483.3	25.3	44	543.2	28.5
05	304.5	16.0	65	364.5	19.1	25	424.4	22.3	85	484.3	25.4	45	544.2	28.5
06	305.5	16.0	66	365.5	19.2	26	425.4	22.3	86	485.3	25.4	46	545.2	28.6
07	306.5	16.1	67	366.5	19.2	27	426.4	22.4	87	486.3	25.5	47	546.2	28.6
08	307.5	16.1	68	367.5	19.3	28	427.4	22.4	88	487.3	25.5	48	547.2	28.7
09	308.5	16.2	69	368.5	19.3	29	428.4	22.5	89	488.3	25.6	49	548.2	28.7
10	309.5	16.2	70	369.5	19.4	30	429.4	22.5	90	489.3	25.6	50	549.2	28.8
311	310.5	16.3	371	370.5	19.4	431	430.4	22.6	491	490.3	25.7	551	550.2	28.8
12	311.5	16.3	72	371.5	19.5	32	431.4	22.6	92	491.3	25.7	52	551.2	28.9
13	312.5	16.4	73	372.5	19.5	33	432.4	22.7	93	492.3	25.8	53	552.2	28.9
14	313.5	16.4	74	373.5	19.6	34	433.4	22.7	94	493.3	25.9	54	553.2	29.0
15	314.5	16.5	75	374.5	19.6	35	434.4	22.8	95	494.3	25.9	55	554.2	29.1
16	315.5	16.6	76	375.5	19.7	36	435.4	22.8	96	495.3	26.0	56	555.2	29.1
17	316.5	16.6	77	376.5	19.8	37	436.4	22.9	97	496.3	26.0	57	556.2	29.2
18	317.5	16.7	78	377.4	19.8	38	437.4	22.9	98	497.3	26.1	58	557.2	29.2
19	318.5	16.7	79	378.4	19.9	39	438.4	23.0	99	498.3	26.1	59	558.2	29.3
20	319.5	16.8	80	379.4	19.9	40	439.4	23.0	500	499.3	26.2	60	559.2	29.3
321	320.5	16.8	381	380.4	20.0	441	440.4	23.1	501	500.3	26.2	561	560.2	29.4
22	321.5	16.9	82	381.4	20.0	42	441.4	23.1	02	501.3	26.3	62	561.2	29.4
23	322.5	16.9	83	382.4	20.1	43	442.4	23.2	03	502.3	26.3	63	562.2	29.5
24	323.5	17.0	84	383.4	20.1	44	443.4	23.3	04	503.3	26.4	64	563.2	29.5
25	324.5	17.0	85	384.4	20.2	45	444.4	23.3	05	504.3	26.4	65	564.2	29.6
26	325.5	17.1	86	385.4	20.2	46	445.4	23.4	06	505.3	26.5	66	565.2	29.6
27	326.5	17.1	87	386.4	20.3	47	446.4	23.4	07	506.3	26.5	67	566.2	29.7
28	327.5	17.2	88	387.4	20.3	48	447.4	23.5	08	507.3	26.6	68	567.2	29.7
29	328.5	17.2	89	388.4	20.4	49	448.4	23.5	09	508.3	26.6	69	568.2	29.8
30	329.5	17.3	90	389.4	20.4	50	449.3	23.6	10	509.3	26.7	70	569.2	29.8
331	330.5	17.3	391	390.4	20.5	451	450.3	23.6	511	510.3	26.7	571	570.2	29.9
32	331.5	17.4	92	391.4	20.5	52	451.3	23.7	12	511.3	26.8	72	571.2	29.9
33	332.5	17.5	93	392.4	20.6	53	452.3	23.7	13	512.3	26.8	73	572.2	30.0
34	333.5	17.5	94	393.4	20.6	54	453.3	23.8	14	513.3	26.9	74	573.2	30.0
35	334.5	17.6	95	394.4	20.7	55	454.3	23.8	15	514.3	27.0	75	574.2	30.1
36	335.5	17.6	96	395.4	20.7	56	455.3	23.9	16	515.3	27.0	76	575.2	30.1
37	336.5	17.7	97	396.4	20.8	57	456.3	23.9	17	516.3	27.1	77	576.2	30.2
38	337.5	17.7	98	397.4	20.8	58	457.3	24.0	18	517.3	27.1	78	577.2	30.2
39	338.5	17.8	99	398.4	20.9	59	458.3	24.0	19	518.3	27.2	79	578.2	30.3
40	339.5	17.8	400	399.4	20.9	60	459.3	24.1	20	519.3	27.2	80	579.2	30.3
341	340.5	17.9	401	400.4	21.0	461	460.3	24.1	521	520.3	27.3	581	580.2	30.4
42	341.5	17.9	02	401.4	21.1	62	461.3	24.2	22	521.3	27.3	82	581.2	30.4
43	342.5	18.0	03	402.4	21.1	63	462.3	24.2	23	522.3	27.4	83	582.2	30.5
44	343.5	18.0	04	403.4	21.2	64	463.3	24.3	24	523.3	27.4	84	583.2	30.5
45	344.5	18.1	05	404.4	21.2	65	464.3	24.4	25	524.3	27.5	85	584.2	30.6
46	345.5	18.1	06	405.4	21.3	66	465.3	24.4	26	525.3	27.5	86	585.2	30.6
47	346.5	18.2	07	406.4	21.3	67	466.3	24.5	27	526.3	27.6	87	586.2	30.7
48	347.5	18.2	08	407.4	21.4	68	467.3	24.5	28	527.3	27.6	88	587.2	30.7
49	348.5	18.3	09	408.4	21.4	69	468.3	24.6	29	528.3	27.7	89	588.2	30.8
50	349.5	18.3	10	409.4	21.5	70	469.3	24.6	30	529.3	27.7	90	589.2	30.9
351	350.5	18.4	411	410.4	21.5	471	470.3	24.7	531	530.3	27.8	591	590.2	30.9
52	351.5	18.4	12	411.4	21.6	72	471.3	24.7	32	531.3	27.8	92	591.2	31.0
53	352.5	18.5	13	412.4	21.6	73	472.3	24.8	33	532.3	27.9	93	592.2	31.0
54	353.5	18.5	14	413.4	21.7	74	473.3	24.8	34	533.3	27.9	94	593.2	31.1
55	354.5	18.6	15	414.4	21.7	75	474.3	24.9	35	534.3	28.0	95	594.2	31.1
56	355.5	18.6	16	415.4	21.8	76	475.3	24.9	36	535.3	28.1	96	595.2	31.2
57	356.5	18.7	17	416.4	21.8	77	476.3	25.0	37	536.3	28.1	97	596.2	31.2
58	357.5	18.8	18	417.4	21.9	78	477.3	25.0	38	537.3	28.2	98	597.2	31.3
59	358.5	18.8	19	418.4	21.9	79	478.3	25.1	39	538.3	28.2	99	598.2	31.3
60	359.5	18.9	20	419.4	22.0	80	479.3	25.1	40	539.3	28.3	600	599.2	31.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

87° (93°, 267°, 273°).

TABLE 2.

Difference of Latitude and Departure for 4° (176°, 184°, 356°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.1	61	60.9	4.3	121	120.7	8.4	181	180.6	12.6	241	240.4	16.8
2	2.0	0.1	62	61.8	4.3	22	121.7	8.5	82	181.6	12.7	42	241.4	16.9
3	3.0	0.2	63	62.8	4.4	23	122.7	8.6	83	182.6	12.8	43	242.4	17.0
4	4.0	0.3	64	63.8	4.5	24	123.7	8.6	84	183.6	12.8	44	243.4	17.0
5	5.0	0.3	65	64.8	4.5	25	124.7	8.7	85	184.5	12.9	45	244.4	17.1
6	6.0	0.4	66	65.8	4.6	26	125.7	8.8	86	185.5	13.0	46	245.4	17.2
7	7.0	0.5	67	66.8	4.7	27	126.7	8.9	87	186.5	13.0	47	246.4	17.2
8	8.0	0.6	68	67.8	4.7	28	127.7	8.9	88	187.5	13.1	48	247.4	17.3
9	9.0	0.6	69	68.8	4.8	29	128.7	9.0	89	188.5	13.2	49	248.4	17.4
10	10.0	0.7	70	69.8	4.9	30	129.7	9.1	90	189.5	13.3	50	249.4	17.4
11	11.0	0.8	71	70.8	5.0	131	130.7	9.1	191	190.5	13.3	251	250.4	17.5
12	12.0	0.8	72	71.8	5.0	32	131.7	9.2	92	191.5	13.4	52	251.4	17.6
13	13.0	0.9	73	72.8	5.1	33	132.7	9.3	93	192.5	13.5	53	252.4	17.6
14	14.0	1.0	74	73.8	5.2	34	133.7	9.3	94	193.5	13.5	54	253.4	17.7
15	15.0	1.0	75	74.8	5.2	35	134.7	9.4	95	194.5	13.6	55	254.4	17.8
16	16.0	1.1	76	75.8	5.3	36	135.7	9.5	96	195.5	13.7	56	255.4	17.9
17	17.0	1.2	77	76.8	5.4	37	136.7	9.6	97	196.5	13.7	57	256.4	17.9
18	18.0	1.3	78	77.8	5.4	38	137.7	9.6	98	197.5	13.8	58	257.4	18.0
19	19.0	1.3	79	78.8	5.5	39	138.7	9.7	99	198.5	13.9	59	258.4	18.1
20	20.0	1.4	80	79.8	5.6	40	139.7	9.8	200	199.5	14.0	60	259.4	18.1
21	20.9	1.5	81	80.8	5.7	141	140.7	9.8	201	200.5	14.0	261	260.4	18.2
22	21.9	1.5	82	81.8	5.7	42	141.7	9.9	02	201.5	14.1	62	261.4	18.3
23	22.9	1.6	83	82.8	5.8	43	142.7	10.0	03	202.5	14.2	63	262.4	18.3
24	23.9	1.7	84	83.8	5.9	44	143.6	10.0	04	203.5	14.2	64	263.4	18.4
25	24.9	1.7	85	84.8	5.9	45	144.6	10.1	05	204.5	14.3	65	264.4	18.5
26	25.9	1.8	86	85.8	6.0	46	145.6	10.2	06	205.5	14.4	66	265.4	18.6
27	26.9	1.9	87	86.8	6.1	47	146.6	10.3	07	206.5	14.4	67	266.3	18.6
28	27.9	2.0	88	87.8	6.1	48	147.6	10.3	08	207.5	14.5	68	267.3	18.7
29	28.9	2.0	89	88.8	6.2	49	148.6	10.4	09	208.5	14.6	69	268.3	18.8
30	29.9	2.1	90	89.8	6.3	50	149.6	10.5	10	209.5	14.6	70	269.3	18.8
31	30.9	2.2	91	90.8	6.3	151	150.6	10.5	211	210.5	14.7	271	270.3	18.9
32	31.9	2.2	92	91.8	6.4	52	151.6	10.6	12	211.5	14.8	72	271.3	19.0
33	32.9	2.3	93	92.8	6.5	53	152.6	10.7	13	212.5	14.9	73	272.3	19.0
34	33.9	2.4	94	93.8	6.6	54	153.6	10.7	14	213.5	14.9	74	273.3	19.1
35	34.9	2.4	95	94.8	6.6	55	154.6	10.8	15	214.5	15.0	75	274.3	19.2
36	35.9	2.5	96	95.8	6.7	56	155.6	10.9	16	215.5	15.1	76	275.3	19.3
37	36.9	2.6	97	96.8	6.8	57	156.6	11.0	17	216.5	15.1	77	276.3	19.3
38	37.9	2.7	98	97.8	6.8	58	157.6	11.0	18	217.5	15.2	78	277.3	19.4
39	38.9	2.7	99	98.8	6.9	59	158.6	11.1	19	218.5	15.3	79	278.3	19.5
40	39.9	2.8	100	99.8	7.0	60	159.6	11.2	20	219.5	15.3	80	279.3	19.5
41	40.9	2.9	101	100.8	7.0	161	160.6	11.2	221	220.5	15.4	281	280.3	19.6
42	41.9	2.9	02	101.8	7.1	62	161.6	11.3	22	221.5	15.5	82	281.3	19.7
43	42.9	3.0	03	102.7	7.2	63	162.6	11.4	23	222.5	15.6	83	282.3	19.7
44	43.9	3.1	04	103.7	7.3	64	163.6	11.4	24	223.5	15.6	84	283.3	19.8
45	44.9	3.1	05	104.7	7.3	65	164.6	11.5	25	224.5	15.7	85	284.3	19.9
46	45.9	3.2	06	105.7	7.4	66	165.6	11.6	26	225.4	15.8	86	285.3	20.0
47	46.9	3.3	07	106.7	7.5	67	166.6	11.6	27	226.4	15.8	87	286.3	20.0
48	47.9	3.3	08	107.7	7.5	68	167.6	11.7	28	227.4	15.9	88	287.3	20.1
49	48.9	3.4	09	108.7	7.6	69	168.6	11.8	29	228.4	16.0	89	288.3	20.2
50	49.9	3.5	10	109.7	7.7	70	169.6	11.9	30	229.4	16.0	90	289.3	20.2
51	50.9	3.6	111	110.7	7.7	171	170.6	11.9	231	230.4	16.1	291	290.3	20.3
52	51.9	3.6	12	111.7	7.8	72	171.6	12.0	32	231.4	16.2	92	291.3	20.4
53	52.9	3.7	13	112.7	7.9	73	172.6	12.1	33	232.4	16.3	93	292.3	20.4
54	53.9	3.8	14	113.7	8.0	74	173.6	12.1	34	233.4	16.3	94	293.3	20.5
55	54.9	3.8	15	114.7	8.0	75	174.6	12.2	35	234.4	16.4	95	294.3	20.6
56	55.9	3.9	16	115.7	8.1	76	175.6	12.3	36	235.4	16.5	96	295.3	20.6
57	56.9	4.0	17	116.7	8.2	77	176.6	12.3	37	236.4	16.5	97	296.3	20.7
58	57.9	4.0	18	117.7	8.2	78	177.6	12.4	38	237.4	16.6	98	297.3	20.8
59	58.9	4.1	19	118.7	8.3	79	178.6	12.5	39	238.4	16.7	99	298.3	20.9
60	59.9	4.2	20	119.7	8.4	80	179.6	12.6	40	239.4	16.7	300	299.3	20.9
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

86°; (94°, 266°, 274°).

TABLE 2.

Difference of Latitude and Departure for 4° (176°, 184°, 356°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	300.3	21.0	361	360.1	25.2	421	420.0	29.4	481	479.8	33.5	541	539.7	37.7
02	301.3	21.1	62	361.1	25.2	22	421.0	29.4	82	480.8	33.6	42	540.7	37.8
03	302.2	21.1	63	362.1	25.3	23	422.0	29.5	83	481.8	33.7	43	541.7	37.9
04	303.2	21.2	64	363.1	25.4	24	423.0	29.6	84	482.8	33.7	44	542.7	37.9
05	304.2	21.3	65	364.1	25.5	25	424.0	29.6	85	483.8	33.8	45	543.7	38.0
06	305.2	21.3	66	365.1	25.5	26	424.9	29.7	86	484.8	33.9	46	544.7	38.1
07	306.2	21.4	67	366.1	25.6	27	425.9	29.8	87	485.8	33.9	47	545.7	38.1
08	307.2	21.5	68	367.1	25.7	28	426.9	29.9	88	486.8	34.0	48	546.7	38.2
09	308.2	21.6	69	368.1	25.7	29	427.9	29.9	89	487.8	34.1	49	547.7	38.3
10	309.2	21.6	70	369.1	25.8	30	428.9	30.0	90	488.8	34.2	50	548.7	38.3
311	310.2	21.7	371	370.1	25.9	431	429.9	30.1	491	489.8	34.2	551	549.7	38.4
12	311.2	21.8	72	371.1	25.9	32	430.9	30.1	92	490.8	34.3	52	550.7	38.5
13	312.2	21.8	73	372.1	26.0	33	431.9	30.2	93	491.8	34.4	53	551.7	38.5
14	313.2	21.9	74	373.1	26.1	34	432.9	30.3	94	492.8	34.4	54	552.7	38.6
15	314.2	22.0	75	374.1	26.2	35	433.9	30.3	95	493.8	34.5	55	553.6	38.7
16	315.2	22.1	76	375.1	26.2	36	434.9	30.4	96	494.8	34.6	56	554.6	38.7
17	316.2	22.1	77	376.1	26.3	37	435.9	30.5	97	495.8	34.6	57	555.6	38.8
18	317.2	22.2	78	377.1	26.4	38	436.9	30.6	98	496.8	34.7	58	556.6	38.9
19	318.2	22.3	79	378.1	26.4	39	437.9	30.6	99	497.8	34.8	59	557.6	38.9
20	319.2	22.3	80	379.1	26.5	40	438.9	30.7	500	498.8	34.8	60	558.6	39.0
321	320.2	22.4	381	380.1	26.6	441	439.9	30.8	501	499.8	34.9	561	559.6	39.1
22	321.2	22.5	82	381.1	26.6	42	440.9	30.8	02	500.8	35.0	62	560.6	39.2
23	322.2	22.5	83	382.1	26.7	43	441.9	30.9	03	501.8	35.0	63	561.6	39.2
24	323.2	22.6	84	383.1	26.8	44	442.9	31.0	04	502.8	35.1	64	562.6	39.3
25	324.2	22.7	85	384.0	26.9	45	443.9	31.0	05	503.8	35.2	65	563.6	39.4
26	325.2	22.7	86	385.0	26.9	46	444.9	31.1	06	504.8	35.2	66	564.6	39.4
27	326.2	22.8	87	386.0	27.0	47	445.9	31.2	07	505.8	35.3	67	565.6	39.5
28	327.2	22.9	88	387.0	27.1	48	446.9	31.2	08	506.8	35.4	68	566.6	39.6
29	328.2	23.0	89	388.0	27.1	49	447.9	31.3	09	507.8	35.5	69	567.6	39.7
30	329.2	23.0	90	389.0	27.2	50	448.9	31.4	10	508.8	35.6	70	568.6	39.8
331	330.2	23.1	391	390.0	27.3	451	449.9	31.5	511	509.8	35.6	571	569.6	39.8
32	331.2	23.2	92	391.0	27.3	52	450.9	31.5	12	510.8	35.7	72	570.6	39.9
33	332.2	23.2	93	392.0	27.4	53	451.9	31.6	13	511.8	35.8	73	571.6	40.0
34	333.2	23.3	94	393.0	27.5	54	452.9	31.7	14	512.7	35.8	74	572.6	40.0
35	334.2	23.4	95	394.0	27.6	55	453.9	31.7	15	513.7	35.9	75	573.6	40.1
36	335.2	23.4	96	395.0	27.6	56	454.9	31.8	16	514.7	36.0	76	574.6	40.2
37	336.2	23.5	97	396.0	27.7	57	455.9	31.9	17	515.7	36.0	77	575.6	40.2
38	337.2	23.6	98	397.0	27.8	58	456.9	31.9	18	516.7	36.1	78	576.6	40.3
39	338.2	23.6	99	398.0	27.8	59	457.9	32.0	19	517.7	36.2	79	577.6	40.4
40	339.2	23.7	400	399.0	27.9	60	458.9	32.1	20	518.7	36.2	80	578.6	40.5
341	340.2	23.8	401	400.0	28.0	461	459.9	32.2	521	519.7	36.3	581	579.6	40.5
42	341.2	23.9	02	401.0	28.0	62	460.9	32.2	22	520.7	36.4	82	580.6	40.6
43	342.2	23.9	03	402.0	28.1	63	461.9	32.3	23	521.7	36.4	83	581.6	40.7
44	343.1	24.0	04	403.0	28.2	64	462.9	32.4	24	522.7	36.5	84	582.6	40.7
45	344.1	24.1	05	404.0	28.2	65	463.9	32.4	25	523.7	36.6	85	583.6	40.8
46	345.1	24.1	06	405.0	28.3	66	464.9	32.5	26	524.7	36.7	86	584.6	40.9
47	346.1	24.2	07	406.0	28.4	67	465.8	32.6	27	525.7	36.8	87	585.6	40.9
48	347.1	24.3	08	407.0	28.5	68	466.8	32.6	28	526.7	36.8	88	586.6	41.0
49	348.1	24.3	09	408.0	28.5	69	467.8	32.7	29	527.7	36.9	89	587.6	41.1
50	349.1	24.4	10	409.0	28.6	70	468.8	32.8	30	528.7	37.0	90	588.6	41.2
351	350.1	24.5	411	410.0	28.7	471	469.8	32.9	531	529.7	37.0	591	589.6	41.3
52	351.1	24.6	12	411.0	28.7	72	470.8	32.9	32	530.7	37.1	92	590.6	41.3
53	352.1	24.6	13	412.0	28.8	73	471.8	33.0	33	531.7	37.2	93	591.6	41.4
54	353.1	24.7	14	413.0	28.9	74	472.8	33.1	34	532.7	37.2	94	592.6	41.5
55	354.1	24.8	15	414.0	28.9	75	473.8	33.1	35	533.7	37.3	95	593.6	41.5
56	355.1	24.8	16	415.0	29.0	76	474.8	33.2	36	534.7	37.4	96	594.6	41.6
57	356.1	24.9	17	416.0	29.1	77	475.8	33.3	37	535.7	37.5	97	595.6	41.7
58	357.1	25.0	18	417.0	29.2	78	476.8	33.3	38	536.7	37.5	98	596.6	41.7
59	358.1	25.0	19	418.0	29.2	79	477.8	33.4	39	537.7	37.6	99	597.6	41.8
60	359.1	25.1	20	419.0	29.3	80	478.8	35.5	40	538.7	37.7	600	598.6	41.9
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat

86°; (94°, 266°, 274°).

TABLE 2.

Difference of Latitude and Departure for 5° (175°, 185°, 355°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.1	61	60.8	5.3	121	120.5	10.5	181	180.3	15.8	241	240.1	21.0
2	2.0	0.2	62	61.8	5.4	22	121.5	10.6	82	181.3	15.9	42	241.1	21.1
3	3.0	0.3	63	62.8	5.5	23	122.5	10.7	83	182.3	15.9	43	242.1	21.2
4	4.0	0.3	64	63.8	5.6	24	123.5	10.8	84	183.3	16.0	44	243.1	21.3
5	5.0	0.4	65	64.8	5.7	25	124.5	10.9	85	184.3	16.1	45	244.1	21.4
6	6.0	0.5	66	65.7	5.8	26	125.5	11.0	86	185.3	16.2	46	245.1	21.4
7	7.0	0.6	67	66.7	5.8	27	126.5	11.1	87	186.3	16.3	47	246.1	21.5
8	8.0	0.7	68	67.7	5.9	28	127.5	11.2	88	187.3	16.4	48	247.1	21.6
9	9.0	0.8	69	68.7	6.0	29	128.5	11.2	89	188.3	16.5	49	248.1	21.7
10	10.0	0.9	70	69.7	6.1	30	129.5	11.3	90	189.3	16.6	50	249.0	21.8
11	11.0	1.0	71	70.7	6.2	131	130.5	11.4	191	190.3	16.6	251	250.0	21.9
12	12.0	1.0	72	71.7	6.3	32	131.5	11.5	92	191.3	16.7	52	251.0	22.0
13	13.0	1.1	73	72.7	6.4	33	132.5	11.6	93	192.3	16.8	53	252.0	22.1
14	13.9	1.2	74	73.7	6.4	34	133.5	11.7	94	193.3	16.9	54	253.0	22.1
15	14.9	1.3	75	74.7	6.5	35	134.5	11.8	95	194.3	17.0	55	254.0	22.2
16	15.9	1.4	76	75.7	6.6	36	135.5	11.9	96	195.3	17.1	56	255.0	22.3
17	16.9	1.5	77	76.7	6.7	37	136.5	11.9	97	196.3	17.2	57	256.0	22.4
18	17.9	1.6	78	77.7	6.8	38	137.5	12.0	98	197.2	17.3	58	257.0	22.5
19	18.9	1.7	79	78.7	6.9	39	138.5	12.1	99	198.2	17.3	59	258.0	22.6
20	19.9	1.7	80	79.7	7.0	40	139.5	12.2	200	199.2	17.4	60	259.0	22.7
21	20.9	1.8	81	80.7	7.1	141	140.5	12.3	201	200.2	17.5	261	260.0	22.7
22	21.9	1.9	82	81.7	7.1	42	141.5	12.4	02	201.2	17.6	62	261.0	22.8
23	22.9	2.0	83	82.7	7.2	43	142.5	12.5	03	202.2	17.7	63	262.0	22.9
24	23.9	2.1	84	83.7	7.3	44	143.5	12.6	04	203.2	17.8	64	263.0	23.0
25	24.9	2.2	85	84.7	7.4	45	144.4	12.6	05	204.2	17.9	65	264.0	23.1
26	25.9	2.3	86	85.7	7.5	46	145.4	12.7	06	205.2	18.0	66	265.0	23.2
27	26.9	2.4	87	86.7	7.6	47	146.4	12.8	07	206.2	18.0	67	266.0	23.3
28	27.9	2.4	88	87.7	7.7	48	147.4	12.9	08	207.2	18.1	68	267.0	23.4
29	28.9	2.5	89	88.7	7.8	49	148.4	13.0	09	208.2	18.2	69	268.0	23.4
30	29.9	2.6	90	89.7	7.8	50	149.4	13.1	10	209.2	18.3	70	269.0	23.5
31	30.9	2.7	91	90.7	7.9	151	150.4	13.2	211	210.2	18.4	271	270.0	23.6
32	31.9	2.8	92	91.6	8.0	52	151.4	13.2	12	211.2	18.5	72	271.0	23.7
33	32.9	2.9	93	92.6	8.1	53	152.4	13.3	13	212.2	18.6	73	272.0	23.8
34	33.9	3.0	94	93.6	8.2	54	153.4	13.4	14	213.2	18.7	74	273.0	23.9
35	34.9	3.1	95	94.6	8.3	55	154.4	13.5	15	214.2	18.7	75	274.0	24.0
36	35.9	3.1	96	95.6	8.4	56	155.4	13.6	16	215.2	18.8	76	274.9	24.1
37	36.9	3.2	97	96.6	8.5	57	156.4	13.7	17	216.2	18.9	77	275.9	24.1
38	37.9	3.3	98	97.6	8.5	58	157.4	13.8	18	217.2	19.0	78	276.9	24.2
39	38.9	3.4	99	98.6	8.6	59	158.4	13.9	19	218.2	19.1	79	277.9	24.3
40	39.8	3.5	100	99.6	8.7	60	159.4	13.9	20	219.2	19.2	80	278.9	24.4
41	40.8	3.6	101	100.6	8.8	161	160.4	14.0	221	220.2	19.3	281	279.9	24.5
42	41.8	3.7	02	101.6	8.9	62	161.4	14.1	22	221.2	19.3	82	280.9	24.6
43	42.8	3.7	03	102.6	9.0	63	162.4	14.2	23	222.2	19.4	83	281.9	24.7
44	43.8	3.8	04	103.6	9.1	64	163.4	14.3	24	223.1	19.5	84	282.9	24.8
45	44.8	3.9	05	104.6	9.2	65	164.4	14.4	25	224.1	19.6	85	283.9	24.8
46	45.8	4.0	06	105.6	9.2	66	165.4	14.5	26	225.1	19.7	86	284.9	24.9
47	46.8	4.1	07	106.6	9.3	67	166.4	14.6	27	226.1	19.8	87	285.9	25.0
48	47.8	4.2	08	107.6	9.4	68	167.4	14.6	28	227.1	19.9	88	286.9	25.1
49	48.8	4.3	09	108.6	9.5	69	168.4	14.7	29	228.1	20.0	89	287.9	25.2
50	49.8	4.4	10	109.6	9.6	70	169.4	14.8	30	229.1	20.0	90	288.9	25.3
51	50.8	4.4	111	110.6	9.7	171	170.3	14.9	231	230.1	20.1	291	289.9	25.4
52	51.8	4.5	12	111.6	9.8	72	171.3	15.0	32	231.1	20.2	92	290.9	25.4
53	52.8	4.6	13	112.6	9.8	73	172.3	15.1	33	232.1	20.3	93	291.9	25.5
54	53.8	4.7	14	113.6	9.9	74	173.3	15.2	34	233.1	20.4	94	292.9	25.6
55	54.8	4.8	15	114.6	10.0	75	174.3	15.3	35	234.1	20.5	95	293.9	25.7
56	55.8	4.9	16	115.6	10.1	76	175.3	15.3	36	235.1	20.6	96	294.9	25.8
57	56.8	5.0	17	116.6	10.2	77	176.3	15.4	37	236.1	20.7	97	295.9	25.9
58	57.8	5.1	18	117.6	10.3	78	177.3	15.5	38	237.1	20.7	98	296.9	26.0
59	58.8	5.1	19	118.5	10.4	79	178.3	15.6	39	238.1	20.8	99	297.9	26.1
60	59.8	5.2	20	119.5	10.5	80	179.3	15.7	40	239.1	20.9	300	298.9	26.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

85° (95°, 265°, 275°).

Difference of Latitude and Departure for 5° (175°, 185°, 355°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	299.9	26.2	361	359.6	31.5	421	419.4	36.7	481	479.2	41.9	541	538.9	47.2
02	300.8	26.3	62	360.6	31.6	22	420.4	36.8	82	480.2	42.0	42	539.9	47.3
03	301.8	26.4	63	361.6	31.6	23	421.4	36.9	83	481.2	42.1	43	540.9	47.4
04	302.8	26.5	64	362.6	31.7	24	422.4	37.0	84	482.2	42.2	44	541.9	47.5
05	303.8	26.6	65	363.6	31.8	25	423.4	37.1	85	483.2	42.3	45	542.9	47.6
06	304.8	26.7	66	364.6	31.9	26	424.4	37.1	86	484.1	42.4	46	543.9	47.7
07	305.8	26.8	67	365.6	32.0	27	425.4	37.2	87	485.1	42.4	47	544.9	47.7
08	306.8	26.9	68	366.6	32.1	28	426.4	37.3	88	486.1	42.5	48	545.9	47.8
09	307.8	26.9	69	367.6	32.2	29	427.4	37.4	89	487.1	42.6	49	546.9	47.9
10	308.8	27.0	70	368.6	32.3	30	428.4	37.5	90	488.1	42.7	50	547.9	48.0
311	309.8	27.1	371	369.6	32.3	431	429.4	37.6	491	489.1	42.8	551	548.9	48.1
12	310.8	27.2	72	370.6	32.4	32	430.4	37.7	92	490.1	42.9	52	549.9	48.2
13	311.8	27.3	73	371.6	32.5	33	431.3	37.7	93	491.1	43.0	53	550.9	48.3
14	312.8	27.4	74	372.6	32.6	34	432.3	37.8	94	492.1	43.1	54	551.9	48.4
15	313.8	27.5	75	373.6	32.7	35	433.3	37.9	95	493.1	43.1	55	552.9	48.4
16	314.8	27.5	76	374.6	32.8	36	434.3	38.0	96	494.1	43.2	56	553.9	48.5
17	315.8	27.6	77	375.6	32.9	37	435.3	38.1	97	495.1	43.3	57	554.9	48.6
18	316.8	27.7	78	376.6	33.0	38	436.3	38.2	98	496.1	43.4	58	555.9	48.7
19	317.8	27.8	79	377.6	33.0	39	437.3	38.3	99	497.1	43.5	59	556.9	48.8
20	318.8	27.9	80	378.6	33.1	40	438.3	38.4	500	498.1	43.6	60	557.9	48.8
321	319.8	28.0	381	379.5	33.2	441	439.3	38.4	501	499.1	43.7	561	558.8	48.9
22	320.8	28.1	82	380.5	33.3	42	440.3	38.5	02	500.1	43.8	62	559.8	49.0
23	321.8	28.2	83	381.5	33.4	43	441.3	38.6	03	501.1	43.8	63	560.8	49.1
24	322.8	28.2	84	382.5	33.5	44	442.3	38.7	04	502.1	43.9	64	561.8	49.2
25	323.8	28.3	85	383.5	33.6	45	443.3	38.8	05	503.1	44.0	65	562.8	49.3
26	324.8	28.4	86	384.5	33.7	46	444.3	38.9	06	504.1	44.1	66	563.8	49.4
27	325.8	28.5	87	385.5	33.7	47	445.3	39.0	07	505.1	44.2	67	564.8	49.5
28	326.7	28.6	88	386.5	33.8	48	446.3	39.1	08	506.1	44.3	68	565.8	49.6
29	327.7	28.7	89	387.5	33.9	49	447.3	39.1	09	507.1	44.4	69	566.8	49.7
30	328.7	28.8	90	388.5	34.0	50	448.3	39.2	10	508.1	44.5	70	567.8	49.7
331	329.7	28.9	391	389.5	34.1	451	449.3	39.3	511	509.0	44.5	571	568.8	49.8
32	330.7	28.9	92	390.5	34.2	52	450.3	39.4	12	510.0	44.6	72	569.8	49.9
33	331.7	29.0	93	391.5	34.3	53	451.3	39.5	13	511.0	44.7	73	570.8	50.0
34	332.7	29.1	94	392.5	34.3	54	452.3	39.6	14	512.0	44.8	74	571.8	50.1
35	333.7	29.2	95	393.5	34.4	55	453.3	39.7	15	513.0	44.9	75	572.8	50.2
36	334.7	29.3	96	394.5	34.5	56	454.3	39.8	16	514.0	45.0	76	573.8	50.3
37	335.7	29.4	97	395.5	34.6	57	455.3	39.8	17	515.0	45.1	77	574.8	50.4
38	336.7	29.5	98	396.5	34.7	58	456.3	39.9	18	516.0	45.2	78	575.8	50.4
39	337.7	29.6	99	397.5	34.8	59	457.3	40.0	19	517.0	45.2	79	576.8	50.5
40	338.7	29.6	400	398.5	34.9	60	458.2	40.1	20	518.0	45.3	80	577.8	50.6
341	339.7	29.7	401	399.5	35.0	461	459.2	40.2	521	519.0	45.4	581	578.8	50.7
42	340.7	29.8	02	400.5	35.0	62	460.2	40.3	22	520.0	45.5	82	579.8	50.8
43	341.7	29.9	03	401.5	35.1	63	461.2	40.4	23	521.0	45.6	83	580.8	50.9
44	342.7	30.0	04	402.5	35.2	64	462.2	40.4	24	522.0	45.7	84	581.8	50.9
45	343.7	30.1	05	403.5	35.3	65	463.2	40.5	25	523.0	45.8	85	582.8	51.0
46	344.7	30.2	06	404.5	35.4	66	464.2	40.6	26	524.0	45.9	86	583.8	51.1
47	345.7	30.3	07	405.4	35.5	67	465.2	40.7	27	525.0	45.9	87	584.8	51.2
48	346.7	30.3	08	406.4	35.6	68	466.2	40.8	28	526.0	46.0	88	585.8	51.3
49	347.7	30.4	09	407.4	35.7	69	467.2	40.9	29	527.0	46.1	89	586.8	51.4
50	348.7	30.5	10	408.4	35.7	70	468.2	41.0	30	528.0	46.2	90	587.8	51.5
351	349.7	30.6	411	409.4	35.8	471	469.2	41.1	531	529.0	46.3	591	588.7	51.6
52	350.7	30.7	12	410.4	35.9	72	470.2	41.1	32	530.0	46.4	92	589.7	51.6
53	351.7	30.8	13	411.4	36.0	73	471.2	41.2	33	531.0	46.5	93	590.7	51.7
54	352.6	30.9	14	412.4	36.1	74	472.2	41.3	34	532.0	46.6	94	591.7	51.8
55	353.6	30.9	15	413.4	36.2	75	473.2	41.4	35	533.0	46.6	95	592.7	51.9
56	354.6	31.0	16	414.4	36.3	76	474.2	41.5	36	533.9	46.7	96	593.7	52.0
57	355.6	31.1	17	415.4	36.4	77	475.2	41.6	37	534.9	46.8	97	594.7	52.1
58	356.6	31.2	18	416.4	36.4	78	476.2	41.7	38	535.9	46.9	98	595.7	52.2
59	357.6	31.3	19	417.4	36.5	79	477.2	41.8	39	536.9	47.0	99	596.7	52.3
60	358.6	31.4	20	418.4	36.6	80	478.2	41.8	40	537.9	47.1	600	597.7	52.3
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

85° (95°, 265°, 275°).

TABLE 2.

Difference of Latitude and Departure for 6° (174°, 186°, 354°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.1	61	60.7	6.4	121	120.3	12.6	181	180.0	18.9	241	239.7	25.2
2	2.0	0.2	62	61.7	6.5	22	121.3	12.8	82	181.0	19.0	42	240.7	25.3
3	3.0	0.3	63	62.7	6.6	23	122.3	12.9	83	182.0	19.1	43	241.7	25.4
4	4.0	0.4	64	63.6	6.7	24	123.3	13.0	84	183.0	19.2	44	242.7	25.5
5	5.0	0.5	65	64.6	6.8	25	124.3	13.1	85	184.0	19.3	45	243.7	25.6
6	6.0	0.6	66	65.6	6.9	26	125.3	13.2	86	185.0	19.4	46	244.7	25.7
7	7.0	0.7	67	66.6	7.0	27	126.3	13.3	87	186.0	19.5	47	245.6	25.8
8	8.0	0.8	68	67.6	7.1	28	127.3	13.4	88	187.0	19.7	48	246.6	25.9
9	9.0	0.9	69	68.6	7.2	29	128.3	13.5	89	188.0	19.8	49	247.6	26.0
10	9.9	1.0	70	69.6	7.3	30	129.3	13.6	90	189.0	19.9	50	248.6	26.1
11	10.9	1.1	71	70.6	7.4	131	130.3	13.7	191	190.0	20.0	251	249.6	26.2
12	11.9	1.3	72	71.6	7.5	32	131.3	13.8	92	190.9	20.1	52	250.6	26.3
13	12.9	1.4	73	72.6	7.6	33	132.3	13.9	93	191.9	20.2	53	251.6	26.4
14	13.9	1.5	74	73.6	7.7	34	133.3	14.0	94	192.9	20.3	54	252.6	26.6
15	14.9	1.6	75	74.6	7.8	35	134.3	14.1	95	193.9	20.4	55	253.6	26.7
16	15.9	1.7	76	75.6	7.9	36	135.3	14.2	96	194.9	20.5	56	254.6	26.8
17	16.9	1.8	77	76.6	8.0	37	136.2	14.3	97	195.9	20.6	57	255.6	26.9
18	17.9	1.9	78	77.6	8.2	38	137.2	14.4	98	196.9	20.7	58	256.6	27.0
19	18.9	2.0	79	78.6	8.3	39	138.2	14.5	99	197.9	20.8	59	257.6	27.1
20	19.9	2.1	80	79.6	8.4	40	139.2	14.6	200	198.9	20.9	60	258.6	27.2
21	20.9	2.2	81	80.6	8.5	141	140.2	14.7	201	199.9	21.0	261	259.6	27.3
22	21.9	2.3	82	81.6	8.6	42	141.2	14.8	02	200.9	21.1	62	260.6	27.4
23	22.9	2.4	83	82.5	8.7	43	142.2	14.9	03	201.9	21.2	63	261.6	27.5
24	23.9	2.5	84	83.5	8.8	44	143.2	15.1	04	202.9	21.3	64	262.6	27.6
25	24.9	2.6	85	84.5	8.9	45	144.2	15.2	05	203.9	21.4	65	263.5	27.7
26	25.9	2.7	86	85.5	9.0	46	145.2	15.3	06	204.9	21.5	66	264.5	27.8
27	26.9	2.8	87	86.5	9.1	47	146.2	15.4	07	205.9	21.6	67	265.5	27.9
28	27.8	2.9	88	87.5	9.2	48	147.2	15.5	08	206.9	21.7	68	266.5	28.0
29	28.8	3.0	89	88.5	9.3	49	148.2	15.6	09	207.9	21.8	69	267.5	28.1
30	29.8	3.1	90	89.5	9.4	50	149.2	15.7	10	208.8	22.0	70	268.5	28.2
31	30.8	3.2	91	90.5	9.5	151	150.2	15.8	211	209.8	22.1	271	269.5	28.3
32	31.8	3.3	92	91.5	9.6	52	151.2	15.9	12	210.8	22.2	72	270.5	28.4
33	32.8	3.4	93	92.5	9.7	53	152.2	16.0	13	211.8	22.3	73	271.5	28.5
34	33.8	3.6	94	93.5	9.8	54	153.2	16.1	14	212.8	22.4	74	272.5	28.6
35	34.8	3.7	95	94.5	9.9	55	154.2	16.2	15	213.8	22.5	75	273.5	28.7
36	35.8	3.8	96	95.5	10.0	56	155.1	16.3	16	214.8	22.6	76	274.5	28.8
37	36.8	3.9	97	96.5	10.1	57	156.1	16.4	17	215.8	22.7	77	275.5	29.0
38	37.8	4.0	98	97.5	10.2	58	157.1	16.5	18	216.8	22.8	78	276.5	29.1
39	38.8	4.1	99	98.5	10.3	59	158.1	16.6	19	217.8	22.9	79	277.5	29.2
40	39.8	4.2	100	99.5	10.5	60	159.1	16.7	20	218.8	23.0	80	278.5	29.3
41	40.8	4.3	101	100.4	10.6	161	160.1	16.8	221	219.8	23.1	281	279.5	29.4
42	41.8	4.4	02	101.4	10.7	62	161.1	16.9	22	220.8	23.2	82	280.5	29.5
43	42.8	4.5	03	102.4	10.8	63	162.1	17.0	23	221.8	23.3	83	281.4	29.6
44	43.8	4.6	04	103.4	10.9	64	163.1	17.1	24	222.8	23.4	84	282.4	29.7
45	44.8	4.7	05	104.4	11.0	65	164.1	17.2	25	223.8	23.5	85	283.4	29.8
46	45.7	4.8	06	105.4	11.1	66	165.1	17.4	26	224.8	23.6	86	284.4	29.9
47	46.7	4.9	07	106.4	11.2	67	166.1	17.5	27	225.8	23.7	87	285.4	30.0
48	47.7	5.0	08	107.4	11.3	68	167.1	17.6	28	226.8	23.8	88	286.4	30.1
49	48.7	5.1	09	108.4	11.4	69	168.1	17.7	29	227.7	23.9	89	287.4	30.2
50	49.7	5.2	10	109.4	11.5	70	169.1	17.8	30	228.7	24.0	90	288.4	30.3
51	50.7	5.3	111	110.4	11.6	171	170.1	17.9	231	229.7	24.1	291	289.4	30.4
52	51.7	5.4	12	111.4	11.7	72	171.1	18.0	32	230.7	24.3	92	290.4	30.5
53	52.7	5.5	13	112.4	11.8	73	172.1	18.1	33	231.7	24.4	93	291.4	30.6
54	53.7	5.6	14	113.4	11.9	74	173.0	18.2	34	232.7	24.5	94	292.4	30.7
55	54.7	5.7	15	114.4	12.0	75	174.0	18.3	35	233.7	24.6	95	293.4	30.8
56	55.7	5.9	16	115.4	12.1	76	175.0	18.4	36	234.7	24.7	96	294.4	30.9
57	56.7	6.0	17	116.4	12.2	77	176.0	18.5	37	235.7	24.8	97	295.4	31.0
58	57.7	6.1	18	117.4	12.3	78	177.0	18.6	38	236.7	24.9	98	296.4	31.1
59	58.7	6.2	19	118.3	12.4	79	178.0	18.7	39	237.7	25.0	99	297.4	31.3
60	59.7	6.3	20	119.3	12.5	80	179.0	18.8	40	238.7	25.1	300	298.4	31.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

84° (96°, 264°, 276°).

TABLE 2.

Difference of Latitude and Departure for 6° (174°, 186°, 354°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	299.3	31.5	361	359.0	37.7	421	418.7	44.0	481	478.4	50.3	541	538.0	56.5
02	300.3	31.6	62	360.0	37.8	22	419.7	44.1	82	479.4	50.4	42	539.0	56.6
03	301.3	31.7	63	361.0	37.9	23	420.7	44.2	83	480.4	50.5	43	540.0	56.7
04	302.3	31.8	64	362.0	38.0	24	421.7	44.3	84	481.3	50.6	44	541.0	56.8
05	303.3	31.9	65	363.0	38.1	25	422.7	44.4	85	482.3	50.7	45	542.0	56.9
06	304.3	32.0	66	364.0	38.3	26	423.7	44.5	86	483.3	50.8	46	543.0	57.0
07	305.3	32.1	67	365.0	38.4	27	424.7	44.6	87	484.3	50.9	47	544.0	57.1
08	306.3	32.2	68	366.0	38.5	28	425.7	44.7	88	485.3	51.0	48	545.0	57.2
09	307.3	32.3	69	367.0	38.6	29	426.6	44.8	89	486.3	51.1	49	546.0	57.3
10	308.3	32.4	70	368.0	38.7	30	427.6	44.9	90	487.3	51.2	50	547.0	57.4
311	309.3	32.5	371	369.0	38.8	431	428.6	45.0	491	488.3	51.3	551	548.0	57.5
12	310.3	32.6	72	370.0	38.9	32	429.6	45.2	92	489.3	51.4	52	549.0	57.6
13	311.3	32.7	73	371.0	39.0	33	430.6	45.3	93	490.3	51.5	53	550.0	57.7
14	312.3	32.8	74	371.9	39.1	34	431.6	45.4	94	491.3	51.6	54	551.0	57.9
15	313.3	32.9	75	372.9	39.2	35	432.6	45.5	95	492.3	51.7	55	552.0	58.0
16	314.3	33.0	76	373.9	39.3	36	433.6	45.6	96	493.3	51.8	56	553.0	58.1
17	315.3	33.1	77	374.9	39.4	37	434.6	45.7	97	494.3	51.9	57	554.0	58.2
18	316.3	33.2	78	375.9	39.5	38	435.6	45.8	98	495.3	52.0	58	555.0	58.3
19	317.3	33.3	79	376.9	39.6	39	436.6	45.9	99	496.3	52.1	59	556.0	58.4
20	318.2	33.4	80	377.9	39.7	40	437.6	46.0	500	497.3	52.3	60	556.9	58.5
321	319.2	33.6	381	378.9	39.8	441	438.6	46.1	501	498.3	52.4	561	557.9	58.6
22	320.2	33.7	82	379.9	39.9	42	439.6	46.2	02	499.3	52.5	62	558.9	58.7
23	321.2	33.8	83	380.9	40.0	43	440.6	46.3	03	500.2	52.6	63	559.9	58.8
24	322.2	33.9	84	381.9	40.1	44	441.6	46.4	04	501.2	52.7	64	560.9	59.0
25	323.2	34.0	85	382.9	40.2	45	442.6	46.5	05	502.2	52.8	65	561.9	59.1
26	324.2	34.1	86	383.9	40.3	46	443.6	46.6	06	503.2	52.9	66	562.9	59.2
27	325.2	34.2	87	384.9	40.5	47	444.5	46.7	07	504.2	53.0	67	563.9	59.3
28	326.2	34.3	88	385.9	40.6	48	445.5	46.8	08	505.2	53.1	68	564.9	59.4
29	327.2	34.4	89	386.9	40.7	49	446.5	46.9	09	506.2	53.2	69	565.9	59.5
30	328.2	34.5	90	387.9	40.8	50	447.5	47.0	10	507.2	53.3	70	566.9	59.6
331	329.2	34.6	391	388.9	40.9	451	448.5	47.1	511	508.2	53.4	571	567.9	59.7
32	330.2	34.7	92	389.9	41.0	52	449.5	47.2	12	509.2	53.5	72	568.9	59.8
33	331.2	34.8	93	390.8	41.1	53	450.5	47.3	13	510.2	53.6	73	569.9	59.9
34	332.2	34.9	94	391.8	41.2	54	451.5	47.5	14	511.2	53.7	74	570.9	60.0
35	333.2	35.0	95	392.8	41.3	55	452.5	47.6	15	512.2	53.8	75	571.9	60.1
36	334.2	35.1	96	393.8	41.4	56	453.5	47.7	16	513.2	53.9	76	572.9	60.2
37	335.2	35.2	97	394.8	41.5	57	454.5	47.8	17	514.2	54.0	77	573.9	60.3
38	336.1	35.3	98	395.8	41.6	58	455.5	47.9	18	515.2	54.1	78	574.9	60.4
39	337.1	35.4	99	396.8	41.7	59	456.5	48.0	19	516.2	54.2	79	575.8	60.5
40	338.1	35.5	400	397.8	41.8	60	457.5	48.1	20	517.2	54.3	80	576.8	60.6
341	339.1	35.6	401	398.8	41.9	461	458.5	48.2	521	518.1	54.5	581	577.8	60.7
42	340.1	35.7	02	399.8	42.0	62	459.5	48.3	22	519.1	54.6	82	578.8	60.8
43	341.1	35.8	03	400.8	42.1	63	460.5	48.4	23	520.1	54.7	83	579.8	60.9
44	342.1	36.0	04	401.8	42.2	64	461.5	48.5	24	521.1	54.8	84	580.8	61.1
45	343.1	36.1	05	402.8	42.3	65	462.5	48.6	25	522.1	54.9	85	581.8	61.2
46	344.1	36.2	06	403.8	42.4	66	463.4	48.7	26	523.1	55.0	86	582.8	61.3
47	345.1	36.3	07	404.8	42.5	67	464.4	48.8	27	524.1	55.1	87	583.8	61.4
48	346.1	36.4	08	405.8	42.6	68	465.4	48.9	28	525.1	55.2	88	584.8	61.5
49	347.1	36.5	09	406.8	42.7	69	466.4	49.0	29	526.1	55.3	89	585.8	61.6
50	348.1	36.6	10	407.8	42.9	70	467.4	49.1	30	527.1	55.4	90	586.8	61.7
351	349.1	36.7	411	408.7	43.0	471	468.4	49.2	531	528.1	55.5	591	587.8	61.8
52	350.1	36.8	12	409.7	43.1	72	469.4	49.3	32	529.1	55.6	92	588.8	61.9
53	351.1	36.9	13	410.7	43.2	73	470.4	49.4	33	530.1	55.7	93	589.8	62.0
54	352.1	37.0	14	411.7	43.3	74	471.4	49.5	34	531.1	55.8	94	590.8	62.1
55	353.1	37.1	15	412.7	43.4	75	472.4	49.6	35	532.1	55.9	95	591.8	62.2
56	354.0	37.2	16	413.7	43.5	76	473.4	49.8	36	533.1	56.0	96	592.8	62.3
57	355.0	37.3	17	414.7	43.6	77	474.4	49.9	37	534.1	56.1	97	593.8	62.4
58	356.0	37.4	18	415.7	43.7	78	475.4	50.0	38	535.1	56.2	98	594.7	62.5
59	357.0	37.5	19	416.7	43.8	79	476.4	50.1	39	536.1	56.3	99	595.7	62.6
60	358.0	37.6	20	417.7	43.9	80	477.4	50.2	40	537.1	56.4	600	596.7	62.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

84° (96°, 264°, 276°).

TABLE 2.

Difference of Latitude and Departure for 7° (173°, 187°, 353°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.1	61	60.5	7.4	121	120.1	14.7	181	179.7	22.1	241	239.2	29.4
2	2.0	0.2	62	61.5	7.6	22	121.1	14.9	82	180.6	22.2	42	240.2	29.5
3	3.0	0.4	63	62.5	7.7	23	122.1	15.0	83	181.6	22.3	43	241.2	29.6
4	4.0	0.5	64	63.5	7.8	24	123.1	15.1	84	182.6	22.4	44	242.2	29.7
5	5.0	0.6	65	64.5	7.9	25	124.1	15.2	85	183.6	22.5	45	243.2	29.9
6	6.0	0.7	66	65.5	8.0	26	125.1	15.4	86	184.6	22.7	46	244.2	30.0
7	6.9	0.9	67	66.5	8.2	27	126.1	15.5	87	185.6	22.8	47	245.2	30.1
8	7.9	1.0	68	67.5	8.3	28	127.0	15.6	88	186.6	22.9	48	246.2	30.2
9	8.9	1.1	69	68.5	8.4	29	128.0	15.7	89	187.6	23.0	49	247.1	30.3
10	9.9	1.2	70	69.5	8.5	30	129.0	15.8	90	188.6	23.2	50	248.1	30.5
11	10.9	1.3	71	70.5	8.7	131	130.0	16.0	191	189.6	23.3	251	249.1	30.6
12	11.9	1.5	72	71.5	8.8	32	131.0	16.1	92	190.6	23.4	52	250.1	30.7
13	12.9	1.6	73	72.5	8.9	33	132.0	16.2	93	191.6	23.5	53	251.1	30.8
14	13.9	1.7	74	73.4	9.0	34	133.0	16.3	94	192.6	23.6	54	252.1	31.0
15	14.9	1.8	75	74.4	9.1	35	134.0	16.5	95	193.5	23.8	55	253.1	31.1
16	15.9	1.9	76	75.4	9.3	36	135.0	16.6	96	194.5	23.9	56	254.1	31.2
17	16.9	2.1	77	76.4	9.4	37	136.0	16.7	97	195.5	24.0	57	255.1	31.3
18	17.9	2.2	78	77.4	9.5	38	137.0	16.8	98	196.5	24.1	58	256.1	31.4
19	18.9	2.3	79	78.4	9.6	39	138.0	16.9	99	197.5	24.3	59	257.1	31.6
20	19.9	2.4	80	79.4	9.7	40	139.0	17.1	200	198.5	24.4	60	258.1	31.7
21	20.8	2.6	81	80.4	9.9	141	139.9	17.2	201	199.5	24.5	261	259.1	31.8
22	21.8	2.7	82	81.4	10.0	42	140.9	17.3	02	200.5	24.6	62	260.0	31.9
23	22.8	2.8	83	82.4	10.1	43	141.9	17.4	03	201.5	24.7	63	261.0	32.1
24	23.8	2.9	84	83.4	10.2	44	142.9	17.5	04	202.5	24.9	64	262.0	32.2
25	24.8	3.0	85	84.4	10.4	45	143.9	17.7	05	203.5	25.0	65	263.0	32.3
26	25.8	3.2	86	85.4	10.5	46	144.9	17.8	06	204.5	25.1	66	264.0	32.4
27	26.8	3.3	87	86.4	10.6	47	145.9	17.9	07	205.5	25.2	67	265.0	32.5
28	27.8	3.4	88	87.3	10.7	48	146.9	18.0	08	206.4	25.3	68	266.0	32.7
29	28.8	3.5	89	88.3	10.8	49	147.9	18.2	09	207.4	25.5	69	267.0	32.8
30	29.8	3.7	90	89.3	11.0	50	148.9	18.3	10	208.4	25.6	70	268.0	32.9
31	30.8	3.8	91	90.3	11.1	151	149.9	18.4	211	209.4	25.7	271	269.0	33.0
32	31.8	3.9	92	91.3	11.2	52	150.9	18.5	12	210.4	25.8	72	270.0	33.1
33	32.8	4.0	93	92.3	11.3	53	151.9	18.6	13	211.4	26.0	73	271.0	33.3
34	33.7	4.1	94	93.3	11.5	54	152.9	18.8	14	212.4	26.1	74	272.0	33.4
35	34.7	4.3	95	94.3	11.6	55	153.8	18.9	15	213.4	26.2	75	273.0	33.5
36	35.7	4.4	96	95.3	11.7	56	154.8	19.0	16	214.4	26.3	76	273.9	33.6
37	36.7	4.5	97	96.3	11.8	57	155.8	19.1	17	215.4	26.4	77	274.9	33.8
38	37.7	4.6	98	97.3	11.9	58	156.8	19.3	18	216.4	26.6	78	275.9	33.9
39	38.7	4.8	99	98.3	12.1	59	157.8	19.4	19	217.4	26.7	79	276.9	34.0
40	39.7	4.9	100	99.3	12.2	60	158.8	19.5	20	218.4	26.8	80	277.9	34.1
41	40.7	5.0	101	100.2	12.3	161	159.8	19.6	221	219.4	26.9	281	278.9	34.2
42	41.7	5.1	02	101.2	12.4	62	160.8	19.7	22	220.3	27.1	82	279.9	34.4
43	42.7	5.2	03	102.2	12.6	63	161.8	19.9	23	221.3	27.2	83	280.9	34.5
44	43.7	5.4	04	103.2	12.7	64	162.8	20.0	24	222.3	27.3	84	281.9	34.6
45	44.7	5.5	05	104.2	12.8	65	163.8	20.1	25	223.3	27.4	85	282.9	34.7
46	45.7	5.6	06	105.2	12.9	66	164.8	20.2	26	224 3	27.5	86	283.9	34.9
47	46.6	5.7	07	106.2	13.0	67	165.8	20.4	27	225.3	27.7	87	284.9	35.0
48	47.6	5.8	08	107.2	13.2	68	166.7	20.5	28	226.3	27.8	88	285.9	35.1
49	48.6	6.0	09	108.2	13.3	69	167.7	20.6	29	227.3	27.9	89	286.8	35.2
50	49.6	6.1	10	109.2	13.4	70	168.7	20.7	30	228.3	28.0	90	287.8	35.3
51	50.6	6.2	111	110.2	13.5	171	169.7	20.8	231	229.3	28.2	291	288.8	35.5
52	51.6	6.3	12	111.2	13.6	72	170.7	21.0	32	230.3	28.3	92	289.8	35.6
53	52.6	6.5	13	112.2	13.8	73	171.7	21.1	33	231.3	28.4	93	290.8	35.7
54	53.6	6.6	14	113.2	13.9	74	172.7	21.2	34	232.3	28.5	94	291.8	35.8
55	54.6	6.7	15	114.1	14.0	75	173.7	21.3	35	233.2	28.6	95	292.8	36.0
56	55.6	6.8	16	115.1	14.1	76	174.7	21.4	36	234.2	28.8	96	293.8	36.1
57	56.6	6.9	17	116.1	14.3	77	175.7	21.6	37	235.2	28.9	97	294.8	36.2
58	57.6	7.1	18	117.1	14.4	78	176.7	21.7	38	236.2	29.0	98	295.8	36.3
59	58.6	7.2	19	118.1	14.5	79	177.7	21.8	39	237.2	29.1	99	296.8	36.4
60	59.6	7.3	20	119.1	14.6	80	178.7	21.9	40	238.2	29.2	300	297.8	36.6
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

83° (97°, 263°, 277°).

Difference of Latitude and Departure for 7° (173°, 187°, 353°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	298.7	36.7	361	358.3	44.0	421	417.9	51.3	481	477.4	58.6	541	537.0	65.9
02	299.7	36.8	62	359.3	44.1	22	418.8	51.4	82	478.4	58.7	42	537.9	66.0
03	300.7	36.9	63	360.3	44.2	23	419.8	51.5	83	479.4	58.8	43	538.9	66.2
04	301.7	37.0	64	361.3	44.4	24	420.8	51.7	84	480.4	59.0	44	539.9	66.3
05	302.7	37.2	65	362.3	44.5	25	421.8	51.8	85	481.4	59.1	45	540.9	66.4
06	303.7	37.3	66	363.3	44.6	26	422.8	51.9	86	482.4	59.2	46	541.9	66.6
07	304.7	37.4	67	364.3	44.7	27	423.8	52.0	87	483.4	59.4	47	542.9	66.7
08	305.7	37.5	68	365.2	44.8	28	424.8	52.2	88	484.3	59.5	48	543.9	66.8
09	306.7	37.7	69	366.2	45.0	29	425.8	52.3	89	485.3	59.6	49	544.9	66.9
10	307.7	37.8	70	367.2	45.1	30	426.8	52.4	90	486.3	59.7	50	545.9	67.0
311	308.7	37.9	371	368.2	45.2	431	427.8	52.5	491	487.3	59.8	551	546.9	67.1
12	309.7	38.0	72	369.2	45.3	32	428.8	52.6	92	488.3	59.9	52	547.9	67.2
13	310.7	38.1	73	370.2	45.5	33	429.8	52.8	93	489.3	60.1	53	548.9	67.4
14	311.7	38.3	74	371.2	45.6	34	430.8	52.9	94	490.3	60.2	54	549.9	67.5
15	312.6	38.4	75	372.2	45.7	35	431.7	53.0	95	491.3	60.3	55	550.8	67.6
16	313.6	38.5	76	373.2	45.8	36	432.7	53.1	96	492.3	60.5	56	551.8	67.8
17	314.6	38.6	77	374.2	45.9	37	433.7	53.3	97	493.3	60.6	57	552.8	67.9
18	315.6	38.7	78	375.2	46.1	38	434.7	53.4	98	494.3	60.7	58	553.8	68.0
19	316.6	38.9	79	376.2	46.2	39	435.7	53.5	99	495.3	60.8	59	554.8	68.1
20	317.6	39.0	80	377.2	46.3	40	436.7	53.6	500	496.3	61.0	60	555.8	68.3
321	318.6	39.1	381	378.1	46.4	441	437.7	53.7	501	497.2	61.1	561	556.8	68.4
22	319.6	39.2	82	379.1	46.5	42	438.7	53.9	02	498.2	61.2	62	557.8	68.5
23	320.6	39.4	83	380.1	46.7	43	439.7	54.0	03	499.2	61.3	63	558.8	68.6
24	321.6	39.5	84	381.1	46.8	44	440.7	54.1	04	500.2	61.4	64	559.8	68.7
25	322.6	39.6	85	382.1	46.9	45	441.7	54.2	05	501.2	61.5	65	560.8	68.9
26	323.6	39.7	86	383.1	47.0	46	442.7	54.3	06	502.2	61.6	66	561.8	69.0
27	324.6	39.8	87	384.1	47.2	47	443.7	54.5	07	503.2	61.8	67	562.8	69.1
28	325.5	40.0	88	385.1	47.3	48	444.7	54.6	08	504.2	61.9	68	563.8	69.2
29	326.5	40.1	89	386.1	47.4	49	445.6	54.7	09	505.2	62.0	69	564.8	69.3
30	327.5	40.2	90	387.1	47.5	50	446.6	54.8	10	506.2	62.1	70	565.8	69.4
331	328.5	40.3	391	388.1	47.6	451	447.6	55.0	511	507.2	62.3	571	566.7	69.6
32	329.5	40.5	92	389.1	47.8	52	448.6	55.1	12	508.2	62.4	72	567.7	69.7
33	330.5	40.6	93	390.1	47.9	53	449.6	55.2	13	509.2	62.5	73	568.7	69.8
34	331.5	40.7	94	391.1	48.0	54	450.6	55.3	14	510.2	62.6	74	569.7	69.9
35	332.5	40.8	95	392.0	48.1	55	451.6	55.4	15	511.1	62.7	75	570.7	70.1
36	333.5	40.9	96	393.0	48.3	56	452.6	55.6	16	512.1	62.9	76	571.7	70.2
37	334.5	41.1	97	394.0	48.4	57	453.6	55.7	17	513.1	63.0	77	572.7	70.3
38	335.5	41.2	98	395.0	48.5	58	454.6	55.8	18	514.1	63.1	78	573.7	70.4
39	336.5	41.3	99	396.0	48.6	59	455.6	55.9	19	515.1	63.2	79	574.7	70.5
40	337.5	41.4	400	397.0	48.7	60	456.6	56.1	20	516.1	63.4	80	575.7	70.7
341	338.4	41.6	401	398.0	48.9	461	457.6	56.2	521	517.1	63.5	581	576.7	70.8
42	339.4	41.7	02	399.0	49.0	62	458.5	56.3	22	518.1	63.6	82	577.6	70.9
43	340.4	41.8	03	400.0	49.1	63	459.5	56.4	23	519.1	63.7	83	578.6	71.0
44	341.4	41.9	04	401.0	49.2	64	460.5	56.5	24	520.1	63.8	84	579.6	71.2
45	342.4	42.0	05	402.0	49.4	65	461.5	56.7	25	521.1	64.0	85	580.6	71.3
46	343.4	42.2	06	403.0	49.5	66	462.5	56.8	26	522.1	64.1	86	581.6	71.4
47	344.4	42.3	07	404.0	49.6	67	463.5	56.9	27	523.1	64.2	87	582.6	71.5
48	345.4	42.4	08	405.0	49.7	68	464.5	57.0	28	524.1	64.3	88	583.6	71.6
49	346.4	42.5	09	405.9	49.8	69	465.5	57.2	29	525.0	64.5	89	584.6	71.8
50	347.4	42.6	10	406.9	50.0	70	466.5	57.3	30	526.0	64.6	90	585.6	71.9
351	348.4	42.8	411	407.9	50.1	471	467.5	57.4	531	527.0	64.7	591	586.6	72.0
52	349.4	42.9	12	408.9	50.2	72	468.5	57.5	32	528.0	64.8	92	587.6	72.1
53	350.4	43.0	13	409.9	50.3	73	469.5	57.6	33	529.0	64.9	93	588.6	72.2
54	351.4	43.1	14	410.9	50.4	74	470.5	57.8	34	530.0	65.1	94	589.6	72.4
55	352.3	43.3	15	411.9	50.6	75	471.5	57.9	35	531.0	65.2	95	590.6	72.5
56	353.3	43.4	16	412.9	50.7	76	472.4	58.0	36	532.0	65.3	96	591.5	72.6
57	354.3	43.5	17	413.9	50.8	77	473.4	58.1	37	533.0	65.4	97	592.5	72.7
58	355.3	43.6	18	414.9	50.9	78	474.4	58.2	38	534.0	65.6	98	593.5	72.9
59	356.3	43.7	19	415.9	51.1	79	475.4	58.4	39	535.0	65.7	99	594.5	73.0
60	357.3	43.9	20	416.9	51.2	80	476.4	58.5	40	536.0	65.8	600	595.5	73.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

83° (97°, 263°, 277°).

TABLE 2.

Difference of Latitude and Departure for 8° (172°, 188°, 352°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.1	61	60.4	8.5	121	119.8	16.8	181	179.2	25.2	241	238.7	33.5
2	2.0	0.3	62	61.4	8.6	22	120.8	17.0	82	180.2	25.3	42	239.6	33.7
3	3.0	0.4	63	62.4	8.8	23	121.8	17.1	83	181.2	25.5	43	240.6	33.8
4	4.0	0.6	64	63.4	8.9	24	122.8	17.3	84	182.2	25.6	44	241.6	34.0
5	5.0	0.7	65	64.4	9.0	25	123.8	17.4	85	183.2	25.7	45	242.6	34.1
6	5.9	0.8	66	65.4	9.2	26	124.8	17.5	86	184.2	25.9	46	243.6	34.2
7	6.9	1.0	67	66.3	9.3	27	125.8	17.7	87	185.2	26.0	47	244.6	34.4
8	7.9	1.1	68	67.3	9.5	28	126.8	17.8	88	186.2	26.2	48	245.6	34.5
9	8.9	1.3	69	68.3	9.6	29	127.7	18.0	89	187.2	26.3	49	246.6	34.7
10	9.9	1.4	70	69.3	9.7	30	128.7	18.1	90	188.2	26.4	50	247.6	34.8
11	10.9	1.5	71	70.3	9.9	131	129.7	18.2	191	189.1	26.6	251	248.6	34.9
12	11.9	1.7	72	71.3	10.0	32	130.7	18.4	92	190.1	26.7	52	249.5	35.1
13	12.9	1.8	73	72.3	10.2	33	131.7	18.5	93	191.1	26.9	53	250.5	35.2
14	13.9	1.9	74	73.3	10.3	34	132.7	18.6	94	192.1	27.0	54	251.5	35.3
15	14.9	2.1	75	74.3	10.4	35	133.7	18.8	95	193.1	27.1	55	252.5	35.5
16	15.8	2.2	76	75.3	10.6	36	134.7	18.9	96	194.1	27.3	56	253.5	35.6
17	16.8	2.4	77	76.3	10.7	37	135.7	19.1	97	195.1	27.4	57	254.5	35.8
18	17.8	2.5	78	77.2	10.9	38	136.7	19.2	98	196.1	27.6	58	255.5	35.9
19	18.8	2.6	79	78.2	11.0	39	137.7	19.3	99	197.1	27.7	59	256.5	36.0
20	19.8	2.8	80	79.2	11.1	40	138.6	19.5	200	198.1	27.8	60	257.5	36.2
21	20.8	2.9	81	80.2	11.3	141	139.6	19.6	201	199.0	28.0	261	258.5	36.3
22	21.8	3.1	82	81.2	11.4	42	140.6	19.8	02	200.0	28.1	62	259.5	36.5
23	22.8	3.2	83	82.2	11.6	43	141.6	19.9	03	201.0	28.3	63	260.4	36.6
24	23.8	3.3	84	83.2	11.7	44	142.6	20.0	04	202.0	28.4	64	261.4	36.7
25	24.8	3.5	85	84.2	11.8	45	143.6	20.2	05	203.0	28.5	65	262.4	36.9
26	25.7	3.6	86	85.2	12.0	46	144.6	20.3	06	204.0	28.7	66	263.4	37.0
27	26.7	3.8	87	86.2	12.1	47	145.6	20.5	07	205.0	28.8	67	264.4	37.2
28	27.7	3.9	88	87.1	12.2	48	146.6	20.6	08	206.0	28.9	68	265.4	37.3
29	28.7	4.0	89	88.1	12.4	49	147.5	20.7	09	207.0	29.1	69	266.4	37.4
30	29.7	4.2	90	89.1	12.5	50	148.5	20.9	10	208.0	29.2	70	267.4	37.6
31	30.7	4.3	91	90.1	12.7	151	149.5	21.0	211	208.9	29.4	271	268.4	37.7
32	31.7	4.5	92	91.1	12.8	52	150.5	21.2	12	209.9	29.5	72	269.4	37.9
33	32.7	4.6	93	92.1	12.9	53	151.5	21.3	13	210.9	29.6	73	270.3	38.0
34	33.7	4.7	94	93.1	13.1	54	152.5	21.4	14	211.9	29.8	74	271.3	38.1
35	34.7	4.9	95	94.1	13.2	55	153.5	21.6	15	212.9	29.9	75	272.3	38.3
36	35.6	5.0	96	95.1	13.4	56	154.5	21.7	16	213.9	30.1	76	273.3	38.4
37	36.6	5.1	97	96.1	13.5	57	155.5	21.9	17	214.9	30.2	77	274.3	38.6
38	37.6	5.3	98	97.0	13.6	58	156.5	22.0	18	215.9	30.3	78	275.3	38.7
39	38.6	5.4	99	98.0	13.8	59	157.5	22.1	19	216.9	30.5	79	276.3	38.8
40	39.6	5.6	100	99.0	13.9	60	158.4	22.3	20	217.9	30.6	80	277.3	39.0
41	40.6	5.7	101	100.0	14.1	161	159.4	22.4	221	218.8	30.8	281	278.3	39.1
42	41.6	5.8	02	101.0	14.2	62	160.4	22.5	22	219.8	30.9	82	279.3	39.2
43	42.6	6.0	03	102.0	14.3	63	161.4	22.7	23	220.8	31.0	83	280.2	39.4
44	43.6	6.1	04	103.0	14.5	64	162.4	22.8	24	221.8	31.2	84	281.2	39.5
45	44.6	6.3	05	104.0	14.6	65	163.4	23.0	25	222.8	31.3	85	282.2	39.7
46	45.6	6.4	06	105.0	14.8	66	164.4	23.1	26	223.8	31.5	86	283.2	39.8
47	46.5	6.5	07	106.0	14.9	67	165.4	23.2	27	224.8	31.6	87	284.2	39.9
48	47.5	6.7	08	106.9	15.0	68	166.4	23.4	28	225.8	31.7	88	285.2	40.1
49	48.5	6.8	09	107.9	15.2	69	167.4	23.5	29	226.8	31.9	89	286.2	40.2
50	49.5	7.0	10	108.9	15.3	70	168.3	23.7	30	227.8	32.0	90	287.2	40.4
51	50.5	7.1	111	109.9	15.4	171	169.3	23.8	231	228.8	32.1	291	288.2	40.5
52	51.5	7.2	12	110.9	15.6	72	170.3	23.9	32	229.7	32.3	92	289.2	40.6
53	52.5	7.4	13	111.9	15.7	73	171.3	24.1	33	230.7	32.4	93	290.1	40.8
54	53.5	7.5	14	112.9	15.9	74	172.3	24.2	34	231.7	32.6	94	291.1	40.9
55	54.5	7.7	15	113.9	16.0	75	173.3	24.4	35	232.7	32.7	95	292.1	41.1
56	55.5	7.8	16	114.9	16.1	76	174.3	24.5	36	233.7	32.8	96	293.1	41.2
57	56.4	7.9	17	115.9	16.3	77	175.3	24.6	37	234.7	33.0	97	294.1	41.3
58	57.4	8.1	18	116.9	16.4	78	176.3	24.8	38	235.7	33.1	98	295.1	41.5
59	58.4	8.2	19	117.8	16.6	79	177.3	24.9	39	236.7	33.3	99	296.1	41.6
60	59.4	8.4	20	118.8	16.7	80	178.2	25.1	40	237.7	33.4	300	297.1	41.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

82° (98°, 262°, 278°).

TABLE 2.

Difference of Latitude and Departure for 8° (172°, 188°, 352°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	298.0	41.9	361	357.5	50.2	421	416.9	58.6	481	476.3	66.9	541	535.7	75.2
02	299.0	42.0	62	358.5	50.4	22	417.9	58.7	82	477.3	67.1	42	536.7	75.4
03	300.0	42.2	63	359.4	50.5	23	418.9	58.9	83	478.3	67.2	43	537.7	75.5
04	301.0	42.3	64	360.4	50.7	24	419.8	59.0	84	479.3	67.4	44	538.7	75.7
05	302.0	42.5	65	361.4	50.8	25	420.8	59.2	85	480.3	67.5	45	539.7	75.8
06	303.0	42.6	66	362.4	50.9	26	421.8	59.3	86	481.2	67.6	46	540.6	75.9
07	304.0	42.7	67	363.4	51.1	27	422.8	59.4	87	482.2	67.8	47	541.6	76.1
08	305.0	42.9	68	364.4	51.2	28	423.8	59.6	88	483.2	67.9	48	542.6	76.2
09	306.0	43.0	69	365.4	51.4	29	424.8	59.7	89	484.2	68.1	49	543.6	76.4
10	307.0	43.1	70	366.4	51.5	30	425.8	59.8	90	485.2	68.2	50	544.6	76.5
311	307.9	43.3	371	367.4	51.6	431	426.8	60.0	491	486.2	68.3	551	545.6	76.6
12	308.9	43.4	72	368.4	51.8	32	427.8	60.1	92	487.2	68.5	52	546.6	76.8
13	309.9	43.6	73	369.3	51.9	33	428.8	60.3	93	488.2	68.6	53	547.6	76.9
14	310.9	43.7	74	370.3	52.1	34	429.8	60.4	94	489.2	68.8	54	548.6	77.1
15	311.9	43.8	75	371.3	52.2	35	430.7	60.5	95	490.2	68.9	55	549.6	77.2
16	312.9	44.0	76	372.3	52.3	36	431.7	60.7	96	491.2	69.0	56	550.6	77.4
17	313.9	44.1	77	373.3	52.5	37	432.7	60.8	97	492.1	69.2	57	551.5	77.5
18	314.9	44.3	78	374.3	52.6	38	433.7	61.0	98	493.1	69.3	58	552.5	77.6
19	315.9	44.4	79	375.3	52.7	39	434.7	61.1	99	494.1	69.5	59	553.5	77.8
20	316.9	44.5	80	376.3	52.9	40	435.7	61.2	500	495.1	69.6	60	554.5	77.9
321	317.9	44.7	381	377.3	53.0	441	436.7	61.4	501	496.1	69.7	561	555.5	78.1
22	318.8	44.8	82	378.3	53.2	42	437.7	61.5	02	497.1	69.9	62	556.5	78.2
23	319.8	45.0	83	379.2	53.3	43	438.7	61.7	03	498.1	70.0	63	557.5	78.3
24	320.8	45.1	84	380.2	53.4	44	439.7	61.8	04	499.1	70.2	64	558.5	78.5
25	321.8	45.2	85	381.2	53.6	45	440.6	61.9	05	500.1	70.3	65	559.5	78.6
26	322.8	45.4	86	382.2	53.7	46	441.6	62.1	06	501.0	70.4	66	560.5	78.8
27	323.8	45.5	87	383.2	53.9	47	442.6	62.2	07	502.0	70.6	67	561.5	78.9
28	324.8	45.7	88	384.2	54.0	48	443.6	62.4	08	503.0	70.7	68	562.5	79.0
29	325.8	45.8	89	385.2	54.1	49	444.6	62.5	09	504.0	70.8	69	563.5	79.1
30	326.8	45.9	90	386.2	54.3	50	445.6	62.6	10	505.0	70.9	70	564.5	79.3
331	327.8	46.1	391	387.2	54.4	451	446.6	62.8	511	506.0	71.1	571	565.4	79.4
32	328.7	46.2	92	388.2	54.6	52	447.6	62.9	12	507.0	71.2	72	566.4	79.6
33	329.7	46.3	93	389.1	54.7	53	448.6	63.0	13	508.0	71.4	73	567.4	79.7
34	330.7	46.5	94	390.1	54.8	54	449.6	63.2	14	509.0	71.5	74	568.4	79.8
35	331.7	46.6	95	391.1	55.0	55	450.5	63.3	15	510.0	71.6	75	569.4	80.0
36	332.7	46.8	96	392.1	55.1	56	451.5	63.5	16	510.9	71.8	76	570.4	80.1
37	333.7	46.9	97	393.1	55.3	57	452.5	63.6	17	511.9	71.9	77	571.4	80.2
38	334.7	47.0	98	394.1	55.4	58	453.5	63.7	18	512.9	72.0	78	572.4	80.4
39	335.7	47.2	99	395.1	55.5	59	454.5	63.9	19	513.9	72.2	79	573.4	80.5
40	336.7	47.3	400	396.1	55.7	60	455.5	64.0	20	514.9	72.3	80	574.4	80.6
341	337.7	47.5	401	397.1	55.8	461	456.5	64.2	521	515.9	72.4	581	575.4	80.8
42	338.6	47.6	02	398.1	56.0	62	457.5	64.3	22	516.9	72.6	82	576.4	80.9
43	339.6	47.7	03	399.1	56.1	63	458.5	64.4	23	517.9	72.8	83	577.4	81.1
44	340.6	47.9	04	400.0	56.2	64	459.5	64.6	24	518.9	73.0	84	578.4	81.3
45	341.6	48.0	05	401.0	56.4	65	460.4	64.7	25	519.9	73.1	85	579.4	81.4
46	342.6	48.2	06	402.0	56.5	66	461.4	64.9	26	520.9	73.2	86	580.3	81.6
47	343.6	48.3	07	403.0	56.6	67	462.4	65.0	27	521.8	73.4	87	581.3	81.7
48	344.6	48.4	08	404.0	56.8	68	463.4	65.1	28	522.8	73.5	88	582.3	81.8
49	345.6	48.6	09	405.0	56.9	69	464.4	65.3	29	523.8	73.7	89	583.3	82.0
50	346.6	48.7	10	406.0	57.1	70	465.4	65.4	30	524.8	73.8	90	584.3	82.1
351	347.6	48.9	411	407.0	57.2	471	466.4	65.6	531	525.8	73.9	591	585.3	82.2
52	348.5	49.0	12	408.0	57.3	72	467.4	65.7	32	526.8	74.1	92	586.3	82.4
53	349.5	49.1	13	409.0	57.5	73	468.4	65.8	33	527.8	74.2	93	587.3	82.5
54	350.5	49.3	14	409.9	57.6	74	469.4	66.0	34	528.8	74.3	94	588.3	82.6
55	351.5	49.4	15	410.9	57.8	75	470.4	66.1	35	529.8	74.5	95	589.3	82.8
56	352.5	49.5	16	411.9	57.9	76	471.3	66.2	36	530.8	74.6	96	590.3	83.0
57	353.5	49.7	17	412.9	58.0	77	472.3	66.4	37	531.7	74.7	97	591.2	83.1
58	354.5	49.8	18	413.9	58.2	78	473.3	66.5	38	532.7	74.9	98	592.2	83.2
59	355.5	50.0	19	414.9	58.3	79	474.3	66.7	39	533.7	75.0	99	593.2	83.3
60	356.5	50.1	20	415.9	58.5	80	475.3	66.8	40	534.7	75.1	600	594.2	83.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

82° (98°, 262°, 278°).

TABLE 2.

Difference of Latitude and Departure for 9° (171°, 189°, 351°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.2	61	60.2	9.5	121	119.5	18.9	181	178.8	28.3	241	238.0	37.7
2	2.0	0.3	62	61.2	9.7	22	120.5	19.1	82	179.8	28.5	42	239.0	37.9
3	3.0	0.5	63	62.2	9.9	23	121.5	19.2	83	180.7	28.6	43	240.0	38.0
4	4.0	0.6	64	63.2	10.0	24	122.5	19.4	84	181.7	28.8	44	241.0	38.2
5	4.9	0.8	65	64.2	10.2	25	123.5	19.6	85	182.7	28.9	45	242.0	38.3
6	5.9	0.9	66	65.2	10.3	26	124.4	19.7	86	183.7	29.1	46	243.0	38.5
7	6.9	1.1	67	66.2	10.5	27	125.4	19.9	87	184.7	29.3	47	244.0	38.6
8	7.9	1.3	68	67.2	10.6	28	126.4	20.0	88	185.7	29.4	48	244.9	38.8
9	8.9	1.4	69	68.2	10.8	29	127.4	20.2	89	186.7	29.6	49	245.9	39.0
10	9.9	1.6	70	69.1	11.0	30	128.4	20.3	90	187.7	29.7	50	246.9	39.1
11	10.9	1.7	71	70.1	11.1	131	129.4	20.5	191	188.6	29.9	251	247.9	39.3
12	11.9	1.9	72	71.1	11.3	32	130.4	20.6	92	189.6	30.0	52	248.9	39.4
13	12.8	2.0	73	72.1	11.4	33	131.4	20.8	93	190.6	30.2	53	249.9	39.6
14	13.8	2.2	74	73.1	11.6	34	132.4	21.0	94	191.6	30.3	54	250.9	39.7
15	14.8	2.3	75	74.1	11.7	35	133.3	21.1	95	192.6	30.5	55	251.9	39.9
16	15.8	2.5	76	75.1	11.9	36	134.3	21.3	96	193.6	30.7	56	252.8	40.0
17	16.8	2.7	77	76.1	12.0	37	135.3	21.4	97	194.6	30.8	57	253.8	40.2
18	17.8	2.8	78	77.0	12.2	38	136.3	21.6	98	195.6	31.0	58	254.8	40.4
19	18.8	3.0	79	78.0	12.4	39	137.3	21.7	99	196.5	31.1	59	255.8	40.5
20	19.8	3.1	80	79.0	12.5	40	138.3	21.9	200	197.5	31.3	60	256.8	40.7
21	20.7	3.3	81	80.0	12.7	141	139.3	22.1	201	198.5	31.4	261	257.8	40.8
22	21.7	3.4	82	81.0	12.8	42	140.3	22.2	02	199.5	31.6	62	258.8	41.0
23	22.7	3.6	83	82.0	13.0	43	141.2	22.4	03	200.5	31.8	63	259.8	41.1
24	23.7	3.8	84	83.0	13.1	44	142.2	22.5	04	201.5	31.9	64	260.7	41.3
25	24.7	3.9	85	84.0	13.3	45	143.2	22.7	05	202.5	32.1	65	261.7	41.5
26	25.7	4.1	86	84.9	13.5	46	144.2	22.8	06	203.5	32.2	66	262.7	41.6
27	26.7	4.2	87	85.9	13.6	47	145.2	23.0	07	204.5	32.4	67	263.7	41.8
28	27.7	4.4	88	86.9	13.8	48	146.2	23.2	08	205.4	32.5	68	264.7	41.9
29	28.6	4.5	89	87.9	13.9	49	147.2	23.3	09	206.4	32.7	69	265.7	42.1
30	29.6	4.7	90	88.9	14.1	50	148.2	23.5	10	207.4	32.9	70	266.7	42.2
31	30.6	4.8	91	89.9	14.2	151	149.1	23.6	211	208.4	33.0	271	267.7	42.4
32	31.6	5.0	92	90.9	14.4	52	150.1	23.8	12	209.4	33.2	72	268.7	42.6
33	32.6	5.2	93	91.9	14.5	53	151.1	23.9	13	210.4	33.3	73	269.6	42.7
34	33.6	5.3	94	92.8	14.7	54	152.1	24.1	14	211.4	33.5	74	270.6	42.9
35	34.6	5.5	95	93.8	14.9	55	153.1	24.2	15	212.4	33.6	75	271.6	43.0
36	35.6	5.6	96	94.8	15.0	56	154.1	24.4	16	213.3	33.8	76	272.6	43.2
37	36.5	5.8	97	95.8	15.2	57	155.1	24.6	17	214.3	33.9	77	273.6	43.3
38	37.5	5.9	98	96.8	15.3	58	156.1	24.7	18	215.3	34.1	78	274.6	43.5
39	38.5	6.1	99	97.8	15.5	59	157.0	24.9	19	216.3	34.3	79	275.6	43.6
40	39.5	6.3	100	98.8	15.6	60	158.0	25.0	20	217.3	34.4	80	276.6	43.8
41	40.5	6.4	101	99.8	15.8	161	159.0	25.2	221	218.3	34.6	281	277.5	44.0
42	41.5	6.6	02	100.7	16.0	62	160.0	25.3	22	219.3	34.7	82	278.5	44.1
43	42.5	6.7	03	101.7	16.1	63	161.0	25.5	23	220.3	34.9	83	279.5	44.3
44	43.5	6.9	04	102.7	16.3	64	162.0	25.7	24	221.2	35.0	84	280.5	44.4
45	44.4	7.0	05	103.7	16.4	65	163.0	25.8	25	222.2	35.2	85	281.5	44.6
46	45.4	7.2	06	104.7	16.6	66	164.0	26.0	26	223.2	35.4	86	282.5	44.7
47	46.4	7.4	07	105.7	16.7	67	164.9	26.1	27	224.2	35.5	87	283.5	44.9
48	47.4	7.5	08	106.7	16.9	68	165.9	26.3	28	225.2	35.7	88	284.5	45.1
49	48.4	7.7	09	107.7	17.1	69	166.9	26.4	29	226.2	35.8	89	285.4	45.2
50	49.4	7.8	10	108.6	17.2	70	167.9	26.6	30	227.2	36.0	90	286.4	45.4
51	50.4	8.0	111	109.6	17.4	171	168.9	26.8	231	228.2	36.1	291	287.4	45.5
52	51.4	8.1	12	110.6	17.5	72	169.9	26.9	32	229.1	36.3	92	288.4	45.7
53	52.3	8.3	13	111.6	17.7	73	170.9	27.1	33	230.1	36.4	93	289.4	45.8
54	53.3	8.4	14	112.6	17.8	74	171.9	27.2	34	231.1	36.6	94	290.4	46.0
55	54.3	8.6	15	113.6	18.0	75	172.8	27.4	35	232.1	36.8	95	291.4	46.1
56	55.3	8.8	16	114.6	18.1	76	173.8	27.5	36	233.1	36.9	96	292.4	46.3
57	56.3	8.9	17	115.6	18.3	77	174.8	27.7	37	234.1	37.1	97	293.3	46.5
58	57.3	9.1	18	116.5	18.5	78	175.8	27.8	38	235.1	37.2	98	294.3	46.6
59	58.3	9.2	19	117.5	18.6	79	176.8	28.0	39	236.1	37.4	99	295.3	46.8
60	59.3	9.4	20	118.5	18.8	80	177.8	28.2	40	237.0	37.5	300	296.3	46.9
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

81° (99°, 261°, 279°).

TABLE 2.

Difference of Latitude and Departure for 9° (171°, 189°, 351°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	297.3	47.1	361	356.6	56.5	421	415.8	65.9	481	475.1	75.2	541	534.4	84.6
02	298.3	47.2	62	357.5	56.7	22	416.8	66.0	82	476.1	75.3	42	535.4	84.7
03	299.3	47.4	63	358.5	56.8	23	417.8	66.2	83	477.1	75.5	43	536.3	84.9
04	300.3	47.6	64	359.5	56.9	24	418.8	66.3	84	478.0	75.6	44	537.3	85.1
05	301.2	47.7	65	360.5	57.1	25	419.8	66.5	85	479.0	75.8	45	538.3	85.3
06	302.2	47.9	66	361.5	57.3	26	420.8	66.6	86	480.0	75.9	46	539.3	85.4
07	303.2	48.0	67	362.5	57.4	27	421.7	66.8	87	481.0	76.1	47	540.3	85.6
08	304.2	48.2	68	363.5	57.6	28	422.7	67.0	88	482.0	76.2	48	541.3	85.7
09	305.2	48.3	69	364.5	57.7	29	423.7	67.1	89	483.0	76.4	49	542.3	85.9
10	306.2	48.5	70	365.4	57.9	30	424.7	67.3	90	484.0	76.5	50	543.3	86.0
311	307.2	48.7	371	366.4	58.1	431	425.7	67.4	491	485.0	76.7	551	544.3	86.2
12	308.2	48.8	72	367.4	58.2	32	426.7	67.6	92	485.9	76.8	52	545.2	86.3
13	309.1	49.0	73	368.4	58.4	33	427.7	67.7	93	486.9	77.0	53	546.2	86.5
14	310.1	49.1	74	369.4	58.5	34	428.7	67.9	94	487.9	77.1	54	547.2	86.6
15	311.1	49.3	75	370.4	58.7	35	429.6	68.1	95	488.9	77.3	55	548.2	86.8
16	312.1	49.4	76	371.4	58.8	36	430.6	68.2	96	489.9	77.5	56	549.2	87.0
17	313.1	49.6	77	372.4	59.0	37	431.6	68.4	97	490.9	77.7	57	550.2	87.1
18	314.1	49.8	78	373.3	59.1	38	432.6	68.5	98	491.9	77.9	58	551.2	87.3
19	315.1	49.9	79	374.3	59.3	39	433.6	68.7	99	492.9	78.0	59	552.2	87.4
20	316.1	50.1	80	375.3	59.5	40	434.6	68.8	500	493.8	78.2	60	553.1	87.6
321	317.0	50.2	381	376.3	59.6	441	435.6	69.0	501	494.8	78.4	561	554.1	87.7
22	318.0	50.4	82	377.3	59.8	42	436.6	69.1	02	495.8	78.5	62	555.1	87.9
23	319.0	50.5	83	378.3	59.9	43	437.5	69.3	03	496.8	78.7	63	556.1	88.0
24	320.0	50.7	84	379.3	60.1	44	438.5	69.5	04	497.8	78.8	64	557.1	88.2
25	321.0	50.8	85	380.3	60.2	45	439.5	69.6	05	498.8	79.0	65	558.1	88.3
26	322.0	51.0	86	381.2	60.4	46	440.5	69.8	06	499.8	79.1	66	559.1	88.5
27	323.0	51.2	87	382.2	60.5	47	441.5	69.9	07	500.8	79.2	67	560.1	88.6
28	324.0	51.3	88	383.2	60.7	48	442.5	70.1	08	501.7	79.4	68	561.0	88.8
29	324.9	51.5	89	384.2	60.9	49	443.5	70.2	09	502.7	79.5	69	562.0	88.9
30	325.9	51.7	90	385.2	61.0	50	444.5	70.4	10	503.7	79.7	70	563.0	89.1
331	326.9	51.8	391	386.2	61.2	451	445.4	70.6	511	504.7	79.8	571	564.0	89.2
32	327.9	51.9	92	387.2	61.3	52	446.4	70.7	12	505.7	80.1	72	565.0	89.4
33	328.9	52.1	93	388.2	61.5	53	447.4	70.9	13	506.7	80.2	73	566.0	89.5
34	329.9	52.3	94	389.1	61.6	54	448.4	71.0	14	507.7	80.3	74	567.0	89.7
35	330.9	52.4	95	390.1	61.8	55	449.4	71.2	15	508.7	80.5	75	568.0	89.9
36	331.9	52.6	96	391.1	62.0	56	450.4	71.3	16	509.6	80.6	76	568.9	90.1
37	332.8	52.7	97	392.1	62.1	57	451.4	71.5	17	510.6	80.8	77	569.9	90.2
38	333.8	52.9	98	393.1	62.3	58	452.4	71.7	18	511.6	80.9	78	570.9	90.3
39	334.8	53.0	99	394.1	62.4	59	453.3	71.8	19	512.6	81.1	79	571.9	90.5
40	335.8	53.2	400	395.1	62.6	60	454.3	72.0	20	513.6	81.3	80	572.9	90.7
341	336.8	53.3	401	396.1	62.7	461	455.3	72.1	521	514.6	81.4	581	573.9	90.9
42	337.8	53.5	02	397.0	62.9	62	456.3	72.3	22	515.6	81.6	82	574.9	91.0
43	338.8	53.7	03	398.0	63.0	63	457.3	72.4	23	516.6	81.8	83	575.9	91.2
44	339.8	53.8	04	399.0	63.2	64	458.3	72.6	24	517.6	81.9	84	576.9	91.3
45	340.8	54.0	05	400.0	63.4	65	459.3	72.7	25	518.6	82.1	85	577.9	91.5
46	341.7	54.1	06	401.0	63.5	66	460.3	72.9	26	519.5	82.3	86	578.8	91.7
47	342.7	54.3	07	402.0	63.7	67	461.2	73.1	27	520.5	82.4	87	579.8	91.8
48	343.7	54.4	08	403.0	63.8	68	462.2	73.2	28	521.5	82.6	88	580.8	92.0
49	344.7	54.6	09	404.0	64.0	69	463.2	73.4	29	522.5	82.7	89	581.8	92.1
50	345.7	54.8	10	405.0	64.1	70	464.2	73.5	30	523.5	82.9	90	582.8	92.2
351	346.7	54.9	411	405.9	64.3	471	465.2	73.7	531	524.5	83.1	591	583.8	92.4
52	347.7	55.1	12	406.9	64.5	72	466.2	73.8	32	525.5	83.2	92	584.8	92.5
53	348.7	55.2	13	407.9	64.6	73	467.2	74.0	33	526.5	83.4	93	585.7	92.7
54	349.6	55.4	14	408.9	64.8	74	468.2	74.2	34	527.5	83.5	94	586.7	92.9
55	350.6	55.5	15	409.9	64.9	75	469.2	74.3	35	528.4	83.7	95	587.7	93.1
56	351.6	55.7	16	410.9	65.1	76	470.1	74.5	36	529.4	83.8	96	588.7	93.2
57	352.6	55.9	17	411.9	65.2	77	471.1	74.6	37	530.4	84.0	97	589.7	93.4
58	353.6	56.0	18	412.9	65.4	78	472.1	74.8	38	531.4	84.1	98	590.7	93.5
59	354.6	56.2	19	413.8	65.6	79	473.1	74.9	39	532.4	84.3	99	591.7	93.7
60	355.6	56.3	20	414.8	65.7	80	474.1	75.0	40	533.4	84.4	600	592.6	93.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

81° (99°, 261°, 279°).

6583—06——25

TABLE 2.

Difference of Latitude and Departure for 10° (170°, 190°, 350°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.2	61	60.1	10.6	121	119.2	21.0	181	178.3	31.4	241	237.3	41.8
2	2.0	0.3	62	61.1	10.8	22	120.1	21.2	82	179.2	31.6	42	238.3	42.0
3	3.0	0.5	63	62.0	10.9	23	121.1	21.4	83	180.2	31.8	43	239.3	42.2
4	3.9	0.7	64	63.0	11.1	24	122.1	21.5	84	181.2	32.0	44	240.3	42.4
5	4.9	0.9	65	64.0	11.3	25	123.1	21.7	85	182.2	32.1	45	241.3	42.5
6	5.9	1.0	66	65.0	11.5	26	124.1	21.9	86	183.2	32.3	46	242.3	42.7
7	6.9	1.2	67	66.0	11.6	27	125.1	22.1	87	184.2	32.5	47	243.2	42.9
8	7.9	1.4	68	67.0	11.8	28	126.1	22.2	88	185.1	32.6	48	244.2	43.1
9	8.9	1.6	69	68.0	12.0	29	127.0	22.4	89	186.1	32.8	49	245.2	43.2
10	9.8	1.7	70	68.9	12.2	30	128.0	22.6	90	187.1	33.0	50	246.2	43.4
11	10.8	1.9	71	69.9	12.3	131	129.0	22.7	191	188.1	33.2	251	247.2	43.6
12	11 8	2.1	72	70.9	12.5	32	130.0	22.9	92	189.1	33.3	52	248.2	43.8
13	12.8	2.3	73	71.9	12.7	33	131.0	23.1	93	190.1	33.5	53	249.2	43.9
14	13.8	2.4	74	72.9	12.8	34	132.0	23.3	94	191.1	33.7	54	250.1	44.1
15	14.8	2.6	75	73.9	13.0	35	132.9	23.4	95	192.0	33.9	55	251.1	44.3
16	15.8	2.8	76	74.8	13.2	36	133.9	23.6	96	193.0	34.0	56	252.1	44.5
17	16.7	3.0	77	75.8	13.4	37	134.9	23.8	97	194.0	34.2	57	253.1	44.6
18	17.7	3.1	78	76.8	13.5	38	135.9	24.0	98	195.0	34.4	58	254.1	44.8
19	18.7	3.3	79	77.8	13.7	39	136.9	24.1	99	196.0	34.6	59	255.1	45.0
20	19.7	3.5	80	78.8	13.9	40	137.9	24.3	200	197.0	34.7	60	256.1	45.1
21	20.7	3.6	81	79.8	14.1	141	138.9	24.5	201	197.9	34.9	261	257.0	45.3
22	21.7	3.8	82	80.8	14.2	42	139.8	24.7	02	198.9	35.1	62	258.0	45.5
23	22.7	4.0	83	81.7	14.4	43	140.8	24.8	03	199.9	35.3	63	259.0	45.7
24	23.6	4.2	84	82.7	14.6	44	141.8	25.0	04	200.9	35.4	64	260.0	45.8
25	24.6	4.3	85	83.7	14.8	45	142.8	25.2	05	201.9	35.6	65	261.0	46.0
26	25.6	4.5	86	84.7	14.9	46	143.8	25.4	06	202.9	35.8	66	262.0	46.2
27	26.6	4.7	87	85.7	15.1	47	144.8	25.5	07	203.9	35.9	67	262.9	46.4
28	27.6	4.9	88	86.7	15.3	48	145.8	25.7	08	204.8	36.1	68	263.9	46.5
29	28.6	5.0	89	87.6	15.5	49	146.7	25.9	09	205.8	36.3	69	264.9	46.7
30	29.5	5.2	90	88.6	15.6	50	147.7	26.0	10	206.8	36.5	70	265.9	46.9
31	30.5	5.4	91	89.6	15.8	151	148.7	26.2	211	207.8	36.6	271	266.9	47.1
32	31.5	5.6	92	90.6	16.0	52	149.7	26.4	12	208.8	36.8	72	267.9	47.2
33	32.5	5.7	93	91.6	16.1	53	150.7	26.6	13	209.8	37.0	73	268.9	47.4
34	33.5	5.9	94	92.6	16.3	54	151.7	26.7	14	210.7	37.2	74	269.8	47.6
35	34.5	6.1	95	93.6	16.5	55	152.6	26.9	15	211.7	37.3	75	270.8	47.8
36	35.5	6.3	96	94.5	16.7	56	153.6	27.1	16	212.7	37.5	76	271.8	47.9
37	36.4	6.4	97	95.5	16.8	57	154.6	27.3	17	213.7	37.7	77	272.8	48.1
38	37.4	6.6	98	96.5	17.0	58	155.6	27.4	18	214.7	37.9	78	273.8	48.3
39	38.4	6.8	99	97.5	17.2	59	156.6	27.6	19	215.7	38.0	79	274.8	48.4
40	39.4	6.9	100	98.5	17.4	60	157.6	27.8	20	216.7	38.2	80	275.7	48.6
41	40.4	7.1	101	99.5	17.5	161	158.6	28.0	221	217.6	38.4	281	276.7	48.8
42	41.4	7.3	02	100.5	17.7	62	159.5	28.1	22	218.6	38.5	82	277.7	49.0
43	42.3	7.5	03	101.4	17.9	63	160.5	28.3	23	219.6	38.7	83	278.7	49.1
44	43.3	7.6	04	102.4	18.1	64	161.5	28.5	24	220.6	38.9	84	279.7	49.3
45	44.3	7.8	05	103.4	18.2	65	162.5	28.7	25	221.6	39.1	85	280.7	49.5
46	45.3	8.0	06	104.4	18.4	66	163.5	28.8	26	222.6	39.2	86	281.7	49.7
47	46.3	8.2	07	105.4	18.6	67	164.5	29.0	27	223.6	39.4	87	282.6	49.8
48	47.3	8.3	08	106.4	18.8	68	165.4	29.2	28	224.5	39.6	88	283.6	50.0
49	48.3	8.5	09	107.3	18.9	69	166.4	29.3	29	225.5	39.8	89	284.6	50.2
50	49.2	8.7	10	108.3	19.1	70	167.4	29.5	30	226.5	39.9	90	285.6	50.4
51	50.2	8.9	111	109.3	19.3	171	168.4	29.7	231	227.5	40.1	291	286.6	50.5
52	51.2	9.0	12	110.3	19.4	72	169.4	29.9	32	228.5	40.3	92	287.6	50.7
53	52.2	9.2	13	111.3	19.6	73	170.4	30.0	33	229.5	40.5	93	288.5	50.9
54	53.2	9.4	14	112.3	19.8	74	171.4	30.2	34	230.4	40.6	94	289.5	51.1
55	54.2	9.6	15	113.3	20.0	75	172.3	30.4	35	231.4	40.8	95	290.5	51.2
56	55.1	9.7	16	114.2	20.1	76	173.3	30.6	36	232.4	41.0	96	291.5	51.4
57	56.1	9.9	17	115.2	20.3	77	174.3	30.7	37	233.4	41.2	97	292.5	51.6
58	57.1	10.1	18	116.2	20.5	78	175.3	30.9	38	234.4	41.3	98	293.5	51.7
59	58.1	10.2	19	117.2	20.7	79	176.3	31.1	39	235.4	41.5	99	294.5	51.9
60	59.1	10.4	20	118.2	20.8	80	177.3	31.3	40	236.4	41.7	300	295.4	52.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

80° (100°, 260°, 280°).

TABLE 2.

Difference of Latitude and Departure for 10° (170°, 190°, 350°)

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	296.4	52.3	361	355.5	62.7	421	414.6	73.1	481	473.7	83.5	541	532.8	93.9
02	297.4	52.5	62	356.5	62.9	22	415.6	73.3	82	474.7	83.7	42	533.8	94.1
03	298.4	52.6	63	357.5	63.0	23	416.6	73.5	83	475.7	83.9	43	534.8	94.3
04	299.4	52.8	64	358.5	63.2	24	417.6	73.6	84	476.6	84.1	44	535.7	94.5
05	300.4	53.0	65	359.5	63.4	25	418.5	73.8	85	477.6	84.2	45	536.7	94.6
06	301.4	53.1	66	360.4	63.6	26	419.5	74.0	86	478.6	84.4	46	537.7	94.8
07	302.3	53.3	67	361.4	63.7	27	420.5	74.2	87	479.6	84.6	47	538.7	95.0
08	303.3	53.5	68	362.4	63.9	28	421.5	74.3	88	480.6	84.7	48	539.7	95.1
09	304.3	53.7	69	363.4	64.1	29	422.5	74.5	89	481.6	84.9	49	540.7	95.3
10	305.3	53.8	70	364.4	64.3	30	423.5	74.7	90	482.6	85.1	50	541.6	95.5
311	306.3	54.0	371	365.4	64.4	431	424.5	74.9	491	483.5	85.2	551	542.6	95.6
12	307.3	54.2	72	366.4	64.6	32	425.4	75.0	92	484.5	85.4	52	543.6	95.8
13	308.2	54.3	73	367.3	64.8	33	426.4	75.2	93	485.5	85.6	53	544.6	96.0
14	309.2	54.5	74	368.3	65.0	34	427.4	75.4	94	486.5	85.8	54	545.6	96.2
15	310.2	54.7	75	369.3	65.1	35	428.4	75.5	95	487.5	85.9	55	546.6	96.3
16	311.2	54.9	76	370.3	65.3	36	429.4	75.7	96	488.5	86.1	56	547.5	96.5
17	312.2	55.1	77	371.3	65.5	37	430.4	75.9	97	489.4	86.3	57	548.5	96.7
18	313.2	55.2	78	372.3	65.6	38	431.3	76.1	98	490.4	86.5	58	549.5	96.9
19	314.2	55.4	79	373.2	65.8	39	432.3	76.2	99	491.4	86.6	59	550.5	97.0
20	315.1	55.6	80	374.2	66.0	40	433.3	76.4	500	492.4	86.8	60	551.5	97.2
321	316.1	55.8	381	375.2	66.2	441	434.3	76.6	501	493.4	87.0	561	552.5	97.4
22	317.1	55.9	82	376.2	66.3	42	435.3	76.8	02	494.4	87.2	62	553.5	97.6
23	318.1	56.1	83	377.2	66.5	43	436.3	76.9	03	495.3	87.3	63	554.4	97.7
24	319.1	56.3	84	378.2	66.7	44	437.3	77.1	04	496.3	87.5	64	555.4	97.9
25	320.1	56.4	85	379.2	66.9	45	438.2	77.3	05	497.3	87.7	65	556.4	98.1
26	321.0	56.6	86	380.1	67.0	46	439.2	77.5	06	498.3	87.9	66	557.4	98.3
27	322.0	56.8	87	381.1	67.2	47	440.2	77.6	07	499.3	88.0	67	558.4	98.4
28	323.0	57.0	88	382.1	67.4	48	441.2	77.8	08	500.3	88.2	68	559.4	98.6
29	324.0	57.1	89	383.1	67.6	49	442.2	78.0	09	501.3	88.4	69	560.3	98.8
30	325.0	57.3	90	384.1	67.7	50	443.2	78.2	10	502.2	88.6	70	561.3	99.0
331	326.0	57.5	391	385.1	67.9	451	444.2	78.3	511	503.2	88.7	571	562.3	99.1
32	327.0	57.7	92	386.0	68.1	52	445.1	78.5	12	504.2	88.9	72	563.3	99.3
33	327.9	57.8	93	387.0	68.2	53	446.1	78.7	13	505.2	89.1	73	564.3	99.5
34	328.9	58.0	94	388.0	68.4	54	447.1	78.8	14	506.2	89.2	74	565.3	99.6
35	329.9	58.2	95	389.0	68.6	55	448.1	79.0	15	507.2	89.4	75	566.3	99.8
36	330.9	58.4	96	390.0	68.8	56	449.1	79.2	16	508.2	89.6	76	567.2	100.0
37	331.9	58.5	97	391.0	68.9	57	450.1	79.4	17	509.1	89.8	77	568.2	100.2
38	332.9	58.7	98	392.0	69.1	58	451.0	79.5	18	510.1	89.9	78	569.2	100.3
39	333.9	58.9	99	392.9	69.3	59	452.0	79.7	19	511.1	90.1	79	570.2	100.5
40	334.8	59.1	400	393.9	69.5	60	453.0	79.9	20	512.1	90.3	80	571.2	100.7
341	335.8	59.2	401	394.9	69.6	461	454.0	80.1	521	513.1	90.5	581	572.2	100.9
42	336.8	59.4	02	395.9	69.8	62	455.0	80.2	22	514.1	90.6	82	573.2	101.0
43	337.8	59.6	03	396.9	70.0	63	456.0	80.4	23	515.1	90.8	83	574.1	101.2
44	338.8	59.8	04	397.9	70.2	64	457.0	80.6	24	516.0	91.0	84	575.1	101.4
45	339.8	59.9	05	398.9	70.3	65	457.9	80.8	25	517.0	91.2	85	576.1	101.6
46	340.7	60.1	06	399.8	70.5	66	458.9	80.9	26	518.0	91.3	86	577.1	101.7
47	341.7	60.3	07	400.8	70.7	67	459.9	81.1	27	519.0	91.5	87	578.1	101.9
48	342.7	60.4	08	401.8	70.9	68	460.9	81.3	28	520.0	91.7	88	579.1	102.1
49	343.7	60.6	09	402.8	71.0	69	461.9	81.5	29	521.0	91.9	89	580.0	102.3
50	344.7	60.8	10	403.8	71.2	70	462.9	81.6	30	521.9	92.0	90	581.0	102.4
351	345.7	61.0	411	404.8	71.4	471	463.8	81.8	531	522.9	92.2	591	582.0	102.6
52	346.7	61.1	12	405.7	71.6	72	464.8	82.0	32	523.9	92.4	92	583.0	102.8
53	347.6	61.3	13	406.7	71.7	73	465.8	82.1	33	524.9	92.5	93	584.0	102.9
54	348.6	61.5	14	407.7	71.9	74	466.8	82.3	34	525.9	92.7	94	585.0	103.1
55	349.6	61.7	15	408.7	72.1	75	467.8	82.5	35	526.9	92.9	95	586.0	103.3
56	350.6	61.8	16	409.7	72.2	76	468.8	82.7	36	527.9	93.1	96	586.9	103.5
57	351.6	62.0	17	410.7	72.4	77	469.8	82.8	37	528.8	93.2	97	587.9	103.6
58	352.6	62.2	18	411.7	72.6	78	470.7	83.0	38	529.8	93.4	98	588.9	103.8
59	353.5	62.4	19	412.6	72.8	79	471.7	83.2	39	530.8	93.6	99	589.9	104.0
60	354.5	62.5	20	413.6	72.9	80	472.7	83.4	40	531.8	93.8	600	590.9	104.2
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

80° (100°, 260°, 280°).

TABLE 2.

Difference of Latitude and Departure for 11° (169°, 191°, 349°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.2	61	59.9	11.6	121	118.8	23.1	181	177.7	34.5	241	236.6	46.0
2	2.0	0.4	62	60.9	11.8	22	119.8	23.3	82	178.7	34.7	42	237.6	46.2
3	2.9	0.6	63	61.8	12.0	23	120.7	23.5	83	179.6	34.9	43	238.5	46.4
4	3.9	0.8	64	62.8	12.2	24	121.7	23.7	84	180.6	35.1	44	239.5	46.6
5	4.9	1.0	65	63.8	12.4	25	122.7	23.9	85	181.6	35.3	45	240.5	46.7
6	5.9	1.1	66	64.8	12.6	26	123.7	24.0	86	182.6	35.5	46	241.5	46.9
7	6.9	1.3	67	65.8	12.8	27	124.7	24.2	87	183.6	35.7	47	242.5	47.1
8	7.9	1.5	68	66.8	13.0	28	125.6	24.4	88	184.5	35.9	48	243.4	47.3
9	8.8	1.7	69	67.7	13.2	29	126.6	24.6	89	185.5	36.1	49	244.4	47.5
10	9.8	1.9	70	68.7	13.4	30	127.6	24.8	90	186.5	36.3	50	245.4	47.7
11	10.8	2.1	71	69.7	13.5	131	128.6	25.0	191	187.5	36.4	251	246.4	47.9
12	11.8	2.3	72	70.7	13.7	32	129.6	25.2	92	188.5	36.6	52	247.4	48.1
13	12.8	2.5	73	71.7	13.9	33	130.6	25.4	93	189.5	36.8	53	248.4	48.3
14	13.7	2.7	74	72.6	14.1	34	131.5	25.6	94	190.4	37.0	54	249.3	48.5
15	14.7	2.9	75	73.6	14.3	35	132.5	25.8	95	191.4	37.2	55	250.3	48.7
16	15.7	3.1	76	74.6	14.5	36	133.5	26.0	96	192.4	37.4	56	251.3	48.8
17	16.7	3.2	77	75.6	14.7	37	134.5	26.1	97	193.4	37.6	57	252.3	49.0
18	17.7	3.4	78	76.6	14.9	38	135.5	26.3	98	194.4	37.8	58	253.3	49.2
19	18.7	3.6	79	77.5	15.1	39	136.4	26.5	99	195.3	38.0	59	254.2	49.4
20	19.6	3.8	80	78.5	15.3	40	137.4	26.7	200	196.3	38.2	60	255.2	49.6
21	20.6	4.0	81	79.5	15.5	141	138.4	26.9	201	197.3	38.4	261	256.2	49.8
22	21.6	4.2	82	80.5	15.6	42	139.4	27.1	02	198.3	38.5	62	257.2	50.0
23	22.6	4.4	83	81.5	15.8	43	140.4	27.3	03	199.3	38.7	63	258.2	50.2
24	23.6	4.6	84	82.5	16.0	44	141.4	27.5	04	200.3	38.9	64	259.1	50.4
25	24.5	4.8	85	83.4	16.2	45	142.3	27.7	05	201.2	39.1	65	260.1	50.6
26	25.5	5.0	86	84.4	16.4	46	143.3	27.9	06	202.2	39.3	66	261.1	50.8
27	26.5	5.2	87	85.4	16.6	47	144.3	28.0	07	203.2	39.5	67	262.1	50.9
28	27.5	5.3	88	86.4	16.8	48	145.3	28.2	08	204.2	39.7	68	263.1	51.1
29	28.5	5.5	89	87.4	17.0	49	146.3	28.4	09	205.2	39.9	69	264.1	51.3
30	29.4	5.7	90	88.3	17.2	50	147.2	28.6	10	206.1	40.1	70	265.0	51.5
31	30.4	5.9	91	89.3	17.4	151	148.2	28.8	211	207.1	40.3	271	266.0	51.7
32	31.4	6.1	92	90.3	17.6	52	149.2	29.0	12	208.1	40.5	72	267.0	51.9
33	32.4	6.3	93	91.3	17.7	53	150.2	29.2	13	209.1	40.6	73	268.0	52.1
34	33.4	6.5	94	92.3	17.9	54	151.2	29.4	14	210.1	40.8	74	269.0	52.3
35	34.4	6.7	95	93.3	18.1	55	152.2	29.6	15	211.0	41.0	75	269.9	52.5
36	35.3	6.9	96	94.2	18.3	56	153.1	29.8	16	212.0	41.2	76	270.9	52.7
37	36.3	7.1	97	95.2	18.5	57	154.1	30.0	17	213.0	41.4	77	271.9	52.9
38	37.3	7.3	98	96.2	18.7	58	155.1	30.1	18	214.0	41.6	78	272.9	53.0
39	38.3	7.4	99	97.2	18.9	59	156.1	30.3	19	215.0	41.8	79	273.9	53.2
40	39.3	7.6	100	98.2	19.1	60	157.1	30.5	20	216.0	42.0	80	274.9	53.4
41	40.2	7.8	101	99.1	19.3	161	158.0	30.7	221	216.9	42.2	281	275.8	53.6
42	41.2	8.0	02	100.1	19.5	62	159.0	30.9	22	217.9	42.4	82	276.8	53.8
43	42.2	8.2	03	101.1	19.7	63	160.0	31.1	23	218.9	42.6	83	277.8	54.0
44	43.2	8.4	04	102.1	19.8	64	161.0	31.3	24	219.9	42.7	84	278.8	54.2
45	44.2	8.6	05	103.1	20.0	65	162.0	31.5	25	220.9	42.9	85	279.8	54.4
46	45.2	8.8	06	104.1	20.2	66	163.0	31.7	26	221.8	43.1	86	280.7	54.6
47	46.1	9.0	07	105.0	20.4	67	163.9	31.9	27	222.8	43.3	87	281.7	54.8
48	47.1	9.2	08	106.0	20.6	68	164.9	32.1	28	223.8	43.5	88	282.7	55.0
49	48.1	9.3	09	107.0	20.8	69	165.9	32.2	29	224.8	43.7	89	283.7	55.1
50	49.1	9.5	10	108.0	21.0	70	166.9	32.4	30	225.8	43.9	90	284.7	55.3
51	50.1	9.7	111	109.0	21.2	171	167.9	32.6	231	226.8	44.1	291	285.7	55.5
52	51.0	9.9	12	109.9	21.4	72	168.8	32.8	32	227.7	44.3	92	286.6	55.7
53	52.0	10.1	13	110.9	21.6	73	169.8	33.0	33	228.7	44.5	93	287.6	55.9
54	53.0	10.3	14	111.9	21.8	74	170.8	33.2	34	229.7	44.6	94	288.6	56.1
55	54.0	10.5	15	112.9	21.9	75	171.8	33.4	35	230.7	44.8	95	289.6	56.3
56	55.0	10.7	16	113.9	22.1	76	172.8	33.6	36	231.7	45.0	96	290.6	56.5
57	56.0	10.9	17	114.9	22.3	77	173.7	33.8	37	232.6	45.2	97	291.5	56.7
58	56.9	11.1	18	115.8	22.5	78	174.7	34.0	38	233.6	45.4	98	292.5	56.9
59	57.9	11.3	19	116.8	22.7	79	175.7	34.2	39	234.6	45.6	99	293.5	57.1
60	58.9	11.4	20	117.8	22.9	80	176.7	34.3	40	235.6	45.8	300	294.5	57.2
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

79° (101°, 259°, 281°).

TABLE 2.

Difference of Latitude and Departure for 11° (169°, 191°, 349°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	295.4	57.4	361	354.3	68.9	421	413.2	80.3	481	472.1	91.8	541	531.0	103.2
02	296.4	57.6	62	355.3	69.1	22	414.2	80.5	82	473.1	92.0	42	532.0	103.4
03	297.4	57.8	63	356.3	69.3	23	415.2	80.7	83	474.1	92.2	43	533.0	103.6
04	298.4	58.0	64	357.3	69.5	24	416.2	80.9	84	475.1	92.4	44	534.0	103.8
05	299.4	58.2	65	358.3	69.6	25	417.2	81.1	85	476.1	92.6	45	535.0	104.0
06	300.3	58.4	66	359.2	69.8	26	418.1	81.3	86	477.0	92.8	46	535.9	104.2
07	301.3	58.6	67	360.2	70.0	27	419.1	81.5	87	478.0	93.0	47	536.9	104.4
08	302.3	58.8	68	361.2	70.2	28	420.1	81.7	88	479.0	93.2	48	537.9	104.6
09	303.3	59.0	69	362.2	70.4	29	421.1	81.9	89	480.0	93.3	49	538.9	104.8
10	304.3	59.2	70	363.2	70.6	30	422.1	82.1	90	481.0	93.5	50	539.9	105.0
311	305.3	59.3	371	364.1	70.8	431	423.0	82.2	491	481.9	93.6	551	540.8	105.1
12	306.2	59.5	72	365.1	71.0	32	424.0	82.4	92	482.9	93.8	52	541.8	105.3
13	307.2	59.7	73	366.1	71.2	33	425.0	82.6	93	483.9	94.0	53	542.8	105.5
14	308.2	59.9	74	367.1	71.4	34	426.0	82.8	94	484.9	94.2	54	543.8	105.7
15	309.2	60.1	75	368.1	71.6	35	427.0	83.0	95	485.9	94.4	55	544.8	105.9
16	310.2	60.3	76	369.1	71.7	36	428.0	83.2	96	486.9	94.6	56	545.8	106.1
17	311.1	60.5	77	370.0	71.9	37	428.9	83.4	97	487.8	94.8	57	546.7	106.3
18	312.1	60.7	78	371.0	72.1	38	429.9	83.6	98	488.8	95.0	58	547.7	106.5
19	313.1	60.9	79	372.0	72.3	39	430.9	83.8	99	489.8	95.2	59	548.7	106.7
20	314.1	61.1	80	373.0	72.5	40	431.9	84.0	500	490.8	95.4	60	549.7	106.9
321	315.1	61.3	381	374.0	72.7	441	432.9	84.1	501	491.8	95.6	561	550.7	107.1
22	316.1	61.4	82	374.9	72.9	42	433.8	84.3	02	492.7	95.8	62	551.6	107.2
23	317.0	61.6	83	375.9	73.1	43	434.8	84.5	03	493.7	96.0	63	552.6	107.4
24	318.0	61.8	84	376.9	73.3	44	435.8	84.7	04	494.7	96.2	64	553.6	107.6
25	319.0	62.0	85	377.9	73.5	45	436.8	84.9	05	495.7	96.4	65	554.6	107.8
26	320.0	62.2	86	378.9	73.7	46	437.8	85.1	06	496.7	96.6	66	555.6	108.0
27	321.0	62.4	87	379.9	73.8	47	438.8	85.3	07	497.7	96.8	67	556.6	108.2
28	321.9	62.6	88	380.8	74.0	48	439.7	85.5	08	498.6	97.0	68	557.6	108.4
29	322.9	62.8	89	381.8	74.2	49	440.7	85.7	09	499.6	97.2	69	558.6	108.6
30	323.9	63.0	90	382.8	74.4	50	441.7	85.9	10	500.6	97.3	70	559.5	108.8
331	324.9	63.2	391	383.8	74.6	451	442.7	86.1	511	501.6	97.5	571	560.5	109.0
32	325.9	63.4	92	384.8	74.8	52	443.7	86.2	12	502.6	97.6	72	561.5	109.1
33	326.8	63.5	93	385.7	75.0	53	444.6	86.4	13	503.5	97.8	73	562.5	109.3
34	327.8	63.7	94	386.7	75.2	54	445.6	86.6	14	504.5	98.0	74	563.5	109.5
35	328.8	63.9	95	387.7	75.4	55	446.6	86.8	15	505.5	98.2	75	564.5	109.7
36	329.8	64.1	96	388.7	75.6	56	447.6	87.0	16	506.5	98.4	76	565.4	109.9
37	330.8	64.3	97	389.7	75.8	57	448.6	87.2	17	507.5	98.6	77	566.4	110.1
38	331.8	64.5	98	390.7	75.9	58	449.6	87.4	18	508.5	98.8	78	567.4	110.3
39	332.7	64.7	99	391.6	76.1	59	450.5	87.6	19	509.4	99.0	79	568.3	110.5
40	333.7	64.9	400	392.6	76.3	60	451.5	87.8	20	510.4	99.2	80	569.3	110.7
341	334.7	65.1	401	393.6	76.5	461	452.5	88.0	521	511.4	99.4	581	570.3	110.9
42	335.7	65.3	02	394.6	76.7	62	453.5	88.2	22	512.4	99.6	82	571.3	111.1
43	336.7	65.5	03	395.6	76.9	63	454.5	88.3	23	513.4	99.8	83	572.3	111.3
44	337.6	65.6	04	396.5	77.1	64	455.4	88.5	24	514.3	100.0	84	573.2	111.5
45	338.6	65.8	05	397.5	77.3	65	456.4	88.7	25	515.3	100.2	85	574.2	111.7
46	339.6	66.0	06	398.5	77.5	66	457.4	88.9	26	516.3	100.4	86	575.2	111.8
47	340.6	66.2	07	399.5	77.7	67	458.4	89.1	27	517.3	100.6	87	576.2	112.1
48	341.6	66.4	08	400.5	77.9	68	459.4	89.3	28	518.3	100.8	88	577.2	112.3
49	342.6	66.6	09	401.5	78.1	69	460.4	89.5	29	519.3	101.0	89	578.2	112.4
50	343.5	66.8	10	402.4	78.2	70	461.3	89.7	30	520.2	101.2	90	579.1	112.6
351	344.5	67.0	411	403.4	78.4	471	462.3	89.9	531	521.2	101.4	591	580.1	112.8
52	345.5	67.2	12	404.4	78.6	72	463.3	90.1	32	522.2	101.6	92	581.1	113.0
53	346.5	67.4	13	405.4	78.8	73	464.3	90.3	33	523.2	101.7	93	582.1	113.2
54	347.5	67.5	14	406.4	79.0	74	465.3	90.4	34	524.2	101.8	94	583.1	113.3
55	348.4	67.7	15	407.3	79.2	75	466.2	90.6	35	525.1	102.0	95	584.0	113.5
56	349.4	67.9	16	408.3	79.4	76	467.2	90.8	36	526.1	102.2	96	585.0	113.7
57	350.4	68.1	17	409.3	79.6	77	468.2	91.0	37	527.1	102.4	97	586.0	113.9
58	351.4	68.3	18	410.3	79.8	78	469.2	91.2	38	528.1	102.6	98	587.0	114.1
59	352.4	68.5	19	411.3	80.0	79	470.2	91.4	39	529.1	102.8	99	588.0	114.3
60	353.4	68.7	20	412.3	80.1	80	471.1	91.6	40	530.1	103.0	600	589.0	114.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

79° (101°, 259°, 281°).

TABLE 2.

Difference of Latitude and Departure for 12° (168°, 192°, 348°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.2	61	59.7	12.7	121	118.4	25.2	181	177.0	37.6	241	235.7	50.1
2	2.0	0.4	62	60.6	12.9	22	119.3	25.4	82	178.0	37.8	42	236.7	50.3
3	2.9	0.6	63	61.6	13.1	23	120.3	25.6	83	179.0	38.0	43	237.7	50.5
4	3.9	0.8	64	62.6	13.3	24	121.3	25.8	84	180.0	38.3	44	238.7	50.7
5	4.9	1.0	65	63.6	13.5	25	122.3	26.0	85	181.0	38.5	45	239.6	50.9
6	5.9	1.2	66	64.6	13.7	26	123.2	26.2	86	181.9	38.7	46	240.6	51.1
7	6.8	1.5	67	65.5	13.9	27	124.2	26.4	87	182.9	38.9	47	241.6	51.4
8	7.8	1.7	68	66.5	14.1	28	125.2	26.6	88	183.9	39.1	48	242.6	51.6
9	8.8	1.9	69	67.5	14.3	29	126.2	26.8	89	184.9	39.3	49	243.6	51.8
10	9.8	2.1	70	68.5	14.6	30	127.2	27.0	90	185.8	39.5	50	244.5	52.0
11	10.8	2.3	71	69.4	14.8	131	128.1	27.2	191	186.8	39.7	251	245.5	52.2
12	11.7	2.5	72	70.4	15.0	32	129.1	27.4	92	187.8	39.9	52	246.5	52.4
13	12.7	2.7	73	71.4	15.2	33	130.1	27.7	93	188.8	40.1	53	247.5	52.6
14	13.7	2.9	74	72.4	15.4	34	131.1	27.9	94	189.8	40.3	54	248.4	52.8
15	14.7	3.1	75	73.4	15.6	35	132.0	28.1	95	190.7	40.5	55	249.4	53.0
16	15.7	3.3	76	74.3	15.8	36	133.0	28.3	96	191.7	40.8	56	250.4	53.2
17	16.6	3.5	77	75.3	16.0	37	134.0	28.5	97	192.7	41.0	57	251.4	53.4
18	17.6	3.7	78	76.3	16.2	38	135.0	28.7	98	193.7	41.2	58	252.4	53.6
19	18.6	4.0	79	77.3	16.4	39	136.0	28.9	99	194.7	41.4	59	253.3	53.8
20	19.6	4.2	80	78.3	16.6	40	136.9	29.1	200	195.6	41.6	60	254.3	54.1
21	20.5	4.4	81	79.2	16.8	141	137.9	29.3	201	196.6	41.8	261	255.3	54.3
22	21.5	4.6	82	80.2	17.0	42	138.9	29.5	02	197.6	42.0	62	256.3	54.5
23	22.5	4.8	83	81.2	17.3	43	139.9	29.7	03	198.6	42.2	63	257.3	54.7
24	23.5	5.0	84	82.2	17.5	44	140.9	29.9	04	199.5	42.4	64	258.2	54.9
25	24.5	5.2	85	83.1	17.7	45	141.8	30.1	05	200.5	42.6	65	259.2	55.1
26	25.4	5.4	86	84.1	17.9	46	142.8	30.4	06	201.5	42.8	66	260.2	55.3
27	26.4	5.6	87	85.1	18.1	47	143.8	30.6	07	202.5	43.0	67	261.2	55.5
28	27.4	5.8	88	86.1	18.3	48	144.8	30.8	08	203.5	43.2	68	262.1	55.7
29	28.4	6.0	89	87.1	18.5	49	145.7	31.0	09	204.4	43.5	69	263.1	55.9
30	29.3	6.2	90	88.0	18.7	50	146.7	31.2	10	205.4	43.7	70	264.1	56.1
31	30.3	6.4	91	89.0	18.9	151	147.7	31.4	211	206.4	43.9	271	265.1	56.3
32	31.3	6.7	92	90.0	19.1	52	148.7	31.6	12	207.4	44.1	72	266.1	56.6
33	32.3	6.9	93	91.0	19.3	53	149.7	31.8	13	208.3	44.3	73	267.0	56.8
34	33.3	7.1	94	91.9	19.5	54	150.6	32.0	14	209.3	44.5	74	268.0	57.0
35	34.2	7.3	95	92.9	19.8	55	151.6	32.2	15	210.3	44.7	75	269.0	57.2
36	35.2	7.5	96	93.9	20.0	56	152.6	32.4	16	211.3	44.9	76	270.0	57.4
37	36.2	7.7	97	94.9	20.2	57	153.6	32.6	17	212.3	45.1	77	270.9	57.6
38	37.2	7.9	98	95.9	20.4	58	154.5	32.9	18	213.2	45.3	78	271.9	57.8
39	38.1	8.1	99	96.8	20.6	59	155.5	33.1	19	214.2	45.5	79	272.9	58.0
40	39.1	8.3	100	97.8	20.8	60	156.5	33.3	20	215.2	45.7	80	273.9	58.2
41	40.1	8.5	101	98.8	21.0	161	157.5	33.5	221	216.2	45.9	281	274.9	58.4
42	41.1	8.7	02	99.8	21.2	62	158.5	33.7	22	217.1	46.2	82	275.8	58.6
43	42.1	8.9	03	100.7	21.4	63	159.4	33.9	23	218.1	46.4	83	276.8	58.8
44	43.0	9.1	04	101.7	21.6	64	160.4	34.1	24	219.1	46.6	84	277.8	59.0
45	44.0	9.4	05	102.7	21.8	65	161.4	34.3	25	220.1	46.8	85	278.8	59.3
46	45.0	9.6	06	103.7	22.0	66	162.4	34.5	26	221.1	47.0	86	279.8	59.5
47	46.0	9.8	07	104.7	22.2	67	163.4	34.7	27	222.0	47.2	87	280.7	59.7
48	47.0	10.0	08	105.7	22.5	68	164.3	34.9	28	223.0	47.4	88	281.7	59.9
49	47.9	10.2	09	106.6	22.7	69	165.3	35.1	29	224.0	47.6	89	282.7	60.1
50	48.9	10.4	10	107.6	22.9	70	166.3	35.3	30	225.0	47.8	90	283.7	60.3
51	49.9	10.6	111	108.6	23.1	171	167.3	35.6	231	226.0	48.0	291	284.6	60.5
52	50.9	10.8	12	109.6	23.3	72	168.2	35.8	32	226.9	48.2	92	285.6	60.7
53	51.8	11.0	13	110.5	23.5	73	169.2	36.0	33	227.9	48.4	93	286.6	60.9
54	52.8	11.2	14	111.5	23.7	74	170.2	36.2	34	228.9	48.7	94	287.6	61.1
55	53.8	11.4	15	112.5	23.9	75	171.2	36.4	35	229.9	48.9	95	288.6	61.3
56	54.8	11.6	16	113.5	24.1	76	172.2	36.6	36	230.8	49.1	96	289.5	61.5
57	55.8	11.9	17	114.4	24.3	77	173.1	36.8	37	231.8	49.3	97	290.5	61.7
58	56.7	12.1	18	115.4	24.5	78	174.1	37.0	38	232.8	49.5	98	291.5	62.0
59	57.7	12.3	19	116.4	24.7	79	175.1	37.2	39	233.8	49.7	99	292.5	62.2
60	58.7	12.5	20	117.4	24.9	80	176.1	37.4	40	234.8	49.9	300	293.4	62.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

78° (102°, 258°, 282°).

TABLE 2.

Difference of Latitude and Departure for 12° (168°, 192°, 348°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	294.4	62.6	361	353.1	75.0	421	411.8	87.5	481	470.5	100.0	541	529.2	112.5
02	295.4	62.8	62	354.1	75.2	22	412.8	87.7	82	471.5	100.2	42	530.2	112.7
03	296.4	63.0	63	355.1	75.4	23	413.8	87.9	83	472.5	100.4	43	531.1	112.9
04	297.4	63.2	64	356.0	75.7	24	414.7	88.1	84	473.4	100.6	44	532.1	113.1
05	298.3	63.4	65	357.0	75.9	25	415.7	88.3	85	474.4	100.8	45	533.1	113.3
06	299.3	63.6	66	358.0	76.1	26	416.7	88.6	86	475.4	101.0	46	534.1	113.5
07	300.3	63.8	67	359.0	76.3	27	417.7	88.8	87	476.4	101.2	47	535.1	113.7
08	301.3	64.0	68	360.0	76.5	28	418.6	89.0	88	477.3	101.4	48	536.0	113.9
09	302.2	64.2	69	360.9	76.7	29	419.6	89.2	89	478.3	101.6	49	537.0	114.1
10	303.2	64.4	70	361.9	76.9	30	420.6	89.4	90	479.3	101.9	50	538.0	114.4
311	304.2	64.6	371	362.9	77.1	431	421.6	89.6	491	480.3	102.1	551	538.9	114.6
12	305.2	64.8	72	363.9	77.3	32	422.6	89.8	92	481.2	102.3	52	539.9	114.8
13	306.2	65.1	73	364.8	77.5	33	423.5	90.0	93	482.2	102.5	53	540.9	115.0
14	307.1	65.3	74	365.8	77.7	34	424.5	90.2	94	483.2	102.7	54	541.9	115.2
15	308.1	65.5	75	366.8	77.9	35	425.5	90.4	95	484.2	102.9	55	542.9	115.4
16	309.1	65.7	76	367.8	78.2	36	426.5	90.6	96	485.2	103.1	56	543.8	115.6
17	310.1	65.9	77	368.8	78.4	37	427.5	90.8	97	486.1	103.3	57	544.8	115.8
18	311.1	66.1	78	369.7	78.6	38	428.4	91.0	98	487.1	103.5	58	545.8	116.0
19	312.0	66.3	79	370.7	78.8	39	429.4	91.3	99	488.1	103.8	59	546.8	116.2
20	313.0	66.5	80	371.7	79.0	40	430.4	91.5	500	489.1	104.0	60	547.8	116.4
321	314.0	66.7	381	372.7	79.2	441	431.4	91.7	501	490.0	104.2	561	548.7	116.6
22	315.0	66.9	82	373.7	79.4	42	432.3	91.9	02	491.0	104.4	62	549.7	116.8
23	315.9	67.1	83	374.6	79.6	43	433.3	92.1	03	492.0	104.6	63	550.7	117.0
24	316.9	67.3	84	375.6	79.8	44	434.3	92.3	04	493.0	104.8	64	551.7	117.2
25	317.9	67.6	85	376.6	80.0	45	435.3	92.5	05	494.0	105.0	65	552.7	117.4
26	318.9	67.8	86	377.6	80.2	46	436.3	92.7	06	495.0	105.2	66	553.7	117.6
27	319.9	68.0	87	378.5	80.4	47	437.2	92.9	07	495.9	105.4	67	554.6	117.8
28	320.8	68.2	88	379.5	80.7	48	438.2	93.1	08	496.9	105.6	68	555.6	118.0
29	321.8	68.4	89	380.5	80.9	49	439.2	93.3	09	497.9	105.8	69	556.6	118.2
30	322.8	68.6	90	381.5	81.1	50	440.2	93.5	10	498.9	106.0	70	557.5	118.5
331	323.8	68.8	391	382.5	81.3	451	441.1	93.7	511	499.8	106.2	571	558.5	118.7
32	324.7	69.0	92	383.4	81.5	52	442.1	93.9	12	500.8	106.4	72	559.5	118.9
33	325.7	69.2	93	384.4	81.7	53	443.1	94.1	13	501.8	106.6	73	560.5	119.1
34	326.7	69.4	94	385.4	81.9	54	444.1	94.4	14	502.8	106.8	74	561.5	119.3
35	327.7	69.6	95	386.4	82.1	55	445.1	94.6	15	503.7	107.0	75	562.4	119.5
36	328.7	69.8	96	387.3	82.3	56	446.0	94.8	16	504.7	107.2	76	563.4	119.7
37	329.6	70.0	97	388.3	82.5	57	447.0	95.0	17	505.7	107.4	77	564.4	119.9
38	330.6	70.3	98	389.3	82.7	58	448.0	95.2	18	506.7	107.6	78	565.4	120.1
39	331.6	70.5	99	390.3	82.9	59	449.0	95.4	19	507.7	107.8	79	566.4	120.3
40	332.6	70.7	400	391.3	83.1	60	450.0	95.6	20	508.7	108.1	80	567.4	120.6
341	333.5	70.9	401	392.2	83.4	461	450.9	95.8	521	509.6	108.3	581	568.3	120.8
42	334.5	71.1	02	393.2	83.6	62	451.9	96.0	22	510.6	108.5	82	569.3	121.0
43	335.5	71.3	03	394.2	83.8	63	452.9	96.2	23	511.6	108.7	83	570.3	121.2
44	336.5	71.5	04	395.2	84.0	64	453.9	96.5	24	512.5	108.9	84	571.2	121.4
45	337.5	71.7	05	396.2	84.2	65	454.8	96.7	25	513.5	109.2	85	572.2	121.6
46	338.4	71.9	06	397.1	84.4	66	455.8	96.9	26	514.5	109.4	86	573.2	121.8
47	339.4	72.1	07	398.1	84.6	67	456.8	97.1	27	515.5	109.6	87	574.2	122.0
48	340.4	72.3	08	399.1	84.8	68	457.8	97.3	28	516.5	109.8	88	575.2	122.2
49	341.4	72.5	09	400.1	85.0	69	458.8	97.5	29	517.5	110.0	89	576.2	122.4
50	342.4	72.7	10	401.0	85.2	70	459.7	97.7	30	518.4	110.2	90	577.1	122.6
351	343.3	73.0	411	402.0	85.4	471	460.7	97.9	531	519.4	110.4	591	578.1	122.8
52	344.3	73.2	12	403.0	85.6	72	461.7	98.1	32	520.4	110.6	92	579.1	123.0
53	345.3	73.4	13	404.0	85.8	73	462.7	98.3	33	521.3	110.8	93	580.0	123.2
54	346.3	73.6	14	405.0	86.1	74	463.6	98.5	34	522.3	111.0	94	581.0	123.4
55	347.2	73.8	15	405.9	86.3	75	464.6	98.7	35	523.3	111.2	95	582.0	123.6
56	348.2	74.0	16	406.9	86.5	76	465.6	98.9	36	524.3	111.4	96	583.0	123.9
57	349.2	74.2	17	407.9	86.7	77	466.6	99.1	37	525.3	111.6	97	584.0	124.1
58	350.2	74.4	18	408.9	86.9	78	467.6	99.4	38	526.2	111.8	98	584.9	124.3
59	351.2	74.6	19	409.8	87.1	79	468.5	99.6	39	527.2	112.0	99	585.9	124.5
60	352.1	74.8	20	410.8	87.3	80	469.5	99.8	40	528.2	112.3	600	586.9	124.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

78° (102°, 258°, 282°).

TABLE 2.

Difference of Latitude and Departure for 13° (167°, 193°, 347°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.2	61	59.4	13.7	121	117.9	27.2	181	176.4	40.7	241	234.8	54.2
2	1.9	0.4	62	60.4	13.9	22	118.9	27.4	82	177.3	40.9	42	235.8	54.4
3	2.9	0.7	63	61.4	14.2	23	119.8	27.7	83	178.3	41.2	43	236.8	54.7
4	3.9	0.9	64	62.4	14.4	24	120.8	27.9	84	179.3	41.4	44	237.7	54.9
5	4.9	1.1	65	63.3	14.6	25	121.8	28.1	85	180.3	41.6	45	238.7	55.1
6	5.8	1.3	66	64.3	14.8	26	122.8	28.3	86	181.2	41.8	46	239.7	55.3
7	6.8	1.6	67	65.3	15.1	27	123.7	28.6	87	182.2	42.1	47	240.7	55.6
8	7.8	1.8	68	66.3	15.3	28	124.7	28.8	88	183.2	42.3	48	241.6	55.8
9	8.8	2.0	69	67.2	15.5	29	125.7	29.0	89	184.2	42.5	49	242.6	56.0
10	9.7	2.2	70	68.2	15.7	30	126.7	29.2	90	185.1	42.7	50	243.6	56.2
11	10.7	2.5	71	69.2	16.0	131	127.6	29.5	191	186.1	43.0	251	244.6	56.5
12	11.7	2.7	72	70.2	16.2	32	128.6	29.7	92	187.1	43.2	52	245.5	56.7
13	12.7	2.9	73	71.1	16.4	33	129.6	29.9	93	188.1	43.4	53	246.5	56.9
14	13.6	3.1	74	72.1	16.6	34	130.6	30.1	94	189.0	43.6	54	247.5	57.1
15	14.6	3.4	75	73.1	16.9	35	131.5	30.4	95	190.0	43.9	55	248.5	57.4
16	15.6	3.6	76	74.1	17.1	36	132.5	30.6	96	191.0	44.1	56	249.4	57.6
17	16.6	3.8	77	75.0	17.3	37	133.5	30.8	97	192.0	44.3	57	250.4	57.8
18	17.5	4.0	78	76.0	17.5	38	134.5	31.0	98	192.9	44.5	58	251.4	58.0
19	18.5	4.3	79	77.0	17.8	39	135.4	31.3	99	193.9	44.8	59	252.4	58.3
20	19.5	4.5	80	77.9	18.0	40	136.4	31.5	200	194.9	45.0	60	253.3	58.5
21	20.5	4.7	81	78.9	18.2	141	137.4	31.7	201	195.8	45.2	261	254.3	58.7
22	21.4	4.9	82	79.9	18.4	42	138.4	31.9	02	196.8	45.4	62	255.3	58.9
23	22.4	5.2	83	80.9	18.7	43	139.3	32.2	03	197.8	45.7	63	256.3	59.2
24	23.4	5.4	84	81.8	18.9	44	140.3	32.4	04	198.8	45.9	64	257.2	59.4
25	24.4	5.6	85	82.8	19.1	45	141.3	32.6	05	199.7	46.1	65	258.2	59.6
26	25.3	5.8	86	83.8	19.3	46	142.3	32.8	06	200.7	46.3	66	259.2	59.8
27	26.3	6.1	87	84.8	19.6	47	143.2	33.1	07	201.7	46.6	67	260.2	60.1
28	27.3	6.3	88	85.7	19.8	48	144.2	33.3	08	202.7	46.8	68	261.1	60.3
29	28.3	6.5	89	86.7	20.0	49	145.2	33.5	09	203.6	47.0	69	262.1	60.5
30	29.2	6.7	90	87.7	20.2	50	146.2	33.7	10	204.6	47.2	70	263.1	60.7
31	30.2	7.0	91	88.7	20.5	151	147.1	34.0	211	205.6	47.5	271	264.1	61.0
32	31.2	7.2	92	89.6	20.7	52	148.1	34.2	12	206.6	47.7	72	265.0	61.2
33	32.2	7.4	93	90.6	20.9	53	149.1	34.4	13	207.5	47.9	73	266.0	61.4
34	33.1	7.6	94	91.6	21.1	54	150.1	34.6	14	208.5	48.1	74	267.0	61.6
35	34.1	7.9	95	92.6	21.4	55	151.0	34.9	15	209.5	48.4	75	268.0	61.9
36	35.1	8.1	96	93.5	21.6	56	152.0	35.1	16	210.5	48.6	76	268.9	62.1
37	36.1	8.3	97	94.5	21.8	57	153.0	35.3	17	211.4	48.8	77	269.9	62.3
38	37.0	8.5	98	95.5	22.0	58	154.0	35.5	18	212.4	49.0	78	270.9	62.5
39	38.0	8.8	99	96.5	22.3	59	154.9	35.8	19	213.4	49.3	79	271.8	62.8
40	39.0	9.0	100	97.4	22.5	60	155.9	36.0	20	214.4	49.5	80	272.8	63.0
41	39.9	9.2	101	98.4	22.7	161	156.9	36.2	221	215.3	49.7	281	273.8	63.2
42	40.9	9.4	02	99.4	22.9	62	157.8	36.4	22	216.3	49.9	82	274.8	63.4
43	41.9	9.7	03	100.4	23.2	63	158.8	36.7	23	217.3	50.2	83	275.7	63.7
44	42.9	9.9	04	101.3	23.4	64	159.8	36.9	24	218.3	50.4	84	276.7	63.9
45	43.8	10.1	05	102.3	23.6	65	160.8	37.1	25	219.2	50.6	85	277.7	64.1
46	44.8	10.3	06	103.3	23.8	66	161.7	37.3	26	220.2	50.8	86	278.7	64.3
47	45.8	10.6	07	104.3	24.1	67	162.7	37.6	27	221.2	51.1	87	279.6	64.6
48	46.8	10.8	08	105.2	24.3	68	163.7	37.8	28	222.2	51.3	88	280.6	64.8
49	47.7	11.0	09	106.2	24.5	69	164.7	38.0	29	223.1	51.5	89	281.6	65.0
50	48.7	11.2	10	107.2	24.7	70	165.6	38.2	30	224.1	51.7	90	282.6	65.2
51	49.7	11.5	111	108.2	25.0	171	166.6	38.5	231	225.1	52.0	291	283.5	65.5
52	50.7	11.7	12	109.1	25.2	72	167.6	38.7	32	226.1	52.2	92	284.5	65.7
53	51.6	11.9	13	110.1	25.4	73	168.6	38.9	33	227.0	52.4	93	285.5	65.9
54	52.6	12.1	14	111.1	25.6	74	169.5	39.1	34	228.0	52.6	94	286.5	66.1
55	53.6	12.4	15	112.1	25.9	75	170.5	39.4	35	229.0	52.9	95	287.4	66.4
56	54.6	12.6	16	113.0	26.1	76	171.5	39.6	36	230.0	53.1	96	288.4	66.6
57	55.5	12.8	17	114.0	26.3	77	172.5	39.8	37	230.9	53.3	97	289.4	66.8
58	56.5	13.0	18	115.0	26.5	78	173.4	40.0	38	231.9	53.5	98	290.4	67.0
59	57.5	13.3	19	116.0	26.8	79	174.4	40.3	39	232.9	53.8	99	291.3	67.3
60	58.5	13.5	20	116.9	27.0	80	175.4	40.5	40	233.8	54.0	300	292.3	67.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

77° (103°, 257°, 283°).

TABLE 2.

Difference of Latitude and Departure for 13° (167°, 193°, 347°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	293.3	67.7	361	351.8	81.2	421	410.2	94.7	481	468.7	108.2	541	527.2	121.7
02	294.3	67.9	62	352.7	81.4	22	411.2	94.9	82	469.7	108.4	42	528.1	121.9
03	295.2	68.1	63	353.7	81.6	23	412.2	95.1	83	470.6	108.6	43	529.1	122.1
04	296.2	68.4	64	354.7	81.9	24	413.1	95.3	84	471.6	108.8	44	530.1	122.3
05	297.2	68.6	65	355.6	82.1	25	414.1	95.6	85	472.6	109.0	45	531.1	122.5
06	298.2	68.8	66	356.6	82.3	26	415.1	95.8	86	473.6	109.3	46	532.0	122.8
07	299.1	69.0	67	357.6	82.5	27	416.1	96.0	87	474.5	109.5	47	533.0	123.0
08	300.1	69.3	68	358.6	82.8	28	417.0	96.2	88	475.5	109.7	48	534.0	123.2
09	301.1	69.5	69	359.5	83.0	29	418.0	96.5	89	476.5	109.9	49	535.0	123.4
10	302.1	69.7	70	360.5	83.2	30	419.0	96.7	90	477.5	110.1	50	535.9	123.7
311	303.0	69.9	371	361.5	83.4	431	420.0	96.9	491	478.4	110.4	551	536.9	123.9
12	304.0	70.2	72	362.5	83.7	32	420.9	97.1	92	479.4	110.6	52	537.9	124.1
13	305.0	70.4	73	363.4	83.9	33	421.9	97.4	93	480.4	110.9	53	538.9	124.4
14	306.0	70.6	74	364.4	84.1	34	422.9	97.6	94	481.4	111.1	54	539.8	124.6
15	306.9	70.8	75	365.4	84.3	35	423.9	97.8	95	482.3	111.3	55	540.8	124.9
16	307.9	71.1	76	366.4	84.6	36	424.8	98.0	96	483.3	111.5	56	541.8	125.1
17	308.9	71.3	77	367.3	84.8	37	425.8	98.3	97	484.3	111.8	57	542.8	125.3
18	309.9	71.5	78	368.3	85.0	38	426.8	98.5	98	485.3	112.0	58	543.7	125.5
19	310.8	71.7	79	369.3	85.2	39	427.8	98.7	99	486.2	112.2	59	544.7	125.8
20	311.8	72.0	80	370.3	85.5	40	428.7	98.9	500	487.2	112.4	60	545.7	126.0
321	312.8	72.2	381	371.2	85.7	441	429.7	99.2	501	488.2	112.6	561	546.7	126.2
22	313.8	72.4	82	372.2	85.9	42	430.7	99.4	02	489.2	112.9	62	547.6	126.4
23	314.7	72.6	83	373.2	86.1	43	431.6	99.6	03	490.1	113.1	63	548.6	126.7
24	315.7	72.9	84	374.2	86.4	44	432.6	99.8	04	491.1	113.3	64	549.6	126.9
25	316.7	73.1	85	375.1	86.6	45	433.6	100.1	05	492.1	113.5	65	550.6	127.1
26	317.6	73.3	86	376.1	86.8	46	434.6	100.3	06	493.1	113.8	66	551.5	127.3
27	318.6	73.5	87	377.1	87.0	47	435.5	100.5	07	494.0	114.0	67	552.5	127.6
28	319.6	73.8	88	378.1	87.3	48	436.5	100.7	08	495.0	114.2	68	553.5	127.8
29	320.6	74.0	89	379.0	87.5	49	437.5	101.0	09	496.0	114.5	69	554.5	128.0
30	321.5	74.2	90	380.0	87.7	50	438.5	101.2	10	496.9	114.7	70	555.4	128.3
331	322.5	74.4	391	381.0	87.9	451	439.4	101.4	511	497.9	114.9	571	556.4	128.5
32	323.5	74.7	92	382.0	88.2	52	440.4	101.6	12	498.9	115.1	72	557.4	128.7
33	324.5	74.9	93	382.9	88.4	53	441.4	101.9	13	499.9	115.4	73	558.4	128.9
34	325.4	75.1	94	383.9	88.6	54	442.4	102.1	14	500.8	115.6	74	559.3	129.2
35	326.4	75.3	95	384.9	88.8	55	443.3	102.3	15	501.8	115.8	75	560.3	129.4
36	327.4	75.6	96	385.9	89.1	56	444.3	102.5	16	502.8	116.0	76	561.3	129.6
37	328.4	75.8	97	386.8	89.3	57	445.3	102.8	17	503.8	116.3	77	562.3	129.8
38	329.3	76.0	98	387.8	89.5	58	446.3	103.0	18	504.7	116.5	78	563.2	130.0
39	330.3	76.2	99	388.8	89.7	59	447.2	103.2	19	505.7	116.7	79	564.2	130.2
40	331.3	76.5	400	389.8	90.0	60	448.2	103.4	20	506.7	116.9	80	565.2	130.4
341	332.3	76.7	401	390.7	90.2	461	449.2	103.7	521	507.7	117.2	581	566.2	130.7
42	333.2	76.9	02	391.7	90.4	62	450.2	103.9	22	508.6	117.5	82	567.1	131.0
43	334.2	77.1	03	392.7	90.6	63	451.1	104.1	23	509.6	117.7	83	568.1	131.2
44	335.2	77.4	04	393.6	90.8	64	452.1	104.3	24	510.6	117.9	84	569.1	131.4
45	336.2	77.6	05	394.6	91.1	65	453.1	104.6	25	511.6	118.1	85	570.1	131.6
46	337.1	77.8	06	395.6	91.3	66	454.1	104.8	26	512.5	118.3	86	571.0	131.8
47	338.1	78.0	07	396.6	91.5	67	455.0	105.0	27	513.5	118.5	87	572.0	132.0
48	339.1	78.3	08	397.5	91.7	68	456.0	105.2	28	514.5	118.7	88	573.0	132.3
49	340.1	78.5	09	398.5	92.0	69	457.0	105.5	29	515.5	119.0	89	573.9	132.5
50	341.0	78.7	10	399.5	92.2	70	458.0	105.7	30	516.4	119.2	90	574.9	132.8
351	342.0	78.9	411	400.5	92.4	471	458.9	105.9	531	517.4	119.4	591	575.9	133.0
52	343.0	79.2	12	401.4	92.6	72	459.9	106.1	32	518.4	119.6	92	576.9	133.2
53	344.0	79.4	13	402.4	92.9	73	460.9	106.4	33	519.4	119.9	93	577.8	133.4
54	344.9	79.6	14	403.4	93.1	74	461.9	106.6	34	520.3	120.1	94	578.8	133.6
55	345.9	79.8	15	404.4	93.3	75	462.8	106.8	35	521.3	120.3	95	579.8	133.8
56	346.9	80.1	16	405.3	93.5	76	463.8	107.0	36	522.3	120.5	96	580.8	134.0
57	347.9	80.3	17	406.3	93.8	77	464.8	107.3	37	523.3	120.8	97	581.7	134.3
58	348.8	80.5	18	407.3	94.0	78	465.8	107.5	38	524.2	121.0	98	582.7	134.5
59	349.8	80.7	19	408.3	94.2	79	466.7	107.7	39	525.2	121.2	99	583.7	134.8
60	350.8	81.0	20	409.2	94.4	80	467.7	107.9	40	526.2	121.5	600	584.6	135.0
Dist.	Dep.	Lat.	Dist	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

77° (103°, 257°, 283°).

TABLE 2.

Difference of Latitude and Departure for 14° (166°, 194°, 346°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.2	61	59.2	14.8	121	117.4	29.3	181	175.6	43.8	241	233.8	58.3
2	1.9	0.5	62	60.2	15.0	22	118.4	29.5	82	176.6	44.0	42	234.8	58.5
3	2.9	0.7	63	61.1	15.2	23	119.3	29.8	83	177.6	44.3	43	235.8	58.8
4	3.9	1.0	64	62.1	15.5	24	120.3	30.0	84	178.5	44.5	44	236.8	59.0
5	4.9	1.2	65	63.1	15.7	25	121.3	30.2	85	179.5	44.8	45	237.7	59.3
6	5.8	1.5	66	64.0	16.0	26	122.3	30.5	86	180.5	45.0	46	238.7	59.5
7	6.8	1.7	67	65.0	16.2	27	123.2	30.7	87	181.4	45.2	47	239.7	59.8
8	7.8	1.9	68	66.0	16.5	28	124.2	31.0	88	182.4	45.5	48	240.6	60.0
9	8.7	2.2	69	67.0	16.7	29	125.2	31.2	89	183.4	45.7	49	241.6	60.2
10	9.7	2.4	70	67.9	16.9	30	126.1	31.4	90	184.4	46.0	50	242.6	60.5
11	10.7	2.7	71	68.9	17.2	131	127.1	31.7	191	185.3	46.2	251	243.5	60.7
12	11.6	2.9	72	69.9	17.4	32	128.1	31.9	92	186.3	46.4	52	244.5	61.0
13	12.6	3.1	73	70.8	17.7	33	129.0	32.2	93	187.3	46.7	53	245.5	61.2
14	13.6	3.4	74	71.8	17.9	34	130.0	32.4	94	188.2	46.9	54	246.5	61.4
15	14.6	3.6	75	72.8	18.1	35	131.0	32.7	95	189.2	47.2	55	247.4	61.7
16	15.5	3.9	76	73.7	18.4	36	132.0	32.9	96	190.2	47.4	56	248.4	61.9
17	16.5	4.1	77	74.7	18.6	37	132.9	33.1	97	191.1	47.7	57	249.4	62.2
18	17.5	4.4	78	75.7	18.9	38	133.9	33.4	98	192.1	47.9	58	250.3	62.4
19	18.4	4.6	79	76.7	19.1	39	134.9	33.6	99	193.1	48.1	59	251.3	62.7
20	19.4	4.8	80	77.6	19.4	40	135.8	33.9	200	194.1	48.4	60	252.3	62.9
21	20.4	5.1	81	78.6	19.6	141	136.8	34.1	201	195.0	48.6	261	253.2	63.1
22	21.3	5.3	82	79.6	19.8	42	137.8	34.4	02	196.0	48.9	62	254.2	63.4
23	22.3	5.6	83	80.5	20.1	43	138.8	34.6	03	197.0	49.1	63	255.2	63.6
24	23.3	5.8	84	81.5	20.3	44	139.7	34.8	04	197.9	49.4	64	256.2	63.9
25	24.3	6.0	85	82.5	20.6	45	140.7	35.1	05	198.9	49.6	65	257.1	64.1
26	25.2	6.3	86	83.4	20.8	46	141.7	35.3	06	199.9	49.8	66	258.1	64.4
27	26.2	6.5	87	84.4	21.0	47	142.6	35.6	07	200.9	50.1	67	259.1	64.6
28	27.2	6.8	88	85.4	21.3	48	143.6	35.8	08	201.8	50.3	68	260.0	64.8
29	28.1	7.0	89	86.4	21.5	49	144.6	36.0	09	202.8	50.6	69	261.0	65.1
30	29.1	7.3	90	87.3	21.8	50	145.5	36.3	10	203.8	50.8	70	262.0	65.3
31	30.1	7.5	91	88.3	22.0	151	146.5	36.5	211	204.7	51.0	271	263.0	65.6
32	31.0	7.7	92	89.3	22.3	52	147.5	36.8	12	205.7	51.3	72	263.9	65.8
33	32.0	8.0	93	90.2	22.5	53	148.5	37.0	13	206.7	51.5	73	264.9	66.0
34	33.0	8.2	94	91.2	22.7	54	149.4	37.3	14	207.6	51.8	74	265.9	66.3
35	34.0	8.5	95	92.2	23.0	55	150.4	37.5	15	208.6	52.0	75	266.8	66.5
36	34.9	8.7	96	93.1	23.2	56	151.4	37.7	16	209.6	52.3	76	267.8	66.8
37	35.9	9.0	97	94.1	23.5	57	152.3	38.0	17	210.6	52.5	77	268.8	67.0
38	36.9	9.2	98	95.1	23.7	58	153.3	38.2	18	211.5	52.7	78	269.7	67.3
39	37.8	9.4	99	96.1	24.0	59	154.3	38.5	19	212.5	53.0	79	270.7	67.5
40	38.8	9.7	100	97.0	24.2	60	155.2	38.7	20	213.5	53.2	80	271.7	67.7
41	39.8	9.9	101	98.0	24.4	161	156.2	38.9	221	214.4	53.5	281	272.7	68.0
42	40.8	10.2	02	99.0	24.7	62	157.2	39.2	22	215.4	53.7	82	273.6	68.2
43	41.7	10.4	03	99.9	24.9	63	158.2	39.4	23	216.4	53.9	83	274.6	68.5
44	42.7	10.6	04	100.9	25.2	64	159.1	39.7	24	217.3	54.2	84	275.6	68.7
45	43.7	10.9	05	101.9	25.4	65	160.1	39.9	25	218.3	54.4	85	276.5	68.9
46	44.6	11.1	06	102.9	25.6	66	161.1	40.2	26	219.3	54.7	86	277.5	69.2
47	45.6	11.4	07	103.8	25.9	67	162.0	40.4	27	220.3	54.9	87	278.5	69.4
48	46.6	11.6	08	104.8	26.1	68	163.0	40.6	28	221.2	55.2	88	279.4	69.7
49	47.5	11.9	09	105.8	26.4	69	164.0	40.9	29	222.2	55.4	89	280.4	69.9
50	48.5	12.1	10	106.7	26.6	70	165.0	41.1	30	223.2	55.6	90	281.4	70.2
51	49.5	12.3	111	107.7	26.9	171	165.9	41.4	231	224.1	55.9	291	282.4	70.4
52	50.5	12.6	12	108.7	27.1	72	166.9	41.6	32	225.1	56.1	92	283.3	70.6
53	51.4	12.8	13	109.6	27.3	73	167.9	41.9	33	226.1	56.4	93	284.3	70.9
54	52.4	13.1	14	110.6	27.6	74	168.8	42.1	34	227.0	56.6	94	285.3	71.1
55	53.4	13.3	15	111.6	27.8	75	169.8	42.3	35	228.0	56.9	95	286.2	71.4
56	54.3	13.5	16	112.6	28.1	76	170.8	42.6	36	229.0	57.1	96	287.2	71.6
57	55.3	13.8	17	113.5	28.3	77	171.7	42.8	37	230.0	57.3	97	288.2	71.9
58	56.3	14.0	18	114.5	28.5	78	172.7	43.1	38	230.9	57.6	98	289.1	72.1
59	57.2	14.3	19	115.5	28.8	79	173.7	43.3	39	231.9	57.8	99	290.1	72.3
60	58.2	14.5	20	116.4	29.0	80	174.7	43.5	40	232.9	58.1	300	291.1	72.6
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

76° (104°, 256°, 284°).

Difference of Latitude and Departure for 14° (166°, 194°, 346°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	292.0	72.8	361	350.2	87.3	421	408.5	101.8	481	466.7	116.3	541	525.0	130.9
02	293.0	73.0	62	351.2	87.6	22	409.4	102.1	82	467.7	116.6	42	525.9	131.2
03	294.0	73.3	63	352.2	87.8	23	410.4	102.3	83	468.6	116.8	43	526.9	131.4
04	294.9	73.5	64	353.2	88.0	24	411.4	102.6	84	469.6	117.1	44	527.9	131.6
05	295.9	73.8	65	354.1	88.3	25	412.3	102.8	85	470.6	117.3	45	528.8	131.9
06	296.9	74.0	66	355.1	88.5	26	413.3	103.0	86	471.5	117.6	46	529.8	132.1
07	297.8	74.2	67	356.1	88.8	27	414.3	103.3	87	472.5	117.8	47	530.8	132.3
08	298.8	74.5	68	357.0	89.0	28	415.3	103.5	88	473.5	118.0	48	531.7	132.6
09	299.8	74.7	69	358.0	89.2	29	416.2	103.8	89	474.5	118.3	49	532.7	132.8
10	300.8	75.0	70	359.0	89.5	30	417.2	104.0	90	475.4	118.5	50	533.7	133.0
311	301.7	75.2	371	359.9	89.7	431	418.2	104.2	491	476.4	118.8	551	534.6	133.3
12	302.7	75.5	72	360.9	90.0	32	419.1	104.5	92	477.4	119.0	52	535.6	133.6
13	303.7	75.7	73	361.9	90.2	33	420.1	104.7	93	478.3	119.2	53	536.6	133.8
14	304.6	75.9	74	362.9	90.5	34	421.1	105.0	94	479.3	119.5	54	537.5	134.0
15	305.6	76.2	75	363.8	90.7	35	422.0	105.2	95	480.3	119.7	55	538.5	134.3
16	306.6	76.4	76	364.8	90.9	36	423.0	105.5	96	481.3	120.0	56	539.5	134.5
17	307.6	76.7	77	365.8	91.2	37	424.0	105.7	97	482.2	120.2	57	540.5	134.8
18	308.5	76.9	78	366.7	91.4	38	425.0	105.9	98	483.2	120.4	58	541.4	135.0
19	309.5	77.2	79	367.7	91.7	39	425.9	106.2	99	484.2	120.7	59	542.4	135.2
20	310.5	77.4	80	368.7	91.9	40	426.9	106.4	500	485.1	121.0	60	543.4	135.5
321	311.4	77.6	381	369.6	92.2	441	427.9	106.7	501	486.1	121.2	561	544.3	135.7
22	312.4	77.9	82	370.6	92.4	42	428.8	106.9	02	487.1	121.4	62	545.3	135.9
23	313.4	78.1	83	371.6	92.6	43	429.8	107.1	03	488.0	121.7	63	546.3	136.2
24	314.3	78.4	84	372.6	92.9	44	430.8	107.4	04	489.0	122.0	64	547.2	136.5
25	315.3	78.6	85	373.5	93.1	45	431.7	107.6	05	490.0	122.1	65	548.2	136.6
26	316.3	78.8	86	374.5	93.4	46	432.7	107.9	06	491.0	122.4	66	549.2	136.9
27	317.3	79.1	87	375.5	93.6	47	433.7	108.1	07	491.9	122.6	67	550.1	137.1
28	318.2	79.3	88	376.4	93.8	48	434.7	108.4	08	492.9	122.9	68	551.1	137.4
29	319.2	79.6	89	377.4	94.1	49	435.6	108.6	09	493.9	123.1	69	552.1	137.6
30	320.2	79.8	90	378.4	94.3	50	436.6	108.8	10	494.9	123.4	70	553.1	137.9
331	321.1	80.1	391	379.4	94.6	451	437.6	109.1	511	495.8	123.6	571	554.0	138.1
32	322.1	80.3	92	380.3	94.8	52	438.5	109.3	12	496.8	123.8	72	555.0	138.3
33	323.1	80.5	93	381.3	95.1	53	439.5	109.6	13	497.8	124.1	73	556.0	138.6
34	324.0	80.8	94	382.3	95.3	54	440.5	109.8	14	498.7	124.3	74	557.0	138.8
35	325.0	81.0	95	383.2	95.5	55	441.5	110.1	15	499.7	124.6	75	557.9	139.1
36	326.0	81.3	96	384.2	95.8	56	442.4	110.3	16	500.7	124.8	76	558.9	139.3
37	327.0	81.5	97	385.2	96.0	57	443.4	110.5	17	501.7	125.0	77	559.9	139.5
38	327.9	81.7	98	386.1	96.3	58	444.4	110.8	18	502.6	125.3	78	560.9	139.8
39	328.9	82.0	99	387.1	96.5	59	445.3	111.0	19	503.6	125.6	79	561.8	140.0
40	329.9	82.2	400	388.1	96.7	60	446.3	111.3	20	504.6	125.8	80	562.8	140.3
341	330.8	82.5	401	389.1	97.0	461	447.3	111.5	521	505.5	126.0	581	563.8	140.5
42	331.8	82.7	02	390.0	97.2	62	448.2	111.7	22	506.5	126.2	82	564.7	140.8
43	332.8	83.0	03	391.0	97.5	63	449.2	112.0	23	507.5	126.5	83	565.7	141.0
44	333.7	83.2	04	392.0	97.7	64	450.2	112.2	24	508.4	126.8	84	566.7	141.3
45	334.7	83.4	05	392.9	98.0	65	451.2	112.5	25	509.4	127.0	85	567.6	141.5
46	335.7	83.7	06	393.9	98.2	66	452.1	112.7	26	510.4	127.2	86	568.6	141.8
47	336.7	83.9	07	394.9	98.4	67	453.1	113.0	27	511.4	127.5	87	569.6	142.0
48	337.6	84.2	08	395.8	98.7	68	454.1	113.2	28	512.3	127.8	88	570.6	142.3
49	338.6	84.4	09	396.8	98.9	69	455.0	113.4	29	513.3	128.0	89	571.5	142.5
50	339.6	84.7	10	397.8	99.2	70	456.0	113.7	30	514.3	128.2	90	572.5	142.8
351	340.5	84.9	411	398.8	99.4	471	457.0	113.9	531	515.3	128.5	591	573.5	143.0
52	341.5	85.1	12	399.7	99.7	72	457.9	114.2	32	516.2	128.8	92	574.4	143.3
53	342.5	85.4	13	400.7	99.9	73	458.9	114.4	33	517.2	129.0	93	575.4	143.5
54	343.5	85.6	14	401.7	100.1	74	459.9	114.6	34	518.2	129.2	94	576.4	143.8
55	344.4	85.9	15	402.6	100.4	75	460.9	114.9	35	519.1	129.4	95	577.3	144.0
56	345.4	86.1	16	403.6	100.6	76	461.8	115.1	36	520.1	129.7	96	578.3	144.2
57	346.4	86.3	17	404.6	100.9	77	462.8	115.4	37	521.1	129.9	97	579.3	144.5
58	347.3	86.6	18	405.5	101.1	78	463.8	115.6	38	522.1	130.2	98	580.3	144.7
59	348.3	86.8	19	406.5	101.3	79	464.7	115.9	39	523.0	130.4	99	581.2	144.9
60	349.3	87.1	20	407.5	101.6	80	465.7	116.1	40	524.0	130.6	600	582.2	145.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

76° (104°, 256°, 284°).

TABLE 2.

Difference of Latitude and Departure for 15° (165°, 195°, 345°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.3	61	58.9	15.8	121	116.9	31.3	181	174.8	46.8	241	232.8	62.4
2	1.9	0.5	62	59.9	16.0	22	117.8	31.6	82	175.8	47.1	42	233.8	62.6
3	2.9	0.8	63	60.9	16.3	23	118.8	31.8	83	176.8	47.4	43	234.7	62.9
4	3.9	1.0	64	61.8	16.6	24	119.8	32.1	84	177.7	47.6	44	235.7	63.2
5	4.8	1.3	65	62.8	16.8	25	120.7	32.4	85	178.7	47.9	45	236.7	63.4
6	5.8	1.6	66	63.8	17.1	26	121.7	32.6	86	179.7	48.1	46	237.6	63.7
7	6.8	1.8	67	64.7	17.3	27	122.7	32.9	87	180.6	48.4	47	238.6	63.9
8	7.7	2.1	68	65.7	17.6	28	123.6	33.1	88	181.6	48.7	48	239.5	64.2
9	8.7	2.3	69	66.6	17.9	29	124.6	33.4	89	182.6	48.9	49	240.5	64.4
10	9.7	2.6	70	67.6	18.1	30	125.6	33.6	90	183.5	49.2	50	241.5	64.7
11	10.6	2.8	71	68.6	18.4	131	126.5	33.9	191	184.5	49.4	251	242.4	65.0
12	11.6	3.1	72	69.5	18.6	32	127.5	34.2	92	185.5	49.7	52	243.4	65.2
13	12.6	3.4	73	70.5	18.9	33	128.5	34.4	93	186.4	50.0	53	244.4	65.5
14	13.5	3.6	74	71.5	19.2	34	129.4	34.7	94	187.4	50.2	54	245.3	65.7
15	14.5	3.9	75	72.4	19.4	35	130.4	34.9	95	188.4	50.5	55	246.3	66.0
16	15.5	4.1	76	73.4	19.7	36	131.4	35.2	96	189.3	50.7	56	247.3	66.3
17	16.4	4.4	77	74.4	19.9	37	132.3	35.5	97	190.3	51.0	57	248.2	66.5
18	17.4	4.7	78	75.3	20.2	38	133.3	35.7	98	191.3	51.2	58	249.2	66.8
19	18.4	4.9	79	76.3	20.4	39	134.3	36.0	99	192.2	51.5	59	250.2	67.0
20	19.3	5.2	80	77.3	20.7	40	135.2	36.2	200	193.2	51.8	60	251.1	67.3
21	20.3	5.4	81	78.2	21.0	141	136.2	36.5	201	194.2	52.0	261	252.1	67.6
22	21.3	5.7	82	79.2	21.2	42	137.2	36.8	02	195.1	52.3	62	253.1	67.8
23	22.2	6.0	83	80.2	21.5	43	138.1	37.0	03	196.1	52.5	63	254.0	68.1
24	23.2	6.2	84	81.1	21.7	44	139.1	37.3	04	197.0	52.8	64	255.0	68.3
25	24.1	6.5	85	82.1	22.0	45	140.1	37.5	05	198.0	53.1	65	256.0	68.6
26	25.1	6.7	86	83.1	22.3	46	141.0	37.8	06	199.0	53.3	66	256.9	68.8
27	26.1	7.0	87	84.0	22.5	47	142.0	38.0	07	199.9	53.6	67	257.9	69.1
28	27.0	7.2	88	85.0	22.8	48	143.0	38.3	08	200.9	53.8	68	258.9	69.4
29	28.0	7.5	89	86.0	23.0	49	143.9	38.6	09	201.9	54.1	69	259.8	69.6
30	29.0	7.8	90	86.9	23.3	50	144.9	38.8	10	202.8	54.4	70	260.8	69.9
31	29.9	8.0	91	87.9	23.6	151	145.9	39.1	211	203.8	54.6	271	261.8	70.1
32	30.9	8.3	92	88.9	23.8	52	146.8	39.3	12	204.8	54.9	72	262.7	70.4
33	31.9	8.5	93	89.8	24.1	53	147.8	39.6	13	205.7	55.1	73	263.7	70.7
34	32.8	8.8	94	90.8	24.3	54	148.8	39.9	14	206.7	55.4	74	264.7	70.9
35	33.8	9.1	95	91.8	24.6	55	149.7	40.1	15	207.7	55.6	75	265.6	71.2
36	34.8	9.3	96	92.7	24.8	56	150.7	40.4	16	208.6	55.9	76	266.6	71.4
37	35.7	9.6	97	93.7	25.1	57	151.7	40.6	17	209.6	56.2	77	267.6	71.7
38	36.7	9.8	98	94.7	25.4	58	152.6	40.9	18	210.6	56.4	78	268.5	72.0
39	37.7	10.1	99	95.6	25.6	59	153.6	41.2	19	211.5	56.7	79	269.5	72.2
40	38.6	10.4	100	96.6	25.9	60	154.5	41.4	20	212.5	56.9	80	270.5	72.5
41	39.6	10.6	101	97.6	26.1	161	155.5	41.7	221	213.5	57.2	281	271.4	72.7
42	40.6	10.9	02	98.5	26.4	62	156.5	41.9	22	214.4	57.5	82	272.4	73.0
43	41.5	11.1	03	99.5	26.7	63	157.4	42.2	23	215.4	57.7	83	273.4	73.2
44	42.5	11.4	04	100.5	26.9	64	158.4	42.4	24	216.4	58.0	84	274.3	73.5
45	43.5	11.6	05	101.4	27.2	65	159.4	42.7	25	217.3	58.2	85	275.3	73.8
46	44.4	11.9	06	102.4	27.4	66	160.3	43.0	26	218.3	58.5	86	276.3	74.0
47	45.4	12.2	07	103.4	27.7	67	161.3	43.2	27	219.3	58.8	87	277.2	74.3
48	46.4	12.4	08	104.3	28.0	68	162.3	43.5	28	220.2	59.0	88	278.2	74.5
49	47.3	12.7	09	105.3	28.2	69	163.2	43.7	29	221.2	59.3	89	279.2	74.8
50	48.3	12.9	10	106.3	28.5	70	164.2	44.0	30	222.2	59.5	90	280.1	75.1
51	49.3	13.2	111	107.2	28.7	171	165.2	44.3	231	223.1	59.8	291	281.1	75.3
52	50.2	13.5	12	108.2	29.0	72	166.1	44.5	32	224.1	60.0	92	282.1	75.6
53	51.2	13.7	13	109.1	29.2	73	167.1	44.8	33	225.1	60.3	93	283.0	75.8
54	52.2	14.0	14	110.1	29.5	74	168.1	45.0	34	226.0	60.6	94	284.0	76.1
55	53.1	14.2	15	111.1	29.8	75	169.0	45.3	35	227.0	60.8	95	284.9	76.4
56	54.1	14.5	16	112.0	30.0	76	170.0	45.6	36	228.0	61.1	96	285.9	76.6
57	55.1	14.8	17	113.0	30.3	77	171.0	45.8	37	228.9	61.3	97	286.9	76.9
58	56.0	15.0	18	114.0	30.5	78	171.9	46.1	38	229.9	61.6	98	287.8	77.1
59	57.0	15.3	19	114.9	30.8	79	172.9	46.3	39	230.9	61.9	99	288.8	77.4
60	58.0	15.5	20	115.9	31.1	80	173.9	46.6	40	231.8	62.1	300	289.8	77.6
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

75° (105°, 255°, 285°).

Difference of Latitude and Departure for 15° (165°, 195°, 345°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	290.7	77.9	361	348.7	93.4	421	406.6	109.0	481	464.6	124.5	541	522.6	140.0
02	291.7	78.2	62	349.6	93.7	22	407.6	109.2	82	465.6	124.8	42	523.5	140.3
03	292.7	78.4	63	350.6	94.0	23	408.6	109.5	83	466.5	125.0	43	524.5	140.5
04	293.6	78.7	64	351.6	94.2	24	409.5	109.7	84	467.5	125.3	44	525.5	140.8
05	294.6	78.9	65	352.5	94.5	25	410.5	110.0	85	468.5	125.6	45	526.4	141.1
06	295.6	79.2	66	353.5	94.7	26	411.5	110.3	86	469.4	125.8	46	527.4	141.4
07	296.5	79.5	67	354.5	95.0	27	412.4	110.5	87	470.4	126.1	47	528.4	141.6
08	297.5	79.7	68	355.4	95.3	28	413.4	110.8	88	471.4	126.4	48	529.3	141.9
09	298.4	80.0	69	356.4	95.5	29	414.4	111.0	89	472.3	126.6	49	530.3	142.1
10	299.4	80.2	70	357.4	95.8	30	415.3	111.3	90	473.3	126.9	50	531.3	142.4
311	300.4	80.5	371	358.3	96.0	431	416.3	111.6	491	474.3	127.1	551	532.2	142.6
12	301.3	80.8	72	359.3	96.3	32	417.3	111.8	92	475.2	127.4	52	533.2	142.9
13	302.3	81.0	73	360.3	96.5	33	418.2	112.1	93	476.2	127.6	53	534.2	143.1
14	303.3	81.3	74	361.2	96.8	34	419.2	112.3	94	477.2	127.9	54	535.1	143.4
15	304.2	81.5	75	362.2	97.1	35	420.2	112.6	95	478.1	128.1	55	536.1	143.7
16	305.2	81.8	76	363.2	97.3	36	421.1	112.9	96	479.1	128.4	56	537.1	143.9
17	306.2	82.1	77	364.1	97.6	37	422.1	113.1	97	480.1	128.6	57	538.0	144.2
18	307.1	82.3	78	365.1	97.8	38	423.1	113.4	98	481.0	128.9	58	539.0	144.4
19	308.1	82.6	79	366.1	98.1	39	424.0	113.6	99	482.0	129.1	59	540.0	144.7
20	309.1	82.8	80	367.0	98.4	40	425.0	113.9	500	483.0	129.4	60	540.9	144.9
321	310.0	83.1	381	368.0	98.6	441	426.0	114.1	501	483.9	129.7	561	541.9	145.2
22	311.0	83.3	82	369.0	98.9	42	426.9	114.4	02	484.9	129.9	62	542.9	145.4
23	312.0	83.6	83	369.9	99.1	43	427.9	114.7	03	485.9	130.2	63	543.8	145.7
24	312.9	83.9	84	370.9	99.4	44	428.8	114.9	04	486.8	130.4	64	544.8	146.0
25	313.9	84.1	85	371.9	99.6	45	429.8	115.2	05	487.8	130.7	65	545.8	146.2
26	314.9	84.4	86	372.8	99.9	46	430.8	115.4	06	488.8	131.0	66	546.7	146.5
27	315.8	84.6	87	373.8	100.2	47	431.7	115.7	07	489.7	131.2	67	547.7	146.7
28	316.8	84.9	88	374.8	100.4	48	432.7	116.0	08	490.7	131.5	68	548.7	147.0
29	317.8	85.1	89	375.7	100.7	49	433.7	116.2	09	491.7	131.7	69	549.6	147.2
30	318.7	85.4	90	376.7	100.9	50	434.6	116.5	10	492.6	132.0	70	550.6	147.5
331	319.7	85.7	391	377.7	101.2	451	435.6	116.7	511	493.6	132.3	571	551.6	147.8
32	320.7	85.9	92	378.6	101.5	52	436.6	117.0	12	494.5	132.5	72	552.5	148.0
33	321.6	86.2	93	379.6	101.7	53	437.5	117.3	13	495.5	132.8	73	553.5	148.3
34	322.6	86.5	94	380.6	102.0	54	438.5	117.5	14	496.5	133.0	74	554.4	148.5
35	323.6	86.7	95	381.5	102.2	55	439.5	117.8	15	497.4	133.3	75	555.4	148.8
36	324.5	87.0	96	382.5	102.5	56	440.4	118.0	16	498.4	133.5	76	556.4	149.0
37	325.5	87.2	97	383.4	102.8	57	441.4	118.3	17	499.4	133.8	77	557.3	149.3
38	326.5	87.5	98	384.4	103.0	58	442.4	118.5	18	500.3	134.0	78	558.3	149.5
39	327.4	87.7	99	385.4	103.3	59	443.3	118.8	19	501.3	134.3	79	559.3	149.8
40	328.4	88.0	400	386.3	103.5	60	444.3	119.1	20	502.3	134.6	80	560.2	150.1
341	329.4	88.3	401	387.3	103.8	461	445.3	119.3	521	503.2	134.8	581	561.2	150.3
42	330.3	88.5	02	388.3	104.1	62	446.2	119.6	22	504.2	135.1	82	562.2	150.6
43	331.3	88.8	03	389.2	104.3	63	447.2	119.8	23	505.2	135.3	83	563.1	150.8
44	332.3	89.0	04	390.2	104.6	64	448.2	120.1	24	506.1	135.6	84	564.1	151.1
45	333.2	89.3	05	391.2	104.8	65	449.1	120.4	25	507.1	135.9	85	565.1	151.4
46	334.2	89.6	06	392.1	105.1	66	450.1	120.6	26	508.1	136.1	86	566.0	151.6
47	335.2	89.8	07	393.1	105.3	67	451.1	120.9	27	509.0	136.4	87	567.0	151.9
48	336.1	90.1	08	394.1	105.6	68	452.0	121.1	28	510.0	136.6	88	568.0	152.2
49	337.1	90.3	09	395.0	105.9	69	453.0	121.4	29	511.0	136.9	89	568.9	152.4
50	338.1	90.6	10	396.0	106.1	70	454.0	121.7	30	511.9	137.2	90	569.9	152.7
351	339.0	90.9	411	397.0	106.4	471	454.9	121.9	531	512.9	137.4	591	570.9	153.0
52	340.0	91.1	12	397.9	106.6	72	455.9	122.2	32	513.9	137.7	92	571.8	153.2
53	340.9	91.4	13	398.9	106.9	73	456.9	122.4	33	514.8	137.9	93	572.8	153.5
54	341.9	91.6	14	399.9	107.2	74	457.8	122.7	34	515.8	138.2	94	573.8	153.7
55	342.9	91.9	15	400.8	107.4	75	458.8	122.9	35	516.8	138.4	95	574.7	154.0
56	343.8	92.1	16	401.8	107.7	76	459.8	123.2	36	517.7	138.7	96	575.7	154.2
57	344.8	92.4	17	402.8	107.9	77	460.7	123.5	37	518.7	139.0	97	576.7	154.5
58	345.8	92.7	18	403.7	108.2	78	461.7	123.7	38	519.7	139.2	98	577.6	154.8
59	346.7	92.9	19	404.7	108.5	79	462.7	124.0	39	520.6	139.5	99	578.6	155.0
60	347.7	93.2	20	405.7	108.7	80	463.6	124.2	40	521.6	139.7	600	579.5	155.3
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

75° (105°, 255°, 285°).

TABLE 2.

Difference of Latitude and Departure for 16° (164°, 196°, 344°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.3	61	58.6	16.8	121	116.3	33.4	181	174.0	49.9	241	231.7	66.4
2	1.9	0.6	62	59.6	17.1	22	117.3	33.6	82	174.9	50.2	42	232.6	66.7
3	2.9	0.8	63	60.6	17.4	23	118.2	33.9	83	175.9	50.4	43	233.6	67.0
4	3.8	1.1	64	61.5	17.6	24	119.2	34.2	84	176.9	50.7	44	234.5	67.3
5	4.8	1.4	65	62.5	17.9	25	120.2	34.5	85	177.8	51.0	45	235.5	67.5
6	5.8	1.7	66	63.4	18.2	26	121.1	34.7	86	178.8	51.3	46	236.5	67.8
7	6.7	1.9	67	64.4	18.5	27	122.1	35.0	87	179.8	51.5	47	237.4	68.1
8	7.7	2.2	68	65.4	18.7	28	123.0	35.3	88	180.7	51.8	48	238.4	68.4
9	8.7	2.5	69	66.3	19.0	29	124.0	35.6	89	181.7	52.1	49	239.4	68.6
10	9.6	2.8	70	67.3	19.3	30	125.0	35.8	90	182.6	52.4	50	240.3	68.9
11	10.6	3.0	71	68.2	19.6	131	125.9	36.1	191	183.6	52.6	251	241.3	69.2
12	11.5	3.3	72	69.2	19.8	32	126.9	36.4	92	184.6	52.9	52	242.2	69.5
13	12.5	3.6	73	70.2	20.1	33	127.8	36.7	93	185.5	53.2	53	243.2	69.7
14	13.5	3.9	74	71.1	20.4	34	128.8	36.9	94	186.5	53.5	54	244.2	70.0
15	14.4	4.1	75	72.1	20.7	35	129.8	37.2	95	187.4	53.7	55	245.1	70.3
16	15.4	4.4	76	73.1	20.9	36	130.7	37.5	96	188.4	54.0	56	246.1	70.6
17	16.3	4.7	77	74.0	21.2	37	131.7	37.8	97	189.4	54.3	57	247.0	70.8
18	17.3	5.0	78	75.0	21.5	38	132.7	38.0	98	190.3	54.6	58	248.0	71.1
19	18.3	5.2	79	75.9	21.8	39	133.6	38.3	99	191.3	54.9	59	249.0	71.4
20	19.2	5.5	80	76.9	22.1	40	134.6	38.6	200	192.3	55.1	60	249.9	71.7
21	20.2	5.8	81	77.9	22.3	141	135.5	38.9	201	193.2	55.4	261	250.9	71.9
22	21.1	6.1	82	78.8	22.6	42	136.5	39.1	02	194.2	55.7	62	251.9	72.2
23	22.1	6.3	83	79.8	22.9	43	137.5	39.4	03	195.1	56.0	63	252.8	72.5
24	23.1	6.6	84	80.7	23.2	44	138.4	39.7	04	196.1	56.2	64	253.8	72.8
25	24.0	6.9	85	81.7	23.4	45	139.4	40.0	05	197.1	56.5	65	254.7	73.0
26	25.0	7.2	86	82.7	23.7	46	140.3	40.2	06	198.0	56.8	66	255.7	73.3
27	26.0	7.4	87	83.6	24.0	47	141.3	40.5	07	199.0	57.1	67	256.7	73.6
28	26.9	7.7	88	84.6	24.3	48	142.3	40.8	08	199.9	57.3	68	257.6	73.9
29	27.9	8.0	89	85.6	24.5	49	143.2	41.1	09	200.9	57.6	69	258.6	74.1
30	28.8	8.3	90	86.5	24.8	50	144.2	41.3	10	201.9	57.9	70	259.5	74.4
31	29.8	8.5	91	87.5	25.1	151	145.2	41.6	211	202.8	58.2	271	260.5	74.7
32	30.8	8.8	92	88.4	25.4	52	146.1	41.9	12	203.8	58.4	72	261.5	75.0
33	31.7	9.1	93	89.4	25.6	53	147.1	42.2	13	204.7	58.7	73	262.4	75.2
34	32.7	9.4	94	90.4	25.9	54	148.0	42.4	14	205.7	59.0	74	263.4	75.5
35	33.6	9.6	95	91.3	26.2	55	149.0	42.7	15	206.7	59.3	75	264.3	75.8
36	34.6	9.9	96	92.3	26.5	56	150.0	43.0	16	207.6	59.5	76	265.3	76.1
37	35.6	10.2	97	93.2	26.7	57	150.9	43.3	17	208.6	59.8	77	266.3	76.4
38	36.5	10.5	98	94.2	27.0	58	151.9	43.6	18	209.6	60.1	78	267.2	76.6
39	37.5	10.7	99	95.2	27.3	59	152.8	43.8	19	210.5	60.4	79	268.2	76.9
40	38.5	11.0	100	96.1	27.6	60	153.8	44.1	20	211.5	60.6	80	269.2	77.2
41	39.4	11.3	101	97.1	27.8	161	154.8	44.4	221	212.4	60.9	281	270.1	77.5
42	40.4	11.6	02	98.0	28.1	62	155.7	44.7	22	213.4	61.2	82	271.1	77.7
43	41.3	11.9	03	99.0	28.4	63	156.7	44.9	23	214.4	61.5	83	272.0	78.0
44	42.3	12.1	04	100.0	28.7	64	157.6	45.2	24	215.3	61.7	84	273.0	78.3
45	43.3	12.4	05	100.9	28.9	65	158.6	45.5	25	216.3	62.0	85	274.0	78.6
46	44.2	12.7	06	101.9	29.2	66	159.6	45.8	26	217.2	62.3	86	274.9	78.8
47	45.2	13.0	07	102.9	29.5	67	160.5	46.0	27	218.2	62.6	87	275.9	79.1
48	46.1	13.2	08	103.8	29.8	68	161.5	46.3	28	219.2	62.8	88	276.8	79.4
49	47.1	13.5	09	104.8	30.0	69	162.5	46.6	29	220.1	63.1	89	277.8	79.7
50	48.1	13.8	10	105.7	30.3	70	163.4	46.9	30	221.1	63.4	90	278.8	79.9
51	49.0	14.1	111	106.7	30.6	171	164.4	47.1	231	222.1	63.7	291	279.7	80.2
52	50.0	14.3	12	107.7	30.9	72	165.3	47.4	32	223.0	63.9	92	280.7	80.5
53	50.9	14.6	13	108.6	31.1	73	166.3	47.7	33	224.0	64.2	93	281.6	80.8
54	51.9	14.9	14	109.6	31.4	74	167.3	48.0	34	224.9	64.5	94	282.6	81.0
55	52.9	15.2	15	110.5	31.7	75	168.2	48.2	35	225.9	64.8	95	283.6	81.3
56	53.8	15.4	16	111.5	32.0	76	169.2	48.5	36	226.9	65.1	96	284.5	81.6
57	54.8	15.7	17	112.5	32.2	77	170.1	48.8	37	227.8	65.3	97	285.5	81.9
58	55.8	16.0	18	113.4	32.5	78	171.1	49.1	38	228.8	65.6	98	286.5	82.1
59	56.7	16.3	19	114.4	32.8	79	172.1	49.3	39	229.7	65.9	99	287.4	82.4
60	57.7	16.5	20	115.4	33.1	80	173.0	49.6	40	230.7	66.2	300	288.4	82.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

74° (106°, 254°, 286°).

TABLE 2.

Difference of Latitude and Departure for 16° (164°, 196°, 344°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	289.3	82.9	361	347.0	99.5	421	404.7	116.0	481	462.4	132.5	541	520.1	149.1
02	290.3	83.2	62	348.0	99.7	22	405.6	116.3	82	463.3	132.8	42	521.0	149.4
03	291.2	83.5	63	348.9	100.0	23	406.6	116.6	83	464.3	133.1	43	522.0	149.7
04	292.2	83.8	64	349.9	100.3	24	407.6	116.8	84	465.2	133.4	44	523.0	150.0
05	293.2	84.0	65	350.8	100.6	25	408.5	117.1	85	466.2	133.6	45	523.9	150.2
06	294.1	84.3	66	351.8	100.8	26	409.5	117.4	86	467.2	133.9	46	524.9	150.4
07	295.1	84.6	67	352.8	101.1	27	410.4	117.7	87	468.1	134.2	47	525.9	150.7
08	296.0	84.9	68	353.7	101.4	28	411.4	117.9	88	469.1	134.5	48	526.8	151.0
09	297.0	85.1	69	354.7	101.7	29	412.4	118.2	89	470.1	134.8	49	527.8	151.3
10	298.0	85.4	70	355.6	101.9	30	413.3	118.5	90	471.0	135.0	50	528.7	151.6
311	298.9	85.7	371	356.6	102.2	431	414.3	118.8	491	472.0	135.3	551	529.7	151.9
12	299.9	86.0	72	357.6	102.5	32	415.2	119.0	92	472.9	135.6	52	530.6	152.2
13	300.9	86.2	73	358.5	102.8	33	416.2	119.3	93	473.9	135.9	53	531.6	152.5
14	301.8	86.5	74	359.5	103.1	34	417.2	119.6	94	474.9	136.2	54	532.6	152.8
15	302.8	86.8	75	360.4	103.3	35	418.1	119.9	95	475.8	136.4	55	533.5	153.0
16	303.7	87.1	76	361.4	103.6	36	419.1	120.1	96	476.8	136.7	56	534.5	153.2
17	304.7	87.3	77	362.4	103.9	37	420.0	120.4	97	477.7	137.0	57	535.4	153.5
18	305.7	87.6	78	363.3	104.2	38	421.0	120.7	98	478.7	137.3	58	536.4	153.8
19	306.6	87.9	79	364.3	104.4	39	422.0	121.0	99	479.7	137.5	59	537.4	154.1
20	307.6	88.2	80	365.3	104.7	40	422.9	121.2	500	480.6	137.8	60	538.3	154.4
321	308.5	88.4	381	366.2	105.0	441	423.9	121.5	501	481.6	138.1	561	539.3	154.7
22	309.5	88.7	82	367.2	105.3	42	424.9	121.8	02	482.6	138.3	62	540.3	154.9
23	310.5	89.0	83	368.1	105.5	43	425.8	122.1	03	483.5	138.6	63	541.2	155.2
24	311.4	89.3	84	369.1	105.8	44	426.8	122.3	04	484.5	138.9	64	542.2	155.4
25	312.4	89.5	85	370.1	106.1	45	427.7	122.6	05	485.4	139.2	65	543.1	155.7
26	313.3	89.8	86	371.0	106.4	46	428.7	122.9	06	486.4	139.4	66	544.1	156.0
27	314.3	90.1	87	372.0	106.6	47	429.7	123.2	07	487.3	139.7	67	545.1	156.3
28	315.3	90.4	88	372.9	106.9	48	430.6	123.4	08	488.3	140.0	68	546.0	156.6
29	316.2	90.6	89	373.9	107.2	49	431.6	123.7	09	489.3	140.3	69	547.0	156.9
30	317.2	90.9	90	374.9	107.5	50	432.6	124.0	10	490.2	140.6	70	547.9	157.1
331	318.2	91.2	391	375.8	107.7	451	433.5	124.3	511	491.2	140.8	571	548.9	157.3
32	319.1	91.5	92	376.8	108.0	52	434.5	124.6	12	492.1	141.1	72	549.8	157.6
33	320.1	91.8	93	377.8	108.3	53	435.4	124.8	13	493.1	141.4	73	550.8	157.9
34	321.0	92.0	94	378.7	108.6	54	436.4	125.1	14	494.1	141.7	74	551.8	158.2
35	322.0	92.3	95	379.7	108.8	55	437.4	125.4	15	495.0	141.9	75	552.7	158.4
36	323.0	92.6	96	380.6	109.1	56	438.3	125.7	16	496.0	142.2	76	553.7	158.7
37	323.9	92.9	97	381.6	109.4	57	439.3	125.9	17	496.9	142.5	77	554.6	159.0
38	324.9	93.1	98	382.6	109.7	58	440.2	126.2	18	497.9	142.8	78	555.6	159.3
39	325.8	93.4	99	383.5	109.9	59	441.2	126.5	19	498.9	143.0	79	556.5	159.5
40	326.8	93.7	400	384.5	110.2	60	442.2	126.8	20	499.8	143.3	80	557.5	159.8
341	327.8	94.0	401	385.4	110.5	461	443.1	127.0	521	500.8	143.6	581	558.4	160.1
42	328.7	94.2	02	386.4	110.8	62	444.1	127.3	22	501.7	143.9	82	559.4	160.4
43	329.7	94.5	03	387.4	111.0	63	445.0	127.6	23	502.7	144.1	83	560.4	160.6
44	330.7	94.8	04	388.3	111.3	64	446.0	127.9	24	503.7	144.4	84	561.3	161.0
45	331.6	95.1	05	389.3	111.6	65	447.0	128.1	25	504.6	144.7	85	562.3	161.3
46	332.6	95.3	06	390.2	111.9	66	447.9	128.4	26	505.6	145.0	86	563.2	161.6
47	333.5	95.6	07	391.2	112.1	67	448.9	128.7	27	506.6	145.3	87	564.2	161.8
48	334.5	95.9	08	392.2	112.4	68	449.8	129.0	28	507.5	145.6	88	565.2	162.1
49	335.5	96.2	09	393.1	112.7	69	450.8	129.2	29	508.5	145.8	89	566.1	162.4
50	336.4	96.4	10	394.1	113.0	70	451.8	129.5	30	509.4	146.1	90	567.1	162.7
351	337.4	96.7	411	395.1	113.3	471	452.7	129.8	531	510.4	146.4	591	568.1	162.9
52	338.3	97.0	12	396.0	113.5	72	453.7	130.1	32	511.4	146.7	92	569.0	163.2
53	339.3	97.3	13	397.0	113.8	73	454.7	130.3	33	512.3	146.9	93	570.0	163.5
54	340.3	97.5	14	397.9	114.1	74	455.6	130.6	34	513.3	147.2	94	571.0	163.8
55	341.2	97.8	15	398.9	114.4	75	456.6	130.9	35	514.3	147.5	95	571.9	164.0
56	342.2	98.1	16	399.9	114.6	76	457.5	131.2	36	515.2	147.8	96	572.9	164.3
57	343.1	98.4	17	400.8	114.9	77	458.5	131.4	37	516.2	148.0	97	573.9	164.6
58	344.1	98.6	18	401.8	115.2	78	459.5	131.7	38	517.2	148.2	98	574.8	164.9
59	345.1	98.9	19	402.7	115.5	79	460.4	132.0	39	518.1	148.5	99	575.8	165.1
60	346.0	99.2	20	403.7	115.8	80	461.4	132.3	40	519.1	148.8	600	576.8	165.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

74° (106°, 254°, 286°).

TABLE 2.

Difference of Latitude and Departure for 17° (163°, 197°, 343°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.3	61	58.3	17.8	121	115.7	35.4	181	173.1	52.9	241	230.5	70.5
2	1.9	0.6	62	59.3	18.1	22	116.7	35.7	82	174.0	53.2	42	231.4	70.8
3	2.9	0.9	63	60.2	18.4	23	117.6	36.0	83	175.0	53.5	43	232.4	71.0
4	3.8	1.2	64	61.2	18.7	24	118.6	36.3	84	176.0	53.8	44	233.3	71.3
5	4.8	1.5	65	62.2	19.0	25	119.5	36.5	85	176.9	54.1	45	234.3	71.6
6	5.7	1.8	66	63.1	19.3	26	120.5	36.8	86	177.9	54.4	46	235.3	71.9
7	6.7	2.0	67	64.1	19.6	27	121.5	37.1	87	178.8	54.7	47	236.2	72.2
8	7.7	2.3	68	65.0	19.9	28	122.4	37.4	88	179.8	55.0	48	237.2	72.5
9	8.6	2.6	69	66.0	20.2	29	123.4	37.7	89	180.7	55.3	49	238.1	72.8
10	9.6	2.9	70	66.9	20.5	30	124.3	38.0	90	181.7	55.6	50	239.1	73.1
11	10.5	3.2	71	67.9	20.8	131	125.3	38.3	191	182.7	55.8	251	240.0	73.4
12	11.5	3.5	72	68.9	21.1	32	126.2	38.6	92	183.6	56.1	52	241.0	73.7
13	12.4	3.8	73	69.8	21.3	33	127.2	38.9	93	184.6	56.4	53	241.9	74.0
14	13.4	4.1	74	70.8	21.6	34	128.1	39.2	94	185.5	56.7	54	242.9	74.3
15	14.3	4.4	75	71.7	21.9	35	129.1	39.5	95	186.5	57.0	55	243.9	74.6
16	15.3	4.7	76	72.7	22.2	36	130.1	39.8	96	187.4	57.3	56	244.8	74.8
17	16.3	5.0	77	73.6	22.5	37	131.0	40.1	97	188.4	57.6	57	245.8	75.1
18	17.2	5.3	78	74.6	22.8	38	132.0	40.3	98	189.3	57.9	58	246.7	75.4
19	18.2	5.6	79	75.5	23.1	39	132.9	40.6	99	190.3	58.2	59	247.7	75.7
20	19.1	5.8	80	76.5	23.4	40	133.9	40.9	200	191.3	58.5	60	248.6	76.0
21	20.1	6.1	81	77.5	23.7	141	134.8	41.2	201	192.2	58.8	261	249.6	76.3
22	21.0	6.4	82	78.4	24.0	42	135.8	41.5	02	193.2	59.1	62	250.6	76.6
23	22.0	6.7	83	79.4	24.3	43	136.8	41.8	03	194.1	59.4	63	251.5	76.9
24	23.0	7.0	84	80.3	24.6	44	137.7	42.1	04	195.1	59.6	64	252.5	77.2
25	23.9	7.3	85	81.3	24.9	45	138.7	42.4	05	196.0	59.9	65	253.4	77.5
26	24.9	7.6	86	82.2	25.1	46	139.6	42.7	06	197.0	60.2	66	254.4	77.8
27	25.8	7.9	87	83.2	25.4	47	140.6	43.0	07	198.0	60.5	67	255.3	78.1
28	26.8	8.2	88	84.2	25.7	48	141.5	43.3	08	198.9	60.8	68	256.3	78.4
29	27.7	8.5	89	85.1	26.0	49	142.5	43.6	09	199.9	61.1	69	257.2	78.6
30	28.7	8.8	90	86.1	26.3	50	143.4	43.9	10	200.8	61.4	70	258.2	78.9
31	29.6	9.1	91	87.0	26.6	151	144.4	44.1	211	201.8	61.7	271	259.2	79.2
32	30.6	9.4	92	88.0	26.9	52	145.4	44.4	12	202.7	62.0	72	260.1	79.5
33	31.6	9.6	93	88.9	27.2	53	146.3	44.7	13	203.7	62.3	73	261.1	79.8
34	32.5	9.9	94	89.9	27.5	54	147.3	45.0	14	204.6	62.6	74	262.0	80.1
35	33.5	10.2	95	90.8	27.8	55	148.2	45.3	15	205.6	62.9	75	263.0	80.4
36	34.4	10.5	96	91.8	28.1	56	149.2	45.6	16	206.6	63.2	76	263.9	80.7
37	35.4	10.8	97	92.8	28.4	57	150.1	45.9	17	207.5	63.4	77	264.9	81.0
38	36.3	11.1	98	93.7	28.7	58	151.1	46.2	18	208.5	63.7	78	265.9	81.3
39	37.3	11.4	99	94.7	28.9	59	152.1	46.5	19	209.4	64.0	79	266.8	81.6
40	38.3	11.7	100	95.6	29.2	60	153.0	46.8	20	210.4	64.3	80	267.8	81.9
41	39.2	12.0	101	96.6	29.5	161	154.0	47.1	221	211.3	64.6	281	268.7	82.2
42	40.2	12.3	02	97.5	29.8	62	154.9	47.4	22	212.3	64.9	82	269.7	82.4
43	41.1	12.6	03	98.5	30.1	63	155.9	47.7	23	213.3	65.2	83	270.6	82.7
44	42.1	12.9	04	99.5	30.4	64	156.8	47.9	24	214.2	65.5	84	271.6	83.0
45	43.0	13.2	05	100.4	30.7	65	157.8	48.2	25	215.2	65.8	85	272.5	83.3
46	44.0	13.4	06	101.4	31.0	66	158.7	48.5	26	216.1	66.1	86	273.5	83.6
47	44.9	13.7	07	102.3	31.3	67	159.7	48.8	27	217.1	66.4	87	274.5	83.9
48	45.9	14.0	08	103.3	31.6	68	160.7	49.1	28	218.0	66.7	88	275.4	84.2
49	46.9	14.3	09	104.2	31.9	69	161.6	49.4	29	219.0	67.0	89	276.4	84.5
50	47.8	14.6	10	105.2	32.2	70	162.6	49.7	30	220.0	67.2	90	277.3	84.8
51	48.8	14.9	111	106.1	32.5	171	163.5	50.0	231	220.9	67.5	291	278.3	85.1
52	49.7	15.2	12	107.1	32.7	72	164.5	50.3	32	221.9	67.8	92	279.2	85.4
53	50.7	15.5	13	108.1	33.0	73	165.4	50.6	33	222.8	68.1	93	280.2	85.7
54	51.6	15.8	14	109.0	33.3	74	166.4	50.9	34	223.8	68.4	94	281.2	86.0
55	52.6	16.1	15	110.0	33.6	75	167.4	51.2	35	224.7	68.7	95	282.1	86.2
56	53.6	16.4	16	110.9	33.9	76	168.3	51.5	36	225.7	69.0	96	283.1	86.5
57	54.5	16.7	17	111.9	34.2	77	169.3	51.7	37	226.6	69.3	97	284.0	86.8
58	55.5	17.0	18	112.8	34.5	78	170.2	52.0	38	227.6	69.6	98	285.0	87.1
59	56.4	17.2	19	113.8	34.8	79	171.2	52.3	39	228.6	69.9	99	285.9	87.4
60	57.4	17.5	20	114.8	35.1	80	172.1	52.6	40	229.5	70.2	300	286.9	87.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

73° (107°, 253°, 287°).

TABLE 2.

Difference of Latitude and Departure for 17° (163°, 197°, 343°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	287.8	88.0	361	345.2	105.5	421	402.6	123.1	481	460.0	140.6	541	517.3	158.2
02	288.8	88.3	62	346.1	105.8	22	403.5	123.4	82	460.9	140.9	42	518.3	158.5
03	289.7	88.6	63	347.1	106.1	23	404.5	123.7	83	461.9	141.2	43	519.2	158.8
04	290.7	88.9	64	348.1	106.4	24	405.4	124.0	84	462.8	141.5	44	520.2	159.1
05	291.6	89.2	65	349.0	106.7	25	406.4	124.3	85	463.8	141.8	45	521.2	159.3
06	292.6	89.5	66	350.0	107.0	26	407.3	124.6	86	464.7	142.1	46	522.1	159.6
07	293.5	89.8	67	350.9	107.3	27	408.3	124.8	87	465.7	142.3	47	523.1	159.9
08	294.5	90.1	68	351.9	107.6	28	409.3	125.1	88	466.7	142.6	48	524.0	160.2
09	295.5	90.3	69	352.8	107.9	29	410.2	125.4	89	467.6	142.9	49	525.0	160.5
10	296.4	90.6	70	353.8	108.2	30	411.2	125.7	90	468.6	143.2	50	526.0	160.8
311	297.4	90.9	371	354.8	108.5	431	412.1	126.0	491	469.5	143.5	551	526.9	161.1
12	298.3	91.2	72	355.7	108.8	32	413.1	126.3	92	470.5	143.8	52	527.9	161.4
13	299.3	91.5	73	356.7	109.1	33	414.0	126.6	93	471.4	144.1	53	528.8	161.7
14	300.2	91.8	74	357.6	109.4	34	415.0	126.9	94	472.4	144.4	54	529.8	162.0
15	301.2	92.1	75	358.6	109.6	35	416.0	127.2	95	473.4	144.7	55	530.8	162.3
16	302.2	92.4	76	359.5	109.9	36	416.9	127.5	96	474.3	145.0	56	531.7	162.6
17	303.1	92.7	77	360.5	110.2	37	417.9	127.8	97	475.3	145.3	57	532.7	162.9
18	304.1	93.0	78	361.4	110.5	38	418.8	128.1	98	476.2	145.6	58	533.6	163.2
19	305.0	93.3	79	362.4	110.8	39	419.8	128.4	99	477.2	145.9	59	534.6	163.5
20	306.0	93.6	80	363.4	111.1	40	420.7	128.6	500	478.1	146.2	60	535.5	163.8
321	306.9	93.9	381	364.3	111.4	441	421.7	128.9	501	479.1	146.5	561	536.5	164.1
22	307.9	94.1	82	365.3	111.7	42	422.7	129.2	02	480.1	146.8	62	537.5	164.4
23	308.8	94.4	83	366.2	112.0	43	423.6	129.5	03	481.0	147.1	63	538.4	164.6
24	309.8	94.7	84	367.2	112.3	44	424.6	129.8	04	482.0	147.4	64	539.4	164.8
25	310.8	95.0	85	368.1	112.6	45	425.5	130.1	05	482.9	147.7	65	540.3	165.1
26	311.7	95.3	86	369.1	112.9	46	426.5	130.4	06	483.9	148.0	66	541.3	165.4
27	312.7	95.6	87	370.1	113.2	47	427.4	130.7	07	484.8	148.3	67	542.2	165.7
28	313.6	95.9	88	371.0	113.4	48	428.4	131.0	08	485.8	148.6	68	543.2	166.0
29	314.6	96.2	89	372.0	113.7	49	429.3	131.3	09	486.7	148.9	69	544.1	166.4
30	315.5	96.5	90	372.9	114.0	50	430.3	131.6	10	487.7	149.1	70	545.1	166.7
331	316.5	96.8	391	373.9	114.3	451	431.3	131.9	511	488.7	149.4	571	546.1	167.0
32	317.5	97.1	92	374.8	114.6	52	432.2	132.2	12	489.6	149.7	72	547.0	167.2
33	318.4	97.4	93	375.8	114.9	53	433.2	132.4	13	490.6	150.0	73	548.0	167.5
34	319.4	97.7	94	376.7	115.2	54	434.1	132.7	14	491.5	150.2	74	548.9	167.8
35	320.3	97.9	95	377.7	115.5	55	435.1	133.0	15	492.5	150.5	75	549.9	168.1
36	321.3	98.2	96	378.7	115.8	56	436.0	133.3	16	493.4	150.8	76	550.8	168.4
37	322.2	98.5	97	379.6	116.1	57	437.0	133.6	17	494.4	151.1	77	551.8	168.7
38	323.2	98.8	98	380.6	116.4	58	438.0	133.9	18	495.3	151.4	78	552.7	169.0
39	324.2	99.1	99	381.5	116.7	59	438.9	134.2	19	496.3	151.7	79	553.7	169.3
40	325.1	99.4	400	382.5	117.0	60	439.9	134.5	20	497.2	152.0	80	554.6	169.6
341	326.1	99.7	401	383.4	117.2	461	440.8	134.8	521	498.2	152.3	581	555.6	169.9
42	327.0	100.0	02	384.4	117.5	62	441.8	135.1	22	499.2	152.6	82	556.5	170.2
43	328.0	100.3	03	385.4	117.8	63	442.7	135.4	23	500.1	152.9	83	557.5	170.5
44	328.9	100.6	04	386.3	118.1	64	443.7	135.7	24	501.1	153.2	84	558.4	170.8
45	329.9	100.9	05	387.3	118.4	65	444.6	136.0	25	502.0	153.5	85	559.4	171.1
46	330.8	101.2	06	388.2	118.7	66	445.6	136.2	26	503.0	153.8	86	560.4	171.3
47	331.8	101.5	07	389.2	119.0	67	446.6	136.5	27	503.9	154.1	87	561.3	171.6
48	332.8	101.8	08	390.1	119.3	68	447.5	136.8	28	504.9	154.4	88	562.3	171.9
49	333.7	102.0	09	391.1	119.6	69	448.5	137.1	29	505.9	154.7	89	563.2	172.2
50	334.7	102.3	10	392.0	119.9	70	449.4	137.4	30	506.8	155.0	90	564.2	172.5
351	335.6	102.6	411	393.0	120.2	471	450.4	137.7	531	507.8	155.3	591	565.1	172.8
52	336.6	102.9	12	394.0	120.5	72	451.3	138.0	32	508.7	155.6	92	566.1	173.1
53	337.5	103.2	13	394.9	120.8	73	452.3	138.3	33	509.7	155.9	93	567.1	173.4
54	338.5	103.5	14	395.9	121.0	74	453.3	138.6	34	510.6	156.2	94	568.0	173.7
55	339.5	103.8	15	396.8	121.3	75	454.2	138.9	35	511.6	156.5	95	569.0	174.0
56	340.4	104.1	16	397.8	121.6	76	455.2	139.2	36	512.6	156.8	96	569.9	174.3
57	341.4	104.4	17	398.7	121.9	77	456.1	139.5	37	513.5	157.1	97	570.9	174.6
58	342.3	104.7	18	399.7	122.2	78	457.1	139.8	38	514.5	157.3	98	571.8	174.9
59	343.3	105.0	19	400.7	122.5	79	458.0	140.0	39	515.4	157.6	99	572.8	175.2
60	344.2	105.3	20	401.6	122.8	80	459.0	140.3	40	516.4	157.9	600	573.8	175.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

73° (107°, 253°, 287°).

6583—06——26

TABLE 2.

Difference of Latitude and Departure for 18° (162°, 198°, 342°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.3	61	58.0	18.9	121	115.1	37.4	181	172.1	55.9	241	229.2	74.5
2	1.9	0.6	62	59.0	19.2	22	116.0	37.7	82	173.1	56.2	42	230.2	74.8
3	2.9	0.9	63	59.9	19.5	23	117.0	38.0	83	174.0	56.6	43	231.1	75.1
4	3.8	1.2	64	60.9	19.8	24	117.9	38.3	84	175.0	56.9	44	232.1	75.4
5	4.8	1.5	65	61.8	20.1	25	118.9	38.6	85	175.9	57.2	45	233.0	75.7
6	5.7	1.9	66	62.8	20.4	26	119.8	38.9	86	176.9	57.5	46	234.0	76.0
7	6.7	2.2	67	63.7	20.7	27	120.8	39.2	87	177.8	57.8	47	234.9	76.3
8	7.6	2.5	68	64.7	21.0	28	121.7	39.6	88	178.8	58.1	48	235.9	76.6
9	8.6	2.8	69	65.6	21.3	29	122.7	39.9	89	179.7	58.4	49	236.8	76.9
10	9.5	3.1	70	66.6	21.6	30	123.6	40.2	90	180.7	58.7	50	237.8	77.3
11	10.5	3.4	71	67.5	21.9	131	124.6	40.5	191	181.7	59.0	251	238.7	77.6
12	11.4	3.7	72	68.5	22.2	32	125.5	40.8	92	182.6	59.3	52	239.7	77.9
13	12.4	4.0	73	69.4	22.6	33	126.5	41.1	93	183.6	59.6	53	240.6	78.2
14	13.3	4.3	74	70.4	22.9	34	127.4	41.4	94	184.5	59.9	54	241.6	78.5
15	14.3	4.6	75	71.3	23.2	35	128.4	41.7	95	185.5	60.3	55	242.5	78.8
16	15.2	4.9	76	72.3	23.5	36	129.3	42.0	96	186.4	60.6	56	243.5	79.1
17	16.2	5.3	77	73.2	23.8	37	130.3	42.3	97	187.4	60.9	57	244.4	79.4
18	17.1	5.6	78	74.2	24.1	38	131.2	42.6	98	188.3	61.2	58	245.4	79.7
19	18.1	5.9	79	75.1	24.4	39	132.2	43.0	99	189.3	61.5	59	246.3	80.0
20	19.0	6.2	80	76.1	24.7	40	133.1	43.3	200	190.2	61.8	60	247.3	80.3
21	20.0	6.5	81	77.0	25.0	141	134.1	43.6	201	191.2	62.1	261	248.2	80.7
22	20.9	6.8	82	78.0	25.3	42	135.1	43.9	02	192.1	62.4	62	249.2	81.0
23	21.9	7.1	83	78.9	25.6	43	136.0	44.2	03	193.1	62.7	63	250.1	81.3
24	22.8	7.4	84	79.9	26.0	44	137.0	44.5	04	194.0	63.0	64	251.1	81.6
25	23.8	7.7	85	80.8	26.3	45	137.9	44.8	05	195.0	63.3	65	252.0	81.9
26	24.7	8.0	86	81.8	26.6	46	138.9	45.1	06	195.9	63.7	66	253.0	82.2
27	25.7	8.3	87	82.7	26.9	47	139.8	45.4	07	196.9	64.0	67	253.9	82.5
28	26.6	8.7	88	83.7	27.2	48	140.8	45.7	08	197.8	64.3	68	254.9	82.8
29	27.6	9.0	89	84.6	27.5	49	141.7	46.0	09	198.8	64.6	69	255.8	83.1
30	28.5	9.3	90	85.6	27.8	50	142.7	46.4	10	199.7	64.9	70	256.8	83.4
31	29.5	9.6	91	86.5	28.1	151	143.6	46.7	211	200.7	65.2	271	257.7	83.7
32	30.4	9.9	92	87.5	28.4	52	144.6	47.0	12	201.6	65.5	72	258.7	84.1
33	31.4	10.2	93	88.4	28.7	53	145.5	47.3	13	202.6	65.8	73	259.6	84.4
34	32.3	10.5	94	89.4	29.0	54	146.5	47.6	14	203.5	66.1	74	260.6	84.7
35	33.3	10.8	95	90.4	29.4	55	147.4	47.9	15	204.5	66.4	75	261.5	85.0
36	34.2	11.1	96	91.3	29.7	56	148.4	48.2	16	205.4	66.7	76	262.5	85.3
37	35.2	11.4	97	92.3	30.0	57	149.3	48.5	17	206.4	67.1	77	263.4	85.6
38	36.1	11.7	98	93.2	30.3	58	150.3	48.8	18	207.3	67.4	78	264.4	85.9
39	37.1	12.1	99	94.2	30.6	59	151.2	49.1	19	208.3	67.7	79	265.3	86.2
40	38.0	12.4	100	95.1	30.9	60	152.2	49.4	20	209.2	68.0	80	266.3	86.5
41	39.0	12.7	101	96.1	31.2	161	153.1	49.8	221	210.2	68.3	281	267.2	86.8
42	39.9	13.0	02	97.0	31.5	62	154.1	50.1	22	211.1	68.6	82	268.2	87.1
43	40.9	13.3	03	98.0	31.8	63	155.0	50.4	23	212.1	68.9	83	269.1	87.5
44	41.8	13.6	04	98.9	32.1	64	156.0	50.7	24	213.0	69.2	84	270.1	87.8
45	42.8	13.9	05	99.9	32.4	65	156.9	51.0	25	214.0	69.5	85	271.1	88.1
46	43.7	14.2	06	100.8	32.8	66	157.9	51.3	26	214.9	69.8	86	272.0	88.4
47	44.7	14.5	07	101.8	33.1	67	158.8	51.6	27	215.9	70.1	87	273.0	88.7
48	45.7	14.8	08	102.7	33.4	68	159.8	51.9	28	216.8	70.5	88	273.9	89.0
49	46.6	15.1	09	103.7	33.7	69	160.7	52.2	29	217.8	70.8	89	274.9	89.3
50	47.6	15.5	10	104.6	34.0	70	161.7	52.5	30	218.7	71.1	90	275.8	89.6
51	48.5	15.8	111	105.6	34.3	171	162.6	52.8	231	219.7	71.4	291	276.8	89.9
52	49.5	16.1	12	106.5	34.6	72	163.6	53.2	32	220.6	71.7	92	277.7	90.2
53	50.4	16.4	13	107.5	34.9	73	164.5	53.5	33	221.6	72.0	93	278.7	90.5
54	51.4	16.7	14	108.4	35.2	74	165.5	53.8	34	222.5	72.3	94	279.6	90.9
55	52.3	17.0	15	109.4	35.5	75	166.4	54.1	35	223.5	72.6	95	280.6	91.2
56	53.3	17.3	16	110.3	35.8	76	167.4	54.4	36	224.4	72.9	96	281.5	91.5
57	54.2	17.6	17	111.3	36.2	77	168.3	54.7	37	225.4	73.2	97	282.5	91.8
58	55.2	17.9	18	112.2	36.5	78	169.3	55.0	38	226.4	73.5	98	283.4	92.1
59	56.1	18.2	19	113.2	36.8	79	170.2	55.3	39	227.3	73.9	99	284.4	92.4
60	57.1	18.5	20	114.1	37.1	80	171.2	55.6	40	228.3	74.2	300	285.3	92.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

72° (108°, 252°, 288°).

TABLE 2.

Difference of Latitude and Departure for 18° (162°, 198°, 342°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	286.3	93.0	361	343.3	111.6	421	400.4	130.1	481	457.5	148.6	541	514.5	167.2
02	287.2	93.3	62	344.3	111.9	22	401.4	130.4	82	458.5	148.9	42	515.5	167.5
03	288.2	93.7	63	345.2	112.2	23	402.3	130.7	83	459.4	149.3	43	516.4	167.9
04	289.1	94.0	64	346.2	112.5	24	403.3	131.0	84	460.4	149.6	44	517.4	168.2
05	290.1	94.3	65	347.1	112.8	25	404.2	131.3	85	461.3	149.9	45	518.3	168.5
06	291.0	94.6	66	348.1	113.1	26	405.2	131.7	86	462.3	150.2	46	519.3	168.8
07	292.0	94.9	67	349.0	113.4	27	406.1	132.0	87	463.2	150.5	47	520.2	169.1
08	292.9	95.2	68	350.0	113.7	28	407.1	132.3	88	464.2	150.8	48	521.2	169.4
09	293.9	95.5	69	350.9	114.0	29	408.0	132.6	89	465.1	151.1	49	522.1	169.7
10	294.8	95.8	70	351.9	114.3	30	409.0	132.9	90	466.1	151.4	50	523.1	170.0
311	295.8	96.1	371	352.9	114.7	431	409.9	133.2	491	467.0	151.7	551	524.0	170.3
12	296.7	96.4	72	353.8	115.0	32	410.9	133.5	92	468.0	152.0	52	525.0	170.6
13	297.7	96.7	73	354.8	115.3	33	411.8	133.8	93	468.9	152.3	53	525.9	170.9
14	298.6	97.0	74	355.7	115.6	34	412.8	134.1	94	469.8	152.6	54	526.9	171.2
15	299.6	97.4	75	356.7	115.9	35	413.7	134.4	95	470.8	153.0	55	527.8	171.5
16	300.5	97.7	76	357.6	116.2	36	414.7	134.7	96	471.7	153.3	56	528.8	171.8
17	301.5	98.0	77	358.6	116.5	37	415.6	135.1	97	472.7	153.6	57	529.7	172.1
18	302.4	98.3	78	359.5	116.8	38	416.6	135.4	98	473.6	153.9	58	530.7	172.4
19	303.4	98.6	79	360.5	117.1	39	417.5	135.7	99	474.6	154.2	59	531.6	172.7
20	304.3	98.9	80	361.4	117.4	40	418.5	136.0	500	475.5	154.5	60	532.6	173.0
321	305.3	99.2	381	362.4	117.7	441	419.4	136.3	501	476.5	154.8	561	533.5	173.3
22	306.2	99.5	82	363.3	118.1	42	420.4	136.6	02	477.4	155.1	62	534.5	173.6
23	307.2	99.8	83	364.3	118.4	43	421.3	136.9	03	478.4	155.4	63	535.4	173.9
24	308.2	100.1	84	365.2	118.7	44	422.3	137.2	04	479.3	155.7	64	536.4	174.2
25	309.1	100.4	85	366.2	119.0	45	423.2	137.5	05	480.3	156.1	65	537.3	174.6
26	310.1	100.7	86	367.1	119.3	46	424.2	137.8	06	481.2	156.4	66	538.3	174.9
27	311.0	101.1	87	368.1	119.6	47	425.1	138.1	07	482.2	156.7	67	539.2	175.2
28	312.0	101.4	88	369.0	119.9	48	426.1	138.4	08	483.2	157.0	68	540.2	175.5
29	312.9	101.7	89	370.0	120.2	49	427.0	138.8	09	484.1	157.3	69	541.1	175.8
30	313.9	102.0	90	370.9	120.5	50	428.0	139.1	10	485.1	157.6	70	542.1	176.1
331	314.8	102.3	391	371.9	120.8	451	428.9	139.4	511	486.0	157.9	571	543.0	176.4
32	315.8	102.6	92	372.8	121.1	52	429.9	139.7	12	487.0	158.2	72	544.0	176.7
33	316.7	102.9	93	373.8	121.5	53	430.8	140.0	13	487.9	158.5	73	544.9	177.0
34	317.7	103.2	94	374.7	121.8	54	431.8	140.3	14	488.9	158.8	74	545.9	177.3
35	318.6	103.5	95	375.7	122.1	55	432.7	140.6	15	489.8	159.1	75	546.8	177.6
36	319.6	103.8	96	376.6	122.4	56	433.7	140.9	16	490.8	159.4	76	547.8	178.0
37	320.5	104.1	97	377.6	122.7	57	434.6	141.2	17	491.7	159.7	77	548.7	178.3
38	321.5	104.5	98	378.5	123.0	58	435.6	141.5	18	492.7	160.0	78	549.7	178.6
39	322.4	104.8	99	379.5	123.3	59	436.5	141.8	19	493.6	160.3	79	550.6	178.9
40	323.4	105.1	400	380.4	123.6	60	437.5	142.2	20	494.6	160.7	80	551.6	179.2
341	324.3	105.4	401	381.4	123.9	461	438.4	142.5	521	495.5	161.0	581	552.5	179.5
42	325.3	105.7	02	382.3	124.2	62	439.4	142.8	22	496.5	161.3	82	553.5	179.8
43	326.2	106.0	03	383.3	124.5	63	440.3	143.1	23	497.4	161.6	83	554.4	180.1
44	327.2	106.3	04	384.2	124.9	64	441.3	143.4	24	498.4	161.9	84	555.4	180.4
45	328.1	106.6	05	385.2	125.2	65	442.2	143.7	25	499.3	162.2	85	556.3	180.7
46	329.1	106.9	06	386.1	125.5	66	443.2	144.0	26	500.3	162.5	86	557.3	181.1
47	330.0	107.2	07	387.1	125.8	67	444.2	144.3	27	501.2	162.9	87	558.2	181.4
48	331.0	107.5	08	388.0	126.1	68	445.1	144.6	28	502.2	163.2	88	559.2	181.7
49	331.9	107.9	09	389.0	126.4	69	446.1	144.9	29	503.1	163.5	89	560.1	182.0
50	332.9	108.2	10	389.9	126.7	70	447.0	145.2	30	504.1	163.8	90	561.1	182.3
351	333.8	108.5	411	390.9	127.0	471	448.0	145.6	531	505.0	164.1	591	562.0	182.7
52	334.8	108.8	12	391.8	127.3	72	448.9	145.9	32	506.0	164.4	92	563.0	183.0
53	335.7	109.1	13	392.8	127.6	73	449.9	146.2	33	506.9	164.7	93	563.9	183.3
54	336.7	109.4	14	393.7	127.9	74	450.8	146.5	34	507.9	165.0	94	564.9	183.6
55	337.6	109.7	15	394.7	128.3	75	451.8	146.8	35	508.8	165.3	95	565.8	183.9
56	338.6	110.0	16	395.6	128.6	76	452.7	147.1	36	509.8	165.6	96	566.8	184.2
57	339.5	110.3	17	396.6	128.9	77	453.7	147.4	37	510.7	165.9	97	567.7	184.5
58	340.5	110.6	18	397.5	129.2	78	454.6	147.7	38	511.7	166.2	98	568.7	184.8
59	341.4	110.9	19	398.5	129.5	79	455.6	148.0	39	512.6	166.5	99	569.6	185.1
60	342.4	111.3	20	399.5	129.8	80	456.5	148.3	40	513.6	166.9	600	570.6	185.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

72° (108, 252°, 288°).

TABLE 2.

Difference of Latitude and Departure for 19° (161°, 199°, 341°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.3	61	57.7	19.9	121	114.4	39.4	181	171.1	58.9	241	227.9	78.5
2	1.9	0.7	62	58.6	20.2	22	115.4	39.7	82	172.1	59.3	42	228.8	78.8
3	2.8	1.0	63	59.6	20.5	23	116.3	40.0	83	173.0	59.6	43	229.8	79.1
4	3.8	1.3	64	60.5	20.8	24	117.2	40.4	84	174.0	59.9	44	230.7	79.4
5	4.7	1.6	65	61.5	21.2	25	118.2	40.7	85	174.9	60.2	45	231.7	79.8
6	5.7	2.0	66	62.4	21.5	26	119.1	41.0	86	175.9	60.6	46	232.6	80.1
7	6.6	2.3	67	63.3	21.8	27	120.1	41.3	87	176.8	60.9	47	233.5	80.4
8	7.6	2.6	68	64.3	22.1	28	121.0	41.7	88	177.8	61.2	48	234.5	80.7
9	8.5	2.9	69	65.2	22.5	29	122.0	42.0	89	178.7	61.5	49	235.4	81.1
10	9.5	3.3	70	66.2	22.8	30	122.9	42.3	90	179.6	61.9	50	236.4	81.4
11	10.4	3.6	71	67.1	23.1	131	123.9	42.6	191	180.6	62.2	251	237.3	81.7
12	11.3	3.9	72	68.1	23.4	32	124.8	43.0	92	181.5	62.5	52	238.3	82.0
13	12.3	4.2	73	69.0	23.8	33	125.8	43.3	93	182.5	62.8	53	239.2	82.4
14	13.2	4.6	74	70.0	24.1	34	126.7	43.6	94	183.4	63.2	54	240.2	82.7
15	14.2	4.9	75	70.9	24.4	35	127.6	44.0	95	184.4	63.5	55	241.1	83.0
16	15.1	5.2	76	71.9	24.7	36	128.6	44.3	96	185.3	63.8	56	242.1	83.3
17	16.1	5.5	77	72.8	25.1	37	129.5	44.6	97	186.3	64.1	57	243.0	83.7
18	17.0	5.9	78	73.8	25.4	38	130.5	44.9	98	187.2	64.5	58	243.9	84.0
19	18.0	6.2	79	74.7	25.7	39	131.4	45.3	99	188.2	64.8	59	244.9	84.3
20	18.9	6.5	80	75.6	26.0	40	132.4	45.6	200	189.1	65.1	60	245.8	84.6
21	19.9	6.8	81	76.6	26.4	141	133.3	45.9	201	190.0	65.4	261	246.8	85.0
22	20.8	7.2	82	77.5	26.7	42	134.3	46.2	02	191.0	65.8	62	247.7	85.3
23	21.7	7.5	83	78.5	27.0	43	135.2	46.6	03	191.9	66.1	63	248.7	85.6
24	22.7	7.8	84	79.4	27.3	44	136.2	46.9	04	192.9	66.4	64	249.6	86.0
25	23.6	8.1	85	80.4	27.7	45	137.1	47.2	05	193.8	66.7	65	250.6	86.3
26	24.6	8.5	86	81.3	28.0	46	138.0	47.5	06	194.8	67.1	66	251.5	86.6
27	25.5	8.8	87	82.3	28.3	47	139.0	47.9	07	195.7	67.4	67	252.5	86.9
28	26.5	9.1	88	83.2	28.7	48	139.9	48.2	08	196.7	67.7	68	253.4	87.3
29	27.4	9.4	89	84.2	29.0	49	140.9	48.5	09	197.6	68.0	69	254.3	87.6
30	28.4	9.8	90	85.1	29.3	50	141.8	48.8	10	198.6	68.4	70	255.3	87.9
31	29.3	10.1	91	86.0	29.6	151	142.8	49.2	211	199.5	68.7	271	256.2	88.2
32	30.3	10.4	92	87.0	30.0	52	143.7	49.5	12	200.4	69.0	72	257.2	88.6
33	31.2	10.7	93	87.9	30.3	53	144.7	49.8	13	201.4	69.3	73	258.1	88.9
34	32.1	11.1	94	88.9	30.6	54	145.6	50.1	14	202.3	69.7	74	259.1	89.2
35	33.1	11.4	95	89.8	30.9	55	146.6	50.5	15	203.3	70.0	75	260.0	89.5
36	34.0	11.7	96	90.8	31.3	56	147.5	50.8	16	204.2	70.3	76	261.0	89.9
37	35.0	12.0	97	91.7	31.6	57	148.4	51.1	17	205.2	70.6	77	261.9	90.2
38	35.9	12.4	98	92.7	31.9	58	149.4	51.4	18	206.1	71.0	78	262.9	90.5
39	36.9	12.7	99	93.6	32.2	59	150.3	51.8	19	207.1	71.3	79	263.8	90.8
40	37.8	13.0	100	94.6	32.6	60	151.3	52.1	20	208.0	71.6	80	264.7	91.2
41	38.8	13.3	101	95.5	32.9	161	152.2	52.4	221	209.0	72.0	281	265.7	91.5
42	39.7	13.7	02	96.4	33.2	62	153.2	52.7	22	209.9	72.3	82	266.6	91.8
43	40.7	14.0	03	97.4	33.5	63	154.1	53.1	23	210.9	72.6	83	267.6	92.1
44	41.6	14.3	04	98.3	33.9	64	155.1	53.4	24	211.8	72.9	84	268.5	92.5
45	42.5	14.7	05	99.3	34.2	65	156.0	53.7	25	212.7	73.3	85	269.5	92.8
46	43.5	15.0	06	100.2	34.5	66	157.0	54.0	26	213.7	73.6	86	270.4	93.1
47	44.4	15.3	07	101.2	34.8	67	157.9	54.4	27	214.6	73.9	87	271.4	93.4
48	45.4	15.6	08	102.1	35.2	68	158.8	54.7	28	215.6	74.2	88	272.3	93.8
49	46.3	16.0	09	103.1	35.5	69	159.8	55.0	29	216.5	74.6	89	273.3	94.1
50	47.3	16.3	10	104.0	35.8	70	160.7	55.3	30	217.5	74.9	90	274.2	94.4
51	48.2	16.6	111	105.0	36.1	171	161.7	55.7	231	218.4	75.2	291	275.1	94.7
52	49.2	16.9	12	105.9	36.5	72	162.6	56.0	32	219.4	75.5	92	276.1	95.1
53	50.1	17.3	13	106.8	36.8	73	163.6	56.3	33	220.3	75.9	93	277.0	95.4
54	51.1	17.6	14	107.8	37.1	74	164.5	56.6	34	221.3	76.2	94	278.0	95.7
55	52.0	17.9	15	108.7	37.4	75	165.5	57.0	35	222.2	76.5	95	278.9	96.0
56	52.9	18.2	16	109.7	37.8	76	166.4	57.3	36	223.1	76.8	96	279.9	96.4
57	53.9	18.6	17	110.6	38.1	77	167.4	57.6	37	224.1	77.2	97	280.8	96.7
58	54.8	18.9	18	111.6	38.4	78	168.3	58.0	38	225.0	77.5	98	281.8	97.0
59	55.8	19.2	19	112.5	38.7	79	169.2	58.3	39	226.0	77.8	99	282.7	97.3
60	56.7	19.5	20	113.5	39.1	80	170.2	58.6	40	226.9	78.1	300	283.7	97.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

71° (109°, 251°, 289°).

TABLE 2.

Difference of Latitude and Departure for 19° (161°, 199°, 341°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	284.6	98.0	361	341.3	117.5	421	398.1	137.0	481	454.8	156.6	541	511.5	176.1
02	285.5	98.3	62	342.3	117.8	22	399.0	137.4	82	455.7	156.9	42	512.4	176.4
03	286.5	98.6	63	343.2	118.2	23	400.0	137.7	83	456.7	157.2	43	513.4	176.8
04	287.4	99.0	64	344.2	118.5	24	400.9	138.0	84	457.6	157.6	44	514.3	177.1
05	288.4	99.3	65	345.1	118.8	25	401.8	138.4	85	458.6	157.9	45	515.3	177.4
06	289.3	99.6	66	346.1	119.1	26	402.8	138.7	86	459.5	158.2	46	516.2	177.7
07	290.3	99.9	67	347.0	119.5	27	403.7	139.0	87	460.5	158.5	47	517.2	178.1
08	291.2	100.3	68	348.0	119.8	28	404.7	139.3	88	461.4	158.9	48	518.1	178.4
09	292.2	100.6	69	348.9	120.1	29	405.6	139.7	89	462.4	159.2	49	519.1	178.7
10	293.1	100.9	70	349.8	120.4	30	406.6	140.0	90	463.3	159.5	50	520.0	179.0
311	294.1	101.2	371	350.8	120.8	431	407.5	140.3	491	464.3	159.8	551	521.0	179.4
12	295.0	101.6	72	351.7	121.1	32	408.5	140.6	92	465.2	160.2	52	521.9	179.7
13	295.9	101.9	73	352.7	121.4	33	409.4	141.0	93	466.1	160.5	53	522.8	180.0
14	296.9	102.2	74	353.6	121.7	34	410.4	141.3	94	467.1	160.8	54	523.8	180.3
15	297.8	102.5	75	354.6	122.1	35	411.3	141.6	95	468.0	161.1	55	524.7	180.7
16	298.8	102.9	76	355.5	122.4	36	412.2	141.9	96	469.0	161.5	56	525.7	181.0
17	299.7	103.2	77	356.5	122.7	37	413.2	142.3	97	469.9	161.8	57	526.6	181.3
18	300.7	103.5	78	357.4	123.0	38	414.1	142.6	98	470.9	162.1	58	527.6	181.6
19	301.6	103.8	79	358.4	123.4	39	415.1	142.9	99	471.8	162.4	59	528.5	182.0
20	302.6	104.2	80	359.3	123.7	40	416.0	143.2	500	472.8	162.8	60	529.5	182.3
321	303.5	104.5	381	360.2	124.0	441	417.0	143.6	501	473.7	163.1	561	530.4	182.6
22	304.5	104.8	82	361.2	124.4	42	417.9	143.9	02	474.7	163.4	62	531.4	182.9
23	305.4	105.1	83	362.1	124.7	43	418.9	144.2	03	475.6	163.7	63	532.3	183.3
24	306.3	105.5	84	363.1	125.0	44	419.8	144.5	04	476.5	164.1	64	533.2	183.6
25	307.3	105.8	85	364.0	125.3	45	420.8	144.9	05	477.5	164.4	65	534.2	183.9
26	308.2	106.1	86	365.0	125.7	46	421.7	145.2	06	478.4	164.7	66	535.1	184.2
27	309.2	106.4	87	365.9	126.0	47	422.6	145.5	07	479.4	165.0	67	536.1	184.6
28	310.1	106.8	88	366.9	126.3	48	423.6	145.8	08	480.3	165.4	68	537.0	184.9
29	311.1	107.1	89	367.8	126.6	49	424.5	146.2	09	481.2	165.7	69	538.0	185.2
30	312.0	107.4	90	368.8	127.0	50	425.5	146.5	10	482.2	166.1	70	538.9	185.6
331	313.0	107.7	391	369.7	127.3	451	426.4	146.8	511	483.1	166.4	571	539.9	185.9
32	313.9	108.1	92	370.6	127.6	52	427.4	147.1	12	484.1	166.7	72	540.8	186.2
33	314.9	108.4	93	371.6	127.9	53	428.3	147.5	13	485.0	167.0	73	541.7	186.5
34	315.8	108.7	94	372.5	128.3	54	429.3	147.8	14	486.0	167.4	74	542.7	186.9
35	316.7	109.1	95	373.5	128.6	55	430.2	148.1	15	486.9	167.7	75	543.6	187.2
36	317.7	109.4	96	374.4	128.9	56	431.2	148.4	16	487.9	168.0	76	544.6	187.5
37	318.6	109.7	97	375.4	129.2	57	432.1	148.8	17	488.8	168.3	77	545.5	187.8
38	319.6	110.0	98	376.3	129.6	58	433.0	149.1	18	489.7	168.7	78	546.5	188.2
39	320.5	110.4	99	377.3	129.9	59	434.0	149.4	19	490.7	169.0	79	547.4	188.5
40	321.5	110.7	400	378.2	130.2	60	434.9	149.7	20	491.6	169.3	80	548.4	188.8
341	322.4	111.0	401	379.2	130.5	461	435.9	150.1	521	492.6	169.6	581	549.3	189.1
42	323.4	111.3	02	380.1	130.9	62	436.8	150.4	22	493.5	170.0	82	550.3	189.5
43	324.3	111.7	03	381.0	131.2	63	437.8	150.7	23	494.5	170.3	83	551.2	189.8
44	325.3	112.0	04	382.0	131.5	64	438.7	151.0	24	495.4	170.6	84	552.2	190.1
45	326.2	112.3	05	382.9	131.8	65	439.7	151.4	25	496.4	170.9	85	553.1	190.4
46	327.1	112.6	06	383.9	132.2	66	440.6	151.7	26	497.3	171.2	86	554.1	190.8
47	328.1	113.0	07	384.8	132.5	67	441.6	152.0	27	498.3	171.6	87	555.0	191.1
48	329.0	113.3	08	385.8	132.8	68	442.5	152.4	28	499.2	171.9	88	555.9	191.4
49	330.0	113.6	09	386.7	133.1	69	443.4	152.7	29	500.1	172.2	89	556.9	191.7
50	330.9	113.9	10	387.7	133.5	70	444.4	153.0	30	501.1	172.5	90	557.8	192.1
351	331.9	114.3	411	388.6	133.8	471	445.3	153.3	531	502.0	172.9	591	558.8	192.4
52	332.8	114.6	12	389.6	134.1	72	446.3	153.7	32	503.0	173.2	92	559.7	192.7
53	333.8	114.9	13	390.5	134.4	73	447.2	154.0	33	503.9	173.5	93	560.7	193.0
54	334.7	115.2	14	391.4	134.8	74	448.2	154.3	34	504.9	173.8	94	561.6	193.4
55	335.7	115.6	15	392.4	135.1	75	449.1	154.6	35	505.8	174.2	95	562.6	193.7
56	336.6	115.9	16	393.3	135.4	76	450.1	155.0	36	506.8	174.5	96	563.5	194.0
57	337.5	116.2	17	394.3	135.7	77	451.0	155.3	37	507.7	174.8	97	564.5	194.3
58	338.5	116.5	18	395.2	136.1	78	452.0	155.6	38	508.7	175.1	98	565.4	194.7
59	339.4	116.9	19	396.2	136.4	79	452.9	155.9	39	509.6	175.5	99	566.4	195.0
60	340.4	117.2	20	397.1	136.7	80	453.8	156.3	40	510.6	175.8	600	567.3	195.3
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

71° (109°, 251°, 289°).

TABLE 2.

Difference of Latitude and Departure for 20° (160°, 200°, 340°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.3	61	57.3	20.9	121	113.7	41.4	181	170.1	61.9	241	226.5	82.4
2	1.9	0.7	62	58.3	21.2	22	114.6	41.7	82	171.0	62.2	42	227.4	82.8
3	2.8	1.0	63	59.2	21.5	23	115.6	42.1	83	172.0	62.6	43	228.3	83.1
4	3.8	1.4	64	60.1	21.9	24	116.5	42.4	84	172.9	62.9	44	229.3	83.5
5	4.7	1.7	65	61.1	22.2	25	117.5	42.8	85	173.8	63.3	45	230.2	83.8
6	5.6	2.1	66	62.0	22.6	26	118.4	43.1	86	174.8	63.6	46	231.2	84.1
7	6.6	2.4	67	63.0	22.9	27	119.3	43.4	87	175.7	64.0	47	232.1	84.5
8	7.5	2.7	68	63.9	23.3	28	120.3	43.8	88	176.7	64.3	48	233.0	84.8
9	8.5	3.1	69	64.8	23.6	29	121.2	44.1	89	177.6	64.6	49	234.0	85.2
10	9.4	3.4	70	65.8	23.9	30	122.2	44.5	90	178.5	65.0	50	234.9	85.5
11	10.3	3.8	71	66.7	24.3	131	123.1	44.8	191	179.5	65.3	251	235.9	85.8
12	11.3	4.1	72	67.7	24.6	32	124.0	45.1	92	180.4	65.7	52	236.8	86.2
13	12.2	4.4	73	68.6	25.0	33	125.0	45.5	93	181.4	66.0	53	237.7	86.5
14	13.2	4.8	74	69.5	25.3	34	125.9	45.8	94	182.3	66.4	54	238.7	86.9
15	14.1	5.1	75	70.5	25.7	35	126.9	46.2	95	183.2	66.7	55	239.6	87.2
16	15.0	5.5	76	71.4	26.0	36	127.8	46.5	96	184.2	67.0	56	240.6	87.6
17	16.0	5.8	77	72.4	26.3	37	128.7	46.9	97	185.1	67.4	57	241.5	87.9
18	16.9	6.2	78	73.3	26.7	38	129.7	47.2	98	186.1	67.7	58	242.4	88.2
19	17.9	6.5	79	74.2	27.0	39	130.6	47.5	99	187.0	68.1	59	243.4	88.6
20	18.8	6.8	80	75.2	27.4	40	131.6	47.9	200	187.9	68.4	60	244.3	88.9
21	19.7	7.2	81	76.1	27.7	141	132.5	48.2	201	188.9	68.7	261	245.3	89.3
22	20.7	7.5	82	77.1	28.0	42	133.4	48.6	02	189.8	69.1	62	246.2	89.6
23	21.6	7.9	83	78.0	28.4	43	134.4	48.9	03	190.8	69.4	63	247.1	90.0
24	22.6	8.2	84	78.9	28.7	44	135.3	49.3	04	191.7	69.8	64	248.1	90.3
25	23.5	8.6	85	79.9	29.1	45	136.3	49.6	05	192.6	70.1	65	249.0	90.6
26	24.4	8.9	86	80.8	29.4	46	137.2	49.9	06	193.6	70.5	66	250.0	91.0
27	25.4	9.2	87	81.8	29.8	47	138.1	50.3	07	194.5	70.8	67	250.9	91.3
28	26.3	9.6	88	82.7	30.1	48	139.1	50.6	08	195.5	71.1	68	251.8	91.7
29	27.3	9.9	89	83.6	30.4	49	140.0	51.0	09	196.4	71.5	69	252.8	92.0
30	28.2	10.3	90	84.6	30.8	50	140.9	51.3	10	197.3	71.8	70	253.7	92.3
31	29.1	10.6	91	85.5	31.1	151	141.9	51.6	211	198.3	72.2	271	254.7	92.7
32	30.1	10.9	92	86.5	31.5	52	142.8	52.0	12	199.2	72.5	72	255.6	93.0
33	31.0	11.3	93	87.4	31.8	53	143.8	52.3	13	200.2	72.9	73	256.5	93.4
34	31.9	11.6	94	88.3	32.1	54	144.7	52.7	14	201.1	73.2	74	257.5	93.7
35	32.9	12.0	95	89.3	32.5	55	145.7	53.0	15	202.0	73.5	75	258.4	94.1
36	33.8	12.3	96	90.2	32.8	56	146.6	53.4	16	203.0	73.9	76	259.4	94.4
37	34.8	12.7	97	91.2	33.2	57	147.5	53.7	17	203.9	74.2	77	260.3	94.7
38	35.7	13.0	98	92.1	33.5	58	148.5	54.0	18	204.9	74.6	78	261.2	95.1
39	36.6	13.3	99	93.0	33.9	59	149.4	54.4	19	205.8	74.9	79	262.2	95.4
40	37.6	13.7	100	94.0	34.2	60	150.4	54.7	20	206.7	75.2	80	263.1	95.8
41	38.5	14.0	101	94.9	34.5	161	151.3	55.1	221	207.7	75.6	281	264.1	96.1
42	39.5	14.4	02	95.8	34.9	62	152.2	55.4	22	208.6	75.9	82	265.0	96.4
43	40.4	14.7	03	96.8	35.2	63	153.2	55.7	23	209.6	76.3	83	265.9	96.8
44	41.3	15.0	04	97.7	35.6	64	154.1	56.1	24	210.5	76.6	84	266.9	97.1
45	42.3	15.4	05	98.7	35.9	65	155.0	56.4	25	211.4	77.0	85	267.8	97.5
46	43.2	15.7	06	99.6	36.3	66	156.0	56.8	26	212.4	77.3	86	268.8	97.8
47	44.2	16.1	07	100.5	36.6	67	156.9	57.1	27	213.3	77.6	87	269.7	98.2
48	45.1	16.4	08	101.5	36.9	68	157.9	57.5	28	214.2	78.0	88	270.6	98.5
49	46.0	16.8	09	102.4	37.3	69	158.8	57.8	29	215.2	78.3	89	271.6	98.8
50	47.0	17.1	10	103.4	37.6	70	159.7	58.1	30	216.1	78.7	90	272.5	99.2
51	47.9	17.4	111	104.3	38.0	171	160.7	58.5	231	217.1	79.0	291	273.5	99.5
52	48.9	17.8	12	105.2	38.3	72	161.6	58.8	32	218.0	79.3	92	274.4	99.9
53	49.8	18.1	13	106.2	38.6	73	162.6	59.2	33	218.9	79.7	93	275.3	100.2
54	50.7	18.5	14	107.1	39.0	74	163.5	59.5	34	219.9	80.0	94	276.3	100.6
55	51.7	18.8	15	108.1	39.3	75	164.4	59.9	35	220.8	80.4	95	277.2	100.9
56	52.6	19.2	16	109.0	39.7	76	165.4	60.2	36	221.8	80.7	96	278.1	101.2
57	53.6	19.5	17	109.9	40.0	77	166.3	60.5	37	222.7	81.1	97	279.1	101.6
58	54.5	19.8	18	110.9	40.4	78	167.3	60.9	38	223.6	81.4	98	280.0	101.9
59	55.4	20.2	19	111.8	40.7	79	168.2	61.2	39	224.6	81.7	99	281.0	102.3
60	56.4	20.5	20	112.8	41.0	80	169.1	61.6	40	225.5	82.1	300	281.9	102.6
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

70° (110°, 250°, 290°).

TABLE 2.

Difference of Latitude and Departure for 20° (160°, 200°, 340°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	282.9	103.0	361	339.2	123.5	421	395.6	144.0	481	452.0	164.5	541	508.4	185.0
02	283.8	103.3	62	340.2	123.8	22	396.6	144.3	82	453.0	164.8	42	509.3	185.4
03	284.7	103.6	63	341.1	124.2	23	397.5	144.7	83	453.9	165.2	43	510.3	185.7
04	285.7	104.0	64	342.1	124.5	24	398.4	145.0	84	454.8	165.5	44	511.2	186.0
05	286.6	104.3	65	343.0	124.8	25	399.4	145.4	85	455.8	165.9	45	512.1	186.4
06	287.6	104.7	66	343.9	125.2	26	400.3	145.7	86	456.7	166.3	46	513.1	186.8
07	288.5	105.0	67	344.9	125.5	27	401.3	146.1	87	457.7	166.6	47	514.0	187.1
08	289.4	105.4	68	345.8	125.9	28	402.2	146.4	88	458.6	166.9	48	515.0	187.4
09	290.4	105.7	69	346.8	126.2	29	403.1	146.7	89	459.5	167.3	49	515.9	187.8
10	291.3	106.0	70	347.7	126.6	30	404.1	147.1	90	460.5	167.7	50	516.8	188.2
311	292.3	106.4	371	348.6	126.9	431	405.0	147.4	491	461.4	168.0	551	517.8	188.5
12	293.2	106.7	72	349.6	127.2	32	406.0	147.8	92	462.4	168.3	52	518.7	188.8
13	294.1	107.1	73	350.5	127.6	33	406.9	148.1	93	463.3	168.6	53	519.7	189.1
14	295.1	107.4	74	351.5	127.9	34	407.8	148.4	94	464.2	168.9	54	520.6	189.4
15	296.0	107.7	75	352.4	128.3	35	408.8	148.8	95	465.2	169.3	55	521.5	189.8
16	297.0	108.1	76	353.3	128.6	36	409.7	149.1	96	466.1	169.6	56	522.5	190.2
17	297.9	108.4	77	354.3	129.0	37	410.7	149.5	97	467.0	170.0	57	523.4	190.5
18	298.8	108.8	78	355.2	129.3	38	411.6	149.8	98	468.0	170.3	58	524.4	190.8
19	299.8	109.1	79	356.2	129.6	39	412.5	150.2	99	468.9	170.7	59	525.3	191.2
20	300.7	109.5	80	357.1	130.0	40	413.5	150.5	500	469.9	171.0	60	526.2	191.6
321	301.6	109.8	381	358.0	130.3	441	414.4	150.8	501	470.8	171.3	561	527.2	191.9
22	302.6	110.1	82	359.0	130.7	42	415.4	151.2	02	471.7	171.7	62	528.1	192.2
23	303.5	110.5	83	359.9	131.0	43	416.3	151.5	03	472.7	172.0	63	529.0	192.5
24	304.5	110.8	84	360.8	131.3	44	417.2	151.9	04	473.6	172.4	64	530.0	192.9
25	305.4	111.2	85	361.8	131.7	45	418.2	152.2	05	474.5	172.7	65	530.9	193.2
26	306.3	111.5	86	362.7	132.0	46	419.1	152.5	06	475.4	173.0	66	531.8	193.6
27	307.3	111.8	87	363.7	132.4	47	420.0	152.9	07	476.4	173.4	67	532.8	193.9
28	308.2	112.2	88	364.6	132.7	48	421.0	153.2	08	477.3	173.7	68	533.7	194.2
29	309.2	112.5	89	365.5	133.1	49	421.9	153.6	09	478.3	174.1	69	534.7	194.6
30	310.1	112.9	90	366.5	133.4	50	422.9	153.9	10	479.2	174.4	70	535.6	195.0
331	311.0	113.2	391	367.4	133.7	451	423.8	154.3	511	480.2	174.8	571	536.6	195.3
32	312.0	113.6	92	368.4	134.1	52	424.7	154.6	12	481.1	175.1	72	537.5	195.6
33	312.9	113.9	93	369.3	134.4	53	425.7	154.9	13	482.1	175.4	73	538.5	195.9
34	313.9	114.2	94	370.2	134.8	54	426.6	155.3	14	483.0	175.8	74	539.4	196.3
35	314.8	114.6	95	371.2	135.1	55	427.6	155.6	15	484.0	176.1	75	540.3	196.6
36	315.7	114.9	96	372.1	135.4	56	428.5	156.0	16	484.9	176.5	76	541.3	197.0
37	316.7	115.3	97	373.1	135.8	57	429.4	156.3	17	485.8	176.8	77	542.2	197.3
38	317.6	115.6	98	374.0	136.1	58	430.4	156.7	18	486.8	177.2	78	543.2	197.7
39	318.6	116.0	99	374.9	136.5	59	431.3	157.0	19	487.7	177.5	79	544.1	198.0
40	319.5	116.3	400	375.9	136.8	60	432.3	157.4	20	488.7	177.9	80	545.0	198.4
341	320.4	116.6	401	376.8	137.2	461	433.2	157.7	521	489.6	178.2	581	546.0	198.7
42	321.4	117.0	02	377.8	137.5	62	434.1	158.0	22	490.5	178.5	82	546.9	199.0
43	322.3	117.3	03	378.7	137.8	63	435.1	158.4	23	491.5	178.9	83	547.9	199.4
44	323.3	117.7	04	379.6	138.2	64	436.0	158.7	24	492.4	179.2	84	548.8	199.8
45	324.2	118.0	05	380.6	138.5	65	437.0	159.0	25	493.4	179.6	85	549.8	200.1
46	325.1	118.4	06	381.5	138.9	66	437.9	159.4	26	494.3	179.9	86	550.7	200.4
47	326.1	118.7	07	382.5	139.2	67	438.8	159.7	27	495.3	180.2	87	551.7	200.8
48	327.0	119.0	08	383.4	139.6	68	439.8	160.1	28	496.2	180.6	88	552.6	201.2
49	328.0	119.4	09	384.3	139.9	69	440.7	160.4	29	497.1	181.0	89	553.5	201.5
50	328.9	119.7	10	385.3	140.2	70	441.7	160.8	30	498.1	181.3	90	554.4	201.8
351	329.8	120.1	411	386.2	140.6	471	442.6	161.1	531	499.0	181.6	591	555.4	202.1
52	330.8	120.4	12	387.2	140.9	72	443.5	161.4	32	499.9	181.9	92	556.3	202.4
53	331.7	120.7	13	388.1	141.3	73	444.5	161.8	33	500.9	182.3	93	557.3	202.8
54	332.7	121.1	14	389.0	141.6	74	445.4	162.1	34	501.8	182.6	94	558.2	203.2
55	333.6	121.4	15	390.0	141.9	75	446.4	162.5	35	502.7	183.0	95	559.1	203.5
56	334.5	121.8	16	390.9	142.3	76	447.3	162.8	36	503.7	183.3	96	560.0	203.8
57	335.5	122.1	17	391.9	142.6	77	448.2	163.2	37	504.6	183.7	97	561.0	204.2
58	336.4	122.5	18	392.8	143.0	78	449.2	163.5	38	505.5	184.0	98	561.9	204.6
59	337.4	122.8	19	393.7	143.3	79	450.1	163.8	39	506.5	184.3	99	562.9	204.9
60	338.3	123.1	20	394.7	143.7	80	451.1	164.2	40	507.4	184.7	600	563.8	205.2
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

70° (110°, 250°, 290°).

TABLE 2.

Difference of Latitude and Departure for 21° (159°, 201°, 339°).

Dist	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.4	61	56.9	21.9	121	113.0	43.4	181	169.0	64.9	241	225.0	86.4
2	1.9	0.7	62	57.9	22.2	22	113.9	43.7	82	169.9	65.2	42	225.9	86.7
3	2.8	1.1	63	58.8	22.6	23	114.8	44.1	83	170.8	65.6	43	226.9	87.1
4	3.7	1.4	64	59.7	22.9	24	115.8	44.4	84	171.8	65.9	44	227.8	87.4
5	4.7	1.8	65	60.7	23.3	25	116.7	44.8	85	172.7	66.3	45	228.7	87.8
6	5.6	2.2	66	61.6	23.7	26	117.6	45.2	86	173.6	66.7	46	229.7	88.2
7	6.5	2.5	67	62.5	24.0	27	118.6	45.5	87	174.6	67.0	47	230.6	88.5
8	7.5	2.9	68	63.5	24.4	28	119.5	45.9	88	175.5	67.4	48	231.5	88.9
9	8.4	3.2	69	64.4	24.7	29	120.4	46.2	89	176.4	67.7	49	232.5	89.2
10	9.3	3.6	70	65.4	25.1	30	121.4	46.6	90	177.4	68.1	50	233.4	89.6
11	10.3	3.9	71	66.3	25.4	131	122.3	46.9	191	178.3	68.4	251	234.3	90.0
12	11.2	4.3	72	67.2	25.8	32	123.2	47.3	92	179.2	68.8	52	235.3	90.3
13	12.1	4.7	73	68.2	26.2	33	124.2	47.7	93	180.2	69.2	53	236.2	90.7
14	13.1	5.0	74	69.1	26.5	34	125.1	48.0	94	181.1	69.5	54	237.1	91.0
15	14.0	5.4	75	70.0	26.9	35	126.0	48.4	95	182.0	69.9	55	238.1	91.4
16	14.9	5.7	76	71.0	27.2	36	127.0	48.7	96	183.0	70.2	56	239.0	91.7
17	15.9	6.1	77	71.9	27.6	37	127.9	49.1	97	183.9	70.6	57	239.9	92.1
18	16.8	6.5	78	72.8	28.0	38	128.8	49.5	98	184.8	71.0	58	240.9	92.5
19	17.7	6.8	79	73.8	28.3	39	129.8	49.8	99	185.8	71.3	59	241.8	92.8
20	18.7	7.2	80	74.7	28.7	40	130.7	50.2	200	186.7	71.7	60	242.7	93.2
21	19.6	7.5	81	75.6	29.0	141	131.6	50.5	201	187.6	72.0	261	243.7	93.5
22	20.5	7.9	82	76.6	29.4	42	132.6	50.9	02	188.6	72.4	62	244.6	93.9
23	21.5	8.2	83	77.5	29.7	43	133.5	51.2	03	189.5	72.7	63	245.5	94.3
24	22.4	8.6	84	78.4	30.1	44	134.4	51.6	04	190.5	73.1	64	246.5	94.6
25	23.3	9.0	85	79.4	30.5	45	135.4	52.0	05	191.4	73.5	65	247.4	95.0
26	24.3	9.3	86	80.3	30.8	46	136.3	52.3	06	192.3	73.8	66	248.3	95.3
27	25.2	9.7	87	81.2	31.2	47	137.2	52.7	07	193.3	74.2	67	249.3	95.7
28	26.1	10.0	88	82.2	31.5	48	138.2	53.0	08	194.2	74.5	68	250.2	96.0
29	27.1	10.4	89	83.1	31.9	49	139.1	53.4	09	195.1	74.9	69	251.1	96.4
30	28.0	10.8	90	84.0	32.3	50	140.0	53.8	10	196.1	75.3	70	252.1	96.8
31	28.9	11.1	91	85.0	32.6	151	141.0	54.1	211	197.0	75.6	271	253.0	97.1
32	29.9	11.5	92	85.9	33.0	52	141.9	54.5	12	197.9	76.0	72	253.9	97.5
33	30.8	11.8	93	86.8	33.3	53	142.8	54.8	13	198.9	76.3	73	254.9	97.8
34	31.7	12.2	94	87.8	33.7	54	143.8	55.2	14	199.8	76.7	74	255.8	98.2
35	32.7	12.5	95	88.7	34.0	55	144.7	55.5	15	200.7	77.0	75	256.7	98.6
36	33.6	12.9	96	89.6	34.4	56	145.6	55.9	16	201.7	77.4	76	257.7	98.9
37	34.5	13.3	97	90.6	34.8	57	146.6	56.3	17	202.6	77.8	77	258.6	99.3
38	35.5	13.6	98	91.5	35.1	58	147.5	56.6	18	203.5	78.1	78	259.5	99.6
39	36.4	14.0	99	92.4	35.5	59	148.4	57.0	19	204.5	78.5	79	260.5	100.0
40	37.3	14.3	100	93.4	35.8	60	149.4	57.3	20	205.4	78.8	80	261.4	100.3
41	38.3	14.7	101	94.3	36.2	161	150.3	57.7	221	206.3	79.2	281	262.3	100.7
42	39.2	15.1	02	95.2	36.6	62	151.2	58.1	22	207.3	79.6	82	263.3	101.1
43	40.1	15.4	03	96.2	36.9	63	152.2	58.4	23	208.2	79.9	83	264.2	101.4
44	41.1	15.8	04	97.1	37.3	64	153.1	58.8	24	209.1	80.3	84	265.1	101.8
45	42.0	16.1	05	98.0	37.6	65	154.0	59.1	25	210.1	80.6	85	266.1	102.1
46	42.9	16.5	06	99.0	38.0	66	155.0	59.5	26	211.0	81.0	86	267.0	102.5
47	43.9	16.8	07	99.9	38.3	67	155.9	59.8	27	211.9	81.3	87	267.9	102.9
48	44.8	17.2	08	100.8	38.7	68	156.8	60.2	28	212.9	81.7	88	268.9	103.2
49	45.7	17.6	09	101.8	39.1	69	157.8	60.6	29	213.8	82.1	89	269.8	103.6
50	46.7	17.9	10	102.7	39.4	70	158.7	60.9	30	214.7	82.4	90	270.7	103.9
51	47.6	18.3	111	103.6	39.8	171	159.6	61.3	231	215.7	82.8	291	271.7	104.3
52	48.5	18.6	12	104.6	40.1	72	160.6	61.6	32	216.6	83.1	92	272.6	104.6
53	49.5	19.0	13	105.5	40.5	73	161.5	62.0	33	217.5	83.5	93	273.5	105.0
54	50.4	19.4	14	106.4	40.9	74	162.4	62.4	34	218.5	83.9	94	274.5	105.4
55	51.3	19.7	15	107.4	41.2	75	163.4	62.7	35	219.4	84.2	95	275.4	105.7
56	52.3	20.1	16	108.3	41.6	76	164.3	63.1	36	220.3	84.6	96	276.3	106.1
57	53.2	20.4	17	109.2	41.9	77	165.2	63.4	37	221.3	84.9	97	277.3	106.4
58	54.1	20.8	18	110.2	42.3	78	166.2	63.8	38	222.2	85.3	98	278.2	106.8
59	55.1	21.1	19	111.1	42.6	79	167.1	64.1	39	233.1	85.6	99	279.1	107.2
60	56.0	21.5	20	112.0	43.0	80	168.0	64.5	40	224.1	86.0	300	280.1	107.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

69° (111°, 249°, 291°).

TABLE 2.

Difference of Latitude and Departure for 21° (159°, 201°, 339°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	281.0	107.9	361	337.0	129.4	421	393.0	150.9	481	449.0	172.4	541	505.1	193.9
02	281.9	108.2	62	337.9	129.7	22	394.0	151.2	82	450.0	172.7	42	506.0	194.2
03	282.9	108.6	63	338.9	130.1	23	394.9	151.6	83	450.9	173.1	43	507.0	194.6
04	283.8	108.9	64	339.8	130.4	24	395.8	152.0	84	451.8	173.5	44	507.9	195.0
05	284.7	109.3	65	340.7	130.8	25	396.8	152.3	85	452.8	173.8	45	508.8	195.3
06	285.7	109.7	66	341.7	131.2	26	397.7	152.7	86	453.7	174.2	46	509.8	195.7
07	286.6	110.0	67	342.6	131.5	27	398.6	153.0	87	454.6	174.5	47	510.7	196.0
08	287.5	110.4	68	343.5	131.9	28	399.6	153.4	88	455.6	174.9	48	511.6	196.4
09	288.5	110.7	79	344.5	132.2	29	400.5	153.7	89	456.5	175.2	49	512.6	196.8
10	289.4	111.1	70	345.4	132.6	30	401.4	154.1	90	457.4	175.6	50	513.5	197.1
311	290.3	111.5	371	346.3	133.0	431	402.4	154.5	491	458.4	176.0	551	514.4	197.5
12	291.3	111.8	72	347.3	133.3	32	403.3	154.8	92	459.3	176.3	52	515.4	197.8
13	292.2	112.2	73	348.2	133.7	33	404.2	155.2	93	460.2	176.7	53	516.3	198.2
14	293.1	112.5	74	349.1	134.0	34	405.2	155.5	94	461.2	177.0	54	517.2	198.6
15	294.1	112.9	75	350.1	134.4	35	406.1	155.9	95	462.1	177.4	55	518.2	198.9
16	295.0	113.2	76	351.0	134.7	36	407.0	156.3	96	463.0	177.8	56	519.1	199.3
17	295.9	113.6	77	351.9	135.1	37	408.0	156.6	97	464.0	178.1	57	520.0	199.6
18	296.9	114.0	78	352.9	135.5	38	408.9	157.0	98	464.9	178.5	58	521.0	200.0
19	297.8	114.3	79	353.8	135.8	39	409.8	157.3	99	465.8	178.8	59	521.9	200.3
20	298.7	114.7	80	354.7	136.2	40	410.8	157.7	500	466.8	179.2	60	522.8	200.7
321	299.7	115.0	381	355.7	136.5	441	411.7	158.0	501	467.7	179.5	561	523.8	201.0
22	300.6	115.4	82	356.6	136.9	42	412.6	158.4	02	468.6	179.9	62	524.7	201.4
23	301.5	115.8	83	357.5	137.3	43	413.6	158.8	03	469.6	180.3	63	525.6	201.8
24	302.5	116.1	84	358.5	137.6	44	414.5	159.1	04	470.5	180.6	64	526.6	202.1
25	303.4	116.5	85	359.4	138.0	45	415.4	159.5	05	471.5	181.0	65	527.5	202.5
26	304.3	116.8	86	360.3	138.3	46	416.4	159.8	06	472.4	181.3	66	528.4	202.8
27	305.3	117.2	87	361.3	138.7	47	417.3	160.2	07	473.3	181.7	67	529.4	203.2
28	306.2	117.5	88	362.2	139.1	48	418.2	160.5	08	474.3	182.0	68	530.3	203.5
29	307.1	117.9	89	363.1	139.4	49	419.2	160.9	09	475.2	182.4	69	531.2	203.9
30	308.1	118.3	90	364.1	139.8	50	420.1	161.3	10	476.1	182.8	70	532.2	204.3
331	309.0	118.6	391	365.0	140.1	451	421.0	161.6	511	477.1	183.1	571	533.1	204.6
32	309.9	119.0	92	365.9	140.5	52	422.0	162.0	12	478.0	183.5	72	534.0	205.0
33	310.9	119.3	93	366.9	140.8	53	422.9	162.3	13	478.9	183.8	73	535.0	205.4
34	311.8	119.7	94	367.8	141.2	54	423.8	162.7	14	479.9	184.2	74	535.9	205.7
35	312.7	120.1	95	368.7	141.6	55	424.8	163.1	15	480.8	184.6	75	536.8	206.1
36	313.7	120.4	96	369.7	141.9	56	425.7	163.4	16	481.7	184.9	76	537.8	206.4
37	314.6	120.8	97	370.6	142.3	57	426.6	163.8	17	482.7	185.3	77	538.7	206.8
38	315.5	121.1	98	371.5	142.6	58	427.6	164.1	18	483.6	185.6	78	539.6	207.1
39	316.5	121.5	99	372.5	143.0	59	428.5	164.5	19	484.5	186.0	79	540.6	207.5
40	317.4	121.8	400	373.4	143.4	60	429.4	164.9	20	485.5	186.4	80	541.5	207.9
341	318.3	122.2	401	374.3	143.7	461	430.4	165.2	521	486.4	186.7	581	542.4	208.2
42	319.3	122.6	02	375.3	144.1	62	431.3	165.6	22	487.3	187.1	82	543.4	208.6
43	320.2	122.9	03	376.2	144.4	63	432.2	165.9	23	488.3	187.4	83	544.3	208.9
44	321.1	123.2	04	377.1	144.8	64	433.2	166.3	24	489.2	187.8	84	545.2	209.3
45	322.1	123.6	05	378.1	145.1	65	434.1	166.6	25	490.1	188.1	85	546.2	209.6
46	323.0	124.0	06	379.0	145.5	66	435.0	167.0	26	491.1	188.5	86	547.1	210.0
47	323.9	124.4	07	379.9	145.9	67	436.0	167.4	27	492.0	188.9	87	548.0	210.4
48	324.9	124.7	08	380.9	146.2	68	436.9	167.7	28	492.9	189.2	88	549.0	210.7
49	325.8	125.1	09	381.8	146.6	69	437.8	168.1	29	493.9	189.6	89	549.9	211.1
50	326.7	125.4	10	382.7	146.9	70	438.8	168.4	30	494.8	189.9	90	550.8	211.4
351	327.7	125.8	411	383.7	147.3	471	439.7	168.8	531	495.7	190.3	591	551.8	211.8
52	328.6	126.1	12	384.6	147.7	72	440.6	169.2	32	496.7	190.7	92	552.7	212.2
53	329.5	126.5	13	385.5	148.0	73	441.6	169.5	33	497.6	191.0	93	553.6	212.5
54	330.5	126.9	14	386.5	148.4	74	442.5	169.9	34	498.5	191.4	94	554.6	212.9
55	331.4	127.2	15	387.4	148.7	75	443.4	170.2	35	499.5	191.7	95	555.5	213.2
56	332.3	127.6	16	388.4	149.1	76	444.4	170.6	36	500.4	192.1	96	556.4	213.6
57	333.3	127.9	17	389.3	149.4	77	445.3	170.9	37	501.3	192.4	97	557.4	213.9
58	334.2	128.3	18	390.2	149.8	78	446.2	171.3	38	502.3	192.8	98	558.2	214.3
59	335.1	128.7	19	391.2	150.2	79	447.2	171.7	39	503.2	193.2	99	559.2	214.7
60	336.1	129.0	20	392.1	150.5	80	448.1	172.0	40	504.1	193.5	600	560.1	215.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

69° (111°, 249°, 291°).

TABLE 2.

Difference of Latitude and Departure for 22° (158°, 202, 338°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.4	61	56.6	22.9	121	112.2	45.3	181	167.8	67.8	241	223.5	90.3
2	1.9	0.7	62	57.5	23.2	22	113.1	45.7	82	168.7	68.2	42	224.4	90.7
3	2.8	1.1	63	58.4	23.6	23	114.0	46.1	83	169.7	68.6	43	225.3	91.0
4	3.7	1.5	64	59.3	24.0	24	115.0	46.5	84	170.6	68.9	44	226.2	91.4
5	4.6	1.9	65	60.3	24.3	25	115.9	46.8	85	171.5	69.3	45	227.2	91.8
6	5.6	2.2	66	61.2	24.7	26	116.8	47.2	86	172.5	69.7	46	228.1	92.2
7	6.5	2.6	67	62.1	25.1	27	117.8	47.6	87	173.4	70.1	47	229.0	92.5
8	7.4	3.0	68	63.0	25.5	28	118.7	47.9	88	174.3	70.4	48	229.9	92.9
9	8.3	3.4	69	64.0	25.8	29	119.6	48.3	89	175.2	70.8	49	230.9	93.3
10	9.3	3.7	70	64.9	26.2	30	120.5	48.7	90	176.2	71.2	50	231.8	93.7
11	10.2	4.1	71	65.8	26.6	131	121.5	49.1	191	177.1	71.5	251	232.7	94.0
12	11.1	4.5	72	66.8	27.0	32	122.4	49.4	92	178.0	71.9	52	233.7	94.4
13	12.1	4.9	73	67.7	27.3	33	123.3	49.8	93	178.9	72.3	53	234.6	94.8
14	13.0	5.2	74	68.6	27.7	34	124.2	50.2	94	179.9	72.7	54	235.5	95.2
15	13.9	5.6	75	69.5	28.1	35	125.2	50.6	95	180.8	73.0	55	236.4	95.5
16	14.8	6.0	76	70.5	28.5	36	126.1	50.9	96	181.7	73.4	56	237.4	95.9
17	15.8	6.4	77	71.4	28.8	37	127.0	51.3	97	182.7	73.8	57	238.3	96.3
18	16.7	6.7	78	72.3	29.2	38	128.0	51.7	98	183.6	74.2	58	239.2	96.6
19	17.6	7.1	79	73.2	29.6	39	128.9	52.1	99	184.5	74.5	59	240.1	97.0
20	18.5	7.5	80	74.2	30.0	40	129.8	52.4	200	185.4	74.9	60	241.1	97.4
21	19.5	7.9	81	75.1	30.3	141	130.7	52.8	201	186.4	75.3	261	242.0	97.8
22	20.4	8.2	82	76.0	30.7	42	131.7	53.2	02	187.3	75.7	62	242.9	98.1
23	21.3	8.6	83	77.0	31.1	43	132.6	53.6	03	188.2	76.0	63	243.8	98.5
24	22.3	9.0	84	77.9	31.5	44	133.5	53.9	04	189.1	76.4	64	244.8	98.9
25	23.2	9.4	85	78.8	31.8	45	134.4	54.3	05	190.1	76.8	65	245.7	99.3
26	24.1	9.7	86	79.7	32.2	46	135.4	54.7	06	191.0	77.2	66	246.6	99.6
27	25.0	10.1	87	80.7	32.6	47	136.3	55.1	07	191.9	77.5	67	247.6	100.0
28	26.0	10.5	88	81.6	33.0	48	137.2	55.4	08	192.9	77.9	68	248.5	100.4
29	26.9	10.9	89	82.5	33.3	49	138.2	55.8	09	193.8	78.3	69	249.4	100.8
30	27.8	11.2	90	83.4	33.7	50	139.1	56.2	10	194.7	78.7	70	250.3	101.1
31	28.7	11.6	91	84.4	34.1	151	140.0	56.6	211	195.6	79.0	271	251.3	101.5
32	29.7	12.0	92	85.3	34.5	52	140.9	56.9	12	196.6	79.4	72	252.2	101.9
33	30.6	12.4	93	86.2	34.8	53	141.9	57.3	13	197.5	79.8	73	253.1	102.3
34	31.5	12.7	94	87.2	35.2	54	142.8	57.7	14	198.4	80.2	74	254.0	102.6
35	32.5	13.1	95	88.1	35.6	55	143.7	58.1	15	199.3	80.5	75	255.0	103.0
36	33.4	13.5	96	89.0	36.0	56	144.6	58.4	16	200.3	80.9	76	255.9	103.4
37	34.3	13.9	97	89.9	36.3	57	145.6	58.8	17	201.2	81.3	77	256.8	103.8
38	35.2	14.2	98	90.9	36.7	58	146.5	59.2	18	202.1	81.7	78	257.8	104.1
39	36.2	14.6	99	91.8	37.1	59	147.4	59.6	19	203.1	82.0	79	258.7	104.5
40	37.1	15.0	100	92.7	37.5	60	148.3	59.9	20	204.0	82.4	80	259.6	104.9
41	38.0	15.4	101	93.6	37.8	161	149.3	60.3	221	204.9	82.8	281	260.5	105.3
42	38.9	15.7	02	94.6	38.2	62	150.2	60.7	22	205.8	83.2	82	261.5	105.6
43	39.9	16.1	03	95.5	38.6	63	151.1	61.1	23	206.8	83.5	83	262.4	106.0
44	40.8	16.5	04	96.4	39.0	64	152.1	61.4	24	207.7	83.9	84	263.3	106.4
45	41.7	16.9	05	97.4	39.3	65	153.0	61.8	25	208.6	84.3	85	264.2	106.8
46	42.7	17.2	06	98.3	39.7	66	153.9	62.2	26	209.5	84.7	86	265.2	107.1
47	43.6	17.6	07	99.2	40.1	67	154.8	62.6	27	210.5	85.0	87	266.1	107.5
48	44.5	18.0	08	100.1	40.5	68	155.8	62.9	28	211.4	85.4	88	267.0	107.9
49	45.4	18.4	09	101.1	40.8	69	156.7	63.3	29	212.3	85.8	89	268.0	108.3
50	46.4	18.7	10	102.0	41.2	70	157.6	63.7	30	213.3	86.2	90	268.9	108.6
51	47.3	19.1	111	102.9	41.6	171	158.5	64.1	231	214.2	86.5	291	269.8	109.0
52	48.2	19.5	12	103.8	42.0	72	159.5	64.4	32	215.1	86.9	92	270.7	109.4
53	49.1	19.9	13	104.8	42.3	73	160.4	64.8	33	216.0	87.3	93	271.7	109.8
54	50.1	20.2	14	105.7	42.7	74	161.3	65.2	34	217.0	87.7	94	272.6	110.1
55	51.0	20.6	15	106.6	43.1	75	162.3	65.6	35	217.9	88.0	95	273.5	110.5
56	51.9	21.0	16	107.6	43.5	76	163.2	65.9	36	218.8	88.4	96	274.4	110.9
57	52.8	21.4	17	108.5	43.8	77	164.1	66.3	37	219.7	88.8	97	275.4	111.3
58	53.8	21.7	18	109.4	44.2	78	165.0	66.7	38	220.7	89.2	98	276.3	111.6
59	54.7	22.1	19	110.3	44.6	79	166.0	67.1	39	221.6	89.5	99	277.2	112.0
60	55.6	22.5	20	111.3	45.0	80	166.9	67.4	40	222.5	89.9	300	278.2	112.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

68° (112°, 248°, 292°).

TABLE 2.

Difference of Latitude and Departure for 22° (158°, 202°, 338°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	279.1	112.7	361	334.7	135.2	421	390.3	157.7	481	446.0	180.2	541	501.6	202.7
02	280.0	113.1	62	335.6	135.6	22	391.3	158.1	82	446.9	180.6	42	502.5	203.1
03	280.9	113.5	63	336.6	136.0	23	392.2	158.4	83	447.8	180.9	43	503.4	203.5
04	281.9	113.9	64	337.5	136.3	24	393.1	158.8	84	448.8	181.3	44	504.4	203.8
05	282.8	114.2	65	338.4	136.7	25	394.1	159.2	85	449.7	181.7	45	505.3	204.2
06	283.7	114.6	66	339.3	137.1	26	395.0	159.6	86	450.6	182.1	46	506.2	204.6
07	284.6	115.0	67	340.3	137.5	27	395.9	159.9	87	451.6	182.4	47	507.2	205.0
08	285.6	115.4	68	341.2	137.8	28	396.8	160.3	88	452.5	182.8	48	508.1	205.3
09	286.5	115.7	69	342.1	138.2	29	397.8	160.7	89	453.4	183.2	49	509.0	205.7
10	287.4	116.1	70	343.1	138.6	30	398.7	161.1	90	454.3	183.6	50	510.0	206.1
311	288.4	116.5	371	344.0	139.0	431	399.6	161.4	491	455.3	184.0	551	510.9	206.5
12	289.3	116.8	72	344.9	139.3	32	400.5	161.8	92	456.2	184.3	52	511.8	206.8
13	290.2	117.2	73	345.8	139.7	33	401.5	162.2	93	457.1	184.7	53	512.7	207.2
14	291.1	117.6	74	346.8	140.1	34	402.4	162.6	94	458.0	185.1	54	513.6	207.6
15	292.1	118.0	75	347.7	140.5	35	403.3	162.9	95	459.0	185.4	55	514.6	208.0
16	293.0	118.3	76	348.6	140.8	36	404.3	163.3	96	459.9	185.8	56	515.5	208.3
17	293.9	118.7	77	349.5	141.2	37	405.2	163.7	97	460.8	186.2	57	516.4	208.7
18	294.8	119.1	78	350.5	141.6	38	406.1	164.1	98	461.8	186.6	58	517.4	209.1
19	295.8	119.5	79	351.4	141.9	39	407.0	164.4	99	462.7	186.9	59	518.3	209.4
20	296.7	119.8	80	352.3	142.3	40	408.0	164.8	500	463.6	187.3	60	519.2	209.8
321	297.6	120.2	381	353.3	142.7	441	408.9	165.2	501	464.5	187.7	561	520.1	210.2
22	298.6	120.6	82	354.2	143.1	42	409.8	165.5	02	465.4	188.0	62	521.0	210.5
23	299.5	121.0	83	355.1	143.4	43	410.7	165.9	03	466.4	188.4	63	522.0	210.9
24	300.4	121.3	84	356.0	143.8	44	411.7	166.3	04	467.3	188.8	64	522.9	211.3
25	301.3	121.7	85	357.0	144.2	45	412.6	166.7	05	468.2	189.2	65	523.8	211.7
26	302.3	122.1	86	357.9	144.6	46	413.5	167.0	06	469.2	189.5	66	524.8	212.0
27	303.2	122.5	87	358.8	144.9	47	414.5	167.4	07	470.1	189.9	67	525.7	212.4
28	304.1	122.8	88	359.7	145.3	48	415.4	167.8	08	471.0	190.3	68	526.6	212.8
29	305.0	123.2	89	360.7	145.7	49	416.3	168.2	09	471.9	190.7	69	527.5	213.2
30	306.0	123.6	90	361.6	146.1	50	417.2	168.5	10	472.9	191.1	70	528.5	213.5
331	306.9	124.0	391	362.5	146.4	451	418.2	168.9	511	473.8	191.4	571	529.4	213.9
32	307.8	124.3	92	363.5	146.8	52	419.1	169.3	12	474.7	191.8	72	530.3	214.3
33	308.8	124.7	93	364.4	147.2	53	420.0	169.7	13	475.6	192.2	73	531.2	214.7
34	309.7	125.1	94	365.3	147.6	54	420.9	170.0	14	476.6	192.5	74	532.2	215.0
35	310.6	125.5	95	366.2	147.9	55	421.9	170.4	15	477.5	192.9	75	533.1	215.4
36	311.5	125.8	96	367.2	148.3	56	422.8	170.8	16	478.4	193.3	76	534.0	215.8
37	312.5	126.2	97	368.1	148.7	57	423.7	171.2	17	479.3	193.7	77	534.9	216.2
38	313.4	126.6	98	369.0	149.1	58	424.6	171.5	18	480.3	194.0	78	535.9	216.5
39	314.3	127.0	99	369.9	149.4	59	425.6	171.9	19	481.2	194.4	79	536.8	216.9
40	315.2	127.3	400	370.9	149.8	60	426.5	172.3	20	482.1	194.8	80	537.7	217.3
341	316.2	127.7	401	371.8	150.2	461	427.4	172.7	521	483.0	195.2	581	538.6	217.7
42	317.1	128.1	02	372.7	150.6	62	428.4	173.0	22	484.0	195.5	82	539.6	218.0
43	318.0	128.5	03	373.7	150.9	63	429.3	173.4	23	484.9	195.9	83	540.5	218.4
44	319.0	128.8	04	374.6	151.3	64	430.2	173.8	24	485.8	196.3	84	541.4	218.8
45	319.9	129.2	05	375.5	151.7	65	431.1	174.2	25	486.7	196.7	85	542.4	219.2
46	320.8	129.6	06	376.4	152.1	66	432.1	174.5	26	487.7	197.0	86	543.3	219.5
47	321.7	130.0	07	377.4	152.4	67	433.0	174.9	27	488.6	197.4	87	544.2	219.9
48	322.7	130.3	08	378.3	152.8	68	433.9	175.3	28	489.5	197.8	88	545.1	220.3
49	323.6	130.7	09	379.2	153.2	69	434.8	175.7	29	490.4	198.2	89	546.1	220.7
50	324.5	131.1	10	380.1	153.6	70	435.8	176.0	30	491.4	198.5	90	547.0	221.0
351	325.4	131.5	411	381.1	153.9	471	436.7	176.4	531	492.3	198.9	591	547.9	221.4
52	326.4	131.8	12	382.0	154.3	72	437.6	176.8	32	493.2	199.3	92	548.9	221.8
53	327.3	132.2	13	382.9	154.7	73	438.6	177.2	33	494.2	199.7	93	549.8	222.2
54	328.2	132.6	14	383.9	155.1	74	439.5	177.5	34	495.1	200.0	94	550.7	222.5
55	329.2	133.0	15	384.8	155.4	75	440.4	177.9	35	496.0	200.4	95	551.7	222.9
56	330.1	133.3	16	385.7	155.8	76	441.3	178.3	36	496.9	200.8	96	552.6	223.3
57	331.0	133.7	17	386.6	156.2	77	442.3	178.7	37	497.9	201.2	97	553.5	223.7
58	332.0	134.1	18	387.6	156.6	78	443.2	179.0	38	498.8	201.5	98	554.4	224.0
59	332.9	134.5	19	388.5	156.9	79	444.1	179.4	39	499.7	201.9	99	555.4	224.4
60	333.8	134.8	20	389.4	157.3	80	445.0	179.8	40	500.7	202.3	600	556.3	224.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

68° (112°, 248°, 292°).

TABLE 2.

Difference of Latitude and Departure for 23° (157°, 203°, 337°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.4	61	56.2	23.8	121	111.4	47.3	181	166.6	70.7	241	221.8	94.2
2	1.8	0.8	62	57.1	24.2	22	112.3	47.7	82	167.5	71.1	42	222.8	94.6
3	2.8	1.2	63	58.0	24.6	23	113.2	48.1	83	168.5	71.5	43	223.7	94.9
4	3.7	1.6	64	58.9	25.0	24	114.1	48.5	84	169.4	71.9	44	224.6	95.3
5	4.6	2.0	65	59.8	25.4	25	115.1	48.8	85	170.3	72.3	45	225.5	95.7
6	5.5	2.3	66	60.8	25.8	26	116.0	49.2	86	171.2	72.7	46	226.4	96.1
7	6.4	2.7	67	61.7	26.2	27	116.9	49.6	87	172.1	73.1	47	227.4	96.5
8	7.4	3.1	68	62.6	26.6	28	117.8	50.0	88	173.1	73.5	48	228.3	96.9
9	8.3	3.5	69	63.5	27.0	29	118.7	50.4	89	174.0	73.8	49	229.2	97.3
10	9.2	3.9	70	64.4	27.4	30	119.7	50.8	90	174.9	74.2	50	230.1	97.7
11	10.1	4.3	71	65.4	27.7	131	120.6	51.2	191	175.8	74.6	251	231.0	98.1
12	11.0	4.7	72	66.3	28.1	32	121.5	51.6	92	176.7	75.0	52	232.0	98.5
13	12.0	5.1	73	67.2	28.5	33	122.4	52.0	93	177.7	75.4	53	232.9	98.9
14	12.9	5.5	74	68.1	28.9	34	123.3	52.4	94	178.6	75.8	54	233.8	99.2
15	13.8	5.9	75	69.0	29.3	35	124.3	52.7	95	179.5	76.2	55	234.7	99.6
16	14.7	6.3	76	70.0	29.7	36	125.2	53.1	96	180.4	76.6	56	235.6	100.0
17	15.6	6.6	77	70.9	30.1	37	126.1	53.5	97	181.3	77.0	57	236.6	100.4
18	16.6	7.0	78	71.8	30.5	38	127.0	53.9	98	182.3	77.4	58	237.5	100.8
19	17.5	7.4	79	72.7	30.9	39	128.0	54.3	99	183.2	77.8	59	238.4	101.2
20	18.4	7.8	80	73.6	31.3	40	128.9	54.7	200	184.1	78.1	60	239.3	101.6
21	19.3	8.2	81	74.6	31.6	141	129.8	55.1	201	185.0	78.5	261	240.3	102.0
22	20.3	8.6	82	75.5	32.0	42	130.7	55.5	02	185.9	78.9	62	241.2	102.4
23	21.2	9.0	83	76.4	32.4	43	131.6	55.9	03	186.9	79.3	63	242.1	102.8
24	22.1	9.4	84	77.3	32.8	44	132.6	56.3	04	187.8	79.7	64	243.0	103.2
25	23.0	9.8	85	78.2	33.2	45	133.5	56.7	05	188.7	80.1	65	243.9	103.5
26	23.9	10.2	86	79.2	33.6	46	134.4	57.0	06	189.6	80.5	66	244.9	103.9
27	24.9	10.5	87	80.1	34.0	47	135.3	57.4	07	190.5	80.9	67	245.8	104.3
28	25.8	10.9	88	81.0	34.4	48	136.2	57.8	08	191.5	81.3	68	246.7	104.7
29	26.7	11.3	89	81.9	34.8	49	137.2	58.2	09	192.4	81.7	69	247.6	105.1
30	27.6	11.7	90	82.8	35.2	50	138.1	58.6	10	193.3	82.1	70	248.5	105.5
31	28.5	12.1	91	83.8	35.6	151	139.0	59.0	211	194.2	82.4	271	249.5	105.9
32	29.5	12.5	92	84.7	35.9	52	139.9	59.4	12	195.1	82.8	72	250.4	106.3
33	30.4	12.9	93	85.6	36.3	53	140.8	59.8	13	196.1	83.2	73	251.3	106.7
34	31.3	13.3	94	86.5	36.7	54	141.8	60.2	14	197.0	83.6	74	252.2	107.1
35	32.2	13.7	95	87.4	37.1	55	142.7	60.6	15	197.9	84.0	75	253.1	107.5
36	33.1	14.1	96	88.4	37.5	56	143.6	61.0	16	198.8	84.4	76	254.1	107.8
37	34.1	14.5	97	89.3	37.9	57	144.5	61.3	17	199.7	84.8	77	255.0	108.2
38	35.0	14.8	98	90.2	38.3	58	145.4	61.7	18	200.7	85.2	78	255.9	108.6
39	35.9	15.2	99	91.1	38.7	59	146.4	62.1	19	201.6	85.6	79	256.8	109.0
40	36.8	15.6	100	92.1	39.1	60	147.3	62.5	20	202.5	86.0	80	257.7	109.4
41	37.7	16.0	101	93.0	39.5	161	148.2	62.9	221	203.4	86.4	281	258.7	109.8
42	38.7	16.4	02	93.9	39.9	62	149.1	63.3	22	204.4	86.7	82	259.6	110.2
43	39.6	16.8	03	94.8	40.2	63	150.0	63.7	23	205.3	87.1	83	260.5	110.6
44	40.5	17.2	04	95.7	40.6	64	151.0	64.1	24	206.2	87.5	84	261.4	111.0
45	41.4	17.6	05	96.7	41.0	65	151.9	64.5	25	207.1	87.9	85	262.3	111.4
46	42.3	18.0	06	97.6	41.4	66	152.8	64.9	26	208.0	88.3	86	263.3	111.7
47	43.3	18.4	07	98.5	41.8	67	153.7	65.3	27	209.0	88.7	87	264.2	112.1
48	44.2	18.8	08	99.4	42.2	68	154.6	65.6	28	209.9	89.1	88	265.1	112.5
49	45.1	19.1	09	100.3	42.6	69	155.6	66.0	29	210.8	89.5	89	266.0	112.9
50	46.0	19.5	10	101.3	43.0	70	156.5	66.4	30	211.7	89.9	90	266.9	113.3
51	46.9	19.9	111	102.2	43.4	171	157.4	66.8	231	212.6	90.3	291	267.9	113.7
52	47.9	20.3	12	103.1	43.8	72	158.3	67.2	32	213.6	90.6	92	268.8	114.1
53	48.8	20.7	13	104.0	44.2	73	159.2	67.6	33	214.5	91.0	93	269.7	114.5
54	49.7	21.1	14	104.9	44.5	74	160.2	68.0	34	215.4	91.4	94	270.6	114.9
55	50.6	21.5	15	105.9	44.9	75	161.1	68.4	35	216.3	91.8	95	271.5	115.3
56	51.5	21.9	16	106.8	45.3	76	162.0	68.8	36	217.2	92.2	96	272.5	115.7
57	52.5	22.3	17	107.7	45.7	77	162.9	69.2	37	218.2	92.6	97	273.4	116.0
58	53.4	22.7	18	108.6	46.1	78	163.8	69.6	38	219.1	93.0	98	274.3	116.4
59	54.3	23.1	19	109.5	46.5	79	164.8	69.9	39	220.0	93.4	99	275.2	116.8
60	55.2	23.4	20	110.5	46.9	80	165.7	70.3	40	220.9	93.8	300	276.2	117.2
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

67° (113°, 247°, 293°).

TABLE 2.

Difference of Latitude and Departure for 23° (157°, 203°, 337°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	277.1	117.6	361	332.3	141.1	421	387.5	164.5	481	442.7	188.0	541	498.0	211.4
02	278.0	118.0	62	333.2	141.5	22	388.5	164.9	82	443.7	188.4	42	498.9	211.8
03	278.9	118.4	63	334.1	141.8	23	389.4	165.3	83	444.6	188.8	43	499.8	212.2
04	279.8	118.8	64	335.1	142.2	24	390.3	165.7	84	445.5	189.2	44	500.7	212.6
05	280.8	119.2	65	336.0	142.6	25	391.2	166.1	85	446.4	189.5	45	501.7	213.0
06	281.7	119.6	66	336.9	143.0	26	392.1	166.5	86	447.3	189.9	46	502.6	213.4
07	282.6	120.0	67	337.8	143.4	27	393.1	166.8	87	448.3	190.2	47	503.5	213.8
08	283.5	120.4	68	338.7	143.8	28	394.0	167.2	88	449.2	190.6	48	504.4	214.2
09	284.4	120.8	69	339.7	144.2	29	394.9	167.6	89	450.1	191.0	49	505.3	214.6
10	285.4	121.2	70	340.6	144.6	30	395.8	168.0	90	451.0	191.4	50	506.3	215.0
311	286.3	121.6	371	341.5	145.0	431	396.7	168.4	491	451.9	191.8	551	507.2	215.3
12	287.2	121.9	72	342.4	145.4	32	397.7	168.8	92	452.9	192.2	52	508.1	215.6
13	288.1	122.3	73	343.4	145.7	33	398.6	169.2	93	453.8	192.6	53	509.0	216.0
14	289.0	122.7	74	344.3	146.1	34	399.5	169.6	94	454.7	193.0	54	509.9	216.4
15	290.0	123.1	75	345.2	146.5	35	400.4	170.0	95	455.6	193.4	55	510.9	216.8
16	290.9	123.5	76	346.1	146.9	36	401.3	170.4	96	456.6	193.8	56	511.8	217.2
17	291.8	123.9	77	347.0	147.3	37	402.3	170.8	97	457.5	194.2	57	512.7	217.6
18	292.7	124.3	78	348.0	147.7	38	403.2	171.1	98	458.4	194.6	58	513.6	218.0
19	293.6	124.6	79	348.9	148.1	39	404.1	171.5	99	459.3	195.0	59	514.5	218.4
20	294.6	125.0	80	349.8	148.5	40	405.0	171.9	500	460.2	195.4	60	515.5	218.8
321	295.5	125.4	381	350.7	148.9	441	405.9	172.3	501	461.2	195.8	561	516.4	219.2
22	296.4	125.8	82	351.6	149.3	42	406.9	172.7	02	462.1	196.2	62	517.3	219.6
23	297.3	126.2	83	352.6	149.7	43	407.8	173.1	03	463.0	196.6	63	518.2	220.0
24	298.2	126.6	84	353.5	150.0	44	408.7	173.5	04	463.9	197.0	64	519.2	220.4
25	299.2	127.0	85	354.4	150.4	45	409.6	173.9	05	464.9	197.4	65	520.1	220.8
26	300.1	127.4	86	355.3	150.8	46	410.5	174.3	06	465.8	197.8	66	521.0	221.2
27	301.0	127.8	87	356.2	151.2	47	411.5	174.7	07	466.7	198.1	67	521.9	221.6
28	301.9	128.2	88	357.2	151.6	48	412.4	175.1	08	467.6	198.5	68	522.8	222.0
29	302.8	128.6	89	358.1	152.0	49	413.3	175.4	09	468.5	198.8	69	523.8	222.3
30	303.8	128.9	90	359.0	152.4	50	414.2	175.8	10	469.5	199.3	70	524.7	222.7
331	304.7	129.3	391	359.9	152.8	451	415.2	176.2	511	470.4	199.7	571	525.6	223.1
32	305.6	129.7	92	360.8	153.2	52	416.1	176.6	12	471.3	200.0	72	526.5	223.4
33	306.5	130.1	93	361.8	153.6	53	417.0	177.0	13	472.2	200.4	73	527.4	223.8
34	307.5	130.5	94	362.7	154.0	54	417.9	177.4	14	473.1	200.8	74	528.4	224.2
35	308.4	130.9	95	363.6	154.3	55	418.8	177.8	15	474.0	201.2	75	529.3	224.6
36	309.3	131.3	96	364.5	154.7	56	419.8	178.2	16	475.0	201.6	76	530.2	225.0
37	310.2	131.7	97	365.4	155.1	57	420.7	178.6	17	475.9	202.0	77	531.1	225.4
38	311.1	132.1	98	366.4	155.5	58	421.6	179.0	18	476.8	202.4	78	532.0	225.8
39	312.1	132.5	99	367.3	155.9	59	422.5	179.4	19	477.7	202.8	79	533.0	226.2
40	313.0	132.9	400	368.2	156.3	60	423.4	179.7	20	478.6	203.2	80	533.9	226.6
341	313.9	133.2	401	369.1	156.7	461	424.4	180.1	521	479.6	203.6	581	534.8	227.0
42	314.8	133.6	02	370.0	157.1	62	425.3	180.5	22	480.5	204.0	82	535.7	227.4
43	315.7	134.0	03	371.0	157.5	63	426.2	180.9	23	481.4	204.4	83	536.6	227.8
44	316.7	134.4	04	371.9	157.9	64	427.1	181.3	24	482.3	204.8	84	537.6	228.2
45	317.6	134.8	05	372.8	158.3	65	428.0	181.7	25	483.2	205.2	85	538.5	228.6
46	318.5	135.2	06	373.7	158.6	66	429.0	182.1	26	484.2	205.5	86	539.4	229.0
47	319.4	135.6	07	374.6	159.0	67	429.9	182.5	27	485.1	205.9	87	540.3	229.4
48	320.3	136.0	08	375.6	159.4	68	430.8	182.9	28	486.0	206.3	88	541.2	229.8
49	321.3	136.4	09	376.5	159.8	69	431.7	183.3	29	486.9	206.7	89	542.2	230.2
50	322.2	136.8	10	377.4	160.2	70	432.6	183.7	30	487.8	207.1	90	543.1	230.6
351	323.1	137.2	411	378.3	160.6	471	433.6	184.0	531	488.8	207.4	591	544.0	231.0
52	324.0	137.5	12	379.3	161.0	72	434.5	184.4	32	489.7	207.8	92	544.9	231.3
53	324.9	137.9	13	380.2	161.4	73	435.4	184.8	33	490.6	208.2	93	545.8	231.7
54	325.9	138.3	14	381.1	161.8	74	436.3	185.2	34	491.5	208.6	94	546.8	232.0
55	326.8	138.7	15	382.0	162.2	75	437.2	185.6	35	492.5	209.0	95	547.7	232.4
56	327.7	139.1	16	382.9	162.5	76	438.2	186.0	36	493.4	209.4	96	548.6	232.8
57	328.6	139.5	17	383.9	162.9	77	439.1	186.4	37	494.3	209.8	97	549.5	233.2
58	329.5	139.9	18	384.8	163.3	78	440.0	186.8	38	495.2	210.2	98	550.4	233.6
59	330.5	140.3	19	385.7	163.7	79	440.9	187.2	39	496.1	210.6	99	551.3	234.0
60	331.4	140.7	20	386.6	164.1	80	441.8	187.6	40	497.1	211.0	600	552.3	234.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

67°(113°, 247°, 293°).

TABLE 2.

Difference of Latitude and Departure for 24° (156°, 204°, 336°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.4	61	55.7	24.8	121	110.5	49.2	181	165.4	73.6	241	220.2	98.0
2	1.8	0.8	62	56.6	25.2	22	111.5	49.6	82	166.3	74.0	42	221.1	98.4
3	2.7	1.2	63	57.6	25.6	23	112.4	50.0	83	167.2	74.4	43	222.0	98.8
4	3.7	1.6	64	58.5	26.0	24	113.3	50.4	84	168.1	74.8	44	222.9	99.2
5	4.6	2.0	65	59.4	26.4	25	114.2	50.8	85	169.0	75.2	45	223.8	99.7
6	5.5	2.4	66	60.3	26.8	26	115.1	51.2	86	169.9	75.7	46	224.7	100.1
7	6.4	2.8	67	61.2	27.3	27	116.0	51.7	87	170.8	76.1	47	225.6	100.5
8	7.3	3.3	68	62.1	27.7	28	116.9	52.1	88	171.7	76.5	48	226.6	100.9
9	8.2	3.7	69	63.0	28.1	29	117.8	52.5	89	172.7	76.9	49	227.5	101.3
10	9.1	4.1	70	63.9	28.5	30	118.8	52.9	90	173.6	77.3	50	228.4	101.7
11	10.0	4.5	71	64.9	28.9	131	119.7	53.3	191	174.5	77.7	251	229.3	102.1
12	11.0	4.9	72	65.8	29.3	32	120.6	53.7	92	175.4	78.1	52	230.2	102.5
13	11.9	5.3	73	66.7	29.7	33	121.5	54.1	93	176.3	78.5	53	231.1	102.9
14	12.8	5.7	74	67.6	30.1	34	122.4	54.5	94	177.2	78.9	54	232.0	103.3
15	13.7	6.1	75	68.5	30.5	35	123.3	54.9	95	178.1	79.3	55	233.0	103.7
16	14.6	6.5	76	69.4	30.9	36	124.2	55.3	96	179.1	79.7	56	233.9	104.1
17	15.5	6.9	77	70.3	31.3	37	125.2	55.7	97	180.0	80.1	57	234.8	104.5
18	16.4	7.3	78	71.3	31.7	38	126.1	56.1	98	180.9	80.5	58	235.7	104.9
19	17.4	7.7	79	72.2	32.1	39	127.0	56.5	99	181.8	80.9	59	236.6	105.3
20	18.3	8.1	80	73.1	32.5	40	127.9	56.9	200	182.7	81.3	60	237.5	105.8
21	19.2	8.5	81	74.0	32.9	141	128.8	57.3	201	183.6	81.8	261	238.4	106.2
22	20.1	8.9	82	74.9	33.4	42	129.7	57.8	02	184.5	82.2	62	239.3	106.6
23	21.0	9.4	83	75.8	33.8	43	130.6	58.2	03	185.4	82.6	63	240.3	107.0
24	21.9	9.8	84	76.7	34.2	44	131.6	58.6	04	186.4	83.0	64	241.2	107.4
25	22.8	10.2	85	77.7	34.6	45	132.5	59.0	05	187.3	83.4	65	242.1	107.8
26	23.8	10.6	86	78.6	35.0	46	133.4	59.4	06	188.2	83.8	66	243.0	108.2
27	24.7	11.0	87	79.5	35.4	47	134.3	59.8	07	189.1	84.2	67	243.9	108.6
28	25.6	11.4	88	80.4	35.8	48	135.2	60.2	08	190.0	84.6	68	244.8	109.0
29	26.5	11.8	89	81.3	36.2	49	136.1	60.6	09	190.9	85.0	69	245.7	109.4
30	27.4	12.2	90	82.2	36.6	50	137.0	61.0	10	191.8	85.4	70	246.7	109.8
31	28.3	12.6	91	83.1	37.0	151	137.9	61.4	211	192.8	85.8	271	247.6	110.2
32	29.2	13.0	92	84.0	37.4	52	138.9	61.8	12	193.7	86.2	72	248.5	110.6
33	30.1	13.4	93	85.0	37.8	53	139.8	62.2	13	194.6	86.6	73	249.4	111.0
34	31.1	13.8	94	85.9	38.2	54	140.7	62.6	14	195.5	87.0	74	250.3	111.4
35	32.0	14.2	95	86.8	38.6	55	141.6	63.0	15	196.4	87.4	75	251.2	111.9
36	32.9	14.6	96	87.7	39.0	56	142.5	63.5	16	197.3	87.9	76	252.1	112.3
37	33.8	15.0	97	88.6	39.5	57	143.4	63.9	17	198.2	88.3	77	253.1	112.7
38	34.7	15.5	98	89.5	39.9	58	144.3	64.3	18	199.2	88.7	78	254.0	113.1
39	35.6	15.9	99	90.4	40.3	59	145.3	64.7	19	200.1	89.1	79	254.9	113.5
40	36.5	16.3	100	91.4	40.7	60	146.2	65.1	20	201.0	89.5	80	255.8	113.9
41	37.5	16.7	101	92.3	41.1	161	147.1	65.5	221	201.9	89.9	281	256.7	114.3
42	38.4	17.1	02	93.2	41.5	62	148.0	65.9	22	202.8	90.3	82	257.6	114.7
43	39.3	17.5	03	94.1	41.9	63	148.9	66.3	23	203.7	90.7	83	258.5	115.1
44	40.2	17.9	04	95.0	42.3	64	149.8	66.7	24	204.6	91.1	84	259.4	115.5
45	41.1	18.3	05	95.9	42.7	65	150.7	67.1	25	205.5	91.5	85	260.4	115.9
46	42.0	18.7	06	96.8	43.1	66	151.6	67.5	26	206.5	91.9	86	261.3	116.3
47	42.9	19.1	07	97.7	43.5	67	152.6	67.9	27	207.4	92.3	87	262.2	116.7
48	43.9	19.5	08	98.7	43.9	68	153.5	68.3	28	208.3	92.7	88	263.1	117.1
49	44.8	19.9	09	99.6	44.3	69	154.4	68.7	29	209.2	93.1	89	264.0	117.5
50	45.7	20.3	10	100.5	44.7	70	155.3	69.1	30	210.1	93.5	90	264.9	118.0
51	46.6	20.7	111	101.4	45.1	171	156.2	69.6	231	211.0	94.0	291	265.8	118.4
52	47.5	21.2	12	102.3	45.6	72	157.1	70.0	32	211.9	94.4	92	266.8	118.8
53	48.4	21.6	13	103.2	46.0	73	158.0	70.4	33	212.9	94.8	93	267.7	119.2
54	49.3	22.0	14	104.1	46.4	74	159.0	70.8	34	213.8	95.2	94	268.6	119.6
55	50.2	22.4	15	105.1	46.8	75	159.9	71.2	35	214.7	95.6	95	269.5	120.0
56	51.2	22.8	16	106.0	47.2	76	160.8	71.6	36	215.6	96.0	96	270.4	120.4
57	52.1	23.2	17	106.9	47.6	77	161.7	72.0	37	216.5	96.4	97	271.3	120.8
58	53.0	23.6	18	107.8	48.0	78	162.6	72.4	38	217.4	96.8	98	272.2	121.2
59	53.9	24.0	19	108.7	48.4	79	163.5	72.8	38	218.3	97.2	99	273.2	121.6
60	54.8	24.4	20	109.6	48.8	80	164.4	73.2	40	219.3	97.6	300	274.1	122.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

66° (114°, 246°, 294°).

TABLE 2.

Difference of Latitude and Departure for 24° (156°, 204°, 336°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	275.0	122.4	361	329.8	146.8	421	384.6	171.2	481	439.4	195.6	541	494.2	220.0
02	275.9	122.8	62	330.7	147.2	22	385.5	171.6	82	440.3	196.0	42	495.1	220.4
03	276.8	123.2	63	331.6	147.6	23	386.4	172.1	83	441.2	196.5	43	496.0	220.9
04	277.7	123.7	64	332.5	148.1	24	387.3	172.5	84	442.1	196.9	44	496.9	221.3
05	278.6	124.1	65	333.4	148.5	25	388.2	172.9	85	443.0	197.3	45	497.8	221.7
06	279.5	124.5	66	334.3	148.9	26	389.2	173.3	86	444.0	197.7	46	498.8	222.1
07	280.4	124.9	67	335.3	149.3	27	390.1	173.7	87	444.9	198.1	47	499.7	222.5
08	281.4	125.3	68	336.2	149.7	28	391.0	174.1	88	445.8	198.5	48	500.6	222.9
09	282.3	125.7	69	337.1	150.1	29	391.9	174.5	89	446.7	198.9	49	501.5	223.3
10	283.2	126.1	70	338.0	150.5	30	392.8	174.9	90	447.6	199.3	50	502.4	223.7
311	284.1	126.5	371	338.9	150.9	431	393.7	175.3	491	448.6	199.7	551	503.4	224.1
12	285.0	126.9	72	339.8	151.3	32	394.6	175.7	92	449.5	200.1	52	504.3	224.5
13	285.9	127.3	73	340.7	151.7	33	395.6	176.1	93	450.4	200.5	53	505.2	224.9
14	286.8	127.7	74	341.7	152.1	34	396.5	176.5	94	451.3	200.9	54	506.1	225.3
15	287.8	128.1	75	342.6	152.5	35	397.4	176.9	95	452.2	201.3	55	507.0	225.7
16	288.7	128.5	76	343.5	152.9	36	398.3	177.3	96	453.1	201.7	56	507.9	226.1
17	289.6	128.9	77	344.4	153.3	37	399.2	177.7	97	454.0	202.2	57	508.8	226.6
18	290.5	129.3	78	345.3	153.7	38	400.1	178.2	98	454.9	202.6	58	509.7	227.0
19	291.4	129.8	79	346.2	154.2	39	401.0	178.6	99	455.8	203.0	59	510.6	227.4
20	292.3	130.2	80	347.1	154.6	40	402.0	179.0	500	456.8	203.4	60	511.6	227.8
321	293.2	130.6	381	348.1	155.0	441	402.9	179.4	501	457.7	203.8	561	512.5	228.2
22	294.2	131.0	82	349.0	155.4	42	403.8	179.8	02	458.6	204.2	62	513.4	228.6
23	295.1	131.4	83	349.9	155.8	43	404.7	180.2	03	459.5	204.6	63	514.3	229.0
24	296.0	131.8	84	350.8	156.2	44	405.6	180.6	04	460.4	205.0	64	515.2	229.4
25	296.9	132.2	85	351.7	156.6	45	406.5	181.0	05	461.3	205.4	65	516.1	229.8
26	297.8	132.6	86	352.6	157.0	46	407.4	181.4	06	462.2	205.8	66	517.0	230.2
27	298.7	133.0	87	353.5	157.4	47	408.3	181.8	07	463.2	206.2	67	518.0	230.6
28	299.6	133.4	88	354.4	157.8	48	409.3	182.2	08	464.1	206.6	68	518.9	231.0
29	300.5	133.8	89	355.4	158.2	49	410.2	182.6	09	465.0	207.0	69	519.8	231.4
30	301.5	134.2	90	356.3	158.6	50	411.1	183.0	10	465.9	207.4	70	520.7	231.8
331	302.4	134.6	391	357.2	159.0	451	412.0	183.4	511	466.8	207.8	571	521.6	232.2
32	303.3	135.0	92	358.1	159.4	52	412.9	183.8	12	467.7	208.2	72	522.5	232.7
33	304.2	135.4	93	359.0	159.8	53	413.8	184.3	13	468.6	208.7	73	523.4	233.1
34	305.1	135.9	94	359.9	160.3	54	414.7	184.7	14	469.5	209.1	74	524.3	233.5
35	306.0	136.3	95	360.8	160.7	55	415.7	185.1	15	470.5	209.5	75	525.3	233.9
36	306.9	136.7	96	361.8	161.1	56	416.6	185.5	16	471.4	209.9	76	526.2	234.3
37	307.9	137.1	97	362.7	161.5	57	417.5	185.9	17	472.3	210.3	77	527.1	234.7
38	308.8	137.5	98	363.6	161.9	58	418.4	186.3	18	473.2	210.7	78	528.0	235.1
39	309.7	137.9	99	364.5	162.3	59	419.3	186.7	19	474.1	211.1	79	528.9	235.5
40	310.6	138.3	400	365.4	162.7	60	420.2	187.1	20	475.0	211.5	80	529.8	235.9
341	311.5	138.7	401	366.3	163.1	461	421.1	187.5	521	475.9	211.9	581	530.8	236.3
42	312.4	139.1	02	367.2	163.5	62	422.0	187.9	22	476.8	212.3	82	531.7	236.7
43	313.3	139.5	03	368.2	163.9	63	423.0	188.3	23	477.8	212.7	83	532.6	237.1
44	314.3	139.9	04	369.1	164.3	64	423.9	188.7	24	478.7	213.1	84	533.5	237.5
45	315.2	140.3	05	370.0	164.7	65	424.8	189.1	25	479.6	213.5	85	534.4	237.9
46	316.1	140.7	06	370.9	165.1	66	425.7	189.5	26	480.5	213.9	86	535.3	238.3
47	317.0	141.1	07	371.8	165.5	67	426.6	189.9	27	481.4	214.4	87	536.2	238.8
48	317.9	141.5	08	372.7	165.9	68	427.5	190.4	28	482.3	214.8	88	537.1	239.2
49	318.8	142.0	09	373.6	166.4	69	428.4	190.8	29	483.2	215.2	89	538.0	239.6
50	319.7	142.4	10	374.5	166.8	70	429.4	191.2	30	484.2	215.6	90	539.0	240.0
351	320.6	142.8	411	375.5	167.2	471	430.3	191.6	531	485.1	216.0	591	539.9	240.4
52	321.6	143.2	12	376.4	167.6	72	431.2	192.0	32	486.0	216.4	92	540.8	240.8
53	322.5	143.6	13	377.3	168.0	73	432.1	192.4	33	486.9	216.8	93	541.7	241.2
54	323.4	144.0	14	378.2	168.4	74	433.0	192.8	34	487.8	217.2	94	542.6	241.6
55	324.3	144.4	15	379.1	168.8	75	433.9	193.2	35	488.7	217.6	95	543.5	242.0
56	325.2	144.8	16	380.0	169.2	76	434.8	193.6	36	489.6	218.0	96	544.4	242.4
57	326.1	145.2	17	380.9	169.6	77	435.8	194.0	37	490.6	218.4	97	545.4	242.8
58	327.0	145.6	18	381.9	170.0	78	436.7	194.4	38	491.5	218.8	98	546.3	243.2
59	328.0	146.0	19	382.8	170.4	79	437.6	194.8	39	492.4	219.2	99	547.2	243.6
60	328.9	146.4	20	383.7	170.8	80	438.5	195.2	40	493.3	219.6	600	548.1	244.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

66° (114°, 246°, 294°).

TABLE 2.

Difference of Latitude and Departure for 25° (155°, 205°, 335°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.4	61	55.3	25.8	121	109.7	51.1	181	164.0	76.5	241	218.4	101.9
2	1.8	0.8	62	56.2	26.2	22	110.6	51.6	82	164.9	76.9	42	219.3	102.3
3	2.7	1.3	63	57.1	26.6	23	111.5	52.0	83	165.9	77.3	43	220.2	102.7
4	3.6	1.7	64	58.0	27.0	24	112.4	52.4	84	166.8	77.8	44	221.1	103.1
5	4.5	2.1	65	58.9	27.5	25	113.3	52.8	85	167.7	78.2	45	222.0	103.5
6	5.4	2.5	66	59.8	27.9	26	114.2	53.2	86	168.6	78.6	46	223.0	104.0
7	6.3	3.0	67	60.7	28.3	27	115.1	53.7	87	169.5	79.0	47	223.9	104.4
8	7.3	3.4	68	61.6	28.7	28	116.0	54.1	88	170.4	79.5	48	224.8	104.8
9	8.2	3.8	69	62.5	29.2	29	116.9	54.5	89	171.3	79.9	49	225.7	105.2
10	9.1	4.2	70	63.4	29.6	30	117.8	54.9	90	172.2	80.3	50	226.6	105.7
11	10.0	4.6	71	64.3	30.0	131	118.7	55.4	191	173.1	80.7	251	227.5	106.1
12	10.9	5.1	72	65.3	30.4	32	119.6	55.8	92	174.0	81.1	52	228.4	106.5
13	11.8	5.5	73	66.2	30.9	33	120.5	56.2	93	174.9	81.6	53	229.3	106.9
14	12.7	5.9	74	67.1	31.3	34	121.4	56.6	94	175.8	82.0	54	230.2	107.3
15	13.6	6.3	75	68.0	31.7	35	122.4	57.1	95	176.7	82.4	55	231.1	107.8
16	14.5	6.8	76	68.9	32.1	36	123.3	57.5	96	177.6	82.8	56	232.0	108.2
17	15.4	7.2	77	69.8	32.5	37	124.2	57.9	97	178.5	83.3	57	232.9	108.6
18	16.3	7.6	78	70.7	33.0	38	125.1	58.3	98	179.4	83.7	58	233.8	109.0
19	17.2	8.0	79	71.6	33.4	39	126.0	58.7	99	180.4	84.1	59	234.7	109.5
20	18.1	8.5	80	72.5	33.8	40	126.9	59.2	200	181.3	84.5	60	235.6	109.9
21	19.0	8.9	81	73.4	34.2	141	127.8	59.6	201	182.2	84.9	261	236.5	110.3
22	19.9	9.3	82	74.3	34.7	42	128.7	60.0	02	183.1	85.4	62	237.5	110.7
23	20.8	9.7	83	75.2	35.1	43	129.6	60.4	03	184.0	85.8	63	238.4	111.1
24	21.8	10.1	84	76.1	35.5	44	130.5	60.9	04	184.9	86.2	64	239.3	111.6
25	22.7	10.6	85	77.0	35.9	45	131.4	61.3	05	185.8	86.6	65	240.2	112.0
26	23.6	11.0	86	77.9	36.3	46	132.3	61.7	06	186.7	87.1	66	241.1	112.4
27	24.5	11.4	87	78.8	36.8	47	133.2	62.1	07	187.6	87.5	67	242.0	112.8
28	25.4	11.8	88	79.8	37.2	48	134.1	62.5	08	188.5	87.9	68	242.9	113.3
29	26.3	12.3	89	80.7	37.6	49	135.0	63.0	09	189.4	88.3	69	243.8	113.7
30	27.2	12.7	90	81.6	38.0	50	135.9	63.4	10	190.3	88.7	70	244.7	114.1
31	28.1	13.1	91	82.5	38.5	151	136.9	63.8	211	191.2	89.2	271	245.6	114.5
32	29.0	13.5	92	83.4	38.9	52	137.8	64.2	12	192.1	89.6	72	246.5	115.0
33	29.9	13.9	93	84.3	39.3	53	138.7	64.7	13	193.0	90.0	73	247.4	115.4
34	30.8	14.4	94	85.2	39.7	54	139.6	65.1	14	193.9	90.4	74	248.3	115.8
35	31.7	14.8	95	86.1	40.1	55	140.5	65.5	15	194.9	90.9	75	249.2	116.2
36	32.6	15.2	96	87.0	40.6	56	141.4	65.9	16	195.8	91.3	76	250.1	116.6
37	33.5	15.6	97	87.9	41.0	57	142.3	66.4	17	196.7	91.7	77	251.0	117.1
38	34.4	16.1	98	88.8	41.4	58	143.2	66.8	18	197.6	92.1	78	252.0	117.5
39	35.3	16.5	99	89.7	41.8	59	144.1	67.2	19	198.5	92.6	79	252.9	117.9
40	36.3	16.9	100	90.6	42.3	60	145.0	67.6	20	199.4	93.0	80	253.8	118.3
41	37.2	17.3	101	91.5	42.7	161	145.9	68.0	221	200.3	93.4	281	254.7	118.8
42	38.1	17.7	02	92.4	43.1	62	146.8	68.5	22	201.2	93.8	82	255.6	119.2
43	39.0	18.2	03	93.3	43.5	63	147.7	68.9	23	202.1	94.2	83	256.5	119.6
44	39.9	18.6	04	94.3	44.0	64	148.6	69.3	24	203.0	94.7	84	257.4	120.0
45	40.8	19.0	05	95.2	44.4	65	149.5	69.7	25	203.9	95.1	85	258.3	120.4
46	41.7	19.4	06	96.1	44.8	66	150.4	70.2	26	204.8	95.5	86	259.2	120.9
47	42.6	19.9	07	97.0	45.2	67	151.4	70.6	27	205.7	95.9	87	260.1	121.3
48	43.5	20.3	08	97.9	45.6	68	152.3	71.0	28	206.6	96.4	88	261.0	121.7
49	44.4	20.7	09	98.8	46.1	69	153.2	71.4	29	207.5	96.8	89	261.9	122.1
50	45.3	21.1	10	99.7	46.5	70	154.1	71.8	30	208.5	97.2	90	262.8	122.6
51	46.2	21.6	111	100.6	46.9	171	155.0	72.3	231	209.4	97.6	291	263.7	123.0
52	47.1	22.0	12	101.5	47.3	72	155.9	72.7	32	210.3	98.0	92	264.6	123.4
53	48.0	22.4	13	102.4	47.8	73	156.8	73.1	33	211.2	98.5	93	265.5	123.8
54	48.9	22.8	14	103.3	48.2	74	157.7	73.5	34	212.1	98.9	94	266.5	124.2
55	49.8	23.2	15	104.2	48.6	75	158.6	74.0	35	213.0	99.3	95	267.4	124.7
56	50.8	23.7	16	105.1	49.0	76	159.5	74.4	36	213.9	99.7	96	268.3	125.1
57	51.7	24.1	17	106.0	49.4	77	160.4	74.8	37	214.8	100.2	97	269.2	125.5
58	52.6	24.5	18	106.9	49.9	78	161.3	75.2	38	215.7	100.6	98	270.1	125.9
59	53.5	24.9	19	107.9	50.3	79	162.2	75.6	39	216.6	101.0	99	271.0	126.4
60	54.4	25.4	20	108.8	50.7	80	163.1	76.1	40	217.5	101.4	300	271.9	126.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

65° (115°, 245°, 295°).

TABLE 2.

Difference of Latitude and Departure for 25° (155°, 205°, 335°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	272.8	127.2	361	327.1	152.5	421	381.5	177.9	481	435.9	203.3	541	490.3	228.6
02	273.7	127.6	62	328.0	153.0	22	382.4	178.3	82	436.8	203.7	42	491.2	229.0
03	274.6	128.0	63	329.0	153.4	23	383.3	178.7	83	437.7	204.1	43	492.1	229.4
04	275.5	128.4	64	329.9	153.8	24	384.2	179.2	84	438.6	204.5	44	493.0	229.9
05	276.4	128.9	65	330.8	154.2	25	385.1	179.6	85	439.5	204.9	45	493.9	230.3
06	277.3	129.3	66	331.7	154.6	26	386.0	180.0	86	440.4	205.4	46	494.8	230.7
07	278.2	129.7	67	332.6	155.1	27	387.0	180.4	87	441.3	205.8	47	495.7	231.1
08	279.1	130.1	68	333.5	155.5	28	387.9	180.9	88	442.2	206.2	48	496.6	231.6
09	280.0	130.6	69	334.4	155.9	29	388.8	181.3	89	443.1	206.6	49	497.5	232.0
10	280.9	131.0	70	335.3	156.3	30	389.7	181.7	90	444.0	207.1	50	498.4	232.4
311	281.8	131.4	371	336.2	156.8	431	390.6	182.1	491	444.9	207.5	551	499.3	232.8
12	282.7	131.8	72	337.1	157.2	32	391.5	182.5	92	445.9	207.9	52	500.2	233.2
13	283.6	132.2	73	338.0	157.6	33	392.4	183.0	93	446.8	208.3	53	501.1	233.7
14	284.5	132.7	74	338.9	158.0	34	393.3	183.4	94	447.7	208.7	54	502.0	234.1
15	285.4	133.1	75	339.8	158.5	35	394.2	183.8	95	448.6	209.1	55	503.0	234.5
16	286.4	133.5	76	340.7	158.9	36	395.1	184.2	96	449.5	209.6	56	503.9	235.0
17	287.3	133.9	77	341.6	159.3	37	396.0	184.7	97	450.4	210.0	57	504.8	235.4
18	288.2	134.4	78	342.5	159.7	38	396.9	185.1	98	451.3	210.4	58	505.7	235.8
19	289.1	134.8	79	343.5	160.1	39	397.8	185.5	99	452.2	210.9	59	506.6	236.2
20	290.0	135.2	80	344.4	160.6	40	398.7	185.9	500	453.1	211.3	60	507.5	236.6
321	290.9	135.6	381	345.3	161.0	441	399.6	186.3	501	454.0	211.7	561	508.4	237.1
22	291.8	136.1	82	346.2	161.4	42	400.6	186.8	02	454.9	212.1	62	509.3	237.5
23	292.7	136.5	83	347.1	161.8	43	401.5	187.2	03	455.8	212.5	63	510.2	237.9
24	293.6	136.9	84	348.0	162.3	44	402.4	187.6	04	456.7	213.0	64	511.1	238.3
25	294.5	137.3	85	348.9	162.7	45	403.3	188.0	05	457.7	213.4	65	512.0	238.7
26	295.4	137.7	86	349.8	163.1	46	404.2	188.5	06	458.6	213.8	66	512.9	239.2
27	296.3	138.2	87	350.7	163.5	47	405.1	188.9	07	459.5	214.2	67	513.8	239.6
28	297.2	138.6	88	351.6	163.9	48	406.0	189.3	08	460.4	214.7	68	514.8	240.1
29	298.1	139.0	89	352.5	164.4	49	406.9	189.7	09	461.3	215.1	69	515.7	240.5
30	299.0	139.4	90	353.4	164.8	50	407.8	190.1	10	462.2	215.5	70	516.6	240.9
331	300.0	139.9	391	354.3	165.2	451	408.7	190.6	511	463.1	215.9	571	517.5	241.3
32	300.9	140.3	92	355.2	165.6	52	409.6	191.0	12	464.0	216.4	72	518.4	241.7
33	301.8	140.7	93	356.1	166.1	53	410.5	191.4	13	464.9	216.8	73	519.3	242.1
34	302.7	141.1	94	357.0	166.5	54	411.4	191.8	14	465.8	217.2	74	520.2	242.6
35	303.6	141.5	95	358.0	166.9	55	412.3	192.3	15	466.7	217.7	75	521.1	243.0
36	304.5	142.0	96	358.9	167.3	56	413.2	192.7	16	467.6	218.1	76	522.0	243.4
37	305.4	142.4	97	359.8	167.7	57	414.1	193.1	17	468.5	218.5	77	522.9	243.8
38	306.3	142.8	98	360.7	168.2	58	415.1	193.5	18	469.4	218.9	78	523.8	244.3
39	307.2	143.2	99	361.6	168.6	59	416.0	194.0	19	470.3	219.3	79	524.7	244.7
40	308.1	143.7	400	362.5	169.0	60	416.9	194.4	20	471.2	219.8	80	525.6	245.1
341	309.0	144.1	401	363.4	169.4	461	417.8	194.8	521	472.2	220.2	581	526.5	245.5
42	309.9	144.5	02	364.3	169.9	62	418.7	195.2	22	473.1	220.6	82	527.4	246.0
43	310.8	144.9	03	365.2	170.3	63	419.6	195.6	23	474.0	221.0	83	528.3	246.4
44	311.7	145.4	04	366.1	170.7	64	420.5	196.1	24	474.9	221.4	84	529.3	246.8
45	312.6	145.8	05	367.0	171.1	65	421.4	196.5	25	475.8	221.9	85	530.2	247.2
46	313.5	146.2	06	367.9	171.6	66	422.3	196.9	26	476.7	222.3	86	531.1	247.7
47	314.5	146.6	07	368.8	172.0	67	423.2	197.3	27	477.6	222.7	87	532.0	248.1
48	315.4	147.0	08	369.7	172.4	68	424.1	197.8	28	478.5	223.2	88	532.9	248.5
49	316.3	147.5	09	370.6	172.8	69	425.0	198.2	29	479.4	223.6	89	533.8	248.9
50	317.2	147.9	10	371.5	173.2	70	425.9	198.6	30	480.3	224.0	90	534.7	249.4
351	318.1	148.3	411	372.5	173.7	471	426.8	199.0	531	481.2	224.4	591	535.6	249.8
52	319.0	148.7	12	373.4	174.1	72	427.7	199.4	32	482.1	224.8	92	536.5	250.2
53	319.9	149.2	13	374.3	174.5	73	428.6	199.9	33	483.0	225.3	93	537.4	250.6
54	320.8	149.6	14	375.2	174.9	74	429.6	200.3	34	483.9	225.7	94	538.3	251.1
55	321.7	150.0	15	376.1	175.4	75	430.5	200.7	35	484.8	226.1	95	539.2	251.5
56	322.6	150.4	16	377.0	175.8	76	431.4	201.1	36	485.7	226.5	96	540.1	251.9
57	323.5	150.8	17	377.9	176.2	77	432.3	201.6	37	486.7	226.9	97	541.0	252.3
58	324.4	151.3	18	378.8	176.6	78	433.2	202.0	38	487.6	227.4	98	541.9	252.7
59	325.3	151.7	19	379.7	177.0	79	434.1	202.4	39	488.5	227.8	99	542.8	253.1
60	326.2	152.1	20	380.6	177.5	80	435.0	202.8	40	489.4	228.2	600	543.8	253.6
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

65° (115°, 245°, 295°).

6583—06——27

TABLE 2.

Difference of Latitude and Departure for 26° (154°, 206°, 334°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.4	61	54.8	26.7	121	108.8	53.0	181	162.7	79.3	241	216.6	105.6
2	1.8	0.9	62	55.7	27.2	22	109.7	53.5	82	163.6	79.8	42	217.5	106.1
3	2.7	1.3	63	56.6	27.6	23	110.6	53.9	83	164.5	80.2	43	218.4	106.5
4	3.6	1.8	64	57.5	28.1	24	111.5	54.4	84	165.4	80.7	44	219.3	107.0
5	4.5	2.2	65	58.4	28.5	25	112.3	54.8	85	166.3	81.1	45	220.2	107.4
6	5.4	2.6	66	59.3	28.9	26	113.2	55.2	86	167.2	81.5	46	221.1	107.8
7	6.3	3.1	67	60.2	29.4	27	114.1	55.7	87	168.1	82.0	47	222.0	108.3
8	7.2	3.5	68	61.1	29.8	28	115.0	56.1	88	169.0	82.4	48	222.9	108.7
9	8.1	3.9	69	62.0	30.2	29	115.9	56.5	89	169.9	82.9	49	223.8	109.2
10	9.0	4.4	70	62.9	30.7	30	116.8	57.0	90	170.8	83.3	50	224.7	109.6
11	9.9	4.8	71	63.8	31.1	131	117.7	57.4	191	171.7	83.7	251	225.6	110.0
12	10.8	5.3	72	64.7	31.6	32	118.6	57.9	92	172.6	84.2	52	226.5	110.5
13	11.7	5.7	73	65.6	32.0	33	119.5	58.3	93	173.5	84.6	53	227.4	110.9
14	12.6	6.1	74	66.5	32.4	34	120.4	58.7	94	174.4	85.0	54	228.3	111.3
15	13.5	6.6	75	67.4	32.9	35	121.3	59.2	95	175.3	85.5	55	229.2	111.8
16	14.4	7.0	76	68.3	33.3	36	122.2	59.6	96	176.2	85.9	56	230.1	112.2
17	15.3	7.5	77	69.2	33.8	37	123.1	60.1	97	177.1	86.4	57	231.0	112.7
18	16.2	7.9	78	70.1	34.2	38	124.0	60.5	98	178.0	86.8	58	231.9	113.1
19	17.1	8.3	79	71.0	34.6	39	124.9	60.9	99	178.9	87.2	59	232.8	113.5
20	18.0	8.8	80	71.9	35.1	40	125.8	61.4	200	179.8	87.7	60	233.7	114.0
21	18.9	9.2	81	72.8	35.5	141	126.7	61.8	201	180.7	88.1	261	234.6	114.4
22	19.8	9.6	82	73.7	35.9	42	127.6	62.2	02	181.6	88.6	62	235.5	114.9
23	20.7	10.1	83	74.6	36.4	43	128.5	62.7	03	182.5	89.0	63	236.4	115.3
24	21.6	10.5	84	75.5	36.8	44	129.4	63.1	04	183.4	89.4	64	237.3	115.7
25	22.5	11.0	85	76.4	37.3	45	130.3	63.6	05	184.3	89.9	65	238.2	116.2
26	23.4	11.4	86	77.3	37.7	46	131.2	64.0	06	185.2	90.3	66	239.1	116.6
27	24.3	11.8	87	78.2	38.1	47	132.1	64.4	07	186.1	90.7	67	240.0	117.0
28	25.2	12.3	88	79.1	38.6	48	133.0	64.9	08	186.9	91.2	68	240.9	117.5
29	26.1	12.7	89	80.0	39.0	49	133.9	65.3	09	187.8	91.6	69	241.8	117.9
30	27.0	13.2	90	80.9	39.5	50	134.8	65.8	10	188.7	92.1	70	242.7	118.4
31	27.9	13.6	91	81.8	39.9	151	135.7	66.2	211	189.6	92.5	271	243.6	118.8
32	28.8	14.0	92	82.7	40.3	52	136.6	66.6	12	190.5	92.9	72	244.5	119.2
33	29.7	14.5	93	83.6	40.8	53	137.5	67.1	13	191.4	93.4	73	245.4	119.7
34	30.6	14.9	94	84.5	41.2	54	138.4	67.5	14	192.3	93.8	74	246.3	120.1
35	31.5	15.3	95	85.4	41.6	55	139.3	67.9	15	193.2	94.2	75	247.2	120.6
36	32.4	15.8	96	86.3	42.1	56	140.2	68.4	16	194.1	94.7	76	248.1	121.0
37	33.3	16.2	97	87.2	42.5	57	141.1	68.8	17	195.0	95.1	77	249.0	121.4
38	34.2	16.7	98	88.1	43.0	58	142.0	69.3	18	195.9	95.6	78	249.9	121.9
39	35.1	17.1	99	89.0	43.4	59	142.9	69.7	19	196.8	96.0	79	250.8	122.3
40	36.0	17.5	100	89.9	43.8	60	143.8	70.1	20	197.7	96.4	80	251.7	122.7
41	36.9	18.0	101	90.8	44.3	161	144.7	70.6	221	198.6	96.9	281	252.6	123.2
42	37.7	18.4	02	91.7	44.7	62	145.6	71.0	22	199.5	97.3	82	253.5	123.6
43	38.6	18.8	03	92.6	45.2	63	146.5	71.5	23	200.4	97.8	83	254.4	124.1
44	39.5	19.3	04	93.5	45.6	64	147.4	71.9	24	201.3	98.2	84	255.3	124.5
45	40.4	19.7	05	94.4	46.0	65	148.3	72.3	25	202.2	98.6	85	256.2	124.9
46	41.3	20.2	06	95.3	46.5	66	149.2	72.8	26	203.1	99.1	86	257.1	125.4
47	42.2	20.6	07	96.2	46.9	67	150.1	73.2	27	204.0	99.5	87	258.0	125.8
48	43.1	21.0	08	97.1	47.3	68	151.0	73.6	28	204.9	99.9	88	258.9	126.3
49	44.0	21.5	09	98.0	47.8	69	151.9	74.1	29	205.8	100.4	89	259.8	126.7
50	44.9	21.9	10	98.9	48.2	70	152.8	74.5	30	206.7	100.8	90	260.7	127.1
51	45.8	22.4	111	99.8	48.7	171	153.7	75.0	231	207.6	101.3	291	261.5	127.6
52	46.7	22.8	12	100.7	49.1	72	154.6	75.4	32	208.5	101.7	92	262.4	128.0
53	47.6	23.2	13	101.6	49.5	73	155.5	75.8	33	209.4	102.1	93	263.3	128.4
54	48.5	23.7	14	102.5	50.0	74	156.4	76.3	34	210.3	102.6	94	264.2	128.9
55	49.4	24.1	15	103.4	50.4	75	157.3	76.7	35	211.2	103.0	95	265.1	129.3
56	50.3	24.5	16	104.3	50.9	76	158.2	77.2	36	212.1	103.5	96	266.0	129.8
57	51.2	25.0	17	105.2	51.3	77	159.1	77.6	37	213.0	103.9	97	266.9	130.2
58	52.1	25.4	18	106.1	51.7	78	160.0	78.0	38	213.9	104.3	98	267.8	130.6
59	53.0	25.9	19	107.0	52.2	79	160.9	78.5	39	214.8	104.8	99	268.7	131.1
60	53.9	26.3	20	107.9	52.6	80	161.8	78.9	40	215.7	105.2	300	269.6	131.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

64° (116°, 244°, 296°).

Difference of Latitude and Departure for 26° (154°, 206°, 334).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	270.5	132.0	361	324.5	158.3	421	378.4	184.6	481	432.3	210.9	541	486.2	237.2
02	271.4	132.4	62	325.4	158.7	22	379.3	185.0	82	433.2	211.3	42	487.1	237.6
03	272.3	132.8	63	326.3	159.1	23	380.2	185.4	83	434.1	211.7	43	488.0	238.0
04	273.2	133.3	64	327.2	159.6	24	381.1	185.9	84	435.0	212.2	44	488.9	238.5
05	274.1	133.7	65	328.1	160.0	25	382.0	186.3	85	435.9	212.6	45	489.8	238.9
06	275.0	134.1	66	329.0	160.4	26	382.9	186.7	86	436.8	213.0	46	490.7	239.3
07	275.9	134.6	67	329.9	160.9	27	383.8	187.2	87	437.7	213.5	47	491.6	239.8
08	276.8	135.0	68	330.8	161.3	28	384.7	187.6	88	438.6	213.9	48	492.5	240.2
09	277.7	135.5	69	331.7	161.8	29	385.6	188.1	89	439.5	214.4	49	493.4	240.7
10	278.6	135.9	70	332.6	162.2	30	386.5	188.5	90	440.4	214.8	50	494.3	241.1
311	279.5	136.3	371	333.5	162.6	431	387.4	188.9	491	441.3	215.2	551	495.2	241.5
12	280.4	136.8	72	334.4	163.1	32	388.3	189.4	92	442.2	215.7	52	496.1	242.0
13	281.3	137.2	73	335.3	163.5	33	389.2	189.8	93	443.1	216.1	53	497.0	242.4
14	282.2	137.7	74	336.2	164.0	34	390.1	190.3	94	444.0	216.6	54	497.9	242.9
15	283.1	138.1	75	337.1	164.4	35	391.0	190.7	95	444.9	217.0	55	498.8	243.3
16	284.0	138.5	76	338.0	164.8	36	391.9	191.1	96	445.8	217.4	56	499.7	243.7
17	284.9	139.0	77	338.9	165.3	37	392.8	191.6	97	446.7	217.9	57	500.6	244.2
18	285.8	139.4	78	339.8	165.7	38	393.7	192.0	98	447.6	218.3	58	501.5	244.6
19	286.7	139.8	79	340.7	166.2	39	394.6	192.4	99	448.5	218.7	59	502.4	245.0
20	287.6	140.3	80	341.5	166.6	40	395.5	192.9	500	449.4	219.2	60	503.3	245.5
321	288.5	140.7	381	342.4	167.0	441	396.4	193.3	501	450.3	219.6	561	504.2	245.9
22	289.4	141.2	82	343.3	167.5	42	397.3	193.8	02	451.2	220.1	62	505.1	246.4
23	290.3	141.6	83	344.2	167.9	43	398.2	194.2	03	452.1	220.5	63	506.0	246.8
24	291.2	142.0	84	345.1	168.3	44	399.1	194.7	04	453.0	221.0	64	506.9	247.3
25	292.1	142.5	85	346.0	168.8	45	400.0	195.1	05	453.9	221.4	65	507.8	247.7
26	293.0	142.9	86	346.9	169.2	46	400.9	195.5	06	454.8	221.8	66	508.7	248.1
27	293.9	143.4	87	347.8	169.7	47	401.8	196.0	07	455.7	222.3	67	509.6	248.6
28	294.8	143.8	88	348.7	170.1	48	402.7	196.4	08	456.6	222.7	68	510.5	249.0
29	295.7	144.2	89	349.6	170.5	49	403.6	196.8	09	457.5	223.1	69	511.4	249.4
30	296.6	144.7	90	350.5	171.0	50	404.5	197.3	10	458.4	223.6	70	512.3	249.9
331	297.5	145.1	391	351.4	171.4	451	405.4	197.7	511	459.3	224.0	571	513.2	250.3
32	298.4	145.6	92	352.3	171.8	52	406.3	198.1	12	460.2	224.4	72	514.1	250.8
33	299.3	146.0	93	353.2	172.3	53	407.2	198.6	13	461.1	224.9	73	515.0	251.2
34	300.2	146.4	94	354.1	172.7	54	408.1	199.0	14	462.0	225.3	74	515.9	251.6
35	301.1	146.9	95	355.0	173.2	55	409.0	199.5	15	462.9	225.8	75	516.8	252.1
36	302.0	147.3	96	355.9	173.6	56	409.9	199.9	16	463.8	226.2	76	517.7	252.5
37	302.9	147.7	97	356.8	174.0	57	410.8	200.3	17	464.7	226.6	77	518.6	252.9
38	303.8	148.2	98	357.7	174.5	58	411.7	200.8	18	465.6	227.1	78	519.5	253.4
39	304.7	148.6	99	358.6	174.9	59	412.6	201.2	19	466.5	227.5	79	520.4	253.8
40	305.6	149.0	400	359.5	175.4	60	413.5	201.7	20	467.4	228.0	80	521.3	254.3
341	306.5	149.5	401	360.4	175.8	461	414.4	202.1	521	468.3	228.4	581	522.2	254.7
42	307.4	149.9	02	361.3	176.2	62	415.2	202.5	22	469.2	228.8	82	523.1	255.1
43	308.3	150.4	03	362.2	176.7	63	416.1	203.0	23	470.1	229.3	83	524.0	255.6
44	309.2	150.8	04	363.1	177.1	64	417.0	203.4	24	471.0	229.7	84	524.9	256.0
45	310.1	151.2	05	364.0	177.5	65	417.9	203.8	25	471.9	230.1	85	525.8	256.4
46	311.0	151.7	06	364.9	178.0	66	418.8	204.3	26	472.8	230.6	86	526.7	256.9
47	311.9	152.1	07	365.8	178.4	67	419.7	204.7	27	473.7	231.0	87	527.6	257.3
48	312.8	152.6	08	366.7	178.9	68	420.6	205.2	28	474.6	231.5	88	528.5	257.8
49	313.7	153.0	09	367.6	179.3	69	421.5	205.6	29	475.5	231.9	89	529.4	258.2
50	314.6	153.4	10	368.5	179.7	70	422.4	206.0	30	476.4	232.3	90	530.3	258.6
351	315.5	153.9	411	369.4	180.2	471	423.3	206.5	531	477.3	232.8	591	531.2	259.1
52	316.4	154.3	12	370.3	180.6	72	424.2	206.9	32	478.2	233.2	92	532.1	259.5
53	317.3	154.7	13	371.2	181.1	73	425.1	207.3	33	479.1	233.6	93	533.0	259.9
54	318.2	155.2	14	372.1	181.5	74	426.0	207.8	34	480.0	234.1	94	533.9	260.4
55	319.1	155.6	15	373.0	181.9	75	426.9	208.2	35	480.9	234.5	95	534.8	260.8
56	320.0	156.1	16	373.9	182.4	76	427.8	208.7	36	481.8	235.0	96	535.7	261.3
57	320.9	156.5	17	374.8	182.8	77	428.7	209.1	37	482.7	235.4	97	536.6	261.7
58	321.8	156.9	18	375.7	183.2	78	429.6	209.5	38	483.6	235.8	98	537.5	262.1
59	322.7	157.4	19	376.6	183.7	79	430.5	210.0	39	484.5	236.3	90	538.4	262.6
60	323.6	157.8	20	377.5	184.1	80	431.4	210.4	40	485.3	236.7	600	539.3	263.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

64° (116°, 244°, 296°).

TABLE 2.

Difference of Latitude and Departure for 27° (153°, 207°, 333°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.5	61	54.4	27.7	121	107.8	54.9	181	161.3	82.2	241	214.7	109.4
2	1.8	0.9	62	55.2	28.1	22	108.7	55.4	82	162.2	82.6	42	215.6	109.9
3	2.7	1.4	63	56.1	28.6	23	109.6	55.8	83	163.1	83.1	43	216.5	110.3
4	3.6	1.8	64	57.0	29.1	24	110.5	56.3	84	163.9	83.5	44	217.4	110.8
5	4.5	2.3	65	57.9	29.5	25	111.4	56.7	85	164.8	84.0	45	218.3	111.2
6	5.3	2.7	66	58.8	30.0	26	112.3	57.2	86	165.7	84.4	46	219.2	111.7
7	6.2	3.2	67	59.7	30.4	27	113.2	57.7	87	166.6	84.9	47	220.1	112.1
8	7.1	3.6	68	60.6	30.9	28	114.0	58.1	88	167.5	85.4	48	221.0	112.6
9	8.0	4.1	69	61.5	31.3	29	114.9	58.6	89	168.4	85.8	49	221.9	113.0
10	8.9	4.5	70	62.4	31.8	30	115.8	59.0	90	169.3	86.3	50	222.8	113.5
11	9.8	5.0	71	63.3	32.2	131	116.7	59.5	191	170.2	86.7	251	223.6	114.0
12	10.7	5.4	72	64.2	32.7	32	117.6	59.9	92	171.1	87.2	52	224.5	114.4
13	11.6	5.9	73	65.0	33.1	33	118.5	60.4	93	172.0	87.6	53	225.4	114.9
14	12.5	6.4	74	65.9	33.6	34	119.4	60.8	94	172.9	88.1	54	226.3	115.3
15	13.4	6.8	75	66.8	34.0	35	120.3	61.3	95	173.7	88.5	55	227.2	115.8
16	14.3	7.3	76	67.7	34.5	36	121.2	61.7	96	174.6	89.0	56	228.1	116.2
17	15.1	7.7	77	68.6	35.0	37	122.1	62.2	97	175.5	89.4	57	229.0	116.7
18	16.0	8.2	78	69.5	35.4	38	123.0	62.7	98	176.4	89.9	58	229.9	117.1
19	16.9	8.6	79	70.4	35.9	39	123.8	63.1	99	177.3	90.3	59	230.8	117.6
20	17.8	9.1	80	71.3	36.3	40	124.7	63.6	200	178.2	90.8	60	231.7	118.0
21	18.7	9.5	81	72.2	36.8	141	125.6	64.0	201	179.1	91.3	261	232.6	118.5
22	19.6	10.0	82	73.1	37.2	42	126.5	64.5	02	180.0	91.7	62	233.4	118.9
23	20.5	10.4	83	74.0	37.7	43	127.4	64.9	03	180.9	92.2	63	234.3	119.4
24	21.4	10.9	84	74.8	38.1	44	128.3	65.4	04	181.8	92.6	64	235.2	119.9
25	22.3	11.3	85	75.7	38.6	45	129.2	65.8	05	182.7	93.1	65	236.1	120.3
26	23.2	11.8	86	76.6	39.0	46	130.1	66.3	06	183.5	93.5	66	237.0	120.8
27	24.1	12.3	87	77.5	39.5	47	131.0	66.7	07	184.4	94.0	67	237.9	121.2
28	24.9	12.7	88	78.4	40.0	48	131.9	67.2	08	185.3	94.4	68	238.8	121.7
29	25.8	13.2	89	79.3	40.4	49	132.8	67.6	09	186.2	94.9	69	239.7	122.1
30	26.7	13.6	90	80.2	40.9	50	133.7	68.1	10	187.1	95.3	70	240.6	122.6
31	27.6	14.1	91	81.1	41.3	151	134.5	68.6	211	188.0	95.8	271	241.5	123.0
32	28.5	14.5	92	82.0	41.8	52	135.4	69.0	12	188.9	96.2	72	242.4	123.5
33	29.4	15.0	93	82.9	42.2	53	136.3	69.5	13	189.8	96.7	73	243.2	123.9
34	30.3	15.4	94	83.8	42.7	54	137.2	69.9	14	190.7	97.2	74	244.1	124.4
35	31.2	15.9	95	84.6	43.1	55	138.1	70.4	15	191.6	97.6	75	245.0	124.8
36	32.1	16.3	96	85.5	43.6	56	139.0	70.8	16	192.5	98.1	76	245.9	125.3
37	33.0	16.8	97	86.4	44.0	57	139.9	71.3	17	193.3	98.5	77	246.8	125.8
38	33.9	17.3	98	87.3	44.5	58	140.8	71.7	18	194.2	99.0	78	247.7	126.2
39	34.7	17.7	99	88.2	44.9	59	141.7	72.2	19	195.1	99.4	79	248.6	126.7
40	35.6	18.2	100	89.1	45.4	60	142.6	72.6	20	196.0	99.9	80	249.5	127.1
41	36.5	18.6	101	90.0	45.9	161	143.5	73.1	221	196.9	100.3	281	250.4	127.6
42	37.4	19.1	02	90.9	46.3	62	144.3	73.5	22	197.8	100.8	82	251.3	128.0
43	38.3	19.5	03	91.8	46.8	63	145.2	74.0	23	198.7	101.2	83	252.2	128.5
44	39.2	20.0	04	92.7	47.2	64	146.1	74.5	24	199.6	101.7	84	253.0	128.9
45	40.1	20.4	05	93.6	47.7	65	147.0	74.9	25	200.5	102.1	85	253.9	129.4
46	41.0	20.9	06	94.4	48.1	66	147.9	75.4	26	201.4	102.6	86	254.8	129.8
47	41.9	21.3	07	95.3	48.6	67	148.8	75.8	27	202.3	103.1	87	255.7	130.3
48	42.8	21.8	08	96.2	49.0	68	149.7	76.3	28	203.1	103.5	88	256.6	130.7
49	43.7	22.2	09	97.1	49.5	69	150.6	76.7	29	204.0	104.0	89	257.5	131.2
50	44.6	22.7	10	98.0	49.9	70	151.5	77.2	30	204.9	104.4	90	258.4	131.7
51	45.4	23.2	111	98.9	50.4	171	152.4	77.6	231	205.8	104.9	291	259.3	132.1
52	46.3	23.6	12	99.8	50.8	72	153.3	78.1	32	206.7	105.3	92	260.2	132.6
53	47.2	24.1	13	100.7	51.3	73	154.1	78.5	33	207.6	105.8	93	261.1	133.0
54	48.1	24.5	14	101.6	51.8	74	155.0	79.0	34	208.5	106.2	94	262.0	133.5
55	49.0	25.0	15	102.5	52.2	75	155.9	79.4	35	209.4	106.7	95	262.8	133.9
56	49.9	25.4	16	103.4	52.7	76	156.8	79.9	36	210.3	107.1	96	263.7	134.4
57	50.8	25.9	17	104.2	53.1	77	157.7	80.4	37	211.2	107.6	97	264.6	134.8
58	51.7	26.3	18	105.1	53.6	78	158.6	80.8	38	212.1	108.0	98	265.5	135.3
59	52.6	26.8	19	106.0	54.0	79	159.5	81.3	39	213.0	108.5	99	266.4	135.7
60	53.5	27.2	20	106.9	54.5	80	160.4	81.7	40	213.8	109.0	300	267.3	136.2
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

63° (117°, 243°, 297°).

TABLE 2.

Difference of Latitude and Departure for 27° (153°, 207°, 333°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	268.2	136.7	361	321.7	163.9	421	375.1	191.1	481	428.6	218.3	541	482.0	245.6
02	269.1	137.1	62	322.5	164.4	22	376.0	191.6	82	429.4	218.8	42	482.9	246.1
03	270.0	137.6	63	323.4	164.8	23	376.9	192.0	83	430.3	219.2	43	483.8	246.5
04	270.9	138.0	64	324.3	165.3	24	377.8	192.5	84	431.2	219.7	44	484.7	247.0
05	271.8	138.5	65	325.2	165.7	25	378.7	193.0	85	432.1	220.1	45	485.6	247.4
06	272.7	138.9	66	326.1	166.2	26	379.6	193.4	86	433.0	220.6	46	486.4	247.9
07	273.5	139.4	67	327.0	166.6	27	380.5	193.9	87	433.9	221.1	47	487.3	248.4
08	274.4	139.8	68	327.9	167.1	28	381.4	194.3	88	434.8	221.5	48	488.2	248.8
09	275.3	140.3	69	328.8	167.5	29	382.2	194.8	89	435.7	222.0	49	489.1	249.2
10	276.2	140.7	70	329.7	168.0	30	383.1	195.2	90	436.6	222.4	50	490.0	249.7
311	277.1	141.2	371	330.6	168.4	431	384.0	195.7	491	437.5	222.9	551	490.9	250.1
12	278.0	141.7	72	331.5	168.9	32	384.9	196.1	92	438.3	223.3	52	491.8	250.6
13	278.9	142.1	73	332.3	169.3	33	385.8	196.6	93	439.2	223.8	53	492.7	251.0
14	279.8	142.6	74	333.2	169.8	34	386.7	197.0	94	440.1	224.2	54	493.6	251.5
15	280.7	143.0	75	334.1	170.3	35	387.6	197.5	95	441.0	224.7	55	494.5	252.0
16	281.6	143.5	76	335.0	170.7	36	388.5	197.9	96	441.9	225.2	56	495.4	252.4
17	282.5	143.9	77	335.9	171.2	37	389.4	198.4	97	442.8	225.6	57	496.3	252.9
18	283.3	144.4	78	336.8	171.6	38	390.3	198.9	98	443.7	226.1	58	497.2	253.3
19	284.2	144.8	79	337.7	172.1	39	391.2	199.3	99	444.6	226.5	59	498.1	253.8
20	285.1	145.3	80	338.6	172.5	40	392.0	199.8	500	445.5	227.0	60	499.0	254.2
321	286.0	145.7	381	339.5	173.0	441	392.9	200.2	501	446.4	227.5	561	499.8	254.7
22	286.9	146.2	82	340.4	173.4	42	393.8	200.7	02	447.3	227.9	62	500.7	255.1
23	287.8	146.6	83	341.3	173.9	43	394.7	201.1	03	448.2	228.4	63	501.6	255.6
24	288.7	147.1	84	342.1	174.3	44	395.6	201.6	04	449.0	228.8	64	502.5	256.0
25	289.6	147.6	85	343.0	174.8	45	396.5	202.0	05	449.9	229.3	65	503.4	256.5
26	290.5	148.0	86	343.9	175.2	46	397.4	202.5	06	450.8	229.8	66	504.3	257.0
27	291.4	148.5	87	344.8	175.7	47	398.3	202.9	07	451.7	230.2	67	505.2	257.4
28	292.3	148.9	88	345.7	176.2	48	399.2	203.4	08	452.6	230.6	68	506.1	257.9
29	293.2	149.4	89	346.6	176.6	49	400.1	203.8	09	453.5	231.0	69	507.0	258.3
30	294.0	149.8	90	347.5	177.1	50	401.0	204.3	10	454.4	231.5	70	507.9	258.8
331	294.9	150.3	391	348.4	177.5	451	401.8	204.7	511	455.3	231.9	571	508.7	259.2
32	295.8	150.7	92	349.3	178.0	52	402.7	205.2	12	456.2	232.4	72	509.6	259.7
33	296.7	151.2	93	350.2	178.4	53	403.6	205.7	13	457.1	232.9	73	510.5	260.1
34	297.6	151.6	94	351.1	178.9	54	404.5	206.1	14	458.0	233.3	74	511.4	260.6
35	298.5	152.1	95	352.0	179.3	55	405.4	206.6	15	458.8	233.8	75	512.3	261.1
36	299.4	152.5	96	352.8	179.8	56	406.3	207.0	16	459.7	234.2	76	513.2	261.5
37	300.3	153.0	97	353.7	180.2	57	407.2	207.5	17	460.6	234.7	77	514.1	262.0
38	301.2	153.5	98	354.6	180.7	58	408.1	207.9	18	461.5	235.2	78	515.0	262.4
39	302.1	153.9	99	355.5	181.2	59	409.0	208.4	19	462.4	235.7	79	515.9	262.9
40	302.9	154.4	400	356.4	181.6	60	409.9	208.8	20	463.3	236.1	80	516.8	263.4
341	303.8	154.8	401	357.3	182.1	461	410.8	209.3	521	464.2	236.6	581	517.7	263.8
42	304.7	155.3	02	358.2	182.5	62	411.6	209.8	22	465.1	237.0	82	518.5	264.3
43	305.6	155.7	03	359.1	183.0	63	412.5	210.2	23	466.0	237.5	83	519.4	264.7
44	306.5	156.2	04	360.0	183.4	64	413.4	210.7	24	466.9	237.9	84	520.3	265.2
45	307.4	156.6	05	360.9	183.9	65	414.3	211.1	25	467.8	238.4	85	521.2	265.6
46	308.3	157.1	06	361.8	184.3	66	415.2	211.6	26	468.7	238.8	86	522.1	266.0
47	309.2	157.5	07	362.6	184.8	67	416.1	212.0	27	469.5	239.3	87	523.0	266.5
48	310.1	158.0	08	363.5	185.2	68	417.0	212.5	28	470.4	239.7	88	523.9	267.0
49	311.0	158.5	09	364.4	185.7	69	417.9	212.9	29	471.3	240.2	89	524.8	267.4
50	311.9	158.9	10	365.3	186.1	70	418.8	213.4	30	472.2	240.6	90	525.7	267.9
351	312.7	159.4	411	366.2	186.6	471	419.7	213.8	531	473.1	241.1	591	526.6	268.3
52	313.6	159.8	12	367.1	187.1	72	420.6	214.3	32	474.0	241.5	92	527.5	268.8
53	314.5	160.3	13	368.0	187.5	73	421.4	214.7	33	474.9	242.0	93	528.4	269.2
54	315.4	160.7	14	368.9	188.0	74	422.3	215.2	34	475.8	242.4	94	529.3	269.7
55	316.3	161.2	15	369.8	188.4	75	423.2	215.7	35	476.7	242.9	95	530.1	270.1
56	317.2	161.6	16	370.7	188.9	76	424.1	216.1	36	477.6	243.4	96	531.0	270.6
57	318.1	162.1	17	371.6	189.3	77	425.0	216.6	37	478.4	243.8	97	531.9	271.1
58	319.0	162.5	18	372.4	189.8	78	425.9	217.0	38	479.3	244.3	98	532.8	271.5
59	319.9	163.0	19	373.3	190.2	79	426.8	217.5	39	480.2	244.7	99	533.7	272.0
60	320.8	163.4	20	374.2	190.7	80	427.7	217.9	40	481.1	245.2	600	534.6	272.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

63° (117°, 243°, 297°).

TABLE 2.

Difference of Latitude and Departure for 28° (152°, 208°, 332°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.5	61	53.9	28.6	121	106.8	56.8	181	159.8	85.0	241	212.8	113.1
2	1.8	0.9	62	54.7	29.1	22	107.7	57.3	82	160.7	85.4	42	213.7	113.6
3	2.6	1.4	63	55.6	29.6	23	108.6	57.7	83	161.6	85.9	43	214.6	114.1
4	3.5	1.9	64	56.5	30.0	24	109.5	58.2	84	162.5	86.4	44	215.4	114.6
5	4.4	2.3	65	57.4	30.5	25	110.4	58.7	85	163.3	86.9	45	216.3	115.0
6	5.3	2.8	66	58.3	31.0	26	111.3	59.2	86	164.2	87.3	46	217.2	115.5
7	6.2	3.3	67	59.2	31.5	27	112.1	59.6	87	165.1	87.8	47	218.1	116.0
8	7.1	3.8	68	60.0	31.9	28	113.0	60.1	88	166.0	88.3	48	219.0	116.4
9	7.9	4.2	69	60.9	32.4	29	113.9	60.6	89	166.9	88.7	49	219.9	116.9
10	8.8	4.7	70	61.8	32.9	30	114.8	61.0	90	167.8	89.2	50	220.7	117.4
11	9.7	5.2	71	62.7	33.3	131	115.7	61.5	191	168.6	89.7	251	221.6	117.8
12	10.6	5.6	72	63.6	33.8	32	116.5	62.0	92	169.5	90.1	52	222.5	118.3
13	11.5	6.1	73	64.5	34.3	33	117.4	62.4	93	170.4	90.6	53	223.4	118.8
14	12.4	6.6	74	65.3	34.7	34	118.3	62.9	94	171.3	91.1	54	224.3	119.2
15	13.2	7.0	75	66.2	35.2	35	119.2	63.4	95	172.2	91.5	55	225.2	119.7
16	14.1	7.5	76	67.1	35.7	36	120.1	63.8	96	173.1	92.0	56	226.0	120.2
17	15.0	8.0	77	68.0	36.1	37	121.0	64.3	97	173.9	92.5	57	226.9	120.7
18	15.9	8.5	78	68.9	36.6	38	121.8	64.8	98	174.8	93.0	58	227.8	121.1
19	16.8	8.9	79	69.8	37.1	39	122.7	65.3	99	175.7	93.4	59	228.7	121.6
20	17.7	9.4	80	70.6	37.6	40	123.6	65.7	200	176.6	93.9	60	229.6	122.1
21	18.5	9.9	81	71.5	38.0	141	124.5	66.2	201	177.5	94.4	261	230.4	122.5
22	19.4	10.3	82	72.4	38.5	42	125.4	66.7	02	178.4	94.8	62	231.3	123.0
23	20.3	10.8	83	73.3	39.0	43	126.3	67.1	03	179.2	95.3	63	232.2	123.5
24	21.2	11.3	84	74.2	39.4	44	127.1	67.6	04	180.1	95.8	64	233.1	123.9
25	22.1	11.7	85	75.1	39.9	45	128.0	68.1	05	181.0	96.2	65	234.0	124.4
26	23.0	12.2	86	75.9	40.4	46	128.9	68.5	06	181.9	96.7	66	234.9	124.9
27	23.8	12.7	87	76.8	40.8	47	129.8	69.0	07	182.8	97.2	67	235.7	125.3
28	24.7	13.1	88	77.7	41.3	48	130.7	69.5	08	183.7	97.7	68	236.6	125.8
29	25.6	13.6	89	78.6	41.8	49	131.6	70.0	09	184.5	98.1	69	237.5	126.3
30	26.5	14.1	90	79.5	42.3	50	132.4	70.4	10	185.4	98.6	70	238.4	126.8
31	27.4	14.6	91	80.3	42.7	151	133.3	70.9	211	186.3	99.1	271	239.3	127.2
32	28.3	15.0	92	81.2	43.2	52	134.2	71.4	12	187.2	99.5	72	240.2	127.7
33	29.1	15.5	93	82.1	43.7	53	135.1	71.8	13	188.1	100.0	73	241.0	128.2
34	30.0	16.0	94	83.0	44.1	54	136.0	72.3	14	189.0	100.5	74	241.9	128.6
35	30.9	16.4	95	83.9	44.6	55	136.9	72.8	15	189.8	100.9	75	242.8	129.1
36	31.8	16.9	96	84.8	45.1	56	137.7	73.2	16	190.7	101.4	76	243.7	129.6
37	32.7	17.4	97	85.6	45.5	57	138.6	73.7	17	191.6	101.9	77	244.6	130.0
38	33.6	17.8	98	86.5	46.0	58	139.5	74.2	18	192.5	102.3	78	245.5	130.5
39	34.4	18.3	99	87.4	46.5	59	140.4	74.6	19	193.4	102.8	79	246.3	131.0
40	35.3	18.8	100	88.3	46.9	60	141.3	75.1	20	194.2	103.3	80	247.2	131.5
41	36.2	19.2	101	89.2	47.4	161	142.2	75.6	221	195.1	103.8	281	248.1	131.9
42	37.1	19.7	02	90.1	47.9	62	143.0	76.1	22	196.0	104.2	82	249.0	132.4
43	38.0	20.2	03	90.9	48.4	63	143.9	76.5	23	196.9	104.7	83	249.9	132.9
44	38.8	20.7	04	91.8	48.8	64	144.8	77.0	24	197.8	105.2	84	250.8	133.3
45	39.7	21.1	05	92.7	49.3	65	145.7	77.5	25	198.7	105.6	85	251.6	133.8
46	40.6	21.6	06	93.6	49.8	66	146.6	77.9	26	199.5	106.1	86	252.5	134.3
47	41.5	22.1	07	94.5	50.2	67	147.5	78.4	27	200.4	106.6	87	253.4	134.7
48	42.4	22.5	08	95.4	50.7	68	148.3	78.9	28	201.3	107.0	88	254.3	135.2
49	43.3	23.0	09	96.2	51.2	69	149.2	79.3	29	202.2	107.5	89	255.2	135.7
50	44.1	23.5	10	97.1	51.6	70	150.1	79.8	30	203.1	108.0	90	256.1	136.1
51	45.0	23.9	111	98.0	52.1	171	151.0	80.3	231	204.0	108.4	291	256.9	136.6
52	45.9	24.4	12	98.9	52.6	72	151.9	80.7	32	204.8	108.9	92	257.8	137.1
53	46.8	24.9	13	99.8	53.1	73	152.7	81.2	33	205.7	109.4	93	258.7	137.6
54	47.7	25.4	14	100.7	53.5	74	153.6	81.7	34	206.6	109.9	94	259.6	138.0
55	48.6	25.8	15	101.5	54.0	75	154.5	82.2	35	207.5	110.3	95	260.5	138.5
56	49.4	26.3	16	102.4	54.5	76	155.4	82.6	36	208.4	110.8	96	261.4	139.0
57	50.3	26.8	17	103.3	54.9	77	156.3	83.1	37	209.3	111.3	97	262.2	139.4
58	51.2	27.2	18	104.2	55.4	78	157.2	83.6	38	210.1	111.7	98	263.1	139.9
59	52.1	27.7	19	105.1	55.9	79	158.0	84.0	39	211.0	112.2	99	264.0	140.4
60	53.0	28.2	20	106.0	56.3	80	158.9	84.5	40	211.9	112.7	300	264.9	140.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

62° (118°, 242°, 298°).

TABLE 2.

Difference of Latitude and Departure for 28° (152°, 208°, 332°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	265.7	141.3	361	318.7	169.5	421	371.7	197.7	481	424.7	225.8	541	477.7	254.0
02	266.6	141.8	62	319.6	170.0	22	372.6	198.1	82	425.6	226.3	42	478.6	254.5
03	267.5	142.3	63	320.5	170.4	23	373.5	198.6	83	426.5	226.8	43	479.4	255.0
04	268.4	142.7	64	321.4	170.9	24	374.3	199.1	84	427.4	227.3	44	480.3	255.5
05	269.3	143.2	65	322.2	171.4	25	375.2	199.5	85	428.3	227.7	45	481.1	255.9
06	270.2	143.7	66	323.1	171.8	26	376.1	200.0	86	429.2	228.2	46	482.0	256.4
07	271.0	144.1	67	324.0	172.3	27	377.0	200.5	87	430.1	228.6	47	482.9	256.9
08	271.9	144.6	68	324.9	172.8	28	377.9	200.9	88	430.9	229.1	48	483.8	257.3
09	272.8	145.1	69	325.8	173.2	29	378.8	201.4	89	431.8	229.6	49	484.7	257.8
10	273.7	145.5	70	326.7	173.7	30	379.6	201.9	90	432.6	230.0	50	485.6	258.2
311	274.6	146.0	371	327.5	174.2	431	380.5	202.3	491	433.5	230.5	551	486.5	258.7
12	275.5	146.5	72	328.4	174.6	32	381.4	202.8	92	434.4	231.0	52	487.4	259.1
13	276.3	146.9	73	329.3	175.1	33	382.3	203.3	93	435.3	231.4	53	488.3	259.6
14	277.2	147.4	74	330.2	175.6	34	383.2	203.8	94	436.2	231.9	54	489.2	260.1
15	278.1	147.9	75	331.1	176.1	35	384.1	204.2	95	437.1	232.4	55	490.1	260.6
16	279.0	148.4	76	332.0	176.5	36	384.9	204.7	96	437.9	232.9	56	490.9	261.0
17	279.9	148.8	77	332.8	177.0	37	385.8	205.2	97	438.8	233.4	57	491.8	261.5
18	280.7	149.3	78	333.7	177.5	38	386.7	205.6	98	439.7	233.8	58	492.7	262.0
19	281.6	149.8	79	334.6	177.9	39	387.6	206.1	99	440.6	234.3	59	493.5	262.5
20	282.5	150.2	80	335.5	178.4	40	388.5	206.6	500	441.5	234.7	60	494.4	262.9
321	283.4	150.7	381	336.4	178.9	441	389.4	207.0	501	442.3	235.2	561	495.3	263.4
22	284.3	151.2	82	337.3	179.3	42	390.2	207.5	02	443.2	235.6	62	496.2	263.8
23	285.2	151.6	83	338.1	179.8	43	391.1	208.0	03	444.1	236.1	63	497.1	264.3
24	286.0	152.1	84	339.0	180.3	44	392.0	208.4	04	445.0	236.6	64	498.0	264.7
25	286.9	152.6	85	339.9	180.8	45	392.9	208.9	05	445.9	237.1	65	498.9	265.2
26	287.8	153.1	86	340.8	181.2	46	393.8	209.4	06	446.8	237.5	66	499.8	265.7
27	288.7	153.5	87	341.7	181.7	47	394.6	209.9	07	447.6	238.0	67	500.7	266.2
28	289.6	154.0	88	342.6	182.2	48	395.5	210.3	08	448.5	238.5	68	501.6	266.6
29	290.5	154.5	89	343.4	182.6	49	396.4	210.8	09	449.4	239.0	69	502.4	267.1
30	291.3	154.9	90	344.3	183.1	50	397.3	211.3	10	450.3	239.4	70	503.3	267.6
331	292.2	155.4	391	345.2	183.6	451	398.2	211.7	511	451.2	239.9	571	504.2	268.0
32	293.1	155.9	92	346.1	184.0	52	399.1	212.2	12	452.1	240.4	72	505.1	268.5
33	294.0	156.3	93	347.0	184.5	53	399.9	212.7	13	452.9	240.8	73	505.9	269.0
34	294.9	156.8	94	347.9	185.0	54	400.8	213.1	14	453.8	241.3	74	506.8	269.4
35	295.8	157.3	95	348.7	185.4	55	401.7	213.6	15	454.7	241.8	75	507.7	269.9
36	296.6	157.7	96	349.6	185.9	56	402.6	214.1	16	455.6	242.2	76	508.6	270.4
37	297.5	158.2	97	350.5	186.4	57	403.5	214.6	17	456.4	242.7	77	509.4	270.9
38	298.4	158.7	98	351.4	186.9	58	404.4	215.0	18	457.3	243.2	78	510.3	271.3
39	299.3	159.2	99	352.3	187.3	59	405.2	215.5	19	458.2	243.7	79	511.2	271.8
40	300.2	159.6	400	353.1	187.8	60	406.1	216.0	20	459.1	244.1	80	512.1	272.3
341	301.0	160.1	401	354.0	188.3	461	407.0	216.4	521	460.0	244.6	581	513.0	272.7
42	301.9	160.6	02	354.9	188.7	62	407.9	216.9	22	460.9	245.0	82	513.9	273.2
43	302.8	161.0	03	355.8	189.2	63	408.8	217.4	23	461.8	245.5	83	514.8	273.7
44	303.7	161.5	04	356.7	189.7	64	409.7	217.8	24	462.7	246.0	84	515.7	274.2
45	304.6	162.0	05	357.6	190.1	65	410.5	218.3	25	463.5	246.5	85	516.5	274.7
46	305.5	162.4	06	358.4	190.6	66	411.4	218.8	26	464.4	246.9	86	517.4	275.1
47	306.4	162.9	07	359.3	191.1	67	412.3	219.2	27	465.3	247.4	87	518.3	275.5
48	307.2	163.4	08	360.2	191.5	68	413.2	219.7	28	466.2	247.9	88	519.2	276.0
49	308.1	163.8	09	361.1	192.0	69	414.1	220.2	29	467.1	248.3	89	520.1	276.5
50	309.0	164.3	10	362.0	192.5	70	415.0	220.7	30	468.0	248.8	90	521.0	277.0
351	309.9	164.8	411	362.9	193.0	471	415.8	221.1	531	468.9	249.3	591	521.8	277.4
52	310.8	165.3	12	363.7	193.4	72	416.7	221.6	32	469.8	249.8	92	522.6	277.9
53	311.7	165.7	13	364.6	193.9	73	417.6	222.1	33	470.7	250.2	93	523.5	278.4
54	312.5	166.2	14	365.5	194.4	74	418.5	222.5	34	471.5	250.7	94	524.4	278.8
55	313.4	166.7	15	366.4	194.8	75	419.4	223.0	35	472.4	251.1	95	525.3	279.3
56	314.3	167.1	16	367.3	195.3	76	420.3	223.5	36	473.3	251.6	96	526.2	279.8
57	315.2	167.6	17	368.2	195.8	77	421.1	223.9	37	474.2	252.1	97	527.1	280.3
58	316.1	168.1	18	369.0	196.2	78	422.0	224.4	38	475.1	252.6	98	528.0	280.8
59	316.9	168.5	19	369.9	196.7	79	422.9	224.9	39	476.0	253.1	99	528.9	281.3
60	317.8	169.0	20	370.8	197.2	80	423.8	225.3	40	476.8	253.6	600	529.8	281.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

62° (118°, 242°, 298°).

TABLE 2.

Difference of Latitude and Departure for 29° (151°, 209°, 331°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.5	61	53.4	29.6	121	105.8	58.7	181	158.3	87.8	241	210.8	116.8
2	1.7	1.0	62	54.2	30.1	22	106.7	59.1	82	159.2	88.2	42	211.7	117.3
3	2.6	1.5	63	55.1	30.5	23	107.6	59.6	83	160.1	88.7	43	212.5	117.8
4	3.5	1.9	64	56.0	31.0	24	108.5	60.1	84	160.9	89.2	44	213.4	118.3
5	4.4	2.4	65	56.9	31.5	25	109.3	60.6	85	161.8	89.7	45	214.3	118.8
6	5.2	2.9	66	57.7	32.0	26	110.2	61.1	86	162.7	90.2	46	215.2	119.3
7	6.1	3.4	67	58.6	32.5	27	111.1	61.6	87	163.6	90.7	47	216.0	119.7
8	7.0	3.9	68	59.5	33.0	28	112.0	62.1	88	164.4	91.1	48	216.9	120.2
9	7.9	4.4	69	60.3	33.5	29	112.8	62.5	89	165.3	91.6	49	217.8	120.7
10	8.7	4.8	70	61.2	33.9	30	113.7	63.0	90	166.2	92.1	50	218.7	121.2
11	9.6	5.3	71	62.1	34.4	131	114.6	63.5	191	167.1	92.6	251	219.5	121.7
12	10.5	5.8	72	63.0	34.9	32	115.4	64.0	92	167.9	93.1	52	220.4	122.2
13	11.4	6.3	73	63.8	35.4	33	116.3	64.5	93	168.8	93.6	53	221.3	122.7
14	12.2	6.8	74	64.7	35.9	34	117.2	65.0	94	169.7	94.1	54	222.2	123.1
15	13.1	7.3	75	65.6	36.4	35	118.1	65.4	95	170.6	94.5	55	223.0	123.6
16	14.0	7.8	76	66.5	36.8	36	118.9	65.9	96	171.4	95.0	56	223.9	124.1
17	14.9	8.2	77	67.3	37.3	37	119.8	66.4	97	172.3	95.5	57	224.8	124.6
18	15.7	8.7	78	68.2	37.8	38	120.7	66.9	98	173.2	96.0	58	225.7	125.1
19	16.6	9.2	79	69.1	38.3	39	121.6	67.4	99	174.0	96.5	59	226.5	125.6
20	17.5	9.7	80	70.0	38.8	40	122.4	67.9	200	174.9	97.0	60	227.4	126.1
21	18.4	10.2	81	70.8	39.3	141	123.3	68.4	201	175.8	97.4	261	228.3	126.5
22	19.2	10.7	82	71.7	39.8	42	124.2	68.8	02	176.7	97.9	62	229.2	127.0
23	20.1	11.2	83	72.6	40.2	43	125.1	69.3	03	177.5	98.4	63	230.0	127.5
24	21.0	11.6	84	73.5	40.7	44	125.9	69.8	04	178.4	98.9	64	230.9	128.0
25	21.9	12.1	85	74.3	41.2	45	126.8	70.3	05	179.3	99.4	65	231.8	128.5
26	22.7	12.6	86	75.2	41.7	46	127.7	70.8	06	180.2	99.9	66	232.6	129.0
27	23.6	13.1	87	76.1	42.2	47	128.6	71.3	07	181.0	100.4	67	233.5	129.4
28	24.5	13.6	88	77.0	42.7	48	129.4	71.8	08	181.9	100.8	68	234.4	129.9
29	25.4	14.1	89	77.8	43.1	49	130.3	72.2	09	182.8	101.3	69	235.3	130.4
30	26.2	14.5	90	78.7	43.6	50	131.2	72.7	10	183.7	101.8	70	236.1	130.9
31	27.1	15.0	91	79.6	44.1	151	132.1	73.2	211	184.5	102.3	271	237.0	131.4
32	28.0	15.5	92	80.5	44.6	52	132.9	73.7	12	185.4	102.8	72	237.9	131.9
33	28.9	16.0	93	81.3	45.1	53	133.8	74.2	13	186.3	103.3	73	238.8	132.4
34	29.7	16.5	94	82.2	45.6	54	134.7	74.7	14	187.2	103.7	74	239.6	132.8
35	30.6	17.0	95	83.1	46.1	55	135.6	75.1	15	188.0	104.2	75	240.5	133.3
36	31.5	17.5	96	84.0	46.5	56	136.4	75.6	16	188.9	104.7	76	241.4	133.8
37	32.4	17.9	97	84.8	47.0	57	137.3	76.1	17	189.8	105.2	77	242.3	134.3
38	33.2	18.4	98	85.7	47.5	58	138.2	76.6	18	190.7	105.7	78	243.1	134.8
39	34.1	18.9	99	86.6	48.0	59	139.1	77.1	19	191.5	106.2	79	244.0	135.3
40	35.0	19.4	100	87.5	48.5	60	139.9	77.6	20	192.4	106.7	80	244.9	135.7
41	35.9	19.9	101	88.3	49.0	161	140.8	78.1	221	193.3	107.1	281	245.8	136.2
42	36.7	20.4	02	89.2	49.5	62	141.7	78.5	22	194.2	107.6	82	246.6	136.7
43	37.6	20.8	03	90.1	49.9	63	142.6	79.0	23	195.0	108.1	83	247.5	137.2
44	38.5	21.3	04	91.0	50.4	64	143.4	79.5	24	195.9	108.6	84	248.4	137.7
45	39.4	21.8	05	91.8	50.9	65	144.3	80.0	25	196.8	109.1	85	249.3	138.2
46	40.2	22.3	06	92.7	51.4	66	145.2	80.5	26	197.7	109.6	86	250.1	138.7
47	41.1	22.8	07	93.6	51.9	67	146.1	81.0	27	198.5	110.1	87	251.0	139.1
48	42.0	23.3	08	94.5	52.4	68	146.9	81.4	28	199.4	110.5	88	251.9	139.6
49	42.9	23.8	09	95.3	52.8	69	147.8	81.9	29	200.3	111.0	89	252.8	140.1
50	43.7	24.2	10	96.2	53.3	70	148.7	82.4	30	201.2	111.5	90	253.6	140.6
51	44.6	24.7	111	97.1	53.8	171	149.6	82.9	231	202.0	112.0	291	254.5	141.1
52	45.5	25.2	12	98.0	54.3	72	150.4	83.4	32	202.9	112.5	92	255.4	141.6
53	46.4	25.7	13	98.8	54.8	73	151.3	83.9	33	203.8	113.0	93	256.3	142.0
54	47.2	26.2	14	99.7	55.3	74	152.2	84.4	34	204.7	113.4	94	257.1	142.5
55	48.1	26.7	15	100.6	55.8	75	153.1	84.8	35	205.5	113.9	95	258.0	143.0
56	49.0	27.1	16	101.5	56.2	76	153.9	85.3	36	206.4	114.4	96	258.9	143.5
57	49.9	27.6	17	102.3	56.7	77	154.8	85.8	37	207.3	114.9	97	259.8	144.0
58	50.7	28.1	18	103.2	57.2	78	155.7	86.3	38	208.2	115.4	98	260.6	144.5
59	51.6	28.6	19	104.1	57.7	79	156.6	86.8	39	209.0	115.9	99	261.5	145.0
60	52.5	29.1	20	105.0	58.2	80	157.4	87.3	40	209.9	116.4	300	262.4	145.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

61° (119°, 241°, 299°).

TABLE 2.

Difference of Latitude and Departure for 29° (151°, 209°, 331°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	263.2	145.9	361	315.7	175.0	421	368.2	204.1	481	420.7	233.2	541	473.2	262.3
02	264.1	146.4	62	316.6	175.5	22	369.1	204.6	82	421.5	233.7	42	474.0	262.8
03	265.0	146.9	63	317.5	176.0	23	369.9	205.1	83	422.4	234.2	43	474.9	263.2
04	265.9	147.4	64	318.3	176.5	24	370.8	205.6	84	423.3	234.6	44	475.8	263.7
05	266.7	147.9	65	319.2	177.0	25	371.7	206.0	85	424.2	235.1	45	476.6	264.2
06	267.6	148.4	66	320.1	177.4	26	372.6	206.5	86	425.0	235.6	46	477.5	264.7
07	268.5	148.8	67	321.0	177.9	27	373.4	207.0	87	425.9	236.1	47	478.4	265.2
08	269.4	149.3	68	321.8	178.4	28	374.3	207.5	88	426.8	236.6	48	479.3	265.7
09	270.2	149.8	69	322.7	178.9	29	375.2	208.0	89	427.7	237.1	49	480.1	266.2
10	271.1	150.3	70	323.6	179.4	30	376.1	208.5	90	428.5	237.6	50	481.0	266.6
311	272.0	150.8	371	324.5	179.9	431	376.9	209.0	491	429.4	238.0	551	481.9	267.1
12	272.9	151.3	72	325.3	180.4	32	377.8	209.4	92	430.3	238.5	52	482.8	267.6
13	273.7	151.7	73	326.2	180.8	33	378.7	209.9	93	431.2	239.0	53	483.6	268.1
14	274.6	152.2	74	327.1	181.3	34	379.6	210.4	94	432.0	239.5	54	484.5	268.6
15	275.5	152.7	75	328.0	181.8	35	380.4	210.9	95	432.9	240.0	55	485.4	269.1
16	276.3	153.2	76	328.8	182.3	36	381.3	211.4	96	433.8	240.5	56	486.3	269.5
17	277.2	153.7	77	329.7	182.8	37	382.2	211.9	97	434.7	240.9	57	487.1	270.0
18	278.1	154.2	78	230.6	183.3	38	383.1	212.3	98	435.5	241.4	58	488.0	270.5
19	279.0	154.7	79	331.4	183.7	39	383.9	212.8	99	436.4	241.9	59	488.9	271.0
20	279.8	155.1	80	332.3	184.2	40	384.8	213.3	500	437.3	242.4	60	489.8	271.5
321	280.7	155.6	381	333.2	184.7	441	385.7	213.8	501	438.2	242.9	561	490.6	272.0
22	281.6	156.1	82	334.1	185.2	42	386.6	214.3	02	439.0	243.4	62	491.5	272.5
23	282.5	156.6	83	334.9	185.7	43	387.4	214.8	03	439.9	243.9	63	492.4	272.9
24	283.3	157.1	84	335.8	186.2	44	388.3	215.3	04	440.8	244.3	64	493.2	273.4
25	284.2	157.6	85	336.7	186.7	45	389.2	215.7	05	441.6	244.8	65	494.1	273.9
26	285.1	158.1	86	337.6	187.1	46	390.0	216.2	06	442.5	245.3	66	495.0	274.4
27	286.0	158.5	87	338.4	187.6	47	390.9	216.7	07	443.4	245.8	67	495.9	274.9
28	286.8	159.0	88	339.3	188.1	48	391.8	217.2	08	444.3	246.3	68	496.8	275.4
29	287.7	159.5	89	340.2	188.6	49	392.7	217.7	09	445.2	246.8	69	497.7	275.9
30	288.6	160.0	90	341.1	189.1	50	393.5	218.2	10	446.1	247.3	70	498.5	276.3
31	289.5	160.5	391	341.9	189.6	451	394.4	218.7	511	447.0	247.8	571	499.4	276.8
32	290.3	161.0	92	342.8	190.0	52	395.3	219.1	12	447.8	248.2	72	500.3	277.3
33	291.2	161.4	93	343.7	190.5	53	396.2	219.6	13	448.6	248.7	73	501.1	277.8
34	292.1	161.9	94	344.6	191.0	54	397.0	220.1	14	449.5	249.2	74	502.0	278.3
35	293.0	162.4	95	345.4	191.5	55	397.9	220.6	15	450.4	249.7	75	502.9	278.8
36	293.8	162.9	96	346.3	192.0	56	398.8	221.1	16	451.3	250.2	76	503.7	279.2
37	294.7	163.4	97	347.2	192.5	57	399.7	221.6	17	452.2	250.6	77	504.6	279.7
38	295.6	163.9	98	348.1	193.0	58	400.5	222.0	18	453.1	251.1	78	505.5	280.2
39	296.5	164.4	99	348.9	193.4	59	401.4	222.5	19	253.9	251.6	79	506.4	280.7
40	297.3	164.8	400	349.8	193.9	60	402.3	223.0	20	454.8	252.1	80	507.2	281.2
341	298.2	165.3	401	350.7	194.4	461	403.2	223.5	521	455.6	252.6	581	508.1	281.7
42	299.1	165.8	02	351.6	194.9	62	404.0	224.0	22	456.5	253.1	82	509.0	282.2
43	300.0	166.3	03	352.4	195.4	63	404.9	224.5	23	457.4	253.6	83	509.9	282.7
44	300.8	166.8	04	353.3	195.9	64	405.8	225.0	24	458.3	254.0	84	510.7	283.2
45	301.7	167.3	05	354.2	196.3	65	406.7	225.4	25	459.1	254.5	85	511.6	283.6
46	302.6	167.7	06	355.1	196.8	66	407.5	225.9	26	460.0	255.0	86	512.5	284.1
47	303.5	168.2	07	355.9	197.3	67	408.4	226.4	27	460.9	255.5	87	513.4	284.6
48	304.3	168.7	08	356.8	197.8	68	409.3	226.9	28	461.8	256.0	88	514.3	285.0
49	305.2	169.2	09	357.7	198.3	69	410.2	227.4	29	462.6	256.5	89	515.1	285.5
50	306.1	169.7	10	358.6	198.8	70	411.0	227.9	30	463.5	256.9	90	516.0	286.0
351	307.0	170.2	411	359.4	199.3	471	411.9	228.3	531	464.4	257.4	591	516.9	286.5
52	307.8	170.7	12	360.3	199.7	72	412.8	228.8	32	465.3	257.9	92	517.7	287.0
53	308.7	171.1	13	361.2	200.2	73	413.7	229.3	33	466.1	258.4	93	518.6	287.5
54	309.6	171.6	14	362.1	200.7	74	414.5	229.8	34	467.0	258.9	94	519.5	288.0
55	310.5	172.1	15	362.9	201.2	75	415.4	230.3	35	467.9	259.4	95	520.4	288.5
56	311.3	172.6	16	363.8	201.7	76	416.3	230.8	36	468.8	259.9	96	521.2	288.9
57	312.2	173.1	17	364.7	202.2	77	417.2	231.3	37	469.6	260.3	97	522.1	289.4
58	313.1	173.6	18	365.6	202.7	78	418.0	231.7	38	470.5	260.8	98	523.0	289.9
59	314.0	174.0	19	366.4	203.1	79	418.9	232.2	39	471.4	261.3	99	523.9	290.4
60	314.8	174.5	20	367.3	203.6	80	419.8	232.7	40	472.3	261.8	600	524.8	290.9
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

61° (119°, 241°, 299°).

TABLE 2.

Difference of Latitude and Departure for 30° (150°, 210°, 330°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.5	61	52.8	30.5	121	104.8	60.5	181	156.8	90.5	241	208.7	120.5
2	1.7	1.0	62	53.7	31.0	22	105.7	61.0	82	157.6	91.0	42	209.6	121.0
3	2.6	1.5	63	54.6	31.5	23	106.5	61.5	83	158.5	91.5	43	210.4	121.5
4	3.5	2.0	64	55.4	32.0	24	107.4	62.0	84	159.3	92.0	44	211.3	122.0
5	4.3	2.5	65	56.3	32.5	25	108.3	62.5	85	160.2	92.5	45	212.2	122.5
6	5.2	3.0	66	57.2	33.0	26	109.1	63.0	86	161.1	93.0	46	213.0	123.0
7	6.1	3.5	67	58.0	33.5	27	110.0	63.5	87	161.9	93.5	47	213.9	123.5
8	6.9	4.0	68	58.9	34.0	28	110.9	64.0	88	162.8	94.0	48	214.8	124.0
9	7.8	4.5	69	59.8	34.5	29	111.7	64.5	89	163.7	94.5	49	215.6	124.5
10	8.7	5.0	70	60.6	35.0	30	112.6	65.0	90	164.5	95.0	50	216.5	125.0
11	9.5	5.5	71	61.5	35.5	131	113.4	65.5	191	165.4	95.5	251	217.4	125.5
12	10.4	6.0	72	62.4	36.0	32	114.3	66.0	92	166.3	96.0	52	218.2	126.0
13	11.3	6.5	73	63.2	36.5	33	115.2	66.5	93	167.1	96.5	53	219.1	126.5
14	12.1	7.0	74	64.1	37.0	34	116.0	67.0	94	168.0	97.0	54	220.0	127.0
15	13.0	7.5	75	65.0	37.5	35	116.9	67.5	95	168.9	97.5	55	220.8	127.5
16	13.9	8.0	76	65.8	38.0	36	117.8	68.0	96	169.7	98.0	56	221.7	128.0
17	14.7	8.5	77	66.7	38.5	37	118.6	68.5	97	170.6	98.5	57	222.6	128.5
18	15.6	9.0	78	67.5	39.0	38	119.5	69.0	98	171.5	99.0	58	223.4	129.0
19	16.5	9.5	79	68.4	39.5	39	120.4	69.5	99	172.3	99.5	59	224.3	129.5
20	17.3	10.0	80	69.3	40.0	40	121.2	70.0	200	173.2	100.0	60	225.2	130.0
21	18.2	10.5	81	70.1	40.5	141	122.1	70.5	201	174.1	100.5	261	226.0	130.5
22	19.1	11.0	82	71.0	41.0	42	123.0	71.0	02	174.9	101.0	62	226.9	131.0
23	19.9	11.5	83	71.9	41.5	43	123.8	71.5	03	175.8	101.5	63	227.8	131.5
24	20.8	12.0	84	72.7	42.0	44	124.7	72.0	04	176.7	102.0	64	228.6	132.0
25	21.7	12.5	85	73.6	42.5	45	125.6	72.5	05	177.5	102.5	65	229.5	132.5
26	22.5	13.0	86	74.5	43.0	46	126.4	73.0	06	178.4	103.0	66	230.4	133.0
27	23.4	13.5	87	75.3	43.5	47	127.3	73.5	07	179.3	103.5	67	231.2	133.5
28	24.2	14.0	88	76.2	44.0	48	128.2	74.0	08	180.1	104.0	68	232.1	134.0
29	25.1	14.5	89	77.1	44.5	49	129.0	74.5	09	181.0	104.5	69	233.0	134.5
30	26.0	15.0	90	77.9	45.0	50	129.9	75.0	10	181.9	105.0	70	233.8	135.0
31	26.8	15.5	91	78.8	45.5	151	130.8	75.5	211	182.7	105.5	271	234.7	135.5
32	27.7	16.0	92	79.7	46.0	52	131.6	76.0	12	183.6	106.0	72	235.6	136.0
33	28.6	16.5	93	80.5	46.5	53	132.5	76.5	13	184.5	106.5	73	236.4	136.5
34	29.4	17.0	94	81.4	47.0	54	133.4	77.0	14	185.3	107.0	74	237.3	137.0
35	30.3	17.5	95	82.3	47.5	55	134.2	77.5	15	186.2	107.5	75	238.2	137.5
36	31.2	18.0	96	83.1	48.0	56	135.1	78.0	16	187.1	108.0	76	239.0	138.0
37	32.0	18.5	97	84.0	48.5	57	136.0	78.5	17	187.9	108.5	77	239.9	138.5
38	32.9	19.0	98	84.9	49.0	58	136.8	79.0	18	188.8	109.0	78	240.8	139.0
39	33.8	19.5	99	85.7	49.5	59	137.7	79.5	19	189.7	109.5	79	241.6	139.5
40	34.6	20.0	100	86.6	50.0	60	138.6	80.0	20	190.5	110.0	80	242.5	140.0
41	35.5	20.5	101	87.5	50.5	161	139.4	80.5	221	191.4	110.5	281	243.4	140.5
42	36.4	21.0	02	88.3	51.0	62	140.3	81.0	22	192.3	111.0	82	244.2	141.0
43	37.2	21.5	03	89.2	51.5	63	141.2	81.5	23	193.1	111.5	83	245.1	141.5
44	38.1	22.0	04	90.1	52.0	64	142.0	82.0	24	194.0	112.0	84	246.0	142.0
45	39.0	22.5	05	90.9	52.5	65	142.9	82.5	25	194.9	112.5	85	246.8	142.5
46	39.8	23.0	06	91.8	53.0	66	143.8	83.0	26	195.7	113.0	86	247.7	143.0
47	40.7	23.5	07	92.7	53.5	67	144.6	83.5	27	196.6	113.5	87	248.5	143.5
48	41.6	24.0	08	93.5	54.0	68	145.5	84.0	28	197.5	114.0	88	249.4	144.0
49	42.4	24.5	09	94.4	54.5	69	146.4	84.5	29	198.3	114.5	89	250.3	144.5
50	43.3	25.0	10	95.3	55.0	70	147.2	85.0	30	199.2	115.0	90	251.1	145.0
51	44.2	25.5	111	96.1	55.5	171	148.1	85.5	231	200.1	115.5	291	252.0	145.5
52	45.0	26.0	12	97.0	56.0	72	149.0	86.0	32	200.9	116.0	92	252.9	146.0
53	45.9	26.5	13	97.9	56.5	73	149.8	86.5	33	201.8	116.5	93	253.7	146.5
54	46.8	27.0	14	98.7	57.0	74	150.7	87.0	34	202.6	117.0	94	254.6	147.0
55	47.6	27.5	15	99.6	57.5	75	151.6	87.5	35	203.5	117.5	95	255.5	147.5
56	48.5	28.0	16	100.5	58.0	76	152.4	88.0	36	204.4	118.0	96	256.3	148.0
57	49.4	28.5	17	101.3	58.5	77	153.3	88.5	37	205.2	118.5	97	257.2	148.5
58	50.2	29.0	18	102.2	59.0	78	154.2	89.0	38	206.1	119.0	98	258.1	149.0
59	51.1	29.5	19	103.1	59.5	79	155.0	89.5	39	207.0	119.5	99	258.9	149.5
60	52.0	30.0	20	103.9	60.0	80	155.9	90.0	40	207.8	120.0	300	259.8	150.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

60° (120°, 240°, 300°).

TABLE 2.

Difference of Latitude and Departure for 30° (150°, 210°, 330°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	260.7	150.5	361	312.6	180.5	421	364.6	210.5	481	416.6	240.5	541	468.5	270.5
02	261.5	151.0	62	313.5	181.0	22	365.5	211.0	82	417.4	241.0	42	469.4	271.0
03	262.4	151.5	63	314.4	181.5	23	366.3	211.5	83	418.3	241.5	43	470.3	271.5
04	263.3	152.0	64	315.2	182.0	24	367.2	212.0	84	419.2	242.0	44	471.1	272.0
05	264.1	152.5	65	316.1	182.5	25	368.1	212.5	85	420.0	242.5	45	472.0	272.5
06	265.0	153.0	66	317.0	183.0	26	368.9	213.0	86	420.9	243.0	46	472.9	273.0
07	265.9	153.5	67	317.8	183.5	27	369.8	213.5	87	421.8	243.5	47	473.7	273.5
08	266.7	154.0	68	318.7	184.0	28	370.7	214.0	88	422.6	244.0	48	474.6	274.0
09	267.6	154.5	69	319.6	184.5	29	371.5	214.5	89	423.5	244.5	49	475.5	274.5
10	268.5	155.0	70	320.4	185.0	30	372.4	215.0	90	424.4	245.0	50	476.3	275.0
311	269.3	155.5	371	321.3	185.5	431	373.3	215.5	491	425.2	245.5	551	477.2	275.5
12	270.2	156.0	72	322.2	186.0	32	374.1	216.0	92	426.1	246.0	52	478.1	276.0
13	271.1	156.5	73	323.0	186.5	33	375.0	216.5	93	426.9	246.5	53	478.9	276.5
14	271.9	157.0	74	323.9	187.0	34	375.9	217.0	94	427.8	247.0	54	479.8	277.0
15	272.8	157.5	75	324.8	187.5	35	376.7	217.5	95	428.7	247.5	55	480.7	277.5
16	273.7	158.0	76	325.6	188.0	36	377.6	218.0	96	429.6	248.0	56	481.5	278.0
17	274.5	158.5	77	326.5	188.5	37	378.5	218.5	97	430.4	248.5	57	482.4	278.5
18	275.4	159.0	78	327.4	189.0	38	379.3	219.0	98	431.3	249.0	58	483.3	279.0
19	276.3	159.5	79	328.2	189.5	39	380.2	219.5	99	432.2	249.5	59	484.1	279.5
20	277.1	160.0	80	329.1	190.0	40	381.1	220.0	500	433.0	250.0	60	485.0	280.0
321	278.0	160.5	381	330.0	190.5	441	381.9	220.5	501	433.9	250.5	561	485.9	280.5
22	278.9	161.0	82	330.8	191.0	42	382.8	221.0	02	434.8	251.0	62	486.7	281.0
23	279.7	161.5	83	331.7	191.5	43	383.7	221.5	03	435.6	251.5	63	487.6	281.5
24	280.6	162.0	84	332.6	192.0	44	384.5	222.0	04	436.5	252.0	64	488.5	282.0
25	281.5	162.5	85	333.4	192.5	45	385.4	222.5	05	437.4	252.5	65	489.3	282.5
26	282.3	163.0	86	334.3	193.0	46	386.3	223.0	06	438.2	253.0	66	490.2	283.0
27	283.2	163.5	87	335.2	193.5	47	387.1	223.5	07	439.1	253.5	67	491.1	283.5
28	284.1	164.0	88	336.0	194.0	48	388.0	224.0	08	440.0	254.0	68	491.9	284.0
29	284.9	164.5	89	336.9	194.5	49	388.9	224.5	09	440.8	254.5	69	492.8	284.5
30	285.8	165.0	90	337.8	195.0	50	389.7	225.0	10	441.7	255.0	70	493.6	285.0
331	286.7	165.5	391	338.6	195.5	451	390.6	225.5	511	442.6	255.5	571	494.5	285.5
32	287.5	166.0	92	339.5	196.0	52	391.5	226.0	12	443.4	256.0	72	495.4	286.0
33	288.4	166.5	93	340.4	196.5	53	392.3	226.5	13	444.3	256.5	73	496.3	286.5
34	289.3	167.0	94	341.2	197.0	54	393.2	227.0	14	445.2	257.0	74	497.1	287.0
35	290.1	167.5	95	342.1	197.5	55	394.0	227.5	15	446.0	257.5	75	497.9	287.5
36	291.0	168.0	96	343.0	198.0	56	394.9	228.0	16	446.9	258.0	76	498.8	288.0
37	291.9	168.5	97	343.8	198.5	57	395.8	228.5	17	447.8	258.5	77	499.7	288.5
38	292.7	169.0	98	344.7	199.0	58	396.6	229.0	18	448.6	259.0	78	500.5	289.0
39	293.6	169.5	99	345.6	199.5	59	397.5	229.5	19	449.4	259.5	79	501.3	289.5
40	294.5	170.0	400	346.4	200.0	60	398.4	230.0	20	450.3	260.0	80	502.2	290.0
341	295.3	170.5	401	347.3	200.5	461	399.2	230.5	521	451.2	260.5	581	503.1	290.5
42	296.2	171.0	02	348.1	201.0	62	400.1	231.0	22	452.1	261.0	82	504.0	291.0
43	297.1	171.5	03	349.0	201.5	63	401.0	231.5	23	452.9	261.5	83	504.9	291.5
44	297.9	172.0	04	349.9	202.0	64	401.8	232.0	24	453.8	262.0	84	505.8	292.0
45	298.8	172.5	05	350.7	202.5	65	402.7	232.5	25	454.7	262.5	85	506.6	292.5
46	299.7	173.0	06	351.6	203.0	66	403.6	233.0	26	455.5	263.0	86	507.5	293.0
47	300.5	173.5	07	352.5	203.5	67	404.4	233.5	27	456.4	263.5	87	508.4	293.5
48	301.4	174.0	08	353.3	204.0	68	405.3	234.0	28	457.3	264.0	88	509.2	294.0
49	302.3	174.5	09	354.2	204.5	69	406.2	234.5	29	458.1	264.5	89	510.1	294.5
50	303.1	175.0	10	355.1	205.0	70	407.0	235.0	30	459.0	265.0	90	511.0	295.0
351	304.0	175.5	411	355.9	205.5	471	407.9	235.5	531	459.9	265.5	591	511.8	295.5
52	304.8	176.0	12	356.8	206.0	72	408.8	236.0	32	460.7	266.0	92	512.7	296.0
53	305.7	176.5	13	357.7	206.5	73	409.6	236.5	33	461.6	266.5	93	513.6	296.5
54	306.6	177.0	14	358.5	207.0	74	410.5	237.0	34	462.5	267.0	94	514.4	297.0
55	307.4	177.5	15	359.4	207.5	75	411.4	237.5	35	463.3	267.5	95	515.3	297.5
56	308.3	178.0	16	360.3	208.0	76	412.2	238.0	36	464.2	268.0	96	516.2	298.0
57	309.2	178.5	17	361.1	208.5	77	413.1	238.5	37	465.1	268.5	97	517.0	298.5
58	310.0	179.0	18	362.0	209.0	78	414.0	239.0	38	465.9	269.0	98	517.9	299.0
59	310.9	179.5	19	362.9	209.5	79	414.8	239.5	39	466.8	269.5	99	518.8	299.5
60	311.8	180.0	20	363.7	210.0	80	415.7	240.0	40	467.7	270.0	600	519.6	300.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

60° (120°, 240°, 300°).

TABLE 2.

Difference of Latitude and Departure for 31° (149°, 211°, 329°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.5	61	52.3	31.4	121	103.7	62.3	181	155.1	93.2	241	206.6	124.1
2	1.7	1.0	62	53.1	31.9	22	104.6	62.8	82	156.0	93.7	42	207.4	124.6
3	2.6	1.5	63	54 0	32.4	23	105.4	63.3	83	156.9	94.3	43	208.3	125.2
4	3.4	2.1	64	54.9	33.0	24	106.3	63.9	84	157.7	94.8	44	209.1	125.7
5	4.3	2.6	65	55.7	33.5	25	107.1	64.4	85	158.6	95.3	45	210.0	126.2
6	5.1	3.1	66	56.6	34.0	26	108.0	64.9	86	159.4	95.8	46	210.9	126.7
7	6.0	3.6	67	57.4	34.5	27	108.9	65.4	87	160.3	96.3	47	211.7	127.2
8	6.9	4.1	68	58.3	35.0	28	109.7	65.9	88	161.1	96.8	48	212.6	127.7
9	7.7	4.6	69	59.1	35.5	29	110.6	66.4	89	162.0	97.3	49	213.4	128.2
10	8.6	5.2	70	60.0	36.1	30	111.4	67.0	90	162.9	97.9	50	214.3	128.8
11	9.4	5.7	71	60.9	36.6	131	112.3	67.5	191	163.7	98.4	251	215.1	129.3
12	10.3	6.2	72	61.7	37.1	32	113.1	68.0	92	164.6	98.9	52	216.0	129.8
13	11.1	6.7	73	62.6	37.6	33	114.0	68.5	93	165.4	99.4	53	216.9	130.3
14	12.0	7.2	74	63.4	38.1	34	114.9	69.0	94	166.3	99.9	54	217.7	130.8
15	12.9	7.7	75	64.3	38.6	35	115.7	69.5	95	167.1	100.4	55	218.6	131.3
16	13.7	8.2	76	65.1	39.1	36	116.6	70.0	96	168.0	100.9	56	219.4	131.8
17	14.6	8.8	77	66.0	39.7	37	117.4	70.6	97	168.9	101.5	57	220.3	132.4
18	15.4	9.3	78	66.9	40.2	38	118.3	71.1	98	169.7	102.0	58	221.1	132.9
19	16.3	9.8	79	67.7	40.7	39	119.1	71.6	99	170.6	102.5	59	222.0	133.4
20	17.1	10.3	80	68.6	41.2	40	120.0	72.1	200	171.4	103.0	60	222.9	133.9
21	18.0	10.8	81	69.4	41.7	141	120.9	72.6	201	172.3	103.5	261	223.7	134.4
22	18.9	11.3	82	70.3	42.2	42	121.7	73.1	02	173.1	104.0	62	224.6	134.9
23	19.7	11.8	83	71.1	42.7	43	122.6	73.7	03	174.0	104.6	63	225.4	135.5
24	20.6	12.4	84	72.0	43.3	44	123.4	74.2	04	174.9	105.1	64	226.3	136.0
25	21.4	12.9	85	72.9	43.8	45	124.3	74.7	05	175.7	105.6	65	227.1	136.5
26	22.3	13.4	86	73.7	44.3	46	125.1	75.2	06	176.6	106.1	66	228.0	137.0
27	23.1	13.9	87	74.6	44.8	47	126.0	75.7	07	177.4	106.6	67	228.9	137.5
28	24.0	14.4	88	75.4	45.3	48	126.9	76.2	08	178.3	107.1	68	229.7	138.0
29	24.9	14.9	89	76.3	45.8	49	127.7	76.7	09	179.1	107.6	69	230.6	138.5
30	25.7	15.5	90	77.1	46.4	50	128.6	77.3	10	180.0	108.2	70	231.4	139.1
31	26.6	16.0	91	78.0	46.9	151	129.4	77.8	211	180.9	108.7	271	232.3	139.6
32	27.4	16.5	92	78.9	47.4	52	130.3	78.3	12	181.7	109.2	72	233.1	140.1
33	28.3	17.0	93	79.7	47.9	53	131.1	78.8	13	182.6	109.7	73	234 0	140.6
34	29.1	17.5	94	80.6	48.4	54	132.0	79.3	14	183.4	110.2	74	234.9	141.1
35	30.0	18.0	95	81.4	48.9	55	132.9	79.8	15	184.3	110.7	75	235.7	141.6
36	30.9	18.5	96	82.3	49.4	56	133.7	80.3	16	185.1	111.2	76	236.6	142.2
37	31.7	19.1	97	83.1	50.0	57	134.6	80.9	17	186.0	111.8	77	237.4	142.7
38	32.6	19.6	98	84.0	50.5	58	135.4	81.4	18	186.9	112.3	78	238.3	143.2
39	33.4	20.1	99	84.9	51.0	59	136.3	81.9	19	187.7	112.8	79	239.1	143.7
40	34.3	20.6	100	85.7	51.5	60	137.1	82.4	20	188.6	113.3	80	240.0	144.2
41	35.1	21.1	101	86.6	52.0	161	138.0	82.9	221	189.4	113.8	281	240.9	144.7
42	36.0	21.6	02	87.4	52.5	62	138.9	83.4	22	190.3	114.3	82	241.7	145.2
43	36.9	22.1	03	88.3	53.0	63	139.7	84.0	23	191.1	114.9	83	242.6	145.8
44	37.7	22.7	04	89.1	53.6	64	140.6	84.5	24	192.0	115.4	84	243.4	146.3
45	38.6	23.2	05	90.0	54.1	65	141.4	85.0	25	192.9	115.9	85	244.3	146.8
46	39.4	23.7	06	90.9	54.6	66	142.3	85.5	26	193.7	116.4	86	245.1	147.3
47	40.3	24.2	07	91.7	55.1	67	143.1	86.0	27	194.6	116.9	87	246.0	147.8
48	41.1	24.7	08	92.6	55.6	68	144.0	86.5	28	195.4	117.4	88	246.9	148.3
49	42.0	25.2	09	93.4	56.1	69	144.9	87.0	29	196.3	117.9	89	247.7	148.8
50	42.9	25.8	10	94.3	56.7	70	145.7	87.6	30	197.1	118.5	90	248.6	149.4
51	43.7	26.3	111	95.1	57.2	171	146.6	88.1	231	198.0	119.0	291	249.4	149.9
52	44.6	26.8	12	96.0	57.7	72	147.4	88.6	32	198.9	119.5	92	250.3	150.4
53	45.4	27.3	13	96.9	58.2	73	148.3	89.1	33	199.7	120.0	93	251.2	150.9
54	46.3	27.8	14	97.7	58.7	74	149.1	89.6	34	200.6	120.5	94	252.0	151.4
55	47.1	28.3	15	98.6	59.2	75	150.0	90.1	35	201.4	121.0	95	252.9	151.9
56	48.0	28.8	16	99.4	59.7	76	150.9	90.6	36	202.3	121.5	96	253.7	152.5
57	48.9	29.4	17	100.3	60.3	77	151.7	91.2	37	203.1	122.1	97	254.6	153.0
58	49.7	29.9	18	101.1	60.8	78	152.6	91.7	38	204.0	122.6	98	255.4	153.5
59	50.6	30.4	19	102.0	61.3	79	153.4	92.2	39	204.9	123.1	99	256.3	154.0
60	51.4	30.9	20	102.9	61.8	80	154.3	92.7	40	205.7	123.6	300	257.1	154.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

59° (121°, 239°, 301°).

Difference of Latitude and Departure for 31° (149°, 211°, 329°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	258.0	155.0	361	309.4	185.9	421	360.9	216.8	481	412.3	247.7	541	463.7	278.6
02	258.9	155.5	62	310.3	186.4	22	361.7	217.3	82	413.2	248.2	42	464.6	279.1
03	259.7	156.1	63	311.2	187.0	23	362.6	217.9	83	414.0	248.8	43	465.4	279.7
04	260.6	156.6	64	312.0	187.5	24	363.4	218.4	84	414.9	249.3	44	466.3	280.2
05	261.4	157.1	65	312.9	188.0	25	364.3	218.9	85	415.7	249.8	45	467.2	280.7
06	262.3	157.6	66	313.7	188.5	26	365.2	219.4	86	416.6	250.3	46	468.0	281.2
07	263.2	158.1	67	314.6	189.0	27	366.0	219.9	87	417.4	250.8	47	468.9	281.7
08	264.0	158.6	68	315.4	189.5	28	366.9	220.4	88	418.3	251.3	48	469.7	282.3
09	264.9	159.2	69	316.3	190.1	29	367.7	221.0	89	419.2	251.9	49	470.6	282.8
10	265.7	159.7	70	317.2	190.6	30	368.6	221.5	90	420.0	252.4	50	471.4	283.3
311	266.6	160.2	371	318.0	191.1	431	369.4	222.0	491	420.9	252.9	551	472.3	283.8
12	267.4	160.7	72	318.9	191.6	32	370.3	222.5	92	421.7	253.4	52	473.2	284.3
13	268.3	161.2	73	319.7	192.1	33	371.2	223.0	93	422.6	253.9	53	474.0	284.8
14	269.2	161.7	74	320.6	192.6	34	372.0	223.5	94	423.4	254.4	54	474.9	285.3
15	270.0	162.2	75	321.4	193.1	35	372.9	224.0	95	424.3	254.9	55	475.7	285.8
16	270.9	162.8	76	322.3	193.7	36	373.7	224.6	96	425.2	255.5	56	476.6	286.4
17	271.7	163.3	77	323.2	194.2	37	374.6	225.1	97	426.0	256.0	57	477.4	286.9
18	272.6	163.8	78	324.0	194.7	38	375.4	225.6	98	426.9	256.5	58	478.3	287.4
19	273.4	164.3	79	324.9	195.2	39	376.3	226.1	99	427.7	257.0	59	479.2	287.9
20	274.3	164.8	80	325.7	195.7	40	377.2	226.6	500	428.6	257.5	60	480.0	288.4
321	275.2	165.3	381	326.6	196.2	441	378.0	227.1	501	429.4	258.0	561	480.9	288.9
22	276.0	165.8	82	327.4	196.7	42	378.9	227.7	02	430.3	258.6	62	481.7	289.5
23	276.9	166.4	83	328.3	197.3	43	379.7	228.2	03	431.2	259.1	63	482.6	290.0
24	277.7	166.9	84	329.2	197.8	44	380.6	228.7	04	432.0	259.6	64	483.4	290.5
25	278.6	167.4	85	330.0	198.3	45	381.4	229.2	05	432.9	260.1	65	484.3	291.0
26	279.4	167.9	86	330.9	198.8	46	382.3	229.7	06	433.7	260.6	66	485.2	291.5
27	280.3	168.4	87	331.7	199.3	47	383.2	230.2	07	434.6	261.1	67	486.0	292.0
28	281.2	168.9	88	332.6	199.8	48	384.0	230.7	08	435.4	261.6	68	486.9	292.5
29	282.0	169.5	89	333.4	200.4	49	384.9	231.3	09	436.3	262.2	69	487.7	293.1
30	282.9	170.0	90	334.3	200.9	50	385.7	231.8	10	437.2	262.7	70	488.6	293.6
331	283.7	170.5	391	335.2	201.4	451	386.6	232.3	511	438.0	263.2	571	489.4	294.1
32	284.6	171.0	92	336.0	201.9	52	387.4	232.8	12	438.9	263.7	72	490.3	294.6
33	285.4	171.5	93	336.9	202.4	53	388.3	233.3	13	439.7	264.2	73	491.2	295.1
34	286.3	172.0	94	337.7	202.9	54	389.2	233.8	14	440.6	264.7	74	492.0	295.6
35	287.2	172.5	95	338.6	203.4	55	390.0	234.3	15	441.4	265.2	75	492.9	296.1
36	288.0	173.1	96	339.4	204.0	56	390.9	234.9	16	442.3	265.8	76	493.7	296.7
37	288.9	173.6	97	340.3	204.5	57	391.7	235.4	17	443.2	266.3	77	494.6	297.2
38	289.7	174.1	98	341.2	205.0	58	392.6	235.9	18	444.0	266.8	78	495.4	297.7
39	290.6	174.6	99	342.0	205.5	59	393.4	236.4	19	444.9	267.3	79	496.3	298.2
40	291.4	175.1	400	342.9	206.0	60	394.3	236.9	20	445.7	267.8	80	497.2	298.7
341	292.3	175.6	401	343.7	206.5	461	395.2	237.4	521	446.6	268.3	581	498.0	299.2
42	293.2	176.1	02	344.6	207.0	62	396.0	238.0	22	447.4	268.9	82	498.9	299.8
43	294.0	176.7	03	345.4	207.6	63	396.9	238.5	23	448.3	269.4	83	499.7	300.3
44	294.9	177.2	04	346.3	208.1	64	397.7	239.0	24	449.2	269.9	84	500.6	300.8
45	295.7	177.7	05	347.2	208.6	65	398.6	239.5	25	450.0	270.4	85	501.4	301.3
46	296.6	178.2	06	348.0	209.1	66	399.4	240.0	26	450.9	270.9	86	502.3	301.8
47	297.4	178.7	07	348.9	209.6	67	400.3	240.5	27	451.7	271.4	87	503.2	302.3
48	298.3	179.2	08	349.7	210.1	68	401.2	241.0	28	452.6	271.9	88	504.0	302.8
49	299.2	179.8	09	350.6	210.7	69	402.0	241.5	29	453.4	272.4	89	504.9	303.3
50	300.0	180.3	10	351.4	211.2	70	402.9	242.1	30	454.3	273.0	90	505.7	303.9
351	300.9	180.8	411	352.3	211.7	471	403.7	242.6	531	455.2	273.5	591	506.6	304.4
52	301.7	181.3	12	353.2	212.2	72	404.6	243.1	32	456.0	274.0	92	507.4	304.9
53	302.6	181.8	13	354.0	212.7	73	405.4	243.6	33	456.9	274.5	93	508.3	305.4
54	303.4	182.3	14	354.9	213.2	74	406.3	244.1	34	457.7	275.0	94	509.2	305.9
55	304.3	182.8	15	355.7	213.7	75	407.2	244.6	35	458.6	275.5	95	510.0	306.4
56	305.2	183.4	16	356.6	214.3	76	408.0	245.2	36	459.4	276.1	96	510.9	307.0
57	306.0	183.9	17	357.4	214.8	77	408.9	245.7	37	460.3	276.6	97	511.7	307.5
58	306.9	184.4	18	358.3	215.3	78	409.7	246.2	38	461.2	277.1	98	512.6	308.0
59	307.7	184.9	19	359.2	215.8	79	410.6	246.7	39	462.0	277.6	99	513.4	308.5
60	308.6	185.4	20	360.0	216.3	80	411.4	247.2	40	462.9	278.1	600	514.3	309.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

59° (121°, 239°, 301°).

TABLE 2.

Difference of Latitude and Departure for 32° (148°, 212°, 328°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.5	61	51.7	32.3	121	102.6	64.1	181	153.5	95.9	241	204.4	127.7
2	1.7	1.1	62	52.6	32.9	22	103.5	64.7	82	154.3	96.4	42	205.2	128.2
3	2.5	1.6	63	53.4	33.4	23	104.3	65.2	83	155.2	97.0	43	206.1	128.8
4	3.4	2.1	64	54.3	33.9	24	105.2	65.7	84	156.0	97.5	44	206.9	129.3
5	4.2	2.6	65	55.1	34.4	25	106.0	66.2	85	156.9	98.0	45	207.8	129.8
6	5.1	3.2	66	56.0	35.0	26	106.9	66.8	86	157.7	98.6	46	208.6	130.4
7	5.9	3.7	67	56.8	35.5	27	107.7	67.3	87	158.6	99.1	47	209.5	130.9
8	6.8	4.2	68	57.7	36.0	28	108.6	67.8	88	159.4	99.6	48	210.3	131.4
9	7.6	4.8	69	58.5	36.6	29	109.4	68.4	89	160.3	100.2	49	211.2	131.9
10	8.5	5.3	70	59.4	37.1	30	110.2	68.9	90	161.1	100.7	50	212.0	132.5
11	9.3	5.8	71	60.2	37.6	131	111.1	69.4	191	162.0	101.2	251	212.9	133.0
12	10.2	6.4	72	61.1	38.2	32	111.9	69.9	92	162.8	101.7	52	213.7	133.5
13	11.0	6.9	73	61.9	38.7	33	112.8	70.5	93	163.7	102.3	53	214.6	134.1
14	11.9	7.4	74	62.8	39.2	34	113.6	71.0	94	164.5	102.8	54	215.4	134.6
15	12.7	7.9	75	63.6	39.7	35	114.5	71.5	95	165.4	103.3	55	216.3	135.1
16	13.6	8.5	76	64.5	40.3	36	115.3	72.1	96	166.2	103.9	56	217.1	135.7
17	14.4	9.0	77	65.3	40.8	37	116.2	72.6	97	167.1	104.4	57	217.9	136.2
18	15.3	9.5	78	66.1	41.3	38	117.0	73.1	98	167.9	104.9	58	218.8	136.7
19	16.1	10.1	79	67.0	41.9	39	117.9	73.7	99	168.8	105.5	59	219.6	137.2
20	17.0	10.6	80	67.8	42.4	40	118.7	74.2	200	169.6	106.0	60	220.5	137.8
21	17.8	11.1	81	68.7	42.9	141	119.6	74.7	201	170.5	106.5	261	221.3	138.3
22	18.7	11.7	82	69.5	43.5	42	120.4	75.2	02	171.3	107.0	62	222.2	138.8
23	19.5	12.2	83	70.4	44.0	43	121.3	75.8	03	172.2	107.6	63	223.0	139.4
24	20.4	12.7	84	71.2	44.5	44	122.1	76.3	04	173.0	108.1	64	223.9	139.9
25	21.2	13.2	85	72.1	45.0	45	123.0	76.8	05	173.8	108.6	65	224.7	140.4
26	22.0	13.8	86	72.9	45.6	46	123.8	77.4	06	174.7	109.2	66	225.6	141.0
27	22.9	14.3	87	73.8	46.1	47	124.7	77.9	07	175.5	109.7	67	226.4	141.5
28	23.7	14.8	88	74.6	46.6	48	125.5	78.4	08	176.4	110.2	68	227.3	142.0
29	24.6	15.4	89	75.5	47.2	49	126.4	79.0	09	177.2	110.8	69	228.1	142.5
30	25.4	15.9	90	76.3	47.7	50	127.2	79.5	10	178.1	111.3	70	229.0	143.1
31	26.3	16.4	91	77.2	48.2	151	128.1	80.0	211	178.9	111.8	271	229.8	143.6
32	27.1	17.0	92	78.0	48.8	52	128.9	80.5	12	179.8	112.3	72	230.7	144.1
33	28.0	17.5	93	78.9	49.3	53	129.8	81.1	13	180.6	112.9	73	231.5	144.7
34	28.8	18.0	94	79.7	49.8	54	130.6	81.6	14	181.5	113.4	74	232.4	145.2
35	29.7	18.5	95	80.6	50.3	55	131.4	82.1	15	182.3	113.9	75	233.2	145.7
36	30.5	19.1	96	81.4	50.9	56	132.3	82.7	16	183.2	114.5	76	234.1	146.3
37	31.4	19.6	97	82.3	51.4	57	133.1	83.2	17	184.0	115.0	77	234.9	146.8
38	32.2	20.1	98	83.1	51.9	58	134.0	83.7	18	184.9	115.5	78	235.8	147.3
39	33.1	20.7	99	84.0	52.5	59	134.8	84.3	19	185.7	116.1	79	236.6	147.8
40	33.9	21.2	100	84.8	53.0	60	135.7	84.8	20	186.6	116.6	80	237.5	148.4
41	34.8	21.7	101	85.7	53.5	161	136.5	85.3	221	187.4	117.1	281	238.3	148.9
42	35.6	22.3	02	86.5	54.1	62	137.4	85.8	22	188.3	117.6	82	239.1	149.4
43	36.5	22.8	03	87.3	54.6	63	138.2	86.4	23	189.1	118.2	83	240.0	150.0
44	37.3	23.3	04	88.2	55.1	64	139.1	86.9	24	190.0	118.7	84	240.8	150.5
45	38.2	23.8	05	89.0	55.6	65	139.9	87.4	25	190.8	119.2	85	241.7	151.0
46	39.0	24.4	06	89.9	56.2	66	140.8	88.0	26	191.7	119.8	86	242.5	151.6
47	39.9	24.9	07	90.7	56.7	67	141.6	88.5	27	192.5	120.3	87	243.4	152.1
48	40.7	25.4	08	91.6	57.2	68	142.5	89.0	28	193.4	120.8	88	244.2	152.6
49	41.6	26.0	09	92.4	57.8	69	143.3	89.6	29	194.2	121.4	89	245.1	153.1
50	42.4	26.5	10	93.3	58.3	70	144.2	90.1	30	195.1	121.9	90	245.9	153.7
51	43.3	27.0	111	94.1	58.8	171	145.0	90.6	231	195.9	122.4	291	246.8	154.2
52	44.1	27.6	12	95.0	59.4	72	145.9	91.1	32	196.7	122.9	92	247.6	154.7
53	44.9	28.1	13	95.8	59.9	73	146.7	91.7	33	197.6	123.5	93	248.5	155.3
54	45.8	28.6	14	96.7	60.4	74	147.6	92.2	34	198.4	124.0	94	249.3	155.8
55	46.6	29.1	15	97.5	60.9	75	148.4	92.7	35	199.3	124.5	95	250.2	156.3
56	47.5	29.7	16	98.4	61.5	76	149.3	93.3	36	200.1	125.1	96	251.0	156.9
57	48.3	30.2	17	99.2	62.0	77	150.1	93.8	37	201.0	125.6	97	251.9	157.4
58	49.2	30.7	18	100.1	62.5	78	151.0	94.3	38	201.8	126.1	98	252.7	157.9
59	50.0	31.3	19	100.9	63.1	79	151.8	94.9	39	202.7	126.7	99	253.6	158.4
60	50.9	31.8	20	101.8	63.6	80	152.6	95.4	40	203.5	127.2	300	254.4	159.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

58° (122°, 238°, 302°).

TABLE 2.

Difference of Latitude and Departure for 32° (148°, 212°, 328°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	255.3	159.5	361	306.2	191.3	421	357.0	223.1	481	407.9	254.9	541	458.8	286.7
02	256.1	160.0	62	307.0	191.8	22	357.9	223.6	82	408.8	255.4	42	459.6	287.2
03	257.0	160.5	63	307.9	192.3	23	358.7	224.1	83	409.6	255.9	43	460.5	287.7
04	257.8	161.1	64	308.7	192.9	24	359.6	224.7	84	410.5	256.5	44	461.3	288.3
05	258.7	161.6	65	309.5	193.4	25	360.4	225.2	85	411.3	257.0	45	462.2	288.8
06	259.5	162.1	66	310.4	193.9	26	361.3	225.7	86	412.2	257.5	46	463.0	289.3
07	260.4	162.7	67	311.2	194.5	27	362.1	226.3	87	413.0	258.1	47	463.9	289.9
08	261.2	163.2	68	312.1	195.0	28	363.0	226.8	88	413.9	258.6	48	464.7	290.4
09	262.1	163.7	69	312.9	195.5	29	363.8	227.3	89	414.7	259.1	49	465.6	290.9
10	262.9	164.3	70	313.8	196.0	30	364.7	227.8	90	415.6	259.6	50	466.4	291.5
311	263.8	164.8	371	314.6	196.6	431	365.5	228.4	491	416.4	260.2	551	467.3	292.0
12	264.6	165.3	72	315.5	197.1	32	366.4	228.9	92	417.3	260.7	52	468.1	292.5
13	265.4	165.8	73	316.3	197.6	33	367.2	229.4	93	418.1	261.2	53	469.0	293.0
14	266.3	166.4	74	317.2	198.2	34	368.1	230.0	94	419.0	261.8	54	469.8	293.6
15	267.1	166.9	75	318.0	198.7	35	368.9	230.5	95	419.8	262.3	55	470.7	294.1
16	268.0	167.4	76	318.9	199.2	36	369.8	231.0	96	420.6	262.8	56	471.5	294.6
17	268.8	168.0	77	319.7	199.8	37	370.6	231.6	97	421.5	263.4	57	472.4	295.2
18	269.7	168.5	78	320.6	200.3	38	371.5	232.1	98	422.3	263.9	58	473.2	295.7
19	270.5	169.0	79	321.4	200.8	39	372.3	232.6	99	423.2	264.4	59	474.1	296.2
20	271.4	169.6	80	322.3	201.3	40	373.2	233.1	500	424.0	265.0	60	474.9	296.7
321	272.2	170.1	381	323.1	201.9	441	374.0	233.7	501	424.9	265.5	561	475.8	297.3
22	273.1	170.6	82	324.0	202.4	42	374.8	234.2	02	425.7	266.0	62	476.6	297.8
23	273.9	171.1	83	324.8	202.9	43	375.7	234.7	03	426.6	266.5	63	477.5	298.3
24	274.8	171.7	84	325.7	203.5	44	376.5	235.3	04	427.4	267.1	64	478.3	298.9
25	275.6	172.2	85	326.5	204.0	45	377.4	235.8	05	428.3	267.6	65	479.2	299.4
26	276.5	172.7	86	327.4	204.5	46	378.2	236.3	06	429.1	268.1	66	480.0	299.9
27	277.3	173.3	87	328.2	205.1	47	379.1	236.9	07	430.0	268.7	67	480.9	300.5
28	278.2	173.8	88	329.1	205.6	48	379.9	237.4	08	430.8	269.2	68	481.7	301.0
29	279.0	174.3	89	329.9	206.1	49	380.8	237.9	09	431.7	269.7	69	482.6	301.5
30	279.9	174.9	90	330.8	206.6	50	381.6	238.4	10	432.5	270.3	70	483.4	302.1
331	280.7	175.4	391	331.6	207.2	451	382.5	239.0	511	433.4	270.8	571	484.3	302.6
32	281.6	175.9	92	332.5	207.7	52	383.3	239.5	12	434.2	271.4	72	485.1	303.2
33	282.4	176.4	93	333.3	208.2	53	384.2	240.0	13	435.1	271.9	73	486.0	303.7
34	283.3	177.0	94	334.2	208.8	54	385.0	240.6	14	435.9	272.4	74	486.8	304.2
35	284.1	177.5	95	335.0	209.3	55	385.9	241.1	15	436.8	272.9	75	487.7	304.7
36	285.0	178.0	96	335.8	209.8	56	386.7	241.6	16	437.6	273.5	76	488.5	305.3
37	285.8	178.6	97	336.7	210.4	57	387.6	242.2	17	438.5	274.0	77	489.4	305.8
38	286.7	179.1	98	337.5	210.9	58	388.4	242.7	18	439.3	274.5	78	490.2	306.3
39	287.5	179.6	99	338.4	211.4	59	389.3	243.2	19	440.2	275.0	79	491.1	306.8
40	288.3	180.2	400	339.2	211.9	60	390.1	243.8	20	441.0	275.6	80	491.9	307.4
341	289.2	180.7	401	340.1	212.5	461	391.0	244.3	521	441.9	276.1	581	492.8	307.9
42	290.0	181.2	02	340.9	213.0	62	391.8	244.8	22	442.7	276.6	82	493.6	308.4
43	290.9	181.7	03	341.8	213.5	63	392.7	245.4	23	443.6	277.2	83	494.5	309.0
44	291.7	182.3	04	342.6	214.1	64	393.5	245.9	24	444.4	277.7	84	495.3	309.5
45	292.6	182.8	05	343.5	214.6	65	394.4	246.4	25	445.3	278.2	85	496.2	310.0
46	293.4	183.3	06	344.3	215.1	66	395.2	246.9	26	446.1	278.7	86	497.0	310.5
47	294.3	183.9	07	345.2	215.7	67	396.0	247.5	27	446.9	279.3	87	497.8	311.1
48	295.1	184.4	08	346.0	216.2	68	396.9	248.0	28	447.8	279.8	88	498.7	311.6
49	296.0	184.9	09	346.9	216.7	69	397.7	248.5	29	448.6	280.3	89	499.5	312.1
50	296.8	185.4	10	347.7	217.2	70	398.6	249.0	30	449.5	280.9	90	500.3	312.6
351	297.7	186.0	411	348.6	217.8	471	399.4	249.6	531	450.3	281.4	591	501.2	313.2
52	298.5	186.5	12	349.4	218.3	72	400.3	250.1	32	451.1	281.9	92	502.0	313.7
53	299.4	187.0	13	350.3	218.8	73	401.1	250.6	33	452.0	282.4	93	502.9	314.2
54	300.2	187.6	14	351.1	219.4	74	402.0	251.2	34	452.8	283.0	94	503.7	314.8
55	301.1	188.1	15	352.0	219.9	75	402.8	251.7	35	453.7	283.5	95	504.6	315.3
56	301.9	188.6	16	352.8	220.4	76	403.7	252.2	36	454.5	284.0	96	505.4	315.8
57	302.8	189.2	17	353.6	221.0	77	404.5	252.8	37	455.4	284.6	97	506.2	316.4
58	303.6	189.7	18	354.5	221.5	78	405.4	253.3	38	456.2	285.1	98	507.1	316.9
59	304.5	190.2	19	355.3	222.0	79	406.2	253.8	39	457.1	285.6	99	508.0	317.4
60	305.3	190.8	20	356.2	222.5	80	407.1	254.3	40	457.9	286.2	600	508.8	318.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

58° (122°, 238°, 302°).

TABLE 2.

Difference of Latitude and Departure for 33° (147°, 213°, 327°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.5	61	51.2	33.2	121	101.5	65.9	181	151.8	98.6	241	202.1	131.3
2	1.7	1.1	62	52.0	33.8	22	102.3	66.4	82	152.6	99.1	42	203.0	131.8
3	2.5	1.6	63	52.8	34.3	23	103.2	67.0	83	153.5	99.7	43	203.8	132.3
4	3.4	2.2	64	53.7	34.9	24	104.0	67.5	84	154.3	100.2	44	204.6	132.9
5	4.2	2.7	65	54.5	35.4	25	104.8	68.1	85	155.2	100.8	45	205.5	133.4
6	5.0	3.3	66	55.4	35.9	26	105.7	68.6	86	156.0	101.3	46	206.3	134.0
7	5.9	3.8	67	56.2	36.5	27	106.5	69.2	87	156.8	101.8	47	207.2	134.5
8	6.7	4.4	68	57.0	37.0	28	107.3	69.7	88	157.7	102.4	48	208.0	135.1
9	7.5	4.9	69	57.9	37.6	29	108.2	70.3	89	158.5	102.9	49	208.8	135.6
10	8.4	5.4	70	58.7	38.1	30	109.0	70.8	90	159.3	103.5	50	209.7	136.2
11	9.2	6.0	71	59.5	38.7	131	109.9	71.3	191	160.2	104.0	251	210.5	136.7
12	10.1	6.5	72	60.4	39.2	32	110.7	71.9	92	161.0	104.6	52	211.3	137.2
13	10.9	7.1	73	61.2	39.8	33	111.5	72.4	93	161.9	105.1	53	212.2	137.8
14	11.7	7.6	74	62.1	40.3	34	112.4	73.0	94	162.7	105.7	54	213.0	138.3
15	12.6	8.2	75	62.9	40.8	35	113.2	73.5	95	163.5	106.2	55	213.9	138.9
16	13.4	8.7	76	63.7	41.4	36	114.1	74.1	96	164.4	106.7	56	214.7	139.4
17	14.3	9.3	77	64.6	41.9	37	114.9	74.6	97	165.2	107.3	57	215.5	140.0
18	15.1	9.8	78	65.4	42.5	38	115.7	75.2	98	166.1	107.8	58	216.4	140.5
19	15.9	10.3	79	66.3	43.0	39	116.6	75.7	99	166.9	108.4	59	217.2	141.1
20	16.8	10.9	80	67.1	43.6	40	117.4	76.2	200	167.7	108.9	60	218.1	141.6
21	17.6	11.4	81	67.9	44.1	141	118.3	76.8	201	168.6	109.5	261	218.9	142.2
22	18.5	12.0	82	68.8	44.7	42	119.1	77.3	02	169.4	110.0	62	219.7	142.7
23	19.3	12.5	83	69.6	45.2	43	119.9	77.9	03	170.3	110.6	63	220.6	143.2
24	20.1	13.1	84	70.4	45.7	44	120.8	78.4	04	171.1	111.1	64	221.4	143.8
25	21.0	13.6	85	71.3	46.3	45	121.6	79.0	05	171.9	111.7	65	222.2	144.3
26	21.8	14.2	86	72.1	46.8	46	122.4	79.5	06	172.2	112.2	66	223.1	144.9
27	22.6	14.7	87	73.0	47.4	47	123.3	80.1	07	173.6	112.7	67	223.9	145.4
28	23.5	15.2	88	73.8	47.9	48	124.1	80.6	08	174.4	113.3	68	224.8	146.0
29	24.3	15.8	89	74.6	48.5	49	125.0	81.2	09	175.3	113.8	69	225.6	146.5
30	25.2	16.3	90	75.5	49.0	50	125.8	81.7	10	176.1	114.4	70	226.4	147.1
31	26.0	16.9	91	76.3	49.6	151	126.6	82.2	211	177.0	114.9	271	227.3	147.6
32	26.8	17.4	92	77.2	50.1	52	127.5	82.8	12	177.8	115.5	72	228.1	148.1
33	27.7	18.0	93	78.0	50.7	53	128.3	83.3	13	178.6	116.0	73	229.0	148.7
34	28.5	18.5	94	78.8	51.2	54	129.2	83.9	14	179.5	116.6	74	229.8	149.2
35	29.4	19.1	95	79.7	51.7	55	130.0	84.4	15	180.3	117.1	75	230.6	149.8
36	30.2	19.6	96	80.5	52.3	56	130.8	85.0	16	181.2	117.6	76	231.5	150.3
37	31.0	20.2	97	81.4	52.8	57	131.7	85.5	17	182.0	118.2	77	232.3	150.9
38	31.9	20.7	98	82.2	53.4	58	132.5	86.1	18	182.8	118.7	78	233.2	151.4
39	32.7	21.2	99	83.0	53.9	59	133.3	86.6	19	183.7	119.3	79	234.0	152.0
40	33.5	21.8	100	83.9	54.5	60	134.2	87.1	20	184.5	119.8	80	234.8	152.5
41	34.4	22.3	101	84.7	55.0	161	135.0	87.7	221	185.3	120.4	281	235.7	153.0
42	35.2	22.9	02	85.5	55.6	62	135.9	88.2	22	186.2	120.9	82	236.5	153.6
43	36.1	23.4	03	86.4	56.1	63	136.7	88.8	23	187.0	121.5	83	237.3	154.1
44	36.9	24.0	04	87.2	56.6	64	137.5	89.3	24	187.9	122.0	84	238.2	154.7
45	37.7	24.5	05	88.1	57.2	65	138.4	89.9	25	188.7	122.5	85	239.0	155.2
46	38.6	25.1	06	88.9	57.7	66	139.2	90.4	26	189.5	123.1	86	239.9	155.8
47	39.4	25.6	07	89.7	58.3	67	140.1	91.0	27	190.4	123.6	87	240.7	156.3
48	40.3	26.1	08	90.6	58.8	68	140.9	91.5	28	191.2	124.2	88	241.5	156.9
49	41.1	26.7	09	91.4	59.4	69	141.7	92.0	29	192.1	124.7	89	242.4	157.4
50	41.9	27.2	10	92.3	59.9	70	142.6	92.6	30	192.9	125.3	90	243.2	157.9
51	42.8	27.8	111	93.1	60.5	171	143.4	93.1	231	193.7	125.8	291	244.1	158.5
52	43.6	28.3	12	93.9	61.0	72	144.3	93.7	32	194.6	126.4	92	244.9	159.0
53	44.4	28.9	13	94.8	61.5	73	145.1	94.2	33	195.4	126.9	93	245.7	159.6
54	45.3	29.4	14	95.6	62.1	74	145.9	94.8	34	196.2	127.4	94	246.6	160.1
55	46.1	30.0	15	96.4	62.6	75	146.8	95.3	35	197.1	128.0	95	247.4	160.7
56	47.0	30.5	16	97.3	63.2	76	147.6	95.9	36	197.9	128.5	96	248.2	161.2
57	47.8	31.0	17	98.1	63.7	77	148.4	96.4	37	198.8	129.1	97	249.1	161.8
58	48.6	31.6	18	99.0	64.3	78	149.3	96.9	38	199.6	129.6	98	249.9	162.3
59	49.5	32.1	19	99.8	64.8	79	150.1	97.5	39	200.4	130.2	99	250.8	162.8
60	50.3	32.7	20	100.6	65.4	80	151.0	98.0	40	201.3	130.7	300	251.6	163.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

57° (123°, 237°, 303°).

Difference of Latitude and Departure for 33° (147°, 213°, 327°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	252.4	163.9	361	302.8	196.6	421	353.1	229.3	481	403.4	262.0	541	453.7	294.6
02	253.3	164.4	62	303.6	197.1	22	353.9	229.8	82	404.2	262.5	42	454.6	295.2
03	254.1	165.0	63	304.4	197.7	23	354.7	230.4	83	405.1	263.1	43	455.4	295.7
04	255.0	165.5	64	305.3	198.2	24	355.6	230.9	84	405.9	263.6	44	456.2	296.2
05	255.8	166.1	65	306.1	198.8	25	356.4	231.4	85	406.7	264.1	45	457.1	296.8
06	256.6	166.6	66	307.0	199.3	26	357.3	232.0	86	407.6	264.7	46	457.9	297.3
07	257.5	167.2	67	307.8	199.8	27	358.1	232.5	87	408.4	265.2	47	458.8	297.9
08	258.3	167.7	68	308.6	200.4	28	359.0	233.1	88	409.3	265.8	48	459.6	298.4
09	259.2	168.3	69	309.5	200.9	29	359.8	233.6	89	410.1	266.3	49	460.4	299.0
10	260.0	168.8	70	310.3	201.5	30	360.6	234.2	90	411.0	266.8	50	461.3	299.5
311	260.8	169.3	371	311.2	202.0	431	361.5	234.7	491	411.8	267.4	551	462.1	300.1
12	261.7	169.9	72	312.0	202.6	32	362.3	235.2	92	412.6	267.9	52	463.0	300.6
13	262.5	170.4	73	312.8	203.1	33	363.1	235.8	93	413.5	268.5	53	463.8	301.2
14	263.3	171.0	74	313.7	203.7	34	364.0	236.3	94	414.3	269.0	54	464.6	301.7
15	264.2	171.5	75	314.5	204.2	35	364.8	236.9	95	415.1	269.6	55	465.5	302.3
16	265.0	172.1	76	315.3	204.7	36	365.7	237.4	96	416.0	270.1	56	466.3	302.9
17	265.9	172.6	77	316.2	205.3	37	366.5	238.0	97	416.8	270.7	57	467.2	303.4
18	266.7	173.2	78	317.0	205.8	38	367.3	238.5	98	417.6	271.2	58	468.0	303.9
19	267.5	173.7	79	317.9	206.4	39	368.2	239.1	99	418.5	271.8	59	468.8	304.5
20	268.4	174.2	80	318.7	206.9	40	369.0	239.6	500	419.3	272.3	60	469.7	305.0
321	269.2	174.8	381	319.5	207.5	441	369.9	240.1	501	420.2	272.8	561	470.5	305.5
22	270.1	175.3	82	320.4	208.0	42	370.7	240.7	02	421.0	273.4	62	471.3	306.1
23	270.9	175.9	83	321.2	208.6	43	371.5	241.2	03	421.9	273.9	63	472.2	306.6
24	271.7	176.4	84	322.1	209.1	44	372.4	241.8	04	422.7	274.5	64	473.0	307.2
25	272.6	177.0	85	322.9	209.6	45	373.2	242.3	05	423.5	275.0	65	473.8	307.7
26	273.4	177.5	86	323.7	210.2	46	374.1	242.9	06	424.4	275.6	66	474.7	308.3
27	274.2	178.1	87	324.6	210.7	47	374.9	243.4	07	425.2	276.1	67	475.5	308.8
28	275.1	178.6	88	325.4	211.3	48	375.7	244.0	08	426.0	276.7	68	476.4	309.4
29	275.9	179.1	89	326.2	211.8	49	376.6	244.5	09	426.9	277.2	69	477.2	309.9
30	276.8	179.7	90	327.1	212.4	50	377.4	245.1	10	427.7	277.8	70	478.0	310.4
331	277.6	180.2	391	327.9	212.9	451	378.2	245.6	511	428.5	278.3	571	478.9	311.0
32	278.4	180.8	92	328.8	213.5	52	379.1	246.1	12	429.4	278.8	72	479.7	311.5
33	279.3	181.3	93	329.6	214.0	53	379.9	246.7	13	430.2	279.4	73	480.6	312.0
34	280.1	181.9	94	330.4	214.6	54	380.8	247.2	14	431.1	279.9	74	481.4	312.6
35	281.0	182.4	95	331.3	215.1	55	381.6	247.8	15	431.9	280.4	75	482.2	313.1
36	281.8	183.0	96	332.1	215.6	56	382.4	248.3	16	432.7	281.0	76	483.1	313.7
37	282.6	183.5	97	333.0	216.2	57	383.3	248.9	17	433.6	281.5	77	483.9	314.2
38	283.5	184.1	98	333.8	216.7	58	384.1	249.4	18	434.4	282.1	78	484.7	314.8
39	284.3	184.6	99	334.6	217.3	59	385.0	250.0	19	435.3	282.6	79	485.6	315.3
40	285.2	185.1	400	335.5	217.8	60	385.8	250.5	20	436.1	283.2	80	486.4	315.9
341	286.0	185.7	401	336.3	218.4	461	386.6	251.0	521	436.9	283.7	581	487.2	316.4
42	286.8	186.2	02	337.1	218.9	62	387.5	251.6	22	437.8	284.3	82	488.1	317.0
43	287.7	186.8	03	338.0	219.5	63	388.3	252.1	23	438.6	284.8	83	488.9	317.5
44	288.5	187.3	04	338.8	220.0	64	389.1	252.7	24	439.4	285.4	84	489.8	318.1
45	289.3	187.9	05	339.7	220.5	65	390.0	253.2	25	440.3	285.9	85	490.6	318.6
46	290.2	188.4	06	340.5	221.1	66	390.8	253.8	26	441.1	286.5	86	491.5	319.2
47	291.0	189.0	07	341.3	221.6	67	391.7	254.3	27	442.0	287.0	87	492.3	319.7
48	291.9	189.5	08	342.2	222.2	68	392.5	254.9	28	442.8	287.5	88	493.1	320.2
49	292.7	190.0	09	343.0	222.7	69	393.3	255.4	29	443.6	288.1	89	494.0	320.8
50	293.5	190.6	10	343.9	223.3	70	394.2	255.9	30	444.5	288.6	90	494.8	321.3
351	294.4	191.1	411	344.7	223.8	471	395.0	256.5	531	445.3	289.2	591	495.7	321.9
52	295.2	191.7	12	345.5	224.4	72	395.8	257.0	32	446.1	289.7	92	496.5	322.4
53	296.1	192.2	13	346.4	224.9	73	396.7	257.6	33	447.0	290.3	93	497.3	322.9
54	296.9	192.8	14	347.2	225.4	74	397.5	258.1	34	447.8	290.8	94	498.1	323.5
55	297.7	193.3	15	348.1	226.0	75	398.3	258.7	35	448.7	291.4	95	499.0	324.1
56	298.6	193.9	16	348.9	226.5	76	399.2	259.2	36	449.5	291.9	96	499.8	324.6
57	299.4	194.4	17	349.7	227.1	77	400.0	259.8	37	450.3	292.5	97	500.6	325.1
58	300.2	194.9	18	350.6	227.6	78	400.9	260.3	38	451.2	293.0	98	501.5	325.7
59	301.1	195.5	19	351.4	228.2	79	401.7	260.9	39	452.0	293.6	99	502.3	326.2
60	301.9	196.0	20	352.2	228.7	80	402.6	261.4	40	452.9	294.1	600	503.2	326.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

57° (123°, 237°, 303°).

6583—06——28

TABLE 2.

Difference of Latitude and Departure for 34° (146°, 214°, 326°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	50.6	34.1	121	100.3	67.7	181	150.1	101.2	241	199.8	134.8
2	1.7	1.1	62	51.4	34.7	22	101.1	68.2	82	150.9	101.8	42	200.6	135.3
3	2.5	1.7	63	52.2	35.2	23	102.0	68.8	83	151.7	102.3	43	201.5	135.9
4	3.3	2.2	64	53.1	35.8	24	102.8	69.3	84	152.5	102.9	44	202.3	136.4
5	4.1	2.8	65	53.9	36.3	25	103.6	69.9	85	153.4	103.5	45	203.1	137.0
6	5.0	3.4	66	54.7	36.9	26	104.5	70.5	86	154.2	104.0	46	203.9	137.6
7	5.8	3.9	67	55.5	37.5	27	105.3	71.0	87	155.0	104.6	47	204.8	138.1
8	6.6	4.5	68	56.4	38.0	28	106.1	71.6	88	155.9	105.1	48	205.6	138.7
9	7.5	5.0	69	57.2	38.6	29	106.9	72.1	89	156.7	105.7	49	206.4	139.2
10	8.3	5.6	70	58.0	39.1	30	107.8	72.7	90	157.5	106.2	50	207.3	139.8
11	9.1	6.2	71	58.9	39.7	131	108.6	73.3	191	158.3	106.8	251	208.1	140.4
12	9.9	6.7	72	59.7	40.3	32	109.4	73.8	92	159.2	107.4	52	208.9	140.9
13	10.8	7.3	73	60.5	40.8	33	110.3	74.4	93	160.0	107.9	53	209.7	141.5
14	11.6	7.8	74	61.3	41.4	34	111.1	74.9	94	160.8	108.5	54	210.6	142.0
15	12.4	8.4	75	62.2	41.9	35	111.9	75.5	95	161.7	109.0	55	211.4	142.6
16	13.3	8.9	76	63.0	42.5	36	112.7	76.1	96	162.5	109.6	56	212.2	143.2
17	14.1	9.5	77	63.8	43.1	37	113.6	76.6	97	163.3	110.2	57	213.1	143.7
18	14.9	10.1	78	64.7	43.6	38	114.4	77.2	98	164.1	110.7	58	213.9	144.3
19	15.8	10.6	79	65.5	44.2	39	115.2	77.7	99	165.0	111.3	59	214.7	144.8
20	16.6	11.2	80	66.3	44.7	40	116.1	78.3	200	165.8	111.8	60	215.5	145.4
21	17.4	11.7	81	67.2	45.3	141	116.9	78.8	201	166.6	112.4	261	216.4	145.9
22	18.2	12.3	82	68.0	45.9	42	117.7	79.4	02	167.5	113.0	62	217.2	146.5
23	19.1	12.9	83	68.8	46.4	43	118.6	80.0	03	168.3	113.5	63	218.0	147.1
24	19.9	13.4	84	69.6	47.0	44	119.4	80.5	04	169.1	114.1	64	218.9	147.6
25	20.7	14.0	85	70.5	47.5	45	120.2	81.1	05	170.0	114.6	65	219.7	148.2
26	21.6	14.5	86	71.3	48.1	46	121.0	81.6	06	170.8	115.2	66	220.5	148.7
27	22.4	15.1	87	72.1	48.6	47	121.9	82.2	07	171.6	115.8	67	221.4	149.3
28	23.2	15.7	88	73.0	49.2	48	122.7	82.8	08	172.4	116.3	68	222.2	149.9
29	24.0	16.2	89	73.8	49.8	49	123.5	83.3	09	173.3	116.9	69	223.0	150.4
30	24.9	16.8	90	74.6	50.3	50	124.4	83.9	10	174.1	117.4	70	223.8	151.0
31	25.7	17.3	91	75.4	50.9	151	125.2	84.4	211	174.9	118.0	271	224.7	151.5
32	26.5	17.9	92	76.3	51.4	52	126.0	85.0	12	175.8	118.5	72	225.5	152.1
33	27.4	18.5	93	77.1	52.0	53	126.8	85.6	13	176.6	119.1	73	226.3	152.7
34	28.2	19.0	94	77.9	52.6	54	127.7	86.1	14	177.4	119.7	74	227.2	153.2
35	29.0	19.6	95	78.8	53.1	55	128.5	86.7	15	178.2	120.2	75	228.0	153.8
36	29.8	20.1	96	79.6	53.7	56	129.3	87.2	16	179.1	120.8	76	228.8	154.3
37	30.7	20.7	97	80.4	54.2	57	130.2	87.8	17	179.9	121.3	77	229.6	154.9
38	31.5	21.2	98	81.2	54.8	58	131.0	88.4	18	180.7	121.9	78	230.5	155.5
39	32.3	21.8	99	82.1	55.4	59	131.8	88.9	19	181.6	122.5	79	231.3	156.0
40	33.2	22.4	100	82.9	55.9	60	132.6	89.5	20	182.4	123.0	80	232.1	156.6
41	34.0	22.9	101	83.7	56.5	161	133.5	90.0	221	183.2	123.6	281	233.0	157.1
42	34.8	23.5	02	84.6	57.0	62	134.3	90.6	22	184.0	124.1	82	233.8	157.7
43	35.6	24.0	03	85.4	57.6	63	135.1	91.1	23	184.9	124.7	83	234.6	158.3
44	36.5	24.6	04	86.2	58.2	64	136.0	91.7	24	185.7	125.3	84	235.4	158.8
45	37.3	25.2	05	87.0	58.7	65	136.8	92.3	25	186.5	125.8	85	236.3	159.4
46	38.1	25.7	06	87.9	59.3	66	137.6	92.8	26	187.4	126.4	86	237.1	159.9
47	39.0	26.3	07	88.7	59.8	67	138.4	93.4	27	188.2	126.9	87	237.9	160.5
48	39.8	26.8	08	89.5	60.4	68	139.3	93.9	28	189.0	127.5	88	238.8	161.0
49	40.6	27.4	09	90.4	61.0	69	140.1	94.5	29	189.8	128.1	89	239.6	161.6
50	41.5	28.0	10	91.2	61.5	70	140.9	95.1	30	190.7	128.6	90	240.4	162.2
51	42.3	28.5	111	92.0	62.1	171	141.8	95.6	231	191.5	129.2	291	241.2	162.7
52	43.1	29.1	12	92.9	62.6	72	142.6	96.2	32	192.3	129.7	92	242.1	163.3
53	43.9	29.6	13	93.7	63.2	73	143.4	96.7	33	193.2	130.3	93	242.9	163.8
54	44.8	30.2	14	94.5	63.7	74	144.3	97.3	34	194.0	130.9	94	243.7	164.4
55	45.6	30.8	15	95.3	64.3	75	145.1	97.9	35	194.8	131.4	95	244.6	165.0
56	46.4	31.3	16	96.2	64.9	76	145.9	98.4	36	195.7	132.0	96	245.4	165.5
57	47.3	31.9	17	97.0	65.4	77	146.7	99.0	37	196.5	132.5	97	246.2	166.1
58	48.1	32.4	18	97.8	66.0	78	147.6	99.5	38	197.3	133.1	98	247.1	166.6
59	48.9	33.0	19	98.7	66.5	79	148.4	100.1	39	198.1	133.6	99	247.9	167.2
60	49.7	33.6	20	99.5	67.1	80	149.2	100.7	40	199.0	134.2	300	248.7	167.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

56° (124°, 236°, 304°).

Difference of Latitude and Departure for 34° (146°, 214°, 326°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	249.5	168.3	361	299.3	201.9	421	349.0	235.4	481	398.8	269.0	541	448.5	302.5
02	250.4	168.9	62	300.1	202.4	22	349.9	236.0	82	399.6	269.5	42	449.4	303.1
03	251.2	169.4	63	300.9	203.0	23	350.7	236.5	83	400.4	270.1	43	450.2	303.6
04	252.0	170.0	64	301.8	203.5	24	351.5	237.1	84	401.3	270.6	44	451.0	304.2
05	252.9	170.6	65	302.6	204.1	25	352.3	237.7	85	402.1	271.2	45	451.8	304.8
06	253.7	171.1	66	303.4	204.7	26	353.2	238.2	86	402.9	271.8	46	452.6	305.3
07	254.5	171.7	67	304.3	205.2	27	354.0	238.8	87	403.8	272.3	47	453.5	305.9
08	255.3	172.2	68	305.1	205.8	28	354.8	239.3	88	404.6	272.8	48	454.3	306.4
09	256.2	172.8	69	305.9	206.3	29	355.7	239.9	89	405.4	273.4	49	455.2	307.0
10	257.0	173.3	70	306.7	206.9	30	356.5	240.4	90	406.2	274.0	50	456.0	307.5
311	257.8	173.9	371	307.6	207.5	431	357.3	241.0	491	407.1	274.6	551	456.8	308.1
12	258.7	174.5	72	308.4	208.0	32	358.1	241.6	92	407.9	275.1	52	457.6	308.7
13	259.5	175.0	73	309.2	208.6	33	359.0	242.1	93	408.7	275.7	53	458.4	309.2
14	260.3	175.6	74	310.1	209.1	34	359.8	242.7	94	409.5	276.2	54	459.3	309.8
15	261.2	176.1	75	310.9	209.7	35	360.6	243.2	95	410.4	276.8	55	460.1	310.3
16	262.0	176.7	76	311.7	210.3	36	361.5	243.8	96	411.2	277.4	56	460.9	310.9
17	262.8	177.3	77	312.6	210.8	37	362.3	244.4	97	412.0	277.9	57	461.7	311.5
18	263.7	177.8	78	313.4	211.4	38	363.1	244.9	98	412.8	278.4	58	462.6	312.0
19	264.5	178.4	79	314.2	211.9	39	364.0	245.5	99	413.7	279.0	59	463.4	312.6
20	265.3	178.9	80	315.0	212.5	40	364.8	246.0	500	414.5	279.6	60	464.2	313.1
321	266.1	179.5	381	315.9	213.0	441	365.6	246.6	501	415.3	280.1	561	465.1	313.7
22	267.0	180.1	82	316.7	213.6	42	366.4	247.2	02	416.2	280.7	62	465.9	314.3
23	267.8	180.6	83	317.5	214.2	43	367.3	247.7	03	417.0	281.3	63	466.8	314.8
24	268.6	181.2	84	318.4	214.7	44	368.1	248.3	04	417.8	281.8	64	467.6	315.4
25	269.5	181.7	85	319.2	215.3	45	368.9	248.8	05	418.6	282.4	65	468.4	315.9
26	270.3	182.3	86	320.0	215.8	46	369.8	249.4	06	419.4	282.9	66	469.2	316.5
27	271.1	182.9	87	320.8	216.4	47	370.6	250.0	07	420.3	283.5	67	470.1	317.1
28	271.9	183.4	88	321.7	217.0	48	371.4	250.5	08	421.1	284.1	68	470.9	317.6
29	272.8	184.0	89	322.5	217.5	49	372.2	251.1	09	421.9	284.6	69	471.7	318.2
30	273.6	184.5	90	323.3	218.1	50	373.1	251.6	10	422.8	285.2	70	472.6	318.7
331	274.4	185.1	391	324.2	218.6	451	373.9	252.2	511	423.6	285.8	571	473.4	319.3
32	275.2	185.6	92	325.0	219.2	52	374.7	252.8	12	424.4	286.3	72	474.2	319.9
33	276.1	186.2	93	325.8	219.8	53	375.6	253.3	13	425.3	286.9	73	475.0	320.4
34	276.9	186.8	94	326.6	220.3	54	376.4	253.9	14	426.1	287.4	74	475.9	321.0
35	277.7	187.3	95	327.5	220.9	55	377.2	254.4	15	426.9	288.0	75	476.7	321.5
36	278.6	187.9	96	328.3	221.4	56	378.0	255.0	16	427.8	288.5	76	477.5	322.1
37	279.4	188.4	97	329.1	222.0	57	378.9	255.5	17	428.6	289.1	77	478.3	322.7
38	280.2	189.0	98	330.0	222.6	58	379.7	256.1	18	429.4	289.6	78	479.2	323.2
39	281.0	189.6	99	330.8	223.1	59	380.5	256.7	19	430.3	290.2	79	480.0	323.8
40	281.9	190.1	400	331.6	223.7	60	381.3	257.2	20	431.1	290.8	80	480.8	324.3
341	282.7	190.7	401	332.4	224.2	461	382.2	257.8	521	431.9	291.3	581	481.6	324.9
42	283.5	191.2	02	333.3	224.8	62	383.0	258.3	22	432.8	291.9	82	482.5	325.4
43	284.4	191.8	03	334.1	225.4	63	383.8	258.9	23	433.6	292.5	83	483.3	326.0
44	285.2	192.4	04	334.9	225.9	64	384.7	259.5	24	434.4	293.0	84	484.1	326.6
45	286.0	192.9	05	335.8	226.5	65	385.5	260.0	25	435.3	293.6	85	485.0	327.2
46	286.9	193.5	06	336.6	227.0	66	386.3	260.6	26	436.1	294.1	86	485.8	327.7
47	287.7	194.0	07	337.4	227.6	67	387.2	261.1	27	436.9	294.7	87	486.6	328.2
48	288.5	194.6	08	338.3	228.1	68	388.0	261.7	28	437.8	295.3	88	487.5	328.8
49	289.3	195.2	09	339.1	228.7	69	388.8	262.3	29	438.6	295.8	89	488.3	329.4
50	290.2	195.7	10	339.9	229.3	70	389.7	262.8	30	439.4	296.4	90	489.2	329.9
351	291.0	196.3	411	340.7	229.8	471	390.5	263.4	531	440.3	296.9	591	490.0	330.5
52	291.8	196.8	12	341.6	230.4	72	391.3	263.9	32	441.1	297.4	92	490.8	331.0
53	292.7	197.4	13	342.4	230.9	73	392.1	264.5	33	441.9	298.0	93	491.6	331.6
54	293.5	198.0	14	343.2	231.5	74	393.0	265.0	34	442.7	298.6	94	492.5	332.2
55	294.3	198.5	15	344.1	232.1	75	393.8	265.6	35	443.6	299.1	95	493.3	332.7
56	295.1	199.1	16	344.9	232.6	76	394.6	266.2	36	444.4	299.7	96	494.1	333.3
57	296.0	199.6	17	345.7	233.2	77	395.5	266.7	37	445.3	300.2	97	494.9	333.8
58	296.8	200.2	18	346.5	233.7	78	396.3	267.3	38	446.1	300.8	98	495.8	334.4
59	297.6	200.7	19	347.4	234.3	79	397.1	267.9	39	446.9	301.4	99	496.6	334.9
60	298.5	201.3	20	348.2	234.9	80	397.9	268.4	40	447.7	302.0	600	497.4	335.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

56° (124°, 236°, 304°).

TABLE 2.

Difference of Latitude and Departure for 35° (145°, 215°, 325°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	50.0	35.0	121	99.1	69.4	181	148.3	103.8	241	197.4	138.2
2	1.6	1.1	62	50.8	35.6	22	99.9	70.0	82	149.1	104.4	42	198.2	138.8
3	2.5	1.7	63	51.6	36.1	23	100.8	70.5	83	149.9	105.0	43	199.1	139.4
4	3.3	2.3	64	52.4	36.7	24	101.6	71.1	84	150.7	105.5	44	199.9	140.0
5	4.1	2.9	65	53.2	37.3	25	102.4	71.7	85	151.5	106.1	45	200.7	140.5
6	4.9	3.4	66	54.1	37.9	26	103.2	72.3	86	152.4	106.7	46	201.5	141.1
7	5.7	4.0	67	54.9	38.4	27	104.0	72.8	87	153.2	107.3	47	202.3	141.7
8	6.6	4.6	68	55.7	39.0	28	104.9	73.4	88	154.0	107.8	48	203.1	142.2
9	7.4	5.2	69	56.5	39.6	29	105.7	74.0	89	154.8	108.4	49	204.0	142.8
10	8.2	5.7	70	57.3	40.2	30	106.5	74.6	90	155.6	109.0	50	204.8	143.4
11	9.0	6.3	71	58.2	40.7	131	107.3	75.1	191	156.5	109.6	251	205.6	144.0
12	9.8	6.9	72	59.0	41.3	32	108.1	75.7	92	157.3	110.1	52	206.4	144.5
13	10.6	7.5	73	59.8	41.9	33	108.9	76.3	93	158.1	110.7	53	207.2	145.1
14	11.5	8.0	74	60.6	42.4	34	109.8	76.9	94	158.9	111.3	54	208.1	145.7
15	12.3	8.6	75	61.4	43.0	35	110.6	77.4	95	159.7	111.8	55	208.9	146.3
16	13.1	9.2	76	62.3	43.6	36	111.4	78.0	96	160.6	112.4	56	209.7	146.8
17	13.9	9.8	77	63.1	44.2	37	112.2	78.6	97	161.4	113.0	57	210.5	147.4
18	14.7	10.3	78	63.9	44.7	38	113.0	79.2	98	162.2	113.6	58	211.3	148.0
19	15.6	10.9	79	64.7	45.3	39	113.9	79.7	99	163.0	114.1	59	212.2	148.6
20	16.4	11.5	80	65.5	45.9	40	114.7	80.3	200	163.8	114.7	60	213.0	149.1
21	17.2	12.0	81	66.4	46.5	141	115.5	80.9	201	164.6	115.3	261	213.8	149.7
22	18.0	12.6	82	67.2	47.0	42	116.3	81.4	02	165.5	115.9	62	214.6	150.3
23	18.8	13.2	83	68.0	47.6	43	117.1	82.0	03	166.3	116.4	63	215.4	150.9
24	19.7	13.8	84	68.8	48.2	44	118.0	82.6	04	167.1	117.0	64	216.3	151.4
25	20.5	14.3	85	69.6	48.8	45	118.8	83.2	05	167.9	117.6	65	217.1	152.0
26	21.3	14.9	86	70.4	49.3	46	119.6	83.7	06	168.7	118.2	66	217.9	152.6
27	22.1	15.5	87	71.3	49.9	47	120.4	84.3	07	169.6	118.7	67	218.7	153.1
28	22.9	16.1	88	72.1	50.5	48	121.2	84.9	08	170.4	119.3	68	219.5	153.7
29	23.8	16.6	89	72.9	51.0	49	122.1	85.5	09	171.2	119.9	69	220.4	154.3
30	24.6	17.2	90	73.7	51.6	50	122.9	86.0	10	172.0	120.5	70	221.2	154.9
31	25.4	17.8	91	74.5	52.2	151	123.7	86.6	211	172.8	121.0	271	222.0	155.4
32	26.2	18.4	92	75.4	52.8	52	124.5	87.2	12	173.7	121.6	72	222.8	156.0
33	27.0	18.9	93	76.2	53.3	53	125.3	87.8	13	174.5	122.2	73	223.6	156.6
34	27.9	19.5	94	77.0	53.9	54	126.1	88.3	14	175.3	122.7	74	224.4	157.2
35	28.7	20.1	95	77.8	54.5	55	127.0	88.9	15	176.1	123.3	75	225.3	157.7
36	29.5	20.6	96	78.6	55.1	56	127.8	89.5	16	176.9	123.9	76	226.1	158.3
37	30.3	21.2	97	79.5	55.6	57	128.6	90.1	17	177.8	124.5	77	226.9	158.9
38	31.1	21.8	98	80.3	56.2	58	129.4	90.6	18	178.6	125.0	78	227.7	159.5
39	31.9	22.4	99	81.1	56.8	59	130.2	91.2	19	179.4	125.6	79	228.5	160.0
40	32.8	22.9	100	81.9	57.4	60	131.1	91.8	20	180.2	126.2	80	229.4	160.6
41	33.6	23.5	101	82.7	57.9	161	131.9	92.3	221	181.0	126.8	281	230.2	161.2
42	34.4	24.1	02	83.6	58.5	62	132.7	92.9	22	181.9	127.3	82	231.0	161.7
43	35.2	24.7	03	84.4	59.1	63	133.5	93.5	23	182.7	127.9	83	231.8	162.3
44	36.0	25.2	04	85.2	59.7	64	134.3	94.1	24	183.5	128.5	84	232.6	162.9
45	36.9	25.8	05	86.0	60.2	65	135.2	94.6	25	184.3	129.1	85	233.5	163.5
46	37.7	26.4	06	86.8	60.8	66	136.0	95.2	26	185.1	129.6	86	234.3	164.0
47	38.5	27.0	07	87.6	61.4	67	136.8	95.8	27	185.9	130.2	87	235.1	164.6
48	39.3	27.5	08	88.5	61.9	68	137.6	96.4	28	186.8	130.8	88	235.9	165.2
49	40.1	28.1	09	89.3	62.5	69	138.4	96.9	29	187.6	131.3	89	236.7	165.8
50	41.0	28.7	10	90.1	63.1	70	139.3	97.5	30	188.4	131.9	90	237.6	166.3
51	41.8	29.3	111	90.9	63.7	171	140.1	98.1	231	189.2	132.5	291	238.4	166.9
52	42.6	29.8	12	91.7	64.2	72	140.9	98.7	32	190.0	133.1	92	239.2	167.5
53	43.4	30.4	13	92.6	64.8	73	141.7	99.2	33	190.9	133.6	93	240.0	168.1
54	44.2	31.0	14	93.4	65.4	74	142.5	99.8	34	191.7	134.2	94	240.8	168.6
55	45.1	31.5	15	94.2	66.0	75	143.4	100.4	35	192.5	134.8	95	241.6	169.2
56	45.9	32.1	16	95.0	66.5	76	144.2	100.9	36	193.3	135.4	96	242.5	169.8
57	46.7	32.7	17	95.8	67.1	77	145.0	101.5	37	194.1	135.9	97	243.3	170.4
58	47.5	33.3	18	96.7	67.7	78	145.8	102.1	38	195.0	136.5	98	244.1	170.9
59	48.3	33.8	19	97.5	68.3	79	146.6	102.7	39	195.8	137.1	99	244.9	171.5
60	49.1	34.4	20	98.3	68.8	80	147.4	103.2	40	196.6	137.7	300	245.7	172.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

55° (125°, 235°, 305°).

TABLE 2.

Difference of Latitude and Departure for 35° (145°, 215°, 325°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	246.6	172.6	361	295.7	207.0	421	344.9	241.5	481	394.0	275.9	541	443.2	310.3
02	247.4	173.2	62	296.5	207.6	22	345.7	242.0	82	394.8	276.4	42	444.0	310.9
03	248.2	173.8	63	297.4	208.2	23	346.5	242.6	83	395.7	277.0	43	444.8	311.4
04	249.0	174.3	64	298.2	208.8	24	347.3	243.2	84	396.5	277.6	44	445.6	312.0
05	249.9	174.9	65	299.0	209.3	25	348.1	243.8	85	397.3	278.2	45	446.4	312.6
06	250.7	175.5	66	299.8	209.9	26	349.0	244.3	86	398.1	278.7	46	447.3	313.2
07	251.5	176.1	67	300.6	210.5	27	349.8	244.9	87	398.9	279.3	47	448.1	313.7
08	252.3	176.6	68	301.5	211.1	28	350.6	245.5	88	399.8	279.9	48	448.9	314.3
09	253.1	177.2	69	302.3	211.6	29	351.4	246.0	89	400.6	280.5	49	449.7	314.9
10	253.9	177.8	70	303.1	212.2	30	352.2	246.6	90	401.4	281.0	50	450.5	315.4
311	254.8	178.4	371	303.9	212.8	431	353.1	247.2	491	402.2	281.6	551	451.4	316.0
12	255.6	178.9	72	304.7	213.4	32	353.9	247.8	92	403.0	282.2	52	452.2	316.6
13	256.4	179.5	73	305.6	213.9	33	354.7	248.3	93	403.9	282.8	53	453.0	317.2
14	257.2	180.1	74	306.4	214.5	34	355.5	248.9	94	404.7	283.3	54	453.8	317.7
15	258.0	180.7	75	307.2	215.1	35	356.3	249.5	95	405.5	283.9	55	454.6	318.3
16	258.9	181.2	76	308.0	215.6	36	357.2	250.1	96	406.3	284.5	56	455.5	318.9
17	259.7	181.8	77	308.8	216.2	37	358.0	250.6	97	407.1	285.1	57	456.3	319.5
18	260.5	182.4	78	309.6	216.8	38	358.8	251.2	98	408.0	285.6	58	457.1	320.0
19	261.3	183.0	79	310.5	217.4	39	359.6	251.8	99	408.8	286.2	59	457.9	320.6
20	262.1	183.5	80	311.3	217.9	40	360.4	252.4	500	409.6	286.8	60	458.7	321.2
321	263.0	184.1	381	312.1	218.5	441	361.3	252.9	501	410.4	287.4	561	459.6	321.8
22	263.8	184.7	82	312.9	219.1	42	362.1	253.5	02	411.2	287.9	62	460.4	322.3
23	264.6	185.2	83	313.7	219.7	43	362.9	254.1	03	412.1	288.5	63	461.2	322.9
24	265.4	185.8	84	314.6	220.2	44	363.7	254.7	04	412.9	289.1	64	462.0	323.5
25	266.2	186.4	85	315.4	220.8	45	364.5	255.2	05	413.7	289.7	65	462.8	324.1
26	267.1	187.0	86	316.2	221.4	46	365.4	255.8	06	414.5	290.2	66	463.7	324.6
27	267.9	187.5	87	317.0	222.0	47	366.2	256.4	07	415.3	290.8	67	464.5	325.2
28	268.7	188.1	88	317.8	222.5	48	367.0	256.9	08	416.1	291.4	68	465.3	325.8
29	269.5	188.7	89	318.7	223.1	49	367.8	257.5	09	417.0	291.9	69	466.1	326.4
30	270.3	189.3	90	319.5	223.7	50	368.6	258.1	10	417.8	292.5	70	466.9	326.9
331	271.1	189.8	391	320.3	224.3	451	369.4	258.7	511	418.6	293.1	571	467.8	327.5
32	272.0	190.4	92	321.1	224.8	52	370.3	259.2	12	419.4	293.7	72	468.6	328.1
33	272.8	191.0	93	321.9	225.4	53	371.1	259.8	13	420.2	294.2	73	469.4	328.7
34	273.6	191.6	94	322.8	226.0	54	371.9	260.4	14	421.1	294.8	74	470.2	329.2
35	274.4	192.1	95	323.6	226.5	55	372.7	261.0	15	421.9	295.4	75	471.0	329.8
36	275.2	192.7	96	324.4	227.1	56	373.5	261.5	16	422.7	296.0	76	471.9	330.4
37	276.1	193.3	97	325.2	227.7	57	374.4	262.1	17	423.5	296.5	77	472.7	331.0
38	276.9	193.9	98	326.0	228.3	58	375.2	262.7	18	424.3	297.1	78	473.5	331.5
39	277.7	194.4	99	326.9	228.8	59	376.0	263.3	19	425.2	297.7	79	474.3	332.1
40	278.5	195.0	400	327.7	229.4	60	376.8	263.8	20	426.0	298.3	80	475.1	332.7
341	279.3	195.6	401	328.5	230.0	461	377.6	264.4	521	426.8	298.8	581	476.0	333.3
42	280.2	196.1	02	329.3	230.6	62	378.5	265.0	22	427.6	299.4	82	476.8	333.8
43	281.0	196.7	03	330.1	231.1	63	379.3	265.5	23	428.4	300.0	83	477.6	334.4
44	281.8	197.3	04	330.9	231.7	64	380.1	266.1	24	429.3	300.5	84	478.4	335.0
45	282.6	197.9	05	331.8	232.3	65	380.9	266.7	25	430.1	301.1	85	479.2	335.6
46	283.4	198.4	06	332.6	232.9	66	381.7	267.3	26	430.9	301.7	86	480.1	336.1
47	284.3	199.0	07	333.4	233.4	67	382.6	267.8	27	431.7	302.3	87	480.9	336.7
48	285.1	199.6	08	334.2	234.0	68	383.4	268.4	28	432.5	302.8	88	481.7	337.3
49	285.9	200.2	09	335.0	234.6	69	384.2	269.0	29	433.4	303.4	89	482.5	337.9
50	286.7	200.7	10	335.9	235.1	70	385.0	269.6	30	434.2	304.0	90	483.3	338.4
351	287.5	201.3	411	336.7	235.7	471	385.8	270.1	531	435.0	304.5	591	484.2	339.0
52	288.3	201.9	12	337.5	236.3	72	386.6	270.7	32	435.8	305.1	92	485.0	339.6
53	289.2	202.5	13	338.3	236.9	73	387.5	271.3	33	436.6	305.7	93	485.8	340.2
54	290.0	203.0	14	339.1	237.4	74	388.3	271.9	34	437.5	306.3	94	486.6	340.7
55	290.8	203.6	15	340.0	238.0	75	389.1	272.4	35	438.3	306.8	95	487.4	341.3
56	291.6	204.2	16	340.8	238.6	76	389.9	273.0	36	439.1	307.4	96	488.3	341.9
57	292.4	204.7	17	341.6	239.2	77	390.7	273.6	37	439.9	308.0	97	489.1	342.5
58	293.3	205.3	18	342.4	239.7	78	391.6	274.2	38	440.7	308.6	98	489.9	343.0
59	294.1	205.9	19	343.2	240.3	79	392.4	274.7	39	441.5	309.1	99	490.7	343.6
60	294.9	206.5	20	344.1	240.9	80	393.2	275.3	40	442.3	309.7	600	491.5	344.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

55° (125°, 235°, 305°).

TABLE 2.

Difference of Latitude and Departure for 36° (144°, 216°, 324°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	49.4	35.9	121	97.9	71.1	181	146.4	106.4	241	195.0	141.7
2	1.6	1.2	62	50.2	36.4	22	98.7	71.7	82	147.2	107.0	42	195.8	142.2
3	2.4	1.8	63	51.0	37.0	23	99.5	72.3	83	148.1	107.6	43	196.6	142.8
4	3.2	2.4	64	51.8	37.6	24	100.3	72.9	84	148.9	108.2	44	197.4	143.4
5	4.0	2.9	65	52.6	38.2	25	101.1	73.5	85	149.7	108.7	45	198.2	144.0
6	4.9	3.5	66	53.4	38.8	26	101.9	74.1	86	150.5	109.3	46	199.0	144.6
7	5.7	4.1	67	54.2	39.4	27	102.7	74.6	87	151.3	109.9	47	199.8	145.2
8	6.5	4.7	68	55.0	40.0	28	103.6	75.2	88	152.1	110.5	48	200.6	145.8
9	7.3	5.3	69	55.8	40.6	29	104.4	75.8	89	152.9	111.1	49	201.4	146.4
10	8.1	5.9	70	56.6	41.1	30	105.2	76.4	90	153.7	111.7	50	202.3	146.9
11	8.9	6.5	71	57.4	41.7	131	106.0	77.0	191	154.5	112.3	251	203.1	147.5
12	9.7	7.1	72	58.2	42.3	32	106.8	77.6	92	155.3	112.9	52	203.9	148.1
13	10.5	7.6	73	59.1	42.9	33	107.6	78.2	93	156.1	113.4	53	204.7	148.7
14	11.3	8.2	74	59.9	43.5	34	108.4	78.8	94	156.9	114.0	54	205.5	149.3
15	12.1	8.8	75	60.7	44.1	35	109.2	79.4	95	157.8	114.6	55	206.3	149.9
16	12.9	9.4	76	61.5	44.7	36	110.0	79.9	96	158.6	115.2	56	207.1	150.5
17	13.8	10.0	77	62.3	45.3	37	110.8	80.5	97	159.4	115.8	57	207.9	151.1
18	14.6	10.6	78	63.1	45.8	38	111.6	81.1	98	160.2	116.4	58	208.7	151.6
19	15.4	11.2	79	63.9	46.4	39	112.5	81.7	99	161.0	117.0	59	209.5	152.2
20	16.2	11.8	80	64.7	47.0	40	113.3	82.3	200	161.8	117.6	60	210.3	152.8
21	17.0	12.3	81	65.5	47.6	141	114.1	82.9	201	162.6	118.1	261	211.2	153.4
22	17.8	12.9	82	66.3	48.2	42	114.9	83.5	02	163.4	118.7	62	212.0	154.0
23	18.6	13.5	83	67.1	48.8	43	115.7	84.1	03	164.2	119.3	63	212.8	154.6
24	19.4	14.1	84	68.0	49.4	44	116.5	84.6	04	165.0	119.9	64	213.6	155.2
25	20.2	14.7	85	68.8	50.0	45	117.3	85.2	05	165.8	120.5	65	214.4	155.8
26	21.0	15.3	86	69.6	50.5	46	118.1	85.8	06	166.7	121.1	66	215.2	156.4
27	21.8	15.9	87	70.4	51.1	47	118.9	86.4	07	167.5	121.7	67	216.0	156.9
28	22.7	16.5	88	71.2	51.7	48	119.7	87.0	08	168.3	122.3	68	216.8	157.5
29	23.5	17.0	89	72.0	52.3	49	120.5	87.6	09	169.1	122.8	69	217.6	158.1
30	24.3	17.6	90	72.8	52.9	50	121.4	88.2	10	169.9	123.4	70	218.4	158.7
31	25.1	18.2	91	73.6	53.5	151	122.2	88.8	211	170.7	124.0	271	219.2	159.3
32	25.9	18.8	92	74.4	54.1	52	123.0	89.3	12	171.5	124.6	72	220.1	159.9
33	26.7	19.4	93	75.2	54.7	53	123.8	89.9	13	172.3	125.2	73	220.9	160.5
34	27.5	20.0	94	76.0	55.3	54	124.6	90.5	14	173.1	125.8	74	221.7	161.1
35	28.3	20.6	95	76.9	55.8	55	125.4	91.1	15	173.9	126.4	75	222.5	161.6
36	29.1	21.2	96	77.7	56.4	56	126.2	91.7	16	174.7	127.0	76	223.3	162.2
37	29.9	21.7	97	78.5	57.0	57	127.0	92.3	17	175.6	127.5	77	224.1	162.8
38	30.7	22.3	98	79.3	57.6	58	127.8	92.9	18	176.4	128.1	78	224.9	163.4
39	31.6	22.9	99	80.1	58.2	59	128.6	93.5	19	177.2	128.7	79	225.7	164.0
40	32.4	23.5	100	80.9	58.8	60	129.4	94.0	20	178.0	129.3	80	226.5	164.6
41	33.2	24.1	101	81.7	59.4	161	130.3	94.6	221	178.8	129.9	281	227.3	165.2
42	34.0	24.7	02	82.5	60.0	62	131.1	95.2	22	179.6	130.5	82	228.1	165.8
43	34.8	25.3	03	83.3	60.5	63	131.9	95.8	23	180.4	131.1	83	229.0	166.3
44	35.6	25.9	04	84.1	61.1	64	132.7	96.4	24	181 2	131.7	84	229.8	166.9
45	36.4	26.5	05	84.9	61.7	65	133.5	97.0	25	182.0	132.3	85	230.6	167.5
46	37.2	27.0	06	85.8	62.3	66	134.3	97.6	26	182.8	132.8	86	231.4	168.1
47	38.0	27.6	07	86.6	62.9	67	135.1	98.2	27	183.6	133.4	87	232.2	168.7
48	38.8	28.2	08	87.4	63.5	68	135.9	98.7	28	184.5	134.0	88	233.0	169.3
49	39.6	28.8	09	88.2	64.1	69	136.7	99.3	29	185.3	134.6	89	233.8	169.9
50	40.5	29.4	10	89.0	64.7	70	137.5	99.9	30	186.1	135.2	90	234.6	170.5
51	41.3	30.0	111	89.8	65.2	171	138.3	100.5	231	186.9	135.8	291	235.4	171.0
52	42.1	30.6	12	90.6	65.8	72	139.2	101.1	32	187.7	136.4	92	236.2	171.6
53	42.9	31.2	13	91.4	66.4	73	140.0	101.7	33	188.5	137.0	93	237.0	172.2
54	43.7	31.7	14	92.2	67.0	74	140.8	102.3	34	189.3	137.5	94	237.9	172.8
55	44.5	32.3	15	93.0	67.6	75	141.6	102.9	35	190.1	138.1	95	238.7	173.4
56	45.3	32.9	16	93.8	68.2	76	142.4	103.5	36	190.9	138.7	96	239.5	174.0
57	46.1	33.5	17	94.7	68.8	77	143.2	104.0	37	191.7	139.3	97	240.3	174.6
58	46.9	34.1	18	95.5	69.4	78	144.0	104.6	38	192.5	139.9	98	241.1	175.2
59	47.7	34.7	19	96.3	69.9	79	144.8	105.2	39	193.4	140.5	99	241.9	175.7
60	48.5	35.3	20	97.1	70.5	80	145.6	105.8	40	194.2	141.1	300	242.7	176.3
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

54° (126°, 234°, 306°).

TABLE 2.

Difference of Latitude and Departure for 36° (144°, 216°, 324°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	243.5	176.9	361	292.1	212.2	421	340.6	247.5	481	389.1	282.7	541	437.7	318.0
02	244.3	177.5	62	292.9	212.8	22	341.4	248.1	82	390.0	283.3	42	438.5	318.6
03	245.1	178.1	63	293.7	213.4	23	342.2	248.6	83	390.8	283.9	43	439.3	319.1
04	246.0	178.7	64	294.5	214.0	24	343.0	249.2	84	391.6	284.5	44	440.2	319.7
05	246.8	179.3	65	295.3	214.6	25	343.8	249.8	85	392.4	285.1	45	441.0	320.3
06	247.6	179.9	66	296.1	215.1	26	344.7	250.4	86	393.2	285.6	46	441.8	320.9
07	248.4	180.5	67	296.9	215.7	27	345.5	251.0	87	394.0	286.2	47	442.6	321.5
08	249.2	181.1	68	297.7	216.3	28	346.3	251.6	88	394.8	286.8	48	443.4	322.1
09	250.0	181.6	69	298.5	216.9	29	347.1	252.2	89	395.6	287.4	49	444.2	322.7
10	250.8	182.2	70	299.3	217.5	30	347.9	252.8	90	396.4	288.0	50	445.0	323.3
311	251.6	182.8	371	300.2	218.1	431	348.7	253.3	491	397.3	288.6	551	445.8	323.8
12	252.4	183.4	72	301.0	218.7	32	349.5	253.9	92	398.1	289.2	52	446.6	324.4
13	253.2	184.0	73	301.8	219.3	33	350.3	254.5	93	398.9	289.8	53	447.4	325.0
14	254.0	184.6	74	302.6	219.8	34	351.1	255.1	94	399.7	290.3	54	448.2	325.6
15	254.9	185.2	75	303.4	220.4	35	351.9	255.7	95	400.5	290.9	55	449.0	326.2
16	255.7	185.8	76	304.2	221.0	36	352.7	256.3	96	401.3	291.5	56	449.8	326.8
17	256.5	186.4	77	305.0	221.6	37	353.6	256.9	97	402.1	292.1	57	450.7	327.4
18	257.3	186.9	78	305.8	222.2	38	354.4	257.5	98	402.9	292.7	58	451.5	328.0
19	258.1	187.5	79	306.6	222.8	39	355.2	258.0	99	403.7	293.3	59	452.3	328.5
20	258.9	188.1	80	307.4	223.4	40	356.0	258.6	500	404.5	293.9	60	453.1	329.1
321	259.7	188.7	381	308.2	224.0	441	356.8	259.2	501	405.3	294.5	561	453.9	329.7
22	260.5	189.3	82	309.1	224.5	42	357.6	259.8	02	406.1	295.0	62	454.7	330.3
23	261.3	189.9	83	309.9	225.1	43	358.4	260.4	03	407.0	295.6	63	455.5	330.9
24	262.1	190.5	84	310.7	225.7	44	359.2	261.0	04	407.8	296.2	64	456.3	331.5
25	262.9	191.0	85	311.5	226.3	45	360.0	261.6	05	408.6	296.8	65	457.1	332.1
26	263.7	191.6	86	312.3	226.9	46	360.8	262.2	06	409.4	297.4	66	457.9	332.7
27	264.6	192.2	87	313.1	227.5	47	361.6	262.8	07	410.2	298.0	67	458.7	333.3
28	265.4	192.8	88	313.9	228.1	48	362.4	263.3	08	411.0	298.6	68	459.5	333.8
29	266.2	193.4	89	314.7	228.7	49	363.3	263.9	09	411.8	299.2	69	460.3	334.4
30	267.0	194.0	90	315.5	229.2	50	364.1	264.5	10	412.6	299.8	70	461.1	335.0
331	267.8	194.6	391	316.3	229.8	451	364.9	265.1	511	413.4	300.3	571	462.0	335.6
32	268.6	195.2	92	317.1	230.4	52	365.7	265.7	12	414.2	300.9	72	462.8	336.2
33	269.4	195.7	93	318.0	231.0	53	366.5	266.3	13	415.1	301.5	73	463.6	336.8
34	270.2	196.3	94	318.8	231.6	54	367.3	266.9	14	415.9	302.1	74	464.4	337.4
35	271.0	196.9	95	319.6	232.2	55	368.1	267.5	15	416.7	302.7	75	465.2	338.0
36	271.8	197.5	96	320.4	232.8	56	368.9	268.0	16	417.5	303.3	76	466.0	338.5
37	272.6	198.1	97	321.2	233.4	57	369.7	268.6	17	418.3	303.9	77	466.8	339.1
38	273.5	198.7	98	322.0	233.9	58	370.5	269.2	18	419.1	304.4	78	467.6	339.7
39	274.3	199.3	99	322.8	234.5	59	371.3	269.8	19	419.9	305.0	79	468.4	340.3
40	275.1	199.9	400	323.6	235.1	60	372.2	270.4	20	420.7	305.6	80	469.3	340.9
341	275.9	200.4	401	324.4	235.7	461	373.0	271.0	521	421.5	306.2	581	470.1	341.5
42	276.7	201.0	02	325.2	236.3	62	373.8	271.6	22	422.3	306.8	82	470.9	342.1
43	277.5	201.6	03	326.0	236.9	63	374.6	272.2	23	423.1	307.4	83	471.7	342.7
44	278.3	202.2	04	326.9	237.5	64	375.4	272.7	24	423.9	308.0	84	472.5	343.2
45	279.1	202.8	05	327.7	238.1	65	376.2	273.3	25	424.7	308.6	85	473.3	343.8
46	279.9	203.4	06	328.5	238.7	66	377.0	273.9	26	425.5	309.2	86	474.1	344.4
47	280.7	204.0	07	329.3	239.2	67	377.8	274.5	27	426.4	309.7	87	474.9	345.0
48	281.5	204.6	08	330.1	239.8	68	378.6	275.1	28	427.2	310.3	88	475.7	345.6
49	282.4	205.1	09	330.9	240.4	69	379.4	275.7	29	428.0	310.9	89	476.5	346.2
50	283.2	205.7	10	331.7	241.0	70	380.2	276.3	30	428.8	311.5	90	477.3	346.8
351	284.0	206.3	411	332.5	241.6	471	381.1	276.9	531	429.6	312.1	591	478.2	347.4
52	284.8	206.9	12	333.3	242.2	72	381.9	277.4	32	430.4	312.7	92	479.0	347.9
53	285.6	207.5	13	334.1	242.8	73	382.7	278.0	33	431.2	313.3	93	479.8	348.5
54	286.4	208.1	14	334.9	243.4	74	383.5	278.6	34	432.0	313.9	94	480.6	349.1
55	287.2	208.7	15	335.8	243.9	75	384.3	279.2	35	432.9	314.4	95	481.4	349.7
56	288.0	209.3	16	336.6	244.5	76	385.1	279.8	36	433.7	315.0	96	482.2	350.3
57	288.8	209.8	17	337.4	245.1	77	385.9	280.4	37	434.5	315.6	97	483.0	350.9
58	289.6	210.4	18	338.2	245.7	78	386.7	281.0	38	435.3	316.2	98	483.8	351.5
59	290.4	211.0	19	339.0	246.3	79	387.5	281.6	39	436.1	316.8	99	484.6	352.1
60	291.3	211.6	20	339.8	246.9	80	388.3	282.1	40	436.9	317.4	600	485.4	352.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

54° (126°, 234°, 306°).

TABLE 2.

Difference of Latitude and Departure for 37° (143°, 217°, 323°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	48.7	36.7	121	96.6	72.8	181	144.6	108.9	241	192.5	145.0
2	1.6	1.2	62	49.5	37.3	22	97.4	73.4	82	145.4	109.5	42	193.3	145.6
3	2.4	1.8	63	50.3	37.9	23	98.2	74.0	83	146.2	110.1	43	194.1	146.2
4	3.2	2.4	64	51.1	38.5	24	99.0	74.6	84	146.9	110.7	44	194.9	146.8
5	4.0	3.0	65	51.9	39.1	25	99.8	75.2	85	147.7	111.3	45	195.7	147.4
6	4.8	3.6	66	52.7	39.7	26	100.6	75.8	86	148.5	111.9	46	196.5	148.0
7	5.6	4.2	67	53.5	40.3	27	101.4	76.4	87	149.3	112.5	47	197.3	148.6
8	6.4	4.8	68	54.3	40.9	28	102.2	77.0	88	150.1	113.1	48	198.1	149.3
9	7.2	5.4	69	55.1	41.5	29	103.0	77.6	89	150.9	113.7	49	198.9	149.9
10	8.0	6.0	70	55.9	42.1	30	103.8	78.2	90	151.7	114.3	50	199.7	150.5
11	8.8	6.6	71	56.7	42.7	131	104.6	78.8	191	152.5	114.9	251	200.5	151.1
12	9.6	7.2	72	57.5	43.3	32	105.4	79.4	92	153.3	115.5	52	201.3	151.7
13	10.4	7.8	73	58.3	43.9	33	106.2	80.0	93	154.1	116.2	53	202.1	152.3
14	11.2	8.4	74	59.1	44.5	34	107.0	80.6	94	154.9	116.8	54	202.9	152.9
15	12.0	9.0	75	59.9	45.1	35	107.8	81.2	95	155.7	117.4	55	203.7	153.5
16	12.8	9.6	76	60.7	45.7	36	108.6	81.8	96	156.5	118.0	56	204.5	154.1
17	13.6	10.2	77	61.5	46.3	37	109.4	82.4	97	157.3	118.6	57	205.2	154.7
18	14.4	10.8	78	62.3	46.9	38	110.2	83.1	98	158.1	119.2	58	206.0	155.3
19	15.2	11.4	79	63.1	47.5	39	111.0	83.7	99	158.9	119.8	59	206.8	155.9
20	16.0	12.0	80	63.9	48.1	40	111.8	84.3	200	159.7	120.4	60	207.6	156.5
21	16.8	12.6	81	64.7	48.7	141	112.6	84.9	201	160.5	121.0	261	208.4	157.1
22	17.6	13.2	82	65.5	49.3	42	113.4	85.5	02	161.3	121.6	62	209.2	157.7
23	18.4	13.8	83	66.3	50.0	43	114.2	86.1	03	162.1	122.2	63	210.0	158.3
24	19.2	14.4	84	67.1	50.6	44	115.0	86.7	04	162.9	122.8	64	210.8	158.9
25	20.0	15.0	85	67.9	51.2	45	115.8	87.3	05	163.7	123.4	65	211.6	159.5
26	20.8	15.6	86	68.7	51.8	46	116.6	87.9	06	164.5	124.0	66	212.4	160.1
27	21.6	16.2	87	69.5	52.4	47	117.4	88.5	07	165.3	124.6	67	213.2	160.7
28	22.4	16.9	88	70.3	53.0	48	118.2	89.1	08	166.1	125.2	68	214.0	161.3
29	23.2	17.5	89	71.1	53.6	49	119.0	89.7	09	166.9	125.8	69	214.8	161.9
30	24.0	18.1	90	71.9	54.2	50	119.8	90.3	10	167.7	126.4	70	215.6	162.5
31	24.8	18.7	91	72.7	54.8	151	120.6	90.9	211	168.5	127.0	271	216.4	163.1
32	25.6	19.3	92	73.5	55.4	52	121.4	91.5	12	169.3	127.6	72	217.2	163.7
33	26.4	19.9	93	74.3	56.0	53	122.2	92.1	13	170.1	128.2	73	218.0	164.3
34	27.2	20.5	94	75.1	56.6	54	123.0	92.7	14	170.9	128.8	74	218.8	164.9
35	28.0	21.1	95	75.9	57.2	55	123.8	93.3	15	171.7	129.4	75	219.6	165.5
36	28.8	21.7	96	76.7	57.8	56	124.6	93.9	16	172.5	130.0	76	220.4	166.1
37	29.5	22.3	97	77.5	58.4	57	125.4	94.5	17	173.3	130.6	77	221.2	166.7
38	30.3	22.9	98	78.3	59.0	58	126.2	95.1	18	174.1	131.2	78	222.0	167.3
39	31.1	23.5	99	79.1	59.6	59	127.0	95.7	19	174.9	131.8	79	222.8	167.9
40	31.9	24.1	100	79.9	60.2	60	127.8	96.3	20	175.7	132.4	80	223.6	168.5
41	32.7	24.7	101	80.7	60.8	161	128.6	96.9	221	176.5	133.0	281	224.4	169.1
42	33.5	25.3	02	81.5	61.4	62	129.4	97.5	22	177.3	133.6	82	225.2	169.7
43	34.3	25.9	03	82.3	62.0	63	130.2	98.1	23	178.1	134.2	83	226.0	170.3
44	35.1	26.5	04	83.1	62.6	64	131.0	98.7	24	178.9	134.8	84	226.8	170.9
45	35.9	27.1	05	83.9	63.2	65	131.8	99.3	25	179.7	135.4	85	227.6	171.5
46	36.7	27.7	06	84.7	63.8	66	132.6	99.9	26	180.5	136.0	86	228.4	172.1
47	37.5	28.3	07	85.5	64.4	67	133.4	100.5	27	181.3	136.6	87	229.2	172.7
48	38.3	28.9	08	86.3	65.0	68	134.2	101.1	28	182.1	137.2	88	230.0	173.3
49	39.1	29.5	09	87.1	65.6	69	135.0	101.7	29	182.9	137.8	89	230.8	173.9
50	39.9	30.1	10	87.8	66.2	70	135.8	102.3	30	183.7	138.4	90	231.6	174.5
51	40.7	30.7	111	88.6	66.8	171	136.6	102.9	231	184.5	139.0	291	232.4	175.1
52	41.5	31.3	12	89.4	67.4	72	137.4	103.5	32	185.3	139.6	92	233.2	175.7
53	42.3	31.9	13	90.2	68.0	73	138.2	104.1	33	186.1	140.2	93	234.0	176.3
54	43.1	32.5	14	91.0	68.6	74	139.0	104.7	34	186.9	140.8	94	234.8	176.9
55	43.9	33.1	15	91.8	69.2	75	139.8	105.3	35	187.7	141.4	95	235.6	177.5
56	44.7	33.7	16	92.6	69.8	76	140.6	105.9	36	188.5	142.0	96	236.4	178.1
57	45.5	34.3	17	93.4	70.4	77	141.4	106.5	37	189.3	142.6	97	237.2	178.7
58	46.3	34.9	18	94.2	71.0	78	142.2	107.1	38	190.1	143.2	98	238.0	179.3
59	47.1	35.5	19	95.0	71.6	79	143.0	107.7	39	190.9	143.8	99	238.8	179.9
60	47.9	36.1	20	95.8	72.2	80	143.8	108.3	40	191.7	144.4	300	239.6	180.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

53° (127°, 233°, 307°).

TABLE 2.

Difference of Latitude and Departure for 37° (143°, 217°, 323°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	240.4	181.1	361	288.3	217.3	421	336.2	253.4	481	384.1	289.5	541	432.0	325.6
02	241.2	181.7	62	289.1	217.9	22	337.0	254.0	82	384.9	290.0	42	432.8	326.2
03	242.0	182.4	63	289.9	218.5	23	337.8	254.6	83	385.7	290.6	43	433.6	326.8
04	242.7	183.0	64	290.7	219.1	24	338.6	255.2	84	386.5	291.2	44	434.4	327.3
05	243.5	183.6	65	291.5	219.7	25	339.4	255.8	85	387.3	291.8	45	435.2	327.9
06	244.3	184.2	66	292.3	220.3	26	340.2	256.4	86	388.1	292.4	46	436.0	328.5
07	245.1	184.8	67	293.1	220.9	27	341.0	257.0	87	388.9	293.0	47	436.8	329.1
08	245.9	185.4	68	293.9	221.5	28	341.8	257.6	88	389.7	293.6	48	437.6	329.7
09	246.7	186.0	69	294.7	222.1	29	342.6	258.2	89	390.5	294.2	49	438.4	330.3
10	247.5	186.6	70	295.5	222.7	30	343.4	258.8	90	391.3	294.8	50	439.2	330.9
311	248.3	187.2	371	296.3	223.3	431	344.2	259.4	491	392.1	295.4	551	440.0	331.5
12	249.1	187.8	72	297.1	223.9	32	345.0	260.0	92	392.9	296.0	52	440.8	332.1
13	249.9	188.4	73	297.9	224.5	33	345.8	260.6	93	393.7	296.6	53	441.6	332.7
14	250.7	189.0	74	298.7	225.1	34	346.6	261.2	94	394.5	297.2	54	442.4	333.3
15	251.5	189.6	75	299.5	225.7	35	347.4	261.8	95	395.3	297.8	55	443.2	333.9
16	252.3	190.2	76	300.3	226.3	36	348.2	262.4	96	396.1	298.5	56	444.0	334.6
17	253.1	190.8	77	301.1	226.9	37	349.0	263.0	97	396.9	299.1	57	444.8	235.2
18	253.9	191.4	78	301.8	227.5	38	349.8	263.6	98	397.7	399.7	58	445.6	335.8
19	254.7	192.0	79	302.6	228.1	39	350.6	264.2	99	398.5	300.3	59	446.4	336.4
20	255.5	192.6	80	303.4	228.7	40	351.4	264.8	500	399.3	300.9	60	447.2	337.0
321	256.3	193.2	381	304.2	229.3	441	352.2	265.4	501	400.1	301.5	561	448.0	337.6
22	257.1	193.8	82	305.0	229.9	42	353.0	266.0	02	400.9	302.1	62	448.8	338.2
23	257.9	194.4	83	305.8	230.5	43	353.8	266.6	03	401.7	302.7	63	449.6	338.8
24	258.7	195.0	84	306.6	231.1	44	354.6	267.2	04	402.5	303.3	64	450.4	339.4
25	259.5	195.6	85	307.4	231.7	45	355.4	267.8	05	403.3	303.9	65	451.2	340.0
26	260.3	196.2	86	308.2	232.3	46	356.2	268.4	06	404.1	304.5	66	452.0	340.6
27	261.1	196.8	87	309.0	232.9	47	357.0	269.0	07	404.9	305.1	67	452.8	341.2
28	261.9	197.4	88	309.8	233.5	48	357.8	269.6	08	405.7	305.7	68	453.6	341.8
29	262.7	198.0	89	310.6	234.1	49	358.6	270.2	09	406.5	306.3	69	454.4	342.4
30	263.5	198.6	90	311.4	234.7	50	359.4	270.8	10	407.3	306.9	70	455.2	343.0
331	264.3	199.2	391	312.2	235.3	451	360.1	271.4	511	408.1	307.5	571	456.0	343.6
32	265.1	199.8	92	313.0	235.9	52	360.9	272.0	12	408.9	308.2	72	456.8	344.3
33	265.9	200.4	93	313.8	236.5	53	361.7	272.6	13	409.7	308.8	73	457.6	344.9
34	266.7	201.0	94	314.6	237.1	54	362.5	273.2	14	410.5	309.4	74	458.4	345.5
35	267.5	201.6	95	315.4	237.7	55	363.3	273.8	15	411.3	310.0	75	459.2	346.1
36	268.3	202.2	96	316.2	238.3	56	364.1	274.4	16	412.1	310.6	76	460.0	346.7
37	269.1	202.8	97	317.0	238.9	57	364.9	275.0	17	412.9	311.2	77	460.8	347.3
38	269.9	203.4	98	317.8	239.5	58	365.7	275.6	18	413.7	311.8	78	461.6	347.9
39	270.7	204.0	99	318.6	240.1	59	366.5	276.2	19	414.5	312.4	79	462.4	348.5
40	271.5	204.6	400	319.4	240.7	60	367.3	276.8	20	415.3	313.0	80	463.2	349.1
341	272.3	205.2	401	320.2	241.3	461	368.1	277.4	521	416.1	313.6	581	464.0	349.7
42	273.1	205.8	02	321.0	241.9	62	368.9	278.0	22	416.9	314.2	82	464.8	350.3
43	273.9	206.4	03	321.8	242.5	63	369.7	278.6	23	417.7	314.8	83	465.6	350.9
44	274.7	207.0	04	322.6	243.1	64	370.5	279.2	24	418.5	315.4	84	466.4	351.5
45	275.5	207.6	05	323.4	243.7	65	371.3	279.8	25	419.3	316.0	85	467.2	352.1
46	276.3	208.2	06	324.2	244.3	66	372.1	280.4	26	420.1	316.6	86	468.0	352.7
47	277.1	208.8	07	325.0	244.9	67	372.9	281.0	27	420.9	317.2	87	468.8	353.3
48	277.9	209.4	08	325.8	245.5	68	373.7	281.6	28	421.7	317.8	88	469.6	353.9
49	278.7	210.0	09	326.6	246.1	69	374.5	282.3	29	422.5	318.4	89	470.4	354.5
50	279.5	210.6	10	327.4	246.7	70	375.3	282.9	30	423.3	319.0	90	471.2	355.1
351	280.3	211.2	411	328.2	247.3	471	376.1	283.5	531	424.1	319.6	591	472.0	355.7
52	281.1	211.8	12	329.0	247.9	72	376.9	284.1	32	424.9	320.2	92	472.8	356.3
53	281.9	212.4	13	329.8	248.5	73	377.7	284.7	33	425.7	320.8	93	473.6	356.9
54	282.7	213.0	14	330.6	249.2	74	378.5	285.3	34	426.5	321.4	94	474.4	357.5
55	283.5	213.6	15	331.4	249.8	75	379.3	285.9	35	427.3	322.0	95	475.2	358.1
56	284.3	214.2	16	332.2	250.4	76	380.1	286.5	36	428.1	322.6	96	476.0	358.7
57	285.1	214.8	17	333.0	251.0	77	380.9	287.1	37	428.9	323.2	97	476.8	359.3
58	285.9	215.4	18	333.8	251.6	78	381.7	287.7	38	429.7	323.8	98	477.6	359.9
59	286.7	216.1	19	334.6	252.2	79	382.5	288.3	39	430.5	324.4	99	478.4	360.5
60	287.5	216.7	20	335.4	252.8	80	383.3	288.9	40	431.3	325.0	600	479.2	361.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

53° (127°, 233°, 307°).

TABLE 2.

Difference of Latitude and Departure for 38° (142°, 218°, 322°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	48.1	37.6	121	95.3	74.5	181	142.6	111.4	241	189.9	148.4
2	1.6	1.2	62	48.9	38.2	22	96.1	75.1	82	143.4	112.1	42	190.7	149.0
3	2.4	1.8	63	49.6	38.8	23	96.9	75.7	83	144.2	112.7	43	191.5	149.6
4	3.2	2.5	64	50.4	39.4	24	97.7	76.3	84	145.0	113.3	44	192.3	150.2
5	3.9	3.1	65	51.2	40.0	25	98.5	77.0	85	145.8	113.9	45	193.1	150.8
6	4.7	3.7	66	52.0	40.6	26	99.3	77.6	86	146.6	114.5	46	193.9	151.5
7	5.5	4.3	67	52.8	41.2	27	100.1	78.2	87	147.4	115.1	47	194.6	152.1
8	6.3	4.9	68	53.6	41.9	28	100.9	78.8	88	148.1	115.7	48	195.4	152.7
9	7.1	5.5	69	54.4	42.5	29	101.7	79.4	89	148.9	116.4	49	196.2	153.3
10	7.9	6.2	70	55.2	43.1	30	102.4	80.0	90	149.7	117.0	50	197.0	153.9
11	8.7	6.8	71	55.9	43.7	131	103.2	80.7	191	150.5	117.6	251	197.8	154.5
12	9.5	7.4	72	56.7	44.3	32	104.0	81.3	92	151.3	118.2	52	198.6	155.1
13	10.2	8.0	73	57.5	44.9	33	104.8	81.9	93	152.1	118.8	53	199.4	155.8
14	11.0	8.6	74	58.3	45.6	34	105.6	82.5	94	152.9	119.4	54	200.2	156.4
15	11.8	9.2	75	59.1	46.2	35	106.4	83.1	95	153.7	120.1	55	200.9	157.0
16	12.6	9.9	76	59.9	46.8	36	107.2	83.7	96	154.5	120.7	56	201.7	157.6
17	13.4	10.5	77	60.7	47.4	37	108.0	84.3	97	155.2	121.3	57	202.5	158.2
18	14.2	11.1	78	61.5	48.0	38	108.7	85.0	98	156.0	121.9	58	203.3	158.8
19	15.0	11.7	79	62.3	48.6	39	109.5	85.6	99	156.8	122.5	59	204.1	159.5
20	15.8	12.3	80	63.0	49.3	40	110.3	86.2	200	157.6	123.1	60	204.9	160.1
21	16.5	12.9	81	63.8	49.9	141	111.1	86.8	201	158.4	123.7	261	205.7	160.7
22	17.3	13.5	82	64.6	50.5	42	111.9	87.4	02	159.2	124.4	62	206.5	161.3
23	18.1	14.2	83	65.4	51.1	43	112.7	88.0	03	160.0	125.0	63	207.2	161.9
24	18.9	14.8	84	66.2	51.7	44	113.5	88.7	04	160.8	125.6	64	208.0	162.5
25	19.7	15.4	85	67.0	52.3	45	114.3	89.3	05	161.5	126.2	65	208.8	163.2
26	20.5	16.0	86	67.8	52.9	46	115.0	89.9	06	162.3	126.8	66	209.6	163.8
27	21.3	16.6	87	68.6	53.6	47	115.8	90.5	07	163.1	127.4	67	210.4	164.4
28	22.1	17.2	88	69.3	54.2	48	116.6	91.1	08	163.9	128.1	68	211.2	165.0
29	22.9	17.9	89	70.1	54.8	49	117.4	91.7	09	164.7	128.7	69	212.0	165.6
30	23.6	18.5	90	70.9	55.4	50	118.2	92.3	10	165.5	129.3	70	212.8	166.2
31	24.4	19.1	91	71.7	56.0	151	119.0	93.0	211	166.3	129.9	271	213.6	166.8
32	25.2	19.7	92	72.5	56.6	52	119.8	93.6	12	167.1	130.5	72	214.3	167.5
33	26.0	20.3	93	73.3	57.3	53	120.6	94.2	13	167.8	131.1	73	215.1	168.1
34	26.8	20.9	94	74.1	57.9	54	121.4	94.8	14	168.6	131.8	74	215.9	168.7
35	27.6	21.5	95	74.9	58.5	55	122.1	95.4	15	169.4	132.4	75	216.7	169.3
36	28.4	22.2	96	75.6	59.1	56	122.9	96.0	16	170.2	133.0	76	217.5	169.9
37	29.2	22.8	97	76.4	59.7	57	123.7	96.7	17	171.0	133.6	77	218.3	170.5
38	29.9	23.4	98	77.2	60.3	58	124.5	97.3	18	171.8	134.2	78	219.1	171.2
39	30.7	24.0	99	78.0	61.0	59	125.3	97.9	19	172.6	134.8	79	219.9	171.8
40	31.5	24.6	100	78.8	61.6	60	126.1	98.5	20	173.4	135.4	80	220.6	172.4
41	32.3	25.2	101	79.6	62.2	161	126.9	99.1	221	174.2	136.1	281	221.4	173.0
42	33.1	25.9	02	80.4	62.8	62	127.7	99.7	22	174.9	136.7	82	222.2	173.6
43	33.9	26.5	03	81.2	63.4	63	128.4	100.4	23	175.7	137.3	83	223.0	174.2
44	34.7	27.1	04	82.0	64.0	64	129.2	101.0	24	176.5	137.9	84	223.8	174.8
45	35.5	27.7	05	82.7	64.6	65	130.0	101.6	25	177.3	138.5	85	224.6	175.5
46	36.2	28.3	06	83.5	65.3	66	130.8	102.2	26	178.1	139.1	86	225.4	176.1
47	37.0	28.9	07	84.3	65.9	67	131.6	102.8	27	178.9	139.8	87	226.2	176.7
48	37.8	29.6	08	85.1	66.5	68	132.4	103.4	28	179.7	140.4	88	226.9	177.3
49	38.6	30.2	09	85.9	67.1	69	133.2	104.0	29	180.5	141.0	89	227.7	177.9
50	39.4	30.8	10	86.7	67.7	70	134.0	104.7	30	181.2	141.6	90	228.5	178.5
51	40.2	31.4	111	87.5	68.3	171	134.7	105.3	231	182.0	142.2	291	229.3	179.2
52	41.0	32.0	12	88.3	69.0	72	135.5	105.9	32	182.8	142.8	92	230.1	179.8
53	41.8	32.6	13	89.0	69.6	73	136.3	106.5	33	183.6	143.4	93	230.9	180.4
54	42.6	33.2	14	89.8	70.2	74	137.1	107.1	34	184.4	144.1	94	231.7	181.0
55	43.3	33.9	15	90.6	70.8	75	137.9	107.7	35	185.2	144.7	95	232.5	181.6
56	44.1	34.5	16	91.4	71.4	76	138.7	108.4	36	186.0	145.3	96	233.3	182.2
57	44.9	35.1	17	92.2	72.0	77	139.5	109.0	37	186.8	145.9	97	234.0	182.9
58	45.7	35.7	18	93.0	72.6	78	140.3	109.6	38	187.5	146.5	98	234.8	183.5
59	46.5	36.3	19	93.8	73.3	79	141.1	110.2	39	188.3	147.1	99	235.6	184.1
60	47.3	36.9	20	94.6	73.9	80	141.8	110.8	40	189.1	147.8	300	236.4	184.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

52° (128°, 232°, 308°).

TABLE 2.

Difference of Latitude and Departure for 38° (142°, 218°, 322°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	237.2	185.3	361	284.5	222.3	421	331.8	259.2	481	379.0	296.2	541	426.3	333.1
02	238.0	185.9	62	285.3	222.9	22	332.5	259.8	82	379.8	296.8	42	427.1	333.7
03	238.8	186.6	63	286.0	223.5	23	333.3	260.4	83	380.6	297.4	43	427.9	334.3
04	239.6	187.2	64	286.8	224.1	24	334.1	261.0	84	381.4	298.0	44	428.7	335.0
05	240.3	187.8	65	287.6	224.7	25	334.9	261.7	85	382.2	298.6	45	429.5	335.6
06	241.1	188.4	66	288.4	225.3	26	335.7	262.3	86	383.0	299.2	46	430.3	336.2
07	241.9	189.0	67	289.2	226.0	27	336.5	262.9	87	383.8	299.8	47	431.0	336.8
08	242.7	189.6	68	290.0	226.6	28	337.3	263.5	88	384.5	300.4	48	431.8	337.4
09	243.5	190.2	69	290.8	227.2	29	338.1	264.1	89	385.3	301.1	49	432.6	338.0
10	244.3	190.9	70	291.6	227.8	30	338.8	264.7	90	386.1	301.7	50	433.4	338.6
311	245.1	191.5	371	292.4	228.4	431	339.6	265.4	491	386.9	302.3	551	434.2	339.3
12	245.9	192.1	72	293.1	229.0	32	340.4	266.0	92	387.7	302.9	52	435.0	339.9
13	246.6	192.7	73	293.9	229.6	33	341.2	266.6	93	388.5	303.5	53	435.8	340.5
14	247.4	193.3	74	294.7	230.3	34	342.0	267.2	94	389.3	304.2	54	436.6	341.1
15	248.2	193.9	75	295.5	230.9	35	342.8	267.8	95	390.1	304.8	55	437.4	341.7
16	249.0	194.6	76	296.3	231.5	36	343.6	268.4	96	390.9	305.4	56	438.1	342.3
17	249.8	195.2	77	297.1	232.1	37	344.4	269.1	97	391.6	306.0	57	438.9	343.0
18	250.6	195.8	78	297.9	232.7	38	345.2	269.7	98	392.4	306.6	58	439.7	343.6
19	251.4	196.4	79	298.7	233.3	39	345.9	270.3	99	393.2	307.2	59	440.5	344.2
20	252.2	197.0	80	299.4	234.0	40	346.7	270.9	500	394.0	307.8	60	441.3	344.8
321	253.0	197.6	381	300.2	234.6	441	347.5	271.5	501	394.8	308.4	561	442.1	345.4
22	253.7	198.2	82	301.0	235.2	42	348.3	272.1	02	395.6	309.1	62	442.9	346.0
23	254.5	198.9	83	301.8	235.8	43	349.1	272.7	03	396.4	309.7	63	443.7	346.6
24	255.3	199.5	84	302.6	236.4	44	349.9	273.4	04	397.2	310.3	64	444.4	347.2
25	256.1	200.1	85	303.4	237.0	45	350.7	274.0	05	397.9	310.9	65	445.2	347.8
26	256.9	200.7	86	304.2	237.7	46	351.5	274.6	06	398.7	311.6	66	446.0	348.5
27	257.7	201.3	87	305.0	238.3	47	352.2	275.2	07	399.5	312.2	67	446.8	349.1
28	258.5	201.9	88	305.7	238.9	48	353.0	275.8	08	400.3	312.8	68	447.6	349.7
29	259.3	202.6	89	306.5	239.5	49	353.8	276.4	09	401.1	313.4	69	448.4	350.3
30	260.0	203.2	90	307.3	240.1	50	354.6	277.1	10	401.9	314.0	70	449.2	350.9
331	260.8	203.8	391	308.1	240.7	451	355.4	277.7	511	402.7	314.6	571	450.0	351.6
32	261.6	204.4	92	308.9	241.3	52	356.2	278.3	12	403.5	315.2	72	450.7	352.2
33	262.4	205.0	93	309.7	242.0	53	357.0	278.9	13	404.2	315.8	73	451.5	352.8
34	263.2	205.6	94	310.5	242.6	54	357.8	279.5	14	405.0	316.4	74	452.3	353.4
35	264.0	206.3	95	311.3	243.2	55	358.5	280.1	15	405.8	317.1	75	453.1	354.0
36	264.8	206.9	96	312.1	243.8	56	359.3	280.7	16	406.6	317.7	76	453.9	354.6
37	265.6	207.5	97	312.8	244.4	57	360.1	281.4	17	407.4	318.3	77	454.7	355.2
38	266.3	208.1	98	313.6	245.0	58	360.9	282.0	18	408.2	318.9	78	455.5	355.8
39	267.1	208.7	99	314.4	245.7	59	361.7	282.6	19	409.0	319.5	79	456.3	356.4
40	267.9	209.3	400	315.2	246.3	60	362.5	283.2	20	409.8	320.2	80	457.1	357.1
341	268.7	209.9	401	316.0	246.9	461	363.3	283.8	521	410.6	320.8	581	457.8	357.7
42	269.5	210.6	02	316.8	247.5	62	364.1	284.4	22	411.3	321.4	82	458.6	358.3
43	270.3	211.2	03	317.6	248.1	63	364.9	285.1	23	412.1	322.0	83	459.4	358.9
44	271.1	211.8	04	318.4	248.7	64	365.6	285.7	24	412.9	322.6	84	460.2	359.5
45	271.9	212.4	05	319.1	249.3	65	366.4	286.3	25	413.7	323.2	85	461.0	360.2
46	272.7	213.0	06	319.9	250.0	66	367.2	286.9	26	414.5	323.8	86	461.8	360.8
47	273.4	213.6	07	320.7	250.6	67	368.0	287.5	27	415.3	324.5	87	462.6	361.4
48	274.2	214.3	08	321.5	251.2	68	368.8	288.1	28	416.1	325.1	88	463.3	362.0
49	275.0	214.9	09	322.3	251.8	69	369.6	288.7	29	416.9	325.7	89	464.1	362.6
50	275.8	215.5	10	323.1	252.4	70	370.4	289.3	30	417.6	326.3	90	464.9	363.2
351	276.6	216.1	411	323.9	253.0	471	371.2	290.0	531	418.4	326.9	591	465.7	363.8
52	277.4	216.7	12	324.7	253.7	72	371.9	290.6	32	419.2	327.5	92	466.5	364.4
53	278.2	217.3	13	325.5	254.3	73	372.7	291.2	33	420.0	328.2	93	467.3	365.1
54	279.0	218.0	14	326.2	254.9	74	373.5	291.8	34	420.8	328.8	94	468.1	365.7
55	279.7	218.6	15	327.0	255.5	75	374.3	292.4	35	421.6	329.4	95	468.9	366.3
56	280.5	219.2	16	327.8	256.1	76	375.1	293.1	36	422.4	330.0	96	469.7	366.9
57	281.3	219.8	17	328.6	256.7	77	375.9	293.7	37	423.2	330.6	97	470.5	367.5
58	282.1	220.4	18	329.4	257.4	78	376.7	294.3	38	424.0	331.2	98	471.2	368.1
59	282.9	221.0	19	330.2	258.0	79	377.5	294.9	39	424.7	331.8	99	472.0	368.7
60	283.7	221.6	20	331.0	258.6	80	378.2	295.5	40	425.5	332.5	600	472.8	369.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

52° (128°, 232°, 308°).

TABLE 2.

Difference of Latitude and Departure for 39° (141°, 219°, 321°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	47.4	38.4	121	94.0	76.1	181	140.7	113.9	241	187.3	151.7
2	1.6	1.3	62	48.2	39.0	22	94.8	76.8	82	141.4	114.5	42	188.1	152.3
3	2.3	1.9	63	49.0	39.6	23	95.6	77.4	83	142.2	115.2	43	188.8	152.9
4	3.1	2.5	64	49.7	40.3	24	96.4	78.0	84	143.0	115.8	44	189.6	153.6
5	3.9	3.1	65	50.5	40.9	25	97.1	78.7	85	143.8	116.4	45	190.4	154.2
6	4.7	3.8	66	51.3	41.5	26	97.9	79.3	86	144.5	117.1	46	191.2	154.8
7	5.4	4.4	67	52.1	42.2	27	98.7	79.9	87	145.3	117.7	47	192.0	155.4
8	6.2	5.0	68	52.8	42.8	28	99.5	80.6	88	146.1	118.3	48	192.7	156.1
9	7.0	5.7	69	53.6	43.4	29	100.3	81.2	89	146.9	118.9	49	193.5	156.7
10	7.8	6.3	70	54.4	44.1	30	101.0	81.8	90	147.7	119.6	50	194.3	157.3
11	8.5	6.9	71	55.2	44.7	131	101.8	82.4	191	148.4	120.2	251	195.1	158.0
12	9.3	7.6	72	56.0	45.3	32	102.6	83.1	92	149.2	120.8	52	195.8	158.6
13	10.1	8.2	73	56.7	45.9	33	103.4	83.7	93	150.0	121.5	53	196.6	159.2
14	10.9	8.8	74	57.5	46.6	34	104.1	84.3	94	150.8	122.1	54	197.4	159.8
15	11.7	9.4	75	58.3	47.2	35	104.9	85.0	95	151.5	122.7	55	198.2	160.5
16	12.4	10.1	76	59.1	47.8	36	105.7	85.6	96	152.3	123.3	56	198.9	161.1
17	13.2	10.7	77	59.8	48.5	37	106.5	86.2	97	153.1	124.0	57	199.7	161.7
18	14.0	11.3	78	60.6	49.1	38	107.2	86.8	98	153.9	124.6	58	200.5	162.4
19	14.8	12.0	79	61.4	49.7	39	108.0	87.5	99	154.7	125.2	59	201.3	163.0
20	15.5	12.6	80	62.2	50.3	40	108.8	88.1	200	155.4	125.9	60	202.1	163.6
21	16.3	13.2	81	62.9	51.0	141	109.6	88.7	201	156.2	126.5	261	202.8	164.3
22	17.1	13.8	82	63.7	51.6	42	110.4	89.4	02	157.0	127.1	62	203.6	164.9
23	17.9	14.5	83	64.5	52.2	43	111.1	90.0	03	157.8	127.8	63	204.4	165.5
24	18.7	15.1	84	65.3	52.9	44	111.9	90.6	04	158.5	128.4	64	205.2	166.1
25	19.4	15.7	85	66.1	53.5	45	112.7	91.3	05	159.3	129.0	65	205.9	166.8
26	20.2	16.4	86	66.8	54.1	46	113.5	91.9	06	160.1	129.6	66	206.7	167.4
27	21.0	17.0	87	67.6	54.8	47	114.2	92.5	07	160.9	130.3	67	207.5	168.0
28	21.8	17.6	88	68.4	55.4	48	115.0	93.1	08	161.6	130.9	68	208.3	168.7
29	22.5	18.3	89	69.2	56.0	49	115.8	93.8	09	162.4	131.5	69	209.1	169.3
30	23.3	18.9	90	69.9	56.6	50	116.6	94.4	10	163.2	132.2	70	209.8	169.9
31	24.1	19.5	91	70.7	57.3	151	117.3	95.0	211	164.0	132.8	271	210.6	170.5
32	24.9	20.1	92	71.5	57.9	52	118.1	95.7	12	164.8	133.4	72	211.4	171.2
33	25.6	20.8	93	72.3	58.5	53	118.9	96.3	13	165.5	134.0	73	212.2	171.8
34	26.4	21.4	94	73.1	59.2	54	119.7	96.9	14	166.3	134.7	74	212.9	172.4
35	27.2	22.0	95	73.8	59.8	55	120.5	97.5	15	167.1	135.3	75	213.7	173.1
36	28.0	22.7	96	74.6	60.4	56	121.2	98.2	16	167.9	135.9	76	214.5	173.7
37	28.8	23.3	97	75.4	61.0	57	122.0	98.8	17	168.6	136.6	77	215.3	174.3
38	29.5	23.9	98	76.2	61.7	58	122.8	99.4	18	169.4	137.2	78	216.0	175.0
39	30.3	24.5	99	76.9	62.3	59	123.6	100.1	19	170.2	137.8	79	216.8	175.6
40	31.1	25.2	100	77.7	62.9	60	124.3	100.7	20	171.0	138.5	80	217.6	176.2
41	31.9	25.8	101	78.5	63.6	161	125.1	101.3	221	171.7	139.1	281	218.4	176.8
42	32.6	26.4	02	79.3	64.2	62	125.9	101.9	22	172.5	139.7	82	219.2	177.5
43	33.4	27.1	03	80.0	64.8	63	126.7	102.6	23	173.3	140.3	83	219.9	178.1
44	34.2	27.7	04	80.8	65.4	64	127.5	103.2	24	174.1	141.0	84	220.7	178.7
45	35.0	28.3	05	81.6	66.1	65	128.2	103.8	25	174.9	141.6	85	221.5	179.4
46	35.7	28.9	06	82.4	66.7	66	129.0	104.5	26	175.6	142.2	86	222.3	180.0
47	36.5	29.6	07	83.2	67.3	67	129.8	105.1	27	176.4	142.9	87	223.0	180.6
48	37.3	30.2	08	83.9	68.0	68	130.6	105.7	28	177.2	143.5	88	223.8	181.2
49	38.1	30.8	09	84.7	68.6	69	131.3	106.4	29	178.0	144.1	89	224.6	181.9
50	38.9	31.5	10	85.5	69.2	70	132.1	107.0	30	178.7	144.7	90	225.4	182.5
51	39.6	32.1	111	86.3	69.9	171	132.9	107.6	231	179.5	145.4	291	226.1	183.1
52	40.4	32.7	12	87.0	70.5	72	133.7	108.2	32	180.3	146.0	92	226.9	183.8
53	41.2	33.4	13	87.8	71.1	73	134.4	108.9	33	181.1	146.6	93	227.7	184.4
54	42.0	34.0	14	88.6	71.7	74	135.2	109.5	34	181.9	147.3	94	228.5	185.0
55	42.7	34.6	15	89.4	72.4	75	136.0	110.1	35	182.6	147.9	95	229.3	185.6
56	43.5	35.2	16	90.1	73.0	76	136.8	110.8	36	183.4	148.5	96	230.0	186.3
57	44.3	35.9	17	90.9	73.6	77	137.6	111.4	37	184.2	149.1	97	230.8	186.9
58	45.1	36.5	18	91.7	74.3	78	138.3	112.0	38	185.0	149.8	98	231.6	187.5
59	45.9	37.1	19	92.5	74.9	79	139.1	112.6	39	185.7	150.4	99	232.4	188.2
60	46.6	37.8	20	93.3	75.5	80	139.9	113.3	40	186.5	151.0	300	233.1	188.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

51° (129°, 231°, 309°).

Difference of Latitude and Departure for 39° (141°, 219°, 321°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	233.9	189.4	361	280.6	227.1	421	327.2	264.9	481	373.8	302.6	541	420.4	340.4
02	234.7	190.0	62	281.3	227.8	22	328.0	265.5	82	374.6	303.3	42	421.2	341.0
03	235.5	190.6	63	282.1	228.4	23	328.7	266.2	83	375.4	303.9	43	422.0	341.7
04	236.3	191.3	64	282.9	229.0	24	329.5	266.8	84	376.1	304.5	44	422.7	342.3
05	237.0	191.9	65	283.7	229.7	25	330.3	267.4	85	376.9	305.2	45	423.5	342.9
06	237.8	192.5	66	284.4	230.3	26	331.1	268.0	86	377.7	305.8	46	424.3	343.6
07	238.6	193.2	67	285.2	230.9	27	331.9	268.7	87	378.5	306.4	47	425.1	344.2
08	239.4	193.8	68	286.0	231.5	28	332.6	269.3	88	379.3	307.1	48	425.9	344.8
09	240.1	194.4	69	286.8	232.2	29	333.4	269.9	89	380.0	307.7	49	426.6	345.5
10	240.9	195.0	70	287.6	232.8	30	334.2	270.6	90	380.8	308.3	50	427.4	346.1
311	241.7	195.7	371	288.3	233.4	431	335.0	271.2	491	381.6	308.9	551	428.2	346.7
12	242.5	196.3	72	289.1	234.1	32	335.7	271.8	92	382.4	309.6	52	429.0	347.4
13	243.3	196.9	73	289.9	234.7	33	336.5	272.5	93	383.1	310.2	53	429.7	348.0
14	244.0	197.6	74	290.7	235.3	34	337.3	273.1	94	383.9	310.8	54	430.5	348.6
15	244.8	198.2	75	291.4	236.0	35	338.1	273.7	95	384.7	311.5	55	431.3	349.2
16	245.6	198.8	76	292.2	236.6	36	338.8	274.3	96	385.5	312.1	56	432.1	349.9
17	246.4	199.5	77	293.0	237.2	37	339.6	275.0	97	386.2	312.7	57	432.8	350.5
18	247.1	200.1	78	293.8	237.8	38	340.4	275.6	98	387.0	313.3	58	433.6	351.1
19	247.9	200.7	79	294.5	238.5	39	341.2	276.2	99	387.8	314.0	59	434.4	351.7
20	248.7	201.3	80	295.3	239.1	40	342.0	276.9	500	388.6	314.7	60	435.2	352.4
321	249.5	202.0	381	296.1	239.7	441	342.7	277.5	501	389.4	315.3	561	435.9	353.0
22	250.3	202.6	82	296.9	240.4	42	343.5	278.1	02	390.1	315.9	62	436.7	353.6
23	251.0	203.2	83	297.7	241.0	43	344.3	278.7	03	390.9	316.5	63	437.5	354.3
24	251.8	203.9	84	298.4	241.6	44	345.1	279.4	04	391.7	317.1	64	438.3	354.9
25	252.6	204.5	85	299.2	242.2	45	345.8	280.0	05	392.5	317.8	65	439.1	355.5
26	253.4	205.1	86	300.0	242.9	46	346.6	280.6	06	393.2	318.4	66	439.8	356.2
27	254.1	205.7	87	300.8	243.5	47	347.4	281.3	07	394.0	319.0	67	440.6	356.8
28	254.9	206.4	88	301.5	244.1	48	348.2	281.9	08	394.8	319.6	68	441.4	357.4
29	255.7	207.0	89	302.3	244.8	49	349.0	282.5	09	395.6	320.3	69	442.2	358.1
30	256.5	207.6	90	303.1	245.4	50	349.7	283.2	10	396.3	320.9	70	443.0	358.7
331	257.2	208.3	391	303.9	246.0	451	350.5	283.8	511	397.1	321.6	571	443.7	359.3
32	258.0	208.9	92	304.7	246.7	52	351.3	284.4	12	397.9	322.2	72	444.5	359.9
33	258.8	209.5	93	305.4	247.3	53	352.1	285.0	13	398.7	322.8	73	445.3	360.6
34	259.6	210.2	94	306.2	247.9	54	352.8	285.7	14	399.4	323.4	74	446.1	361.2
35	260.4	210.8	95	307.0	248.5	55	353.6	286.3	15	400.2	324.1	75	446.9	361.8
36	261.1	211.4	96	307.8	249.2	56	354.4	286.9	16	401.0	324.7	76	447.6	362.4
37	261.9	212.0	97	308.5	249.8	57	355.2	287.6	17	401.8	325.3	77	448.4	363.1
38	262.7	212.7	98	309.3	250.4	58	355.9	288.2	18	402.5	325.9	78	449.2	363.7
39	263.5	213.3	99	310.1	251.1	59	356.7	288.8	19	403.3	326.6	79	450.0	364.3
40	264.2	213.9	400	310.9	251.7	60	357.5	289.4	20	404.1	327.2	80	450.7	365.0
341	265.0	214.6	401	311.6	252.3	461	358.3	290.1	521	404.9	327.8	581	451.5	365.6
42	265.8	215.2	02	312.4	252.9	62	359.1	290.7	22	405.7	328.5	82	452.3	366.2
43	266.6	215.8	03	313.2	253.6	63	359.8	291.3	23	406.4	329.1	83	453.1	366.9
44	267.3	216.4	04	314.0	254.2	64	360.6	292.0	24	407.2	329.7	84	453.9	367.5
45	268.1	217.1	05	314.8	254.8	65	361.4	292.6	25	408.0	330.4	85	454.6	368.1
46	268.9	217.7	06	315.5	255.5	66	362.2	293.2	26	408.8	331.0	86	455.4	368.8
47	269.7	218.3	07	316.3	256.1	67	362.9	293.8	27	409.5	331.6	87	456.2	369.4
48	270.5	219.0	08	317.1	256.7	68	363.7	294.5	28	410.3	332.3	88	457.0	370.0
49	271.2	219.6	09	317.9	257.3	69	364.5	295.1	29	411.1	332.9	89	457.8	370.6
50	272.0	220.2	10	318.6	258.0	70	365.3	295.7	30	411.9	333.5	90	458.5	371.3
351	272.8	220.8	411	319.4	258.6	471	366.0	296.4	531	412.6	334.1	591	459.3	371.9
52	273.6	221.5	12	320.2	259.2	72	366.8	297.0	32	413.4	334.8	92	460.1	372.5
53	274.3	222.1	13	321.0	259.9	73	367.6	297.6	33	414.2	335.4	93	460.9	373.2
54	275.1	222.7	14	321.8	260.5	74	368.4	298.3	34	415.0	336.1	94	461.6	373.8
55	275.9	223.4	15	322.5	261.1	75	369.2	298.9	35	415.8	336.7	95	462.4	374.4
56	276.7	224.0	16	323.3	261.8	76	369.9	299.5	36	416.5	337.3	96	463.2	375.1
57	277.5	224.6	17	324.1	262.4	77	370.7	300.1	37	417.3	337.9	97	464.0	375.7
58	278.2	225.3	18	324.9	263.0	78	371.5	300.8	38	418.1	338.5	98	464.8	376.3
59	279.0	225.9	19	325.6	263.6	79	372.3	301.4	39	418.9	339.1	99	465.5	376.9
60	279.8	226.5	20	326.4	264.3	80	373.0	302.0	40	419.6	339.8	600	466.3	377.6
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

51° (129°, 231°, 309°).

TABLE 2.

Difference of Latitude and Departure for 40° (140°, 220°, 320°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	46.7	39.2	121	92.7	77.8	181	138.7	116.3	241	184.6	154.9
2	1.5	1.3	62	47.5	39.9	22	93.5	78.4	82	139.4	117.0	42	185.4	155.6
3	2.3	1.9	63	48.3	40.5	23	94.2	79.1	83	140.2	117.6	43	186.1	156.2
4	3.1	2.6	64	49.0	41.1	24	95.0	79.7	84	141.0	118.3	44	186.9	156.8
5	3.8	3.2	65	49.8	41.8	25	95.8	80.3	85	141.7	118.9	45	187.7	157.5
6	4.6	3.9	66	50.6	42.4	26	96.5	81.0	86	142.5	119.6	46	188.4	158.1
7	5.4	4.5	67	51.3	43.1	27	97.3	81.6	87	143.3	120.2	47	189.2	158.8
8	6.1	5.1	68	52.1	43.7	28	98.1	82.3	88	144.0	120.8	48	190.0	159.4
9	6.9	5.8	69	52.9	44.4	29	98.8	82.9	89	144.8	121.5	49	190.7	160.1
10	7.7	6.4	70	53.6	45.0	30	99.6	83.6	90	145.5	122.1	50	191.5	160.7
11	8.4	7.1	71	54.4	45.6	131	100.4	84.2	191	146.3	122.8	251	192.3	161.3
12	9.2	7.7	72	55.2	46.3	32	101.1	84.8	92	147.1	123.4	52	193.0	162.0
13	10.0	8.4	73	55.9	46.9	33	101.9	85.5	93	147.8	124.1	53	193.8	162.6
14	10.7	9.0	74	56.7	47.6	34	102.6	86.1	94	148.6	124.7	54	194.6	163.3
15	11.5	9.6	75	57.5	48.2	35	103.4	86.8	95	149.4	125.3	55	195.3	163.9
16	12.3	10.3	76	58.2	48.9	36	104.2	87.4	96	150.1	126.0	56	196.1	164.6
17	13.0	10.9	77	59.0	49.5	37	104.9	88.1	97	150.9	126.6	57	196.9	165.2
18	13.8	11.6	78	59.8	50.1	38	105.7	88.7	98	151.7	127.3	58	197.6	165.8
19	14.6	12.2	79	60.5	50.8	39	106.5	89.3	99	152.4	127.9	59	198.4	166.5
20	15.3	12.9	80	61.3	51.4	40	107.2	90.0	200	153.2	128.6	60	199.2	167.1
21	16.1	13.5	81	62.0	52.1	141	108.0	90.6	201	154.0	129.2	261	199.9	167.8
22	16.9	14.1	82	62.8	52.7	42	108.8	91.3	02	154.7	129.8	62	200.7	168.4
23	17.6	14.8	83	63.6	53.4	43	109.5	91.9	03	155.5	130.5	63	201.5	169.1
24	18.4	15.4	84	64.3	54.0	44	110.3	92.6	04	156.3	131.1	64	202.2	169.7
25	19.2	16.1	85	65.1	54.6	45	111.1	93.2	05	157.0	131.8	65	203.0	170.3
26	19.9	16.7	86	65.9	55.3	46	111.8	93.8	06	157.8	132.4	66	203.8	171.0
27	20.7	17.4	87	66.6	55.9	47	112.6	94.5	07	158.6	133.1	67	204.5	171.6
28	21.4	18.0	88	67.4	56.6	48	113.4	95.1	08	159.3	133.7	68	205.3	172.3
29	22.2	18.6	89	68.2	57.2	49	114.1	95.8	09	160.1	134.3	69	206.1	172.9
30	23.0	19.3	90	68.9	57.9	50	114.9	96.4	10	160.9	135.0	70	206.8	173.6
31	23.7	19.9	91	69.7	58.5	151	115.7	97.1	211	161.6	135.6	271	207.6	174.2
32	24.5	20.6	92	70.5	59.1	52	116.4	97.7	12	162.4	136.3	72	208.4	174.8
33	25.3	21.2	93	71.2	59.8	53	117.2	98.3	13	163.2	136.9	73	209.1	175.5
34	26.0	21.9	94	72.0	60.4	54	118.0	99.0	14	163.9	137.6	74	209.9	176.1
35	26.8	22.5	95	72.8	61.1	55	118.7	99.6	15	164.7	138.2	75	210.7	176.8
36	27.6	23.1	96	73.5	61.7	56	119.5	100.3	16	165.5	138.8	76	211.4	177.4
37	28.3	23.8	97	74.3	62.4	57	120.3	100.9	17	166.2	139.5	77	212.2	178.1
38	29.1	24.4	98	75.1	63.0	58	121.0	101.6	18	167.0	140.1	78	213.0	178.7
39	29.9	25.1	99	75.8	63.6	59	121.8	102.2	19	167.8	140.8	79	213.7	179.3
40	30.6	25.7	100	76.6	64.3	60	122.6	102.8	20	168.5	141.4	80	214.5	180.0
41	31.4	26.4	101	77.4	64.9	161	123.3	103.5	221	169.3	142.1	281	215.3	180.6
42	32.2	27.0	02	78.1	65.6	62	124.1	104.1	22	170.1	142.7	82	216.0	181.3
43	32.9	27.6	03	78.9	66.2	63	124.9	104.8	23	170.8	143.3	83	216.8	181.9
44	33.7	28.3	04	79.7	66.8	64	125.6	105.4	24	171.6	144.0	84	217.6	182.6
45	34.5	28.9	05	80.4	67.5	65	126.4	106.1	25	172.4	144.6	85	218.3	183.2
46	35.2	29.6	06	81.2	68.1	66	127.2	106.7	26	173.1	145.3	86	219.1	183.8
47	36.0	30.2	07	82.0	68.8	67	127.9	107.3	27	173.9	145.9	87	219.9	184.5
48	36.8	30.9	08	82.7	69.4	68	128.7	108.0	28	174.7	146.6	88	220.6	185.1
49	37.5	31.5	09	83.5	70.1	69	129.5	108.6	29	175.4	147.2	89	221.4	185.8
50	38.3	32.1	10	84.3	70.7	70	130.2	109.3	30	176.2	147.8	90	222.2	186.4
51	39.1	32.8	111	85.0	71.3	171	131.0	109.9	231	177.0	148.5	291	222.9	187.1
52	39.8	33.4	12	85.8	72.0	72	131.8	110.6	32	177.7	149.1	92	223.7	187.7
53	40.6	34.1	13	86.6	72.6	73	132.5	111.2	33	178.5	149.8	93	224.5	188.3
54	41.4	34.7	14	87.3	73.3	74	133.3	111.8	34	179.3	150.4	94	225.2	189.0
55	42.1	35.4	15	88.1	73.9	75	134.1	112.5	35	180.0	151.1	95	226.0	189.6
56	42.9	36.0	16	88.9	74.6	76	134.8	113.1	36	180.8	151.7	96	226.7	190.3
57	43.7	36.6	17	89.6	75.2	77	135.6	113.8	37	181.6	152.3	97	227.5	190.9
58	44.4	37.3	18	90.4	75.8	78	136.4	114.4	38	182.3	153.0	98	228.3	191.6
59	45.2	37.9	19	91.2	76.5	79	137.1	115.1	39	183.1	153.6	99	229.0	192.2
60	46.0	38.6	20	91.9	77.1	80	137.9	115.7	40	183.9	154.3	300	229.8	192.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

50° (130°, 230°, 310°).

TABLE 2.

Difference of Latitude and Departure for 40° (140°, 220°, 320°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	230.6	193.5	361	276.5	232.1	421	322.5	270.6	481	368.5	309.2	541	414.4	347.7
02	231.3	194.1	62	277.3	232.7	22	323.3	271.3	82	369.2	309.8	42	415.2	348.4
03	232.1	194.8	63	278.1	233.3	23	324.0	271.9	83	370.0	310.5	43	416.0	349.0
04	232.9	195.4	64	278.8	234.0	24	324.8	272.6	84	370.8	311.1	44	416.7	349.7
05	233.6	196.1	65	279.6	234.6	25	325.6	273.2	85	371.5	311.7	45	417.5	350.3
06	234.4	196.7	66	280.4	235.3	26	326.3	273.8	86	372.3	312.4	46	418.3	351.0
07	235.2	197.3	67	281.1	235.9	27	327.1	274.5	87	373.1	313.0	47	419.0	351.6
08	235.9	198.0	68	281.9	236.6	28	327.9	275.1	88	373.8	313.6	48	419.8	352.2
09	236.7	198.6	69	282.7	237.2	29	328.6	275.8	89	374.6	314.3	49	420.6	352.9
10	237.5	199.3	70	283.4	237.8	30	329.4	276.4	90	375.4	314.9	50	421.3	353.5
311	238.2	199.9	371	284.2	238.5	431	330.2	277.1	491	376.1	315.6	551	422.1	354.2
12	239.0	200.6	72	285.0	239.1	32	330.9	277.7	92	376.9	316.2	52	422.9	354.8
13	239.8	201.2	73	285.7	239.7	33	331.7	278.3	93	377.7	316.9	53	423.6	355.5
14	240.5	201.8	74	286.5	240.4	34	332.5	279.0	94	378.4	317.5	54	424.4	356.1
15	241.3	202.5	75	287.3	241.0	35	333.2	279.6	95	379.2	318.2	55	425.2	356.8
16	242.1	203.1	76	288.0	241.7	36	334.0	280.3	96	380.0	318.8	56	425.9	357.4
17	242.8	203.8	77	288.8	242.3	37	334.8	280.9	97	380.7	319.5	57	426.7	358.0
18	243.6	204.4	78	289.6	243.0	38	335.5	281.6	98	381.5	320.1	58	427.5	358.7
19	244.4	205.1	79	290.3	243.6	39	336.3	282.2	99	382.3	320.8	59	428.2	359.3
20	245.1	205.7	80	291.1	244.3	40	337.1	282.8	500	383.0	321.4	60	429.0	360.0
321	245.9	206.3	381	291.9	244.9	441	337.8	283.5	501	383.8	322.0	561	429.8	360.6
22	246.7	207.0	82	292.6	245.6	42	338.6	284.1	02	384.6	322.7	62	430.5	361.2
23	247.4	207.6	83	293.4	246.2	43	339.4	284.8	03	385.3	323.3	63	431.3	361.9
24	248.2	208.3	84	294.2	246.8	44	340.1	285.4	04	386.1	324.0	64	432.1	362.5
25	249.0	208.9	85	294.9	247.5	45	340.9	286.0	05	386.8	324.6	65	432.8	363.2
26	249.7	209.6	86	295.7	248.1	46	341.7	286.7	06	387.6	325.2	66	433.6	363.8
27	250.5	210.2	87	296.5	248.8	47	342.4	287.3	07	388.4	325.9	67	434.3	364.5
28	251.3	210.8	88	297.2	249.4	48	343.2	288.0	08	389.2	326.5	68	435.1	365.1
29	252.0	211.5	89	298.0	250.1	49	344.0	288.6	09	389.9	327.1	69	435.9	365.8
30	252.8	212.1	90	298.8	250.7	50	344.7	289.3	10	390.7	327.8	70	436.6	366.4
331	253.6	212.8	391	299.5	251.3	451	345.5	289.9	511	391.5	328.4	571	437.4	367.0
32	254.3	213.4	92	300.3	252.0	52	346.3	290.5	12	392.2	329.1	72	438.2	367.7
33	255.1	214.1	93	301.1	252.6	53	347.0	291.2	13	393.0	329.7	73	438.9	368.3
34	255.9	214.7	94	301.8	253.3	54	347.8	291.8	14	393.8	330.4	74	439.7	369.0
35	256.6	215.3	95	302.6	253.9	55	348.6	292.5	15	394.5	331.0	75	440.5	369.6
36	257.4	216.0	96	303.4	254.6	56	349.3	293.1	16	395.3	331.6	76	441.2	370.2
37	258.2	216.6	97	304.1	255.2	57	350.1	293.8	17	396.1	332.3	77	442.0	370.9
38	258.9	217.3	98	304.9	255.8	58	350.8	294.4	18	396.8	332.9	78	442.8	371.5
39	259.7	217.9	99	305.7	256.5	59	351.6	295.0	19	397.6	333.6	79	443.5	372.2
40	260.5	218.6	400	306.4	257.1	60	352.4	295.7	20	398.3	334.2	80	444.3	372.8
341	261.2	219.2	401	307.2	257.8	461	353.1	296.3	521	399.1	334.9	581	445.1	373.5
42	262.0	219.8	02	308.0	258.4	62	353.9	297.0	22	399.9	335.5	82	445.8	374.1
43	262.8	220.5	03	308.7	259.1	63	354.7	297.6	23	400.6	336.1	83	446.6	374.8
44	263.5	221.1	04	309.5	259.7	64	355.4	298.3	24	401.4	336.8	84	447.4	375.4
45	264.3	221.8	05	310.2	260.3	65	356.2	298.9	25	402.2	337.4	85	448.1	376.0
46	265.1	222.4	06	311.0	261.0	66	357.0	299.5	26	402.9	338.1	86	448.9	376.7
47	265.8	223.1	07	311.8	261.6	67	357.7	300.2	27	403.7	338.7	87	449.7	377.3
48	266.6	223.7	08	312.5	262.3	68	358.5	300.8	28	404.5	339.4	88	450.4	378.0
49	267.4	224.3	09	313.3	262.9	69	359.3	301.5	29	405.2	340.0	89	451.2	378.6
50	268.1	225.0	10	314.1	263.6	70	360.0	302.1	30	406.0	340.6	90	452.0	379.2
351	268.9	225.6	411	314.8	264.2	471	360.8	302.8	531	406.8	341.3	591	452.7	379.9
52	269.6	226.3	12	315.6	264.8	72	361.6	303.4	32	407.5	341.9	92	453.5	380.5
53	270.4	226.9	13	316.4	265.5	73	362.3	304.0	33	408.3	342.6	93	454.3	381.2
54	271.2	227.6	14	317.1	266.1	74	363.1	304.7	34	409.1	343.2	94	455.0	381.8
55	271.9	228.2	15	317.9	266.8	75	363.9	305.3	35	409.8	343.9	95	455.8	382.4
56	272.7	228.8	16	318.7	267.4	76	364.6	306.0	36	410.6	344.5	96	456.6	383.1
57	273.5	229.5	17	319.4	268.1	77	365.4	306.6	37	411.4	345.2	97	457.3	383.7
58	274.2	230.1	18	320.2	268.7	78	366.2	307.3	38	412.1	345.8	98	458.1	384.4
59	275.0	230.8	19	321.0	269.3	79	366.9	307.9	39	412.9	346.4	99	458.9	385.0
60	275.8	231.4	20	321.7	270.0	80	367.7	308.5	40	413.7	347.1	600	459.6	385.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

50° (130°, 230°, 310°).

TABLE 2.

Difference of Latitude and Departure for 41° (139°, 221°, 319°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.7	61	46.0	40.0	121	91.3	79.4	181	136.6	118.7	241	181.9	158.1
2	1.5	1.3	62	46.8	40.7	22	92.1	80.0	82	137.4	119.4	42	182.6	158.8
3	2.3	2.0	63	47.5	41.3	23	92.8	80.7	83	138.1	120.1	43	183.4	159.4
4	3.0	2.6	64	48.3	42.0	24	93.6	81.4	84	138.9	120.7	44	184.1	160.1
5	3.8	3.3	65	49.1	42.6	25	94.3	82.0	85	139.6	121.4	45	184.9	160.7
6	4.5	3.9	66	49.8	43.3	26	95.1	82.7	86	140.4	122.0	46	185.7	161.4
7	5.3	4.6	67	50.6	44.0	27	95.8	83.3	87	141.1	122.7	47	186.4	162.0
8	6.0	5.2	68	51.3	44.6	28	96.6	84.0	88	141.9	123.3	48	187.2	162.7
9	6.8	5.9	69	52.1	45.3	29	97.4	84.6	89	142.6	124.0	49	187.9	163.4
10	7.5	6.6	70	52.8	45.9	30	98.1	85.3	90	143.4	124.7	50	188.7	164.0
11	8.3	7.2	71	53.6	46.6	131	98.9	85.9	191	144.1	125.3	251	189.4	164.7
12	9.1	7.9	72	54.3	47.2	32	99.6	86.6	92	144.9	126.0	52	190.2	165.3
13	9.8	8.5	73	55.1	47.9	33	100.4	87.3	93	145.7	126.6	53	190.9	166.0
14	10.6	9.2	74	55.8	48.5	34	101.1	87.9	94	146.4	127.3	54	191.7	166.6
15	11.3	9.8	75	56.6	49.2	35	101.9	88.6	95	147.2	127.9	55	192.5	167.3
16	12.1	10.5	76	57.4	49.9	36	102.6	89.2	96	147.9	128.6	56	193.2	168.0
17	12.8	11.2	77	58.1	50.5	37	103.4	89.9	97	148.7	129.2	57	194.0	168.6
18	13.6	11.8	78	58.9	51.2	38	104.1	90.5	98	149.4	129.9	58	194.7	169.3
19	14.3	12.5	79	59.6	51.8	39	104.9	91.2	99	150.2	130.6	59	195.5	169.9
20	15.1	13.1	80	60.4	52.5	40	105.7	91.8	200	150.9	131.2	60	196.2	170.6
21	15.8	13.8	81	61.1	53.1	141	106.4	92.5	201	151.7	131.9	261	197.0	171.2
22	16.6	14.4	82	61.9	53.8	42	107.2	93.2	02	152.5	132.5	62	197.7	171.9
23	17.4	15.1	83	62.6	54.5	43	107.9	93.8	03	153.2	133.2	63	198.5	172.5
24	18.1	15.7	84	63.4	55.1	44	108.7	94.5	04	154.0	133.8	64	199.2	173.2
25	18.9	16.4	85	64.2	55.8	45	109.4	95.1	05	154.7	134.5	65	200.0	173.9
26	19.6	17.1	86	64.9	56.4	46	110.2	95.8	06	155.5	135.1	66	200.8	174.5
27	20.4	17.7	87	65.7	57.1	47	110.9	96.4	07	156.2	135.8	67	201.5	175.2
28	21.1	18.4	88	66.4	57.7	48	111.7	97.1	08	157.0	136.5	68	202.3	175.8
29	21.9	19.0	89	67.2	58.4	49	112.5	97.8	09	157.7	137.1	69	203.0	176.5
30	22.6	19.7	90	67.9	59.0	50	113.2	98.4	10	158.5	137.8	70	203.8	177.1
31	23.4	20.3	91	68.7	59.7	151	114.0	99.1	211	159.2	138.4	271	204.5	177.8
32	24.2	21.0	92	69.4	60.4	52	114.7	99.7	12	160.0	139.1	72	205.3	178.4
33	24.9	21.6	93	70.2	61.0	53	115.5	100.4	13	160.8	139.7	73	206.0	179.1
34	25.7	22.3	94	70.9	61.7	54	116.2	101.0	14	161.5	140.4	74	206.8	179.8
35	26.4	23.0	95	71.7	62.3	55	117.0	101.7	15	162.3	141.1	75	207.5	180.4
36	27.2	23.6	96	72.5	63.0	56	117.7	102.3	16	163.0	141.7	76	208.3	181.1
37	27.9	24.3	97	73.2	63.6	57	118.5	103.0	17	163.8	142.4	77	209.1	181.7
38	28.7	24.9	98	74.0	64.3	58	119.2	103.7	18	164.5	143.0	78	209.8	182.4
39	29.4	25.6	99	74.7	64.9	59	120.0	104.3	19	165.3	143.7	79	210.6	183.0
40	30.2	26.2	100	75.5	65.6	60	120.8	105.0	20	166.0	144.3	80	211.3	183.7
41	30.9	26.9	101	76.2	66.3	161	121.5	105.6	221	166.8	145.0	281	212.1	184.4
42	31.7	27.6	02	77.0	66.9	62	122.3	106.3	22	167.5	145.6	82	212.8	185.0
43	32.5	28.2	03	77.7	67.6	63	123.0	106.9	23	168.3	146.3	83	213.6	185.7
44	33.2	28.9	04	78.5	68.2	64	123.8	107.6	24	169.1	147.0	84	214.3	186.3
45	34.0	29.5	05	79.2	68.9	65	124.5	108.2	25	169.8	147.6	85	215.1	187.0
46	34.7	30.2	06	80.0	69.5	66	125.3	108.9	26	170.6	148.3	86	215.8	187.6
47	35.5	30.8	07	80.8	70.2	67	126.0	109.6	27	171.3	148.9	87	216.6	188.3
48	36.2	31.5	08	81.5	70.9	68	126.8	110.2	28	172.1	149.6	88	217.4	188.9
49	37.0	32.1	09	82.3	71.5	69	127.5	110.9	29	172.8	150.2	89	218.1	189.6
50	37.7	32.8	10	83.0	72.2	70	128.3	111.5	30	173.6	150.9	90	218.9	190.3
51	38.5	33.5	111	83.8	72.8	171	129.1	112.2	231	174.3	151.5	291	219.6	190.9
52	39.2	34.1	12	84.5	73.5	72	129.8	112.8	32	175.1	152.2	92	220.4	191.6
53	40.0	34.8	13	85.3	74.1	73	130.6	113.5	33	175.8	152.9	93	221.1	192.2
54	40.8	35.4	14	86.0	74.8	74	131.3	114.2	34	176.6	153.5	94	221.9	192.9
55	41.5	36.1	15	86.8	75.4	75	132.1	114.8	35	177.4	154.2	95	222.6	193.5
56	42.3	36.7	16	87.5	76.1	76	132.8	115.5	36	178.1	154.8	96	223.4	194.2
57	43.0	37.4	17	88.3	76.8	77	133.6	116.1	37	178.9	155.5	97	224.1	194.8
58	43.8	38.1	18	89.1	77.4	78	134.3	116.8	38	179.6	156.1	98	224.9	195.5
59	44.5	38.7	19	89.8	78.1	79	135.1	117.4	39	180.4	156.8	99	225.7	196.2
60	45.3	39.4	20	90.6	78.7	80	135.8	118.1	40	181.1	157.5	300	226.4	196.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

49° (131°, 229°, 311°).

TABLE 2.

Difference of Latitude and Departure for 41° (139°, 221°, 319°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	227.2	197.5	361	272.5	236.9	421	317.7	276.2	481	363.0	315.6	541	408.3	354.9
02	227.9	198.1	62	273.2	237.5	22	318.5	276.9	82	363.8	316.2	42	409.0	355.6
03	228.7	198.8	63	274.0	238.2	23	319.2	277.5	83	364.5	316.9	43	409.8	356.2
04	229.4	199.4	64	274.7	238.8	24	320.0	278.2	84	365.3	317.5	44	410.6	356.9
05	230.2	200.1	65	275.5	239.5	25	320.8	278.8	85	366.0	318.2	45	411.3	357.5
06	230.9	200.8	66	276.2	240.1	26	321.5	279.5	86	366.8	318.8	46	412.1	358.2
07	231.7	201.4	67	277.0	240.8	27	322.3	280.1	87	367.5	319.5	47	412.8	358.8
08	232.5	202.1	68	277.7	241.4	28	323.0	280.8	88	368.3	320.1	48	413.6	359.5
09	233.2	202.7	69	278.5	242.1	29	323.8	281.5	89	369.0	320.8	49	414.3	360.2
10	234.0	203.4	70	279.2	242.7	30	324.5	282.1	90	369.8	321.5	50	415.1	360.8
311	234.7	204.0	371	280.0	243.4	431	325.3	282.8	491	370.6	322.1	551	415.8	361.5
12	235.5	204.7	72	280.8	244.1	32	326.0	283.4	92	371.3	322.8	52	416.6	362.1
13	236.2	205.4	73	281.5	244.7	33	326.8	284.1	93	372.1	323.4	53	417.3	362.8
14	237.0	206.0	74	282.3	245.4	34	327.5	284.7	94	372.8	324.1	54	418.1	363.4
15	237.7	206.7	75	283.0	246.0	35	328.3	285.4	95	373.6	324.7	55	418.9	364.1
16	238.5	207.3	76	283.8	246.7	36	329.1	286.0	96	374.3	325.4	56	419.6	364.8
17	239.2	208.0	77	284.5	247.3	37	329.8	286.7	97	375.1	326.0	57	420.4	365.4
18	240.0	208.6	78	285.3	248.0	38	330.6	287.4	98	375.8	326.7	58	421.1	366.1
19	240.8	209.3	79	286.0	248.7	39	331.3	288.0	99	376.6	327.4	59	421.9	366.7
20	241.5	209.9	80	286.8	249.3	40	332.1	288.7	500	377.3	328.0	60	422.6	367.4
321	242.3	210.6	381	287.5	250.0	441	332.8	289.3	501	378.1	328.7	561	423.4	368.0
22	243.0	211.3	82	288.3	250.6	42	333.6	290.0	02	378.9	329.3	62	424.1	368.7
23	243.8	211.9	83	289.1	251.3	43	334.3	290.6	03	379.6	330.0	63	424.9	369.4
24	244.5	212.6	84	289.8	251.9	44	335.1	291.3	04	380.4	330.6	64	425.7	370.0
25	245.3	213.2	85	290.6	252.6	45	335.8	292.0	05	381.1	331.3	65	426.4	370.7
26	246.0	213.9	86	291.3	253.2	46	336.6	292.6	06	381.9	332.0	66	427.2	371.3
27	246.8	214.5	87	292.1	253.9	47	337.4	293.3	07	382.6	332.6	67	427.9	372.0
28	247.5	215.2	88	292.8	254.6	48	338.1	293.9	08	383.4	333.3	68	428.7	372.6
29	248.3	215.9	89	293.6	255.2	49	338.9	294.6	09	384.1	333.9	69	429.4	373.3
30	249.1	216.5	90	294.3	255.9	50	339.6	295.2	10	384.9	334.6	70	430.2	374.0
331	249.8	217.2	391	295.1	256.5	451	340.4	295.9	511	385.7	335.2	571	430.9	374.6
32	250.6	217.8	92	295.8	257.2	52	341.1	296.5	12	386.4	335.9	72	431.7	375.3
33	251.3	218.5	93	296.6	257.8	53	341.9	297.2	13	387.2	336.5	73	432.4	375.9
34	252.1	219.1	94	297.4	258.5	54	342.6	297.9	14	387.9	337.2	74	433.2	376.6
35	252.8	219.8	95	298.1	259.2	55	343.4	298.5	15	388.7	337.9	75	434.0	377.2
36	253.6	220.4	96	298.9	259.8	56	344.1	299.2	16	389.4	338.5	76	434.7	377.9
37	254.3	221.1	97	299.6	260.5	57	344.9	299.8	17	390.2	339.2	77	435.5	378.5
38	255.1	221.8	98	300.4	261.1	58	345.7	300.5	18	390.9	339.8	78	436.2	379.2
39	255.8	222.4	99	301.1	261.8	59	346.4	301.1	19	391.7	340.5	79	437.0	379.8
40	256.6	223.1	400	301.9	262.4	60	347.2	301.8	20	392.4	341.1	80	437.7	380.5
341	257.4	223.7	401	302.6	263.1	461	347.9	302.5	521	393.2	341.8	581	438.5	381.2
42	258.1	224.4	02	303.4	263.7	62	348.7	303.1	22	394.0	342.5	82	439.2	381.8
43	258.9	225.0	03	304.2	264.4	63	349.4	303.8	23	394.7	343.1	83	440.0	382.5
44	259.6	225.7	04	304.9	265.1	64	350.2	304.4	24	395.5	343.8	84	440.7	383.2
45	260.4	226.3	05	305.7	265.7	65	350.9	305.1	25	396.2	344.4	85	441.5	383.8
46	261.1	227.0	06	306.4	266.4	66	351.7	305.7	26	397.0	345.1	86	442.3	384.5
47	261.9	227.7	07	307.2	267.0	67	352.5	306.4	27	397.7	345.7	87	443.0	385.1
48	262.6	228.3	08	307.9	267.7	68	353.2	307.0	28	398.5	346.4	88	443.8	385.8
49	263.4	229.0	09	308.7	268.3	69	354.0	307.7	29	399.2	347.0	89	444.5	386.4
50	264.2	229.6	10	309.4	269.0	70	354.7	308.4	30	400.0	347.7	90	445.3	387.1
351	264.9	230.3	411	310.2	269.6	471	355.5	309.0	531	400.7	348.4	591	446.0	387.7
52	265.7	230.9	12	310.9	270.3	72	356.2	309.7	32	401.5	349.0	92	446.8	388.4
53	266.4	231.6	13	311.7	271.0	73	357.0	310.3	33	402.2	349.7	93	447.5	389.1
54	267.2	232.3	14	312.5	271.6	74	357.7	311.0	34	403.0	350.3	94	448.3	389.7
55	267.9	232.9	15	313.2	272.3	75	358.5	311.6	35	403.8	351.0	95	449.1	390.4
56	268.7	233.6	16	314.0	272.9	76	359.2	312.3	36	404.5	351.6	96	449.8	391.0
57	269.4	234.2	17	314.7	273.6	77	360.0	312.9	37	405.3	352.3	97	450.6	391.7
58	270.2	234.9	18	315.5	274.2	78	360.8	313.6	38	406.0	352.9	98	451.3	392.3
59	270.9	235.5	19	316.2	274.9	79	361.5	314.3	39	406.8	353.6	99	452.1	393.0
60	271.7	236.2	20	317.0	275.6	80	362.3	314.9	40	407.5	354.3	600	452.8	393.6
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

49° (131°, 229°, 311°).

6583—06——29

TABLE 2.

Difference of Latitude and Departure for 42° (138°, 222°, 318°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.7	0.7	61	45.3	40.8	121	89.9	81.0	181	134.5	121.1	241	179.1	161.3
2	1.5	1.3	62	46.1	41.5	22	90.7	81.6	82	135.3	121.8	42	179.8	161.9
3	2.2	2.0	63	46.8	42.2	23	91.4	82.3	83	136.0	122.5	43	180.6	162.6
4	3.0	2.7	64	47.6	42.8	24	92.1	83.0	84	136.7	123.1	44	181.3	163.3
5	3.7	3.3	65	48.3	43.5	25	92.9	83.6	85	137.5	123.8	45	182.1	163.9
6	4.5	4.0	66	49.0	44.2	26	93.6	84.3	86	138.2	124.5	46	182.8	164.6
7	5.2	4.7	67	49.8	44.8	27	94.4	85.0	87	139.0	125.1	47	183.6	165.3
8	5.9	5.4	68	50.5	45.5	28	95.1	85.6	88	139.7	125.8	48	184.3	165.9
9	6.7	6.0	69	51.3	46.2	29	95.9	86.3	89	140.5	126.5	49	185.0	166.6
10	7.4	6.7	70	52.0	46.8	30	96.6	87.0	90	141.2	127.1	50	185.8	167.3
11	8.2	7.4	71	52.8	47.5	131	97.4	87.7	191	141.9	127.8	251	186.5	168.0
12	8.9	8.0	72	53.5	48.2	32	98.1	88.3	92	142.7	128.5	52	187.3	168.6
13	9.7	8.7	73	54.2	48.8	33	98.8	89.0	93	143.4	129.1	53	188.0	169.3
14	10.4	9.4	74	55.0	49.5	34	99.6	89.7	94	144.2	129.8	54	188.8	170.0
15	11.1	10.0	75	55.7	50.2	35	100.3	90.3	95	144.9	130.5	55	189.5	170.6
16	11.9	10.7	76	56.5	50.9	36	101.1	91.0	96	145.7	131.1	56	190.2	171.3
17	12.6	11.4	77	57.2	51.5	37	101.8	91.7	97	146.4	131.8	57	191.0	172.0
18	13.4	12.0	78	58.0	52.2	38	102.6	92.3	98	147.1	132.5	58	191.7	172.6
19	14.1	12.7	79	58.7	52.9	39	103.3	93.0	99	147.9	133.2	59	192.5	173.3
20	14.9	13.4	80	59.5	53.5	40	104.0	93.7	200	148.6	133.8	60	193.2	174.0
21	15.6	14.1	81	60.2	54.2	141	104.8	94.3	201	149.4	134.5	261	194.0	174.6
22	16.3	14.7	82	60.9	54.9	42	105.5	95.0	02	150.1	135.2	62	194.7	175.3
23	17.1	15.4	83	61.7	55.5	43	106.3	95.7	03	150.9	135.8	63	195.4	176.0
24	17.8	16.1	84	62.4	56.2	44	107.0	96.4	04	151.6	136.5	64	196.2	176.7
25	18.6	16.7	85	63.2	56.9	45	107.8	97.0	05	152.3	137.2	65	196.9	177.3
26	19.3	17.4	86	63.9	57.5	46	108.5	97.7	06	153.1	137.8	66	197.7	178.0
27	20.1	18.1	87	64.7	58.2	47	109.2	98.4	07	153.8	138.5	67	198.4	178.7
28	20.8	18.7	88	65.4	58.9	48	110.0	99.0	08	154.6	139.2	68	199.2	179.3
29	21.6	19.4	89	66.1	59.6	49	110.7	99.7	09	155.3	139.8	69	199.9	180.0
30	22.3	20.1	90	66.9	60.2	50	111.5	100.4	10	156.1	140.5	70	200.6	180.7
31	23.0	20.7	91	67.6	60.9	151	112.2	101.0	211	156.8	141.2	271	201.4	181.3
32	23.8	21.4	92	68.4	61.6	52	113.0	101.7	12	157.5	141.9	72	202.1	182.0
33	24.5	22.1	93	69.1	62.2	53	113.7	102.4	13	158.3	142.5	73	202.9	182.7
34	25.3	22.8	94	69.9	62.9	54	114.4	103.0	14	159.0	143.2	74	203.6	183.3
35	26.0	23.4	95	70.6	63.6	55	115.2	103.7	15	159.8	143.9	75	204.4	184.0
36	26.8	24.1	96	71.3	64.2	56	115.9	104.4	16	160.5	144.5	76	205.1	184.7
37	27.5	24.8	97	72.1	64.9	57	116.7	105.1	17	161.3	145.2	77	205.9	185.3
38	28.2	25.4	98	72.8	65.6	58	117.4	105.7	18	162.0	145.9	78	206.6	186.0
39	29.0	26.1	99	73.6	66.2	59	118.2	106.4	19	162.7	146.5	79	207.3	186.7
40	29.7	26.8	100	74.3	66.9	60	118.9	107.1	20	163.5	147.2	80	208.1	187.4
41	30.5	27.4	101	75.1	67.6	161	119.6	107.7	221	164.2	147.9	281	208.8	188.0
42	31.2	28.1	02	75.8	68.3	62	120.4	108.4	22	165.0	148.5	82	209.6	188.7
43	32.0	28.8	03	76.5	68.9	63	121.1	109.1	23	165.7	149.2	83	210.3	189.4
44	32.7	29.4	04	77.3	69.6	64	121.9	109.7	24	166.5	149.9	84	211.1	190.0
45	33.4	30.1	05	78.0	70.3	65	122.6	110.4	25	167.2	150.6	85	211.8	190.7
46	34.2	30.8	06	78.8	70.9	66	123.4	111.1	26	168.0	151.2	86	212.5	191.4
47	34.9	31.4	07	79.5	71.6	67	124.1	111.7	27	168.7	151.9	87	213.3	192.0
48	35.7	32.1	08	80.3	72.3	68	124.8	112.4	28	169.4	152.6	88	214.0	192.7
49	36.4	32.8	09	81.0	72.9	69	125.6	113.1	29	170.2	153.2	89	214.8	193.4
50	37.2	33.5	10	81.7	73.6	70	126.3	113.8	30	170.9	153.9	90	215.5	194.0
51	37.9	34.1	111	82.5	74.3	171	127.1	114.4	231	171.7	154.6	291	216.3	194.7
52	38.6	34.8	12	83.2	74.9	72	127.8	115.1	32	172.4	155.2	92	217.0	195.4
53	39.4	35.5	13	84.0	75.6	73	128.6	115.8	33	173.2	155.9	93	217.7	196.1
54	40.1	36.1	14	84.7	76.3	74	129.3	116.4	34	173.9	156.6	94	218.5	196.7
55	40.9	36.8	15	85.5	77.0	75	130.1	117.1	35	174.6	157.2	95	219.2	197.4
56	41.6	37.5	16	86.2	77.6	76	130.8	117.8	36	175.4	157.9	96	220.0	198.1
57	42.4	38.1	17	86.9	78.3	77	131.5	118.4	37	176.1	158.6	97	220.7	198.7
58	43.1	38.8	18	87.7	79.0	78	132.3	119.1	38	176.9	159.3	98	221.5	199.4
59	43.8	39.5	19	88.4	79.6	79	133.0	119.8	39	177.6	159.9	99	222.2	200.1
60	44.6	40.1	20	89.2	80.3	80	133.8	120.4	40	178.4	160.6	300	222.9	200.7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

48° (132°, 228°, 312).

TABLE 2.

Difference of Latitude and Departure for 42° (138°, 222°, 318°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	223.7	201.4	361	268.3	241.6	421	312.9	281.7	481	357.5	321.9	541	402.1	362.0
02	224.4	202.1	62	269.0	242.2	22	313.6	282.4	82	358.2	322.5	42	402.8	362.7
03	225.2	202.8	63	269.8	242.9	23	314.4	283.0	83	358.9	323.2	43	403.5	363.3
04	225.9	203.4	64	270.5	243.6	24	315.1	283.7	84	359.7	323.9	44	404.3	364.0
05	226.6	204.1	65	271.2	244.2	25	315.8	284.4	85	360.4	324.6	45	405.0	364.7
06	227.4	204.8	66	272.0	244.9	26	316.6	285.1	86	361.2	325.2	46	405.8	365.4
07	228.1	205.4	67	272.7	245.6	27	317.3	285.7	87	361.9	325.9	47	406.5	366.0
08	228.9	206.1	68	273.5	246.2	48	318.1	286.4	88	362.7	326.6	48	407.2	366.7
09	229.6	206.8	69	274.2	246.9	29	318.8	287.1	89	363.4	327.2	49	408.0	367.4
10	230.4	207.4	70	275.0	247.6	30	319.6	287.7	90	364.1	327.9	50	408.7	368.0
311	231.1	208.1	371	275.7	248.3	431	320.3	288.4	491	364.9	328.6	551	409.5	368.7
12	231.9	208.8	72	276.5	248.9	32	321.0	289.1	92	365.6	329.2	52	410.2	369.4
13	232.6	209.4	73	277.2	249.6	33	321.8	289.7	93	366.4	329.9	53	411.0	370.0
14	233.3	210.1	74	277.9	250.3	34	322.5	290.4	94	367.1	330.6	54	411.7	370.7
15	234.1	210.8	75	278.7	250.9	35	323.3	291.1	95	367.9	331.3	55	412.4	371.4
16	234.8	211.5	76	279.4	251.6	36	324.0	291.7	96	368.6	331.9	56	413.2	372.0
17	235.6	212.1	77	280.2	252.3	37	324.8	292.4	97	369.3	332.6	57	413.9	372.7
18	236.3	212.8	78	280.9	252.9	38	325.5	293.1	98	370.1	333.3	58	414.7	373.4
19	237.1	213.5	79	281.7	253.6	39	326.2	293.8	99	370.8	333.9	59	415.4	374.1
20	237.8	214.1	80	282.4	254.3	40	327.0	294.4	500	371.6	334.6	60	416.2	374.7
321	238.6	214.8	381	283.1	254.9	441	327.7	295.1	501	372.3	335.3	561	416.9	375.4
22	239.3	215.5	82	283.9	255.6	42	328.5	295.8	02	373.1	335.9	62	417.6	376.1
23	240.0	216.1	83	284.6	256.3	43	329.2	296.4	03	373.8	336.6	63	418.4	376.7
24	240.8	216.8	84	285.4	257.0	44	330.0	297.1	04	374.5	337.2	64	419.1	377.4
25	241.5	217.5	85	286.1	257.6	45	330.7	297.8	05	375.3	337.9	65	419.9	378.1
26	242.3	218.1	86	286.9	258.3	46	331.4	298.4	06	376.0	338.6	66	420.6	378.7
27	243.0	218.8	87	287.6	259.0	47	332.2	299.1	07	376.8	339.3	67	421.4	379.4
28	243.8	219.5	88	288.3	259.6	48	332.9	299.8	08	377.5	339.9	68	422.1	380.1
29	244.5	220.1	89	289.1	260.3	49	333.7	300.4	09	378.3	340.6	69	422.8	380.7
30	245.2	220.8	90	289.8	261.0	50	334.4	301.1	10	379.0	341.3	70	423.6	381.4
331	246.0	221.5	391	290.6	261.6	451	335.2	301.8	511	379.7	341.9	571	424.3	382.1
32	246.7	222.2	92	291.3	262.3	52	335.9	302.5	12	380.5	342.6	72	425.1	382.8
33	247.5	222.8	93	292.1	263.0	53	336.6	303.1	13	381.2	343.3	73	425.8	383.4
34	248.2	223.5	94	292.8	263.6	54	337.4	303.8	14	382.0	343.9	74	426.6	384.1
35	249.0	224.2	95	293.5	264.3	55	338.1	304.5	15	382.7	344.6	75	427.3	384.8
36	249.7	224.8	96	294.3	265.0	56	338.9	305.1	16	383.5	345.3	76	428.0	385.4
37	250.4	225.5	97	295.0	265.7	57	339.6	305.8	17	384.2	346.0	77	428.8	386.1
38	251.2	226.2	98	295.8	266.3	58	340.4	306.5	18	384.9	346.6	78	429.5	386.8
39	251.9	226.8	99	296.5	267.0	59	341.1	307.1	19	385.7	347.3	79	430.3	387.4
40	252.7	227.5	400	297.3	267.7	60	341.8	307.8	20	386.4	348.0	80	431.0	388.1
341	253.4	228.2	401	298.0	268.3	461	342.6	308.5	521	387.2	348.6	581	431.8	388.8
42	254.2	228.8	02	298.7	269.0	62	343.3	309.1	22	387.9	349.3	82	432.5	389.4
43	254.9	229.5	03	299.5	269.7	63	344.1	309.8	23	388.7	350.0	83	433.2	390.1
44	255.6	230.2	04	300.2	270.3	64	344.8	310.5	24	389.4	350.6	84	434.0	390.8
45	256.4	230.9	05	301.0	271.0	65	345.6	311.2	25	390.1	351.3	85	434.7	391.4
46	257.1	231.5	06	301.7	271.7	66	346.3	311.8	26	390.9	352.0	86	435.5	392.1
47	257.9	232.2	07	302.5	272.3	67	347.0	312.5	27	391.6	352.6	87	436.2	392.8
48	258.6	232.9	08	303.2	273.0	68	347.8	313.2	28	392.4	353.3	88	437.0	393.4
49	259.4	233.5	09	303.9	273.7	69	348.5	313.8	29	393.1	354.0	89	437.7	394.1
50	260.1	234.2	10	304.7	274.3	70	349.3	314.5	30	393.9	354.6	90	438.4	394.8
351	260.8	234.9	411	305.4	275.0	471	350.0	315.2	531	394.6	355.3	591	439.2	395.4
52	261.6	235.5	12	306.2	275.7	72	350.8	315.8	32	395.3	356.0	92	440.0	396.1
53	262.3	236.2	13	306.9	276.4	73	351.5	316.5	33	396.1	356.6	93	440.7	396.8
54	263.1	236.9	14	307.7	277.0	74	352.3	317.2	34	396.8	357.3	94	441.4	397.5
55	263.8	237.5	15	308.4	277.7	75	353.0	317.8	35	397.6	358.0	95	442.2	398.1
56	264.6	238.2	16	309.1	278.4	76	353.7	318.5	36	398.3	358.6	96	442.9	398.8
57	265.3	238.9	17	309.9	279.0	77	354.5	319.2	37	399.1	359.3	97	443.7	399.5
58	266.0	239.6	18	310.6	279.7	78	355.2	319.9	38	399.8	360.0	98	444.4	400.1
59	266.8	240.2	19	311.4	280.4	79	356.0	320.5	39	400.6	360.6	99	445.2	400.8
60	267.5	240.9	20	312.1	281.0	80	356.7	321.2	40	401.3	361.3	600	445.9	401.5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

48° (132°, 228°, 312°).

TABLE 2.

Difference of Latitude and Departure for 43° (137°, 223°, 317°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.7	0.7	61	44.6	41.6	121	88.5	82.5	181	132.4	123.4	241	176.3	164.4
2	1.5	1.4	62	45.3	42.3	22	89.2	83.2	82	133.1	124.1	42	177.0	165.0
3	2.2	2.0	63	46.1	43.0	23	90.0	83.9	83	133.8	124.8	43	177.7	165.7
4	2.9	2.7	64	46.8	43.6	24	90.7	84.6	84	134.6	125.5	44	178.5	166.4
5	3.7	3.4	65	47.5	44.3	25	91.4	85.2	85	135.3	126.2	45	179.2	167.1
6	4.4	4.1	66	48.3	45.0	26	92.2	85.9	86	136.0	126.9	46	179.9	167.8
7	5.1	4.8	67	49.0	45.7	27	92.9	86.6	87	136.8	127.5	47	180.6	168.5
8	5.9	5.5	68	49.7	46.4	28	93.6	87.3	88	137.5	128.2	48	181.4	169.1
9	6.6	6.1	69	50.5	47.1	29	94.3	88.0	89	138.2	128.9	49	182.1	169.8
10	7.3	6.8	70	51.2	47.7	30	95.1	88.7	90	139.0	129.6	50	182.8	170.5
11	8.0	7.5	71	51.9	48.4	131	95.8	89.3	191	139.7	130.3	251	183.6	171.2
12	8.8	8.2	72	52.7	49.1	32	96.5	90.0	92	140.4	130.9	52	184.3	171.9
13	9.5	8.9	73	53.4	49.8	33	97.3	90.7	93	141.2	131.6	53	185.0	172.5
14	10.2	9.5	74	54.1	50.5	34	98.0	91.4	94	141.9	132.3	54	185.8	173.2
15	11.0	10.2	75	54.9	51.1	35	98.7	92.1	95	142.6	133.0	55	186.5	173.9
16	11.7	10.9	76	55.6	51.8	36	99.5	92.8	96	143.3	133.7	56	187.2	174.6
17	12.4	11.6	77	56.3	52.5	37	100.2	93.4	97	144.1	134.4	57	188.0	175.3
18	13.2	12.3	78	57.0	53.2	38	100.9	94.1	98	144.8	135.0	58	188.7	176.0
19	13.9	13.0	79	57.8	53.9	39	101.7	94.8	99	145.5	135.7	59	189.4	176.6
20	14.6	13.6	80	58.5	54.6	40	102.4	95.5	200	146.3	136.4	60	190.2	177.3
21	15.4	14.3	81	59.2	55.2	141	103.1	96.2	201	147.0	137.1	261	190.9	178.0
22	16.1	15.0	82	60.0	55.9	42	103.9	96.8	02	147.7	137.8	62	191.6	178.7
23	16.8	15.7	83	60.7	56.6	43	104.6	97.5	03	148.5	138.4	63	192.3	179.4
24	17.6	16.4	84	61.4	57.3	44	105.3	98.2	04	149.2	139.1	64	193.1	180.0
25	18.3	17.0	85	62.2	58.0	45	106.0	98.9	05	149.9	139.8	65	193.8	180.7
26	19.0	17.7	86	62.9	58.7	46	106.8	99.6	06	150.7	140.5	66	194.5	181.4
27	19.7	18.4	87	63.6	59.3	47	107.5	100.3	07	151.4	141.2	67	195.3	182.1
28	20.5	19.1	88	64.4	60.0	48	108.2	100.9	08	152.1	141.9	68	196.0	182.8
29	21.2	19.8	89	65.1	60.7	49	109.0	101.6	09	152.9	142.5	69	196.7	183.5
30	21.9	20.5	90	65.8	61.4	50	109.7	102.3	10	153.6	143.2	70	197.5	184.1
31	22.7	21.1	91	66.6	62.1	151	110.4	103.0	211	154.3	143.9	271	198.2	184.8
32	23.4	21.8	92	67.3	62.7	52	111.2	103.7	12	155.0	144.6	72	198.9	185.5
33	24.1	22.5	93	68.0	63.4	53	111.9	104.3	13	155.8	145.3	73	199.7	186.2
34	24.9	23.2	94	68.7	64.1	54	112.6	105.0	14	156.5	145.9	74	200.4	186.9
35	25.6	23.9	95	69.5	64.8	55	113.4	105.7	15	157.2	146.6	75	201.1	187.5
36	26.3	24.6	96	70.2	65.5	56	114.1	106.4	16	158.0	147.3	76	201.9	188.2
37	27.1	25.2	97	70.9	66.2	57	114.8	107.1	17	158.7	148.0	77	202.6	188.9
38	27.8	25.9	98	71.7	66.8	58	115.6	107.8	18	159.4	148.7	78	203.3	189.6
39	28.5	26.6	99	72.4	67.5	59	116.3	108.4	19	160.2	149.4	79	204.0	190.3
40	29.3	27.3	100	73.1	68.2	60	117.0	109.1	20	160.9	150.0	80	204.8	191.0
41	30.0	28.0	101	73.9	68.9	161	117.7	109.8	221	161.6	150.7	281	205.5	191.6
42	30.7	28.6	02	74.6	69.6	62	118.5	110.5	22	162.4	151.4	82	206.2	192.3
43	31.4	29.3	03	75.3	70.2	63	119.2	111.2	23	163.1	152.1	83	207.0	193.0
44	32.2	30.0	04	76.1	70.9	64	119.9	111.8	24	163.8	152.8	84	207.7	193.7
45	32.9	30.7	05	76.8	71.6	65	120.7	112.5	25	164.6	153.4	85	208.4	194.4
46	33.6	31.4	06	77.5	72.3	66	121.4	113.2	26	165.3	154.1	86	209.2	195.1
47	34.4	32.1	07	78.3	73.0	67	122.1	113.9	27	166.0	154.8	87	209.9	195.7
48	35.1	32.7	08	79.0	73.7	68	122.9	114.6	28	166.7	155.5	88	210.6	196.4
49	35.8	33.4	09	79.7	74.3	69	123.6	115.3	29	167.5	156.2	89	211.4	197.1
50	36.6	34.1	10	80.4	75.0	70	124.3	115.9	30	168.2	156.9	90	212.1	197.8
51	37.3	34.8	111	81.2	75.7	171	125.1	116.6	231	168.9	157.5	291	212.8	198.5
52	38.0	35.5	12	81.9	76.4	72	125.8	117.3	32	169.7	158.2	92	213.6	199.1
53	38.8	36.1	13	82.6	77.1	73	126.5	118.0	33	170.4	158.9	93	214.3	199.8
54	39.5	36.8	14	83.4	77.7	74	127.3	118.7	34	171.1	159.6	94	215.0	200.5
55	40.2	37.5	15	84.1	78.4	75	128.0	119.3	35	171.9	160.3	95	215.7	201.2
56	41.0	38.2	16	84.8	79.1	76	128.7	120.0	36	172.6	161.0	96	216.5	201.9
57	41.7	38.9	17	85.6	79.8	77	129.4	120.7	37	173.3	161.6	97	217.2	202.6
58	42.4	39.6	18	86.3	80.5	78	130.2	121.4	38	174.1	162.3	98	217.9	203.2
59	43.1	40.2	19	87.0	81.2	79	130.9	122.1	39	174.8	163.0	99	218.7	203.9
60	43.9	40.9	20	87.8	81.8	80	131.6	122.8	40	175.5	163.7	300	219.4	204.6
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

47° (133°, 227°, 313°).

Difference of Latitude and Departure for 43° (137°, 223°, 317°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	220.1	205.3	361	264.0	246.2	421	307.9	287.1	481	351.8	328.1	541	395.7	369.0
02	220.9	206.0	62	264.8	246.9	22	308.6	287.8	82	352.5	328.7	42	396.4	369.7
03	221.6	206.7	63	265.5	247.6	23	309.4	288.5	83	353.2	329.4	43	397.1	370.3
04	222.3	207.3	64	266.2	248.3	24	310.1	289.2	84	354.0	330.1	44	397.9	371.0
05	223.1	208.0	65	267.0	248.9	25	310.8	289.9	85	354.7	330.8	45	398.6	371.7
06	223.8	208.7	66	267.7	249.6	26	311.6	290.5	86	355.4	331.4	46	399.3	372.4
07	224.5	209.4	67	268.4	250.3	27	312.3	291.2	87	356.2	332.1	47	400.1	373.1
08	225.3	210.1	68	269.1	251.0	28	313.0	291.9	88	356.9	332.8	48	400.8	373.7
09	226.0	210.7	69	269.9	251.7	29	313.8	292.6	89	357.7	333.5	49	401.5	374.4
10	226.7	211.4	70	270.6	252.3	30	314.5	293.3	90	358.4	334.2	50	402.2	375.1
311	227.5	212.1	371	271.3	253.0	431	315.2	293.9	491	359.1	334.9	551	403.0	375.8
12	228.2	212.8	72	272.1	253.7	32	316.0	294.6	92	359.8	335.5	52	403.7	376.5
13	228.9	213.5	73	272.8	254.4	33	316.7	295.3	93	360.6	336.2	53	404.4	377.1
14	229.7	214.2	74	273.5	255.1	34	317.4	296.0	94	361.3	336.9	54	405.2	377.8
15	230.4	214.8	75	274.3	255.8	35	318.1	296.7	95	362.0	337.6	55	405.9	378.5
16	231.1	215.5	76	275.0	256.4	36	318.9	297.4	96	362.8	338.3	56	406.6	379.2
17	231.8	216.2	77	275.7	257.1	37	319.6	298.0	97	363.5	338.9	57	407.4	379.9
18	232.6	216.9	78	276.5	257.8	38	320.3	298.7	98	364.2	339.6	58	408.1	380.6
19	233.3	217.6	79	277.2	258.5	39	321.1	299.4	99	364.9	340.3	59	408.8	381.2
20	234.0	218.2	80	277.9	259.2	40	321.8	300.1	500	365.7	341.0	60	409.6	381.9
321	234.8	218.9	381	278.7	259.8	441	322.5	300.8	501	366.4	341.7	561	410.3	382.6
22	235.5	219.6	82	279.4	260.5	42	323.3	301.4	02	367.1	342.4	62	411.0	383.3
23	236.2	220.3	83	280.1	261.2	43	324.0	302.1	03	367.8	343.0	63	411.8	384.0
24	237.0	221.0	84	280.8	261.9	44	324.7	302.8	04	368.6	343.7	64	412.5	384.6
25	237.7	221.7	85	281.6	262.6	45	325.5	303.5	05	369.3	344.4	65	413.2	385.3
26	238.4	222.3	86	282.3	263.3	46	326.2	304.2	06	370.0	345.1	66	414.0	386.0
27	239.2	223.0	87	283.0	263.9	47	326.9	304.9	07	370.8	345.8	67	414.7	386.7
28	239.9	223.7	88	283.7	264.6	48	327.7	305.5	08	371.5	346.5	68	415.4	387.4
29	240.6	224.4	89	284.5	265.3	49	328.4	306.2	09	372.3	347.1	69	416.2	388.1
30	241.4	225.1	90	285.2	266.0	50	329.1	306.9	10	373.0	347.8	70	416.9	388.7
331	242.1	225.7	391	286.0	266.7	451	329.9	307.6	511	373.8	348.5	571	417.6	389.4
32	242.8	226.4	92	286.7	267.3	52	330.6	308.3	12	374.5	349.2	72	418.3	390.1
33	243.5	227.1	93	287.4	268.0	53	331.3	309.0	13	375.2	349.9	73	419.1	390.8
34	244.3	227.8	94	288.2	268.7	54	332.1	309.6	14	376.0	350.5	74	419.8	391.5
35	245.0	228.5	95	288.9	269.4	55	332.8	310.3	15	376.6	351.2	75	420.5	392.2
36	245.7	229.2	96	289.6	270.1	56	333.5	311.0	16	377.4	351.9	76	421.3	392.8
37	246.5	229.8	97	290.4	270.8	57	334.3	311.7	17	378.2	352.6	77	422.0	393.5
38	247.2	230.5	98	291.1	271.4	58	335.0	312.4	18	378.9	353.3	78	422.7	394.2
39	247.9	231.2	99	291.8	272.1	59	335.7	313.0	19	379.6	354.0	79	423.5	394.9
40	248.7	231.9	400	292.6	272.8	60	336.5	313.7	20	380.3	354.6	80	424.2	395.6
341	249.4	232.6	401	293.3	273.5	461	337.2	314.4	521	381.1	355.3	581	424.9	396.2
42	250.1	233.2	02	294.0	274.2	62	337.9	315.1	22	381.8	356.0	82	425.7	396.9
43	250.9	233.9	03	294.7	274.9	63	338.7	315.8	23	382.6	356.7	83	426.4	397.6
44	251.6	234.6	04	295.5	275.5	64	339.4	316.5	24	383.3	357.4	84	427.1	398.3
45	252.3	235.3	05	296.2	276.2	65	340.1	317.1	25	384.0	358.1	85	427.9	399.0
46	253.1	236.0	06	296.9	276.9	66	340.8	317.8	26	384.7	358.7	86	428.6	399.6
47	253.8	236.7	07	297.7	277.6	67	341.6	318.5	27	385.5	359.4	87	429.3	400.3
48	254.5	237.3	08	298.4	278.3	68	342.3	319.2	28	386.2	360.1	88	430.1	401.0
49	255.3	238.0	09	299.1	278.9	69	343.0	319.9	29	386.9	360.8	89	430.8	401.7
50	256.0	238.7	10	299.9	279.6	70	343.7	320.5	30	387.6	361.5	90	431.5	402.4
351	256.7	239.4	411	300.6	280.3	471	344.5	321.2	531	388.4	362.1	591	432.3	403.1
52	257.4	240.1	12	301.3	281.0	72	345.2	321.9	32	389.1	362.8	92	433.0	403.7
53	258.2	240.8	13	302.1	281.7	73	345.9	322.6	33	389.9	363.5	93	433.7	404.4
54	258.9	241.4	14	302.8	282.4	74	346.7	323.3	34	390.6	364.2	94	434.5	405.1
55	259.6	242.1	15	303.5	283.0	75	347.4	324.0	35	391.3	364.9	95	435.2	405.8
56	260.4	242.8	16	304.3	283.7	76	348.1	324.6	36	392.0	365.5	96	435.9	406.5
57	261.1	243.5	17	305.0	284.4	77	348.9	325.3	37	392.8	366.2	97	436.7	407.2
58	261.8	244.2	18	305.7	285.1	78	349.6	326.0	38	393.5	366.9	98	437.4	407.8
59	262.6	244.8	19	306.4	285.8	79	350.3	326.7	39	394.2	367.6	99	438.1	408.5
60	263.3	245.5	20	307.2	286.4	80	351.1	327.4	40	394.9	368.3	600	438.8	409.2
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

47° (133°, 227°, 313°).

TABLE 2.

Difference of Latitude and Departure for 44° (136°, 224°, 316°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.7	0.7	61	43.9	42.4	121	87.0	84.1	181	130.2	125.7	241	173.4	167.4
2	1.4	1.4	62	44.6	43.1	22	87.8	84.7	82	130.9	126.4	42	174.1	168.1
3	2.2	2.1	63	45.3	43.8	23	88.5	85.4	83	131.6	127.1	43	174.8	168.8
4	2.9	2.8	64	46.0	44.5	24	89.2	86.1	84	132.4	127.8	44	175.5	169.5
5	3.6	3.5	65	46.8	45.2	25	89.9	86.8	85	133.1	128.5	45	176.2	170.2
6	4.3	4.2	66	47.5	45.8	26	90.6	87.5	86	133.8	129.2	46	177.0	170.9
7	5.0	4.9	67	48.2	46.5	27	91.4	88.2	87	134.5	129.9	47	177.7	171.6
8	5.8	5.6	68	48.9	47.2	28	92.1	88.9	88	135.2	130.6	48	178.4	172.3
9	6.5	6.3	69	49.6	47.9	29	92.8	89.6	89	136.0	131.3	49	179.1	173.0
10	7.2	6.9	70	50.4	48.6	30	93.5	90.3	90	136.7	132.0	50	179.8	173.7
11	7.9	7.6	71	51.1	49.3	131	94.2	91.0	191	137.4	132.7	251	180.6	174.4
12	8.6	8.3	72	51.8	50.0	32	95.0	91.7	92	138.1	133.4	52	181.3	175.1
13	9.4	9.0	73	52.5	50.7	33	95.7	92.4	93	138.8	134.1	53	182.0	175.7
14	10.1	9.7	74	53.2	51.4	34	96.4	93.1	94	139.6	134.8	54	182.7	176.4
15	10.8	10.4	75	54.0	52.1	35	97.1	93.8	95	140.3	135.5	55	183.4	177.1
16	11.5	11.1	76	54.7	52.8	36	97.8	94.5	96	141.0	136.2	56	184.2	177.8
17	12.2	11.8	77	55.4	53.5	37	98.5	95.2	97	141.7	136.8	57	184.9	178.5
18	12.9	12.5	78	56.1	54.2	38	99.3	95.9	98	142.4	137.5	58	185.6	179.2
19	13.7	13.2	79	56.8	54.9	39	100.0	96.6	99	143.1	138.2	59	186.3	179.9
20	14.4	13.9	80	57.5	55.6	40	100.7	97.3	200	143.9	138.9	60	187.0	180.6
21	15.1	14.6	81	58.3	56.3	141	101.4	97.9	201	144.6	139.6	261	187.7	181.3
22	15.8	15.3	82	59.0	57.0	42	102.1	98.6	02	145.3	140.3	62	188.5	182.0
23	16.5	16.0	83	59.7	57.7	43	102.9	99.3	03	146.0	141.0	63	189.2	182.7
24	17.3	16.7	84	60.4	58.4	44	103.6	100.0	04	146.7	141.7	64	189.9	183.4
25	18.0	17.4	85	61.1	59.0	45	104.3	100.7	05	147.5	142.4	65	190.6	184.1
26	18.7	18.1	86	61.9	59.7	46	105.0	101.4	06	148.2	143.1	66	191.3	184.8
27	19.4	18.8	87	62.6	60.4	47	105.7	102.1	07	148.9	143.8	67	192.1	185.5
28	20.1	19.5	88	63.3	61.1	48	106.5	102.8	08	149.6	144.5	68	192.8	186.2
29	20.9	20.1	89	64.0	61.8	49	107.2	103.5	09	150.3	145.2	69	193.5	186.9
30	21.6	20.8	90	64.7	62.5	50	107.9	104.2	10	151.1	145.9	70	194.2	187.6
31	22.3	21.5	91	65.5	63.2	151	108.6	104.9	211	151.8	146.6	271	194.9	188.3
32	23.0	22.2	92	66.2	63.9	52	109.3	105.6	12	152.5	147.3	72	195.7	188.9
33	23.7	22.9	93	66.9	64.6	53	110.1	106.3	13	153.2	148.0	73	196.4	189.6
34	24.5	23.6	94	67.6	65.3	54	110.8	107.0	14	153.9	148.7	74	197.1	190.3
35	25.2	24.3	95	68.3	66.0	55	111.5	107.7	15	154.7	149.4	75	197.8	191.0
36	25.9	25.0	96	69.1	66.7	56	112.2	108.4	16	155.4	150.0	76	198.5	191.7
37	26.6	25.7	97	69.8	67.4	57	112.9	109.1	17	156.1	150.7	77	199.3	192.4
38	27.3	26.4	98	70.5	68.1	58	113.7	109.8	18	156.8	151.4	78	200.0	193.1
39	28.1	27.1	99	71.2	68.8	59	114.4	110.5	19	157.5	152.1	79	200.7	193.8
40	28.8	27.8	100	71.9	69.5	60	115.1	111.1	20	158.3	152.8	80	201.4	194.5
41	29.5	28.5	101	72.7	70.2	161	115.8	111.8	221	159.0	153.5	281	202.1	195.2
42	30.2	29.2	02	73.4	70.9	62	116.5	112.5	22	159.7	154.2	82	202.9	195.9
43	30.9	29.9	03	74.1	71.5	63	117.3	113.2	23	160.4	154.9	83	203.6	196.6
44	31.7	30.6	04	74.8	72.2	64	118.0	113.9	24	161.1	155.6	84	204.3	197.3
45	32.4	31.3	05	75.5	72.9	65	118.7	114.6	25	161.9	156.3	85	205.0	198.0
46	33.1	32.0	06	76.3	73.6	66	119.4	115.3	26	162.6	157.0	86	205.7	198.7
47	33.8	32.6	07	77.0	74.3	67	120.1	116.0	27	163.3	157.7	87	206.5	199.4
48	34.5	33.3	08	77.7	75.0	68	120.8	116.7	28	164.0	158.4	88	207.2	200.1
49	35.2	34.0	09	78.4	75.7	69	121.6	117.4	29	164.7	159.1	89	207.9	200.8
50	36.0	34.7	10	79.1	76.4	70	122.3	118.1	30	165.4	159.8	90	208.6	201.5
51	36.7	35.4	111	79.8	77.1	171	123.0	118.8	231	166.2	160.5	291	209.3	202.1
52	37.4	36.1	12	80.6	77.8	72	123.7	119.5	32	166.9	161.2	92	210.0	202.8
53	38.1	36.8	13	81.3	78.5	73	124.4	120.2	33	167.6	161.9	93	210.8	203.5
54	38.8	37.5	14	82.0	79.2	74	125.2	120.9	34	168.3	162.6	94	211.5	204.2
55	39.6	38.2	15	82.7	79.9	75	125.9	121.6	35	169.0	163.2	95	212.2	204.9
56	40.3	38.9	16	83.4	80.6	76	126.6	122.3	36	169.8	163.9	96	212.9	205.6
57	41.0	39.6	17	84.2	81.3	77	127.3	123.0	37	170.5	164.6	97	213.6	206.3
58	41.7	40.3	18	84.9	82.0	78	128.0	123.6	38	171.2	165.3	98	214.4	207.0
59	42.4	41.0	19	85.6	82.7	79	128.8	124.3	39	171.9	166.0	99	215.1	207.7
60	43.2	41.7	20	86.3	83.4	80	129.5	125.0	40	172.6	166.7	300	215.8	208.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

46° (134°, 226°, 314°).

TABLE 2.

Difference of Latitude and Departure for 44° (136°, 224°, 316°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	216.5	209.1	361	259.7	250.8	421	302.8	292.5	481	346.0	334.1	541	389.2	375.8
02	217.2	209.8	62	260.4	251.5	22	303.6	293.2	82	346.7	334.8	42	389.9	376.5
03	218.0	210.5	63	261.1	252.2	23	304.3	293.8	83	347.4	335.5	43	390.6	377.2
04	218.7	211.2	64	261.8	252.9	24	305.0	294.5	84	348.2	336.2	44	391.3	377.9
05	219.4	211.9	65	262.6	253.6	25	305.7	295.2	85	348.9	336.9	45	392.0	378.6
06	220.1	212.6	66	263.3	254.3	26	306.4	295.9	86	349.6	337.6	46	392.8	379.3
07	220.8	213.3	67	264.0	254.9	27	307.2	296.6	87	350.3	338.3	47	393.5	380.0
08	221.6	214.0	68	264.7	255.6	28	307.9	297.3	88	351.0	339.0	48	394.2	380.7
09	222.3	214.7	69	265.4	256.3	29	308.6	298.0	89	351.7	339.7	49	394.9	381.4
10	223.0	215.4	70	266.2	257.0	30	309.3	298.7	90	352.5	340.4	50	395.6	382.1
311	223.7	216.0	371	266.9	257.7	431	310.0	299.4	491	353.2	341.1	551	396.4	382.7
12	224.4	216.7	72	267.6	258.4	32	310.8	300.1	92	353.9	341.8	52	397.1	383.4
13	225.2	217.4	73	268.3	259.1	33	311.5	300.8	93	354.6	342.5	53	397.8	384.1
14	225.9	218.1	74	269.0	259.8	34	312.2	301.5	94	355.3	343.2	54	398.5	384.8
15	226.6	218.8	75	269.8	260.5	35	312.9	302.2	95	356.1	343.9	55	399.2	385.5
16	227.3	219.5	76	270.5	261.2	36	313.6	302.9	96	356.8	344.6	56	400.0	386.2
17	228.0	220.2	77	271.2	261.9	37	314.4	303.6	97	357.5	345.2	57	400.7	386.9
18	228.8	220.9	78	271.9	262.6	38	315.1	304.3	98	358.2	345.9	58	401.4	387.6
19	229.5	221.6	79	272.6	263.3	39	315.8	305.0	99	358.9	346.6	59	402.1	388.3
20	230.2	222.3	80	273.4	264.0	40	316.5	305.7	500	359.7	347.3	60	402.8	389.0
321	230.9	223.0	381	274.1	264.7	441	317.2	306.4	501	360.4	348.0	561	403.6	389.7
22	231.6	223.7	82	274.8	265.4	42	318.0	307.0	02	361.1	348.7	62	404.3	390.4
23	232.3	224.4	83	275.5	266.1	43	318.7	307.7	03	361.8	349.4	63	405.0	391.1
24	233.1	225.1	84	276.2	266.8	44	319.4	308.4	04	362.5	350.1	64	405.7	391.8
25	233.8	225.8	85	276.9	267.5	45	320.1	309.1	05	363.3	350.8	65	406.4	392.5
26	234.5	226.5	86	277.7	268.1	46	320.8	309.8	06	364.0	351.5	66	407.2	393.2
27	235.2	227.2	87	278.4	268.8	47	321.5	310.5	07	364.7	352.2	67	407.9	393.9
28	235.9	227.9	88	279.1	269.5	48	322.3	311.2	08	365.4	352.9	68	408.6	394.6
29	236.7	228.6	89	279.8	270.2	49	323.0	311.9	09	366.1	353.6	69	409.3	395.3
30	237.4	229.2	90	280.5	270.9	50	323.7	312.6	10	366.9	354.3	70	410.0	396.0
331	238.1	229.9	391	281.3	271.6	451	324.4	313.3	511	367.6	355.0	571	410.7	396.7
32	238.8	230.6	92	282.0	272.3	52	325.2	314.0	12	368.3	355.7	72	411.5	397.3
33	239.5	231.3	93	282.7	273.0	53	325.9	314.7	13	369.0	356.4	73	412.2	398.0
34	240.3	232.0	94	283.4	273.7	54	326.6	315.4	14	369.7	357.1	74	412.9	398.7
35	241.0	232.7	95	284.1	274.4	55	327.3	316.1	15	370.5	357.8	75	413.6	399.4
36	241.7	233.4	96	284.9	275.1	56	328.0	316.8	16	371.2	358.4	76	414.3	400.1
37	242.4	234.1	97	285.6	275.8	57	328.7	317.5	17	371.9	359.1	77	415.1	400.8
38	243.1	234.8	98	286.3	276.5	58	329.5	318.2	18	372.6	359.8	78	415.8	401.5
39	243.9	235.5	99	287.0	277.2	59	330.2	318.9	19	373.3	360.5	79	416.5	402.2
40	244.6	236.2	400	287.7	277.9	60	330.9	319.6	20	374.1	361.2	80	417.2	402.9
341	245.3	236.9	401	288.5	278.6	461	331.6	320.2	521	374.8	361.9	581	417.9	403.6
42	246.0	237.6	02	289.2	279.3	62	332.3	320.9	22	375.5	362.6	82	418.7	404.3
43	246.7	238.3	03	289.9	280.0	63	333.1	321.6	23	376.2	363.3	83	419.4	405.0
44	247.5	239.0	04	290.6	280.7	64	333.8	322.3	24	376.9	364.0	84	420.1	405.7
45	248.2	239.7	05	291.3	281.3	65	334.5	323.0	25	377.7	364.7	85	420.8	406.4
46	248.9	240.4	06	292.1	282.0	66	335.2	323.7	26	378.4	365.4	86	421.5	407.1
47	249.6	241.1	07	292.8	282.7	67	335.9	324.4	27	379.1	366.1	87	422.3	407.8
48	250.3	241.7	08	293.5	283.4	68	336.7	325.1	28	379.8	366.8	88	423.0	408.5
49	251.1	242.4	09	294.2	284.1	69	337.4	325.8	29	380.5	367.5	89	423.7	409.1
50	251.8	243.1	10	294.9	284.8	70	338.1	326.5	30	381.2	368.2	90	424.4	409.9
351	252.5	243.8	411	295.7	285.5	471	338.8	327.2	531	382.0	368.9	591	425.1	410.5
52	253.2	244.5	12	296.4	286.2	72	339.5	327.9	32	382.7	369.6	92	425.9	411.2
53	253.9	245.2	13	297.1	286.9	73	340.3	328.6	33	383.4	370.3	93	426.6	411.9
54	254.6	245.9	14	297.8	287.6	74	341.0	329.3	34	384.1	371.0	94	427.3	412.6
55	255.4	246.6	15	298.5	288.3	75	341.7	330.0	35	384.8	371.7	95	428.0	413.3
56	256.1	247.3	16	299.2	289.0	76	342.4	330.7	36	385.6	372.4	96	428.7	414.0
57	256.8	248.0	17	300.0	289.7	77	343.1	331.4	37	386.3	373.1	97	429.5	414.7
58	257.5	248.7	18	300.7	290.4	78	343.8	332.1	38	387.0	373.7	98	430.2	415.4
59	258.2	249.4	19	301.4	291.1	79	344.6	332.7	39	387.7	374.4	99	430.9	416.1
60	259.0	250.1	20	302.1	291.8	80	345.3	333.4	40	388.4	375.1	600	431.6	416.8
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

46° (134°, 226°, 314°).

TABLE 2.

Difference of Latitude and Departure for 45° (135°, 225°, 315°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.7	0.7	61	43.1	43.1	121	85.6	85.6	181	128.0	128.0	241	170.4	170.4
2	1.4	1.4	62	43.8	43.8	22	86.3	86.3	82	128.7	128.7	42	171.1	171.1
3	2.1	2.1	63	44.5	44.5	23	87.0	87.0	83	129.4	129.4	43	171.8	171.8
4	2.8	2.8	64	45.3	45.3	24	87.7	87.7	84	130.1	130.1	44	172.5	172.5
5	3.5	3.5	65	46.0	46.0	25	88.4	88.4	85	130.8	130.8	45	173.2	173.2
6	4.2	4.2	66	46.7	46.7	26	89.1	89.1	86	131.5	131.5	46	173.9	173.9
7	4.9	4.9	67	47.4	47.4	27	89.8	89.8	87	132.2	132.2	47	174.7	174.7
8	5.7	5.7	68	48.1	48.1	28	90.5	90.5	88	132.9	132.9	48	175.4	175.4
9	6.4	6.4	69	48.8	48.8	29	91.2	91.2	89	133.6	133.6	49	176.1	176.1
10	7.1	7.1	70	49.5	49.5	30	91.9	91.9	90	134.4	134.4	50	176.8	176.8
11	7.8	7.8	71	50.2	50.2	131	92.6	92.6	191	135.1	135.1	251	177.5	177.5
12	8.5	8.5	72	50.9	50.9	32	93.3	93.3	92	135.8	135.8	52	178.2	178.2
13	9.2	9.2	73	51.6	51.6	33	94.0	94.0	93	136.5	136.5	53	178.9	178.9
14	9.9	9.9	74	52.3	52.3	34	94.8	94.8	94	137.2	137.2	54	179.6	179.6
15	10.6	10.6	75	53.0	53.0	35	95.5	95.5	95	137.9	137.9	55	180.3	180.3
16	11.3	11.3	76	53.7	53.7	36	96.2	96.2	96	138.6	138.6	56	181.0	181.0
17	12.0	12.0	77	54.4	54.4	37	96.9	96.9	97	139.3	139.3	57	181.7	181.7
18	12.7	12.7	78	55.2	55.2	38	97.6	97.6	98	140.0	140.0	58	182.4	182.4
19	13.4	13.4	79	55.9	55.9	39	98.3	98.3	99	140.7	140.7	59	183.1	183.1
20	14.1	14.1	80	56.6	56.6	40	99.0	99.0	200	141.4	141.4	60	183.8	183.8
21	14.8	14.8	81	57.3	57.3	141	99.7	99.7	201	142.1	142.1	261	184.6	184.6
22	15.6	15.6	82	58.0	58.0	42	100.4	100.4	02	142.8	142.8	62	185.3	185.3
23	16.3	16.3	83	58.7	58.7	43	101.1	101.1	03	143.5	143.5	63	186.0	186.0
24	17.0	17.0	84	59.4	59.4	44	101.8	101.8	04	144.2	144.2	64	186.7	186.7
25	17.7	17.7	85	60.1	60.1	45	102.5	102.5	05	145.0	145.0	65	187.4	187.4
26	18.4	18.4	86	60.8	60.8	46	103.2	103.2	06	145.7	145.7	66	188.1	188.1
27	19.1	19.1	87	61.5	61.5	47	103.9	103.9	07	146.4	146.4	67	188.8	188.8
28	19.8	19.8	88	62.2	62.2	48	104.7	104.7	08	147.1	147.1	68	189.5	189.5
29	20.5	20.5	89	62.9	62.9	49	105.4	105.4	09	147.8	147.8	69	190.2	190.2
30	21.2	21.2	90	63.6	63.6	50	106.1	106.1	10	148.5	148.5	70	190.9	190.9
31	21.9	21.9	91	64.3	64.3	151	106.8	106.8	211	149.2	149.2	271	191.6	191.6
32	22.6	22.6	92	65.1	65.1	52	107.5	107.5	12	149.9	149.9	72	192.3	192.3
33	23.3	23.3	93	65.8	65.8	53	108.2	108.2	13	150.6	150.6	73	193.0	193.0
34	24.0	24.0	94	66.5	66.5	54	108.9	108.9	14	151.3	151.3	74	193.7	193.7
35	24.7	24.7	95	67.2	67.2	55	109.6	109.6	15	152.0	152.0	75	194.5	194.5
36	25.5	25.5	96	67.9	67.9	56	110.3	110.3	16	152.7	152.7	76	195.2	195.2
37	26.2	26.2	97	68.6	68.6	57	111.0	111.0	17	153.4	153.4	77	195.9	195.9
38	26.9	26.9	98	69.3	69.3	58	111.7	111.7	18	154.1	154.1	78	196.6	196.6
39	27.6	27.6	99	70.0	70.0	59	112.4	112.4	19	154.9	154.9	79	197.3	197.3
40	28.3	28.3	100	70.7	70.7	60	113.1	113.1	20	155.6	155.6	80	198.0	198.0
41	29.0	29.0	101	71.4	71.4	161	113.8	113.8	221	156.3	156.3	281	198.7	198.7
42	29.7	29.7	02	72.1	72.1	62	114.6	114.6	22	157.0	157.0	82	199.4	199.4
43	30.4	30.4	03	72.8	72.8	63	115.3	115.3	23	157.7	157.7	83	200.1	200.1
44	31.1	31.1	04	73.5	73.5	64	116.0	116.0	24	158.4	158.4	84	200.8	200.8
45	31.8	31.8	05	74.2	74.2	65	116.7	116.7	25	159.1	159.1	85	201.5	201.5
46	32.5	32.5	06	75.0	75.0	66	117.4	117.4	26	159.8	159.8	86	202.2	202.2
47	33.2	33.2	07	75.7	75.7	67	118.1	118.1	27	160.5	160.5	87	202.9	202.9
48	33.9	33.9	08	76.4	76.4	68	118.8	118.8	28	161.2	161.2	88	203.6	203.6
49	34.6	34.6	09	77.1	77.1	69	119.5	119.5	29	161.9	161.9	89	204.4	204.4
50	35.4	35.4	10	77.8	77.8	70	120.2	120.2	30	162.6	162.6	90	205.1	205.1
51	36.1	36.1	111	78.5	78.5	171	120.9	120.9	231	163.3	163.3	291	205.8	205.8
52	36.8	36.8	12	79.2	79.2	72	121.6	121.6	32	164.0	164.0	92	206.5	206.5
53	37.5	37.5	13	79.9	79.9	73	122.3	122.3	33	164.8	164.8	93	207.2	207.2
54	38.2	38.2	14	80.6	80.6	74	123.0	123.0	34	165.5	165.5	94	207.9	207.9
55	38.9	38.9	15	81.3	81.3	75	123.7	123.7	35	166.2	166.2	95	208.6	208.6
56	39.6	39.6	16	82.0	82.0	76	124.5	124.5	36	166.9	166.9	96	209.3	209.3
57	40.3	40.3	17	82.7	82.7	77	125.2	125.2	37	167.6	167.6	97	210.0	210.0
58	41.0	41.0	18	83.4	83.4	78	125.9	125.9	38	168.3	168.3	98	210.7	210.7
59	41.7	41.7	19	84.1	84.1	79	126.6	126.6	39	169.0	169.0	99	211.4	211.4
60	42.4	42.4	20	84.9	84.9	80	127.3	127.3	40	169.7	169.7	300	212.1	212.1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

45° (135°, 225°, 315°).

Difference of Latitude and Departure for 45° (135°, 225°, 315°).

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
301	212.8	212.8	361	255.3	255.3	421	297.7	297.7	481	340.1	340.1	541	382.5	382.5
02	213.5	213.5	62	256.0	256.0	22	298.4	298.4	82	340.8	340.8	42	383.2	383.2
03	214.3	214.3	63	256.7	256.7	23	299.1	299.1	83	341.5	341.5	43	383.9	383.9
04	215.0	215.0	64	257.4	257.4	24	299.8	299.8	84	342.2	342.2	44	384.7	384.7
05	215.7	215.7	65	258.1	258.1	25	300.5	300.5	85	342.9	342.9	45	385.4	385.4
06	216.4	216.4	66	258.8	258.8	26	301.2	301.2	86	343.6	343.6	46	386.1	386.1
07	217.1	217.1	67	259.5	259.5	27	301.9	301.9	87	344.3	344.3	47	386.8	386.8
08	217.8	217.8	68	260.2	260.2	28	302.6	302.6	88	345.1	345.1	48	387.5	387.5
09	218.5	218.5	69	260.9	260.9	29	303.4	303.4	89	345.8	345.8	49	388.2	388.2
10	219.2	219.2	70	261.6	261.6	30	304.1	304.1	90	346.5	346.5	50	388.9	388.9
311	219.9	219.9	371	262.3	262.3	431	304.8	304.8	491	347.2	347.2	551	389.6	389.6
12	220.6	220.6	72	263.0	263.0	32	305.5	305.5	92	347.9	347.9	52	390.3	390.3
13	221.3	221.3	73	263.8	263.8	33	306.2	306.2	93	348.6	348.6	53	391.0	391.0
14	222.0	222.0	74	264.5	264.5	34	306.9	306.9	94	349.3	349.3	54	391.7	391.7
15	222.7	222.7	75	265.2	265.2	35	307.6	307.6	95	350.0	350.0	55	392.4	392.4
16	223.4	223.4	76	265.9	265.9	36	308.3	308.3	96	350.7	350.7	56	393.1	393.1
17	224.2	224.2	77	266.6	266.6	37	309.0	309.0	97	351.4	351.4	57	393.9	393.9
18	224.9	224.9	78	267.3	267.3	38	309.7	309.7	98	352.1	352.1	58	394.6	394.6
19	225.6	225.6	79	268.0	268.0	39	310.4	310.4	99	352.8	352.8	59	395.3	395.3
20	226.3	226.3	80	268.7	268.7	40	311.1	311.1	500	353.5	353.5	60	396.0	396.0
321	227.0	227.0	381	269.4	269.4	441	311.8	311.8	501	354.3	354.3	561	396.7	396.7
22	227.7	227.7	82	270.1	270.1	42	312.5	312.5	02	355.0	355.0	62	397.4	397.4
23	228.4	228.4	83	270.8	270.8	43	313.3	313.3	03	355.7	355.7	63	398.1	398.1
24	229.1	229.1	84	271.5	271.5	44	314.0	314.0	04	356.4	356.4	64	398.8	398.8
25	229.8	229.8	85	272.2	272.2	45	314.7	314.7	05	357.1	357.1	65	399.5	399.5
26	230.5	230.5	86	272.9	272.9	46	315.4	315.4	06	357.8	357.8	66	400.2	400.2
27	231.2	231.2	87	273.7	273.7	47	316.1	316.1	07	358.5	358.5	67	400.9	400.9
28	231.9	231.9	88	274.4	274.4	48	316.8	316.8	08	359.2	359.2	68	401.6	401.6
29	232.6	232.6	89	275.1	275.1	49	317.5	317.5	09	359.9	359.9	69	402.3	402.3
30	233.3	233.3	90	275.8	275.8	50	318.2	318.2	10	360.6	360.6	70	403.0	403.0
331	234.1	234.1	391	276.5	276.5	451	318.9	318.9	511	361.3	361.3	571	403.8	403.8
32	234.8	234.8	92	277.2	277.2	52	319.6	319.6	12	362.0	362.0	72	404.5	404.5
33	235.5	235.5	93	277.9	277.9	53	320.3	320.3	13	362.7	362.7	73	405.2	405.2
34	236.2	236.2	94	278.6	278.6	54	321.0	321.0	14	363.5	363.5	74	405.9	405.9
35	236.9	236.9	95	279.3	279.3	55	321.7	321.7	15	364.2	364.2	75	406.6	406.6
36	237.6	237.6	96	280.0	280.0	56	322.4	322.4	16	364.9	364.9	76	407.3	407.3
37	238.3	238.3	97	280.7	280.7	57	323.2	323.2	17	365.6	365.6	77	408.0	408.0
38	239.0	239.0	98	281.4	281.4	58	323.9	323.9	18	366.3	366.3	78	408.7	408.7
39	239.7	239.7	99	282.1	282.1	59	324.6	324.6	19	367.0	367.0	79	409.4	409.4
40	240.4	240.4	400	282.8	282.8	60	325.3	325.3	20	367.7	367.7	80	410.1	410.1
341	241.1	241.1	401	283.6	283.6	461	326.0	326.0	521	368.4	368.4	581	410.8	410.8
42	241.8	241.8	02	284.3	284.3	62	326.7	326.7	22	369.1	369.1	82	411.5	411.5
43	242.5	242.5	03	285.0	285.0	63	327.4	327.4	23	369.8	369.8	83	412.2	412.2
44	243.2	243.2	04	285.7	285.7	64	328.1	328.1	24	370.5	370.5	84	412.9	412.9
45	244.0	244.0	05	286.4	286.4	65	328.8	328.8	25	371.2	371.2	85	413.7	413.7
46	244.7	244.7	06	287.1	287.1	66	329.5	329.5	26	371.9	371.9	86	414.4	414.4
47	245.4	245.4	07	287.8	287.8	67	330.2	330.2	27	372.6	372.6	87	415.1	415.1
48	246.1	246.1	08	288.5	288.5	68	330.9	330.9	28	373.4	373.4	88	415.8	415.8
49	246.8	246.8	09	289.2	289.2	69	331.6	331.6	29	374.1	374.1	89	416.5	416.5
50	247.5	247.5	10	289.9	289.9	70	332.3	332.3	30	374.8	374.8	90	417.2	417.2
351	248.2	248.2	411	290.6	290.6	471	333.1	333.1	531	375.5	375.5	591	417.9	417.9
52	248.9	248.9	12	291.3	291.3	72	333.8	333.8	32	376.2	376.2	92	418.6	418.6
53	249.6	249.6	13	292.0	292.0	73	334.5	334.5	33	376.9	376.9	93	419.3	419.3
54	250.3	250.3	14	292.7	292.7	74	335.2	335.2	34	377.6	377.6	94	420.0	420.0
55	251.0	251.0	15	293.5	293.5	75	335.9	335.9	35	378.3	378.3	95	420.7	420.7
56	251.7	251.7	16	294.2	294.2	76	336.6	336.6	36	379.0	379.0	96	421.4	421.4
57	252.4	252.4	17	294.9	294.9	77	337.3	337.3	37	379.7	379.7	97	422.1	422.1
58	253.1	253.1	18	295.6	295.6	78	338.0	338.0	38	380.4	380.4	98	422.8	422.8
59	253.9	253.9	19	296.3	296.3	79	338.7	338.7	39	381.1	381.1	99	423.6	423.6
60	254.6	254.6	20	297.0	297.0	80	339.4	339.4	40	381.8	381.8	600	424.3	424.3
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.

45° (135°, 225°, 315°).

TABLE 3.

Meridional Parts, or Increased Latitudes.

Comp. $\frac{1}{293.465}$

M.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	M.
0	0.0	59.6	119.2	178.9	238.6	298.3	358.2	418.2	478.3	538.6	0
1	1.0	60.6	20.2	79.9	39.6	99.3	59.2	19.2	79.3	39.6	1
2	2.0	61.6	21.2	80.8	40.6	300.3	60.2	20.2	80.3	40.6	2
3	3.0	62.6	22.2	81.8	41.6	01.3	61.2	21.2	81.3	41.6	3
4	4.0	63.6	23.2	82.8	42.5	02.3	62.2	22.2	82.3	42.6	4
5	5.0	64.6	124.2	183.8	243.5	303.3	363.2	423.2	483.3	543.6	5
6	6.0	65.6	25.2	84.8	44.5	04.3	64.2	24.2	84.3	44.6	6
7	7.0	66.5	26.2	85.8	45.5	05.3	65.2	25.2	85.3	45.6	7
8	7.9	67.5	27.2	86.8	46.5	06.3	66.2	26.2	86.3	46.6	8
9	8.9	68.5	28.2	87.8	47.5	07.3	67.2	27.2	87.3	47.6	9
10	9.9	69.5	129.1	188.8	248.5	308.3	368.2	428.2	488.3	548.6	10
11	10.9	70.5	30.1	89.8	49.5	09.3	69.2	29.2	89.3	49.6	11
12	11.9	71.5	31.1	90.8	50.5	10.3	70.2	30.2	90.4	50.6	12
13	12.9	72.5	32.1	91.8	51.5	11.3	71.2	31.2	91.4	51.7	13
14	13.9	73.5	33.1	92.8	52.5	12.3	72.2	32.2	92.4	52.7	14
15	14.9	74.5	134.1	193.8	253.5	313.3	373.2	433.2	493.4	553.7	15
16	15.9	75.5	35.1	94.8	54.5	14.3	74.2	34.2	94.4	54.7	16
17	16.9	76.5	36.1	95.8	55.5	15.3	75.2	35.2	95.4	55.7	17
18	17.9	77.5	37.1	96.8	56.5	16.3	76.2	36.2	96.4	56.7	18
19	18.9	78.5	38.1	97.8	57.5	17.3	77.2	37.2	97.4	57.7	19
20	19.9	79.5	139.1	198.8	258.5	318.3	378.2	438.2	498.4	558.7	20
21	20.9	80.5	40.1	99.7	59.5	19.3	79.2	39.2	99.4	59.7	21
22	21.9	81.5	41.1	200.7	60.5	20.3	80.2	40.2	500.4	60.7	22
23	22.8	82.4	42.1	01.7	61.5	21.3	81.2	41.2	01.4	61.7	23
24	23.8	83.4	43.1	02.7	62.5	22.3	82.2	42.2	02.4	62.7	24
25	24.8	84.4	144.1	203.7	263.5	323.3	383.2	443.2	503.4	563.7	25
26	25.8	85.4	45.1	04.7	64.5	24.3	84.2	44.2	04.4	64.7	26
27	26.8	86.4	46.0	05.7	65.5	25.3	85.2	45.2	05.4	65.7	27
28	27.8	87.4	47.0	06.7	66.5	26.3	86.2	46.2	06.4	66.8	28
29	28.8	88.4	48.0	07.7	67.4	27.3	87.2	47.2	07.4	67.8	29
30	29.8	89.4	149.0	208.7	268.4	328.3	388.2	448.2	508.4	568.8	30
31	30.8	90.4	50.0	09.7	69.4	29.3	89.2	49.2	09.4	69.8	31
32	31.8	91.4	51.0	10.7	70.4	30.3	90.2	50.2	10.4	70.8	32
33	32.8	92.4	52.0	11.7	71.4	31.3	91.2	51.2	11.4	71.8	33
34	33.8	93.4	53.0	12.7	72.4	32.3	92.2	52.2	12.4	72.8	34
35	34.8	94.4	154.0	213.7	273.4	333.3	393.2	453.2	513.4	573.8	35
36	35.8	95.4	55.0	14.7	74.4	34.3	94.2	54.3	14.5	74.8	36
37	36.7	96.4	56.0	15.7	75.4	35.3	95.2	55.3	15.5	75.8	37
38	37.7	97.3	57.0	16.7	76.4	36.2	96.2	56.3	16.5	76.8	38
39	38.7	98.3	58.0	17.7	77.4	37.2	97.2	57.3	17.5	77.8	39
40	39.7	99.3	159.0	218.7	278.4	338.2	398.2	458.3	518.5	578.8	40
41	40.7	100.3	60.0	19.7	79.4	39.2	99.2	59.3	19.5	79.9	41
42	41.7	01.3	61.0	20.6	80.4	40.2	400.2	60.3	20.5	80.9	42
43	42.7	02.3	62.0	21.6	81.4	41.2	01.2	61.3	21.5	81.9	43
44	43.7	03.3	63.0	22.6	82.4	42.2	02.2	62.3	22.5	82.9	44
45	44.7	104.3	164.0	223.6	283.4	343.2	403.2	463.3	523.5	583.9	45
46	45.7	05.3	65.0	24.6	84.4	44.2	04.2	64.3	24.5	84.9	46
47	46.7	06.3	66.0	25.6	85.4	45.2	05.2	65.3	25.5	85.9	47
48	47.7	07.3	67.0	26.6	86.4	46.2	06.2	66.3	26.5	86.9	48
49	48.7	08.3	68.0	27.6	87.4	47.2	07.2	67.3	27.5	87.9	49
50	49.7	109.3	168.9	228.6	288.4	348.2	408.2	468.3	528.5	588.9	50
51	50.7	10.3	69.9	29.6	89.4	49.2	09.2	69.3	29.5	89.9	51
52	51.6	11.3	70.9	30.6	90.4	50.2	10.2	70.3	30.5	90.9	52
53	52.6	12.3	71.9	31.6	91.4	51.2	11.2	71.3	31.5	91.9	53
54	53.6	13.2	72.9	32.6	92.4	52.2	12.2	72.3	32.5	93.0	54
55	54.6	114.2	173.9	233.6	293.4	353.2	413.2	473.3	533.5	594.0	55
56	55.6	15.2	74.9	34.6	94.4	54.2	14.2	74.3	34.6	95.0	56
57	56.6	16.2	75.9	35.6	95.4	55.2	15.2	75.3	35.6	96.0	57
58	57.6	17.2	76.9	36.6	96.3	56.2	16.2	76.3	36.6	97.0	58
59	58.6	18.2	77.9	37.6	97.3	57.2	17.2	77.3	37.6	98.0	59
M.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	M.

TABLE 3.

Meridional Parts, or Increased Latitudes.

Comp. $\frac{1}{293.465}$

M.	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	M.
0	599.0	659.6	720.5	781.5	842.8	904.4	966.3	1028.5	1091.0	1153.9	0
1	600.0	60.6	21.5	82.5	43.9	05.4	67.3	29.5	92.0	54.9	1
2	01.0	61.7	22.5	83.6	44.9	06.5	68.3	30.5	93.1	56.0	2
3	02.0	62.7	23.5	84.6	45.9	07.5	69.4	31.6	94.1	57.0	3
4	03.0	63.7	24.5	85.6	46.9	08.5	70.4	32.6	95.2	58.1	4
5	604.1	664.7	725.5	786.6	847.9	909.6	971.4	1033.7	1096.2	1159.1	5
6	05.1	65.7	26.6	87.6	49.0	10.6	72.5	34.7	97.3	60.2	6
7	06.1	66.7	27.6	88.7	50.0	11.6	73.5	35.7	98.3	61.2	7
8	07.1	67.7	28.6	89.7	51.0	12.6	74.6	36.8	99.4	62.3	8
9	08.1	68.7	29.6	90.7	52.0	13.7	75.6	37.8	1100.4	63.3	9
10	609.1	669.8	730.6	791.7	853.1	914.7	976.6	1038.9	1101.4	1164.4	10
11	10.1	70.8	31.6	92.7	54.1	15.7	77.7	39.9	02.5	65.4	11
12	11.1	71.8	32.7	93.8	55.1	16.8	78.7	40.9	03.5	66.5	12
13	12.1	72.8	33.7	94.8	56.1	17.8	79.7	42.0	04.6	67.5	13
14	13.1	73.8	34.7	95.8	57.2	18.8	80.8	43.0	05.6	68.6	14
15	614.1	674.8	735.7	796.8	858.2	919.8	981.8	1044.1	1106.7	1169.7	15
16	15.2	75.8	36.7	97.8	59.2	20.9	82.8	45.1	07.7	70.7	16
17	16.2	76.8	37.7	98.9	60.2	21.9	83.9	46.1	08.8	71.8	17
18	17.2	77.9	38.8	99.9	61.3	22.9	84.9	47.2	09.8	72.8	18
19	18.2	78.9	39.8	800.9	62.3	24.0	85.9	48.2	10.9	73.9	19
20	619.2	679.9	740.8	801.9	863.3	925.0	987.0	1049.3	1111.9	1174.9	20
21	20.2	80.9	41.8	02.9	64.3	26.0	88.0	50.3	13.0	76.0	21
22	21.2	81.9	42.8	04.0	65.4	27.1	89.0	51.3	14.0	77.0	22
23	22.2	82.9	43.8	05.0	66.4	28.1	90.1	52.4	15.0	78.1	23
24	23.2	83.9	44.9	06.0	67.4	29.1	91.1	53.4	16.1	79.1	24
25	624.2	684.9	745.9	807.0	868.5	930.1	992.1	1054.5	1117.1	1180.2	25
26	25.3	86.0	46.9	08.1	69.5	31.2	93.2	55.5	18.2	81.2	26
27	26.3	87.0	47.9	09.1	70.5	32.2	94.2	56.6	19.2	82.3	27
28	27.3	88.0	48.9	10.1	71.5	33.2	95.3	57.6	20.3	83.3	28
29	28.3	89.0	49.9	11.1	72.6	34.3	96.3	58.6	21.3	84.4	29
30	629.3	690.0	751.0	812.1	873.6	935.3	997.3	1059.7	1122.4	1185.5	30
31	30.3	91.0	52.0	13.2	74.6	36.3	98.4	60.7	23.4	86.5	31
32	31.3	92.0	53.0	14.2	75.6	37.4	99.4	61.8	24.5	87.6	32
33	32.3	93.1	54.0	15.2	76.7	38.4	1000.4	62.8	25.5	88.6	33
34	33.3	94.1	55.0	16.2	77.7	39.4	01.5	63.9	26.6	89.7	34
35	634.3	695.1	756.0	817.3	878.7	940.5	1002.5	1064.9	1127.6	1190.7	35
36	35.4	96.1	57.1	18.3	79.7	41.5	03.6	65.9	28.7	91.8	36
37	36.4	97.1	58.1	19.3	80.8	42.5	04.6	67.0	29.7	92.8	37
38	37.4	98.1	59.1	20.3	81.8	43.6	05.6	68.0	30.8	93.9	38
39	38.4	99.1	60.1	21.3	82.8	44.6	06.7	69.1	31.8	95.0	39
40	639.4	700.2	761.1	822.4	883.8	945.6	1007.7	1070.1	1132.9	1196.0	40
41	40.4	01.2	62.2	23.4	84.9	46.7	08.7	71.2	33.9	97.1	41
42	41.4	02.2	63.2	24.4	85.9	47.7	09.8	72.2	35.0	98.1	42
43	42.4	03.2	64.2	25.4	86.9	48.7	10.8	73.2	36.0	99.2	43
44	43.4	04.2	65.2	26.5	88.0	49.7	11.8	74.3	37.1	1200.2	44
45	644.5	705.2	766.2	827.5	889.0	950.8	1012.9	1075.3	1138.1	1201.3	45
46	45.5	06.2	67.3	28.5	90.0	51.8	13.9	76.4	39.2	02.3	46
47	46.5	07.3	68.3	29.5	91.0	52.8	15.0	77.4	40.2	03.4	47
48	47.5	08.3	69.3	30.5	92.1	53.9	16.0	78.5	41.3	04.5	48
49	48.5	09.3	70.3	31.6	93.1	54.9	17.0	79.5	42.3	05.5	49
50	649.5	710.3	771.3	832.6	894.1	955.9	1018.1	1080.5	1143.4	1206.6	50
51	50.5	11.3	72.3	33.6	95.2	57.0	19.1	81.6	44.4	07.6	51
52	51.5	12.3	73.4	34.6	96.2	58.0	20.2	82.6	45.5	08.7	52
53	52.5	13.4	74.4	35.7	97.2	59.0	21.2	83.7	46.5	09.7	53
54	53.6	14.4	75.4	36.7	98.2	60.1	22.2	84.7	47.6	10.8	54
55	654.6	715.4	776.4	837.7	899.3	961.1	1023.3	1085.8	1148.6	1211.8	55
56	55.6	16.4	77.4	38.7	900.3	62.1	24.3	86.8	49.7	12.9	56
57	56.6	17.4	78.5	39.8	01.3	63.2	25.3	87.9	50.7	14.0	57
58	57.6	18.4	79.5	40.8	02.3	64.2	26.4	88.9	51.8	15.0	58
59	58.6	19.4	80.5	41.8	03.4	65.2	27.4	89.9	52.8	16.1	59
M.	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	M.

TABLE 3.

Meridional Parts, or Increased Latitudes.

Comp. $\frac{1}{293.465}$

M.	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	M.
0	1217.1	1280.8	1344.9	1409.5	1474.5	1540.1	1606.2	1672.9	1740.2	1808.1	0
1	18.2	81.9	46.0	10.6	75.6	41.2	07.3	74.0	41.3	09.2	1
2	19.3	82.9	47.1	11.6	76.7	42.3	08.4	75.1	42.4	10.4	2
3	20.3	84.0	48.1	12.7	77.8	43.4	09.5	76.2	43.6	11.5	3
4	21.4	85.1	49.2	13.8	78.9	44.5	10.6	77.4	44.7	12.6	4
5	1222.4	1286.1	1350.3	1414.9	1480.0	1545.6	1611.7	1678.5	1745.8	1813.8	5
6	23.5	87.2	51.4	16.0	81.1	46.7	12.9	79.6	46.9	14.9	6
7	24.5	88.3	52.4	17.1	82.2	47.8	14.0	80.7	48.1	16.1	7
8	25.6	89.3	53.5	18.1	83.3	48.9	15.1	81.8	49.2	17.2	8
9	26.7	90.4	54.6	19.2	84.3	50.0	16.2	82.9	50.3	18.3	9
10	1227.7	1291.5	1355.7	1420.3	1485.4	1551.1	1617.3	1684.1	1751.5	1819.5	10
11	28.8	92.5	56.7	21.4	86.5	52.2	18.4	85.2	52.6	20.6	11
12	29.8	93.6	57.8	22.5	87.6	53.3	19.5	86.3	53.7	21.8	12
13	30.9	94.7	58.9	23.5	88.7	54.4	20.6	87.4	54.8	22.9	13
14	32.0	95.7	59.9	24.6	89.8	55.5	21.7	88.5	56.0	24.0	14
15	1233.0	1296.8	1361.0	1425.7	1490.9	1556.6	1622.8	1689.7	1757.1	1825.2	15
16	34.1	97.9	62.1	26.8	92.0	57.7	23.9	90.8	58.2	26.3	16
17	35.1	98.9	63.2	27.9	93.1	58.8	25.0	91.9	59.4	27.5	17
18	36.2	1300.0	64.2	29.0	94.2	59.9	26.2	93.0	60.5	28.6	18
19	37.3	01.1	65.3	30.0	95.2	61.0	27.3	94.1	61.6	29.7	19
20	1238.3	1302.1	1366.4	1431.1	1496.3	1562.1	1628.4	1695.3	1762.7	1830.9	20
21	39.4	03.2	67.5	32.2	97.4	63.2	29.5	96.4	63.9	32.0	21
22	40.4	04.3	68.5	33.3	98.5	64.3	30.6	97.5	65.0	33.2	22
23	41.5	05.3	69.6	34.4	99.6	65.4	31.7	98.6	66.1	34.3	23
24	42.6	06.4	70.7	35.4	1500.7	66.5	32.8	99.7	67.3	35.4	24
25	1243.6	1307.5	1371.8	1436.5	1501.8	1567.6	1633.9	1700.9	1768.4	1836.6	25
26	44.7	08.5	72.8	37.6	02.9	68.7	35.0	02.0	69.5	37.7	26
27	45.7	09.6	73.9	38.7	04.0	69.8	36.1	03.1	70.7	38.9	27
28	46.8	10.7	75.0	39.8	05.1	70.9	37.3	04.2	71.8	40.0	28
29	47.9	11.7	76.1	40.9	06.2	72.0	38.4	05.3	72.9	41.2	29
30	1248.9	1312.8	1377.1	1442.0	1507.3	1573.1	1639.5	1706.5	1774.1	1842.3	30
31	50.0	13.9	78.2	43.0	08.4	74.2	40.6	07.6	75.2	43.4	31
32	51.0	14.9	79.3	44.1	09.4	75.3	41.7	08.7	76.3	44.6	32
33	52.1	16.0	80.4	45.2	10.5	76.4	42.8	09.8	77.4	45.7	33
34	53.2	17.1	81.5	46.3	11.6	77.5	43.9	10.9	78.6	46.9	34
35	1254.2	1318.2	1382.5	1447.4	1512.7	1578.6	1645.0	1712.1	1779.7	1848.0	35
36	55.3	19.2	83.6	48.5	13.8	79.7	46.2	13.2	80.8	49.2	36
37	56.4	20.3	84.7	49.5	14.9	80.8	47.3	14.3	82.0	50.3	37
38	57.4	21.4	85.8	50.6	16.0	81.9	48.4	15.4	83.1	51.4	38
39	58.5	22.4	86.8	51.7	17.1	83.0	49.5	16.6	84.2	52.6	39
40	1259.5	1323.5	1387.9	1452.8	1518.2	1584.1	1650.6	1717.7	1785.4	1853.7	40
41	60.6	24.6	89.0	53.9	19.3	85.2	51.7	18.8	86.5	54.9	41
42	61.7	25.6	90.1	55.0	20.4	86.3	52.8	19.9	87.6	56.0	42
43	62.7	26.7	91.1	56.1	21.5	87.4	53.9	21.1	88.8	57.2	43
44	63.8	27.8	92.2	57.1	22.6	88.5	55.1	22.2	89.9	58.3	44
45	1264.9	1328.9	1393.3	1458.2	1523.7	1589.6	1656.2	1723.3	1791.1	1859.5	45
46	65.9	29.9	94.4	59.3	24.8	90.7	57.3	24.4	92.2	60.6	46
47	67.0	31.0	95.5	60.4	25.9	91.8	58.4	25.5	93.3	61.8	47
48	68.0	32.1	96.5	61.5	27.0	92.9	59.5	26.7	94.5	62.9	48
49	69.1	33.1	97.6	62.6	28.0	94.1	60.6	27.8	95.6	64.0	49
50	1270.2	1334.2	1398.7	1463.7	1529.1	1595.2	1661.7	1728.9	1796.7	1865.2	50
51	71.2	35.3	99.8	64.8	30.2	96.3	62.9	30.0	97.9	66.3	51
52	72.3	36.3	1400.9	65.8	31.3	97.4	64.0	31.2	99.0	67.5	52
53	73.4	37.4	01.9	66.9	32.4	98.5	65.1	32.3	1800.1	68.6	53
54	74.4	38.5	03.0	68.0	33.5	99.6	66.2	33.4	01.3	69.8	54
55	1275.5	1339.6	1404.1	1469.1	1534.6	1600.7	1667.3	1734.5	1802.4	1870.9	55
56	76.6	40.6	05.2	70.2	35.7	01.8	68.4	35.7	03.5	72.1	56
57	77.6	41.7	06.2	71.3	36.8	02.9	69.5	36.8	04.7	73.2	57
58	78.7	42.8	07.3	72.4	37.9	04.0	70.7	37.9	05.8	74.4	58
59	79.7	43.8	08.4	73.5	39.0	05.1	71.8	39.1	07.0	75.5	59
M.	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	M.

TABLE 3.

Meridional Parts, or Increased Latitudes.

Comp. $\frac{1}{293.465}$.

M.	30°	31°	32°	33°	34°	35°	36°	37°	38°	39°	M.
0	1876.7	1946.0	2016.0	2086.8	2158.4	2230.9	2304.2	2378.5	2453.8	2530.2	0
1	77.8	47.1	17.2	88.0	59.6	32.1	05.5	79.8	55.1	31.5	1
2	79.0	48.3	18.3	89.2	60.8	33.3	06.7	81.0	56.4	32.8	2
3	80.1	49.4	19.5	90.3	62.0	34.5	07.9	82.3	57.6	34.0	3
4	81.3	50.6	20.7	91.5	63.2	35.7	09.2	83.5	58.9	35.3	4
5	1882.4	1951.8	2021.9	2092.7	2164.4	2236.9	2310.4	2384.8	2460.2	2536.6	5
6	83.6	52.9	23.0	93.9	65.6	38.2	11.6	86.0	61.4	37.9	6
7	84.7	54.1	24.2	95.1	66.8	39.4	12.9	87.3	62.7	39.2	7
8	85.9	55.3	25.4	96.3	68.0	40.6	14.1	88.5	64.0	40.5	8
9	87.0	56.4	26.6	97.5	69.2	41.8	15.3	89.8	65.2	41.7	9
10	1888.2	1957.6	2027.7	2098.7	2170.4	2243.0	2316.5	2391.0	2466.5	2543.0	10
11	89.3	58.7	28.9	99.8	71.6	44.2	17.8	92.3	67.8	44.3	11
12	90.5	59.9	30.1	2101.0	72.8	45.5	19.0	93.5	69.0	45.6	12
13	91.6	61.1	31.3	02.2	74.0	46.7	20.3	94.8	70.3	46.9	13
14	92.8	62.2	32.4	03.4	75.2	47.9	21.5	96.0	71.6	48.2	14
15	1893.9	1963.4	2033.6	2104.6	2176.4	2249.1	2322.7	2397.3	2472.8	2549.5	15
16	95.1	64.6	34.8	05.8	77.6	50.3	24.0	98.5	74.1	50.7	16
17	96.2	65.7	36.0	07.0	78.8	51.6	25.2	99.8	75.4	52.0	17
18	97.4	66.9	37.1	08.2	80.0	52.8	26.4	2401.0	76.6	53.3	18
19	98.5	68.1	38.3	09.4	81.2	54.0	27.7	02.3	77.9	54.6	19
20	1899.7	1969.2	2039.5	2110.6	2182.5	2255.2	2328.9	2403.5	2479.2	2555.9	20
21	1900.8	70.4	40.7	11.8	83.7	56.4	30.1	04.8	80.4	57.2	21
22	02.0	71.5	41.8	12.9	84.9	57.7	31.4	06.0	81.7	58.5	22
23	03.1	72.7	43.0	14.1	86.1	58.9	32.6	07.3	83.0	59.8	23
24	04.3	73.9	44.2	15.3	87.3	60.1	33.8	08.5	84.3	61.0	24
25	1905.5	1975.0	2045.4	2116.5	2188.5	2261.3	2335.1	2409.8	2485.5	2562.3	25
26	06.6	76.2	46.6	17.7	89.7	62.5	36.3	11.1	86.8	63.6	26
27	07.8	77.4	47.7	18.9	90.9	63.8	37.6	12.3	88.1	64.9	27
28	08.9	78.5	48.9	20.1	92.1	65.0	38.8	13.6	89.3	66.2	28
29	10.1	79.7	50.1	21.3	93.3	66.2	40.0	14.8	90.6	67.5	29
30	1911.2	1980.9	2051.3	2122.5	2194.5	2267.4	2341.3	2416.1	2491.9	2568.8	30
31	12.4	82.0	52.5	23.7	95.7	68.7	42.5	17.3	93.2	70.1	31
32	13.5	83.2	53.6	24.9	96.9	69.9	43.7	18.6	94.4	71.4	32
33	14.7	84.4	54.8	26.1	98.1	71.1	45.0	19.8	95.7	72.7	33
34	15.8	85.5	56.0	27.3	99.4	72.3	46.2	21.1	97.0	73.9	34
35	1917.0	1986.7	2057.2	2128.5	2200.6	2273.5	2347.5	2422.3	2498.3	2575.2	35
36	18.2	87.9	58.4	29.6	01.8	74.8	48.7	23.6	99.5	76.5	36
37	19.3	89.1	59.5	30.8	03.0	76.0	49.9	24.9	2500.8	77.8	37
38	20.5	90.2	60.7	32.0	04.2	77.2	51.2	26.1	02.1	79.1	38
39	21.6	91.4	61.9	33.2	05.4	78.4	52.4	27.4	03.4	80.4	39
40	1922.8	1992.6	2063.1	2134.4	2206.6	2279.7	2353.7	2428.6	2504.6	2581.7	40
41	23.9	93.7	64.3	35.6	07.8	80.9	54.9	29.9	05.9	83.0	41
42	25.1	94.9	65.5	36.8	09.0	82.1	56.1	31.2	07.2	84.3	42
43	26.3	96.1	66.6	38.0	10.2	83.3	57.4	32.4	08.5	85.6	43
44	27.4	97.2	67.8	39.2	11.5	84.6	58.6	33.7	09.7	86.9	44
45	1928.6	1998.4	2069.0	2140.4	2212.7	2285.8	2359.9	2434.9	2511.0	2588.2	45
46	29.7	99.6	70.2	41.6	13.9	87.0	61.1	36.2	12.3	89.5	46
47	30.9	2000.7	71.4	42.8	15.1	88.3	62.4	37.4	13.6	90.8	47
48	32.0	01.9	72.6	44.0	16.3	89.5	63.6	38.7	14.8	92.1	48
49	33.2	03.1	73.7	45.2	17.5	90.7	64.8	40.0	16.1	93.4	49
50	1934.4	2004.3	2074.9	2146.4	2218.7	2291.9	2366.1	2441.2	2517.4	2594.7	50
51	35.5	05.4	76.1	47.6	19.9	93.2	67.3	42.5	18.7	96.0	51
52	36.7	06.6	77.3	48.8	21.1	94.4	68.6	43.7	20.0	97.3	52
53	37.8	07.8	78.5	50.0	22.4	95.6	69.8	45.0	21.2	98.5	53
54	39.0	08.9	79.7	51.2	23.6	96.9	71.1	46.3	22.5	99.8	54
55	1940.2	2010.1	2080.8	2152.4	2224.8	2298.1	2372.3	2447.5	2523.8	2601.1	55
56	41.3	11.3	82.0	53.6	26.0	99.3	73.6	48.8	25.1	02.4	56
57	42.5	12.5	83.2	54.8	27.2	2300.5	74.8	50.1	26.4	03.7	57
58	43.6	13.6	84.4	56.0	28.4	01.8	76.1	51.3	27.6	05.0	58
59	44.8	14.8	85.6	57.2	29.6	03.0	77.3	52.6	28.9	06.3	59
M.	30°	31°	32°	33°	34°	35°	36°	37°	38°	39°	M.

TABLE 3.

Meridional Parts, or Increased Latitudes.

Comp. $\frac{1}{293.465}$

M.	40°	41°	42°	43°	44°	45°	46°	47°	48°	49°	M.
0	2607.6	2686.2	2766.0	2847.1	2929.5	3013.4	3098.7	3185.6	3274.1	3364.4	0
1	08.9	87.6	67.4	48.5	30.9	14.8	3100.1	87.1	75.6	65.9	1
2	10.2	88.9	68.7	49.9	32.3	16.2	01.6	88.5	77.1	67.4	2
3	11.5	90.2	70.1	51.2	33.7	17.6	03.0	90.0	78.6	69.0	3
4	12.8	91.5	71.4	52.6	35.1	19.0	04.4	91.4	80.1	70.5	4
5	2614.1	2692.8	2772.8	2853.9	2936.5	3020.4	3105.9	3192.9	3281.6	3372.0	5
6	15.4	94.2	74.1	55.3	37.9	21.8	07.3	94.4	83.1	73.5	6
7	16.8	95.5	75.4	56.7	39.3	23.3	08.8	95.8	84.6	75.1	7
8	18.1	96.8	76.8	58.0	40.6	24.7	10.2	97.3	86.1	76.6	8
9	19.4	98.1	78.1	59.4	42.0	26.1	11.6	98.8	87.6	78.1	9
10	2620.7	2699.5	2779.5	2860.8	2943.4	3027.5	3113.1	3200.2	3289.0	3379.6	10
11	22.0	2700.8	80.8	62.1	44.8	28.9	14.5	01.7	90.5	81.2	11
12	23.3	02.1	82.2	63.5	46.2	30.3	16.0	03.2	92.0	82.7	12
13	24.6	03.4	83.5	64.9	47.6	31.7	17.4	04.6	93.5	84.2	13
14	25.9	04.8	84.8	66.2	49.0	33.2	18.8	06.1	95.0	85.7	14
15	2627.2	2706.1	2786.2	2867.6	2950.4	3034.6	3120.3	3207.6	3296.5	3387.3	15
16	28.5	07.4	87.5	69.0	51.8	36.0	21.7	09.0	98.0	88.8	16
17	29.8	08.7	88.9	70.3	53.2	37.4	23.2	10.5	99.5	90.3	17
18	31.1	10.1	90.2	71.7	54.5	38.8	24.6	12.0	3301.0	91.8	18
19	32.4	11.4	91.6	73.1	55.9	40.2	26.0	13.4	02.5	93.4	19
20	2633.7	2712.7	2792.9	2874.4	2957.3	3041.7	3127.5	3214.9	3304.0	3394.9	20
21	35.0	14.0	94.3	75.8	58.7	43.1	28.9	16.4	05.5	96.4	21
22	36.3	15.4	95.6	77.2	60.1	44.5	30.4	17.9	07.0	98.0	22
23	37.6	16.7	97.0	78.6	61.5	45.9	31.8	19.3	08.5	99.5	23
24	38.9	18.0	98.3	79.9	62.9	47.3	33.3	20.8	10.0	3401.0	24
25	2640.2	2719.3	2799.7	2881.3	2964.3	3048.7	3134.7	3222.3	3311.5	3402.6	25
26	41.6	20.7	2801.0	82.7	65.7	50.2	36.2	23.7	13.0	04.1	26
27	42.9	22.0	02.4	84.0	67.1	51.6	37.6	25.2	14.5	05.6	27
28	44.2	23.3	03.7	85.4	68.5	53.0	39.0	26.7	16.0	07.2	28
29	45.5	24.7	05.1	86.8	69.9	54.4	40.5	28.2	17.5	08.7	29
30	2646.8	2726.0	2806.4	2888.2	2971.3	3055.9	3141.9	3229.6	3319.0	3410.2	30
31	48.1	27.3	07.8	89.5	72.7	57.3	43.4	31.1	20.5	11.8	31
32	49.4	28.6	09.1	90.9	74.1	58.7	44.8	32.6	22.1	13.3	32
33	50.7	30.0	10.5	92.3	75.5	60.1	46.3	34.1	23.6	14.8	33
34	52.0	31.3	11.8	93.7	76.9	61.5	47.7	35.6	25.1	16.4	34
35	2653.3	2732.6	2813.2	2895.0	2978.3	3063.0	3149.2	3237.0	3326.6	3417.9	35
36	54.7	34.0	14.5	96.4	79.7	64.4	50.6	38.5	28.1	19.5	36
37	56.0	35.3	15.9	97.8	81.1	65.8	52.1	40.0	29.6	21.0	37
38	57.3	36.6	17.2	99.2	82.5	67.2	53.5	41.5	31.1	22.5	38
39	58.6	38.0	18.6	2900.5	83.9	68.7	55.0	42.9	32.6	24.1	39
40	2659.9	2739.3	2820.0	2901.9	2985.3	3070.1	3156.4	3244.4	3334.1	3425.6	40
41	61.2	40.6	21.3	03.3	86.7	71.5	57.9	45.9	35.6	27.2	41
42	62.5	42.0	22.7	04.7	88.1	72.9	59.4	47.4	37.1	28.7	42
43	63.9	43.3	24.0	06.1	89.5	74.4	60.8	48.9	38.6	30.2	43
44	65.2	44.6	25.4	07.4	90.9	75.8	62.3	50.3	40.2	31.8	44
45	2666.5	2746.0	2826.7	2908.8	2992.3	3077.2	3163.7	3251.8	3341.7	3433.3	45
46	67.8	47.3	28.1	10.2	93.7	78.7	65.2	53.3	43.2	34.9	46
47	69.1	48.6	29.4	11.6	95.1	80.1	66.6	54.8	44.7	36.4	47
48	70.4	50.0	30.8	13.0	96.5	81.5	68.1	56.3	46.2	38.0	48
49	71.7	51.3	32.2	14.3	97.9	82.9	69.5	57.8	47.7	39.5	49
50	2673.1	2752.7	2833.5	2915.7	2999.3	3084.4	3171.0	3259.3	3349.2	3441.0	50
51	74.4	54.0	34.9	17.1	3000.7	85.8	72.5	60.7	50.8	42.6	51
52	75.7	55.3	36.2	18.5	02.1	87.2	73.9	62.2	52.3	44.1	52
53	77.0	56.7	37.6	19.9	03.5	88.7	75.4	63.7	53.8	45.7	53
54	78.3	58.0	39.0	21.2	04.9	90.1	76.8	65.2	55.3	47.2	54
55	2679.6	2759.3	2840.3	2922.6	3006.3	3091.5	3178.3	3266.7	3356.8	3448.8	55
56	81.0	60.7	41.7	24.0	07.7	93.0	79.7	68.2	58.3	50.3	56
57	82.3	62.0	43.0	25.4	09.2	94.4	81.2	69.7	59.9	51.9	57
58	83.6	63.4	44.4	26.8	10.6	95.8	82.7	71.1	61.4	53.4	58
59	84.9	64.7	45.8	28.2	12.0	97.3	84.1	72.6	62.9	55.0	59
M.	40°	41°	42°	43°	44°	45°	46°	47°	48°	49°	M.

TABLE 3.

Meridional Parts, or Increased Latitudes.

Comp. $\frac{1}{293.465}$

M.	50°	51°	52°	53°	54°	55°	56°	57°	58°	59°	M.
0	3456.5	3550.6	3646.7	3745.1	3845.7	3948.8	4054.5	4163.0	4274.4	4389.1	0
1	58.1	52.2	48.4	46.7	47.4	50.5	56.3	64.8	76.3	91.0	1
2	59.6	53.8	50.0	48.4	49.1	52.3	58.1	66.6	78.2	92.9	2
3	61.2	55.4	51.6	50.0	50.8	54.0	59.8	68.5	80.1	94.9	3
4	62.7	56.9	53.2	51.7	52.5	55.7	61.6	70.3	82.0	96.8	4
5	3464.3	3558.5	3654.8	3753.4	3854.2	3957.5	4063.4	4172.1	4283.9	4398.8	5
6	65.9	60.1	56.5	55.0	55.9	59.2	65.2	74.0	85.7	4400.7	6
7	67.4	61.7	58.1	56.7	57.6	61.0	67.0	75.8	87.6	02.6	7
8	69.0	63.3	59.7	58.3	59.3	62.7	68.8	77.7	89.5	04.6	8
9	70.5	64.9	61.3	60.0	61.0	64.5	70.6	79.5	91.4	06.5	9
10	3472.1	3566.5	3663.0	3761.7	3862.7	3966.2	4072.4	4181.3	4293.3	4408.5	10
11	73.6	68.1	64.6	63.3	64.4	68.0	74.2	83.2	95.2	10.4	11
12	75.2	69.7	66.2	65.0	66.1	69.7	76.0	85.0	97.1	12.4	12
13	76.7	71.3	67.9	66.7	67.8	71.5	77.7	86.9	99.0	14.3	13
14	78.3	72.8	69.5	68.3	69.5	73.2	79.5	88.7	4300.9	16.3	14
15	3479.9	3574.4	3671.1	3770.0	3871.2	3975.0	4081.3	4190.6	4302.8	4418.2	15
16	81.4	76.0	72.7	71.7	72.9	76.7	83.1	92.4	04.7	20.2	16
17	83.0	77.6	74.4	73.3	74.6	78.5	84.9	94.2	06.6	22.1	17
18	84.5	79.2	76.0	75.0	76.3	80.2	86.7	96.1	08.5	24.1	18
19	86.1	80.8	77.6	76.7	78.1	82.0	88.5	97.9	10.4	26.1	19
20	3487.7	3582.4	3679.3	3778.3	3879.8	3983.7	4090.3	4199.8	4312.3	4428.0	20
21	89.2	84.0	80.9	80.0	81.5	85.5	92.1	4201.6	14.2	30.0	21
22	90.8	85.6	82.5	81.7	83.2	87.2	93.9	03.5	16.1	31.9	22
23	92.4	87.2	84.2	83.3	84.9	89.0	95.7	05.3	18.0	33.9	23
24	93.9	88.8	85.8	85.0	86.6	90.7	97.5	07.2	19.9	35.8	24
25	3495.5	3590.4	3687.4	3786.7	3888.3	3992.5	4099.3	4209.0	4321.8	4437.8	25
26	97.1	92.0	89.1	88.4	90.0	94.3	4101.1	10.9	23.7	39.8	26
27	98.6	93.6	90.7	90.0	91.8	96.0	02.9	12.8	25.6	41.7	27
28	3500.2	95.2	92.3	91.7	93.5	97.8	04.8	14.6	27.5	43.7	28
29	01.8	96.8	94.0	93.4	95.2	99.5	06.6	16.5	29.4	45.7	29
30	3503.3	3598.4	3695.6	3795.1	3896.9	4001.3	4108.4	4218.3	4331.3	4447.6	30
31	04.9	3600.0	97.3	96.8	98.6	03.1	10.2	20.2	33.2	49.6	31
32	06.5	01.6	98.9	98.4	3900.4	04.8	12.0	22.0	35.2	51.6	32
33	08.0	03.2	3700.5	3800.1	02.1	06.6	13.8	23.9	37.1	53.5	33
34	09.6	04.8	02.2	01.8	03.8	08.3	15.6	25.8	39.0	55.5	34
35	3511.2	3606.4	3703.8	3803.5	3905.5	4010.1	4117.4	4227.6	4340.9	4457.5	35
36	12.7	08.0	05.5	05.1	07.2	11.9	19.2	29.5	42.8	59.4	36
37	14.3	09.6	07.1	06.8	09.0	13.6	21.0	31.3	44.7	61.4	37
38	15.9	11.2	08.7	08.5	10.7	15.4	22.9	33.2	46.6	63.4	38
39	17.5	12.8	10.4	10.2	12.4	17.2	24.7	35.1	48.6	65.4	39
40	3519.0	3614.5	3712.0	3811.9	3914.1	4018.9	4126.5	4236.9	4350.5	4467.3	40
41	20.6	16.1	13.7	13.6	15.9	20.7	28.3	38.8	52.4	69.3	41
42	22.2	17.7	15.3	15.2	17.6	22.5	30.1	40.7	54.3	71.3	42
43	23.7	19.3	17.0	17.0	19.3	24.3	31.9	42.5	56.2	73.3	43
44	25.3	20.9	18.6	18.6	21.0	26.0	33.8	44.4	58.2	75.3	44
45	3526.9	3622.5	3720.3	3820.3	3922.8	4027.8	4135.6	4246.3	4360.1	4477.2	45
46	28.5	24.1	21.9	22.0	24.5	29.6	37.4	48.1	62.0	79.2	46
47	30.1	25.7	23.6	23.7	26.2	31.4	39.2	50.0	63.9	81.2	47
48	31.6	27.3	25.2	25.4	28.0	33.1	41.0	51.9	65.9	83.2	48
49	33.2	29.0	26.9	27.1	29.7	34.9	42.9	53.8	67.8	85.2	49
50	3534.8	3630.6	3728.5	3828.7	3931.4	4036.7	4144.7	4255.6	4369.7	4487.2	50
51	36.4	32.2	30.2	30.4	33.2	38.5	46.5	57.5	71.7	89.1	51
52	37.9	33.8	31.8	32.1	34.9	40.2	48.3	59.4	73.6	91.1	52
53	39.5	35.4	33.5	33.8	36.6	42.0	50.2	61.3	75.5	93.1	53
54	41.1	37.0	35.1	35.5	38.4	43.8	52.0	63.1	77.4	95.1	54
55	3542.7	3638.6	3736.8	3837.2	3940.1	4045.6	4153.8	4265.0	4379.4	4497.1	55
56	44.3	40.3	38.4	38.9	41.8	47.4	55.7	66.9	81.3	99.1	56
57	45.9	41.9	40.1	40.6	43.6	49.1	57.5	68.8	83.2	4501.1	57
58	47.4	43.5	41.7	42.3	45.3	50.9	59.3	70.7	85.2	03.1	58
59	49.0	45.1	43.4	45.0	47.0	52.7	61.1	72.5	87.1	05.1	59
M.	50°	51°	52°	53°	54°	55°	56°	57°	58°	59°	M.

TABLE 3.

Meridional Parts, or Increased Latitudes.

Comp. $\frac{1}{293.465}$

M.	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°	M.
0	4507.1	4628.7	4754.3	4884.1	5018.4	5157.6	5302.1	5452.4	5609.1	5772.7	0
1	09.1	30.8	56.4	86.3	20.6	59.9	04.6	55.0	11.8	75.5	1
2	11.1	32.9	58.6	88.5	22.9	62.3	07.0	57.6	14.4	78.3	2
3	13.1	34.9	60.7	90.7	25.2	64.7	09.5	60.1	17.1	81.1	3
4	15.1	37.0	62.8	92.9	27.5	67.0	11.9	62.7	19.8	83.8	4
5	4517.1	4639.0	4764.9	4895.1	5029.8	5169.4	5314.4	5465.2	5622.4	5786.6	5
6	19.1	41.1	67.1	97.3	32.1	71.8	16.9	67.8	25.1	89.4	6
7	21.1	43.2	69.2	99.5	34.3	74.2	19.3	70.4	27.8	92.2	7
8	23.1	45.2	71.3	4901.7	36.6	76.5	21.8	72.9	30.5	95.1	8
9	25.1	47.3	73.5	03.9	38.9	78.9	24.3	75.5	33.2	97.9	9
10	4527.1	4649.4	4775.6	4906.1	5041.2	5181.3	5326.7	5477.1	5635.9	5800.7	10
11	29.1	51.5	77.8	08.3	43.5	83.7	29.2	80.7	38.5	03.5	11
12	31.1	53.5	79.9	10.5	45.8	86.0	31.7	83.2	41.2	06.3	12
13	33.1	55.6	82.0	12.8	48.1	88.4	34.2	85.8	43.9	09.1	13
14	35.1	57.7	84.2	15.0	50.4	90.8	36.6	88.4	46.6	11.9	14
15	4537.1	4659.7	4786.3	4917.2	5052.7	5193.2	5339.1	5491.0	5649.3	5814.7	15
16	39.2	61.8	88.5	19.4	55.0	95.6	41.6	93.6	52.0	17.6	16
17	41.2	63.9	90.6	21.6	57.3	98.0	44.1	96.2	54.7	20.4	17
18	43.2	66.0	92.8	23.9	59.6	5200.4	46.6	98.7	57.4	23.2	18
19	45.2	68.1	94.9	26.1	61.9	02.7	49.1	5501.3	60.1	26.0	19
20	4547.2	4670.1	4797.1	4928.3	5064.2	5205.1	5351.5	5503.9	5662.8	5828.9	20
21	49.2	72.2	99.2	30.5	66.5	07.5	54.0	06.5	65.5	31.7	21
22	51.3	74.3	4801.4	32.8	68.8	09.9	56.5	09.1	68.2	34.5	22
23	53.3	76.4	03.5	35.0	71.1	12.3	59.0	11.7	70.9	37.4	23
24	55.3	78.5	05.7	37.2	73.4	14.7	61.5	14.3	73.7	40.2	24
25	4557.3	4680.6	4807.8	4939.4	5075.7	5217.1	5364.0	5516.9	5676.4	5843.0	25
26	59.3	82.6	10.0	41.7	78.1	19.5	66.5	19.5	79.1	45.9	26
27	61.4	84.7	12.1	43.9	80.4	21.9	69.0	22.1	81.8	48.7	27
28	63.4	86.8	14.3	46.1	82.7	24.3	71.5	24.7	84.5	51.6	28
29	65.4	88.9	16.5	48.4	85.0	26.7	74.0	27.3	87.3	54.4	29
30	4567.4	4691.0	4818.6	4950.6	5087.3	5229.1	5376.5	5529.9	5690.0	5857.3	30
31	69.5	93.1	20.8	52.9	89.6	31.6	79.0	32.5	92.7	60.1	31
32	71.5	95.2	23.0	55.1	92.0	34.0	81.5	35.2	95.4	63.0	32
33	73.5	97.3	25.1	57.3	94.3	36.4	84.0	37.8	98.2	65.9	33
34	75.6	99.4	27.3	59.6	96.6	38.8	86.5	40.4	5700.9	68.7	34
35	4577.6	4701.5	4829.5	4961.8	5098.9	5241.2	5389.1	5543.0	5703.6	5871.6	35
36	79.6	03.6	31.6	64.1	5101.3	43.6	91.6	45.6	06.4	74.4	36
37	81.7	05.7	33.8	66.3	03.6	46.0	94.1	48.3	09.1	77.3	37
38	83.7	07.8	36.0	68.6	05.9	48.5	96.6	50.9	11.9	80.2	38
39	85.7	09.9	38.1	70.8	08.3	50.9	99.1	53.5	14.6	83.1	39
40	4587.8	4712.0	4840.3	4973.1	5110.6	5253.3	5401.6	5556.1	5717.3	5885.9	40
41	89.8	14.1	42.5	75.3	12.9	55.7	04.2	58.8	20.1	88.8	41
42	91.8	16.2	44.7	77.6	15.3	58.2	06.7	61.4	22.8	91.7	42
43	93.9	18.3	46.8	79.8	17.6	60.6	09.2	64.0	25.6	94.6	43
44	95.9	20.4	49.0	82.1	19.9	63.0	11.8	66.7	28.3	97.4	44
45	4598.0	4722.5	4851.2	4984.3	5122.3	5265.4	5414.3	5569.3	5731.1	5900.3	45
46	4600.0	24.6	53.4	86.6	24.6	67.9	16.8	71.9	33.9	03.2	46
47	02.1	26.7	55.6	88.9	27.0	70.3	19.3	74.6	36.6	06.1	47
48	04.1	28.9	57.8	91.1	29.3	72.8	21.9	77.2	39.4	09.0	48
49	06.1	31.0	59.9	93.4	31.7	75.2	24.4	79.9	42.1	11.9	49
50	4608.2	4733.1	4862.1	4995.6	5134.0	5277.6	5427.0	5582.5	5744.9	5914.8	50
51	10.2	35.2	64.3	97.9	36.4	80.1	29.5	85.2	47.7	17.7	51
52	12.3	37.3	66.5	5000.2	38.7	82.5	32.0	87.8	50.4	20.6	52
53	14.3	39.4	68.7	02.4	41.1	85.0	34.6	90.5	53.2	23.5	53
54	16.4	41.6	70.9	04.7	43.4	87.4	37.1	93.1	56.0	26.4	54
55	4618.5	4743.7	4873.1	5007.0	5145.8	5289.8	5439.7	5595.8	5758.8	5929.3	55
56	20.5	45.8	75.3	09.3	48.1	92.3	42.2	98.4	61.5	32.2	56
57	22.6	47.9	77.5	11.5	50.5	94.7	44.8	5601.1	64.3	35.1	57
58	24.6	50.0	79.7	13.8	52.8	97.2	47.3	03.8	67.1	38.1	58
59	26.7	52.2	81.9	16.1	55.2	99.7	49.9	06.4	69.9	41.0	59
M.	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°	M.

TABLE 3.

Meridional Parts, or Increased Latitudes.

Comp. $\frac{1}{293.465}$

M.	70°	71°	72°	73°	74°	75°	76°	77°	78°	79°	M.
0	5943.9	6123.5	6312.5	6512.0	6723.2	6947.7	7187.3	7444.4	7721.6	8022.7	0
1	46.8	26.6	15.8	15.4	26.8	51.6	91.5	48.8	26.4	27.9	1
2	49.7	29.7	19.0	18.9	30.5	55.4	95.6	53.3	31.3	33.2	2
3	52.7	32.8	22.3	22.3	34.1	59.3	99.7	57.7	36.1	38.5	3
4	55.6	35.8	25.5	25.7	37.7	63.2	7203.9	62.2	40.9	43.7	4
5	5958.5	6138.9	6328.8	6529.1	6741.4	6967.1	7208.0	7466.7	7745.8	8049.0	5
6	61.5	42.0	32.0	32.6	45.0	70.9	12.2	71.1	50.6	54.3	6
7	64.4	45.1	35.3	36.0	48.7	74.8	16.4	75.6	55.5	59.6	7
8	67.3	48.2	38.5	39.5	52.3	78.7	20.5	80.1	60.3	64.9	8
9	70.3	51.3	41.8	42.9	56.0	82.6	24.7	84.6	65.2	70.2	9
10	5973.2	6154.4	6345.0	6546.4	6759.7	6986.5	7228.9	7489.1	7770.1	8075.5	10
11	76.2	57.5	48.3	49.8	63.3	90.4	33.1	93.6	74.9	80.8	11
12	79.1	60.6	51.6	53.3	67.0	94.3	37.3	98.1	79.8	86.1	12
13	82.1	63.7	54.8	56.7	70.7	98.3	41.5	7502.6	84.7	91.5	13
14	85.0	66.8	58.1	60.2	74.3	7002.2	45.7	07.1	89.6	96.8	14
15	5988.0	6169.9	6361.4	6563.7	6778.0	7006.1	7249.9	7511.7	7794.5	8102.2	15
16	90.9	73.0	64.7	67.1	81.7	10.0	54.1	16.2	99.4	07.5	16
17	93.9	76.1	67.9	70.6	85.4	14.0	58.3	20.7	7804.3	12.9	17
18	96.9	79.2	71.2	74.1	89.1	17.9	62.5	25.3	09.3	18.3	18
19	99.8	82.3	74.5	77.6	92.8	21.8	66.7	29.8	14.2	23.7	19
20	6002.8	6185.5	6377.8	6581.0	6796.5	7025.8	7270.9	7534.4	7819.1	8129.1	20
21	05.8	88.6	81.1	84.5	6800.2	29.7	75.2	38.9	24.1	34.5	21
22	08.7	91.7	84.4	88.0	03.9	33.7	79.4	43.5	29.0	39.9	22
23	11.7	94.8	87.7	91.5	07.6	37.7	83.7	48.1	34.0	45.3	23
24	14.7	98.0	91.0	95.0	11.3	41.6	87.9	52.7	39.0	50.8	24
25	6017.7	6201.1	6394.3	6598.5	6815.0	7045.6	7292.2	7557.3	7844.0	8156.2	25
26	20.7	04.2	97.6	6602.0	18.8	49.6	96.4	61.8	48.9	61.6	26
27	23.6	07.4	6400.9	05.5	22.5	53.5	7300.7	66.4	53.9	67.1	27
28	26.6	10.5	04.3	09.0	26.2	57.5	05.0	71.0	58.9	72.6	28
29	29.6	13.7	07.6	12.5	30.0	61.5	09.2	75.7	63.9	78.0	29
30	6032.6	6216.8	6410.9	6616.1	6833.7	7065.5	7313.5	7580.3	7868.9	8183.5	30
31	35.6	20.0	14.2	19.6	37.4	69.5	17.8	84.9	74.0	89.0	31
32	38.6	23.1	17.6	23.1	41.2	73.5	22.1	89.5	79.0	94.5	32
33	41.6	26.3	20.9	26.6	44.9	77.5	26.4	94.2	84.0	8200.0	33
34	44.6	29.4	24.2	30.2	48.7	81.5	30.7	98.8	89.1	05.5	34
35	6047.6	6232.6	6427.6	6633.7	6852.4	7085.5	7335.0	7603.4	7894.1	8211.1	35
36	50.6	35.8	30.9	37.2	56.2	89.5	39.3	08.1	99.2	16.6	36
37	53.6	38.9	34.2	40.8	60.0	93.5	43.6	12.8	7904.2	22.1	37
38	56.6	42.1	37.6	44.3	63.7	97.6	47.9	17.4	09.3	27.7	38
39	59.7	45.3	40.9	47.9	67.5	7101.6	52.3	22.1	14.4	33.3	39
40	6062.7	6248.4	6444.3	6651.4	6871.3	7105.6	7356.6	7626.8	7919.4	8238.8	40
41	65.7	51.6	47.6	55.0	75.1	09.7	60.9	31.4	24.5	44.4	41
42	68.7	54.8	51.0	58.5	78.9	13.7	65.3	36.1	29.6	50.0	42
43	71.7	58.0	54.4	62.1	82.6	17.8	69.6	40.8	34.7	55.6	43
44	74.8	61.2	57.7	65.7	86.4	21.8	74.0	45.5	39.9	61.2	44
45	6077.8	6264.4	6461.1	6669.2	6890.2	7125.9	7378.3	7650.2	7945.0	8266.8	45
46	80.8	67.6	64.5	72.8	94.0	29.9	82.7	55.0	50.1	72.4	46
47	83.9	70.8	67.8	76.4	97.8	34.0	87.1	59.7	55.2	78.1	47
48	86.9	74.0	71.2	80.0	6901.7	38.1	91.4	64.4	60.4	83.7	48
49	89.9	77.2	74.6	83.5	05.5	42.2	95.8	69.1	65.5	89.3	49
50	6093.0	6280.4	6478.0	6687.1	6909.3	7146.2	7400.2	7673.9	7970.7	8295.0	50
51	96.0	83.6	81.4	90.7	13.1	50.3	04.6	78.6	75.9	8300.7	51
52	99.1	86.8	84.8	94.3	16.9	54.4	09.0	83.4	81.0	06.4	52
53	6102.1	90.0	88.2	97.9	20.8	58.5	13.4	88.1	86.2	12.0	53
54	05.2	93.2	91.6	6701.5	24.6	62.6	17.8	92.9	91.4	17.7	54
55	6108.2	6296.4	6495.0	6705.1	6928.4	7166.7	7422.2	7697.7	7996.6	8323.4	55
56	11.3	99.6	98.4	08.7	32.3	70.8	26.6	7702.5	8001.8	29.2	56
57	14.3	6302.9	6501.8	12.4	36.1	75.0	31.1	07.2	07.0	34.9	57
58	17.4	06.1	05.2	16.0	40.0	79.1	35.5	12.0	12.2	40.6	58
59	20.5	09.3	08.6	19.6	43.8	83.2	39.9	16.8	17.5	46.4	59
M.	70°	71°	72°	73°	74°	75°	76°	77°	78°	79°	M.

6583—06——30

TABLE 4.

Length of a Degree in Latitude and Longitude.

Lat.	Degree of Long.			Degree of Lat.			Lat.
	Naut. miles.	Statute miles.	Meters.	Naut. miles.	Statute miles.	Meters.	
°							°
0	60.068	69.172	111 321	59.661	68.704	110 567	0
1	0.059	9.162	1 304	.661	.704	568	1
2	0.031	9.130	1 253	.662	.705	569	2
3	59.986	9.078	1 169	.663	.706	570	3
4	9.922	9.005	1 051	.664	.708	573	4
5	59.840	68.911	110 900	59.666	68.710	110 576	5
6	9.741	8.795	0 715	.668	.712	580	6
7	9.622	8.660	0 497	.670	.715	584	7
8	9.487	8.504	0 245	.673	.718	589	8
9	9.333	8.326	109 959	.676	.721	595	9
10	59.161	68.129	109 641	59.680	68.725	110 601	10
11	8.971	7.910	9 289	.684	.730	608	11
12	8.764	7.670	8 904	.687	.734	616	12
13	8.538	7.410	8 486	.692	.739	624	13
14	8.295	7.131	8 036	.697	.744	633	14
15	58.034	66.830	107 553	59.702	68.751	110 643	15
16	7.756	6.510	7 036	.707	.757	653	16
17	7.459	6.169	6 487	.713	.764	663	17
18	7.146	5.808	5 906	.719	.771	675	18
19	6.816	5.427	5 294	.725	.778	686	19
20	56.468	65.026	104 649	59.732	68.786	110 699	20
21	6.102	4.606	3 972	.739	.794	712	21
22	5.720	4.166	3 264	.746	.802	725	22
23	5.321	3.706	2 524	.754	.811	739	23
24	4.905	3.228	1 754	.761	.820	753	24
25	54.473	62.729	100 952	59.769	68.829	110 768	25
26	4.024	2.212	0 119	.777	.839	783	26
27	3.558	1.676	99 257	.786	.848	799	27
28	3.076	1.122	8 364	.795	.858	815	28
29	2.578	0.548	7 441	.804	.869	832	29
30	52.064	59.956	96 488	59.813	68.879	110 849	30
31	1.534	9.345	5 506	.822	.890	866	31
32	0.989	8.716	4 495	.831	.901	883	32
33	0.428	8.071	3 455	.841	.912	901	33
34	49.851	7.407	2 387	.851	.923	919	34
35	49.259	56.725	91 290	59.861	68.935	110 938	35
36	8.653	6.027	0 166	.871	.946	956	36
37	8.031	5.311	89 014	.881	.958	975	37
38	7.395	4.579	7 835	.891	.969	994	38
39	6.744	3.829	6 629	.902	.981	111 013	39
40	46.079	53.063	85 396	59.912	68.993	111 033	40
41	5.399	2.281	4 137	.923	69.006	052	41
42	4.706	1.483	2 853	.933	.018	072	42
43	4.000	0.669	1 543	.944	.030	091	43
44	3.280	49.840	0 208	.954	.042	111	44
45	2.546	8.995	78 849	.965	.054	131	45

TABLE 4.

Length of a Degree in Latitude and Longitude.

Lat.	Degree of Long. Naut. miles.	Degree of Long. Statute miles.	Degree of Long. Meters.	Degree of Lat. Naut. miles.	Degree of Lat. Statute miles.	Degree of Lat. Meters.	Lat.
°							°
45	42.546	48.995	78 849	59.965	69.054	111 131	45
46	1.801	8.136	7 466	.976	.066	151	46
47	1.041	7.261	6 058	.987	.079	170	47
48	0.268	6.372	4 628	.997	.091	190	48
49	39.484	5.469	3 174	60.008	.103	210	49
50	38.688	44.552	71 698	60.019	69.115	111 229	50
51	7.880	3.621	0 200	.029	.127	249	51
52	7.060	2.676	68 680	.039	.139	268	52
53	6.229	1.719	7 140	.050	.151	287	53
54	5.386	0.749	5 578	.060	.163	306	54
55	34.532	39.766	63 996	60.070	69.175	111 325	55
56	3.668	8.771	2 395	.080	.086	343	56
57	2.794	7.764	0 774	.090	.197	362	57
58	1.909	6.745	59 135	.100	.209	380	58
59	1.015	5.716	7 478	.109	.220	397	59
60	30.110	34.674	55 802	60.118	69.230	111 415	60
61	29.197	3.623	4 110	.128	.241	432	61
62	8.275	2.560	2 400	.137	.251	448	62
63	7.344	1.488	0 675	.145	.261	464	63
64	6.404	0.406	48 934	.154	.271	480	64
65	25.456	29.315	47 177	60.162	69.281	111 496	65
66	4.501	8.215	5 407	.170	.290	511	66
67	3.538	7.106	3 622	.178	.299	525	67
68	2.567	5.988	1 823	.186	.308	539	68
69	1.590	4.862	0 012	.193	.316	553	69
70	20.606	23.729	38 188	60.200	69.324	111 566	70
71	19.616	2.589	6 353	.207	.332	578	71
72	8.619	1.441	4 506	.213	.340	590	72
73	7.617	0.287	2 648	.220	.347	602	73
74	6.609	19.127	0 781	.225	.354	613	74
75	15.596	17.960	28 903	60.231	69.360	111 623	75
76	4.578	6.788	7 017	.236	.366	633	76
77	3.556	5.611	5 123	.241	.372	642	77
78	2.529	4.428	3 220	.246	.377	650	78
79	1.499	3.242	1 311	.250	.382	658	79
80	10.465	12.051	19 394	60.254	69.386	111 665	80
81	9.428	10.857	7 472	.257	.390	671	81
82	8.388	9.659	5 545	.260	.394	677	82
83	7.345	8.458	3 612	.263	.397	682	83
84	6.300	7.255	1 675	.265	.400	687	84
85	5.253	6.049	9 735	60.268	69.402	111 691	85
86	4.205	4.842	7 792	.269	.404	694	86
87	3.154	3.632	5 846	.270	.405	696	87
88	2.103	2.422	3 898	.271	.407	698	88
89	1.052	1.211	1 949	.272	.407	699	89
90	0	0	0	.272	.407	699	90

TABLE 5A.

Distance of an Object by Two Bearings.

Difference between the course and second bearing, in points.	Difference between the course and first bearing, in points.													
	2		2¼		2½		2¾		3		3¼		3½	
3	1.96	1.09												
3¼	1.57	0.94	2.19	1.31										
3½	1.32	0.84	1.76	1.12	2.42	1.53								
3¾	1.14	0.76	1.47	0.99	1.94	1.30	2.64	1.77						
4	1.00	0.71	1.27	0.90	1.62	1.15	2.12	1.50	2.85	2.01				
4¼	0.90	0.66	1.12	0.83	1.40	1.04	1.77	1.31	2.29	1.69	3.05	2.26		
4½	0.81	0.63	1.00	0.77	1.23	0.95	1.53	1.18	1.91	1.48	2.45	1.90	3.25	2.51
4¾	0.74	0.60	0.91	0.73	1.10	0.89	1.34	1.08	1.65	1.32	2.05	1.65	2.61	2.10
5	0.69	0.57	0.83	0.69	1.00	0.83	1.20	1.00	1.45	1.21	1.77	1.47	2.19	1.82
5¼	0.64	0.55	0.77	0.66	0.92	0.79	1.09	0.94	1.30	1.11	1.56	1.34	1.88	1.62
5½	0.60	0.53	0.72	0.63	0.85	0.75	1.00	0.88	1.18	1.04	1.39	1.23	1.66	1.46
5¾	0.57	0.52	0.68	0.61	0.79	0.72	0.93	0.84	1.08	0.98	1.26	1.14	1.48	1.34
6	0.54	0.50	0.64	0.59	0.74	0.69	0.86	0.80	1.00	0.92	1.16	1.07	1.35	1.24
6¼	0.52	0.49	0.60	0.57	0.70	0.66	0.81	0.76	0.93	0.88	1.07	1.01	1.23	1.16
6½	0.50	0.47	0.58	0.55	0.67	0.64	0.77	0.73	0.88	0.84	1.00	0.96	1.14	1.09
6¾	0.48	0.46	0.55	0.54	0.64	0.62	0.73	0.71	0.83	0.80	0.94	0.91	1.06	1.03
7	0.46	0.45	0.53	0.52	0.61	0.60	0.69	0.68	0.79	0.77	0.89	0.87	1.00	0.98
7¼	0.45	0.44	0.51	0.51	0.59	0.58	0.67	0.66	0.75	0.74	0.84	0.83	0.94	0.93
7½	0.43	0.43	0.50	0.50	0.57	0.56	0.64	0.64	0.72	0.72	0.80	0.80	0.90	0.89
7¾	0.42	0.42	0.48	0.48	0.55	0.55	0.62	0.62	0.69	0.69	0.77	0.77	0.86	0.86
8	0.41	0.41	0.47	0.47	0.53	0.53	0.60	0.60	0.67	0.67	0.74	0.74	0.82	0.82
8¼	0.41	0.41	0.46	0.46	0.52	0.52	0.58	0.58	0.65	0.65	0.72	0.72	0.79	0.79
8½	0.40	0.40	0.45	0.45	0.51	0.51	0.57	0.57	0.63	0.63	0.69	0.69	0.76	0.76
8¾	0.39	0.39	0.45	0.44	0.50	0.50	0.56	0.55	0.61	0.61	0.68	0.67	0.74	0.73
9	0.39	0.38	0.44	0.43	0.49	0.48	0.55	0.54	0.60	0.59	0.66	0.65	0.72	0.71
9¼	0.39	0.38	0.44	0.42	0.49	0.47	0.54	0.52	0.59	0.57	0.64	0.63	0.70	0.68
9½	0.38	0.37	0.43	0.41	0.48	0.46	0.53	0.51	0.58	0.56	0.63	0.61	0.69	0.66
9¾	0.38	0.36	0.43	0.40	0.48	0.45	0.52	0.49	0.57	0.54	0.62	0.59	0.67	0.63
10	0.38	0.35	0.43	0.40	0.47	0.44	0.52	0.48	0.57	0.52	0.61	0.57	0.66	0.61
10¼	0.38	0.35	0.43	0.39	0.47	0.43	0.52	0.47	0.56	0.51	0.61	0.55	0.65	0.59
10½	0.38	0.34	0.43	0.38	0.47	0.42	0.51	0.45	0.56	0.49	0.60	0.53	0.65	0.57
10¾	0.39	0.33	0.43	0.37	0.47	0.40	0.51	0.44	0.56	0.48	0.60	0.51	0.64	0.55
11	0.39	0.32	0.43	0.36	0.47	0.39	0.51	0.43	0.56	0.46	0.60	0.50	0.64	0.53
11¼	0.39	0.31	0.44	0.35	0.48	0.38	0.52	0.41	0.56	0.45	0.60	0.48	0.64	0.51
11½	0.40	0.31	0.44	0.34	0.48	0.37	0.52	0.40	0.56	0.43	0.60	0.46	0.63	0.49
11¾	0.41	0.30	0.45	0.33	0.49	0.36	0.52	0.39	0.56	0.42	0.60	0.44	0.64	0.47
12	0.41	0.29	0.45	0.32	0.49	0.35	0.53	0.37	0.57	0.40	0.60	0.43	0.64	0.45
12¼	0.42	0.28	0.46	0.31	0.50	0.34	0.54	0.36	0.57	0.38	0.61	0.41	0.64	0.42
12½	0.43	0.28	0.47	0.30	0.51	0.32	0.55	0.35	0.58	0.37	0.61	0.39	0.65	0.41
12¾	0.45	0.27	0.48	0.29	0.52	0.31	0.56	0.33	0.59	0.35	0.62	0.37	0.65	0.39
13	0.46	0.26	0.50	0.28	0.53	0.30	0.57	0.32	0.60	0.33	0.63	0.35	0.66	0.37
13¼	0.48	0.24	0.51	0.26	0.55	0.28	0.58	0.30	0.61	0.32	0.64	0.33	0.67	0.35
13½	0.50	0.23	0.53	0.25	0.57	0.27	0.60	0.28	0.63	0.30	0.66	0.31	0.69	0.32
13¾	0.52	0.22	0.55	0.24	0.59	0.25	0.62	0.26	0.65	0.28	0.68	0.29	0.70	0.30
14	0.54	0.21	0.58	0.22	0.61	0.23	0.64	0.24	0.67	0.26	0.69	0.27	0.72	0.28

TABLE 5A.

Distance of an Object by Two Bearings.

Difference between the course and second bearing, in points.	Difference between the course and first bearing, in points.													
	3¾		4		4¼		4½		4¾		5		5¼	
4¾	3.44	2.76												
5	2.76	2.30	3.62	3.01										
5¼	2.31	1.98	2.91	2.50	3.80	3.26								
5½	1.99	1.76	2.44	2.15	3.05	2.69	3.96	3.49						
5¾	1.75	1.59	2.10	1.90	2.55	2.31	3.18	2.88	4.12	3.72				
6	1.57	1.45	1.85	1.71	2.20	2.03	2.66	2.46	3.31	3.05	4.26	3.94		
6¼	1.42	1.34	1.65	1.56	1.94	1.82	2.29	2.16	2.77	2.61	3.42	3.22	4.40	4.14
6½	1.31	1.25	1.50	1.44	1.73	1.66	2.02	1.93	2.38	2.28	2.86	2.74	3.53	3.38
6¾	1.21	1.17	1.38	1.33	1.57	1.52	1.81	1.75	2.10	2.04	2.47	2.39	2.95	2.87
7	1.13	1.11	1.27	1.25	1.44	1.41	1.64	1.61	1.88	1.84	2.17	2.13	2.55	2.50
7¼	1.06	1.05	1.19	1.17	1.33	1.32	1.50	1.49	1.70	1.69	1.94	1.92	2.24	2.22
7½	1.00	1.00	1.11	1.11	1.24	1.24	1.39	1.38	1.56	1.55	1.76	1.76	2.01	2.00
7¾	0.95	0.95	1.05	1.05	1.17	1.17	1.30	1.30	1.45	1.44	1.62	1.62	1.82	1.82
8	0.91	0.91	1.00	1.00	1.10	1.10	1.22	1.22	1.35	1.35	1.50	1.50	1.67	1.67
8¼	0.87	0.87	0.95	0.95	1.05	1.05	1.15	1.15	1.27	1.26	1.40	1.39	1.54	1.54
8½	0.84	0.83	0.91	0.91	1.00	1.00	1.09	1.09	1.20	1.19	1.31	1.30	1.44	1.43
8¾	0.81	0.80	0.88	0.87	0.96	0.95	1.04	1.03	1.14	1.12	1.24	1.22	1.35	1.34
9	0.78	0.77	0.85	0.83	0.92	0.90	1.00	0.98	1.08	1.06	1.18	1.15	1.28	1.25
9¼	0.76	0.74	0.82	0.80	0.89	0.86	0.96	0.93	1.04	1.01	1.12	1.09	1.21	1.18
9½	0.74	0.71	0.80	0.77	0.86	0.83	0.93	0.89	1.00	0.96	1.08	1.03	1.16	1.11
9¾	0.73	0.68	0.78	0.74	0.84	0.79	0.90	0.85	0.97	0.91	1.04	0.97	1.11	1.04
10	0.71	0.66	0.77	0.71	0.82	0.76	0.88	0.81	0.94	0.87	1.00	0.92	1.07	0.99
10¼	0.70	0.63	0.75	0.68	0.80	0.72	0.86	0.77	0.91	0.82	0.97	0.88	1.03	0.93
10½	0.69	0.61	0.74	0.65	0.79	0.69	0.84	0.74	0.89	0.78	0.94	0.83	1.00	0.88
10¾	0.68	0.59	0.73	0.63	0.77	0.66	0.82	0.70	0.87	0.75	0.92	0.79	0.97	0.83
11	0.68	0.56	0.72	0.60	0.76	0.64	0.81	0.67	0.85	0.71	0.90	0.75	0.95	0.79
11¼	0.67	0.54	0.71	0.57	0.76	0.61	0.80	0.64	0.84	0.67	0.88	0.71	0.93	0.75
11½	0.67	0.52	0.71	0.55	0.75	0.58	0.79	0.61	0.83	0.64	0.87	0.67	0.91	0.70
11¾	0.67	0.50	0.71	0.52	0.74	0.55	0.78	0.58	0.82	0.61	0.86	0.64	0.90	0.66
12	0.67	0.48	0.71	0.50	0.74	0.52	0.78	0.55	0.81	0.57	0.85	0.60	0.88	0.63
12¼	0.67	0.45	0.71	0.48	0.74	0.50	0.77	0.52	0.81	0.54	0.84	0.56	0.87	0.59
12½	0.68	0.43	0.71	0.45	0.74	0.47	0.77	0.49	0.80	0.51	0.84	0.53	0.87	0.55
12¾	0.68	0.41	0.71	0.43	0.74	0.44	0.77	0.46	0.80	0.48	0.83	0.50	0.86	0.51
13	0.69	0.38	0.72	0.40	0.75	0.42	0.78	0.43	0.80	0.45	0.83	0.46	0.86	0.48
13¼	0.70	0.36	0.73	0.37	0.76	0.39	0.78	0.40	0.81	0.41	0.83	0.43	0.86	0.44
13½	0.71	0.34	0.74	0.35	0.76	0.36	0.79	0.37	0.81	0.38	0.84	0.39	0.86	0.41
13¾	0.73	0.31	0.75	0.32	0.77	0.33	0.80	0.34	0.82	0.35	0.84	0.36	0.86	0.37
14	0.74	0.28	0.77	0.29	0.79	0.30	0.81	0.31	0.83	0.32	0.85	0.32	0.87	0.33

	5½		5¾		6		6¼		6½		6¾		7	
6½	4.52	4.33												
6¾	3.63	3.52	4.63	4.49										
7	3.04	2.98	3.72	3.65	4.74	4.64								
7¼	2.62	2.59	3.11	3.08	3.80	3.76	4.83	4.77						
7½	2.30	2.29	2.68	2.67	3.18	3.17	3.87	3.86	4.91	4.88				
7¾	2.06	2.06	2.36	2.36	2.74	2.74	3.24	3.24	3.94	3.93	4.97	4.97		
8	1.87	1.87	2.11	2.11	2.41	2.41	2.79	2.79	3.30	3.30	3.99	3.99	5.03	5.03
8¼	1.72	1.71	1.92	1.92	2.16	2.16	2.46	2.46	2.84	2.84	3.34	3.34	4.04	4.03
8½	1.59	1.58	1.76	1.75	1.96	1.95	2.20	2.19	2.50	2.49	2.88	2.87	3.38	3.36
8¾	1.48	1.46	1.63	1.61	1.80	1.78	2.00	1.98	2.24	2.21	2.53	2.51	2.91	2.88
9	1.39	1.36	1.52	1.49	1.66	1.63	1.83	1.80	2.03	1.99	2.27	2.23	2.56	2.51
9¼	1.31	1.27	1.42	1.38	1.55	1.50	1.69	1.64	1.86	1.81	2.06	2.00	2.29	2.23
9½	1.25	1.19	1.35	1.29	1.46	1.39	1.58	1.51	1.72	1.65	1.89	1.81	2.08	1.99
9¾	1.19	1.12	1.28	1.20	1.38	1.30	1.48	1.40	1.61	1.51	1.75	1.64	1.91	1.80
10	1.14	1.05	1.22	1.13	1.31	1.21	1.40	1.30	1.51	1.39	1.62	1.50	1.77	1.63
10¼	1.10	0.99	1.17	1.06	1.25	1.13	1.33	1.20	1.42	1.29	1.53	1.38	1.65	1.49
10½	1.06	0.94	1.13	0.99	1.20	1.05	1.27	1.12	1.35	1.19	1.44	1.27	1.55	1.36
10¾	1.03	0.88	1.09	0.93	1.15	0.99	1.22	1.04	1.29	1.11	1.37	1.18	1.46	1.25
11	1.00	0.83	1.05	0.88	1.11	0.92	1.17	0.97	1.24	1.03	1.31	1.09	1.39	1.15
11¼	0.98	0.78	1.03	0.82	1.08	0.87	1.13	0.91	1.19	0.96	1.25	1.01	1.32	1.06
11½	0.95	0.73	1.00	0.77	1.05	0.81	1.10	0.85	1.15	0.89	1.21	0.93	1.27	0.98
11¾	0.94	0.69	0.98	0.72	1.02	0.76	1.07	0.79	1.12	0.83	1.17	0.86	1.22	0.90
12	0.92	0.65	0.96	0.68	1.00	0.71	1.04	0.73	1.09	0.77	1.13	0.80	1.18	0.83
12¼	0.91	0.61	0.94	0.63	0.98	0.66	1.02	0.68	1.06	0.71	1.10	0.74	1.14	0.77
12½	0.90	0.57	0.93	0.59	0.97	0.61	1.00	0.63	1.04	0.66	1.07	0.68	1.11	0.71
12¾	0.89	0.53	0.92	0.55	0.95	0.57	0.98	0.59	1.02	0.61	1.05	0.63	1.08	0.65
13	0.89	0.49	0.91	0.51	0.94	0.52	0.97	0.54	1.00	0.56	1.03	0.57	1.06	0.59
13¼	0.88	0.45	0.91	0.47	0.93	0.48	0.96	0.49	0.99	0.51	1.01	0.52	1.04	0.54
13½	0.88	0.42	0.91	0.43	0.93	0.44	0.95	0.45	0.98	0.46	1.00	0.47	1.02	0.48
13¾	0.88	0.38	0.90	0.39	0.92	0.40	0.95	0.41	0.97	0.41	0.99	0.42	1.01	0.43
14	0.89	0.34	0.91	0.35	0.92	0.35	0.94	0.36	0.90	0.37	0.98	0.38	1.00	0.38

TABLE 5A.

Distance of an Object by Two Bearings.

Difference between the course and second bearing, in points.	Difference between the course and first bearing, in points.															
	7¼		7½		7¾		8		8¼		8½		8¾		9	
8¼	5.07	5.06														
8½	4.07	4.05	5.10	5.08												
8¾	3.41	3.37	4.10	4.06	5.12	5.06										
9	2.94	2.88	3.43	3.36	4.11	4.03	5.13	5.03								
9¼	2.58	2.51	2.95	2.87	3.44	3.34	4.12	3.39	5.12	4.97						
9½	2.31	2.21	2.60	2.49	2.96	2.84	3.44	3.30	4.11	3.93	5.10	4.88				
9¾	2.10	1.98	2.33	2.19	2.61	2.46	2.97	2.79	3.44	3.24	4.10	3.86	5.07	4.77		
10	1.92	1.78	2.11	1.95	2.34	2.16	2.61	2.41	2.96	2.74	3.43	3.17	4.07	3.76	5.03	4.64
10¼	1.78	1.61	1.93	1.75	2.12	1.92	2.34	2.11	2.61	2.36	2.95	2.67	3.41	3.08	4.04	3.65
10½	1.66	1.46	1.79	1.58	1.94	1.71	2.12	1.87	2.34	2.06	2.60	2.29	2.94	2.59	3.38	2.98
10¾	1.56	1.34	1.67	1.43	1.80	1.54	1.95	1.67	2.12	1.82	2.33	2.00	2.58	2.22	2.91	2.50
11	1.47	1.22	1.57	1.30	1.68	1.39	1.80	1.50	1.94	1.62	2.11	1.76	2.31	1.92	2.56	2.13
11¼	1.40	1.12	1.48	1.19	1.57	1.26	1.68	1.35	1.80	1.44	1.93	1.55	2.10	1.69	2.29	1.84
11½	1.34	1.03	1.41	1.09	1.49	1.15	1.58	1.22	1.68	1.30	1.79	1.38	1.92	1.49	2.08	1.61
11¾	1.28	0.95	1.34	1.00	1.41	1.05	1.49	1.10	1.57	1.17	1.67	1.24	1.78	1.32	1.91	1.41
12	1.23	0.87	1.29	0.91	1.35	0.95	1.41	1.00	1.49	1.05	1.57	1.11	1.66	1.17	1.77	1.25
12¼	1.19	0.80	1.24	0.83	1.29	0.87	1.35	0.91	1.41	0.95	1.48	1.00	1.56	1.05	1.65	1.11
12½	1.15	0.73	1.20	0.76	1.24	0.79	1.29	0.82	1.35	0.86	1.41	0.89	1.47	0.93	1.55	0.98
12¾	1.12	0.67	1.16	0.69	1.20	0.72	1.25	0.74	1.29	0.77	1.34	0.80	1.40	0.83	1.46	0.87
13	1.09	0.61	1.13	0.63	1.16	0.65	1.20	0.67	1.24	0.69	1.29	0.72	1.34	0.74	1.39	0.77
13¼	1.07	0.55	1.10	0.57	1.13	0.58	1.17	0.60	1.20	0.62	1.24	0.64	1.28	0.66	1.32	0.68
13½	1.05	0.50	1.08	0.51	1.10	0.52	1.13	0.53	1.16	0.55	1.20	0.56	1.23	0.58	1.27	0.60
13¾	1.03	0.44	1.06	0.45	1.08	0.46	1.11	0.47	1.13	0.48	1.16	0.50	1.19	0.51	1.22	0.52
14	1.02	0.39	1.04	0.40	1.06	0.41	1.08	0.41	1.10	0.42	1.13	0.43	1.15	0.44	1.18	0.45
	9¼		9½		9¾		10		10¼		10½		10¾		11	
10¼	4.97	4.50														
10½	3.99	3.52	4.91	4.33												
10¾	3.34	2.87	3.94	3.38	4.83	4.14										
11	2.88	2.39	3.30	2.74	3.87	3.22	4.74	3.94								
11¼	2.53	2.04	2.84	2.28	3.24	2.61	3.80	3.05	4.63	3.72						
11½	2.27	1.75	2.50	1.93	2.79	2.16	3.18	2.46	3.72	2.88	4.52	3.49				
11¾	2.06	1.52	2.24	1.66	2.46	1.82	2.74	2.03	3.11	2.31	3.63	2.69	4.40	3.20		
12	1.89	1.33	2.03	1.44	2.20	1.56	2.41	1.71	2.68	1.90	3.04	2.15	3.53	2.50	4.26	3.01
12¼	1.75	1.18	1.86	1.25	2.00	1.34	2.16	1.45	2.36	1.59	2.62	1.76	2.95	1.98	3.42	2.30
12½	1.62	1.03	1.72	1.09	1.83	1.16	1.96	1.24	2.11	1.34	2.30	1.46	2.55	1.62	2.86	1.82
12¾	1.53	0.91	1.61	0.96	1.69	1.01	1.80	1.07	1.92	1.14	2.06	1.23	2.24	1.34	2.47	1.47
13	1.44	0.80	1.51	0.84	1.58	0.88	1.66	0.92	1.76	0.98	1.87	1.04	2.01	1.11	2.17	1.21
13¼	1.37	0.71	1.42	0.73	1.48	0.76	1.55	0.80	1.63	0.84	1.72	0.88	1.82	0.94	1.94	1.00
13½	1.31	0.62	1.35	0.64	1.40	0.66	1.46	0.69	1.52	0.72	1.59	0.75	1.67	0.79	1.76	0.83
13¾	1.25	0.54	1.29	0.55	1.33	0.57	1.38	0.59	1.42	0.61	1.48	0.63	1.54	0.66	1.62	0.69
14	1.21	0.46	1.24	0.47	1.27	0.49	1.31	0.50	1.35	0.52	1.39	0.53	1.44	0.55	1.50	0.57
	11¼		11½		11¾		12		12¼		12½		12¾		13	
12¼	4.12	2.77														
12½	3.31	2.10	3.96	2.51												
12¾	2.77	1.65	3.18	1.90	3.80	2.26										
13	2.38	1.32	2.66	1.48	3.05	1.69	3.62	2.01								
13¼	2.10	1.08	2.29	1.18	2.55	1.31	2.91	1.50	3.44	1.77						
13½	1.88	0.89	2.02	0.95	2.20	1.04	2.44	1.15	2.76	1.30	3.25	1.53				
13¾	1.70	0.73	1.81	0.77	1.94	0.83	2.10	0.90	2.31	0.99	2.61	1.12	3.05	1.31		
14	1.56	0.60	1.64	0.63	1.73	0.66	1.85	0.71	1.99	0.76	2.19	0.84	2.45	0.94	2.85	1.09

TABLE 5B.

Distance of an Object by Two Bearings.

Difference between the course and second bearing.	Difference between the course and first bearing.													
	20°		22°		24°		26°		28°		30°		32°	
30°	1.97	0.98												
32	1.64	0.87	2.16	1.14										
34	1.41	0.79	1.80	1.01	2.34	1.31								
36	1.24	0.73	1.55	0.91	1.96	1.15	2.52	1.48						
38	1.11	0.68	1.36	0.84	1.68	1.04	2.11	1.30	2.70	1.66				
40	1.00	0.64	1.21	0.78	1.48	0.95	1.81	1.16	2.26	1.45	2.88	1.85		
42	0.91	0.61	1.10	0.73	1.32	0.88	1.59	1.06	1.94	1.30	2.40	1.61	3.05	2.04
44	0.84	0.58	1.00	0.69	1.19	0.83	1.42	0.98	1.70	1.18	2.07	1.44	2.55	1.77
46	0.78	0.56	0.92	0.66	1.09	0.78	1.28	0.92	1.52	1.09	1.81	1.30	2.19	1.58
48	0.73	0.54	0.85	0.64	1.00	0.74	1.17	0.87	1.37	1.02	1.62	1.20	1.92	1.43
50	0.68	0.52	0.80	0.61	0.93	0.71	1.08	0.83	1.25	0.96	1.46	1.12	1.71	1.31
52	0.65	0.51	0.75	0.59	0.87	0.68	1.00	0.79	1.15	0.91	1.33	1.05	1.55	1.22
54	0.61	0.49	0.71	0.57	0.81	0.66	0.93	0.76	1.07	0.87	1.23	0.99	1.41	1.14
56	0.58	0.48	0.67	0.56	0.77	0.64	0.88	0.73	1.00	0.83	1.14	0.95	1.30	1.08
58	0.56	0.47	0.64	0.54	0.73	0.62	0.83	0.70	0.94	0.80	1.07	0.90	1.21	1.03
60	0.53	0.46	0.61	0.53	0.69	0.60	0.78	0.68	0.89	0.77	1.00	0.87	1.13	0.98
62	0.51	0.45	0.58	0.51	0.66	0.58	0.75	0.66	0.84	0.74	0.94	0.83	1.06	0.94
64	0.49	0.44	0.56	0.50	0.63	0.57	0.71	0.64	0.80	0.72	0.89	0.80	1.00	0.90
66	0.48	0.43	0.54	0.49	0.61	0.56	0.68	0.62	0.76	0.70	0.85	0.78	0.95	0.87
68	0.46	0.43	0.52	0.48	0.59	0.54	0.66	0.61	0.73	0.68	0.81	0.75	0.90	0.84
70	0.45	0.42	0.50	0.47	0.57	0.53	0.63	0.59	0.70	0.66	0.78	0.73	0.86	0.81
72	0.43	0.41	0.49	0.47	0.55	0.52	0.61	0.58	0.68	0.64	0.75	0.71	0.82	0.78
74	0.42	0.41	0.48	0.46	0.53	0.51	0.59	0.57	0.65	0.63	0.72	0.69	0.79	0.76
76	0.41	0.40	0.46	0.45	0.52	0.50	0.57	0.56	0.63	0.61	0.70	0.67	0.76	0.74
78	0.40	0.39	0.45	0.44	0.50	0.49	0.56	0.54	0.61	0.60	0.67	0.66	0.74	0.72
80	0.39	0.39	0.44	0.44	0.49	0.48	0.54	0.53	0.60	0.59	0.65	0.64	0.71	0.70
82	0.39	0.38	0.43	0.43	0.48	0.47	0.53	0.52	0.58	0.57	0.63	0.63	0.69	0.69
84	0.38	0.38	0.42	0.42	0.47	0.47	0.52	0.51	0.57	0.56	0.62	0.61	0.67	0.67
86	0.37	0.37	0.42	0.42	0.46	0.46	0.51	0.51	0.55	0.55	0.60	0.60	0.66	0.65
88	0.37	0.37	0.41	0.41	0.45	0.45	0.50	0.50	0.54	0.54	0.59	0.59	0.64	0.64
90	0.36	0.36	0.40	0.40	0.45	0.45	0.49	0.49	0.53	0.53	0.58	0.58	0.62	0.62
92	0.36	0.36	0.40	0.40	0.44	0.44	0.48	0.48	0.52	0.52	0.57	0.57	0.61	0.61
94	0.36	0.35	0.39	0.39	0.43	0.43	0.47	0.47	0.51	0.51	0.56	0.55	0.60	0.60
96	0.35	0.35	0.39	0.39	0.43	0.43	0.47	0.46	0.51	0.50	0.55	0.54	0.59	0.59
98	0.35	0.35	0.39	0.38	0.42	0.42	0.46	0.46	0.50	0.50	0.54	0.53	0.58	0.57
100	0.35	0.34	0.38	0.38	0.42	0.41	0.46	0.45	0.49	0.49	0.53	0.52	0.57	0.56
102	0.35	0.34	0.38	0.37	0.42	0.41	0.45	0.44	0.49	0.48	0.53	0.51	0.56	0.55
104	0.34	0.33	0.38	0.37	0.41	0.40	0.45	0.43	0.48	0.47	0.52	0.50	0.56	0.54
106	0.34	0.33	0.38	0.36	0.41	0.39	0.45	0.43	0.48	0.46	0.52	0.50	0.55	0.53
108	0.34	0.32	0.38	0.36	0.41	0.39	0.44	0.42	0.48	0.45	0.51	0.49	0.55	0.52
110	0.34	0.32	0.37	0.35	0.41	0.38	0.44	0.41	0.47	0.44	0.51	0.48	0.54	0.51
112	0.34	0.32	0.37	0.35	0.41	0.38	0.44	0.41	0.47	0.44	0.50	0.47	0.54	0.50
114	0.34	0.31	0.37	0.34	0.41	0.37	0.44	0.40	0.47	0.43	0.50	0.46	0.54	0.49
116	0.34	0.31	0.38	0.34	0.41	0.37	0.44	0.39	0.47	0.42	0.50	0.45	0.53	0.48
118	0.35	0.31	0.38	0.33	0.41	0.36	0.44	0.39	0.47	0.41	0.50	0.44	0.53	0.47
120	0.35	0.30	0.38	0.33	0.41	0.36	0.44	0.38	0.47	0.41	0.50	0.43	0.53	0.46
122	0.35	0.30	0.38	0.32	0.41	0.35	0.44	0.37	0.47	0.40	0.50	0.42	0.53	0.45
124	0.35	0.29	0.38	0.32	0.41	0.34	0.44	0.37	0.47	0.39	0.50	0.42	0.53	0.44
126	0.36	0.29	0.39	0.31	0.42	0.34	0.45	0.36	0.47	0.38	0.50	0.41	0.53	0.43
128	0.36	0.28	0.39	0.31	0.42	0.33	0.45	0.35	0.48	0.38	0.50	0.40	0.53	0.42
130	0.36	0.28	0.39	0.30	0.42	0.32	0.45	0.35	0.48	0.37	0.51	0.39	0.54	0.41
132	0.37	0.27	0.40	0.30	0.43	0.32	0.46	0.34	0.48	0.36	0.51	0.38	0.54	0.40
134	0.37	0.27	0.40	0.29	0.43	0.31	0.46	0.33	0.49	0.35	0.52	0.37	0.54	0.39
136	0.38	0.26	0.41	0.28	0.44	0.30	0.47	0.32	0.49	0.34	0.52	0.36	0.55	0.38
138	0.39	0.26	0.42	0.28	0.45	0.30	0.47	0.32	0.50	0.33	0.53	0.35	0.55	0.37
140	0.39	0.25	0.42	0.27	0.45	0.29	0.48	0.31	0.51	0.33	0.53	0.34	0.56	0.36
142	0.40	0.25	0.43	0.27	0.46	0.28	0.49	0.30	0.51	0.32	0.54	0.33	0.56	0.35
144	0.41	0.24	0.44	0.26	0.47	0.28	0.50	0.29	0.52	0.31	0.55	0.32	0.57	0.34
146	0.42	0.24	0.45	0.25	0.48	0.27	0.51	0.28	0.53	0.30	0.56	0.31	0.58	0.32
148	0.43	0.23	0.46	0.25	0.49	0.26	0.52	0.27	0.54	0.29	0.57	0.30	0.59	0.31
150	0.45	0.22	0.48	0.24	0.50	0.25	0.53	0.26	0.55	0.28	0.58	0.29	0.60	0.30
152	0.46	0.22	0.49	0.23	0.52	0.24	0.54	0.25	0.57	0.27	0.59	0.28	0.61	0.29
154	0.48	0.21	0.50	0.22	0.53	0.23	0.56	0.24	0.58	0.25	0.60	0.26	0.62	0.27
156	0.49	0.20	0.52	0.21	0.55	0.22	0.57	0.23	0.60	0.24	0.62	0.25	0.64	0.26
158	0.51	0.19	0.54	0.20	0.57	0.21	0.59	0.22	0.61	0.23	0.63	0.24	0.66	0.25
160	0.53	0.18	0.56	0.19	0.59	0.20	0.61	0.21	0.63	0.22	0.65	0.22	0.67	0.23

TABLE 5B.

Distance of an Object by Two Bearings.

Difference between the course and second bearing.	Difference between the course and first bearing.													
	34°		36°		38°		40°		42°		44°		46°	
44°	3.22	2.24												
46	2.69	1.93	3.39	2.43										
48	2.31	1.72	2.83	2.10	3.55	2.63								
50	2.03	1.55	2.43	1.86	2.96	2.27	3.70	2.84						
52	1.81	1.43	2.13	1.68	2.54	2.01	3.09	2.44	3.85	3.04				
54	1.63	1.32	1.90	1.54	2.23	1.81	2.66	2.15	3.22	2.60	4.00	3.24		
56	1.49	1.24	1.72	1.42	1.99	1.65	2.33	1.93	2.77	2.29	3.34	2.77	4.14	3.43
58	1.37	1.17	1.57	1.33	1.80	1.53	2.08	1.76	2.43	2.06	2.87	2.44	3.46	2.93
60	1.28	1.10	1.45	1.25	1.64	1.42	1.88	1.63	2.17	1.88	2.52	2.18	2.97	2.57
62	1.19	1.05	1.34	1.18	1.51	1.34	1.72	1.52	1.96	1.73	2.25	1.98	2.61	2.30
64	1.12	1.01	1.25	1.13	1.40	1.26	1.58	1.42	1.79	1.61	2.03	1.83	2.33	2.09
66	1.06	0.96	1.18	1.07	1.31	1.20	1.47	1.34	1.65	1.51	1.85	1.69	2.10	1.92
68	1.00	0.93	1.11	1.03	1.23	1.14	1.37	1.27	1.53	1.42	1.71	1.58	1.92	1.78
70	0.95	0.89	1.05	0.99	1.16	1.09	1.29	1.21	1.43	1.34	1.58	1.49	1.77	1.66
72	0.91	0.86	1.00	0.95	1.10	1.05	1.21	1.15	1.34	1.27	1.48	1.41	1.64	1.56
74	0.87	0.84	0.95	0.92	1.05	1.01	1.15	1.10	1.26	1.21	1.39	1.34	1.53	1.47
76	0.84	0.81	0.91	0.89	1.00	0.97	1.09	1.06	1.20	1.16	1.31	1.27	1.44	1.40
78	0.80	0.79	0.88	0.86	0.96	0.94	1.04	1.02	1.14	1.11	1.24	1.22	1.36	1.33
80	0.78	0.77	0.85	0.83	0.92	0.91	1.00	0.98	1.09	1.07	1.18	1.16	1.28	1.27
82	0.75	0.75	0.82	0.81	0.89	0.88	0.96	0.95	1.04	1.03	1.13	1.12	1.22	1.21
84	0.73	0.73	0.79	0.79	0.86	0.85	0.93	0.92	1.00	0.99	1.08	1.07	1.17	1.16
86	0.71	0.71	0.77	0.77	0.83	0.83	0.89	0.89	0.96	0.96	1.04	1.04	1.12	1.12
88	0.69	0.69	0.75	0.75	0.80	0.80	0.86	0.86	0.93	0.93	1.00	1.00	1.08	1.07
90	0.67	0.67	0.73	0.73	0.78	0.78	0.84	0.84	0.90	0.90	0.97	0.97	1.04	1.04
92	0.66	0.66	0.71	0.71	0.76	0.76	0.82	0.82	0.87	0.87	0.93	0.93	1.00	1.00
94	0.65	0.64	0.69	0.69	0.74	0.74	0.79	0.79	0.85	0.85	0.91	0.90	0.97	0.97
96	0.63	0.63	0.68	0.67	0.73	0.72	0.78	0.77	0.83	0.82	0.88	0.88	0.94	0.93
98	0.62	0.62	0.67	0.66	0.71	0.70	0.76	0.75	0.81	0.80	0.86	0.85	0.91	0.90
100	0.61	0.60	0.65	0.64	0.70	0.69	0.74	0.73	0.79	0.78	0.84	0.83	0.89	0.88
102	0.60	0.59	0.64	0.63	0.68	0.67	0.73	0.71	0.77	0.76	0.82	0.80	0.87	0.85
104	0.60	0.58	0.63	0.61	0.67	0.65	0.72	0.69	0.76	0.74	0.80	0.78	0.85	0.82
106	0.59	0.57	0.63	0.60	0.66	0.64	0.70	0.68	0.74	0.72	0.79	0.76	0.83	0.80
108	0.58	0.55	0.62	0.59	0.66	0.62	0.69	0.66	0.73	0.70	0.77	0.74	0.81	0.77
110	0.58	0.54	0.61	0.57	0.65	0.61	0.68	0.64	0.72	0.68	0.76	0.71	0.80	0.75
112	0.57	0.53	0.61	0.56	0.64	0.59	0.68	0.63	0.71	0.66	0.75	0.69	0.79	0.73
114	0.57	0.52	0.60	0.55	0.63	0.58	0.67	0.61	0.70	0.64	0.74	0.68	0.78	0.71
116	0.56	0.51	0.60	0.54	0.63	0.57	0.66	0.60	0.70	0.63	0.73	0.66	0.77	0.69
118	0.56	0.50	0.59	0.52	0.63	0.55	0.66	0.58	0.69	0.61	0.72	0.64	0.76	0.67
120	0.56	0.49	0.59	0.51	0.62	0.54	0.65	0.57	0.68	0.59	0.72	0.62	0.75	0.65
122	0.56	0.47	0.59	0.50	0.62	0.53	0.65	0.55	0.68	0.58	0.71	0.60	0.74	0.63
124	0.56	0.46	0.59	0.49	0.62	0.51	0.65	0.54	0.68	0.56	0.71	0.58	0.74	0.61
126	0.56	0.45	0.59	0.48	0.62	0.50	0.64	0.52	0.67	0.54	0.70	0.57	0.73	0.59
128	0.56	0.44	0.59	0.46	0.62	0.49	0.64	0.51	0.67	0.53	0.70	0.55	0.73	0.57
130	0.56	0.43	0.59	0.45	0.62	0.47	0.64	0.49	0.67	0.51	0.70	0.53	0.72	0.55
132	0.56	0.42	0.59	0.44	0.62	0.46	0.64	0.48	0.67	0.50	0.70	0.52	0.72	0.54
134	0.57	0.41	0.59	0.43	0.62	0.45	0.64	0.46	0.67	0.48	0.69	0.50	0.72	0.52
136	0.57	0.40	0.60	0.41	0.62	0.43	0.65	0.45	0.67	0.47	0.70	0.48	0.72	0.50
138	0.58	0.39	0.60	0.40	0.63	0.42	0.65	0.43	0.67	0.45	0.70	0.47	0.72	0.48
140	0.58	0.37	0.61	0.39	0.63	0.40	0.65	0.42	0.68	0.43	0.70	0.45	0.72	0.46
142	0.59	0.36	0.61	0.38	0.63	0.39	0.66	0.41	0.68	0.42	0.70	0.43	0.72	0.45
144	0.60	0.35	0.62	0.36	0.64	0.38	0.66	0.39	0.68	0.40	0.71	0.41	0.73	0.43
146	0.60	0.34	0.63	0.35	0.65	0.36	0.67	0.37	0.69	0.39	0.71	0.40	0.73	0.41
148	0.61	0.32	0.63	0.34	0.66	0.35	0.68	0.36	0.70	0.37	0.72	0.38	0.74	0.39
150	0.62	0.31	0.64	0.32	0.66	0.33	0.68	0.34	0.70	0.35	0.72	0.36	0.74	0.37
152	0.63	0.30	0.65	0.31	0.67	0.32	0.69	0.33	0.71	0.33	0.73	0.34	0.75	0.35
154	0.65	0.28	0.67	0.29	0.68	0.30	0.70	0.31	0.72	0.32	0.74	0.32	0.76	0.33
156	0.66	0.27	0.68	0.28	0.70	0.28	0.72	0.29	0.73	0.30	0.75	0.30	0.77	0.31
158	0.67	0.25	0.69	0.26	0.71	0.27	0.73	0.27	0.74	0.28	0.76	0.28	0.78	0.29
160	0.69	0.24	0.71	0.24	0.73	0.25	0.74	0.25	0.76	0.26	0.77	0.26	0.79	0.27

TABLE 5B.

Distance of an Object by Two Bearings.

Difference between the course and second bearing.	Difference between the course and first bearing.													
	48°		50°		52°		54°		56°		58°		60°	
58°	4.28	3.63												
60	3.57	3.10	4.41	3.82										
62	3.07	2.71	3.68	3.25	4.54	4.01								
64	2.70	2.42	3.17	2.85	3.79	3.41	4.66	4.19						
66	2.40	2.20	2.78	2.54	3.26	2.98	3.89	3.55	4.77	4.36				
68	2.17	2.01	2.48	2.30	2.86	2.65	3.34	3.10	3.99	3.71	4.88	4.53		
70	1.98	1.86	2.24	2.10	2.55	2.39	2.94	2.76	3.43	3.22	4.08	3.83	4.99	4.69
72	1.83	1.74	2.04	1.94	2.30	2.19	2.62	2.49	3.01	2.86	3.51	3.33	4.17	3.96
74	1.70	1.63	1.88	1.81	2.10	2.02	2.37	2.27	2.68	2.58	3.08	2.96	3.58	3.44
76	1.58	1.54	1.75	1.70	1.94	1.88	2.16	2.10	2.42	2.35	2.74	2.66	3.14	3.05
78	1.49	1.45	1.63	1.60	1.80	1.76	1.99	1.95	2.21	2.16	2.48	2.43	2.80	2.74
80	1.40	1.38	1.53	1.51	1.68	1.65	1.85	1.82	2.04	2.01	2.26	2.23	2.53	2.49
82	1.33	1.32	1.45	1.43	1.58	1.56	1.72	1.71	1.89	1.87	2.08	2.06	2.31	2.29
84	1.26	1.26	1.37	1.36	1.49	1.48	1.62	1.61	1.77	1.76	1.93	1.92	2.13	2.12
86	1.21	1.20	1.30	1.30	1.41	1.41	1.53	1.52	1.66	1.65	1.81	1.80	1.98	1.97
88	1.16	1.16	1.24	1.24	1.34	1.34	1.45	1.45	1.56	1.56	1.70	1.70	1.84	1.84
90	1.11	1.11	1.19	1.19	1.28	1.28	1.38	1.38	1.48	1.48	1.60	1.60	1.73	1.73
92	1.07	1.07	1.14	1.14	1.23	1.23	1.31	1.31	1.41	1.41	1.52	1.52	1.63	1.63
94	1.03	1.03	1.10	1.10	1.18	1.17	1.26	1.26	1.35	1.34	1.44	1.44	1.55	1.54
96	1.00	0.99	1.06	1.06	1.13	1.13	1.21	1.20	1.29	1.28	1.38	1.37	1.47	1.47
98	0.97	0.96	1.03	1.02	1.10	1.08	1.16	1.15	1.24	1.23	1.32	1.31	1.41	1.39
100	0.94	0.93	1.00	0.98	1.06	1.04	1.12	1.11	1.19	1.18	1.27	1.25	1.35	1.33
102	0.92	0.90	0.97	0.95	1.03	1.01	1.09	1.06	1.15	1.13	1.22	1.19	1.29	1.27
104	0.90	0.87	0.95	0.92	1.00	0.97	1.06	1.02	1.12	1.08	1.18	1.14	1.25	1.21
106	0.88	0.84	0.92	0.89	0.97	0.94	1.03	0.99	1.09	1.04	1.14	1.10	1.20	1.16
108	0.86	0.82	0.90	0.86	0.95	0.90	1.00	0.95	1.05	1.00	1.11	1.05	1.17	1.11
110	0.84	0.79	0.88	0.83	0.93	0.87	0.98	0.92	1.02	0.96	1.08	1.01	1.13	1.06
112	0.83	0.77	0.87	0.80	0.91	0.84	0.95	0.88	1.00	0.93	1.05	0.97	1.10	1.02
114	0.81	0.74	0.85	0.78	0.89	0.82	0.93	0.85	0.98	0.89	1.02	0.93	1.07	0.98
116	0.80	0.72	0.84	0.75	0.88	0.79	0.92	0.82	0.96	0.85	1.00	0.90	1.04	0.94
118	0.79	0.70	0.83	0.73	0.86	0.76	0.90	0.79	0.94	0.83	0.98	0.86	1.02	0.90
120	0.78	0.68	0.82	0.71	0.85	0.74	0.89	0.77	0.91	0.80	0.96	0.83	1.00	0.87
122	0.77	0.66	0.81	0.68	0.84	0.71	0.87	0.74	0.90	0.77	0.95	0.80	0.98	0.83
124	0.77	0.63	0.80	0.66	0.83	0.69	0.86	0.71	0.90	0.74	0.93	0.77	0.96	0.80
126	0.76	0.61	0.79	0.64	0.82	0.66	0.85	0.69	0.88	0.71	0.91	0.74	0.95	0.77
128	0.75	0.59	0.78	0.62	0.81	0.64	0.84	0.66	0.87	0.69	0.90	0.71	0.93	0.74
130	0.75	0.57	0.78	0.60	0.81	0.62	0.83	0.64	0.86	0.66	0.89	0.68	0.92	0.71
132	0.75	0.56	0.77	0.57	0.80	0.59	0.83	0.61	0.85	0.64	0.88	0.66	0.91	0.68
134	0.74	0.54	0.77	0.55	0.80	0.57	0.82	0.59	0.85	0.61	0.87	0.63	0.90	0.65
136	0.74	0.52	0.77	0.53	0.80	0.55	0.82	0.57	0.84	0.58	0.87	0.60	0.89	0.62
138	0.74	0.50	0.77	0.51	0.79	0.53	0.81	0.54	0.84	0.56	0.86	0.58	0.89	0.59
140	0.74	0.48	0.77	0.49	0.79	0.51	0.81	0.52	0.83	0.54	0.86	0.55	0.88	0.57
142	0.74	0.46	0.77	0.47	0.79	0.49	0.81	0.50	0.83	0.51	0.85	0.52	0.87	0.54
144	0.75	0.44	0.77	0.45	0.79	0.46	0.81	0.48	0.83	0.49	0.85	0.50	0.87	0.51
146	0.75	0.42	0.77	0.43	0.79	0.44	0.81	0.45	0.83	0.46	0.85	0.47	0.87	0.49
148	0.76	0.40	0.77	0.41	0.79	0.42	0.81	0.43	0.83	0.44	0.85	0.45	0.87	0.46
150	0.76	0.38	0.78	0.39	0.80	0.40	0.81	0.41	0.83	0.42	0.85	0.42	0.87	0.43
152	0.77	0.36	0.78	0.37	0.80	0.38	0.82	0.38	0.83	0.39	0.85	0.40	0.87	0.41
154	0.77	0.34	0.79	0.35	0.81	0.35	0.82	0.36	0.84	0.37	0.85	0.37	0.87	0.38
156	0.78	0.32	0.80	0.32	0.81	0.33	0.83	0.34	0.84	0.34	0.86	0.35	0.87	0.35
158	0.79	0.30	0.81	0.30	0.82	0.31	0.83	0.31	0.85	0.32	0.86	0.32	0.87	0.33
160	0.80	0.27	0.82	0.28	0.83	0.28	0.84	0.29	0.85	0.29	0.86	0.30	0.88	0.30

TABLE 5B.

Distance of an Object by Two Bearings.

Difference between the course and second bearing.	Difference between the course and first bearing.															
	62°		64°		66°		68°		70°		72°		74°		76°	
72°	5.08	4.84														
74	4.25	4.08	5.18	4.98												
76	3.65	3.54	4.32	4.19	5.26	5.10										
78	3.20	3.13	3.72	3.63	4.39	4.30	5.34	5.22								
80	2.86	2.81	3.26	3.21	3.78	3.72	4.46	4.39	5.41	5.33						
82	2.58	2.56	2.91	2.88	3.31	3.28	3.83	3.80	4.52	4.48	5.48	5.42				
84	2.36	2.34	2.63	2.61	2.96	2.94	3.36	3.35	3.88	3.86	4.57	4.55	5.54	5.51		
86	2.17	2.17	2.40	2.39	2.67	2.66	3.00	2.99	3.41	3.40	3.93	3.92	4.62	4.61	5.59	5.57
88	2.01	2.01	2.21	2.21	2.44	2.44	2.71	2.71	3.04	3.04	3.45	3.45	3.97	3.97	4.67	4.66
90	1.88	1.88	2.05	2.05	2.25	2.25	2.48	2.48	2.75	2.75	3.08	3.08	3.49	3.49	4.01	4.01
92	1.77	1.76	1.91	1.91	2.08	2.08	2.28	2.28	2.51	2.51	2.78	2.78	3.11	3.11	3.52	3.52
94	1.67	1.66	1.80	1.79	1.95	1.94	2.12	2.11	2.31	2.30	2.54	2.53	2.81	2.80	3.14	3.13
96	1.58	1.57	1.70	1.69	1.83	1.82	1.97	1.96	2.14	2.13	2.34	2.33	2.57	2.55	2.84	2.82
98	1.50	1.49	1.61	1.59	1.72	1.71	1.85	1.84	2.00	1.98	2.17	2.15	2.36	2.34	2.59	2.56
100	1.43	1.41	1.53	1.51	1.63	1.61	1.75	1.72	1.88	1.85	2.03	2.00	2.19	2.16	2.39	2.35
102	1.37	1.34	1.46	1.43	1.55	1.52	1.66	1.62	1.77	1.73	1.90	1.86	2.05	2.00	2.21	2.16
104	1.32	1.28	1.40	1.36	1.48	1.44	1.58	1.53	1.68	1.63	1.79	1.74	1.92	1.87	2.07	2.01
106	1.27	1.22	1.34	1.29	1.42	1.37	1.51	1.45	1.60	1.54	1.70	1.63	1.81	1.74	1.94	1.87
108	1.23	1.17	1.29	1.23	1.37	1.30	1.44	1.37	1.53	1.45	1.62	1.54	1.72	1.63	1.83	1.74
110	1.19	1.12	1.25	1.17	1.32	1.24	1.39	1.30	1.46	1.37	1.54	1.45	1.64	1.54	1.74	1.63
112	1.15	1.07	1.21	1.12	1.27	1.18	1.33	1.24	1.40	1.30	1.48	1.37	1.56	1.45	1.65	1.53
114	1.12	1.02	1.17	1.07	1.23	1.12	1.29	1.18	1.35	1.24	1.42	1.30	1.50	1.37	1.58	1.44
116	1.09	0.98	1.14	1.03	1.19	1.07	1.25	1.12	1.31	1.17	1.37	1.23	1.44	1.29	1.51	1.36
118	1.07	0.94	1.11	0.98	1.16	1.02	1.21	1.07	1.26	1.12	1.32	1.17	1.38	1.22	1.45	1.28
120	1.04	0.90	1.08	0.94	1.13	0.98	1.18	1.02	1.23	1.06	1.28	1.11	1.34	1.16	1.40	1.21
122	1.02	0.86	1.06	0.90	1.10	0.93	1.15	0.97	1.19	1.01	1.24	1.05	1.29	1.10	1.35	1.14
124	1.00	0.83	1.04	0.86	1.08	0.89	1.12	0.93	1.16	0.96	1.21	1.00	1.25	1.04	1.31	1.08
126	0.98	0.79	1.02	0.82	1.05	0.85	1.09	0.88	1.13	0.92	1.18	0.95	1.22	0.99	1.27	1.02
128	0.97	0.76	1.00	0.79	1.03	0.82	1.07	0.84	1.11	0.87	1.15	0.90	1.19	0.94	1.23	0.97
130	0.95	0.73	0.98	0.75	1.02	0.78	1.05	0.80	1.09	0.83	1.12	0.86	1.16	0.89	1.20	0.92
132	0.94	0.70	0.97	0.72	1.00	0.74	1.03	0.77	1.06	0.79	1.10	0.82	1.13	0.84	1.17	0.87
134	0.93	0.67	0.96	0.69	0.99	0.71	1.01	0.73	1.04	0.75	1.08	0.77	1.11	0.80	1.14	0.82
136	0.92	0.64	0.95	0.66	0.97	0.68	1.00	0.69	1.03	0.71	1.06	0.74	1.09	0.76	1.12	0.78
138	0.91	0.61	0.94	0.63	0.96	0.64	0.99	0.66	1.01	0.68	1.04	0.70	1.07	0.72	1.10	0.74
140	0.90	0.58	0.93	0.60	0.95	0.61	0.97	0.63	1.00	0.64	1.03	0.66	1.05	0.68	1.08	0.70
142	0.90	0.55	0.92	0.57	0.94	0.58	0.96	0.59	0.99	0.61	1.01	0.62	1.04	0.64	1.06	0.65
144	0.89	0.52	0.91	0.54	0.93	0.55	0.96	0.56	0.98	0.57	1.00	0.59	1.02	0.60	1.05	0.62
146	0.89	0.50	0.91	0.51	0.93	0.52	0.95	0.53	0.97	0.54	0.99	0.55	1.01	0.57	1.03	0.58
148	0.89	0.47	0.90	0.48	0.92	0.49	0.94	0.50	0.96	0.51	0.98	0.52	1.00	0.53	1.02	0.54
150	0.88	0.44	0.90	0.45	0.92	0.46	0.94	0.47	0.95	0.48	0.97	0.49	0.99	0.50	1.01	0.50
152	0.88	0.41	0.90	0.42	0.92	0.43	0.93	0.44	0.95	0.45	0.97	0.45	0.98	0.46	1.00	0.47
154	0.88	0.39	0.90	0.39	0.91	0.40	0.93	0.41	0.94	0.41	0.96	0.42	0.98	0.43	0.99	0.43
156	0.89	0.36	0.90	0.37	0.91	0.37	0.93	0.38	0.94	0.38	0.96	0.39	0.97	0.39	0.99	0.40
158	0.89	0.33	0.90	0.34	0.91	0.34	0.93	0.35	0.94	0.35	0.95	0.36	0.97	0.36	0.98	0.37
160	0.89	0.30	0.90	0.31	0.91	0.31	0.93	0.32	0.94	0.32	0.95	0.33	0.96	0.33	0.98	0.33

TABLE 5B.

Distance of an Object by Two Bearings.

Difference between the course and second bearing.	Difference between the course and first bearing.															
	78°		80°		82°		84°		86°		88°		90°		92°	
88°	5. 63	5. 63														
90	4. 70	4. 70	5. 67	5. 67												
92	4. 04	4. 04	4. 74	4. 73	5. 70	5. 70										
94	3. 55	3. 54	4. 07	4. 06	4. 76	4. 75	5. 73	5. 71								
96	3. 17	3. 15	3. 57	3. 55	4. 09	4. 07	4. 78	4. 76	5. 74	5. 71						
98	2. 86	2. 83	3. 19	3. 16	3. 59	3. 56	4. 11	4. 07	4. 80	4. 75	5. 76	5. 70				
100	2. 61	2. 57	2. 88	2. 84	3. 20	3. 16	3. 61	3. 55	4. 12	4. 06	4. 81	4. 73	5. 76	5. 67		
102	2. 40	2. 35	2. 63	2. 57	2. 90	2. 83	3. 22	3. 15	3. 62	3. 54	4. 13	4. 04	4. 81	4. 70	5. 76	5. 63
104	2. 23	2. 16	2. 42	2. 35	2. 64	2. 56	2. 91	2. 82	3. 23	3. 13	3. 63	3. 52	4. 13	4. 01	4. 81	4. 66
106	2. 08	2. 00	2. 25	2. 16	2. 43	2. 34	2. 65	2. 55	2. 92	2. 80	3. 23	3. 11	3. 63	3. 49	4. 13	3. 97
108	1. 96	1. 86	2. 10	2. 00	2. 26	2. 15	2. 45	2. 33	2. 66	2. 53	2. 92	2. 78	3. 24	3. 08	3. 63	3. 45
110	1. 85	1. 73	1. 97	1. 85	2. 11	1. 98	2. 27	2. 13	2. 45	2. 31	2. 67	2. 51	2. 92	2. 75	3. 23	3. 04
112	1. 75	1. 62	1. 86	1. 72	1. 98	1. 83	2. 12	1. 96	2. 28	2. 11	2. 46	2. 28	2. 67	2. 48	2. 92	2. 71
114	1. 66	1. 52	1. 76	1. 61	1. 87	1. 71	1. 99	1. 82	2. 12	1. 94	2. 28	2. 08	2. 46	2. 25	2. 67	2. 44
116	1. 59	1. 43	1. 68	1. 51	1. 77	1. 59	1. 88	1. 69	2. 00	1. 79	2. 13	1. 91	2. 28	2. 05	2. 46	2. 21
118	1. 52	1. 34	1. 60	1. 41	1. 68	1. 49	1. 78	1. 57	1. 88	1. 66	2. 00	1. 76	2. 13	1. 88	2. 28	2. 01
120	1. 46	1. 27	1. 53	1. 33	1. 61	1. 39	1. 69	1. 47	1. 78	1. 54	1. 89	1. 63	2. 00	1. 73	2. 13	1. 84
122	1. 41	1. 19	1. 47	1. 25	1. 54	1. 31	1. 62	1. 37	1. 70	1. 44	1. 79	1. 52	1. 89	1. 60	2. 00	1. 70
124	1. 36	1. 13	1. 42	1. 18	1. 48	1. 23	1. 55	1. 28	1. 62	1. 34	1. 70	1. 41	1. 79	1. 48	1. 89	1. 56
126	1. 32	1. 06	1. 37	1. 11	1. 43	1. 15	1. 48	1. 20	1. 55	1. 26	1. 62	1. 31	1. 70	1. 38	1. 79	1. 45
128	1. 28	1. 01	1. 33	1. 04	1. 38	1. 08	1. 43	1. 13	1. 49	1. 17	1. 55	1. 23	1. 62	1. 28	1. 70	1. 34
130	1. 24	0. 95	1. 29	0. 98	1. 33	1. 02	1. 38	1. 06	1. 44	1. 10	1. 49	1. 14	1. 56	1. 19	1. 62	1. 24
132	1. 21	0. 90	1. 25	0. 93	1. 29	0. 96	1. 34	0. 99	1. 39	1. 03	1. 44	1. 07	1. 49	1. 11	1. 55	1. 16
134	1. 18	0. 85	1. 22	0. 88	1. 26	0. 90	1. 30	0. 93	1. 34	0. 97	1. 39	1. 00	1. 44	1. 04	1. 49	1. 07
136	1. 15	0. 80	1. 19	0. 83	1. 22	0. 85	1. 26	0. 88	1. 30	0. 90	1. 34	0. 93	1. 39	0. 97	1. 44	1. 00
138	1. 13	0. 76	1. 16	0. 78	1. 19	0. 80	1. 23	0. 82	1. 27	0. 85	1. 30	0. 87	1. 35	0. 90	1. 39	0. 93
140	1. 11	0. 71	1. 14	0. 73	1. 17	0. 75	1. 20	0. 77	1. 23	0. 79	1. 27	0. 82	1. 31	0. 84	1. 34	0. 86
142	1. 09	0. 67	1. 12	0. 69	1. 14	0. 70	1. 17	0. 72	1. 20	0. 74	1. 24	0. 76	1. 27	0. 78	1. 30	0. 80
144	1. 07	0. 63	1. 10	0. 64	1. 12	0. 66	1. 15	0. 67	1. 18	0. 69	1. 21	0. 71	1. 24	0. 73	1. 27	0. 75
146	1. 05	0. 59	1. 08	0. 60	1. 10	0. 62	1. 13	0. 63	1. 15	0. 64	1. 18	0. 66	1. 21	0. 67	1. 24	0. 69
148	1. 04	0. 55	1. 06	0. 56	1. 08	0. 57	1. 11	0. 59	1. 13	0. 60	1. 15	0. 61	1. 18	0. 62	1. 21	0. 64
150	1. 03	0. 51	1. 05	0. 52	1. 07	0. 53	1. 09	0. 54	1. 11	0. 55	1. 13	0. 57	1. 15	0. 58	1. 18	0. 59
152	1. 02	0. 48	1. 04	0. 49	1. 05	0. 49	1. 07	0. 50	1. 09	0. 51	1. 11	0. 52	1. 13	0. 53	1. 15	0. 54
154	1. 01	0. 44	1. 02	0. 45	1. 04	0. 46	1. 06	0. 46	1. 08	0. 47	1. 09	0. 48	1. 11	0. 49	1. 13	0. 50
156	1. 00	0. 41	1. 01	0. 41	1. 03	0. 42	1. 05	0. 43	1. 06	0. 43	1. 08	0. 44	1. 09	0. 45	1. 11	0. 45
158	0. 99	0. 37	1. 01	0. 38	1. 02	0. 38	1. 03	0. 39	1. 05	0. 39	1. 06	0. 40	1. 08	0. 40	1. 09	0. 41
160	0. 99	0. 34	1. 00	0. 34	1. 01	0. 35	1. 02	0. 35	1. 04	0. 35	1. 05	0. 36	1. 06	0. 36	1. 08	0. 37
	94°		96°		98°		100°		102°		104°		106°		108°	
104°	5. 74	5. 57														
106	4. 80	4. 61	5. 78	5. 51												
108	4. 12	3. 92	4. 78	4. 55	5. 70	5. 42										
110	3. 62	3. 40	4. 11	3. 86	4. 76	4. 48	5. 67	5. 33								
112	3. 23	2. 99	3. 61	3. 35	4. 09	3. 80	4. 74	4. 40	5. 63	5. 22						
114	2. 92	2. 66	3. 22	2. 94	3. 59	3. 28	4. 07	3. 72	4. 70	4. 30	5. 59	5. 10				
116	2. 66	2. 39	2. 91	2. 61	3. 20	2. 88	3. 57	3. 21	4. 04	3. 63	4. 67	4. 19	5. 54	4. 98		
118	2. 45	2. 17	2. 65	2. 34	2. 90	2. 56	3. 19	2. 81	3. 55	3. 13	4. 01	3. 54	4. 62	4. 08	5. 48	4. 84
120	2. 28	1. 97	2. 45	2. 12	2. 64	2. 29	2. 88	2. 49	3. 17	2. 74	3. 52	3. 05	3. 97	3. 44	4. 57	3. 96
122	2. 12	1. 80	2. 27	1. 92	2. 43	2. 06	2. 63	2. 23	2. 86	2. 43	3. 14	2. 66	3. 49	2. 96	3. 93	3. 33
124	2. 00	1. 65	2. 12	1. 76	2. 26	1. 87	2. 42	2. 01	2. 61	2. 16	2. 84	2. 35	3. 11	2. 58	3. 45	2. 86
126	1. 88	1. 52	1. 99	1. 61	2. 11	1. 71	2. 25	1. 82	2. 40	1. 95	2. 59	2. 10	2. 81	2. 27	3. 08	2. 49
128	1. 78	1. 41	1. 88	1. 48	1. 98	1. 56	2. 10	1. 65	2. 23	1. 76	2. 39	1. 88	2. 57	2. 02	2. 78	2. 19
130	1. 70	1. 30	1. 78	1. 36	1. 87	1. 43	1. 97	1. 51	2. 08	1. 60	2. 21	1. 70	2. 36	1. 81	2. 54	1. 94
132	1. 62	1. 20	1. 69	1. 26	1. 77	1. 32	1. 86	1. 38	1. 96	1. 45	2. 07	1. 54	2. 19	1. 63	2. 34	1. 74
134	1. 55	1. 12	1. 62	1. 16	1. 68	1. 21	1. 76	1. 27	1. 85	1. 33	1. 94	1. 40	2. 05	1. 47	2. 17	1. 56
136	1. 49	1. 04	1. 55	1. 07	1. 61	1. 12	1. 68	1. 16	1. 75	1. 22	1. 83	1. 27	1. 92	1. 34	2. 03	1. 41
138	1. 44	0. 96	1. 49	0. 99	1. 54	1. 03	1. 60	1. 07	1. 66	1. 11	1. 74	1. 16	1. 81	1. 21	1. 90	1. 27
140	1. 39	0. 89	1. 43	0. 92	1. 48	0. 95	1. 53	0. 98	1. 59	1. 02	1. 65	1. 06	1. 72	1. 10	1. 79	1. 15
142	1. 34	0. 83	1. 38	0. 85	1. 43	0. 88	1. 47	0. 91	1. 52	0. 94	1. 58	0. 97	1. 64	1. 01	1. 70	1. 05
144	1. 30	0. 77	1. 34	0. 79	1. 38	0. 81	1. 42	0. 83	1. 46	0. 86	1. 51	0. 89	1. 56	0. 92	1. 62	0. 95
146	1. 27	0. 71	1. 30	0. 73	1. 33	0. 75	1. 37	0. 77	1. 41	0. 79	1. 45	0. 81	1. 50	0. 84	1. 54	0. 86
148	1. 23	0. 65	1. 26	0. 67	1. 29	0. 69	1. 33	0. 70	1. 36	0. 72	1. 40	0. 74	1. 44	0. 76	1. 48	0. 78
150	1. 20	0. 60	1. 23	0. 61	1. 26	0. 63	1. 29	0. 64	1. 32	0. 66	1. 35	0. 67	1. 38	0. 69	1. 42	0. 71
152	1. 18	0. 55	1. 20	0. 56	1. 22	0. 57	1. 25	0. 59	1. 28	0. 60	1. 31	0. 61	1. 34	0. 63	1. 37	0. 64
154	1. 15	0. 50	1. 17	0. 51	1. 19	0. 52	1. 22	0. 53	1. 24	0. 54	1. 27	0. 56	1. 29	0. 57	1. 32	0. 58
156	1. 13	0. 46	1. 15	0. 47	1. 17	0. 47	1. 19	0. 48	1. 21	0. 49	1. 23	0. 50	1. 25	0. 51	1. 28	0. 52
158	1. 11	0. 42	1. 13	0. 42	1. 14	0. 43	1. 16	0. 44	1. 18	0. 44	1. 20	0. 45	1. 22	0. 46	1. 24	0. 47
160	1. 09	0. 37	1. 11	0. 38	1. 12	0. 38	1. 14	0. 39	1. 15	0. 39	1. 17	0. 40	1. 19	0. 41	1. 21	0. 41

TABLE 5B.

Distance of an Object by Two Bearings.

Difference between the course and second bearing.	Difference between the course and first bearing.													
	110°		112°		114°		116°		118°		120°		122°	
120°	5.41	4.69												
122	4.52	3.83	5.34	4.53										
124	3.88	3.22	4.46	3.70	5.26	4.36								
126	3.41	2.76	3.83	3.10	4.39	3.55	5.18	4.19						
128	3.04	2.40	3.36	2.65	3.78	2.98	4.32	3.41	5.08	4.01				
130	2.75	2.10	3.00	2.30	3.31	2.54	3.72	2.85	4.25	3.25	4.99	3.82		
132	2.51	1.86	2.71	2.01	2.96	2.20	3.26	2.42	3.65	2.71	4.17	3.10	4.88	3.63
134	2.31	1.66	2.48	1.78	2.67	1.92	2.91	2.09	3.20	2.30	3.58	2.57	4.08	2.93
136	2.14	1.49	2.28	1.58	2.44	1.69	2.63	1.83	2.86	1.98	3.14	2.18	3.51	2.44
138	2.00	1.34	2.12	1.42	2.25	1.50	2.40	1.61	2.58	1.73	2.80	1.88	3.08	2.06
140	1.88	1.21	1.97	1.27	2.08	1.34	2.21	1.42	2.36	1.52	2.53	1.63	2.74	1.76
142	1.77	1.09	1.85	1.14	1.95	1.20	2.05	1.26	2.17	1.34	2.31	1.42	2.48	1.53
144	1.68	0.99	1.75	1.03	1.83	1.07	1.91	1.13	2.01	1.18	2.13	1.25	2.26	1.33
146	1.60	0.89	1.66	0.93	1.72	0.96	1.80	1.01	1.88	1.05	1.98	1.10	2.08	1.17
148	1.53	0.81	1.58	0.84	1.63	0.87	1.70	0.90	1.77	0.94	1.84	0.98	1.93	1.03
150	1.46	0.73	1.51	0.75	1.55	0.78	1.61	0.80	1.67	0.83	1.73	0.87	1.81	0.90
152	1.40	0.66	1.44	0.68	1.48	0.70	1.53	0.72	1.58	0.74	1.63	0.77	1.70	0.80
154	1.35	0.59	1.39	0.61	1.42	0.62	1.46	0.64	1.50	0.66	1.55	0.68	1.60	0.70
156	1.31	0.53	1.33	0.54	1.37	0.56	1.40	0.57	1.43	0.58	1.47	0.60	1.52	0.62
158	1.26	0.47	1.29	0.48	1.32	0.49	1.34	0.50	1.37	0.51	1.41	0.53	1.44	0.54
160	1.23	0.42	1.25	0.43	1.27	0.43	1.29	0.44	1.32	0.45	1.35	0.46	1.38	0.47

	124°		126°		128°		130°		132°		134°		136°	
134°	4.77	3.43												
136	3.99	2.77	4.66	3.23										
138	3.43	2.29	3.89	2.60	4.54	3.04								
140	3.01	1.93	3.34	2.15	3.79	2.44	4.41	2.84						
142	2.68	1.65	2.94	1.81	3.26	2.01	3.66	2.27	4.28	2.63				
144	2.42	1.42	2.62	1.54	2.86	1.68	3.17	1.86	3.57	2.10	4.14	2.43		
146	2.21	1.24	2.37	1.32	2.55	1.43	2.78	1.55	3.07	1.72	3.46	1.93	4.00	2.24
148	2.04	1.08	2.16	1.14	2.30	1.22	2.48	1.31	2.70	1.43	2.97	1.58	3.34	1.77
150	1.89	0.95	1.99	0.99	2.10	1.05	2.24	1.12	2.40	1.20	2.61	1.30	2.87	1.44
152	1.77	0.83	1.85	0.87	1.94	0.91	2.04	0.96	2.17	1.02	2.33	1.09	2.52	1.18
154	1.66	0.73	1.72	0.76	1.80	0.79	1.88	0.83	1.98	0.87	2.10	0.92	2.25	0.99
156	1.56	0.64	1.62	0.66	1.68	0.68	1.75	0.71	1.83	0.74	1.92	0.78	2.03	0.83
158	1.48	0.56	1.53	0.57	1.58	0.59	1.63	0.61	1.70	0.64	1.77	0.66	1.85	0.69
160	1.41	0.48	1.45	0.49	1.49	0.51	1.53	0.52	1.58	0.54	1.64	0.56	1.71	0.58

	138°		140°		142°		144°		146°		148°		150°	
148°	3.85	2.04												
150	3.22	1.61	3.70	1.85										
152	2.77	1.30	3.09	1.45	3.55	1.66								
154	2.43	1.06	2.66	1.16	2.96	1.30	3.38	1.48						
156	2.17	0.88	2.33	0.95	2.54	1.04	2.83	1.15	3.22	1.31				
158	1.96	0.73	2.08	0.78	2.23	0.84	2.43	0.91	2.69	1.01	3.05	1.14		
160	1.79	0.61	1.88	0.64	1.99	0.68	2.13	0.73	2.31	0.79	2.55	0.87	2.88	0.98

TABLE 6.

Distance of Visibility of Objects at Sea.

Height, feet.	Nautical miles.	Statute miles.	Height, feet.	Nautical miles.	Statute miles.	Height, feet.	Nautical miles.	Statute miles.
1	1.1	1.3	100	11.5	13.2	760	31.6	36.4
2	1.7	1.9	105	11.7	13.5	780	32.0	36.9
3	2.0	2.3	110	12.0	13.8	800	32.4	37.3
4	2.3	2.6	115	12.3	14.1	820	32.8	37.8
5	2.5	2.9	120	12.6	14.5	840	33.2	38.3
6	2.8	3.2	125	12.9	14.8	860	33.6	38.7
7	2.9	3.5	130	13.1	15.1	880	34.0	39.2
8	3.1	3.7	135	13.3	15.3	900	34.4	39.6
9	3.5	4.0	140	13.6	15.6	920	34.7	40.0
10	3.6	4.2	145	13.8	15.9	940	35.2	40.5
11	3.8	4.4	150	14.1	16.2	960	35.5	40.9
12	4.0	4.6	160	14.5	16.7	980	35.9	41.3
13	4.2	4.8	170	14.9	17.2	1,000	36.2	41.7
14	4.3	4.9	180	15.4	17.7	1,100	38.0	43.8
15	4.4	5.1	190	15.8	18.2	1,200	39.6	45.6
16	4.6	5.3	200	16.2	18.7	1,300	41.3	47.6
17	4.7	5.4	210	16.6	19.1	1,400	42.9	49.4
18	4.9	5.6	220	17.0	19.6	1,500	44.4	51.1
19	5.0	5.8	230	17.4	20.0	1,600	45.8	52.8
20	5.1	5.9	240	17.7	20.4	1,700	47.2	54.4
21	5.3	6.1	250	18.2	20.9	1,800	48.6	56.0
22	5.4	6.2	260	18.5	21.3	1,900	49.9	57.5
23	5.5	6.3	270	18.9	21.7	2,000	51.2	59.0
24	5.6	6.5	280	19.2	22.1	2,100	52.5	60.5
25	5.7	6.6	290	19.6	22.5	2,200	53.8	61.9
26	5.8	6.7	300	19.9	22.9	2,300	55.0	63.3
27	6.0	6.9	310	20.1	23.2	2,400	56.2	64.7
28	6.1	7.0	320	20.5	23.6	2,500	57.3	66.0
29	6.2	7.1	330	20.8	24.0	2,600	58.5	67.3
30	6.3	7.2	340	21.1	24.3	2,700	59.6	68.6
31	6.4	7.3	350	21.5	24.7	2,800	60.6	69.8
32	6.5	7.5	360	21.7	25.0	2,900	61.8	71.1
33	6.6	7.6	370	22.1	25.4	3,000	62.8	72.3
34	6.7	7.7	380	22.3	25.7	3,100	63.8	73.5
35	6.8	7.8	390	22.7	26.1	3,200	64.9	74.7
36	6.9	7.9	400	22.9	26.4	3,300	65.9	75.9
37	6.9	8.0	410	23.2	26.7	3,400	66.9	77.0
38	7.0	8.1	420	23.5	27.1	3,500	67.8	78.1
39	7.1	8.2	430	23.8	27.4	3,600	68.8	79.2
40	7.2	8.3	440	24.1	27.7	3,700	69.7	80.3
41	7.3	8.4	450	24.3	28.0	3,800	70.7	81.4
42	7.4	8.5	460	24.6	28.3	3,900	71.6	82.4
43	7.5	8.7	470	24.8	28.6	4,000	72.5	83.5
44	7.6	8.8	480	25.1	28.9	4,100	73.4	84.5
45	7.7	8.9	490	25.4	29.2	4,200	74.3	85.6
46	7.8	9.0	500	25.6	29.5	4,300	75.2	86.6
47	7.9	9.0	520	26.1	30.1	4,400	76.1	87.6
48	7.9	9.1	540	26.7	30.7	4,500	76.9	88.5
49	8.0	9.2	560	27.1	31.2	4,600	77.7	89.5
50	8.1	9.3	580	27.6	31.8	4,700	78.6	90.5
55	8.5	9.8	600	28.0	32.3	4,800	79.4	91.4
60	8.9	10.2	620	28.6	32.9	4,900	80.2	92.4
65	9.2	10.6	640	29.0	33.4	5,000	81.0	93.3
70	9.6	11.0	660	29.4	33.9	6,000	88.8	102.2
75	9.9	11.4	680	29.9	34.4	7,000	96.0	110.5
80	10.3	11.8	700	30.3	34.9	8,000	102.6	118.1
85	10.6	12.2	720	30.7	35.4	9,000	108.7	125.2
90	10.9	12.5	740	31.1	35.9	10,000	114.6	132.0
95	11.2	12.9						

TABLE 7.

For converting Arc into Time, and the reverse.

°	H. M.	°	H. M.	°	H. M.	°	H. M.	°	H. M.	°	H. M.
′	M. S.	′	M. S.	′	M. S.	′	M. S.	′	M. S.	′	M. S.
″	S. $\frac{1}{60}$	″	S. $\frac{1}{60}$	″	S. $\frac{1}{60}$	″	S. $\frac{1}{60}$	″	S. $\frac{1}{60}$	″	S. $\frac{1}{60}$
1	0 4	61	4 4	121	8 4	181	12 4	241	16 4	301	20 4
2	0 8	62	4 8	122	8 8	182	12 8	242	16 8	302	20 8
3	0 12	63	4 12	123	8 12	183	12 12	243	16 12	303	20 12
4	0 16	64	4 16	124	8 16	184	12 16	244	16 16	304	20 16
5	0 20	65	4 20	125	8 20	185	12 20	245	16 20	305	20 20
6	0 24	66	4 24	126	8 24	186	12 24	246	16 24	306	20 24
7	0 28	67	4 28	127	8 28	187	12 28	247	16 28	307	20 28
8	0 32	68	4 32	128	8 32	188	12 32	248	16 32	308	20 32
9	0 36	69	4 36	129	8 36	189	12 36	249	16 36	309	20 36
10	0 40	70	4 40	130	8 40	190	12 40	250	16 40	310	20 40
11	0 44	71	4 44	131	8 44	191	12 44	251	16 44	311	20 44
12	0 48	72	4 48	132	8 48	192	12 48	252	16 48	312	20 48
13	0 52	73	4 52	133	8 52	193	12 52	253	16 52	313	20 52
14	0 56	74	4 56	134	8 56	194	12 56	254	16 56	314	20 56
15	1 0	75	5 0	135	9 0	195	13 0	255	17 0	315	21 0
16	1 4	76	5 4	136	9 4	196	13 4	256	17 4	316	21 4
17	1 8	77	5 8	137	9 8	197	13 8	257	17 8	317	21 8
18	1 12	78	5 12	138	9 12	198	13 12	258	17 12	318	21 12
19	1 16	79	5 16	139	9 16	199	13 16	259	17 16	319	21 16
20	1 20	80	5 20	140	9 20	200	13 20	260	17 20	320	21 20
21	1 24	81	5 24	141	9 24	201	13 24	261	17 24	321	21 24
22	1 28	82	5 28	142	9 28	202	13 28	262	17 28	322	21 28
23	1 32	83	5 32	143	9 32	203	13 32	263	17 32	323	21 32
24	1 36	84	5 36	144	9 36	204	13 36	264	17 36	324	21 36
25	1 40	85	5 40	145	9 40	205	13 40	265	17 40	325	21 40
26	1 44	86	5 44	146	9 44	206	13 44	266	17 44	326	21 44
27	1 48	87	5 48	147	9 48	207	13 48	267	17 48	327	21 48
28	1 52	88	5 52	148	9 52	208	13 52	268	17 52	328	21 52
29	1 56	89	5 56	149	9 56	209	13 56	269	17 56	329	21 56
30	2 0	90	6 0	150	10 0	210	14 0	270	18 0	330	22 0
31	2 4	91	6 4	151	10 4	211	14 4	271	18 4	331	22 4
32	2 8	92	6 8	152	10 8	212	14 8	272	18 8	332	22 8
33	2 12	93	6 12	153	10 12	213	14 12	273	18 12	333	22 12
34	2 16	94	6 16	154	10 16	214	14 16	274	18 16	334	22 16
35	2 20	95	6 20	155	10 20	215	14 20	275	18 20	335	22 20
36	2 24	96	6 24	156	10 24	216	14 24	276	18 24	336	22 24
37	2 28	97	6 28	157	10 28	217	14 28	277	18 28	337	22 28
38	2 32	98	6 32	158	10 32	218	14 32	278	18 32	338	22 32
39	2 36	99	6 36	159	10 36	219	14 36	279	18 36	339	22 36
40	2 40	100	6 40	160	10 40	220	14 40	280	18 40	340	22 40
41	2 44	101	6 44	161	10 44	221	14 44	281	18 44	341	22 44
42	2 48	102	6 48	162	10 48	222	14 48	282	18 48	342	22 48
43	2 52	103	6 52	163	10 52	223	14 52	283	18 52	343	22 52
44	2 56	104	6 56	164	10 56	224	14 56	284	18 56	344	22 56
45	3 0	105	7 0	165	11 0	225	15 0	285	19 0	345	23 0
46	3 4	106	7 4	166	11 4	226	15 4	286	19 4	346	23 4
47	3 8	107	7 8	167	11 8	227	15 8	287	19 8	347	23 8
48	3 12	108	7 12	168	11 12	228	15 12	288	19 12	348	23 12
49	3 16	109	7 16	169	11 16	229	15 16	289	19 16	349	23 16
50	3 20	110	7 20	170	11 20	230	15 20	290	19 20	350	23 20
51	3 24	111	7 24	171	11 24	231	15 24	291	19 24	351	23 24
52	3 28	112	7 28	172	11 28	232	15 28	292	19 28	352	23 28
53	3 32	113	7 32	173	11 32	233	15 32	293	19 32	353	23 32
54	3 36	114	7 36	174	11 36	234	15 36	294	19 36	354	23 36
55	3 40	115	7 40	175	11 40	235	15 40	295	19 40	355	23 40
56	3 44	116	7 44	176	11 44	236	15 44	296	19 44	356	23 44
57	3 48	117	7 48	177	11 48	237	15 48	297	19 48	357	23 48
58	3 52	118	7 52	178	11 52	238	15 52	298	19 52	358	23 52
59	3 56	119	7 56	179	11 56	239	15 56	299	19 56	359	23 56
60	4 0	120	8 0	180	12 0	240	16 0	300	20 0	360	24 0

NOTE.—When turning seconds of arc into time, and vice versa, it should be remembered that the fractions are sixtieths; thus, the value in time of 42″ is not $2^s.48$, but $2^s\frac{48}{60}=2^s.8$.

TABLE 8.

Sidereal into Mean Solar Time.

To be subtracted from a sidereal time interval.

Sidereal.	0^h	1^h	2^h	3^h	4^h	5^h	6^h	7^h	For seconds.	
m.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	s.	s.
0	0 0.000	0 9.830	0 19.659	0 29.489	0 39.318	0 49.148	0 58.977	1 8.807		
1	0 0.164	0 9.993	0 19.823	0 29.653	0 39.482	0 49.312	0 59.141	1 8.971	1	0.003
2	0 0.328	0 10.157	0 19.987	0 29.816	0 39.646	0 49.475	0 59.305	1 9.135	2	.005
3	0 0.491	0 10.321	0 20.151	0 29.980	0 39.810	0 49.639	0 59.469	1 9.298	3	.008
4	0 0.655	0 10.485	0 20.314	0 30.144	0 39.974	0 49.803	0 59.633	1 9.462	4	.011
5	0 0.819	0 10.649	0 20.478	0 30.308	0 40.137	0 49.967	0 59.796	1 9.626	5	.014
6	0 0.983	0 10.813	0 20.642	0 30.472	0 40.301	0 50.131	0 59.960	1 9.790	6	.016
7	0 1.147	0 10.976	0 20.806	0 30.635	0 40.465	0 50.295	1 0.124	1 9.954	7	.019
8	0 1.311	0 11.140	0 20.970	0 30.799	0 40.629	0 50.458	1 0.288	1 10.118	8	.022
9	0 1.474	0 11.304	0 21.134	0 30.963	0 40.793	0 50.622	1 0.452	1 10.281	9	.025
10	0 1.638	0 11.468	0 21.297	0 31.127	0 40.956	0 50.786	1 0.616	1 10.445	10	.027
11	0 1.802	0 11.632	0 21.461	0 31.291	0 41.120	0 50.950	1 0.779	1 10.609	11	.030
12	0 1.966	0 11.795	0 21.625	0 31.455	0 41.284	0 51.114	1 0.943	1 10.773	12	.033
13	0 2.130	0 11.959	0 21.789	0 31.618	0 41.448	0 51.278	1 1.107	1 10.937	13	.035
14	0 2.294	0 12.123	0 21.953	0 31.782	0 41.612	0 51.441	1 1.271	1 11.100	14	.038
15	0 2.457	0 12.287	0 22.117	0 31.946	0 41.776	0 51.605	1 1.435	1 11.264	15	.041
16	0 2.621	0 12.451	0 22.280	0 32.110	0 41.939	0 51.769	1 1.599	1 11.428	16	.044
17	0 2.785	0 12.615	0 22.444	0 32.274	0 42.103	0 51.933	1 1.762	1 11.592	17	.046
18	0 2.949	0 12.778	0 22.608	0 32.438	0 42.267	0 52.097	1 1.926	1 11.756	18	.049
19	0 3.113	0 12.942	0 22.772	0 32.601	0 42.431	0 52.260	1 2.090	1 11.920	19	.052
20	0 3.277	0 13.106	0 22.936	0 32.765	0 42.595	0 52.424	1 2.254	1 12.083	20	.055
21	0 3.440	0 13.270	0 23.099	0 32.929	0 42.759	0 52.588	1 2.418	1 12.247	21	.057
22	0 3.604	0 13.434	0 23.263	0 33.093	0 42.922	0 52.752	1 2.582	1 12.411	22	.060
23	0 3.768	0 13.598	0 23.427	0 33.257	0 43.086	0 52.916	1 2.745	1 12.575	23	.063
24	0 3.932	0 13.761	0 23.591	0 33.420	0 43.250	0 53.080	1 2.909	1 12.739	24	.066
25	0 4.096	0 13.925	0 23.755	0 33.584	0 43.414	0 53.243	1 3.073	1 12.903	25	.068
26	0 4.259	0 14.089	0 23.919	0 33.748	0 43.578	0 53.407	1 3.237	1 13.066	26	.071
27	0 4.423	0 14.253	0 24.082	0 33.912	0 43.742	0 53.571	1 3.401	1 13.230	27	.074
28	0 4.587	0 14.417	0 24.246	0 34.076	0 43.905	0 53.735	1 3.564	1 13.394	28	.076
29	0 4.751	0 14.581	0 24.410	0 34.240	0 44.069	0 53.899	1 3.728	1 13.558	29	.079
30	0 4.915	0 14.744	0 24.574	0 34.403	0 44.233	0 54.063	1 3.892	1 13.722	30	.082
31	0 5.079	0 14.908	0 24.738	0 34.567	0 44.397	0 54.226	1 4.056	1 13.886	31	.085
32	0 5.242	0 15.072	0 24.902	0 34.731	0 44.561	0 54.390	1 4.220	1 14.049	32	.087
33	0 5.406	0 15.236	0 25.065	0 34.895	0 44.724	0 54.554	1 4.384	1 14.213	33	.090
34	0 5.570	0 15.400	0 25.229	0 35.059	0 44.888	0 54.718	1 4.547	1 14.377	34	.093
35	0 5.734	0 15.563	0 25.393	0 35.223	0 45.052	0 54.882	1 4.711	1 14.541	35	.096
36	0 5.898	0 15.727	0 25.557	0 35.386	0 45.216	0 55.046	1 4.875	1 14.705	36	.098
37	0 6.062	0 15.891	0 25.721	0 35.550	0 45.380	0 55.209	1 5.039	1 14.868	37	.101
38	0 6.225	0 16.055	0 25.885	0 35.714	0 45.544	0 55.373	1 5.203	1 15.032	38	.104
39	0 6.389	0 16.219	0 26.048	0 35.878	0 45.707	0 55.537	1 5.367	1 15.196	39	.106
40	0 6.553	0 16.383	0 26.212	0 36.042	0 45.871	0 55.701	1 5.530	1 15.360	40	.109
41	0 6.717	0 16.546	0 26.376	0 36.206	0 46.035	0 55.865	1 5.694	1 15.524	41	.112
42	0 6.881	0 16.710	0 26.540	0 36.369	0 46.199	0 56.028	1 5.858	1 15.688	42	.115
43	0 7.045	0 16.874	0 26.704	0 36.533	0 46.363	0 56.192	1 6.022	1 15.851	43	.117
44	0 7.208	0 17.038	0 26.867	0 36.697	0 46.527	0 56.356	1 6.186	1 16.015	44	.120
45	0 7.372	0 17.202	0 27.031	0 36.861	0 46.690	0 56.520	1 6.350	1 16.179	45	.123
46	0 7.536	0 17.366	0 27.195	0 37.025	0 46.854	0 56.684	1 6.513	1 16.343	46	.126
47	0 7.700	0 17.529	0 27.359	0 37.188	0 47.018	0 56.848	1 6.677	1 16.507	47	.128
48	0 7.864	0 17.693	0 27.523	0 37.352	0 47.182	0 57.011	1 6.841	1 16.671	48	.131
49	0 8.027	0 17.857	0 27.687	0 37.516	0 47.346	0 57.175	1 7.005	1 16.834	49	.134
50	0 8.191	0 18.021	0 27.850	0 37.680	0 47.510	0 57.339	1 7.169	1 16.998	50	.137
51	0 8.355	0 18.185	0 28.014	0 37.844	0 47.673	0 57.503	1 7.332	1 17.162	51	.139
52	0 8.519	0 18.349	0 28.178	0 38.008	0 47.837	0 57.667	1 7.496	1 17.326	52	.142
53	0 8.683	0 18.512	0 28.342	0 38.171	0 48.001	0 57.831	1 7.660	1 17.490	53	.145
54	0 8.847	0 18.676	0 28.506	0 38.335	0 48.165	0 57.994	1 7.824	1 17.654	54	.147
55	0 9.010	0 18.840	0 28.670	0 38.499	0 48.329	0 58.158	1 7.988	1 17.817	55	.150
56	0 9.174	0 19.004	0 28.833	0 38.663	0 48.492	0 58.322	1 8.152	1 17.981	56	.153
57	0 9.338	0 19.168	0 28.997	0 38.827	0 48.656	0 58.486	1 8.315	1 18.145	57	.156
58	0 9.502	0 19.331	0 29.161	0 38.991	0 48.820	0 58.650	1 8.479	1 18.309	58	.158
59	0 9.666	0 19.495	0 29.325	0 39.154	0 48.984	0 58.814	1 8.643	1 18.473	59	0.161

TABLE 8.

Sidereal into Mean Solar Time.

To be subtracted from a sidereal time interval.

Sidereal.	8h	9h	10h	11h	12h	13h	14h	15h	For seconds.	
m.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	s.	s.
0	1 18.636	1 28.466	1 38.296	1 48.125	1 57.955	2 7.784	2 17.614	2 27.443		
1	1 18.800	1 28.630	1 38.459	1 48.289	1 58.119	2 7.948	2 17.778	2 27.607	1	0.003
2	1 18.964	1 28.794	1 38.623	1 48.453	1 58.282	2 8.112	2 17.941	2 27.771	2	.005
3	1 19.128	1 28.958	1 38.787	1 48.617	1 58.446	2 8.276	2 18.105	2 27.935	3	.008
4	1 19.292	1 29.121	1 38.951	1 48.780	1 58.610	2 8.440	2 18.269	2 28.099	4	.011
5	1 19.456	1 29.285	1 39.115	1 48.944	1 58.774	2 8.603	2 18.433	2 28.263	5	.014
6	1 19.619	1 29.449	1 39.279	1 49.108	1 58.938	2 8.767	2 18.597	2 28.426	6	.016
7	1 19.783	1 29.613	1 39.442	1 49.272	1 59.101	2 8.931	2 18.761	2 28.590	7	.019
8	1 19.947	1 29.777	1 39.606	1 49.436	1 59.265	2 9.095	2 18.924	2 28.754	8	.022
9	1 20.111	1 29.940	1 39.770	1 49.600	1 59.429	2 9.259	2 19.088	2 28.918	9	.025
10	1 20.275	1 30.104	1 39.934	1 49.763	1 59.593	2 9.423	2 19.252	2 29.082	10	.027
11	1 20.439	1 30.268	1 40.098	1 49.927	1 59.757	2 9.586	2 19.416	2 29.245	11	.030
12	1 20.602	1 30.432	1 40.261	1 50.091	1 59.921	2 9.750	2 19.580	2 29.409	12	.033
13	1 20.766	1 30.596	1 40.425	1 50.255	2 0.084	2 9.914	2 19.744	2 29.573	13	.035
14	1 20.930	1 30.760	1 40.589	1 50.419	2 0.248	2 10.078	2 19.907	2 29.737	14	.038
15	1 21.094	1 30.923	1 40.753	1 50.583	2 0.412	2 10.242	2 20.071	2 29.901	15	.041
16	1 21.258	1 31.087	1 40.917	1 50.746	2 0.576	2 10.405	2 20.235	2 30.065	16	.044
17	1 21.422	1 31.251	1 41.081	1 50.910	2 0.740	2 10.569	2 20.399	2 30.228	17	.046
18	1 21.585	1 31.415	1 41.244	1 51.074	2 0.904	2 10.733	2 20.563	2 30.392	18	.049
19	1 21.749	1 31.579	1 41.408	1 51.238	2 1.067	2 10.897	2 20.727	2 30.556	19	.052
20	1 21.913	1 31.743	1 41.572	1 51.402	2 1.231	2 11.061	2 20.890	2 30.720	20	.055
21	1 22.077	1 31.906	1 41.736	1 51.565	2 1.395	2 11.225	2 21.054	2 30.884	21	.057
22	1 22.241	1 32.070	1 41.900	1 51.729	2 1.559	2 11.388	2 21.218	2 31.048	22	.060
23	1 22.404	1 32.234	1 42.064	1 51.893	2 1.723	2 11.552	2 21.382	2 31.211	23	.063
24	1 22.568	1 32.398	1 42.227	1 52.057	2 1.887	2 11.716	2 21.546	2 31.375	24	.066
25	1 22.732	1 32.562	1 42.391	1 52.221	2 2.050	2 11.880	2 21.709	2 31.539	25	.068
26	1 22.896	1 32.726	1 42.555	1 52.385	2 2.214	2 12.044	2 21.873	2 31.703	26	.071
27	1 23.060	1 32.889	1 42.719	1 52.548	2 2.378	2 12.208	2 22.037	2 31.867	27	.074
28	1 23.224	1 33.053	1 42.883	1 52.712	2 2.542	2 12.371	2 22.201	2 32.031	28	.076
29	1 23.387	1 33.217	1 43.047	1 52.876	2 2.706	2 12.535	2 22.365	2 32.194	29	.079
30	1 23.551	1 33.381	1 43.210	1 53.040	2 2.869	2 12.699	2 22.529	2 32.358	30	.082
31	1 23.715	1 33.545	1 43.374	1 53.204	2 3.033	2 12.863	2 22.692	2 32.522	31	.085
32	1 23.879	1 33.708	1 43.538	1 53.368	2 3.197	2 13.027	2 22.856	2 32.686	32	.087
33	1 24.043	1 33.872	1 43.702	1 53.531	2 3.361	2 13.191	2 23.020	2 32.850	33	.090
34	1 24.207	1 34.036	1 43.866	1 53.695	2 3.525	2 13.354	2 23.184	2 33.013	34	.093
35	1 24.370	1 34.200	1 44.029	1 53.859	2 3.689	2 13.518	2 23.348	2 33.177	35	.096
36	1 24.534	1 34.364	1 44.193	1 54.023	2 3.852	2 13.682	2 23.512	2 33.341	36	.098
37	1 24.698	1 34.528	1 44.357	1 54.187	2 4.016	2 13.846	2 23.675	2 33.505	37	.101
38	1 24.862	1 34.691	1 44.521	1 54.351	2 4.180	2 14.010	2 23.839	2 33.669	38	.104
39	1 25.026	1 34.855	1 44.685	1 54.514	2 4.344	2 14.173	2 24.003	2 33.833	39	.106
40	1 25.190	1 35.019	1 44.849	1 54.678	2 4.508	2 14.337	2 24.167	2 33.996	40	.109
41	1 25.353	1 35.183	1 45.012	1 54.842	2 4.672	2 14.501	2 24.331	2 34.160	41	.112
42	1 25.517	1 35.347	1 45.176	1 55.006	2 4.835	2 14.665	2 24.495	2 34.324	42	.115
43	1 25.681	1 35.511	1 45.340	1 55.170	2 4.999	2 14.829	2 24.658	2 34.488	43	.117
44	1 25.845	1 35.674	1 45.504	1 55.333	2 5.163	2 14.993	2 24.822	2 34.652	44	.120
45	1 26.009	1 35.838	1 45.668	1 55.497	2 5.327	2 15.156	2 24.986	2 34.816	45	.123
46	1 26.172	1 36.002	1 45.832	1 55.661	2 5.491	2 15.320	2 25.150	2 34.979	46	.126
47	1 26.336	1 36.166	1 45.995	1 55.825	2 5.655	2 15.484	2 25.314	2 35.143	47	.128
48	1 26.500	1 36.330	1 46.159	1 55.989	2 5.818	2 15.648	2 25.477	2 35.307	48	.131
49	1 26.664	1 36.493	1 46.323	1 56.153	2 5.982	2 15.812	2 25.641	2 35.471	49	.134
50	1 26.828	1 36.657	1 46.487	1 56.316	2 6.146	2 15.976	2 25.805	2 35.635	50	.137
51	1 26.992	1 36.821	1 46.651	1 56.480	2 6.310	2 16.139	2 25.969	2 35.798	51	.139
52	1 27.155	1 36.985	1 46.815	1 56.644	2 6.474	2 16.303	2 26.133	2 35.962	52	.142
53	1 27.319	1 37.149	1 46.978	1 56.808	2 6.637	2 16.467	2 26.297	2 36.126	53	.145
54	1 27.483	1 37.313	1 47.142	1 56.972	2 6.801	2 16.631	2 26.460	2 36.290	54	.147
55	1 27.647	1 37.476	1 47.306	1 57.136	2 6.965	2 16.795	2 26.624	2 36.454	55	.150
56	1 27.811	1 37.640	1 47.470	1 57.299	2 7.129	2 16.959	2 26.788	2 36.618	56	.153
57	1 27.975	1 37.804	1 47.634	1 57.463	2 7.293	2 17.122	2 26.952	2 36.781	57	.156
58	1 28.138	1 37.968	1 47.797	1 57.627	2 7.457	2 17.286	2 27.116	2 36.945	58	.158
59	1 28.302	1 38.132	1 47.961	1 57.791	2 7.620	2 17.450	2 27.280	2 37.109	59	0.161

TABLE 8.

Sidereal into Mean Solar Time.

To be subtracted from a sidereal time interval.

Sidereal.	16h	17h	18h	19h	20h	21h	22h	23h	For seconds.	
m.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	s.	s.
0	2 37.273	2 47.102	2 56.932	3 6.762	3 16.591	3 26.421	3 36.250	3 46.080		
1	2 37.437	2 47.266	2 57.096	3 6.925	3 16.755	3 26.585	3 36.414	3 46.244	1	0.003
2	2 37.601	2 47.430	2 57.260	3 7.089	3 16.919	3 26.748	3 36.578	3 46.407	2	.005
3	2 37.764	2 47.594	2 57.424	3 7.253	3 17.083	3 26.912	3 36.742	3 46.571	3	.008
4	2 37.928	2 47.758	2 57.587	3 7.417	3 17.246	3 27.076	3 36.906	3 46.735	4	.011
5	2 38.092	2 47.922	2 57.751	3 7.581	3 17.410	3 27.240	3 37.069	3 46.899	5	.014
6	2 38.256	2 48.085	2 57.915	3 7.745	3 17.574	3 27.404	3 37.233	3 47.063	6	.016
7	2 38.420	2 48.249	2 58.079	3 7.908	3 17.738	3 27.568	3 37.397	3 47.227	7	.019
8	2 38.584	2 48.413	2 58.243	3 8.072	3 17.902	3 27.731	3 37.561	3 47.390	8	.022
9	2 38.747	2 48.577	2 58.406	3 8.236	3 18.066	3 27.895	3 37.725	3 47.554	9	.025
10	2 38.911	2 48.741	2 58.570	3 8.400	3 18.229	3 28.059	3 37.889	3 47.718	10	.027
11	2 39.075	2 48.905	2 58.734	3 8.564	3 18.393	3 28.223	3 38.052	3 47.882	11	.030
12	2 39.239	2 49.068	2 58.898	3 8.728	3 18.557	3 28.387	3 38.216	3 48.046	12	.033
13	2 39.403	2 49.232	2 59.062	3 8.891	3 18.721	3 28.550	3 38.380	3 48.210	13	.035
14	2 39.566	2 49.396	2 59.226	3 9.055	3 18.885	3 28.714	3 38.544	3 48.373	14	.038
15	2 39.730	2 49.560	2 59.389	3 9.219	3 19.049	3 28.878	3 38.708	3 48.537	15	.041
16	2 39.894	2 49.724	2 59.553	3 9.383	3 19.212	3 29.042	3 38.871	3 48.701	16	.044
17	2 40.058	2 49.888	2 59.717	3 9.547	3 19.376	3 29.206	3 39.035	3 48.865	17	.046
18	2 40.222	2 50.051	2 59.881	3 9.710	3 19.540	3 29.370	3 39.199	3 49.029	18	.049
19	2 40.386	2 50.215	3 0.045	3 9.874	3 19.704	3 29.533	3 39.363	3 49.193	19	.052
20	2 40.549	2 50.379	3 0.209	3 10.038	3 19.868	3 29.697	3 39.527	3 49.356	20	.055
21	2 40.713	2 50.543	3 0.372	3 10.202	3 20.032	3 29.861	3 39.691	3 49.520	21	.057
22	2 40.877	2 50.707	3 0.536	3 10.366	3 20.195	3 30.025	3 39.854	3 49.684	22	.060
23	2 41.041	2 50.870	3 0.700	3 10.530	3 20.359	3 30.189	3 40.018	3 49.848	23	.063
24	2 41.205	2 51.034	3 0.864	3 10.693	3 20.523	3 30.353	3 40.182	3 50.012	24	.066
25	2 41.369	2 51.198	3 1.028	3 10.857	3 20.687	3 30.516	3 40.346	3 50.175	25	.068
26	2 41.532	2 51.362	3 1.192	3 11.021	3 20.851	3 30.680	3 40.510	3 50.339	26	.071
27	2 41.696	2 51.526	3 1.355	3 11.185	3 21.014	3 30.844	3 40.674	3 50.503	27	.074
28	2 41.860	2 51.690	3 1.519	3 11.349	3 21.178	3 31.008	3 40.837	3 50.667	28	.076
29	2 42.024	2 51.853	3 1.683	3 11.513	3 21.342	3 31.172	3 41.001	3 50.831	29	.079
30	2 42.188	2 52.017	3 1.847	3 11.676	3 21.506	3 31.336	3 41.165	3 50.995	30	.082
31	2 42.352	2 52.181	3 2.011	3 11.840	3 21.670	3 31.499	3 41.329	3 51.158	31	.085
32	2 42.515	2 52.345	3 2.174	3 12.004	3 21.834	3 31.663	3 41.493	3 51.322	32	.087
33	2 42.679	2 52.509	3 2.338	3 12.168	3 21.997	3 31.827	3 41.657	3 51.486	33	.090
34	2 42.843	2 52.673	3 2.502	3 12.332	3 22.161	3 31.991	3 41.820	3 51.650	34	.093
35	2 43.007	2 52.836	3 2.666	3 12.496	3 22.325	3 32.155	3 41.984	3 51.814	35	.096
36	2 43.171	2 53.000	3 2.830	3 12.659	3 22.489	3 32.318	3 42.148	3 51.978	36	.098
37	2 43.334	2 53.164	3 2.994	3 12.823	3 22.653	3 32.482	3 42.312	3 52.141	37	.101
38	2 43.498	2 53.328	3 3.157	3 12.987	3 22.817	3 32.646	3 42.476	3 52.305	38	.104
39	2 43.662	2 53.492	3 3.321	3 13.151	3 22.980	3 32.810	3 42.639	3 52.469	39	.106
40	2 43.826	2 53.656	3 3.485	3 13.315	3 23.144	3 32.974	3 42.803	3 52.633	40	.109
41	2 43.990	2 53.819	3 3.649	3 13.478	3 23.308	3 33.138	3 42.967	3 52.797	41	.112
42	2 44.154	2 53.983	3 3.813	3 13.642	3 23.472	3 33.301	3 43.131	3 52.961	42	.115
43	2 44.317	2 54.147	3 3.977	3 13.806	3 23.636	3 33.465	3 43.295	3 53.124	43	.117
44	2 44.481	2 54.311	3 4.140	3 13.970	3 23.800	3 33.629	3 43.459	3 53.288	44	.120
45	2 44.645	2 54.475	3 4.304	3 14.134	3 23.963	3 33.793	3 43.622	3 53.452	45	.123
46	2 44.809	2 54.638	3 4.468	3 14.298	3 24.127	3 33.957	3 43.786	3 53.616	46	.126
47	2 44.973	2 54.802	3 4.632	3 14.461	3 24.291	3 34.121	3 43.950	3 53.780	47	.128
48	2 45.137	2 54.966	3 4.796	3 14.625	3 24.455	3 34.284	3 44.114	3 53.943	48	.131
49	2 45.300	2 55.130	3 4.960	3 14.789	3 24.619	3 34.448	3 44.278	3 54.107	49	.134
50	2 45.464	2 55.294	3 5.123	3 14.953	3 24.782	3 34.612	3 44.442	3 54.271	50	.137
51	2 45.628	2 55.458	3 5.287	3 15.117	3 24.946	3 34.776	3 44.605	3 54.435	51	.139
52	2 45.792	2 55.621	3 5.451	3 15.281	3 25.110	3 34.940	3 44.769	3 54.599	52	.142
53	2 45.956	2 55.785	3 5.615	3 15.444	3 25.274	3 35.104	3 44.933	3 54.763	53	.145
54	2 46.120	2 55.949	3 5.779	3 15.608	3 25.438	3 35.267	3 45.097	3 54.926	54	.147
55	2 46.283	2 56.113	3 5.942	3 15.772	3 25.602	3 35.431	3 45.261	3 55.090	55	.150
56	2 46.447	2 56.277	3 6.106	3 15.936	3 25.765	3 35.595	3 45.425	3 55.254	56	.153
57	2 46.611	2 56.441	3 6.270	3 16.100	3 25.929	3 35.759	3 45.588	3 55.418	57	.156
58	2 46.755	2 56.604	3 6.434	3 16.264	3 26.093	3 35.923	3 45.752	3 55.582	58	.158
59	2 46.939	2 56.768	3 6.598	3 16.427	3 26.257	3 36.086	3 45.916	3 55.746	59	0.161

6583—06——31

TABLE 9.

Mean Solar into Sidereal Time.

To be added to a mean time interval.

Mean.	0h	1h	2h	3h	4h	5h	6h	7h	For seconds.	
m.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	s.	s.
0	0 0.000	0 9.856	0 19.713	0 29.569	0 39.426	0 49.282	0 59.139	1 8.995		
1	0 0.164	0 10.021	0 19.877	0 29.734	0 39.590	0 49.447	0 59.303	1 9.160	1	0.003
2	0 0.329	0 10.185	0 20.041	0 29.898	0 39.754	0 49.611	0 59.467	1 9.324	2	.005
3	0 0.493	0 10.349	0 20.206	0 30.062	0 39.919	0 49.775	0 59.632	1 9.488	3	.008
4	0 0.657	0 10.514	0 20.370	0 30.227	0 40.083	0 49.939	0 59.796	1 9.652	4	.011
5	0 0.821	0 10.678	0 20.534	0 30.391	0 40.247	0 50.104	0 59.960	1 9.817	5	.014
6	0 0.986	0 10.842	0 20.699	0 30.555	0 40.412	0 50.268	1 0.124	1 9.981	6	.016
7	0 1.150	0 11.006	0 20.863	0 30.719	0 40.576	0 50.432	1 0.289	1 10.145	7	.019
8	0 1.314	0 11.171	0 21.027	0 30.884	0 40.740	0 50.597	1 0.453	1 10.310	8	.022
9	0 1.478	0 11.335	0 21.191	0 31.048	0 40.904	0 50.761	1 0.617	1 10.474	9	.025
10	0 1.643	0 11.499	0 21.356	0 31.212	0 41.069	0 50.925	1 0.782	1 10.638	10	.027
11	0 1.807	0 11.663	0 21.520	0 31.376	0 41.233	0 51.089	1 0.946	1 10.802	11	.030
12	0 1.971	0 11.828	0 21.684	0 31.541	0 41.397	0 51.254	1 1.110	1 10.967	12	.033
13	0 2.136	0 11.992	0 21.849	0 31.705	0 41.561	0 51.418	1 1.274	1 11.131	13	.036
14	0 2.300	0 12.156	0 22.013	0 31.869	0 41.726	0 51.582	1 1.439	1 11.295	14	.038
15	0 2.464	0 12.321	0 22.177	0 32.034	0 41.890	0 51.746	1 1.603	1 11.459	15	.041
16	0 2.628	0 12.485	0 22.341	0 32.198	0 42.054	0 51.911	1 1.767	1 11.624	16	.044
17	0 2.793	0 12.649	0 22.506	0 32.362	0 42.219	0 52.075	1 1.932	1 11.788	17	.047
18	0 2.957	0 12.813	0 22.670	0 32.526	0 42.383	0 52.239	1 2.096	1 11.952	18	.049
19	0 3.121	0 12.978	0 22.834	0 32.691	0 42.547	0 52.404	1 2.260	1 12.117	19	.052
20	0 3.285	0 13.142	0 22.998	0 32.855	0 42.711	0 52.568	1 2.424	1 12.281	20	.055
21	0 3.450	0 13.306	0 23.163	0 33.019	0 42.876	0 52.732	1 2.589	1 12.445	21	.057
22	0 3.614	0 13.471	0 23.327	0 33.183	0 43.040	0 52.896	1 2.753	1 12.609	22	.060
23	0 3.778	0 13.635	0 23.491	0 33.348	0 43.204	0 53.061	1 2.917	1 12.774	23	.063
24	0 3.943	0 13.799	0 23.656	0 33.512	0 43.368	0 53.225	1 3.081	1 12.938	24	.066
25	0 4.107	0 13.963	0 23.820	0 33.676	0 43.533	0 53.389	1 3.246	1 13.102	25	.068
26	0 4.271	0 14.128	0 23.984	0 33.841	0 43.697	0 53.554	1 3.410	1 13.266	26	.071
27	0 4.435	0 14.292	0 24.148	0 34.005	0 43.861	0 53.718	1 3.574	1 13.431	27	.074
28	0 4.600	0 14.456	0 24.313	0 34.169	0 44.026	0 53.882	1 3.739	1 13.595	28	.077
29	0 4.764	0 14.620	0 24.477	0 34.333	0 44.190	0 54.046	1 3.903	1 13.759	29	.079
30	0 4.928	0 14.785	0 24.641	0 34.498	0 44.354	0 54.211	1 4.067	1 13.924	30	.082
31	0 5.093	0 14.949	0 24.805	0 34.662	0 44.518	0 54.375	1 4.231	1 14.088	31	.085
32	0 5.257	0 15.113	0 24.970	0 34.826	0 44.683	0 54.539	1 4.396	1 14.252	32	.088
33	0 5.421	0 15.278	0 25.134	0 34.990	0 44.847	0 54.703	1 4.560	1 14.416	33	.090
34	0 5.585	0 15.442	0 25.298	0 35.155	0 45.011	0 54.868	1 4.724	1 14.581	34	.093
35	0 5.750	0 15.606	0 25.463	0 35.319	0 45.176	0 55.032	1 4.888	1 14.745	35	.096
36	0 5.914	0 15.770	0 25.627	0 35.483	0 45.340	0 55.196	1 5.053	1 14.909	36	.099
37	0 6.078	0 15.935	0 25.791	0 35.648	0 45.504	0 55.361	1 5.217	1 15.073	37	.101
38	0 6.242	0 16.099	0 25.955	0 35.812	0 45.668	0 55.525	1 5.381	1 15.238	38	.104
39	0 6.407	0 16.263	0 26.120	0 35.976	0 45.833	0 55.689	1 5.546	1 15.402	39	.107
40	0 6.571	0 16.427	0 26.284	0 36.140	0 45.997	0 55.853	1 5.710	1 15.566	40	.110
41	0 6.735	0 16.592	0 26.448	0 36.305	0 46.161	0 56.018	1 5.874	1 15.731	41	.112
42	0 6.900	0 16.756	0 26.612	0 36.469	0 46.325	0 56.182	1 6.038	1 15.895	42	.115
43	0 7.064	0 16.920	0 26.777	0 36.633	0 46.490	0 56.346	1 6.203	1 16.059	43	.118
44	0 7.228	0 17.085	0 26.941	0 36.798	0 46.654	0 56.510	1 6.367	1 16.223	44	.120
45	0 7.392	0 17.249	0 27.105	0 36.962	0 46.818	0 56.675	1 6.531	1 16.388	45	.123
46	0 7.557	0 17.413	0 27.270	0 37.126	0 46.983	0 56.839	1 6.695	1 16.552	46	.126
47	0 7.721	0 17.577	0 27.434	0 37.290	0 47.147	0 57.003	1 6.860	1 16.716	47	.129
48	0 7.885	0 17.742	0 27.598	0 37.455	0 47.311	0 57.168	1 7.024	1 16.881	48	.131
49	0 8.049	0 17.906	0 27.762	0 37.619	0 47.475	0 57.332	1 7.188	1 17.045	49	.134
50	0 8.214	0 18.070	0 27.927	0 37.783	0 47.640	0 57.496	1 7.353	1 17.209	50	.137
51	0 8.378	0 18.234	0 28.091	0 37.947	0 47.804	0 57.660	1 7.517	1 17.373	51	.140
52	0 8.542	0 18.399	0 28.255	0 38.112	0 47.968	0 57.825	1 7.681	1 17.538	52	.142
53	0 8.707	0 18.563	0 28.420	0 38.276	0 48.132	0 57.989	1 7.845	1 17.702	53	.145
54	0 8.871	0 18.727	0 28.584	0 38.440	0 48.297	0 58.153	1 8.010	1 17.866	54	.148
55	0 9.035	0 18.892	0 28.748	0 38.605	0 48.461	0 58.317	1 8.174	1 18.030	55	.151
56	0 9.199	0 19.056	0 28.912	0 38.769	0 48.625	0 58.482	1 8.338	1 18.195	56	.153
57	0 9.364	0 19.220	0 29.077	0 38.933	0 48.790	0 58.646	1 8.502	1 18.359	57	.156
58	0 9.528	0 19.384	0 29.241	0 39.097	0 48.954	0 58.810	1 8.667	1 18.523	58	.159
59	0 9.692	0 19.549	0 29.405	0 39.262	0 49.118	0 58.975	1 8.831	1 18.688	59	0.162

TABLE 9.

Mean Solar into Sidereal Time.

To be added to a mean time interval.

Mean.	8h	9h	10h	11h	12h	13h	14h	15h	For seconds.	
m.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	s.	s.
0	1 18.852	1 28.708	1 38.565	1 48.421	1 58.278	2 8.134	2 17.991	2 27.847		
1	1 19.016	1 28.873	1 38.729	1 48.585	1 58.442	2 8.298	2 18.155	2 28.011	1	0.003
2	1 19.180	1 29.037	1 38.893	1 48.750	1 58.606	2 8.463	2 18.319	2 28.176	2	.005
3	1 19.345	1 29.201	1 39.058	1 48.914	1 58.771	2 8.627	2 18.483	2 28.340	3	.008
4	1 19.509	1 29.365	1 39.222	1 49.078	1 58.935	2 8.791	2 18.648	2 28.504	4	.011
5	1 19.673	1 29.530	1 39.386	1 49.243	1 59.099	2 8.956	2 18.812	2 28.668	5	.014
6	1 19.837	1 29.694	1 39.550	1 49.407	1 59.263	2 9.120	2 18.976	2 28.833	6	.016
7	1 20.002	1 29.858	1 39.715	1 49.571	1 59.428	2 9.284	2 19.141	2 28.997	7	.019
8	1 20.166	1 30.022	1 39.879	1 49.735	1 59.592	2 9.448	2 19.305	2 29.161	8	.022
9	1 20.330	1 30.187	1 40.043	1 49.900	1 59.756	2 9.613	2 19.469	2 29.326	9	.025
10	1 20.495	1 30.351	1 40.207	1 50.064	1 59.920	2 9.777	2 19.633	2 29.490	10	.027
11	1 20.659	1 30.515	1 40.372	1 50.228	2 0.085	2 9.941	2 19.798	2 29.654	11	.030
12	1 20.823	1 30.680	1 40.536	1 50.393	2 0.249	2 10.105	2 19.962	2 29.818	12	.033
13	1 20.987	1 30.844	1 40.700	1 50.557	2 0.413	2 10.270	2 20.126	2 29.983	13	.036
14	1 21.152	1 31.008	1 40.865	1 50.721	2 0.578	2 10.434	2 20.290	2 30.147	14	.038
15	1 21.316	1 31.172	1 41.029	1 50.885	2 0.742	2 10.598	2 20.455	2 30.311	15	.041
16	1 21.480	1 31.337	1 41.193	1 51.050	2 0.906	2 10.763	2 20.619	2 30.476	16	.044
17	1 21.644	1 31.501	1 41.357	1 51.214	2 1.070	2 10.927	2 20.783	2 30.640	17	.047
18	1 21.809	1 31.665	1 41.522	1 51.378	2 1.235	2 11.091	2 20.948	2 30.804	18	.049
19	1 21.973	1 31.829	1 41.686	1 51.542	2 1.399	2 11.255	2 21.112	2 30.968	19	.052
20	1 22.137	1 31.994	1 41.850	1 51.707	2 1.563	2 11.420	2 21.276	2 31.133	20	.055
21	1 22.302	1 32.158	1 42.015	1 51.871	2 1.727	2 11.584	2 21.440	2 31.297	21	.057
22	1 22.466	1 32.322	1 42.179	1 52.035	2 1.892	2 11.748	2 21.605	2 31.461	22	.060
23	1 22.630	1 32.487	1 42.343	1 52.200	2 2.056	2 11.912	2 21.769	2 31.625	23	.063
24	1 22.794	1 32.651	1 42.507	1 52.364	2 2.220	2 12.077	2 21.933	2 31.790	24	.066
25	1 22.959	1 32.815	1 42.672	1 52.528	2 2.385	2 12.241	2 22.098	2 31.954	25	.068
26	1 23.123	1 32.979	1 42.836	1 52.692	2 2.549	2 12.405	2 22.262	2 32.118	26	.071
27	1 23.287	1 33.144	1 43.000	1 52.857	2 2.713	2 12.570	2 22.426	2 32.283	27	.074
28	1 23.451	1 33.308	1 43.164	1 53.021	2 2.877	2 12.734	2 22.590	2 32.447	28	.077
29	1 23.616	1 33.472	1 43.329	1 53.185	2 3.042	2 12.898	2 22.755	2 32.611	29	.079
30	1 23.780	1 33.637	1 43.493	1 53.349	2 3.206	2 13.062	2 22.919	2 32.775	30	.082
31	1 23.944	1 33.801	1 43.657	1 53.514	2 3.370	2 13.227	2 23.083	2 32.940	31	.085
32	1 24.109	1 33.965	1 43.822	1 53.678	2 3.534	2 13.391	2 23.247	2 33.104	32	.088
33	1 24.273	1 34.129	1 43.986	1 53.842	2 3.699	2 13.555	2 23.412	2 33.268	33	.090
34	1 24.437	1 34.294	1 44.150	1 54.007	2 3.863	2 13.720	2 23.576	2 33.432	34	.093
35	1 24.601	1 34.458	1 44.314	1 54.171	2 4.027	2 13.884	2 23.740	2 33.597	35	.096
36	1 24.766	1 34.622	1 44.479	1 54.335	2 4.192	2 14.048	2 23.905	2 33.761	36	.099
37	1 24.930	1 34.786	1 44.643	1 54.499	2 4.356	2 14.212	2 24.069	2 33.925	37	.101
38	1 25.094	1 34.951	1 44.807	1 54.664	2 4.520	2 14.377	2 24.233	2 34.090	38	.104
39	1 25.259	1 35.115	1 44.971	1 54.828	2 4.684	2 14.541	2 24.397	2 34.254	39	.107
40	1 25.423	1 35.279	1 45.136	1 54.992	2 4.849	2 14.705	2 24.562	2 34.418	40	.110
41	1 25.587	1 35.444	1 45.300	1 55.156	2 5.013	2 14.869	2 24.726	2 34.582	41	.112
42	1 25.751	1 35.608	1 45.464	1 55.321	2 5.177	2 15.034	2 24.890	2 34.747	42	.115
43	1 25.916	1 35.772	1 45.629	1 55.485	2 5.342	2 15.198	2 25.054	2 34.911	43	.118
44	1 26.080	1 35.936	1 45.793	1 55.649	2 5.506	2 15.362	2 25.219	2 35.075	44	.120
45	1 26.244	1 36.101	1 45.957	1 55.814	2 5.670	2 15.527	2 25.383	2 35.239	45	.123
46	1 26.408	1 36.265	1 46.121	1 55.978	2 5.834	2 15.691	2 25.547	2 35.404	46	.126
47	1 26.573	1 36.429	1 46.286	1 56.142	2 5.999	2 15.855	2 25.712	2 35.568	47	.129
48	1 26.737	1 36.593	1 46.450	1 56.306	2 6.163	2 16.019	2 25.876	2 35.732	48	.131
49	1 26.901	1 36.758	1 46.614	1 56.471	2 6.327	2 16.184	2 26.040	2 35.897	49	.134
50	1 27.066	1 36.922	1 46.778	1 56.635	2 6.491	2 16.348	2 26.204	2 36.061	50	.137
51	1 27.230	1 37.086	1 46.943	1 56.799	2 6.656	2 16.512	2 26.369	2 36.225	51	.140
52	1 27.394	1 37.251	1 47.107	1 56.964	2 6.820	2 16.676	2 26.533	2 36.389	52	.142
53	1 27.558	1 37.415	1 47.271	1 57.128	2 6.984	2 16.841	2 26.697	2 36.554	53	.145
54	1 27.723	1 37.579	1 47.436	1 57.292	2 7.149	2 17.005	2 26.861	2 36.718	54	.148
55	1 27.887	1 37.743	1 47.600	1 57.456	2 7.313	2 17.169	2 27.026	2 36.882	55	.151
56	1 28.051	1 37.908	1 47.764	1 57.621	2 7.477	2 17.334	2 27.190	2 37.047	56	.153
57	1 28.215	1 38.072	1 47.928	1 57.785	2 7.641	2 17.498	2 27.354	2 37.211	57	.156
58	1 28.380	1 38.236	1 48.093	1 57.949	2 7.806	2 17.662	2 27.519	2 37.375	58	.159
59	1 28.544	1 38.400	1 48.257	1 58.113	2 7.970	2 17.826	2 27.683	2 37.539	59	0.162

TABLE 9.

Mean Solar into Sidereal time.

To be added to a mean time interval.

Mean.	16h	17h	18h	19h	20h	21h	22h	23h	For seconds.	
m.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	m. s.	s.	s.
0	2 37.704	2 47.560	2 57.417	3 7.273	3 17.129	3 26.986	3 36.842	3 46.699		
1	2 37.868	2 47.724	2 57.581	3 7.437	3 17.294	3 27.150	3 37.007	3 46.863	1	0.003
2	2 38.032	2 47.889	2 57.745	3 7.602	3 17.458	3 27.315	3 37.171	3 47.027	2	.005
3	2 38.196	2 48.053	2 57.909	3 7.766	3 17.622	3 27.479	3 37.335	3 47.192	3	.008
4	2 38.361	2 48.217	2 58.074	3 7.930	3 17.787	3 27.643	3 37.500	3 47.356	4	.011
5	2 38.525	2 48.381	2 58.238	3 8.094	3 17.951	3 27.807	3 37.664	3 47.520	5	.014
6	2 38.689	2 48.546	2 58.402	3 8.259	3 18.115	3 27.972	3 37.828	3 47.685	6	.016
7	2 38.854	2 48.710	2 58.566	3 8.423	3 18.279	3 28.136	3 37.992	3 47.849	7	.019
8	2 39.018	2 48.874	2 58.731	3 8.587	3 18.444	3 28.300	3 38.157	3 48.013	8	.022
9	2 39.182	2 49.039	2 58.895	3 8.751	3 18.608	3 28.464	3 38.321	3 48.177	9	.025
10	2 39.346	2 49.203	2 59.059	3 8.916	3 18.772	3 28.629	3 38.485	3 48.342	10	.027
11	2 39.511	2 49.367	2 59.224	3 9.080	3 18.937	3 28.793	3 38.649	3 48.506	11	.030
12	2 39.675	2 49.531	2 59.388	3 9.244	3 19.101	3 28.957	3 38.814	3 48.670	12	.033
13	2 39.839	2 49.696	2 59.552	3 9.409	3 19.265	3 29.122	3 38.978	3 48.834	13	.036
14	2 40.003	2 49.860	2 59.716	3 9.573	3 19.429	3 29.286	3 39.142	3 48.999	14	.038
15	2 40.168	2 50.024	2 59.881	3 9.737	3 19.594	3 29.450	3 39.307	3 49.163	15	.041
16	2 40.332	2 50.188	3 0.045	3 9.901	3 19.758	3 29.614	3 39.471	3 49.327	16	.044
17	2 40.496	2 50.353	3 0.209	3 10.066	3 19.922	3 29.779	3 39.635	3 49.492	17	.047
18	2 40.661	2 50.517	3 0.373	3 10.230	3 20.086	3 29.943	3 39.799	3 49.656	18	.049
19	2 40.825	2 50.681	3 0.538	3 10.394	3 20.251	3 30.107	3 39.964	3 49.820	19	.052
20	2 40.989	2 50.846	3 0.702	3 10.559	3 20.415	3 30.271	3 40.128	3 49.984	20	.055
21	2 41.153	2 51.010	3 0.866	3 10.723	3 20.579	3 30.436	3 40.292	3 50.149	21	.057
22	2 41.318	2 51.174	3 1.031	3 10.887	3 20.744	3 30.600	3 40.456	3 50.313	22	.060
23	2 41.482	2 51.338	3 1.195	3 11.051	3 20.908	3 30.764	3 40.621	3 50.477	23	.063
24	2 41.646	2 51.503	3 1.359	3 11.216	3 21.072	3 30.929	3 40.785	3 50.642	24	.066
25	2 41.810	2 51.667	3 1.523	3 11.380	3 21.236	3 31.093	3 40.949	3 50.806	25	.068
26	2 41.975	2 51.831	3 1.688	3 11.544	3 21.401	3 31.257	3 41.114	3 50.970	26	.071
27	2 42.139	2 51.995	3 1.852	3 11.708	3 21.565	3 31.421	3 41.278	3 51.134	27	.074
28	2 42.303	2 52.160	3 2.016	3 11.873	3 21.729	3 31.586	3 41.442	3 51.299	28	.077
29	2 42.468	2 52.324	3 2.181	3 12.037	3 21.893	3 31.750	3 41.606	3 51.463	29	.079
30	2 42.632	2 52.488	3 2.345	3 12.201	3 22.058	3 31.914	3 41.771	3 51.627	30	.082
31	2 42.796	2 52.653	3 2.509	3 12.366	3 22.222	3 32.078	3 41.935	3 51.791	31	.085
32	2 42.960	2 52.817	3 2.673	3 12.530	3 22.386	3 32.243	3 42.099	3 51.956	32	.088
33	2 43.125	2 52.981	3 2.838	3 12.694	3 22.551	3 32.407	3 42.264	3 52.120	33	.090
34	2 43.289	2 53.145	3 3.002	3 12.858	3 22.715	3 32.571	3 42.428	3 52.284	34	.093
35	2 43.453	2 53.310	3 3.166	3 13.023	3 22.879	3 32.736	3 42.592	3 52.449	35	.096
36	2 43.617	2 53.474	3 3.330	3 13.187	3 23.043	3 32.900	3 42.756	3 52.613	36	.099
37	2 43.782	2 53.638	3 3.495	3 13.351	3 23.208	3 33.064	3 42.921	3 52.777	37	.101
38	2 43.946	2 53.803	3 3.659	3 13.515	3 23.372	3 33.228	3 43.085	3 52.941	38	.104
39	2 44.110	2 53.967	3 3.823	3 13.680	3 23.536	3 33.393	3 43.249	3 53.106	39	.107
40	2 44.275	2 54.131	3 3.988	3 13.844	3 23.700	3 33.557	3 43.413	3 53.270	40	.110
41	2 44.439	2 54.295	3 4.152	3 14.008	3 23.865	3 33.721	3 43.578	3 53.434	41	.112
42	2 44.603	2 54.460	3 4.316	3 14.173	3 24.029	3 33.886	3 43.742	3 53.598	42	.115
43	2 44.767	2 54.624	3 4.480	3 14.337	3 24.193	3 34.050	3 43.906	3 53.763	43	.118
44	2 44.932	2 54.788	3 4.645	3 14.501	3 24.358	3 34.214	3 44.071	3 53.927	44	.120
45	2 45.096	2 54.952	3 4.809	3 14.665	3 24.522	3 34.378	3 44.235	3 54.091	45	.123
46	2 45.260	2 55.117	3 4.973	3 14.830	3 24.686	3 34.543	3 44.399	3 54.256	46	.126
47	2 45.425	2 55.281	3 5.137	3 14.994	3 24.850	3 34.707	3 44.563	3 54.420	47	.129
48	2 45.589	2 55.445	3 5.302	3 15.158	3 25.015	3 34.871	3 44.728	3 54.584	48	.131
49	2 45.753	2 55.610	3 5.466	3 15.322	3 25.179	3 35.035	3 44.892	3 54.748	49	.134
50	2 45.917	2 55.774	3 5.630	3 15.487	3 25.343	3 35.200	3 45.056	3 54.913	50	.137
51	2 46.082	2 55.938	3 5.795	3 15.651	3 25.508	3 35.364	3 45.220	3 55.077	51	.140
52	2 46.246	2 56.102	3 5.959	3 15.815	3 25.672	3 35.528	3 45.385	3 55.241	52	.142
53	2 46.410	2 56.267	3 6.123	3 15.980	3 25.836	3 35.693	3 45.549	3 55.405	53	.145
54	2 46.574	2 56.431	3 6.287	3 16.144	3 26.000	3 35.857	3 45.713	3 55.570	54	.148
55	2 46.739	2 56.595	3 6.452	3 16.308	3 26.165	3 36.021	3 45.878	3 55.734	55	.151
56	2 46.903	2 56.759	3 6.616	3 16.472	3 26.329	3 36.185	3 46.042	3 55.898	56	.153
57	2 47.067	2 56.924	3 6.780	3 16.637	3 26.493	3 36.350	3 46.206	3 56.063	57	.156
58	2 47.232	2 57.088	3 6.944	3 16.801	3 26.657	3 36.514	3 46.370	3 56.227	58	.159
59	2 47.396	2 57.252	3 7.109	3 16.965	3 26.822	3 36.678	3 46.535	3 56.391	59	0.162

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 0° to 20°—March 21 to June 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	MARCH.					APRIL.										MAY.							JUNE.			Approx. date.	Lat. N.
		21	23	26	28	31	3	5	8	11	13	16	19	22	25	28	1	5	8	12	16	21	26	1	10	22		
	Dec. N.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
0	R.	6 04	6 03	6 02	6 01	6 00	6 00	5 59	5 58	5 57	5 57	5 56	5 55	5 55	5 54	5 53	5 53	5 53	5 52	5 52	5 52	5 52	5 53	5 54	5 55	5 57	R.	0
	S.	6 11	6 11	6 10	6 09	6 08	6 08	6 07	6 06	6 05	6 05	6 04	6 03	6 03	6 02	6 01	6 01	6 01	6 00	6 00	6 00	6 00	6 01	6 02	6 03	6 05	S.	
1	R.	6 04	6 03	6 02	6 01	6 00	6 00	5 59	5 58	5 57	5 56	5 55	5 55	5 54	5 53	5 52	5 52	5 52	5 51	5 51	5 51	5 51	5 51	5 52	5 54	5 56	R.	1
	S.	6 11	6 11	6 10	6 09	6 08	6 08	6 07	6 06	6 05	6 05	6 04	6 04	6 03	6 03	6 02	6 02	6 02	6 01	6 01	6 01	6 02	6 02	6 03	6 05	6 07	S.	
2	R.	6 04	6 03	6 02	6 01	6 00	6 00	5 59	5 58	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 51	5 51	5 50	5 50	5 50	5 49	5 50	5 51	5 52	5 54	R.	2
	S.	6 11	6 11	6 10	6 09	6 08	6 08	6 07	6 07	6 06	6 05	6 05	6 04	6 04	6 04	6 03	6 03	6 03	6 02	6 02	6 03	6 03	6 04	6 05	6 06	6 08	S.	
3	R.	6 04	6 03	6 02	6 01	6 00	5 59	5 58	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 50	5 50	5 49	5 49	5 48	5 48	5 48	5 49	5 50	5 52	R.	3
	S.	6 11	6 11	6 10	6 09	6 09	6 08	6 07	6 07	6 06	6 06	6 06	6 05	6 05	6 05	6 04	6 04	6 04	6 03	6 04	6 04	6 05	6 05	6 06	6 08	6 10	S.	
4	R.	6 04	6 03	6 02	6 01	6 00	5 59	5 58	5 57	5 56	5 55	5 54	5 53	5 52	5 50	5 49	5 49	5 49	5 48	5 47	5 47	5 46	5 47	5 48	5 49	5 51	R.	4
	S.	6 11	6 11	6 10	6 09	6 09	6 08	6 08	6 08	6 07	6 07	6 06	6 06	6 06	6 06	6 05	6 05	6 05	6 05	6 05	6 06	6 06	6 07	6 08	6 10	6 12	S.	
5	R.	6 04	6 03	6 02	6 01	6 00	5 59	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 49	5 48	5 48	5 47	5 46	5 46	5 45	5 45	5 45	5 46	5 47	5 49	R.	5
	S.	6 11	6 11	6 10	6 10	6 09	6 09	6 08	6 08	6 08	6 08	6 07	6 07	6 07	6 06	6 06	6 06	6 06	6 06	6 07	6 07	6 08	6 08	6 09	6 11	6 13	S.	
6	R.	6 03	6 02	6 01	6 01	5 59	5 58	5 57	5 55	5 54	5 53	5 52	5 51	5 50	5 49	5 47	5 47	5 46	5 45	5 45	5 44	5 43	5 44	5 45	5 46	5 47	R.	6
	S.	6 11	6 11	6 10	6 10	6 09	6 09	6 09	6 08	6 08	6 08	6 08	6 07	6 07	6 07	6 07	6 07	6 07	6 07	6 08	6 08	6 09	6 10	6 11	6 13	6 15	S.	
7	R.	6 03	6 02	6 01	6 00	5 59	5 58	5 56	5 55	5 54	5 53	5 51	5 50	5 49	5 48	5 46	5 46	5 45	5 44	5 43	5 43	5 42	5 42	5 43	5 44	5 46	R.	7
	S.	6 11	6 11	6 10	6 10	6 10	6 10	6 09	6 09	6 09	6 09	6 08	6 08	6 08	6 08	6 08	6 09	6 09	6 09	6 09	6 10	6 11	6 12	6 13	6 15	6 17	S.	
8	R.	6 03	6 02	6 01	6 00	5 58	5 57	5 56	5 54	5 53	5 52	5 50	5 49	5 48	5 47	5 45	5 45	5 44	5 43	5 42	5 41	5 40	5 40	5 41	5 42	5 44	R.	8
	S.	6 11	6 11	6 10	6 10	6 10	6 10	6 10	6 09	6 09	6 09	6 09	6 09	6 09	6 09	6 09	6 10	6 10	6 10	6 11	6 11	6 12	6 13	6 15	6 17	6 19	S.	
9	R.	6 03	6 02	6 01	6 00	5 58	5 57	5 55	5 54	5 52	5 51	5 49	5 48	5 47	5 46	5 44	5 44	5 42	5 41	5 40	5 40	5 39	5 39	5 39	5 40	5 42	R.	9
	S.	6 11	6 11	6 11	6 11	6 11	6 11	6 10	6 10	6 10	6 10	6 10	6 10	6 10	6 10	6 10	6 11	6 11	6 11	6 12	6 13	6 14	6 15	6 17	6 19	6 21	S.	
10	R.	6 03	6 02	6 01	6 00	5 58	5 57	5 55	5 53	5 52	5 51	5 49	5 48	5 47	5 45	5 43	5 43	5 41	5 40	5 39	5 38	5 37	5 37	5 37	5 38	5 40	R.	10
	S.	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 12	6 12	6 12	6 13	6 14	6 15	6 16	6 18	6 20	6 22	S.	
11	R.	6 03	6 02	6 01	5 59	5 57	5 56	5 54	5 53	5 51	5 50	5 48	5 47	5 46	5 44	5 42	5 42	5 40	5 39	5 38	5 37	5 36	5 36	5 36	5 36	5 38	R.	11
	S.	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 11	6 12	6 12	6 12	6 12	6 12	6 12	6 13	6 13	6 14	6 15	6 16	6 17	6 18	6 20	6 22	6 24	S.	
12	R.	6 03	6 02	6 01	5 59	5 57	5 56	5 54	5 52	5 51	5 49	5 47	5 46	5 45	5 43	5 41	5 41	5 39	5 38	5 37	5 36	5 34	5 34	5 34	5 35	5 36	R.	12
	S.	6 11	6 11	6 11	6 11	6 11	6 12	6 12	6 12	6 12	6 12	6 12	6 12	6 13	6 13	6 13	6 14	6 14	6 15	6 16	6 17	6 18	6 19	6 21	6 24	6 26	S.	
13	R.	6 03	6 02	6 00	5 59	5 57	5 55	5 53	5 52	5 50	5 48	5 46	5 45	5 44	5 42	5 40	5 39	5 38	5 36	5 35	5 34	5 33	5 33	5 33	5 33	5 34	R.	13
	S.	6 11	6 11	6 11	6 12	6 12	6 12	6 12	6 12	6 13	6 13	6 13	6 13	6 14	6 14	6 14	6 15	6 16	6 16	6 17	6 18	6 20	6 21	6 23	6 26	6 28	S.	
14	R.	6 03	6 02	6 00	5 59	5 57	5 55	5 53	5 51	5 49	5 48	5 46	5 44	5 43	5 41	5 39	5 38	5 37	5 35	5 34	5 33	5 32	5 31	5 31	5 31	5 32	R.	14
	S.	6 11	6 11	6 11	6 12	6 12	6 12	6 13	6 13	6 13	6 14	6 14	6 14	6 15	6 15	6 15	6 16	6 17	6 18	6 19	6 20	6 21	6 23	6 25	6 28	6 30	S.	
15	R.	6 03	6 02	6 00	5 58	5 56	5 55	5 53	5 51	5 49	5 47	5 45	5 43	5 42	5 40	5 38	5 37	5 35	5 34	5 32	5 31	5 30	5 29	5 29	5 29	5 30	R.	15
	S.	6 11	6 12	6 12	6 12	6 12	6 13	6 13	6 14	6 14	6 14	6 15	6 15	6 16	6 16	6 16	6 17	6 18	6 19	6 20	6 21	6 23	6 24	6 27	6 30	6 32	S.	
16	R.	6 03	6 02	6 00	5 58	5 56	5 54	5 52	5 50	5 48	5 47	5 45	5 43	5 41	5 39	5 37	5 36	5 34	5 32	5 30	5 29	5 28	5 28	5 28	5 28	5 28	R.	16
	S.	6 11	6 12	6 12	6 12	6 13	6 13	6 14	6 14	6 14	6 15	6 15	6 16	6 17	6 17	6 17	6 18	6 19	6 20	6 21	6 23	6 24	6 26	6 28	6 31	6 34	S.	
17	R.	6 03	6 02	6 00	5 58	5 56	5 54	5 52	5 50	5 48	5 46	5 44	5 42	5 40	5 38	5 36	5 35	5 33	5 31	5 29	5 28	5 26	5 26	5 26	5 26	5 26	R.	17
	S.	6 11	6 12	6 13	6 13	6 13	6 14	6 14	6 15	6 15	6 16	6 16	6 17	6 18	6 18	6 19	6 20	6 21	6 22	6 23	6 25	6 26	6 28	6 30	6 33	6 36	S.	
18	R.	6 03	6 02	6 00	5 58	5 55	5 54	5 51	5 49	5 47	5 45	5 43	5 41	5 39	5 37	5 35	5 34	5 32	5 30	5 28	5 26	5 25	5 24	5 24	5 24	5 24	R.	18
	S.	6 11	6 12	6 12	6 13	6 13	6 14	6 14	6 15	6 16	6 16	6 17	6 18	6 19	6 19	6 20	6 21	6 22	6 23	6 25	6 26	6 28	6 29	6 32	6 35	6 38	S.	
19	R.	6 03	6 01	5 59	5 57	5 55	5 53	5 51	5 49	5 46	5 44	5 42	5 40	5 38	5 36	5 34	5 32	5 30	5 28	5 26	5 25	5 23	5 22	5 22	5 22	5 22	R.	19
	S.	6 11	6 12	6 12	6 13	6 14	6 14	6 15	6 16	6 16	6 17	6 18	6 19	6 20	6 20	6 21	6 22	6 23	6 24	6 26	6 28	6 29	6 31	6 34	6 37	6 40	S.	
20	R.	6 03	6 01	5 59	5 57	5 55	5 53	5 50	5 48	5 46	5 44	5 41	5 39	5 37	5 35	5 33	5 31	5 29	5 27	5 25	5 23	5 22	5 21	5 20	5 20	5 20	R.	20
	S.	6 11	6 12	6 12	6 13	6 14	6 15	6 15	6 16	6 17	6 18	6 19	6 20	6 21	6 21	6 22	6 23	6 25	6 26	6 28	6 29	6 31	6 33	6 36	6 39	6 42	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 21° to 40°—March 21 to June 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	MARCH.					APRIL.										MAY.							JUNE.			Approx. date.	Lat. N.
		21	23	26	28	31	3	5	8	11	13	16	19	22	25	28	1	5	8	12	16	21	26	1	10	22		
	Dec. N.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
21	R.	6 03	6 01	5 59	5 57	5 54	5 52	5 50	5 48	5 45	5 43	5 40	5 38	5 36	5 33	5 31	5 30	5 28	5 25	5 23	5 22	5 20	5 19	5 18	5 17	5 18	R.	21
	S.	6 11	6 12	6 13	6 14	6 14	6 15	6 16	6 17	6 18	6 19	6 20	6 21	6 22	6 22	6 23	6 25	6 26	6 27	6 29	6 31	6 33	6 35	6 38	6 41	6 44	S.	
22	R.	6 03	6 01	5 59	5 57	5 54	5 52	5 49	5 47	5 44	5 42	5 40	5 37	5 35	5 32	5 30	5 28	5 26	5 24	5 22	5 20	5 18	5 17	5 16	5 15	5 16	R.	22
	S.	6 11	6 12	6 13	6 14	6 14	6 15	6 16	6 17	6 18	6 19	6 20	6 21	6 23	6 23	6 24	6 26	6 27	6 29	6 31	6 32	6 34	6 37	6 40	6 43	6 46	S.	
23	R.	6 03	6 01	5 59	5 56	5 54	5 52	5 49	5 47	5 44	5 42	5 39	5 36	5 34	5 31	5 29	5 27	5 25	5 22	5 20	5 18	5 16	5 15	5 14	5 13	5 14	R.	23
	S.	6 11	6 12	6 13	6 14	6 15	6 16	6 17	6 18	6 19	6 20	6 21	6 22	6 24	6 25	6 26	6 27	6 29	6 30	6 32	6 34	6 36	6 39	6 42	6 45	6 48	S.	
24	R.	6 03	6 01	5 59	5 56	5 53	5 51	5 48	5 46	5 43	5 41	5 38	5 35	5 33	5 30	5 28	5 26	5 23	5 21	5 19	5 17	5 15	5 13	5 12	5 11	5 12	R.	24
	S.	6 11	6 12	6 13	6 14	6 15	6 16	6 17	6 18	6 19	6 21	6 22	6 23	6 25	6 26	6 27	6 29	6 30	6 32	6 34	6 36	6 38	6 40	6 44	6 47	6 50	S.	
25	R.	6 03	6 01	5 58	5 56	5 53	5 51	5 48	5 45	5 42	5 40	5 37	5 34	5 32	5 29	5 26	5 24	5 22	5 19	5 17	5 15	5 13	5 11	5 10	5 09	5 10	R.	25
	S.	6 11	6 12	6 13	6 15	6 16	6 17	6 18	6 19	6 20	6 22	6 23	6 24	6 26	6 27	6 28	6 30	6 32	6 33	6 36	6 38	6 40	6 42	6 46	6 50	6 53	S.	
26	R.	6 03	6 01	5 58	5 56	5 53	5 50	5 47	5 45	5 42	5 39	5 36	5 33	5 31	5 28	5 25	5 23	5 20	5 18	5 15	5 13	5 11	5 09	5 08	5 07	5 08	R.	26
	S.	6 11	6 12	6 13	6 15	6 16	6 17	6 18	6 20	6 21	6 22	6 24	6 25	6 27	6 28	6 29	6 31	6 33	6 35	6 37	6 39	6 41	6 44	6 48	6 52	6 55	S.	
27	R.	6 03	6 01	5 58	5 55	5 52	5 50	5 47	5 44	5 41	5 38	5 35	5 32	5 30	5 27	5 24	5 22	5 19	5 16	5 14	5 12	5 09	5 07	5 06	5 05	5 06	R.	27
	S.	6 11	6 13	6 14	6 15	6 16	6 18	6 19	6 20	6 22	6 23	6 25	6 26	6 28	6 29	6 31	6 33	6 35	6 36	6 39	6 41	6 43	6 46	6 50	6 54	6 58	S.	
28	R.	6 03	6 01	5 58	5 55	5 52	5 49	5 46	5 43	5 40	5 37	5 34	5 31	5 29	5 26	5 22	5 20	5 17	5 15	5 12	5 10	5 07	5 05	5 04	5 03	5 04	R.	28
	S.	6 11	6 13	6 14	6 15	6 17	6 18	6 19	6 21	6 23	6 24	6 26	6 27	6 29	6 30	6 32	6 34	6 36	6 38	6 40	6 43	6 45	6 48	6 52	6 56	7 00	S.	
29	R.	6 03	6 01	5 57	5 55	5 52	5 49	5 45	5 42	5 39	5 36	5 33	5 30	5 27	5 24	5 21	5 19	5 16	5 13	5 10	5 08	5 05	5 03	5 01	5 00	5 01	R.	29
	S.	6 11	6 13	6 14	6 16	6 17	6 19	6 20	6 22	6 24	6 25	6 27	6 28	6 30	6 32	6 34	6 36	6 38	6 40	6 42	6 45	6 47	6 50	6 54	6 58	7 02	S.	
30	R.	6 03	6 00	5 57	5 54	5 51	5 48	5 45	5 42	5 38	5 35	5 32	5 29	5 26	5 23	5 20	5 17	5 14	5 11	5 09	5 06	5 03	5 01	4 59	4 58	4 59	R.	30
	S.	6 12	6 13	6 14	6 16	6 17	6 19	6 21	6 23	6 24	6 26	6 28	6 29	6 31	6 33	6 35	6 37	6 39	6 41	6 44	6 46	6 49	6 52	6 56	7 01	7 05	S.	
31	R.	6 03	6 00	5 57	5 54	5 51	5 48	5 44	5 41	5 37	5 34	5 31	5 28	5 25	5 22	5 18	5 16	5 13	5 10	5 07	5 04	5 01	4 59	4 57	4 55	4 56	R.	31
	S.	6 12	6 13	6 15	6 17	6 18	6 20	6 21	6 23	6 25	6 27	6 29	6 31	6 33	6 35	6 37	6 39	6 41	6 43	6 46	6 48	6 51	6 55	6 59	7 03	7 07	S.	
32	R.	6 03	6 00	5 56	5 53	5 50	5 47	5 44	5 41	5 37	5 34	5 30	5 27	5 24	5 21	5 17	5 14	5 11	5 08	5 05	5 02	4 59	4 56	4 54	4 53	4 54	R.	32
	S.	6 12	6 14	6 15	6 17	6 18	6 20	6 22	6 24	6 26	6 28	6 30	6 32	6 34	6 36	6 38	6 40	6 42	6 45	6 48	6 50	6 53	6 57	7 01	7 06	7 10	S.	
33	R.	6 03	6 00	5 56	5 53	5 50	5 47	5 43	5 40	5 36	5 33	5 29	5 26	5 22	5 19	5 15	5 12	5 09	5 06	5 03	5 00	4 57	4 54	4 52	4 50	4 51	R.	33
	S.	6 12	6 14	6 15	6 17	6 19	6 21	6 23	6 25	6 27	6 29	6 31	6 33	6 35	6 37	6 39	6 42	6 44	6 47	6 50	6 53	6 56	6 59	7 04	7 08	7 12	S.	
34	R.	6 03	6 00	5 56	5 53	5 49	5 46	5 42	5 39	5 35	5 32	5 28	5 25	5 21	5 18	5 14	5 11	5 08	5 04	5 01	4 58	4 55	4 52	4 50	4 48	4 49	R.	34
	S.	6 12	6 14	6 16	6 18	6 19	6 21	6 23	6 25	6 27	6 30	6 32	6 34	6 36	6 39	6 41	6 43	6 46	6 49	6 52	6 55	6 58	7 02	7 06	7 11	7 15	S.	
35	R.	6 03	6 00	5 56	5 52	5 49	5 45	5 41	5 38	5 34	5 31	5 27	5 23	5 20	5 16	5 12	5 09	5 06	5 02	4 59	4 56	4 52	4 49	4 47	4 45	4 46	R.	35
	S.	6 12	6 14	6 16	6 18	6 20	6 22	6 24	6 26	6 28	6 31	6 33	6 35	6 38	6 40	6 42	6 45	6 48	6 51	6 54	6 57	7 00	7 04	7 09	7 13	7 18	S.	
36	R.	6 03	6 00	5 56	5 52	5 48	5 45	5 41	5 37	5 33	5 30	5 26	5 22	5 18	5 15	5 11	5 08	5 04	5 00	4 57	4 53	4 50	4 47	4 44	4 42	4 43	R.	36
	S.	6 12	6 14	6 16	6 18	6 20	6 23	6 25	6 27	6 29	6 32	6 34	6 36	6 39	6 42	6 44	6 47	6 50	6 53	6 56	6 59	7 03	7 07	7 11	7 16	7 21	S.	
37	R.	6 03	5 59	5 55	5 52	5 48	5 44	5 40	5 36	5 32	5 28	5 24	5 21	5 17	5 13	5 09	5 06	5 02	4 58	4 54	4 51	4 47	4 44	4 41	4 39	4 40	R.	37
	S.	6 12	6 14	6 16	6 19	6 21	6 24	6 26	6 28	6 30	6 33	6 35	6 38	6 41	6 43	6 46	6 49	6 52	6 55	6 58	7 02	7 05	7 09	7 14	7 19	7 24	S.	
38	R.	6 02	5 59	5 55	5 51	5 47	5 43	5 39	5 35	5 31	5 27	5 23	5 19	5 15	5 12	5 08	5 04	5 00	4 56	4 52	4 49	4 45	4 41	4 38	4 36	4 37	R.	38
	S.	6 12	6 14	6 16	6 19	6 21	6 24	6 26	6 28	6 31	6 34	6 36	6 39	6 42	6 45	6 48	6 51	6 54	6 57	7 00	7 04	7 08	7 12	7 17	7 22	7 27	S.	
39	R.	6 02	5 59	5 55	5 51	5 47	5 43	5 38	5 34	5 30	5 26	5 22	5 18	5 14	5 10	5 06	5 02	4 58	4 54	4 50	4 46	4 42	4 39	4 36	4 33	4 34	R.	39
	S.	6 12	6 15	6 17	6 20	6 22	6 25	6 27	6 29	6 32	6 35	6 38	6 41	6 44	6 47	6 50	6 53	6 56	6 59	7 03	7 06	7 10	7 15	7 20	7 25	7 30	S.	
40	R.	6 02	5 58	5 54	5 50	5 46	5 42	5 38	5 33	5 29	5 25	5 21	5 17	5 12	5 08	5 04	5 00	4 56	4 52	4 48	4 44	4 40	4 36	4 33	4 30	4 31	R.	40
	S.	6 12	6 15	6 17	6 20	6 22	6 25	6 28	6 30	6 33	6 36	6 39	6 42	6 45	6 48	6 51	6 54	6 58	7 01	7 05	7 09	7 13	7 18	7 23	7 28	7 33	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 41° to 60°—March 21 to June 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	MARCH.					APRIL.										MAY.							JUNE.			Approx. date.	Lat. N.
		21	23	26	28	31	3	5	8	11	13	16	19	22	25	28	1	5	8	12	16	21	26	1	10	22		
	Dec. N.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
41	R.	6 02	5 58	5 54	5 50	5 46	5 41	5 37	5 32	5 28	5 24	5 19	5 15	5 11	5 07	5 02	4 58	4 54	4 49	4 45	4 41	4 37	4 33	4 30	4 27	4 27	R.	41
	S.	6 12	6 15	6 18	6 21	6 23	6 26	6 29	6 31	6 34	6 37	6 40	6 43	6 47	6 50	6 53	6 56	7 00	7 03	7 07	7 11	7 16	7 21	7 26	7 31	7 36	S.	
42	R.	6 02	5 58	5 54	5 50	5 45	5 41	5 36	5 32	5 27	5 23	5 18	5 14	5 09	5 05	5 00	4 56	4 52	4 47	4 43	4 39	4 34	4 30	4 27	4 24	4 24	R.	42
	S.	6 12	6 15	6 18	6 21	6 24	6 27	6 29	6 32	6 35	6 38	6 41	6 45	6 48	6 52	6 55	6 58	7 02	7 05	7 09	7 14	7 18	7 23	7 29	7 35	7 40	S.	
43	R.	6 02	5 58	5 53	5 49	5 44	5 40	5 35	5 31	5 26	5 22	5 17	5 12	5 08	5 03	4 58	4 54	4 49	4 45	4 40	4 36	4 31	4 27	4 23	4 20	4 20	R.	43
	S.	6 12	6 15	6 18	6 21	6 24	6 27	6 30	6 33	6 36	6 40	6 43	6 46	6 50	6 53	6 57	7 00	7 04	7 08	7 12	7 17	7 21	7 26	7 32	7 38	7 43	S.	
44	R.	6 02	5 58	5 53	5 49	5 44	5 39	5 34	5 30	5 25	5 21	5 15	5 11	5 06	5 01	4 56	4 52	4 47	4 42	4 37	4 33	4 28	4 24	4 20	4 16	4 16	R.	44
	S.	6 13	6 16	6 19	6 22	6 25	6 28	6 31	6 34	6 37	6 41	6 44	6 48	6 51	6 55	6 59	7 03	7 07	7 11	7 15	7 20	7 25	7 30	7 36	7 42	7 47	S.	
45	R.	6 02	5 57	5 52	5 48	5 43	5 38	5 33	5 28	5 24	5 19	5 14	5 09	5 04	4 59	4 54	4 49	4 44	4 39	4 34	4 30	4 25	4 20	4 16	4 12	4 12	R.	45
	S.	6 13	6 16	6 19	6 22	6 26	6 29	6 32	6 35	6 39	6 42	6 46	6 49	6 53	6 57	7 01	7 05	7 09	7 13	7 18	7 23	7 28	7 34	7 40	7 46	7 51	S.	
46	R.	6 02	5 57	5 52	5 48	5 42	5 37	5 32	5 27	5 22	5 17	5 12	5 08	5 03	4 57	4 52	4 47	4 42	4 36	4 31	4 26	4 21	4 16	4 12	4 08	4 08	R.	46
	S.	6 13	6 16	6 19	6 23	6 26	6 30	6 33	6 36	6 40	6 44	6 47	6 51	6 55	6 59	7 03	7 07	7 12	7 16	7 21	7 26	7 31	7 37	7 43	7 50	7 55	S.	
47	R.	6 02	5 57	5 52	5 47	5 42	5 37	5 31	5 26	5 21	5 16	5 10	5 06	5 01	4 55	4 50	4 45	4 39	4 34	4 28	4 23	4 18	4 13	4 08	4 04	4 04	R.	47
	S.	6 13	6 16	6 20	6 23	6 27	6 31	6 34	6 37	6 41	6 45	6 49	6 53	6 57	7 01	7 05	7 10	7 14	7 19	7 24	7 29	7 35	7 41	7 47	7 54	8 00	S.	
48	R.	6 02	5 57	5 51	5 47	5 41	5 36	5 30	5 25	5 20	5 15	5 09	5 04	4 59	4 53	4 47	4 42	4 36	4 31	4 25	4 20	4 14	4 09	4 04	4 00	3 59	R.	48
	S.	6 13	6 17	6 20	6 24	6 27	6 31	6 35	6 39	6 43	6 47	6 51	6 55	6 59	7 03	7 08	7 13	7 17	7 22	7 27	7 33	7 38	7 44	7 51	7 59	8 04	S.	
49	R.	6 01	5 56	5 51	5 46	5 40	5 35	5 29	5 24	5 18	5 13	5 07	5 02	4 56	4 51	4 45	4 39	4 33	4 27	4 22	4 16	4 11	4 05	4 00	3 55	3 55	R.	49
	S.	6 13	6 17	6 21	6 25	6 28	6 32	6 36	6 40	6 44	6 49	6 53	6 57	7 01	7 06	7 10	7 15	7 20	7 25	7 31	7 36	7 42	7 49	7 56	8 03	8 09	S.	
50	R.	6 01	5 56	5 51	5 45	5 40	5 34	5 28	5 22	5 17	5 11	5 05	5 00	4 54	4 48	4 42	4 36	4 30	4 24	4 18	4 13	4 07	4 01	3 55	3 50	3 50	R.	50
	S.	6 13	6 17	6 21	6 25	6 29	6 33	6 37	6 41	6 46	6 50	6 54	6 59	7 03	7 08	7 13	7 18	7 23	7 28	7 34	7 40	7 46	7 53	8 00	8 08	8 14	S.	
51	R.	6 01	5 56	5 50	5 45	5 39	5 33	5 27	5 21	5 15	5 09	5 03	4 58	4 52	4 46	4 39	4 33	4 27	4 21	4 15	4 09	4 02	3 56	3 51	3 45	3 44	R.	51
	S.	6 13	6 17	6 21	6 26	6 30	6 34	6 39	6 43	6 47	6 52	6 56	7 01	7 06	7 11	7 15	7 21	7 26	7 32	7 38	7 44	7 50	7 57	8 05	8 13	8 19	S.	
52	R.	6 01	5 56	5 50	5 44	5 38	5 32	5 26	5 19	5 14	5 08	5 01	4 55	4 49	4 43	4 36	4 30	4 24	4 17	4 11	4 04	3 58	3 51	3 45	3 40	3 39	R.	52
	S.	6 13	6 18	6 22	6 26	6 31	6 35	6 40	6 44	6 49	6 54	6 58	7 03	7 08	7 13	7 18	7 24	7 30	7 36	7 42	7 48	7 55	8 02	8 10	8 19	8 25	S.	
53	R.	6 01	5 55	5 49	5 43	5 37	5 31	5 24	5 18	5 12	5 06	4 59	4 53	4 47	4 40	4 33	4 27	4 20	4 13	4 07	4 00	3 53	3 46	3 40	3 34	3 33	R.	53
	S.	6 13	6 18	6 23	6 27	6 32	6 37	6 41	6 46	6 51	6 56	7 00	7 05	7 11	7 16	7 21	7 27	7 33	7 39	7 46	7 53	8 00	8 07	8 16	8 25	8 31	S.	
54	R.	6 01	5 55	5 49	5 43	5 36	5 30	5 23	5 16	5 10	5 04	4 57	4 51	4 44	4 37	4 30	4 24	4 17	4 09	4 02	3 55	3 48	3 41	3 34	3 28	3 26	R.	54
	S.	6 14	6 18	6 23	6 28	6 33	6 38	6 42	6 47	6 52	6 58	7 03	7 08	7 13	7 19	7 25	7 31	7 37	7 43	7 50	7 57	8 05	8 13	8 22	8 31	8 37	S.	
55	R.	6 01	5 55	5 48	5 42	5 35	5 29	5 22	5 15	5 08	5 02	4 55	4 48	4 41	4 34	4 27	4 20	4 13	4 05	3 58	3 50	3 43	3 35	3 28	3 21	3 19	R.	55
	S.	6 14	6 19	6 24	6 29	6 34	6 39	6 44	6 49	6 54	7 00	7 05	7 10	7 16	7 22	7 28	7 34	7 41	7 47	7 55	8 02	8 10	8 18	8 28	8 38	8 44	S.	
56	R.	6 01	5 54	5 48	5 41	5 34	5 27	5 20	5 13	5 06	4 59	4 52	4 45	4 38	4 31	4 23	4 16	4 08	4 00	3 53	3 45	3 37	3 29	3 21	3 14	3 12	R.	56
	S.	6 14	6 19	6 24	6 29	6 35	6 40	6 45	6 50	6 56	7 02	7 07	7 13	7 19	7 26	7 32	7 38	7 45	7 52	8 00	8 07	8 15	8 24	8 34	8 45	8 52	S.	
57	R.	6 00	5 54	5 47	5 40	5 33	5 26	5 19	5 11	5 04	4 57	4 49	4 42	4 35	4 27	4 19	4 12	4 04	3 56	3 48	3 39	3 31	3 22	3 14	3 06	3 04	R.	57
	S.	6 14	6 20	6 25	6 30	6 36	6 41	6 47	6 52	6 58	7 04	7 10	7 16	7 23	7 29	7 35	7 42	7 50	7 57	8 05	8 13	8 22	8 31	8 41	8 52	9 00	S.	
58	R.	6 00	5 53	5 46	5 39	5 32	5 25	5 17	5 09	5 02	4 55	4 47	4 39	4 31	4 23	4 15	4 07	3 59	3 50	3 42	3 33	3 24	3 15	3 06	2 57	2 55	R.	58
	S.	6 14	6 20	6 25	6 31	6 37	6 43	6 48	6 54	7 00	7 07	7 13	7 19	7 26	7 33	7 39	7 47	7 55	8 02	8 10	8 19	8 28	8 39	8 50	9 01	9 09	S.	
59	R.	6 00	5 53	5 45	5 38	5 30	5 23	5 15	5 07	5 00	4 52	4 44	4 36	4 28	4 20	4 11	4 02	3 54	3 45	3 36	3 27	3 17	3 07	2 58	2 48	2 45	R.	59
	S.	6 15	6 21	6 26	6 32	6 38	6 44	6 50	6 56	7 03	7 09	7 16	7 23	7 30	7 37	7 44	7 52	8 00	8 08	8 16	8 26	8 36	8 47	8 58	9 10	9 18	S.	
60	R.	6 00	5 52	5 45	5 37	5 29	5 22	5 13	5 05	4 58	4 50	4 41	4 32	4 24	4 16	4 07	3 58	3 48	3 39	3 30	3 20	3 10	3 00	2 50	2 39	2 35	R.	60
	S.	6 15	6 21	6 27	6 33	6 39	6 46	6 52	6 58	7 05	7 12	7 18	7 26	7 33	7 41	7 49	7 57	8 05	8 13	8 23	8 33	8 43	8 54	9 06	9 19	9 28	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 0° to 20°—June 22 to September 23.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date	JUNE.	JULY.					AUGUST.										SEPTEMBER.									Approx. date	Lat. N.
		22	8	12	19	24	28	2	5	9	12	16	19	22	25	28	30	2	5	8	10	13	16	18	21	23		
	Dec. N.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
0	R.	5 57	6 00	6 01	6 02	6 02	6 02	6 02	6 02	6 01	6 01	6 00	6 00	5 59	5 58	5 57	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 49	5 49	R.	0
	S.	6 05	6 08	6 09	6 10	6 10	6 10	6 10	6 10	6 09	6 09	6 08	6 08	6 07	6 06	6 05	6 05	6 04	6 03	6 02	6 01	6 00	5 59	5 58	5 57	5 56	S.	
1	R.	5 56	5 58	6 00	6 00	6 01	6 01	6 01	6 01	6 00	6 00	5 59	5 59	5 58	5 58	5 57	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 49	5 49	R.	1
	S.	6 07	6 09	6 11	6 11	6 12	6 11	6 11	6 11	6 10	6 10	6 09	6 08	6 07	6 07	6 06	6 05	6 04	6 03	6 02	6 01	6 00	5 59	5 58	5 57	5 56	S.	
2	R.	5 54	5 57	5 58	5 59	5 59	6 00	6 00	6 00	5 59	5 59	5 58	5 58	5 58	5 57	5 56	5 56	5 55	5 54	5 53	5 53	5 52	5 51	5 50	5 49	5 49	R.	2
	S.	6 08	6 11	6 12	6 13	6 13	6 13	6 12	6 12	6 11	6 11	6 10	6 09	6 08	6 07	6 06	6 05	6 04	6 03	6 02	6 01	6 00	5 59	5 58	5 57	5 56	S.	
3	R.	5 52	5 55	5 57	5 57	5 58	5 58	5 59	5 59	5 58	5 58	5 57	5 57	5 57	5 56	5 55	5 55	5 55	5 54	5 53	5 53	5 52	5 51	5 50	5 49	5 49	R.	3
	S.	6 10	6 13	6 14	6 14	6 15	6 14	6 14	6 13	6 12	6 12	6 11	6 10	6 09	6 08	6 07	6 06	6 05	6 04	6 03	6 02	6 01	5 59	5 58	5 57	5 56	S.	
4	R.	5 51	5 53	5 55	5 56	5 56	5 57	5 57	5 57	5 57	5 57	5 56	5 56	5 56	5 56	5 55	5 55	5 54	5 53	5 53	5 53	5 52	5 51	5 50	5 49	5 49	R.	4
	S.	6 12	6 14	6 16	6 16	6 16	6 16	6 15	6 14	6 13	6 13	6 12	6 11	6 10	6 09	6 08	6 07	6 06	6 04	6 03	6 02	6 01	5 59	5 58	5 57	5 56	S.	
5	R.	5 49	5 52	5 53	5 54	5 55	5 55	5 56	5 56	5 56	5 56	5 55	5 55	5 55	5 55	5 54	5 54	5 53	5 53	5 52	5 52	5 51	5 51	5 50	5 49	5 49	R.	5
	S.	6 13	6 16	6 17	6 17	6 18	6 17	6 17	6 16	6 15	6 14	6 13	6 12	6 11	6 10	6 09	6 08	6 06	6 05	6 03	6 02	6 01	6 00	5 59	5 57	5 56	S.	
6	R.	5 47	5 50	5 52	5 53	5 53	5 54	5 55	5 55	5 55	5 55	5 54	5 54	5 54	5 54	5 53	5 53	5 53	5 52	5 52	5 52	5 51	5 51	5 50	5 49	5 48	R.	6
	S.	6 15	6 17	6 19	6 19	6 19	6 18	6 18	6 17	6 16	6 15	6 14	6 13	6 11	6 10	6 09	6 08	6 07	6 05	6 04	6 03	6 01	6 00	5 59	5 57	5 56	S.	
7	R.	5 46	5 48	5 50	5 51	5 52	5 53	5 53	5 53	5 53	5 53	5 53	5 54	5 53	5 53	5 53	5 53	5 52	5 52	5 51	5 51	5 51	5 50	5 50	5 49	5 48	R.	7
	S.	6 17	6 19	6 21	6 21	6 21	6 20	6 19	6 18	6 17	6 16	6 15	6 14	6 12	6 11	6 10	6 09	6 07	6 06	6 04	6 03	6 02	6 00	5 59	5 57	5 56	S.	
8	R.	5 44	5 46	5 48	5 49	5 50	5 51	5 52	5 52	5 52	5 52	5 52	5 53	5 52	5 52	5 52	5 52	5 52	5 51	5 51	5 51	5 50	5 50	5 50	5 49	5 48	R.	8
	S.	6 19	6 21	6 22	6 22	6 22	6 21	6 21	6 19	6 18	6 17	6 16	6 15	6 13	6 12	6 11	6 09	6 08	6 06	6 05	6 04	6 02	6 00	5 59	5 57	5 56	S.	
9	R.	5 42	5 44	5 46	5 48	5 49	5 50	5 50	5 51	5 51	5 51	5 51	5 52	5 51	5 51	5 51	5 51	5 51	5 51	5 50	5 50	5 50	5 50	5 49	5 49	5 48	R.	9
	S.	6 21	6 23	6 24	6 24	6 24	6 23	6 22	6 21	6 20	6 18	6 17	6 16	6 14	6 13	6 12	6 10	6 09	6 07	6 05	6 04	6 03	6 01	5 59	5 58	5 56	S.	
10	R.	5 40	5 43	5 45	5 46	5 47	5 48	5 49	5 50	5 50	5 50	5 50	5 51	5 51	5 51	5 50	5 50	5 50	5 50	5 50	5 50	5 50	5 50	5 49	5 49	5 48	R.	10
	S.	6 22	6 25	6 26	6 25	6 25	6 24	6 23	6 22	6 21	6 19	6 18	6 17	6 15	6 14	6 12	6 11	6 09	6 07	6 06	6 05	6 03	6 01	5 59	5 58	5 56	S.	
11	R.	5 38	5 41	5 43	5 45	5 46	5 47	5 48	5 48	5 49	5 49	5 49	5 50	5 50	5 50	5 50	5 50	5 50	5 50	5 49	5 49	5 49	5 49	5 49	5 49	5 48	R.	11
	S.	6 24	6 27	6 27	6 27	6 27	6 26	6 25	6 23	6 22	6 20	6 19	6 18	6 16	6 15	6 13	6 12	6 10	6 08	6 06	6 05	6 03	6 01	5 59	5 58	5 56	S.	
12	R.	5 36	5 39	5 42	5 43	5 44	5 46	5 47	5 47	5 48	5 48	5 48	5 49	5 49	5 49	5 49	5 49	5 49	5 49	5 49	5 49	5 49	5 49	5 49	5 49	5 48	R.	12
	S.	6 26	6 28	6 29	6 28	6 28	6 27	6 26	6 24	6 23	6 21	6 20	6 19	6 17	6 15	6 14	6 12	6 10	6 08	6 07	6 05	6 03	6 01	5 59	5 58	5 56	S.	
13	R.	5 34	5 37	5 40	5 42	5 43	5 44	5 45	5 46	5 46	5 47	5 47	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 49	5 49	5 49	5 49	5 49	5 48	R.	13
	S.	6 28	6 30	6 31	6 30	6 30	6 28	6 27	6 26	6 24	6 23	6 21	6 20	6 18	6 16	6 15	6 13	6 11	6 09	6 07	6 06	6 04	6 02	6 00	5 58	5 56	S.	
14	R.	5 32	5 35	5 38	5 40	5 41	5 43	5 44	5 45	5 45	5 46	5 46	5 47	5 47	5 47	5 47	5 48	5 48	5 48	5 48	5 49	5 49	5 49	5 49	5 49	5 48	R.	14
	S.	6 30	6 32	6 32	6 32	6 31	6 30	6 29	6 27	6 25	6 24	6 22	6 21	6 19	6 17	6 15	6 14	6 12	6 10	6 08	6 06	6 04	6 02	6 00	5 58	5 56	S.	
15	R.	5 30	5 33	5 36	5 38	5 40	5 41	5 42	5 43	5 44	5 45	5 45	5 46	5 46	5 46	5 46	5 47	5 47	5 47	5 47	5 48	5 48	5 48	5 48	5 48	5 48	R.	15
	S.	6 32	6 34	6 34	6 33	6 33	6 31	6 30	6 28	6 27	6 25	6 23	6 22	6 20	6 18	6 16	6 14	6 12	6 10	6 08	6 06	6 04	6 02	6 00	5 58	5 56	S.	
16	R.	5 28	5 32	5 35	5 37	5 38	5 40	5 41	5 42	5 43	5 44	5 44	5 45	5 45	5 46	5 46	5 47	5 47	5 47	5 47	5 48	5 48	5 48	5 48	5 48	5 48	R.	16
	S.	6 34	6 36	6 36	6 35	6 34	6 33	6 32	6 30	6 28	6 26	6 24	6 23	6 21	6 19	6 17	6 15	6 13	6 11	6 09	6 07	6 05	6 02	6 00	5 58	5 56	S.	
17	R.	5 26	5 30	5 33	5 35	5 36	5 38	5 39	5 40	5 41	5 42	5 43	5 44	5 44	5 45	5 45	5 46	5 46	5 46	5 46	5 47	5 47	5 48	5 48	5 48	5 48	R.	17
	S.	6 36	6 38	6 38	6 37	6 36	6 35	6 33	6 31	6 29	6 27	6 26	6 24	6 22	6 20	6 18	6 16	6 14	6 11	6 09	6 07	6 05	6 03	6 00	5 58	5 56	S.	
18	R.	5 24	5 28	5 31	5 33	5 35	5 36	5 38	5 39	5 40	5 41	5 42	5 43	5 43	5 44	5 44	5 45	5 45	5 46	5 46	5 47	5 47	5 48	5 48	5 48	5 48	R.	18
	S.	6 38	6 39	6 39	6 38	6 38	6 36	6 35	6 32	6 30	6 28	6 27	6 25	6 23	6 21	6 18	6 16	6 14	6 12	6 09	6 07	6 05	6 03	6 00	5 58	5 56	S.	
19	R.	5 22	5 26	5 29	5 31	5 33	5 35	5 36	5 38	5 39	5 40	5 41	5 42	5 42	5 43	5 43	5 44	5 45	5 45	5 46	5 47	5 47	5 47	5 48	5 48	5 48	R.	19
	S.	6 40	6 41	6 41	6 40	6 39	6 38	6 36	6 34	6 32	6 30	6 28	6 26	6 24	6 22	6 19	6 17	6 15	6 12	6 10	6 08	6 06	6 03	6 01	5 58	5 56	S.	
20	R.	5 20	5 24	5 27	5 30	5 32	5 33	5 35	5 36	5 37	5 39	5 40	5 41	5 41	5 42	5 43	5 44	5 44	5 45	5 45	5 46	5 47	5 47	5 48	5 48	5 48	R.	20
	S.	6 42	6 43	6 43	6 42	6 41	6 39	6 37	6 35	6 33	6 31	6 29	6 27	6 25	6 22	6 20	6 18	6 15	6 13	6 10	6 08	6 06	6 03	6 01	5 58	5 56	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 21° to 40°—June 22 to September 23.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	JUNE.	JULY.					AUGUST.										SEPTEMBER.									Approx. date.	Lat. N.
		22	3	12	19	24	28	2	5	9	12	16	19	22	25	28	30	1	5	8	10	13	16	18	21	23		
	Dec. N.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
21	R.	5 18	5 22	5 25	5 28	5 30	5 32	5 33	5 35	5 36	5 37	5 38	5 39	5 40	5 41	5 42	5 43	5 43	5 44	5 45	5 46	5 46	5 47	5 47	5 48	5 48	R.	21
	S.	6 44	6 46	6 45	6 44	6 43	6 41	6 39	6 37	6 35	6 32	6 30	6 28	6 26	6 23	6 21	6 19	6 16	6 13	6 11	6 09	6 06	6 04	6 01	5 59	5 56	S.	
22	R.	5 16	5 20	5 23	5 26	5 28	5 30	5 32	5 33	5 35	5 36	5 37	5 38	5 39	5 40	5 41	5 42	5 43	5 44	5 44	5 45	5 46	5 47	5 47	5 48	5 48	R.	22
	S.	6 46	6 48	6 47	6 46	6 44	6 42	6 40	6 38	6 36	6 33	6 31	6 29	6 27	6 24	6 21	6 19	6 17	6 14	6 11	6 09	6 06	6 04	6 01	5 59	5 56	S.	
23	R.	5 14	5 18	5 21	5 24	5 26	5 28	5 30	5 32	5 33	5 35	5 36	5 37	5 38	5 39	5 40	5 42	5 42	5 43	5 44	5 45	5 46	5 46	5 47	5 48	5 48	R.	23
	S.	6 48	6 50	6 49	6 48	6 46	6 44	6 42	6 40	6 37	6 35	6 33	6 30	6 28	6 25	6 22	6 20	6 17	6 14	6 12	6 10	6 07	6 04	6 01	5 59	5 56	S.	
24	R.	5 12	5 16	5 19	5 22	5 25	5 27	5 29	5 30	5 32	5 33	5 35	5 36	5 37	5 38	5 39	5 41	5 42	5 43	5 43	5 44	5 45	5 46	5 47	5 48	5 48	R.	24
	S.	6 50	6 52	6 51	6 49	6 48	6 46	6 44	6 41	6 39	6 36	6 34	6 31	6 29	6 26	6 23	6 21	6 18	6 15	6 12	6 10	6 07	6 04	6 01	5 59	5 56	S.	
25	R.	5 10	5 13	5 17	5 20	5 23	5 25	5 27	5 29	5 30	5 32	5 33	5 35	5 36	5 37	5 38	5 40	5 41	5 42	5 43	5 44	5 45	5 46	5 47	5 48	5 48	R.	25
	S.	6 53	6 54	6 53	6 51	6 50	6 48	6 46	6 43	6 40	6 38	6 35	6 33	6 30	6 27	6 24	6 22	6 19	6 16	6 13	6 10	6 08	6 05	6 02	5 59	5 56	S.	
26	R.	5 08	5 11	5 15	5 18	5 21	5 23	5 25	5 27	5 29	5 31	5 32	5 34	5 35	5 36	5 37	5 39	5 40	5 41	5 42	5 44	5 45	5 46	5 47	5 48	5 48	R.	26
	S.	6 55	6 56	6 55	6 53	6 51	6 49	6 47	6 44	6 42	6 39	6 36	6 34	6 31	6 28	6 25	6 22	6 19	6 16	6 13	6 11	6 08	6 05	6 02	5 59	5 56	S.	
27	R.	5 06	5 09	5 13	5 16	5 19	5 22	5 24	5 26	5 27	5 29	5 31	5 33	5 34	5 35	5 36	5 38	5 39	5 41	5 42	5 43	5 44	5 45	5 46	5 47	5 48	R.	27
	S.	6 58	6 58	6 57	6 55	6 53	6 51	6 49	6 46	6 43	6 40	6 38	6 35	6 32	6 29	6 26	6 23	6 20	6 17	6 14	6 11	6 08	6 05	6 02	5 59	5 57	S.	
28	R.	5 04	5 07	5 11	5 14	5 17	5 20	5 22	5 24	5 26	5 28	5 29	5 31	5 33	5 34	5 35	5 37	5 38	5 40	5 41	5 43	5 44	5 45	5 46	5 47	5 48	R.	28
	S.	7 00	7 00	6 59	6 57	6 55	6 53	6 50	6 47	6 45	6 42	6 39	6 36	6 33	6 30	6 27	6 24	6 21	6 18	6 15	6 12	6 09	6 06	6 03	6 00	5 57	S.	
29	R.	5 01	5 05	5 09	5 12	5 15	5 18	5 20	5 22	5 24	5 26	5 28	5 30	5 31	5 33	5 34	5 36	5 37	5 39	5 40	5 42	5 44	5 45	5 46	5 47	5 48	R.	29
	S.	7 02	7 03	7 02	6 59	6 57	6 55	6 52	6 49	6 46	6 43	6 41	6 38	6 34	6 31	6 28	6 25	6 22	6 19	6 15	6 12	6 09	6 06	6 03	6 00	5 57	S.	
30	R.	4 59	5 02	5 07	5 10	5 13	5 16	5 19	5 21	5 23	5 25	5 27	5 29	5 30	5 32	5 33	5 35	5 37	5 38	5 40	5 42	5 43	5 44	5 46	5 47	5 48	R.	30
	S.	7 05	7 05	7 04	7 01	6 59	6 56	6 53	6 51	6 48	6 45	6 42	6 39	6 35	6 32	6 29	6 26	6 23	6 19	6 16	6 13	6 09	6 06	6 03	6 00	5 57	S.	
31	R.	4 56	5 00	5 04	5 08	5 11	5 14	5 17	5 19	5 21	5 23	5 25	5 27	5 29	5 31	5 32	5 34	5 36	5 38	5 39	5 41	5 43	5 44	5 45	5 47	5 48	R.	31
	S.	7 07	7 08	7 06	7 04	7 01	6 58	6 55	6 52	6 49	6 46	6 43	6 40	6 37	6 34	6 30	6 27	6 24	6 20	6 16	6 13	6 10	6 07	6 03	6 00	5 57	S.	
32	R.	4 54	4 58	5 02	5 06	5 09	5 12	5 15	5 17	5 20	5 22	5 24	5 26	5 28	5 30	5 31	5 33	5 35	5 37	5 39	5 41	5 42	5 43	5 45	5 46	5 48	R.	32
	S.	7 10	7 10	7 09	7 06	7 03	7 00	6 57	6 54	6 51	6 48	6 45	6 41	6 38	6 35	6 31	6 28	6 24	6 20	6 17	6 14	6 10	6 07	6 04	6 00	5 57	S.	
33	R.	4 51	4 55	4 59	5 03	5 07	5 10	5 13	5 15	5 18	5 20	5 22	5 24	5 26	5 28	5 30	5 32	5 34	5 36	5 38	5 40	5 42	5 43	5 45	5 46	5 48	R.	33
	S.	7 12	7 13	7 11	7 08	7 06	7 03	7 00	6 56	6 53	6 49	6 46	6 43	6 39	6 36	6 32	6 29	6 25	6 21	6 18	6 15	6 11	6 07	6 04	6 00	5 57	S.	
34	R.	4 49	4 52	4 57	5 01	5 05	5 08	5 11	5 13	5 16	5 19	5 21	5 23	5 25	5 27	5 29	5 31	5 34	5 36	5 37	5 39	5 41	5 43	5 45	5 46	5 48	R.	34
	S.	7 15	7 15	7 14	7 11	7 08	7 05	7 02	6 58	6 54	6 51	6 48	6 44	6 40	6 37	6 33	6 30	6 26	6 22	6 18	6 15	6 11	6 08	6 04	6 00	5 57	S.	
35	R.	4 46	4 50	4 54	4 58	5 02	5 06	5 09	5 11	5 14	5 17	5 19	5 22	5 24	5 26	5 28	5 30	5 33	5 35	5 37	5 39	5 41	5 42	5 44	5 46	5 48	R.	35
	S.	7 18	7 18	7 16	7 13	7 10	7 07	7 04	7 00	6 56	6 53	6 49	6 46	6 42	6 38	6 34	6 31	6 27	6 23	6 19	6 16	6 12	6 08	6 04	6 00	5 57	S.	
36	R.	4 43	4 47	4 52	4 56	5 00	5 03	5 06	5 09	5 12	5 15	5 18	5 20	5 22	5 25	5 27	5 29	5 32	5 34	5 36	5 38	5 40	5 42	5 44	5 46	5 48	R.	36
	S.	7 21	7 21	7 19	7 16	7 13	7 09	7 06	7 02	6 58	6 54	6 51	6 47	6 43	6 39	6 35	6 32	6 28	6 24	6 20	6 16	6 12	6 08	6 04	6 00	5 57	S.	
37	R.	4 40	4 44	4 49	4 53	4 57	5 01	5 04	5 07	5 10	5 13	5 16	5 19	5 21	5 24	5 26	5 28	5 31	5 33	5 35	5 37	5 40	5 42	5 44	5 46	5 48	R.	37
	S.	7 24	7 24	7 21	7 18	7 15	7 12	7 08	7 04	7 00	6 56	6 53	6 49	6 45	6 41	6 37	6 33	6 29	6 25	6 21	6 17	6 13	6 09	6 05	6 01	5 57	S.	
38	R.	4 37	4 41	4 46	4 51	4 55	4 59	5 02	5 05	5 08	5 11	5 14	5 17	5 19	5 22	5 25	5 27	5 30	5 32	5 34	5 37	5 39	5 41	5 44	5 46	5 47	R.	38
	S.	7 27	7 27	7 24	7 21	7 18	7 14	7 10	7 06	7 02	6 58	6 54	6 50	6 46	6 42	6 38	6 34	6 30	6 25	6 21	6 18	6 13	6 09	6 05	6 01	5 57	S.	
39	R.	4 34	4 38	4 43	4 48	4 52	4 56	5 00	5 03	5 06	5 09	5 12	5 15	5 18	5 21	5 23	5 26	5 29	5 31	5 33	5 36	5 39	5 41	5 43	5 45	5 47	R.	39
	S.	7 30	7 30	7 27	7 24	7 20	7 16	7 13	7 08	7 04	7 00	6 56	6 52	6 48	6 44	6 39	6 35	6 31	6 26	6 22	6 18	6 14	6 10	6 05	6 01	5 57	S.	
40	R.	4 31	4 35	4 40	4 45	4 50	4 54	4 58	5 01	5 04	5 08	5 11	5 14	5 17	5 20	5 22	5 25	5 28	5 30	5 33	5 36	5 38	5 40	5 43	5 45	5 47	R.	40
	S.	7 33	7 33	7 30	7 26	7 23	7 19	7 15	7 10	7 06	7 02	6 58	6 54	6 49	6 45	6 40	6 36	6 32	6 27	6 23	6 19	6 14	6 10	6 06	6 01	5 57	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 41° to 60°—June 22 to September 23.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	JUNE. 22	JULY. 3	JULY. 12	JULY. 19	JULY. 24	JULY. 28	AUGUST. 2	AUGUST. 5	AUGUST. 9	AUGUST. 12
	Dec. N.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
41	R.	4 27	4 32	4 37	4 42	4 47	4 51	4 55	4 59	5 02	5 06
	S.	7 36	7 36	7 33	7 29	7 26	7 21	7 17	7 13	7 08	7 04
42	R.	4 24	4 29	4 34	4 39	4 44	4 49	4 53	4 57	5 00	5 04
	S.	7 40	7 39	7 36	7 32	7 28	7 24	7 20	7 15	7 10	7 06
43	R.	4 20	4 25	4 31	4 36	4 41	4 46	4 50	4 54	4 58	5 02
	S.	7 43	7 43	7 40	7 35	7 31	7 27	7 22	7 17	7 13	7 08
44	R.	4 16	4 21	4 27	4 33	4 38	4 43	4 47	4 51	4 55	4 59
	S.	7 47	7 47	7 44	7 39	7 34	7 30	7 25	7 20	7 15	7 10
45	R.	4 12	4 17	4 23	4 29	4 35	4 40	4 44	4 49	4 53	4 57
	S.	7 51	7 51	7 47	7 42	7 38	7 33	7 28	7 23	7 18	7 13
46	R.	4 08	4 13	4 19	4 25	4 31	4 36	4 41	4 46	4 50	4 55
	S.	7 55	7 55	7 51	7 46	7 41	7 36	7 31	7 26	7 20	7 15
47	R.	4 04	4 09	4 16	4 22	4 28	4 33	4 38	4 43	4 48	4 52
	S.	8 00	7 59	7 55	7 50	7 45	7 39	7 34	7 28	7 23	7 17
48	R.	3 59	4 04	4 11	4 18	4 24	4 30	4 35	4 40	4 45	4 49
	S.	8 04	8 03	7 59	7 53	7 48	7 43	7 37	7 31	7 26	7 20
49	R.	3 55	4 00	4 07	4 14	4 21	4 26	4 32	4 37	4 42	4 47
	S.	8 09	8 08	8 03	7 57	7 52	7 46	7 41	7 35	7 29	7 23
50	R.	3 50	3 55	4 03	4 10	4 17	4 23	4 28	4 34	4 39	4 44
	S.	8 14	8 13	8 08	8 02	7 56	7 50	7 44	7 38	7 32	7 26
51	R.	3 44	3 50	3 58	4 05	4 12	4 19	4 25	4 30	4 36	4 41
	S.	8 19	8 18	8 12	8 06	8 00	7 54	7 48	7 41	7 35	7 29
52	R.	3 39	3 44	3 53	4 00	4 08	4 14	4 21	4 27	4 32	4 38
	S.	8 25	8 23	8 18	8 11	8 05	7 58	7 52	7 45	7 38	7 32
53	R.	3 33	3 38	3 47	3 55	4 03	4 10	4 17	4 23	4 29	4 35
	S.	8 31	8 29	8 23	8 16	8 10	8 03	7 56	7 49	7 42	7 35
54	R.	3 26	3 32	3 41	3 50	3 58	4 05	4 12	4 19	4 25	4 31
	S.	8 37	8 35	8 29	8 22	8 15	8 07	8 00	7 53	7 45	7 38
55	R.	3 19	3 25	3 35	3 44	3 53	4 00	4 08	4 15	4 21	4 28
	S.	8 44	8 42	8 35	8 27	8 20	8 12	8 05	7 57	7 49	7 42
56	R.	3 12	3 18	3 29	3 38	3 47	3 55	4 03	4 10	4 17	4 24
	S.	8 52	8 49	8 42	8 33	8 25	8 17	8 10	8 02	7 54	7 46
57	R.	3 04	3 11	3 22	3 31	3 41	3 49	3 58	4 05	4 12	4 19
	S.	9 00	8 57	8 49	8 40	8 32	8 23	8 15	8 06	7 58	7 50
58	R.	2 55	3 02	3 14	3 24	3 34	3 43	3 52	4 00	4 07	4 15
	S.	9 09	9 06	8 57	8 48	8 38	8 29	8 20	8 12	8 03	7 55
59	R.	2 45	2 53	3 05	3 16	3 27	3 37	3 46	3 54	4 02	4 10
	S.	9 18	9 15	9 05	8 55	8 45	8 36	8 26	8 17	8 08	8 00
60	R.	2 35	2 43	2 57	3 09	3 20	3 30	3 40	3 49	3 57	4 05
	S.	9 28	9 25	9 13	9 03	8 53	8 43	8 33	8 23	8 14	8 04

Lat. N.	AUGUST. 16	AUGUST. 19	AUGUST. 22	AUGUST. 25	AUGUST. 28	AUGUST. 30	SEPTEMBER. 2	SEPTEMBER. 5	SEPTEMBER. 8	SEPTEMBER. 10	SEPTEMBER. 13	SEPTEMBER. 16	SEPTEMBER. 18	SEPTEMBER. 21	SEPTEMBER. 23	Approx. date.	Lat. N.
	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. N.	
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
41	5 09	5 12	5 15	5 18	5 21	5 24	5 27	5 29	5 32	5 35	5 38	5 40	5 42	5 45	5 47	R.	41
	7 00	6 55	6 51	6 46	6 42	6 37	6 33	6 28	6 24	6 20	6 15	6 10	6 06	6 02	5 57	S.	
42	5 07	5 10	5 13	5 17	5 20	5 23	5 26	5 29	5 31	5 34	5 37	5 40	5 42	5 45	5 47	R.	42
	7 02	6 57	6 52	6 48	6 43	6 38	6 34	6 29	6 24	6 20	6 16	6 11	6 06	6 02	5 57	S.	
43	5 05	5 09	5 12	5 15	5 18	5 22	5 25	5 28	5 30	5 33	5 36	5 39	5 42	5 45	5 47	R.	43
	7 04	6 59	6 54	6 49	6 44	6 40	6 35	6 30	6 25	6 21	6 16	6 11	6 07	6 02	5 57	S.	
44	5 03	5 07	5 10	5 14	5 17	5 21	5 24	5 27	5 29	5 32	5 35	5 38	5 41	5 44	5 47	R.	44
	7 06	7 01	6 56	6 51	6 46	6 41	6 36	6 31	6 26	6 22	6 17	6 12	6 07	6 02	5 58	S.	
45	5 01	5 05	5 08	5 12	5 15	5 19	5 22	5 25	5 28	5 32	5 35	5 38	5 41	5 44	5 47	R.	45
	7 08	7 03	6 57	6 52	6 47	6 42	6 37	6 32	6 27	6 23	6 18	6 13	6 08	6 03	5 58	S.	
46	4 59	5 03	5 07	5 11	5 14	5 18	5 21	5 24	5 27	5 31	5 34	5 38	5 41	5 44	5 47	R.	46
	7 10	7 05	6 59	6 54	6 49	6 44	6 38	6 33	6 28	6 23	6 18	6 13	6 08	6 03	5 58	S.	
47	4 56	5 01	5 05	5 09	5 12	5 16	5 20	5 23	5 26	5 30	5 34	5 37	5 40	5 44	5 47	R.	47
	7 12	7 07	7 01	6 56	6 51	6 45	6 40	6 34	6 29	6 24	6 19	6 13	6 08	6 03	5 58	S.	
48	4 54	4 59	5 03	5 07	5 10	5 14	5 18	6 22	5 25	5 29	5 33	5 37	5 40	5 43	5 47	R.	48
	7 15	7 09	7 03	6 58	6 59	6 47	6 41	6 36	6 30	6 25	6 19	6 14	6 09	6 03	5 58	S.	
49	4 51	4 56	5 00	5 05	5 09	5 13	5 17	5 21	5 24	5 28	5 32	5 36	5 39	5 43	5 47	R.	49
	7 17	7 11	7 05	7 00	6 54	6 49	6 43	6 37	6 31	6 26	6 20	6 15	6 09	6 04	5 58	S.	
50	4 49	4 54	4 58	5 03	5 07	5 11	5 15	5 19	5 23	5 28	5 32	5 35	5 39	5 43	5 46	R.	50
	7 20	7 14	7 07	7 02	6 56	6 50	6 44	6 38	6 32	6 27	6 21	6 15	6 09	6 04	5 58	S.	
51	4 46	4 51	4 56	5 01	5 05	5 10	5 14	5 18	5 22	5 27	5 31	5 35	5 39	5 43	5 46	R.	51
	7 22	7 16	7 10	7 04	6 58	6 52	6 46	6 40	6 34	6 28	6 22	6 16	6 10	6 04	5 58	S.	
52	4 43	4 49	4 53	4 58	5 03	5 08	5 12	5 16	5 21	5 26	5 30	5 34	5 38	5 42	5 46	R.	52
	7 25	7 19	7 12	7 06	7 00	6 54	6 47	6 41	6 35	6 29	6 23	6 16	6 10	6 04	5 58	S.	
53	4 40	4 46	4 51	4 56	5 01	5 06	5 10	5 15	5 19	5 24	5 29	5 33	5 38	5 42	5 46	R.	53
	7 28	7 22	7 15	7 08	7 02	6 56	6 49	6 43	6 36	6 30	6 24	6 17	6 11	6 05	5 58	S.	
54	4 37	4 43	4 48	4 54	4 59	5 04	5 09	5 13	5 18	5 23	5 28	5 33	5 37	5 42	5 46	R.	54
	7 31	7 25	7 18	7 11	7 04	6 58	6 51	6 44	6 37	6 31	6 25	6 18	6 11	6 05	5 59	S.	
55	4 34	4 40	4 45	4 51	4 56	5 02	5 07	5 12	5 17	5 22	5 27	5 32	5 37	5 41	5 46	R.	55
	7 35	7 28	7 20	7 13	7 06	7 00	6 53	6 46	6 39	6 32	6 26	6 19	6 12	6 05	5 59	S.	
56	4 30	4 36	4 42	4 48	4 54	5 00	5 05	5 10	5 15	5 21	5 26	5 31	5 36	5 41	5 45	R.	56
	7 38	7 31	7 23	7 16	7 09	7 02	6 55	6 47	6 40	6 34	6 27	6 19	6 12	6 06	5 59	S.	
57	4 26	4 33	4 39	4 45	4 51	4 57	5 03	5 08	5 14	5 20	5 25	5 30	5 35	5 40	5 45	R.	57
	7 42	7 35	7 27	7 19	7 12	7 04	6 57	6 49	6 42	6 35	6 28	6 20	6 13	6 06	5 59	S.	
58	4 22	4 29	4 35	4 42	4 48	4 55	5 01	5 06	5 12	5 18	5 24	5 29	5 35	5 40	5 45	R.	58
	7 46	7 38	7 30	7 22	7 14	7 07	6 59	6 51	6 43	6 36	6 29	6 21	6 14	6 07	5 59	S.	
59	4 18	4 25	4 32	4 39	4 45	4 52	4 58	5 04	5 10	5 16	5 22	5 28	5 34	5 39	5 45	R.	59
	7 51	7 42	7 34	7 26	7 17	7 09	7 01	6 53	6 45	6 38	6 30	6 22	6 15	6 07	6 00	S.	
60	4 13	4 21	4 28	4 36	4 43	4 50	4 56	5 02	5 08	5 15	5 21	5 27	5 33	5 39	5 45	R.	60
	7 55	7 46	7 37	7 29	7 20	7 12	7 03	6 55	6 47	6 39	6 31	6 23	6 15	6 08	6 00	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 0° to 20°—September 23 to December 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	SEPTEMBER.			OCTOBER.												NOVEMBER.							DECEMBER.			Approx. date.	Lat. N.
		23	26	28	1	4	6	9	11	14	17	19	22	25	28	31	3	6	10	14	17	22	27	3	11	22		
	Dec. S.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. S.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
0	R.	5 49	5 48	5 47	5 46	5 45	5 44	5 44	5 43	5 42	5 42	5 41	5 41	5 40	5 40	5 40	5 40	5 40	5 40	5 40	5 41	5 42	5 44	5 46	5 49	5 54	R.	0
	S.	5 56	5 55	5 55	5 54	5 53	5 52	5 52	5 51	5 50	5 50	5 49	5 49	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 49	5 50	5 52	5 54	5 57	6 02	S.	
1	R.	5 49	5 48	5 47	5 46	5 46	5 45	5 44	5 43	5 43	5 43	5 42	5 42	5 41	5 41	5 41	5 41	5 41	5 41	5 42	5 43	5 44	5 45	5 47	5 51	5 56	R.	1
	S.	5 56	5 55	5 54	5 53	5 53	5 52	5 51	5 50	5 49	5 49	5 48	5 48	5 47	5 47	5 47	5 47	5 46	5 46	5 47	5 48	5 49	5 50	5 52	5 56	6 01	S.	
2	R.	5 49	5 48	5 47	5 46	5 46	5 45	5 45	5 44	5 44	5 43	5 43	5 42	5 42	5 41	5 42	5 42	5 42	5 42	5 43	5 44	5 45	5 47	5 49	5 52	5 57	R.	2
	S.	5 56	5 55	5 54	5 53	5 53	5 52	5 51	5 50	5 49	5 48	5 48	5 47	5 47	5 46	5 46	5 46	5 45	5 45	5 46	5 47	5 47	5 49	5 51	5 54	5 59	S.	
3	R.	5 49	5 48	5 47	5 46	5 46	5 45	5 45	5 44	5 44	5 44	5 43	5 43	5 43	5 42	5 43	5 43	5 43	5 43	5 44	5 45	5 47	5 48	5 50	5 54	5 59	R.	3
	S.	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 49	5 48	5 48	5 47	5 47	5 46	5 45	5 45	5 45	5 44	5 44	5 44	5 45	5 46	5 47	5 49	5 53	5 57	S.	
4	R.	5 49	5 48	5 47	5 47	5 46	5 45	5 45	5 45	5 45	5 44	5 44	5 44	5 44	5 43	5 44	5 44	5 44	5 44	5 45	5 47	5 48	5 50	5 52	5 55	6 01	R.	4
	S.	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 49	5 48	5 47	5 47	5 46	5 45	5 44	5 44	5 44	5 43	5 43	5 43	5 44	5 44	5 46	5 48	5 51	5 56	S.	
5	R.	5 49	5 48	5 47	5 47	5 47	5 46	5 46	5 45	5 45	5 45	5 45	5 45	5 45	5 44	5 45	5 45	5 46	5 46	5 47	5 48	5 50	5 51	5 54	5 57	6 03	R.	5
	S.	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 48	5 47	5 47	5 46	5 45	5 44	5 43	5 43	5 42	5 42	5 42	5 42	5 42	5 43	5 44	5 46	5 49	5 54	S.	
6	R.	5 48	5 48	5 47	5 47	5 47	5 46	5 46	5 46	5 46	5 45	5 45	5 45	5 45	5 45	5 46	5 46	5 47	5 47	5 48	5 49	5 51	5 53	5 55	5 59	6 04	R.	6
	S.	5 56	5 55	5 54	5 53	5 52	5 50	5 49	5 48	5 47	5 46	5 45	5 44	5 43	5 42	5 42	5 41	5 41	5 41	5 41	5 41	5 42	5 43	5 44	5 48	5 52	S.	
7	R.	5 48	5 48	5 48	5 47	5 47	5 47	5 47	5 46	5 46	5 46	5 46	5 46	5 46	5 46	5 47	5 47	5 48	5 48	5 49	5 51	5 52	5 54	5 57	6 01	6 06	R.	7
	S.	5 56	5 55	5 54	5 52	5 51	5 50	5 49	5 47	5 46	5 45	5 44	5 43	5 42	5 41	5 41	5 40	5 40	5 39	5 39	5 40	5 40	5 41	5 43	5 46	5 50	S.	
8	R.	5 48	5 48	5 48	5 47	5 47	5 47	5 47	5 47	5 47	5 47	5 47	5 47	5 47	5 47	5 48	5 48	5 49	5 49	5 50	5 52	5 54	5 56	5 58	6 02	6 08	R.	8
	S.	5 56	5 55	5 54	5 52	5 51	5 50	5 48	5 47	5 46	5 45	5 44	5 43	5 41	5 40	5 40	5 39	5 39	5 38	5 38	5 39	5 39	5 40	5 41	5 44	5 49	S.	
9	R.	5 48	5 48	5 48	5 48	5 48	5 47	5 47	5 47	5 48	5 48	5 48	5 48	5 48	5 48	5 49	5 49	5 50	5 51	5 52	5 53	5 55	5 57	6 00	6 04	6 10	R.	9
	S.	5 56	5 55	5 54	5 52	5 51	5 49	5 48	5 46	5 45	5 44	5 43	5 42	5 40	5 39	5 39	5 38	5 37	5 37	5 37	5 37	5 37	5 38	5 39	5 42	5 47	S.	
10	R.	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 49	5 49	5 50	5 50	5 51	5 52	5 53	5 55	5 57	5 59	6 02	6 06	6 11	R.	10
	S.	5 56	5 55	5 54	5 52	5 51	5 49	5 48	5 46	5 44	5 43	5 42	5 41	5 40	5 39	5 38	5 37	5 36	5 36	5 36	5 36	5 36	5 37	5 38	5 41	5 45	S.	
11	R.	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 49	5 49	5 49	5 49	5 50	5 50	5 51	5 51	5 52	5 53	5 54	5 56	5 58	6 00	6 03	6 08	6 13	R.	11
	S.	5 56	5 55	5 53	5 52	5 50	5 48	5 47	5 45	5 44	5 43	5 41	5 40	5 39	5 38	5 37	5 36	5 35	5 35	5 34	5 34	5 34	5 35	5 36	5 39	5 43	S.	
12	R.	5 48	5 48	5 48	5 48	5 49	5 49	5 49	5 49	5 49	5 49	5 50	5 50	5 51	5 51	5 52	5 52	5 53	5 54	5 56	5 58	6 00	6 02	6 05	6 09	6 15	R.	12
	S.	5 56	5 55	5 53	5 51	5 50	5 48	5 47	5 45	5 43	5 42	5 41	5 39	5 38	5 37	5 36	5 35	5 34	5 33	5 33	5 33	5 33	5 34	5 35	5 37	5 42	S.	
13	R.	5 48	5 48	5 49	5 49	5 49	5 49	5 49	5 49	5 50	5 50	5 51	5 51	5 52	5 52	5 53	5 54	5 55	5 56	5 57	5 59	6 01	6 04	6 07	6 11	6 17	R.	13
	S.	5 56	5 54	5 53	5 51	5 49	5 48	5 46	5 44	5 43	5 41	5 40	5 38	5 37	5 36	5 35	5 34	5 33	5 32	5 31	5 31	5 31	5 32	5 33	5 35	5 40	S.	
14	R.	5 48	5 48	5 49	5 49	5 49	5 49	5 50	5 50	5 50	5 51	5 51	5 52	5 52	5 53	5 54	5 55	5 56	5 57	5 59	6 01	6 03	6 05	6 08	6 13	6 18	R.	14
	S.	5 56	5 54	5 53	5 51	5 49	5 47	5 46	5 44	5 42	5 41	5 39	5 38	5 36	5 35	5 34	5 33	5 32	5 31	5 30	5 30	5 30	5 30	5 31	5 34	5 38	S.	
15	R.	5 48	5 48	5 49	5 49	5 50	5 50	5 50	5 50	5 51	5 51	5 52	5 52	5 53	5 54	5 55	5 56	5 57	5 58	6 00	6 02	6 04	6 07	6 10	6 15	6 20	R.	15
	S.	5 56	5 54	5 52	5 50	5 49	5 47	5 45	5 43	5 42	5 40	5 39	5 37	5 35	5 34	5 33	5 32	5 30	5 29	5 28	5 28	5 28	5 29	5 29	5 32	5 36	S.	
16	R.	5 48	5 48	5 49	5 49	5 50	5 50	5 51	5 51	5 51	5 52	5 53	5 53	5 54	5 55	5 56	5 57	5 58	6 00	6 02	6 04	6 06	6 08	6 12	6 17	6 22	R.	16
	S.	5 56	5 54	5 52	5 50	5 49	5 47	5 45	5 43	5 41	5 40	5 38	5 36	5 34	5 33	5 32	5 31	5 29	5 28	5 27	5 27	5 27	5 27	5 28	5 30	5 34	S.	
17	R.	5 48	5 48	5 49	5 49	5 50	5 50	5 51	5 51	5 52	5 53	5 53	5 54	5 55	5 56	5 57	5 58	6 00	6 01	6 03	6 05	6 08	6 10	6 14	6 19	6 24	R.	17
	S.	5 56	5 54	5 52	5 50	5 48	5 46	5 44	5 42	5 40	5 39	5 37	5 35	5 33	5 32	5 30	5 29	5 28	5 26	5 26	5 25	5 25	5 25	5 26	5 28	5 32	S.	
18	R.	5 48	5 48	5 49	5 49	5 50	5 50	5 51	5 52	5 53	5 53	5 54	5 55	5 56	5 57	5 58	5 59	6 01	6 02	6 04	6 07	6 09	6 12	6 15	6 20	6 26	R.	18
	S.	5 56	5 54	5 52	5 50	5 48	5 46	5 44	5 42	5 40	5 38	5 36	5 34	5 32	5 31	5 29	5 28	5 27	5 25	5 24	5 24	5 23	5 24	5 24	5 26	5 30	S.	
19	R.	5 48	5 48	5 49	5 50	5 51	5 51	5 52	5 52	5 53	5 54	5 55	5 56	5 57	5 58	5 59	6 01	6 02	6 04	6 06	6 08	6 11	6 14	6 17	6 22	6 28	R.	19
	S.	5 56	5 54	5 52	5 50	5 48	5 46	5 44	5 41	5 39	5 37	5 35	5 33	5 31	5 30	5 28	5 27	5 25	5 24	5 23	5 22	5 22	5 22	5 22	5 24	5 28	S.	
20	R.	5 48	5 48	5 49	5 50	5 51	5 51	5 52	5 53	5 54	5 55	5 56	5 57	5 58	5 59	6 00	6 02	6 03	6 05	6 07	6 10	6 12	6 15	6 19	6 24	6 30	R.	20
	S.	5 56	5 54	5 52	5 50	5 48	5 45	5 43	5 41	5 39	5 37	5 35	5 33	5 31	5 29	5 27	5 26	5 24	5 23	5 21	5 21	5 20	5 20	5 20	5 22	5 26	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 21° to 40°—September 23 to December 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	SEPTEMBER.			OCTOBER.											
		23	26	28	1	4	6	9	11	14	17	19	22	25	28	31
	Dec. S.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
21	R.	5 48	5 49	5 50	5 50	5 51	5 52	5 53	5 53	5 55	5 56	5 57	5 58	5 59	6 00	6 01
	S.	5 56	5 54	5 52	5 49	5 47	5 45	5 43	5 40	5 38	5 36	5 34	5 32	5 30	5 28	5 26
22	R.	5 48	5 49	5 50	5 50	5 51	5 52	5 53	5 54	5 55	5 56	5 57	5 58	6 00	6 01	6 02
	S.	5 56	5 54	5 52	5 49	5 47	5 45	5 42	5 40	5 37	5 35	5 33	5 31	5 29	5 27	5 25
23	R.	5 48	5 49	5 50	5 51	5 52	5 53	5 54	5 55	5 56	5 57	5 58	5 59	6 01	6 02	6 04
	S.	5 56	5 54	5 52	5 49	5 47	5 44	5 42	5 39	5 37	5 35	5 32	5 30	5 28	5 26	5 24
24	R.	5 48	5 49	5 50	5 51	5 52	5 53	5 54	5 55	5 56	5 57	5 59	6 00	6 02	6 03	6 05
	S.	5 56	5 54	5 52	5 49	5 46	5 44	5 41	5 39	5 36	5 34	5 32	5 29	5 27	5 25	5 23
25	R.	5 48	5 49	5 50	5 51	5 52	5 53	5 55	5 56	5 57	5 58	6 00	6 01	6 03	6 04	6 06
	S.	5 56	5 54	5 51	5 48	5 46	5 43	5 41	5 38	5 35	5 33	5 31	5 28	5 26	5 23	5 21
26	R.	5 48	5 49	5 50	5 51	5 53	5 54	5 55	5 56	5 58	5 59	6 00	6 02	6 04	6 05	6 07
	S.	5 56	5 54	5 51	5 48	5 46	5 43	5 40	5 37	5 35	5 33	5 30	5 28	5 25	5 22	5 20
27	R.	5 48	5 49	5 50	5 51	5 53	5 54	5 56	5 57	5 58	6 00	6 01	6 03	6 05	6 06	6 08
	S.	5 57	5 54	5 51	5 48	5 45	5 42	5 40	5 37	5 34	5 32	5 29	5 27	5 24	5 21	5 19
28	R.	5 48	5 49	5 51	5 52	5 53	5 54	5 56	5 57	5 59	6 00	6 02	6 04	6 06	6 07	6 09
	S.	5 57	5 54	5 51	5 48	5 45	5 42	5 39	5 36	5 34	5 31	5 28	5 26	5 23	5 20	5 18
29	R.	5 48	5 49	5 51	5 52	5 54	5 55	5 57	5 58	6 00	6 01	6 03	6 05	6 07	6 09	6 11
	S.	5 57	5 54	5 51	5 48	5 45	5 42	5 39	5 36	5 33	5 30	5 27	5 25	5 22	5 19	5 17
30	R.	5 48	5 49	5 51	5 52	5 54	5 55	5 57	5 58	6 00	6 02	6 04	6 06	6 08	6 10	6 12
	S.	5 57	5 54	5 51	5 48	5 45	5 41	5 38	5 35	5 32	5 30	5 27	5 24	5 21	5 18	5 15
31	R.	5 48	5 49	5 51	5 52	5 54	5 56	5 58	5 59	6 01	6 03	6 05	6 07	6 09	6 11	6 14
	S.	5 57	5 54	5 51	5 47	5 44	5 41	5 38	5 34	5 31	5 29	5 26	5 23	5 20	5 17	5 14
32	R.	5 48	5 49	5 51	5 52	5 54	5 56	5 58	6 00	6 02	6 04	6 06	6 08	6 10	6 12	6 15
	S.	5 57	5 54	5 51	5 47	5 43	5 40	5 37	5 34	5 31	5 28	5 25	5 22	5 19	5 16	5 13
33	R.	5 48	5 49	5 51	5 53	5 55	5 57	5 59	6 01	6 03	6 05	6 07	6 09	6 11	6 13	6 16
	S.	5 57	5 53	5 50	5 47	5 43	5 40	5 37	5 33	5 30	5 27	5 24	5 21	5 17	5 14	5 11
34	R.	5 48	5 49	5 51	5 53	5 55	5 57	5 59	6 01	6 03	6 05	6 08	6 10	6 12	6 15	6 18
	S.	5 57	5 53	5 50	5 47	5 43	5 39	5 36	5 33	5 29	5 26	5 23	5 20	5 16	5 13	5 10
35	R.	5 48	5 50	5 52	5 53	5 55	5 58	6 00	6 02	6 04	6 06	6 09	6 11	6 14	6 16	6 19
	S.	5 57	5 53	5 50	5 46	5 42	5 39	5 36	5 32	5 28	5 25	5 22	5 18	5 15	5 11	5 08
36	R.	5 48	5 50	5 52	5 54	5 56	5 58	6 00	6 02	6 05	6 07	6 10	6 12	6 15	6 17	6 21
	S.	5 57	5 53	5 50	5 46	5 42	5 38	5 35	5 31	5 28	5 24	5 21	5 17	5 14	5 10	5 07
37	R.	5 48	5 50	5 52	5 54	5 56	5 59	6 01	6 03	6 06	6 08	6 11	6 13	6 16	6 19	6 22
	S.	5 57	5 53	5 49	5 45	5 41	5 38	5 34	5 30	5 27	5 23	5 20	5 16	5 12	5 09	5 05
38	R.	5 47	5 50	5 52	5 54	5 56	5 59	6 02	6 04	6 06	6 09	6 12	6 14	6 17	6 20	6 24
	S.	5 57	5 53	5 49	5 45	5 41	5 37	5 34	5 30	5 26	5 22	5 19	5 15	5 11	5 07	5 04
39	R.	5 47	5 50	5 52	5 54	5 57	6 00	6 02	6 05	6 07	6 10	6 13	6 16	6 19	6 22	6 25
	S.	5 57	5 53	5 49	5 45	5 41	5 37	5 33	5 29	5 25	5 21	5 18	5 14	5 10	5 06	5 02
40	R.	5 47	5 50	5 52	5 55	5 57	6 00	6 03	6 06	6 08	6 11	6 14	6 17	6 20	6 23	6 27
	S.	5 57	5 53	5 49	5 45	5 40	5 36	5 32	5 28	5 24	5 20	5 17	5 13	5 08	5 04	5 01

Lat. N.	Approx. date.	NOVEMBER.							DECEMBER.			Approx. date.	Lat. N.
		3	6	10	14	17	22	27	3	11	22		
	Dec. S.	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. S.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
21	R.	6 03	6 05	6 06	6 09	6 11	6 14	6 17	6 21	6 26	6 32	R.	21
	S.	5 25	5 23	5 21	5 20	5 19	5 18	5 18	5 18	5 20	5 24	S.	
22	R.	6 04	6 06	6 08	6 10	6 13	6 16	6 19	6 23	6 28	6 31	R.	22
	S.	5 24	5 22	5 20	5 18	5 18	5 17	5 17	5 17	5 18	5 22	S.	
23	R.	6 05	6 07	6 09	6 12	6 14	6 17	6 21	6 25	6 30	6 36	R.	23
	S.	5 22	5 20	5 18	5 17	5 16	5 15	5 15	5 15	5 16	5 20	S.	
24	R.	6 07	6 09	6 11	6 13	6 16	6 19	6 22	6 27	6 32	6 38	R.	24
	S.	5 21	5 19	5 17	5 15	5 15	5 14	5 13	5 13	5 14	5 18	S.	
25	R.	6 08	6 10	6 12	6 15	6 18	6 21	6 24	6 29	6 34	6 40	R.	25
	S.	5 19	5 17	5 15	5 14	5 13	5 12	5 11	5 11	5 12	5 16	S.	
26	R.	6 09	6 11	6 13	6 16	6 19	6 22	6 26	6 31	6 36	6 42	R.	26
	S.	5 18	5 16	5 14	5 12	5 11	5 10	5 09	5 09	5 10	5 14	S.	
27	R.	6 10	6 13	6 15	6 18	6 21	6 24	6 28	6 33	6 39	6 45	R.	27
	S.	5 17	5 15	5 13	5 11	5 10	5 08	5 07	5 07	5 08	5 12	S.	
28	R.	6 12	6 14	6 16	6 19	6 23	6 26	6 30	6 35	6 41	6 47	R.	28
	S.	5 16	5 13	5 11	5 09	5 08	5 06	5 05	5 05	5 06	5 10	S.	
29	R.	6 13	6 16	6 18	6 21	6 25	6 28	6 32	6 37	6 43	6 49	R.	29
	S.	5 14	5 12	5 09	5 07	5 06	5 04	5 03	5 03	5 04	5 07	S.	
30	R.	6 15	6 17	6 20	6 23	6 26	6 30	6 34	6 39	6 45	6 51	R.	30
	S.	5 13	5 10	5 08	5 06	5 04	5 02	5 01	5 01	5 02	5 05	S.	
31	R.	6 16	6 19	6 21	6 24	6 28	6 32	6 36	6 41	6 47	6 54	R.	31
	S.	5 11	5 09	5 06	5 04	5 02	5 00	4 59	4 58	4 59	5 03	S.	
32	R.	6 17	6 20	6 23	6 26	6 30	6 34	6 38	6 43	6 50	6 56	R.	32
	S.	5 10	5 07	5 05	5 02	5 00	4 58	4 57	4 56	4 57	5 00	S.	
33	R.	6 19	6 22	6 25	6 28	6 32	6 36	6 41	6 46	6 52	6 59	R.	33
	S.	5 09	5 06	5 03	5 00	4 58	4 56	4 55	4 54	4 54	4 58	S.	
34	R.	6 20	6 23	6 26	6 30	6 34	6 38	6 43	6 48	6 55	7 01	R.	34
	S.	5 07	5 04	5 01	4 59	4 57	4 54	4 53	4 52	4 52	4 55	S.	
35	R.	6 22	6 25	6 28	6 32	6 36	6 40	6 45	6 50	6 57	7 04	R.	35
	S.	5 05	5 02	4 59	4 57	4 55	4 52	4 51	4 49	4 49	4 53	S.	
36	R.	6 24	6 27	6 30	6 34	6 38	6 42	6 47	6 53	7 00	7 06	R.	36
	S.	5 04	5 01	4 58	4 55	4 53	4 50	4 48	4 47	4 47	4 50	S.	
37	R.	6 25	6 29	6 32	6 36	6 40	6 45	6 50	6 55	7 02	7 09	R.	37
	S.	5 02	4 59	4 56	4 53	4 50	4 48	4 46	4 44	4 44	4 47	S.	
38	R.	6 27	6 30	6 34	6 38	6 42	6 47	6 52	6 58	7 05	7 12	R.	38
	S.	5 01	4 57	4 54	4 51	4 48	4 45	4 43	4 42	4 41	4 44	S.	
39	R.	6 29	6 32	6 36	6 40	6 45	6 50	6 55	7 01	7 08	7 15	R.	39
	S.	4 59	4 55	4 52	4 48	4 46	4 43	4 41	4 39	4 38	4 41	S.	
40	R.	6 30	6 34	6 38	6 42	6 47	6 52	6 57	7 03	7 11	7 18	R.	40
	S.	4 57	4 53	4 50	4 46	4 43	4 40	4 38	4 36	4 35	4 38	S.	

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 41° to 60°—September 23 to December 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	SEPTEMBER.			OCTOBER.												NOVEMBER.							DECEMBER.			Approx. date.	Lat. N.
		23	26	28	1	4	6	9	11	14	17	19	22	25	28	31	3	6	10	14	17	22	27	3	11	22		
	Dec. S.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. S.	
°		h. m.	h. m.	h. m.	h. m.	h. m	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
41	R.	5 47	5 50	5 53	5 55	5 58	6 01	6 04	6 06	6 09	6 12	6 15	6 18	6 22	6 25	6 29	6 32	6 36	6 40	6 45	6 50	6 55	7 00	7 06	7 14	7 21	R.	41
	S.	5 57	5 53	5 49	5 44	5 40	5 36	5 32	5 27	5 23	5 19	5 15	5 11	5 07	5 03	4 59	4 55	4 51	4 47	4 44	4 41	4 38	4 35	4 33	4 82	4 35	S.	
42	R.	5 47	5 50	5 53	5 55	5 58	6 01	6 04	6 07	6 10	6 13	6 16	6 20	6 23	6 26	6 30	6 34	6 38	6 42	6 47	6 52	6 57	7 03	7 09	7 17	7 24	R.	42
	S.	5 57	5 53	5 49	5 44	5 39	5 35	5 31	5 27	5 22	5 18	5 14	5 10	5 05	5 01	4 57	4 53	4 49	4 45	4 42	4 39	4 35	4 33	4 30	4 29	4 32	S.	
43	R.	5 47	5 50	5 53	5 56	5 59	6 02	6 05	6 08	6 11	6 14	6 18	6 21	6 25	6 28	6 32	6 36	6 40	6 44	6 49	6 54	7 00	7 06	7 12	7 20	7 28	R.	43
	S.	5 57	5 53	5 48	5 44	5 39	5 35	5 30	5 26	5 21	5 17	5 13	5 08	5 04	4 59	4 55	4 51	4 47	4 43	4 39	4 36	4 33	4 30	4 27	4 26	4 29	S.	
44	R.	5 47	5 50	5 53	5 56	5 59	6 02	6 06	6 09	6 12	6 16	6 19	6 23	6 26	6 30	6 34	6 38	6 42	6 47	6 52	6 57	7 03	7 09	7 15	7 24	7 31	R.	44
	S.	5 58	5 53	5 48	5 44	5 39	5 34	5 30	5 25	5 20	5 16	5 11	5 07	5 02	4 58	4 54	4 49	4 45	4 41	4 37	4 33	4 30	4 27	4 24	4 23	4 25	S.	
45	R.	5 47	5 50	5 53	5 56	5 59	6 03	6 06	6 09	6 13	6 17	6 20	6 24	6 28	6 31	6 36	6 40	6 45	6 49	6 54	7 00	7 06	7 12	7 19	7 27	7 35	R.	45
	S.	5 58	5 53	5 48	5 43	5 38	5 34	5 29	5 24	5 19	5 15	5 10	5 05	5 01	4 56	4 52	4 47	4 43	4 38	4 34	4 31	4 27	4 24	4 21	4 19	4 22	S.	
46	R.	5 47	5 50	5 53	5 56	6 00	6 03	6 07	6 10	6 14	6 18	6 22	6 26	6 29	6 33	6 38	6 42	6 47	6 52	6 57	7 03	7 09	7 15	7 22	7 31	7 38	R.	46
	S.	5 58	5 53	5 48	5 43	5 38	5 33	5 28	5 23	5 18	5 14	5 09	5 04	4 59	4 54	4 50	4 45	4 41	4 36	4 32	4 28	4 24	4 20	4 17	4 16	4 18	S.	
47	R.	5 47	5 50	5 54	5 57	6 01	6 04	6 08	6 11	6 15	6 19	6 23	6 27	6 31	6 35	6 40	6 44	6 49	6 54	7 00	7 06	7 12	7 19	7 26	7 35	7 42	R.	47
	S.	5 58	5 53	5 48	5 43	5 38	5 33	5 28	5 22	5 17	5 12	5 07	5 02	4 57	4 53	4 48	4 43	4 38	4 33	4 29	4 25	4 21	4 17	4 14	4 12	4 14	S.	
48	R.	5 47	5 50	5 54	5 57	6 01	6 05	6 09	6 12	6 16	6 20	6 25	6 29	6 33	6 37	6 42	6 47	6 52	6 57	7 03	7 09	7 15	7 22	7 30	7 39	7 46	R.	48
	S.	5 58	5 53	5 48	5 42	5 37	5 32	5 27	5 21	5 16	5 11	5 06	5 01	4 56	4 51	4 46	4 41	4 36	4 31	4 26	4 22	4 17	4 13	4 10	4 08	4 10	S.	
49	R.	5 47	5 50	5 54	5 58	6 02	6 05	6 09	6 13	6 18	6 22	6 26	6 30	6 35	6 39	6 44	6 49	6 55	7 00	7 06	7 12	7 19	7 26	7 34	7 43	7 51	R.	49
	S.	5 58	5 53	5 48	5 42	5 37	5 31	5 26	5 20	5 15	5 10	5 04	4 59	4 54	4 49	4 43	4 38	4 33	4 28	4 23	4 18	4 14	4 10	4 06	4 04	4 06	S.	
50	R.	5 46	5 50	5 54	5 58	6 02	6 06	6 10	6 14	6 19	6 23	6 28	6 32	6 37	6 41	6 47	6 52	6 57	7 03	7 09	7 16	7 23	7 30	7 38	7 47	7 55	R.	50
	S.	5 58	5 53	5 47	5 41	5 36	5 30	5 25	5 19	5 14	5 08	5 03	4 57	4 52	4 46	4 41	4 36	4 30	4 25	4 20	4 15	4 10	4 06	4 02	3 59	4 01	S.	
51	R.	5 46	5 50	5 55	5 59	6 03	6 07	6 11	6 16	6 20	6 25	6 29	6 34	6 39	6 44	6 49	6 55	7 00	7 06	7 12	7 19	7 26	7 34	7 42	7 52	8 00	R.	51
	S.	5 58	5 52	5 47	5 41	5 35	5 29	5 24	5 18	5 12	5 07	5 01	4 56	4 50	4 44	4 38	4 33	4 27	4 22	4 16	4 11	4 06	4 02	3 57	3 55	3 56	S.	
52	R.	5 46	5 50	5 55	5 59	6 04	6 08	6 12	6 17	6 21	6 26	6 31	6 36	6 41	6 46	6 52	6 57	7 03	7 09	7 16	7 23	7 30	7 38	7 47	7 57	8 05	R.	52
	S.	5 58	5 52	5 47	5 41	5 35	5 29	5 23	5 17	5 11	5 05	5 00	4 54	4 48	4 42	4 36	4 30	4 24	4 18	4 13	4 08	4 02	3 57	3 53	3 50	3 51	S.	
53	R.	5 46	5 50	5 55	5 59	6 04	6 09	6 13	6 18	6 23	6 28	6 33	6 38	6 43	6 48	6 54	7 00	7 06	7 13	7 19	7 27	7 35	7 43	7 52	8 02	8 11	R.	53
	S.	5 58	5 52	5 46	5 40	5 34	5 28	5 22	5 16	5 10	5 04	4 58	4 52	4 45	4 39	4 33	4 27	4 21	4 15	4 09	4 04	3 58	3 53	3 48	3 44	3 46	S.	
54	R.	5 46	5 50	5 55	6 00	6 05	6 09	6 14	6 19	6 24	6 29	6 35	6 40	6 45	6 51	6 57	7 03	7 10	7 16	7 23	7 31	7 39	7 48	7 57	8 08	8 16	R.	54
	S.	5 59	5 52	5 46	5 40	5 34	5 27	5 21	5 15	5 08	5 02	4 56	4 50	4 43	4 37	4 30	4 24	4 18	4 11	4 05	4 00	3 54	3 48	3 43	3 39	3 40	S.	
55	R.	5 46	5 50	5 55	6 00	6 05	6 10	6 15	6 20	6 26	6 31	6 37	6 42	6 48	6 54	7 00	7 07	7 13	7 20	7 27	7 35	7 44	7 53	8 02	8 13	8 22	R.	55
	S.	5 59	5 52	5 46	5 39	5 33	5 26	5 20	5 13	5 07	5 00	4 54	4 47	4 41	4 34	4 27	4 21	4 14	4 08	4 01	3 55	3 49	3 43	3 37	3 33	3 34	S.	
56	R.	5 45	5 50	5 56	6 01	6 06	6 11	6 17	6 22	6 27	6 33	6 39	6 45	6 51	6 57	7 03	7 10	7 17	7 24	7 32	7 40	7 49	7 58	8 08	8 20	8 29	R.	56
	S.	5 59	5 52	5 46	5 39	5 32	5 25	5 19	5 12	5 05	4 58	4 52	4 45	4 38	4 31	4 24	4 17	4 11	4 04	3 57	3 50	3 44	3 37	3 31	3 27	3 27	S.	
57	R.	5 45	5 50	5 56	6 01	6 06	6 12	6 18	6 23	6 29	6 35	6 41	6 47	6 53	7 00	7 07	7 14	7 21	7 28	7 36	7 45	7 54	8 04	8 14	8 27	8 36	R.	57
	S.	5 59	5 52	5 45	5 38	5 31	5 24	5 17	5 10	5 03	4 56	4 49	4 42	4 35	4 28	4 21	4 14	4 07	3 59	3 52	3 45	3 38	3 31	3 25	3 20	3 20	S.	
58	R.	5 45	5 50	5 56	6 02	6 07	6 13	6 19	6 25	6 31	6 37	6 43	6 50	6 56	7 03	7 10	7 17	7 25	7 33	7 41	7 50	8 00	8 10	8 21	8 34	8 44	R.	58
	S.	5 59	5 52	5 45	5 38	5 31	5 23	5 16	5 09	5 02	4 54	4 47	4 40	4 32	4 25	4 17	4 10	4 03	3 55	3 47	3 40	3 33	3 25	3 18	3 13	3 13	S.	
59	R.	5 45	5 51	5 57	6 02	6 08	6 14	6 21	6 27	6 33	6 39	6 46	6 52	6 59	7 06	7 14	7 21	7 29	7 38	7 47	7 56	8 06	8 17	8 28	8 42	8 52	R.	59
	S.	6 00	5 52	5 45	5 37	5 30	5 22	5 15	5 07	5 00	4 52	4 45	4 37	4 29	4 21	4 14	4 06	3 58	3 50	3 42	3 35	3 27	3 19	3 11	3 05	3 05	S.	
60	R.	5 45	5 51	5 57	6 03	6 09	6 16	6 22	6 28	6 35	6 42	6 48	6 55	7 02	7 10	7 18	7 26	7 34	7 43	7 52	8 02	8 13	8 24	8 36	8 51	9 01	R.	60
	S.	6 00	5 52	5 44	5 36	5 29	5 21	5 13	5 05	4 58	4 50	4 42	4 34	4 26	4 18	4 10	4 02	3 53	3 45	3 36	3 28	3 20	3 12	3 03	2 56	2 56	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 0° to 20°—December 22 to March 21.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	DECEMBER.	JANUARY.						FEBRUARY.									MARCH.									Approx. date.	Lat. N.
		22	2	10	16	21	25	29	2	5	9	12	15	18	20	23	26	1	3	6	8	11	13	16	18	21		
	Dec. S.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. S.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
0	R.	5 54	6 00	6 04	6 06	6 07	6 08	6 09	6 10	6 10	6 10	6 10	6 10	6 10	6 10	6 10	6 09	6 09	6 08	6 08	6 07	6 06	6 06	6 05	6 04	6 04	R.	0
	S.	6 02	6 08	6 12	6 14	6 15	6 16	6 17	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 17	6 17	6 16	6 16	6 15	6 14	6 14	6 13	6 12	6 11	S.	
1	R.	5 56	6 01	6 05	6 07	6 09	6 10	6 11	6 11	6 12	6 11	6 11	6 11	6 11	6 11	6 11	6 10	6 10	6 09	6 08	6 08	6 07	6 06	6 05	6 05	6 04	R.	1
	S.	6 01	6 06	6 10	6 12	6 14	6 15	6 16	6 16	6 17	6 17	6 17	6 17	6 17	6 17	6 17	6 16	6 16	6 16	6 15	6 15	6 14	6 13	6 12	6 12	6 11	S.	
2	R.	5 57	6 03	6 07	6 09	6 10	6 11	6 12	6 12	6 13	6 12	6 12	6 12	6 12	6 11	6 11	6 11	6 10	6 09	6 09	6 08	6 07	6 06	6 05	6 05	6 04	R.	2
	S.	5 59	6 05	6 09	6 11	6 12	6 14	6 15	6 15	6 16	6 16	6 16	6 17	6 17	6 16	6 16	6 16	6 15	6 15	6 15	6 15	6 14	6 13	6 12	6 12	6 11	S.	
3	R.	5 59	6 04	6 08	6 10	6 12	6 12	6 13	6 13	6 14	6 13	6 13	6 13	6 13	6 12	6 12	6 11	6 11	6 10	6 09	6 08	6 07	6 06	6 05	6 05	6 04	R.	3
	S.	5 57	6 03	6 07	6 09	6 11	6 12	6 13	6 14	6 15	6 15	6 15	6 16	6 16	6 16	6 16	6 15	6 15	6 15	6 14	6 14	6 13	6 13	6 12	6 12	6 11	S.	
4	R.	6 01	6 06	6 10	6 12	6 13	6 14	6 14	6 14	6 15	6 14	6 14	6 14	6 14	6 13	6 12	6 12	6 11	6 10	6 09	6 08	6 07	6 07	6 06	6 05	6 04	R.	4
	S.	5 56	6 02	6 06	6 08	6 09	6 11	6 12	6 13	6 14	6 14	6 14	6 15	6 15	6 15	6 15	6 15	6 14	6 14	6 14	6 14	6 13	6 13	6 12	6 12	6 11	S.	
5	R.	6 03	6 08	6 12	6 13	6 14	6 15	6 16	6 16	6 16	6 16	6 15	6 15	6 15	6 14	6 13	6 12	6 12	6 11	6 10	6 09	6 08	6 07	6 06	6 05	6 04	R.	5
	S.	5 54	6 00	6 04	6 06	6 08	6 09	6 11	6 12	6 12	6 13	6 13	6 14	6 14	6 14	6 14	6 14	6 14	6 14	6 14	6 14	6 13	6 13	6 12	6 12	6 11	S.	
6	R.	6 04	6 09	6 13	6 15	6 16	6 16	6 17	6 17	6 17	6 17	6 16	6 16	6 15	6 14	6 14	6 13	6 12	6 11	6 10	6 09	6 08	6 07	6 06	6 05	6 03	R.	6
	S.	5 52	5 58	6 02	6 05	6 07	6 08	6 10	6 11	6 11	6 12	6 12	6 13	6 13	6 13	6 14	6 14	6 13	6 13	6 13	6 13	6 13	6 13	6 12	6 12	6 11	S.	
7	R.	6 06	6 11	6 15	6 16	6 17	6 18	6 18	6 18	6 18	6 18	6 17	6 17	6 16	6 15	6 15	6 14	6 13	6 12	6 11	6 10	6 08	6 07	6 06	6 05	6 03	R.	7
	S.	5 50	5 56	6 01	6 03	6 05	6 07	6 08	6 09	6 10	6 11	6 11	6 12	6 12	6 12	6 13	6 13	6 13	6 13	6 13	6 13	6 12	6 12	6 12	6 12	6 11	S.	
8	R.	6 08	6 13	6 16	6 18	6 19	6 19	6 19	6 19	6 19	6 19	6 18	6 18	6 17	6 16	6 15	6 14	6 13	6 12	6 11	6 10	6 08	6 07	6 06	6 05	6 03	R.	8
	S.	5 49	5 55	5 59	6 02	6 04	6 06	6 07	6 08	6 09	6 10	6 10	6 11	6 11	6 12	6 12	6 12	6 12	6 12	6 13	6 13	6 12	6 12	6 12	6 12	6 11	S.	
9	R.	6 10	6 15	6 18	6 19	6 20	6 20	6 21	6 21	6 21	6 20	6 19	6 19	6 18	6 17	6 16	6 15	6 14	6 13	6 11	6 10	6 09	6 07	6 06	6 05	6 03	R.	9
	S.	5 47	5 53	5 57	6 00	6 02	6 04	6 06	6 07	6 08	6 09	6 09	6 10	6 10	6 11	6 11	6 11	6 11	6 12	6 12	6 12	6 12	6 12	6 12	6 12	6 11	S.	
10	R.	6 11	6 16	6 20	6 21	6 22	6 22	6 22	6 22	6 22	6 21	6 20	6 19	6 19	6 18	6 17	6 16	6 15	6 13	6 12	6 11	6 09	6 07	6 06	6 05	6 03	R.	10
	S.	5 45	5 51	5 56	5 59	6 01	6 03	6 05	6 06	6 07	6 08	6 08	6 09	6 10	6 10	6 11	6 11	6 11	6 11	6 12	6 12	6 12	6 12	6 12	6 12	6 11	S.	
11	R.	6 13	6 18	6 21	6 22	6 23	6 23	6 23	6 23	6 23	6 22	6 21	6 20	6 20	6 19	6 18	6 16	6 15	6 14	6 12	6 11	6 09	6 08	6 06	6 05	6 03	R.	11
	S.	5 43	5 49	5 54	5 57	5 59	6 01	6 03	6 05	6 06	6 07	6 07	6 08	6 09	6 09	6 10	6 10	6 10	6 11	6 11	6 11	6 11	6 12	6 12	6 12	6 11	S.	
12	R.	6 15	6 20	6 23	6 24	6 25	6 25	6 25	6 24	6 24	6 23	6 22	6 21	6 21	6 19	6 18	6 17	6 16	6 14	6 13	6 11	6 10	6 08	6 06	6 05	6 03	R.	12
	S.	5 42	5 48	5 53	5 56	5 58	6 00	6 02	6 03	6 05	6 06	6 06	6 07	6 08	6 08	6 09	6 10	6 10	6 10	6 11	6 11	6 11	6 11	6 11	6 12	6 11	S.	
13	R.	6 17	6 22	6 25	6 26	6 26	6 26	6 26	6 26	6 25	6 24	6 23	6 22	6 22	6 20	6 19	6 18	6 16	6 15	6 13	6 12	6 10	6 09	6 07	6 05	6 03	R.	13
	S.	5 40	5 46	5 51	5 54	5 56	5 58	6 00	6 02	6 03	6 04	6 05	6 06	6 07	6 07	6 08	6 09	6 09	6 10	6 10	6 11	6 11	6 11	6 11	6 11	6 11	S.	
14	R.	6 18	6 23	6 26	6 27	6 28	6 28	6 28	6 27	6 26	6 25	6 24	6 23	6 22	6 21	6 20	6 18	6 17	6 15	6 14	6 12	6 10	6 09	6 07	6 05	6 03	R.	14
	S.	5 38	5 44	5 49	5 52	5 55	5 57	5 59	6 01	6 02	6 03	6 04	6 05	6 06	6 07	6 08	6 08	6 09	6 09	6 10	6 10	6 10	6 11	6 11	6 11	6 11	S.	
15	R.	6 20	6 25	6 28	6 29	6 29	6 29	6 29	6 28	6 28	6 26	6 25	6 24	6 23	6 21	6 20	6 19	6 17	6 16	6 14	6 13	6 11	6 09	6 07	6 05	6 03	R.	15
	S.	5 36	5 42	5 47	5 51	5 53	5 55	5 57	5 59	6 01	6 02	6 03	6 04	6 05	6 06	6 07	6 08	6 08	6 09	6 09	6 10	6 10	6 10	6 11	6 11	6 11	S.	
16	R.	6 22	6 27	6 30	6 30	6 31	6 31	6 30	6 30	6 29	6 27	6 26	6 25	6 24	6 22	6 21	6 19	6 18	6 16	6 15	6 13	6 11	6 09	6 07	6 05	6 03	R.	16
	S.	5 34	5 40	5 46	5 49	5 52	5 54	5 56	5 58	6 00	6 01	6 02	6 03	6 04	6 05	6 06	6 07	6 08	6 08	6 09	6 10	6 10	6 10	6 11	6 11	6 11	S.	
17	R.	6 24	6 29	6 32	6 32	6 33	6 32	6 32	6 31	6 30	6 29	6 28	6 26	6 25	6 23	6 22	6 20	6 19	6 17	6 15	6 13	6 11	6 09	6 07	6 05	6 03	R.	17
	S.	5 32	5 38	5 44	5 47	5 50	5 52	5 55	5 56	5 58	6 00	6 01	6 02	6 03	6 04	6 05	6 06	6 07	6 08	6 08	6 09	6 09	6 10	6 10	6 11	6 11	S.	
18	R.	6 26	6 31	6 33	6 34	6 34	6 34	6 33	6 32	6 31	6 30	6 29	6 27	6 26	6 24	6 23	6 21	6 19	6 17	6 15	6 13	6 11	6 09	6 07	6 05	6 03	R.	18
	S.	5 30	5 37	5 42	5 46	5 48	5 51	5 53	5 55	5 57	5 59	6 00	6 01	6 02	6 03	6 04	6 05	6 06	6 07	6 08	6 09	6 09	6 10	6 10	6 11	6 11	S.	
19	R.	6 28	6 33	6 35	6 36	6 36	6 35	6 35	6 34	6 33	6 31	6 30	6 28	6 27	6 25	6 24	6 22	6 20	6 18	6 16	6 14	6 12	6 10	6 07	6 05	6 03	R.	19
	S.	5 28	5 35	5 40	5 44	5 47	5 49	5 52	5 54	5 56	5 57	5 59	6 00	6 01	6 02	6 04	6 05	6 06	6 07	6 08	6 09	6 09	6 10	6 10	6 11	6 11	S.	
20	R.	6 30	6 35	6 37	6 37	6 37	6 37	6 36	6 35	6 34	6 32	6 31	6 29	6 28	6 26	6 24	6 22	6 20	6 18	6 16	6 14	6 12	6 10	6 07	6 05	6 03	R.	20
	S.	5 26	5 33	5 38	5 42	5 45	5 48	5 50	5 53	5 55	5 56	5 58	5 59	6 01	6 02	6 03	6 04	6 05	6 06	6 07	6 08	6 09	6 10	6 10	6 11	6 11	S.	

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 21° to 40°—December 22 to March 21.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	DECEMBER.	JANUARY.						FEBRUARY.									MARCH.									Approx. date.	Lat. N.
		22	2	10	16	21	25	29	2	5	9	12	15	18	20	23	26	1	3	6	8	11	13	16	18	21		
	Dec. S.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. S.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
21	R.	6 32	6 37	6 39	6 39	6 39	6 38	6 37	6 36	6 35	6 33	6 32	6 30	6 29	6 27	6 25	6 23	6 21	6 19	6 17	6 15	6 12	6 10	6 08	6 06	6 03	R.	21
	S.	5 24	5 31	5 36	5 40	5 43	5 46	5 49	5 51	5 53	5 55	5 57	5 58	6 00	6 01	6 02	6 03	6 04	6 06	6 07	6 08	6 08	6 09	6 10	6 11	6 11	S.	
22	R.	6 34	6 39	6 41	6 41	6 41	6 40	6 39	6 38	6 36	6 34	6 33	6 31	6 30	6 28	6 26	6 24	6 22	6 19	6 17	6 15	6 12	6 10	6 08	6 06	6 03	R.	22
	S.	5 22	5 29	5 35	5 39	5 42	5 45	5 47	5 50	5 52	5 54	5 56	5 57	5 59	6 00	6 02	6 03	6 04	6 05	6 06	6 08	6 08	6 09	6 10	6 11	6 11	S.	
23	R.	6 36	6 41	6 43	6 43	6 42	6 41	6 41	6 39	6 38	6 36	6 34	6 32	6 31	6 28	6 27	6 24	6 22	6 20	6 18	6 15	6 13	6 10	6 08	6 06	6 03	R.	23
	S.	5 20	5 27	5 33	5 37	5 40	5 43	5 46	5 48	5 51	5 53	5 54	5 56	5 58	5 59	6 01	6 02	6 03	6 05	6 06	6 07	6 08	6 09	6 10	6 11	6 11	S.	
24	R.	6 38	6 43	6 45	6 44	6 44	6 43	6 42	6 41	6 39	6 37	6 35	6 33	6 32	6 29	6 27	6 25	6 23	6 20	6 18	6 16	6 13	6 11	6 08	6 06	6 03	R.	24
	S.	5 18	5 25	5 31	5 35	5 39	5 42	5 44	5 47	5 49	5 51	5 53	5 55	5 57	5 58	6 00	6 02	6 03	6 04	6 05	6 07	6 08	6 09	6 10	6 11	6 11	S.	
25	R.	6 40	6 45	6 47	6 46	6 46	6 45	6 44	6 42	6 41	6 39	6 37	6 35	6 33	6 30	6 28	6 26	6 24	6 21	6 19	6 16	6 13	6 11	6 08	6 06	6 03	R.	25
	S.	5 16	5 23	5 29	5 33	5 37	5 40	5 43	5 45	5 48	5 50	5 52	5 54	5 56	5 57	5 59	6 01	6 02	6 03	6 05	6 06	6 07	6 08	6 09	6 10	6 11	S.	
26	R.	6 42	6 47	6 49	6 48	6 47	6 46	6 45	6 43	6 42	6 40	6 38	6 36	6 34	6 31	6 29	6 26	6 24	6 22	6 19	6 17	6 14	6 11	6 08	6 06	6 03	R.	26
	S.	5 14	5 21	5 27	5 31	5 35	5 38	5 41	5 44	5 47	5 49	5 51	5 53	5 55	5 57	5 59	6 00	6 01	6 03	6 04	6 06	6 07	6 08	6 09	6 10	6 11	S.	
27	R.	6 45	6 49	6 51	6 50	6 49	6 48	6 47	6 45	6 43	6 41	6 39	6 37	6 35	6 32	6 30	6 27	6 25	6 22	6 20	6 17	6 14	6 11	6 08	6 06	6 03	R.	27
	S.	5 12	5 18	5 25	5 29	5 33	5 37	5 40	5 43	5 45	5 48	5 50	5 52	5 54	5 56	5 58	5 59	6 01	6 02	6 04	6 05	6 06	6 08	6 09	6 10	6 11	S.	
28	R.	6 47	6 51	6 53	6 52	6 51	6 50	6 48	6 46	6 45	6 42	6 40	6 38	6 36	6 33	6 31	6 28	6 25	6 23	6 20	6 17	6 14	6 12	6 09	6 06	6 03	R.	28
	S.	5 10	5 16	5 23	5 27	5 31	5 35	5 38	5 41	5 44	5 46	5 49	5 51	5 53	5 55	5 57	5 59	6 00	6 02	6 03	6 05	6 06	6 08	6 09	6 10	6 11	S.	
29	R.	6 49	6 53	6 55	6 54	6 53	6 52	6 50	6 48	6 46	6 44	6 41	6 39	6 37	6 34	6 32	6 29	6 26	6 23	6 21	6 18	6 15	6 12	6 09	6 06	6 03	R.	29
	S.	5 07	5 14	5 21	5 25	5 29	5 33	5 36	5 39	5 42	5 45	5 47	5 50	5 52	5 54	5 56	5 58	5 59	6 01	6 03	6 05	6 06	6 08	6 09	6 10	6 11	S.	
30	R.	6 51	6 55	6 57	6 56	6 55	6 53	6 52	6 50	6 48	6 45	6 43	6 40	6 38	6 35	6 32	6 29	6 27	6 24	6 21	6 18	6 15	6 12	6 09	6 06	6 03	R.	30
	S.	5 05	5 12	5 19	5 23	5 27	5 31	5 35	5 38	5 41	5 43	5 46	5 48	5 51	5 53	5 55	5 57	5 59	6 01	6 02	6 04	6 06	6 08	6 09	6 10	6 12	S.	
31	R.	6 54	6 58	6 59	6 58	6 57	6 55	6 53	6 51	6 49	6 47	6 44	6 41	6 39	6 36	6 33	6 30	6 28	6 25	6 22	6 19	6 15	6 12	6 09	6 06	6 03	R.	31
	S.	5 03	5 10	5 16	5 21	5 25	5 29	5 33	5 36	5 39	5 42	5 44	5 47	5 50	5 52	5 54	5 56	5 58	6 00	6 02	6 04	6 05	6 07	6 09	6 10	6 12	S.	
32	R.	6 56	7 00	7 01	7 00	6 59	6 57	6 55	6 53	6 51	6 48	6 45	6 42	6 40	6 37	6 34	6 31	6 28	6 25	6 22	6 19	6 16	6 12	6 09	6 06	6 03	R.	32
	S.	5 00	5 07	5 14	5 19	5 23	5 27	5 31	5 35	5 38	5 41	5 43	5 46	5 49	5 51	5 58	5 55	5 57	5 59	6 01	6 03	6 05	6 07	6 09	6 10	6 12	S.	
33	R.	6 59	7 03	7 04	7 03	7 01	6 59	6 57	6 55	6 52	6 49	6 47	6 44	6 41	6 38	6 35	6 32	6 29	6 26	6 23	6 20	6 16	6 13	6 09	6 06	6 03	R.	33
	S.	4 58	5 05	5 12	5 17	5 21	5 25	5 29	5 33	5 36	5 39	5 42	5 45	5 47	5 50	5 52	5 54	5 56	5 59	6 01	6 03	6 05	6 07	6 08	6 10	6 12	S.	
34	R.	7 01	7 05	7 06	7 05	7 03	7 01	6 59	6 56	6 54	6 51	6 48	6 45	6 42	6 39	6 36	6 33	6 30	6 26	6 23	6 20	6 16	6 13	6 09	6 06	6 03	R.	34
	S.	4 55	5 02	5 10	5 15	5 19	5 24	5 28	5 31	5 35	5 38	5 40	5 43	5 46	5 49	5 51	5 54	5 56	5 58	6 00	6 02	6 04	6 06	6 08	6 10	6 12	S.	
35	R.	7 04	7 08	7 08	7 07	7 05	7 03	7 01	6 58	6 56	6 53	6 50	6 47	6 44	6 40	6 37	6 34	6 31	6 27	6 24	6 21	6 17	6 13	6 10	6 06	6 03	R.	35
	S.	4 53	5 00	5 07	5 13	5 17	5 22	5 26	5 29	5 33	5 36	5 39	5 42	5 45	5 47	5 50	5 53	5 55	5 57	6 00	6 02	6 04	6 06	6 08	6 10	6 12	S.	
36	R.	7 06	7 10	7 11	7 09	7 07	7 05	7 03	7 00	6 57	6 54	6 51	6 48	6 45	6 41	6 38	6 35	6 31	6 28	6 24	6 21	6 17	6 14	6 10	6 06	6 03	R.	36
	S.	4 50	4 57	5 05	5 10	5 15	5 20	5 24	5 28	5 31	5 34	5 37	5 41	5 44	5 46	5 49	5 52	5 54	5 57	5 59	6 01	6 03	6 06	6 08	6 10	6 12	S.	
37	R.	7 09	7 13	7 13	7 12	7 10	7 07	7 05	7 02	6 59	6 56	6 53	6 49	6 46	6 42	6 39	6 36	6 32	6 29	6 25	6 22	6 18	6 14	6 10	6 06	6 03	R.	37
	S	4 47	4 55	5 02	5 08	5 13	5 17	5 22	5 26	5 29	5 33	5 36	5 39	5 42	5 45	5 48	5 51	5 53	5 56	5 58	6 01	6 03	6 05	6 07	6 10	6 12	S.	
38	R.	7 12	7 16	7 16	7 14	7 12	7 09	7 07	7 04	7 01	6 57	6 54	6 51	6 47	6 43	6 40	6 36	6 33	6 29	6 26	6 22	6 18	6 14	6 10	6 06	6 02	R.	38
	S.	4 44	4 52	5 00	5 05	5 10	5 15	5 20	5 24	5 28	5 31	5 34	5 38	5 41	5 44	5 47	5 50	5 53	5 55	5 58	6 00	6 03	6 05	6 07	6 10	6 12	S.	
39	R.	7 15	7 19	7 19	7 17	7 15	7 12	7 09	7 06	7 03	6 59	6 56	6 52	6 49	6 45	6 41	6 37	6 34	6 30	6 26	6 23	6 18	6 14	6 10	6 06	6 02	R.	39
	S.	4 41	4 49	4 57	5 03	5 08	5 13	5 17	5 22	5 26	5 29	5 33	5 36	5 40	5 43	5 46	5 49	5 52	5 54	5 57	6 00	6 02	6 05	6 07	6 10	6 12	S.	
40	R.	7 18	7 22	7 21	7 19	7 17	7 14	7 11	7 08	7 05	7 01	6 57	6 54	6 50	6 46	6 42	6 38	6 35	6 31	6 27	6 23	6 19	6 15	6 10	6 06	6 02	R.	40
	S.	4 38	4 46	4 54	5 00	5 05	5 10	5 15	5 20	5 24	5 28	5 31	5 35	5 38	5 41	5 45	5 48	5 51	5 53	5 56	5 59	6 02	6 05	6 07	6 10	6 12	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

North Latitude: 41° to 60°—December 22 to March 21.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. N.	Approx. date.	DECEMBER.	JANUARY.						FEBRUARY.									MARCH.								
		22	2	10	16	21	25	29	2	5	9	12	15	18	20	23	26	1	3	6	8	11	13	16	18	21
	Dec. S.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
41	R.	7 21	7 25	7 24	7 22	7 20	7 17	7 14	7 10	7 07	7 03	6 59	6 55	6 52	6 48	6 44	6 40	6 36	6 32	6 28	6 24	6 19	6 15	6 11	6 07	6 02
	S.	4 35	4 43	4 51	4 57	5 03	5 08	5 13	5 17	5 22	5 26	5 29	5 33	5 37	5 40	5 44	5 47	5 50	5 53	5 56	5 59	6 01	6 04	6 07	6 10	6 12
42	R.	7 24	7 28	7 27	7 25	7 22	7 19	7 16	7 12	7 09	7 05	7 01	6 57	6 53	6 49	6 45	6 41	6 37	6 32	6 28	6 24	6 20	6 15	6 11	6 07	6 02
	S.	4 32	4 40	4 48	4 55	5 00	5 06	5 11	5 15	5 20	5 24	5 28	5 32	5 35	5 39	5 43	5 46	5 49	5 52	5 55	5 58	6 01	6 04	6 07	6 10	6 12
43	R.	7 28	7 31	7 30	7 28	7 25	7 21	7 18	7 14	7 11	7 07	7 03	6 59	6 55	6 50	6 46	6 42	6 38	6 33	6 29	6 25	6 20	6 16	6 11	6 07	6 02
	S.	4 29	4 37	4 45	4 52	4 58	5 03	5 08	5 13	5 18	5 22	5 26	5 30	5 34	5 37	5 41	5 45	5 48	5 51	5 54	5 58	6 01	6 04	6 07	6 10	6 12
44	R.	7 31	7 34	7 33	7 31	7 28	7 24	7 21	7 17	7 13	7 09	7 04	7 00	6 56	6 52	6 48	6 43	6 39	6 34	6 30	6 25	6 20	6 16	6 11	6 07	6 02
	S.	4 25	4 33	4 42	4 49	4 55	5 00	5 06	5 11	5 16	5 20	5 24	5 28	5 32	5 36	5 40	5 43	5 47	5 50	5 54	5 57	6 00	6 03	6 06	6 10	6 13
45	R.	7 35	7 38	7 37	7 34	7 31	7 27	7 23	7 19	7 15	7 11	7 06	7 02	6 58	6 53	6 49	6 44	6 40	6 35	6 30	6 26	6 21	6 16	6 11	6 07	6 02
	S.	4 22	4 30	4 39	4 46	4 52	4 58	5 03	5 08	5 13	5 18	5 22	5 27	5 31	5 35	5 39	5 42	5 46	5 50	5 53	5 57	6 00	6 03	6 06	6 10	6 13
46	R.	7 38	7 41	7 40	7 37	7 34	7 30	7 26	7 22	7 17	7 13	7 08	7 04	6 59	6 55	6 50	6 45	6 41	6 36	6 31	6 26	6 21	6 16	6 11	6 07	6 02
	S.	4 18	4 26	4 35	4 42	4 49	4 55	5 01	5 06	5 11	5 16	5 20	5 25	5 29	5 33	5 37	5 41	5 45	5 49	5 52	5 56	5 59	6 03	6 06	6 10	6 13
47	R.	7 42	7 45	7 44	7 41	7 37	7 33	7 29	7 24	7 20	7 15	7 10	7 06	7 01	6 56	6 52	6 47	6 42	6 37	6 32	6 27	6 22	6 17	6 12	6 07	6 02
	S.	4 14	4 22	4 32	4 39	4 46	4 52	4 58	5 03	5 09	5 14	5 18	5 23	5 27	5 31	5 36	5 40	5 44	5 48	5 52	5 56	5 59	6 03	6 06	6 10	6 13
48	R.	7 46	7 49	7 48	7 44	7 40	7 36	7 32	7 27	7 22	7 17	7 12	7 08	7 03	6 58	6 53	6 48	6 43	6 38	6 33	6 28	6 22	6 17	6 12	6 07	6 02
	S.	4 10	4 18	4 28	4 35	4 42	4 49	4 55	5 01	5 06	5 11	5 16	5 21	5 26	5 30	5 34	5 39	5 43	5 47	5 51	5 55	5 58	6 02	6 06	6 10	6 13
49	R.	7 51	7 53	7 52	7 48	7 44	7 39	7 35	7 30	7 25	7 20	7 15	7 10	7 05	6 59	6 54	6 49	6 44	6 39	6 33	6 28	6 23	6 18	6 12	6 07	6 01
	S.	4 06	4 14	4 24	4 32	4 39	4 45	4 52	4 58	5 03	5 09	5 14	5 19	5 24	5 28	5 33	5 37	5 41	5 46	5 50	5 54	5 58	6 02	6 06	6 10	6 13
50	R.	7 55	7 58	7 56	7 52	7 48	7 43	7 38	7 33	7 28	7 22	7 17	7 12	7 07	7 01	6 56	6 51	6 45	6 40	6 34	6 29	6 23	6 18	6 12	6 07	6 01
	S.	4 01	4 10	4 20	4 28	4 35	4 42	4 49	4 55	5 01	5 06	5 11	5 17	5 22	5 26	5 31	5 36	5 40	5 45	5 49	5 53	5 57	6 01	6 05	6 10	6 13
51	R.	8 00	8 02	8 00	7 56	7 51	7 46	7 41	7 36	7 31	7 25	7 20	7 14	7 09	7 03	6 58	6 52	6 47	6 41	6 35	6 30	6 24	6 19	6 13	6 07	6 01
	S.	3 56	4 05	4 15	4 24	4 31	4 38	4 45	4 52	4 58	5 03	5 09	5 14	5 20	5 25	5 30	5 34	5 39	5 43	5 48	5 52	5 56	6 01	6 05	6 09	6 13
52	R.	8 05	8 07	8 05	8 00	7 55	7 50	7 45	7 39	7 34	7 28	7 22	7 16	7 11	7 05	6 59	6 54	6 48	6 42	6 36	6 31	6 25	6 19	6 13	6 07	6 01
	S.	3 51	4 00	4 11	4 19	4 27	4 35	4 42	4 48	4 55	5 01	5 06	5 12	5 18	5 23	5 28	5 33	5 38	5 42	5 47	5 52	5 56	6 01	6 05	6 09	6 13
53	R.	8 11	8 13	8 10	8 05	7 59	7 54	7 48	7 43	7 37	7 31	7 25	7 19	7 13	7 07	7 01	6 55	6 49	6 43	6 37	6 31	6 25	6 19	6 13	6 07	6 01
	S.	3 46	3 55	4 06	4 15	4 23	4 31	4 38	4 45	4 52	4 58	5 04	5 10	5 15	5 21	5 26	5 31	5 36	5 41	5 46	5 51	5 56	6 00	6 04	6 09	6 13
54	R.	8 16	8 18	8 15	8 09	8 04	7 58	7 52	7 46	7 40	7 34	7 28	7 21	7 15	7 09	7 03	6 57	6 51	6 44	6 38	6 32	6 26	6 20	6 13	6 07	6 01
	S.	3 40	3 49	4 01	4 10	4 19	4 27	4 34	4 41	4 48	4 55	5 01	5 07	5 13	5 19	5 24	5 30	5 35	5 40	5 45	5 50	5 55	6 00	6 04	6 09	6 14
55	R.	8 22	8 24	8 20	8 15	8 09	8 02	7 56	7 50	7 44	7 37	7 31	7 24	7 18	7 11	7 05	6 59	6 52	6 46	6 40	6 33	6 27	6 20	6 13	6 07	6 01
	S.	3 34	3 44	3 55	4 05	4 14	4 22	4 30	4 38	4 45	4 51	4 58	5 04	5 11	5 16	5 22	5 28	5 33	5 39	5 44	5 49	5 54	5 59	6 04	6 09	6 14
56	R.	8 29	8 30	8 26	8 20	8 14	8 07	8 01	7 54	7 47	7 41	7 34	7 27	7 21	7 14	7 07	7 01	6 54	6 47	6 41	6 34	6 27	6 21	6 14	6 07	6 01
	S.	3 27	3 37	3 49	3 59	4 08	4 17	4 26	4 34	4 41	4 48	4 55	5 01	5 08	5 14	5 20	5 26	5 32	5 37	5 43	5 48	5 53	5 59	6 04	6 09	6 14
57	R.	8 36	8 37	8 32	8 26	8 19	8 12	8 05	7 58	7 51	7 44	7 37	7 30	7 23	7 16	7 10	7 03	6 56	6 49	6 42	6 35	6 28	6 21	6 14	6 07	6 00
	S.	3 20	3 30	3 43	3 54	4 03	4 12	4 21	4 29	4 37	4 44	4 51	4 58	5 05	5 11	5 18	5 24	5 80	5 36	5 41	5 47	5 52	5 58	6 03	6 09	6 14
58	R.	8 44	8 44	8 39	8 32	8 25	8 17	8 10	8 03	7 55	7 48	7 41	7 33	7 26	7 19	7 12	7 05	6 57	6 50	6 43	6 36	6 29	6 22	6 14	6 07	6 00
	S.	3 13	3 23	3 36	3 47	3 57	4 07	4 16	4 25	4 33	4 41	4 48	4 55	5 02	5 09	5 16	5 22	5 28	5 34	5 40	5 46	5 52	5 58	6 03	6 09	6 14
59	R.	8 52	8 52	8 46	8 39	8 31	8 23	8 15	8 08	8 00	7 52	7 44	7 37	7 29	7 21	7 14	7 07	6 59	6 52	6 45	6 37	6 30	6 22	6 15	6 07	6 00
	S.	3 05	3 15	3 29	3 41	3 52	4 02	4 11	4 20	4 29	4 37	4 44	4 52	4 59	5 06	5 13	5 20	5 26	5 33	5 39	5 45	5 51	5 57	6 03	6 09	6 15
60	R.	9 01	9 01	8 54	8 46	8 38	8 29	8 21	8 13	8 05	7 56	7 48	7 40	7 32	7 24	7 17	7 09	7 01	6 54	6 46	6 39	6 31	6 23	6 15	6 08	6 00
	S.	2 56	3 06	3 21	3 34	3 45	3 55	4 05	4 15	4 24	4 32	4 40	4 48	4 56	5 03	5 10	5 17	5 24	5 31	5 37	5 44	5 50	5 56	6 02	6 09	6 15

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

South latitude: 0° to 20°—March 21 to June 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date	MARCH.					APRIL.										MAY.							JUNE.			Approx. date	Lat. S.
		21	23	26	28	31	3	5	8	11	13	16	19	22	25	28	1	5	8	12	16	21	26	1	10	22		
	Dec. N.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
0	R.	6 04	6 03	6 02	6 01	6 00	6 00	5 59	5 58	5 57	5 57	5 56	5 55	5 55	5 54	5 54	5 53	5 53	5 52	5 52	5 52	5 52	5 53	5 54	5 55	5 57	R.	0
	S.	6 11	6 11	6 10	6 09	6 08	6 08	6 07	6 06	6 05	6 05	6 04	6 03	6 03	6 02	6 02	6 01	6 01	6 00	6 00	6 00	6 00	6 01	6 02	6 03	6 05	S.	
1	R.	6 04	6 03	6 02	6 02	6 01	6 00	5 59	5 58	5 58	5 58	5 57	5 56	5 56	5 55	5 55	5 54	5 54	5 54	5 54	5 54	5 54	5 54	5 55	5 57	5 59	R.	1
	S.	6 11	6 10	6 09	6 09	6 08	6 07	6 06	6 05	6 04	6 04	6 03	6 02	6 02	6 01	6 01	6 00	5 59	5 59	5 59	5 59	5 59	5 59	6 00	6 02	6 04	S.	
2	R.	6 04	6 03	6 02	6 02	6 01	6 00	6 00	5 59	5 59	5 58	5 57	5 57	5 56	5 56	5 56	5 55	5 55	5 55	5 55	5 55	5 55	5 56	5 57	5 58	6 01	R.	2
	S.	6 11	6 10	6 09	6 09	6 08	6 07	6 06	6 05	6 04	6 03	6 02	6 02	6 01	6 00	6 00	5 59	5 58	5 58	5 58	5 58	5 57	5 58	5 59	6 00	6 03	S.	
3	R.	6 04	6 03	6 02	6 02	6 01	6 01	6 00	5 59	5 59	5 59	5 58	5 57	5 57	5 57	5 57	5 56	5 56	5 56	5 56	5 56	5 57	5 57	5 58	6 00	6 03	R.	3
	S.	6 11	6 10	6 09	6 08	6 07	6 06	6 05	6 04	6 03	6 03	6 02	6 01	6 00	6 00	5 59	5 58	5 57	5 57	5 56	5 56	5 56	5 56	5 57	5 59	6 01	S.	
4	R.	6 04	6 03	6 02	6 02	6 01	6 01	6 00	6 00	6 00	5 59	5 58	5 58	5 58	5 58	5 58	5 57	5 57	5 57	5 57	5 58	5 58	5 59	6 00	6 01	6 04	R.	4
	S.	6 11	6 10	6 09	6 08	6 07	6 06	6 05	6 04	6 03	6 02	6 01	6 00	5 59	5 59	5 58	5 57	5 56	5 56	5 55	5 55	5 55	5 55	5 56	5 57	5 59	S.	
5	R.	6 04	6 03	6 02	6 02	6 02	6 01	6 01	6 00	6 00	6 00	5 59	5 59	5 59	5 59	5 59	5 58	5 58	5 58	5 59	5 59	5 59	6 00	6 02	6 03	6 06	R.	5
	S.	6 11	6 10	6 09	6 08	6 07	6 06	6 05	6 03	6 02	6 01	6 00	5 59	5 58	5 58	5 57	5 56	5 55	5 54	5 54	5 53	5 53	5 53	5 54	5 55	5 57	S.	
6	R.	6 03	6 03	6 02	6 02	6 02	6 02	6 01	6 01	6 01	6 01	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 01	6 02	6 03	6 05	6 08	R.	6
	S.	6 11	6 10	6 09	6 08	6 07	6 06	6 04	6 03	6 02	6 01	6 00	5 59	5 58	5 57	5 56	5 55	5 54	5 53	5 53	5 52	5 52	5 52	5 52	5 54	5 56	S.	
7	R.	6 03	6 03	6 03	6 03	6 02	6 02	6 02	6 01	6 01	6 01	6 01	6 01	6 01	6 01	6 01	6 01	6 01	6 01	6 01	6 02	6 02	6 03	6 05	6 07	6 10	R.	7
	S.	6 11	6 10	6 09	6 08	6 06	6 05	6 04	6 02	6 01	6 00	5 59	5 58	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 51	5 50	5 50	5 51	5 52	5 54	S.	
8	R.	6 03	6 03	6 03	6 03	6 02	6 02	6 02	6 02	6 02	6 02	6 01	6 01	6 02	6 02	6 02	6 02	6 02	6 02	6 02	6 03	6 04	6 05	6 06	6 08	6 11	R.	8
	S.	6 11	6 10	6 09	6 08	6 06	6 05	6 04	6 02	6 01	6 00	5 58	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 50	5 49	5 49	5 49	5 50	5 52	S.	
9	R.	6 03	6 03	6 03	6 03	6 03	6 03	6 02	6 02	6 02	6 02	6 02	6 02	6 03	6 03	6 03	6 03	6 03	6 03	6 04	6 04	6 05	6 06	6 08	6 10	6 13	R.	9
	S.	6 11	6 10	6 09	6 08	6 06	6 05	6 03	6 01	6 00	5 59	5 57	5 56	5 55	5 54	5 53	5 52	5 50	5 49	5 49	5 48	5 47	5 47	5 47	5 48	5 50	S.	
10	R.	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 04	6 04	6 04	6 04	6 05	6 06	6 07	6 08	6 10	6 12	6 15	R.	10
	S.	6 11	6 10	6 09	6 08	6 06	6 05	6 03	6 01	5 59	5 58	5 57	5 56	5 54	5 53	5 52	5 51	5 49	5 48	5 48	5 47	5 46	5 46	5 46	5 47	5 49	S.	
11	R.	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 03	6 04	6 04	6 04	6 04	6 04	6 04	6 05	6 05	6 05	6 05	6 06	6 07	6 08	6 09	6 11	6 14	6 17	R.	11
	S.	6 11	6 10	6 08	6 07	6 05	6 04	6 02	6 00	5 59	5 58	5 56	5 55	5 53	5 52	5 51	5 50	5 48	5 47	5 46	5 45	5 44	5 44	5 44	5 45	5 47	S.	
12	R.	6 03	6 03	6 03	6 04	6 04	6 04	6 04	6 04	6 04	6 04	6 04	6 05	6 05	6 05	6 06	6 06	6 06	6 07	6 08	6 09	6 10	6 11	6 13	6 15	6 18	R.	12
	S.	6 11	6 10	6 08	6 07	6 05	6 04	6 02	6 00	5 58	5 57	5 55	5 54	5 52	5 51	5 50	5 49	5 47	5 46	5 45	5 44	5 43	5 43	5 43	5 43	5 45	S.	
13	R.	6 03	6 04	6 04	6 04	6 04	6 04	6 04	6 04	6 05	6 05	6 05	6 06	6 06	6 06	6 07	6 07	6 08	6 08	6 09	6 10	6 11	6 13	6 15	6 17	6 20	R.	13
	S.	6 11	6 10	6 08	6 06	6 04	6 03	6 01	5 59	5 58	5 56	5 54	5 53	5 51	5 50	5 49	5 47	5 46	5 44	5 43	5 42	5 41	5 41	5 41	5 41	5 43	S.	
14	R.	6 03	6 04	6 04	6 04	6 04	6 05	6 05	6 05	6 05	6 06	6 06	6 06	6 07	6 07	6 08	6 08	6 09	6 10	6 11	6 12	6 13	6 14	6 16	6 19	6 22	R.	14
	S.	6 11	6 10	6 08	6 06	6 04	6 03	6 01	5 59	5 57	5 56	5 54	5 52	5 51	5 49	5 48	5 46	5 45	5 43	5 42	5 41	5 40	5 39	5 39	5 40	5 42	S.	
15	R.	6 03	6 04	6 04	6 05	6 05	6 05	6 05	6 05	6 06	6 06	6 06	6 07	6 08	6 08	6 09	6 09	6 10	6 11	6 12	6 13	6 14	6 16	6 18	6 21	6 24	R.	15
	S.	6 11	6 10	6 08	6 06	6 04	6 02	6 00	5 58	5 57	5 55	5 53	5 52	5 50	5 48	5 47	5 46	5 43	5 42	5 41	5 39	5 38	5 38	5 37	5 38	5 40	S.	
16	R.	6 03	6 04	6 04	6 05	6 05	6 05	6 06	6 06	6 06	6 07	6 07	6 08	6 09	6 09	6 10	6 10	6 11	6 12	6 13	6 15	6 16	6 18	6 20	6 23	6 26	R.	16
	S.	6 11	6 10	6 08	6 06	6 04	6 02	6 00	5 58	5 56	5 54	5 52	5 51	5 49	5 47	5 46	5 44	5 42	5 40	5 39	5 38	5 37	5 36	5 36	5 36	5 38	S.	
17	R.	6 03	6 04	6 04	6 05	6 05	6 06	6 06	6 06	6 07	6 08	6 08	6 09	6 10	6 10	6 11	6 12	6 13	6 14	6 15	6 16	6 18	6 20	6 22	6 25	6 28	R.	17
	S.	6 11	6 10	6 08	6 06	6 04	6 02	6 00	5 58	5 56	5 54	5 52	5 50	5 48	5 46	5 44	5 43	5 41	5 39	5 38	5 36	5 35	5 34	5 34	5 34	5 36	S.	
18	R.	6 03	6 04	6 04	6 05	6 05	6 06	6 06	6 07	6 08	6 08	6 09	6 10	6 11	6 11	6 12	6 13	6 14	6 15	6 16	6 18	6 19	6 21	6 23	6 26	6 30	R.	18
	S.	6 11	6 09	6 07	6 05	6 03	6 01	5 59	5 57	5 55	5 53	5 51	5 49	5 47	5 45	5 43	5 42	5 40	5 38	5 36	5 35	5 33	5 33	5 32	5 32	5 34	S.	
19	R.	6 03	6 04	6 04	6 05	6 06	6 06	6 07	6 07	6 08	6 09	6 10	6 11	6 12	6 12	6 13	6 14	6 15	6 16	6 18	6 19	6 21	6 23	6 25	6 28	6 32	R.	19
	S.	6 11	6 09	6 07	6 05	6 03	6 01	5 59	5 56	5 54	5 52	5 50	5 48	5 46	5 44	5 42	5 40	5 38	5 36	5 35	5 33	5 32	5 31	5 30	5 30	5 32	S.	
20	R.	6 03	6 04	6 04	6 05	6 06	6 07	6 07	6 08	6 09	6 10	6 10	6 11	6 12	6 13	6 14	6 15	6 16	6 17	6 19	6 21	6 22	6 24	6 27	6 30	6 34	R.	20
	S.	6 11	6 09	6 07	6 05	6 03	6 01	5 58	5 56	5 54	5 52	5 49	5 47	5 45	5 43	5 41	5 39	5 37	5 35	5 33	5 32	5 30	5 29	5 28	5 28	5 30	S.	

6583—06——32

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

South latitude: 21° to 40°—March 21 to June 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	March 21	March 23	March 26	March 28	March 31	April 3	April 5	April 8	April 11	April 13	April 16	April 19	April 22	April 25	April 28
	Dec. N.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
21	R.	6 03	6 04	6 05	6 06	6 06	6 07	6 08	6 09	6 10	6 11	6 11	6 12	6 13	6 14	6 15
	S.	6 11	6 09	6 07	6 05	6 02	6 00	5 58	5 55	5 53	5 51	5 48	5 46	5 44	5 42	5 40
22	R.	6 03	6 04	6 05	6 06	6 06	6 07	6 08	6 09	6 10	6 11	6 12	6 13	6 14	6 15	6 16
	S.	6 11	6 09	6 07	6 05	6 02	6 00	5 57	5 55	5 52	5 50	5 48	5 46	5 43	5 41	5 39
23	R.	6 03	6 04	6 05	6 06	6 07	6 08	6 09	6 10	6 11	6 12	6 13	6 14	6 15	6 16	6 17
	S.	6 11	6 09	6 07	6 05	6 02	6 00	5 57	5 54	5 52	5 50	5 47	5 45	5 42	5 40	5 37
24	R.	6 03	6 04	6 05	6 06	6 07	6 08	6 09	6 10	6 11	6 12	6 13	6 15	6 16	6 17	6 18
	S.	6 11	6 09	6 07	6 04	6 01	5 59	5 56	5 54	5 51	5 49	5 46	5 44	5 41	5 39	5 36
25	R.	6 03	6 04	6 05	6 07	6 08	6 09	6 10	6 11	6 12	6 13	6 14	6 16	6 17	6 19	6 20
	S.	6 11	6 09	6 06	6 04	6 01	5 59	5 56	5 53	5 50	5 48	5 45	5 43	5 40	5 38	5 35
26	R.	6 03	6 04	6 05	6 07	6 08	6 09	6 10	6 11	6 13	6 14	6 15	6 16	6 18	6 20	6 21
	S.	6 11	6 09	6 06	6 04	6 01	5 58	5 55	5 52	5 50	5 48	5 45	5 42	5 39	5 37	5 34
27	R.	6 03	6 04	6 05	6 07	6 08	6 10	6 11	6 12	6 13	6 15	6 16	6 17	6 19	6 21	6 22
	S.	6 11	6 09	6 06	6 03	6 00	5 58	5 55	5 52	5 49	5 47	5 44	5 41	5 38	5 36	5 33
28	R.	6 03	6 04	6 06	6 07	6 08	6 10	6 11	6 12	6 14	6 15	6 17	6 18	6 20	6 22	6 23
	S.	6 11	6 09	6 06	6 03	6 00	5 57	5 54	5 51	5 49	5 46	5 43	5 40	5 37	5 35	5 32
29	R.	6 03	6 04	6 06	6 07	6 09	6 10	6 12	6 13	6 15	6 16	6 18	6 19	6 21	6 23	6 24
	S.	6 11	6 09	6 06	6 03	6 00	5 57	5 54	5 51	5 48	5 45	5 42	5 39	5 36	5 33	5 30
30	R.	6 03	6 04	6 06	6 07	6 09	6 11	6 12	6 13	6 15	6 17	6 18	6 20	6 22	6 24	6 26
	S.	6 12	6 09	6 06	6 03	6 00	5 57	5 53	5 50	5 47	5 44	5 41	5 38	5 35	5 32	5 29
31	R.	6 03	6 04	6 06	6 08	6 09	6 11	6 13	6 14	6 16	6 18	6 19	6 21	6 23	6 25	6 28
	S.	6 12	6 09	6 06	6 03	5 59	5 56	5 53	5 49	5 46	5 43	5 40	5 37	5 34	5 31	5 28
32	R.	6 03	6 05	6 06	6 08	6 10	6 12	6 13	6 15	6 17	6 19	6 20	6 22	6 24	6 26	6 29
	S.	6 12	6 09	6 06	6 03	5 59	5 56	5 52	5 49	5 46	5 43	5 39	5 36	5 33	5 30	5 27
33	R.	6 03	6 05	6 06	6 08	6 10	6 12	6 14	6 15	6 17	6 19	6 21	6 23	6 26	6 28	6 30
	S.	6 12	6 09	6 05	6 02	5 58	5 55	5 52	5 48	5 45	5 42	5 38	5 35	5 32	5 29	5 25
34	R.	6 03	6 05	6 07	6 09	6 11	6 13	6 14	6 16	6 18	6 20	6 22	6 24	6 27	6 29	6 32
	S.	6 12	6 09	6 05	6 02	5 58	5 55	5 51	5 48	5 44	5 41	5 37	5 34	5 31	5 27	5 24
35	R.	6 03	6 05	6 07	6 09	6 11	6 13	6 15	6 17	6 19	6 21	6 23	6 26	6 28	6 31	6 33
	S.	6 12	6 09	6 05	6 02	5 58	5 54	5 51	5 47	5 43	5 40	5 36	5 33	5 29	5 26	5 22
36	R.	6 03	6 05	6 07	6 09	6 11	6 14	6 16	6 18	6 20	6 22	6 24	6 27	6 29	6 32	6 35
	S.	6 12	6 09	6 05	6 01	5 57	5 54	5 50	5 46	5 43	5 39	5 35	5 32	5 28	5 25	5 21
37	R.	6 03	6 05	6 07	6 10	6 12	6 14	6 16	6 18	6 21	6 23	6 25	6 28	6 31	6 33	6 36
	S.	6 12	6 08	6 04	6 01	5 57	5 53	5 49	5 45	5 42	5 38	5 34	5 31	5 27	5 23	5 19
38	R.	6 02	6 05	6 07	6 10	6 12	6 15	6 17	6 19	6 21	6 24	6 26	6 29	6 32	6 35	6 38
	S.	6 12	6 08	6 04	6 01	5 57	5 53	5 49	5 45	5 41	5 37	5 33	5 30	5 26	5 22	5 18
39	R.	6 02	6 05	6 07	6 10	6 12	6 15	6 17	6 20	6 22	6 25	6 27	6 30	6 33	6 36	6 39
	S.	6 12	6 08	6 04	6 00	5 56	5 52	5 48	5 44	5 40	5 36	5 32	5 28	5 24	5 20	5 16
40	R.	6 02	6 05	6 07	6 10	6 13	6 16	6 18	6 21	6 23	6 26	6 28	6 31	6 35	6 38	6 41
	S.	6 12	6 08	6 04	6 00	5 56	5 52	5 47	5 43	5 39	5 35	5 31	5 27	5 23	5 19	5 15

Lat. S.	Approx. date.	May 1	May 5	May 8	May 12	May 16	May 21	May 26	June 1	June 10	June 22	Approx. date.	Lat. S.
	Dec. N.	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
21	R.	6 16	6 18	6 19	6 21	6 22	6 24	6 26	6 29	6 32	6 36	R.	21
	S.	5 38	5 36	5 34	5 32	5 30	5 28	5 27	5 26	5 26	5 28	S.	
22	R.	6 17	6 19	6 20	6 22	6 24	6 26	6 28	6 31	6 34	6 38	R.	22
	S.	5 37	5 35	5 33	5 31	5 29	5 27	5 26	5 25	5 24	5 26	S.	
23	R.	6 19	6 20	6 22	6 24	6 25	6 27	6 30	6 33	6 36	6 40	R.	23
	S.	5 35	5 33	5 31	5 29	5 27	5 25	5 24	5 23	5 22	5 24	S.	
24	R.	6 20	6 22	6 23	6 25	6 27	6 29	6 31	6 34	6 38	6 42	R.	24
	S.	5 34	5 32	5 30	5 28	5 26	5 24	5 22	5 21	5 20	5 22	S.	
25	R.	6 22	6 23	6 25	6 27	6 29	6 31	6 33	6 36	6 40	6 44	R.	25
	S.	5 33	5 30	5 28	5 26	5 24	5 22	5 20	5 19	5 18	5 20	S.	
26	R.	6 23	6 24	6 26	6 28	6 30	6 32	6 35	6 39	6 42	6 46	R.	26
	S.	5 32	5 29	5 27	5 24	5 22	5 20	5 18	5 17	5 16	5 18	S.	
27	R.	6 24	6 26	6 28	6 30	6 32	6 34	6 37	6 41	6 45	6 48	R.	27
	S.	5 31	5 28	5 25	5 23	5 21	5 18	5 16	5 15	5 14	5 15	S.	
28	R.	6 25	6 27	6 29	6 31	6 34	6 36	6 39	6 43	6 47	6 50	R.	28
	S.	5 29	5 26	5 24	5 21	5 19	5 16	5 14	5 13	5 12	5 13	S.	
29	R.	6 27	6 29	6 31	6 33	6 36	6 38	6 41	6 45	6 49	6 53	R.	29
	S.	5 28	5 25	5 22	5 19	5 17	5 14	5 12	5 11	5 10	5 11	S.	
30	R.	6 28	6 30	6 32	6 35	6 37	6 40	6 43	6 47	6 51	6 55	R.	30
	S.	5 26	5 23	5 20	5 18	5 15	5 12	5 10	5 09	5 08	5 09	S.	
31	R.	6 30	6 32	6 34	6 36	6 39	6 42	6 45	6 49	6 53	6 57	R.	31
	S.	5 25	5 22	5 19	5 16	5 13	5 10	5 08	5 06	5 05	5 06	S.	
32	R.	6 31	6 33	6 35	6 38	6 41	6 44	6 47	6 51	6 56	7 00	R.	32
	S.	5 24	5 20	5 17	5 14	5 11	5 08	5 06	5 04	5 03	5 04	S.	
33	R.	6 32	6 35	6 37	6 40	6 43	6 46	6 50	6 54	6 58	7 02	R.	33
	S.	5 22	5 19	5 15	5 12	5 09	5 06	5 04	5 02	5 00	5 01	S.	
34	R.	6 34	6 36	6 39	6 42	6 45	6 48	6 52	6 56	7 01	7 05	R.	34
	S.	5 21	5 17	5 14	5 11	5 07	5 04	5 02	5 00	4 58	4 59	S.	
35	R.	6 36	6 38	6 41	6 44	6 47	6 50	6 54	6 58	7 03	7 07	R.	35
	S.	5 19	5 15	5 12	5 09	5 06	5 02	5 00	4 57	4 55	4 56	S.	
36	R.	6 37	6 40	6 43	6 46	6 49	6 52	6 56	7 01	7 06	7 10	R.	36
	S.	5 17	5 14	5 10	5 07	5 04	5 00	4 57	4 55	4 53	4 54	S.	
37	R.	6 39	6 42	6 45	6 48	6 51	6 55	6 59	7 03	7 08	7 13	R.	37
	S.	5 16	5 12	5 08	5 05	5 01	4 58	4 55	4 52	4 50	4 51	S.	
38	R.	6 40	6 43	6 46	6 50	6 53	6 57	7 01	7 06	7 11	7 16	R.	38
	S.	5 14	5 10	5 06	5 03	4 59	4 55	4 52	4 50	4 47	4 48	S.	
39	R.	6 42	6 45	6 48	6 52	6 56	7 00	7 04	7 09	7 14	7 19	R.	39
	S.	5 12	5 08	5 04	5 00	4 57	4 53	4 50	4 47	4 44	4 45	S.	
40	R.	6 44	6 47	6 50	6 54	6 58	7 02	7 06	7 11	7 17	7 22	R.	40
	S.	5 11	5 06	5 02	4 58	4 54	4 50	4 47	4 44	4 41	4 42	S.	

Mean Time of Sun's Visible Rising and Setting.

South Latitude: 41° to 60°—March 21 to June 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	MARCH.					APRIL.										MAY.							JUNE.			Approx. date.	Lat. S.
		21	23	26	28	31	3	5	8	11	13	16	19	22	25	28	1	5	8	12	16	21	26	1	10	22		
	Dec. N.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
41	R.	6 02	6 05	6 08	6 11	6 13	6 16	6 19	6 21	6 24	6 27	6 30	6 33	6 36	6 39	6 43	6 46	6 49	6 53	6 57	7 01	7 05	7 09	7 14	7 20	7 25	R.	41
	S.	6 12	6 08	6 04	6 00	5 55	5 51	5 47	5 42	5 38	5 34	5 30	5 26	5 21	5 17	5 13	5 09	5 04	5 00	4 56	4 52	4 48	4 44	4 41	4 38	4 39	S.	
42	R.	6 02	6 05	6 08	6 11	6 14	6 17	6 19	6 22	6 25	6 28	6 31	6 34	6 38	6 41	6 44	6 48	6 51	6 55	6 59	7 03	7 07	7 12	7 17	7 23	7 28	R.	42
	S.	6 12	6 08	6 04	6 00	5 55	5 51	5 46	5 42	5 37	5 33	5 29	5 24	5 20	5 16	5 11	5 07	5 02	4 58	4 54	4 50	4 46	4 42	4 38	4 35	4 36	S.	
43	R.	6 02	6 05	6 08	6 11	6 14	6 17	6 20	6 23	6 26	6 29	6 32	6 36	6 39	6 43	6 46	6 50	6 53	6 57	7 01	7 05	7 10	7 15	7 20	7 26	7 31	R.	43
	S.	6 12	6 08	6 03	5 59	5 54	5 50	5 45	5 41	5 36	5 32	5 27	5 23	5 18	5 14	5 09	5 05	5 00	4 56	4 51	4 47	4 43	4 39	4 35	4 32	4 32	S.	
44	R.	6 02	6 05	6 08	6 11	6 14	6 18	6 21	6 24	6 27	6 31	6 34	6 37	6 41	6 44	6 48	6 52	6 55	6 59	7 04	7 08	7 13	7 18	7 23	7 30	7 35	R.	44
	S.	6 13	6 08	6 03	5 59	5 54	5 50	5 45	5 40	5 35	5 31	5 26	5 21	5 17	5 12	5 08	5 03	4 58	4 53	4 49	4 44	4 40	4 36	4 32	4 29	4 29	S.	
45	R.	6 02	6 05	6 08	6 12	6 15	6 18	6 21	6 24	6 28	6 32	6 35	6 39	6 42	6 46	6 50	6 54	6 58	7 02	7 06	7 11	7 16	7 21	7 27	7 33	7 38	R.	45
	S.	6 13	6 08	6 03	5 59	5 54	5 49	5 44	5 39	5 34	5 30	5 25	5 20	5 15	5 11	5 06	5 01	4 56	4 51	4 46	4 42	4 37	4 33	4 29	4 25	4 25	S.	
46	R.	6 02	6 05	6 08	6 12	6 15	6 19	6 22	6 25	6 29	6 33	6 36	6 40	6 44	6 48	6 52	6 56	7 00	7 04	7 09	7 14	7 19	7 24	7 30	7 37	7 42	R.	46
	S.	6 13	6 08	6 03	5 58	5 53	5 48	5 43	5 38	5 33	5 28	5 23	5 18	5 14	5 09	5 04	4 59	4 54	4 49	4 44	4 39	4 34	4 29	4 25	4 22	4 22	S.	
47	R.	6 02	6 05	6 09	6 12	6 16	6 19	6 23	6 26	6 30	6 34	6 38	6 42	6 46	6 50	6 54	6 58	7 02	7 07	7 12	7 17	7 22	7 28	7 34	7 41	7 46	R.	47
	S.	6 13	6 08	6 03	5 58	5 53	5 48	5 43	5 37	5 32	5 27	5 22	5 17	5 12	5 07	5 02	4 57	4 51	4 46	4 41	4 36	4 31	4 26	4 22	4 18	4 18	S.	
48	R.	6 02	6 05	6 09	6 13	6 16	6 20	6 24	6 27	6 31	6 35	6 39	6 43	6 47	6 52	6 56	7 00	7 05	7 10	7 15	7 20	7 25	7 31	7 38	7 45	7 50	R.	48
	S.	6 13	6 08	6 03	5 58	5 52	5 47	5 42	5 36	5 31	5 26	5 20	5 15	5 10	5 05	5 00	4 54	4 49	4 43	4 38	4 33	4 27	4 22	4 18	4 14	4 14	S.	
49	R.	6 01	6 05	6 09	6 13	6 17	6 21	6 24	6 28	6 33	6 37	6 41	6 45	6 49	6 54	6 58	7 03	7 08	7 13	7 18	7 23	7 29	7 35	7 42	7 49	7 54	R.	49
	S.	6 13	6 08	6 03	5 57	5 52	5 47	5 41	5 35	5 30	5 25	5 19	5 14	5 08	5 03	4 57	4 52	4 46	4 40	4 35	4 29	4 24	4 19	4 14	4 10	4 09	S.	
50	R.	6 01	6 05	6 09	6 13	6 17	6 21	6 25	6 29	6 34	6 38	6 42	6 47	6 51	6 56	7 01	7 05	7 10	7 15	7 21	7 27	7 33	7 39	7 46	7 53	7 59	R.	50
	S.	6 13	6 08	6 02	5 56	5 51	5 46	5 40	5 34	5 29	5 23	5 17	5 12	5 06	5 01	4 55	4 49	4 43	4 37	4 32	4 26	4 20	4 15	4 10	4 05	4 05	S.	
51	R.	6 01	6 06	6 10	6 14	6 18	6 22	6 26	6 31	6 35	6 40	6 44	6 48	6 53	6 58	7 03	7 08	7 13	7 18	7 24	7 30	7 36	7 43	7 50	7 58	8 04	R.	51
	S.	6 13	6 08	6 02	5 56	5 50	5 45	5 39	5 33	5 27	5 22	5 16	5 10	5 04	4 58	4 52	4 46	4 40	4 34	4 28	4 22	4 16	4 11	4 05	4 01	4 00	S.	
52	R.	6 01	6 06	6 10	6 14	6 19	6 23	6 27	6 32	6 36	6 41	6 45	6 50	6 55	7 00	7 06	7 11	7 16	7 22	7 28	7 34	7 40	7 47	7 55	8 03	8 09	R.	52
	S.	6 13	6 08	6 02	5 56	5 50	5 44	5 38	5 32	5 26	5 20	5 14	5 08	5 02	4 56	4 50	4 44	4 37	4 31	4 25	4 19	4 12	4 06	4 01	3 56	3 55	S.	
53	R.	6 01	6 06	6 10	6 15	6 19	6 24	6 28	6 33	6 38	6 43	6 47	6 52	6 58	7 03	7 08	7 14	7 19	7 25	7 31	7 38	7 45	7 52	8 00	8 08	8 14	R.	53
	S.	6 13	6 08	6 02	5 56	5 49	5 43	5 37	5 31	5 25	5 19	5 12	5 06	5 00	4 54	4 47	4 41	4 34	4 27	4 21	4 15	4 08	4 02	3 56	3 50	3 49	S.	
54	R.	6 01	6 06	6 10	6 15	6 20	6 25	6 29	6 34	6 39	6 44	6 49	6 54	7 00	7 05	7 11	7 17	7 23	7 29	7 35	7 42	7 49	7 57	8 05	8 14	8 20	R.	54
	S.	6 14	6 08	6 01	5 55	5 49	5 43	5 36	5 30	5 23	5 17	5 10	5 04	4 58	4 51	4 44	4 38	4 31	4 24	4 17	4 11	4 04	3 57	3 51	3 45	3 44	S.	
55	R.	6 01	6 06	6 11	6 16	6 21	6 26	6 31	6 36	6 41	6 46	6 51	6 57	7 02	7 08	7 14	7 20	7 26	7 32	7 39	7 46	7 54	8 02	8 10	8 19	8 26	R.	55
	S.	6 14	6 08	6 01	5 55	5 48	5 42	5 35	5 28	5 22	5 15	5 08	5 02	4 55	4 48	4 41	4 34	4 27	4 20	4 13	4 06	3 59	3 52	3 45	3 39	3 38	S.	
56	R.	6 01	6 06	6 11	6 16	6 21	6 27	6 32	6 37	6 42	6 48	6 53	6 59	7 05	7 11	7 17	7 24	7 30	7 37	7 44	7 51	7 59	8 07	8 16	8 26	8 33	R.	56
	S.	6 14	6 08	6 01	5 54	5 47	5 41	5 34	5 27	5 20	5 13	5 06	4 59	4 52	4 45	4 38	4 31	4 24	4 16	4 09	4 01	3 54	3 46	3 39	3 33	3 31	S.	
57	R.	6 00	6 06	6 11	6 17	6 22	6 28	6 33	6 38	6 44	6 50	6 56	7 02	7 08	7 14	7 21	7 27	7 34	7 41	7 48	7 56	8 04	8 13	8 22	8 33	8 40	R.	57
	S.	6 14	6 08	6 01	5 54	5 47	5 40	5 32	5 25	5 18	5 11	5 04	4 57	4 50	4 42	4 35	4 27	4 20	4 12	4 04	3 56	3 48	3 41	3 33	3 26	3 24	S.	
58	R.	6 00	6 06	6 11	6 17	6 23	6 29	6 34	6 40	6 46	6 52	6 58	7 04	7 11	7 17	7 24	7 31	7 38	7 45	7 53	8 01	8 10	8 19	8 29	8 40	8 47	R.	58
	S.	6 14	6 07	6 00	5 53	5 46	5 39	5 31	5 24	5 17	5 09	5 02	4 54	4 47	4 39	4 31	4 23	4 15	4 07	3 59	3 51	3 43	3 34	3 26	3 19	3 16	S.	
59	R.	6 00	6 06	6 12	6 18	6 24	6 30	6 36	6 42	6 48	6 54	7 00	7 07	7 14	7 21	7 28	7 35	7 42	7 50	7 58	8 07	8 16	8 26	8 37	8 48	8 55	R.	59
	S.	6 15	6 07	6 00	5 53	5 45	5 38	5 30	5 22	5 15	5 07	4 59	4 52	4 44	4 36	4 28	4 20	4 11	4 02	3 54	3 46	3 37	3 28	3 19	3 11	3 08	S.	
60	R.	6 00	6 06	6 12	6 19	6 25	6 31	6 37	6 43	6 50	6 57	7 03	7 10	7 17	7 24	7 32	7 39	7 47	7 55	8 04	8 13	8 23	8 33	8 45	8 57	9 04	R.	60
	S.	6 15	6 07	5 59	5 52	5 44	5 36	5 28	5 20	5 13	5 05	4 57	4 49	4 41	4 32	4 24	4 15	4 06	3 57	3 48	3 39	3 30	3 21	3 11	3 02	2 59	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

South Latitude: 0° to 20°.—June 22 to September 23.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	JUNE.	JULY.					AUGUST.										SEPTEMBER.									Approx. date.	Lat. S.
		22	3	12	19	24	28	2	5	9	12	16	19	22	25	28	30	2	5	8	10	13	16	18	21	23		
	Dec. N.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
0	R.	5 57	6 00	6 01	6 02	6 02	6 02	6 02	6 02	6 01	6 01	6 00	6 00	5 59	5 58	5 57	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 49	5 49	R.	0
	S.	6 05	6 08	6 09	6 10	6 10	6 10	6 10	6 10	6 09	6 09	6 08	6 08	6 07	6 06	6 05	6 05	6 04	6 03	6 02	6 01	6 00	5 59	5 58	5 57	5 56	S.	
1	R.	5 59	6 01	6 02	6 03	6 04	6 04	6 04	6 03	6 03	6 02	6 01	6 01	6 00	5 59	5 58	5 57	5 56	5 55	5 54	5 54	5 53	5 52	5 51	5 50	5 49	R.	1
	S.	6 04	6 06	6 07	6 08	6 09	6 09	6 09	6 08	6 08	6 08	6 07	6 07	6 06	6 05	6 04	6 04	6 03	6 02	6 01	6 01	6 00	5 59	5 58	5 57	5 56	S.	
2	R.	6 01	6 03	6 04	6 05	6 05	6 05	6 05	6 04	6 04	6 03	6 02	6 01	6 00	6 00	5 59	5 58	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 49	R.	2
	S.	6 03	6 05	6 06	6 07	6 07	6 08	6 08	6 07	6 07	6 07	6 06	6 06	6 05	6 05	6 04	6 03	6 02	6 02	6 01	6 01	6 00	5 59	5 58	5 57	5 56	S.	
3	R.	6 03	6 05	6 06	6 06	6 07	6 06	6 06	6 05	6 05	6 04	6 03	6 02	6 01	6 00	5 59	5 58	5 57	5 56	5 55	5 54	5 53	5 52	5 51	5 50	5 49	R.	3
	S.	6 01	6 03	6 05	6 05	6 06	6 06	6 06	6 06	6 06	6 06	6 05	6 05	6 04	6 04	6 03	6 03	6 02	6 01	6 00	6 00	5 59	5 59	5 58	5 57	5 56	S.	
4	R.	6 04	6 06	6 07	6 08	6 08	6 08	6 07	6 06	6 06	6 05	6 04	6 03	6 02	6 01	6 00	5 59	5 58	5 57	5 55	5 54	5 53	5 52	5 51	5 50	5 49	R.	4
	S.	5 59	6 02	6 03	6 04	6 04	6 05	6 05	6 05	6 05	6 05	6 04	6 04	6 03	6 03	6 03	6 02	6 01	6 01	6 00	6 00	5 59	5 58	5 58	5 57	5 56	S.	
5	R.	6 06	6 08	6 09	6 09	6 10	6 09	6 09	6 08	6 07	6 06	6 05	6 04	6 03	6 02	6 01	6 00	5 59	5 57	5 56	5 55	5 54	5 52	5 51	5 50	5 49	R.	5
	S.	5 57	6 00	6 01	6 02	6 03	6 03	6 04	6 04	6 03	6 03	6 03	6 03	6 02	6 02	6 02	6 02	6 01	6 00	6 00	6 00	5 59	5 58	5 58	5 57	5 56	S.	
6	R.	6 08	6 10	6 11	6 11	6 11	6 10	6 10	6 09	6 08	6 07	6 06	6 05	6 04	6 03	6 01	6 00	5 59	5 58	5 56	5 55	5 54	5 52	5 51	5 50	5 48	R.	6
	S.	5 56	5 58	6 00	6 01	6 02	6 02	6 03	6 03	6 02	6 02	6 02	6 02	6 02	6 02	6 01	6 01	6 00	6 00	5 59	5 59	5 59	5 58	5 58	5 57	6 56	S.	
7	R.	6 10	6 11	6 12	6 12	6 12	6 12	6 11	6 10	6 09	6 08	6 07	6 06	6 05	6 04	6 02	6 01	6 00	5 58	5 57	5 56	5 54	5 53	5 51	5 50	5 48	R.	7
	S.	5 54	5 56	5 58	5 59	6 00	6 01	6 01	6 01	6 01	6 01	6 01	6 01	6 01	6 01	6 00	6 00	6 00	5 59	5 59	5 59	5 58	5 58	5 57	5 57	5 56	S.	
8	R.	6 11	6 13	6 14	6 14	6 14	6 13	6 12	6 11	6 10	6 09	6 08	6 07	6 06	6 04	6 03	6 02	6 00	5 59	5 57	5 56	5 54	5 53	5 51	5 50	5 48	R.	8
	S.	5 52	5 55	5 57	5 58	5 59	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	6 00	5 59	5 59	5 59	5 59	5 58	5 58	5 57	5 57	5 56	S.	
9	R.	6 13	6 15	6 16	6 15	6 15	6 14	6 14	6 13	6 12	6 10	6 09	6 08	6 07	6 05	6 04	6 03	6 01	5 59	5 57	5 56	5 55	5 53	5 51	5 50	5 48	R.	9
	S.	5 50	5 53	5 55	5 56	5 57	5 58	5 59	5 59	5 59	5 59	5 59	5 59	5 59	5 59	5 59	5 59	5 58	5 58	5 58	5 58	5 58	5 58	5 57	5 57	5 56	S.	
10	R.	6 15	6 16	6 17	6 17	6 17	6 16	6 15	6 14	6 13	6 11	6 10	6 09	6 07	6 06	6 04	6 03	6 02	6 00	5 58	5 56	5 55	5 53	5 51	5 50	5 48	R.	10
	S.	5 49	5 51	5 53	5 55	5 56	5 57	5 58	5 58	5 58	5 58	5 58	5 59	5 58	5 58	5 58	5 58	5 58	5 58	5 58	5 58	5 58	5 58	5 57	5 57	5 56	S.	
11	R.	6 17	6 18	6 19	6 18	6 18	6 17	6 16	6 15	6 14	6 12	6 11	6 10	6 08	6 07	6 05	6 04	6 02	6 00	5 58	5 57	5 55	5 53	5 52	5 50	5 48	R.	11
	S.	5 47	5 49	5 52	5 53	5 54	5 55	5 56	5 57	5 57	5 57	5 57	5 58	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 56	S.	
12	R.	6 18	6 20	6 20	6 20	6 20	6 19	6 18	6 16	6 15	6 13	6 12	6 11	6 09	6 08	6 06	6 04	6 03	6 01	5 59	5 58	5 56	5 54	5 52	5 50	5 48	R.	12
	S.	5 45	5 48	5 50	5 52	5 53	5 54	5 55	5 55	5 56	5 56	5 56	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 57	5 56	S.	
13	R.	6 20	6 22	6 22	6 22	6 21	6 20	6 19	6 18	6 16	6 15	6 13	6 12	6 10	6 09	6 07	6 05	6 03	6 01	5 59	5 58	5 56	5 54	5 52	5 50	5 48	R.	13
	S.	5 43	5 46	5 48	5 50	5 51	5 52	5 53	5 54	5 54	5 55	5 55	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	S.	
14	R.	6 22	6 23	6 24	6 23	6 23	6 22	6 20	6 19	6 17	6 16	6 14	6 13	6 11	6 09	6 07	6 06	6 04	6 02	6 00	5 58	5 56	5 54	5 52	5 50	5 48	R.	14
	S.	5 42	5 44	5 46	5 48	5 50	5 51	5 52	5 53	5 53	5 54	5 54	5 55	5 55	5 55	5 55	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	S.	
15	R.	6 24	6 25	6 26	6 25	6 24	6 23	6 22	6 20	6 19	6 17	6 15	6 14	6 12	6 10	6 08	6 06	6 04	6 02	6 00	5 58	5 56	5 54	5 52	5 50	5 48	R.	15
	S.	5 40	5 42	5 45	5 47	5 48	5 49	5 50	5 51	5 52	5 53	5 53	5 54	5 54	5 55	5 55	5 55	5 55	5 55	5 55	5 56	5 56	5 56	5 56	5 56	5 56	S.	
16	R.	6 26	6 27	6 27	6 26	6 26	6 25	6 23	6 22	6 20	6 18	6 16	6 15	6 13	6 11	6 09	6 07	6 05	6 03	6 01	5 59	5 57	5 55	5 52	5 50	5 48	R.	16
	S.	5 38	5 40	5 43	5 45	5 47	5 48	5 49	5 50	5 51	5 52	5 52	5 53	5 53	5 54	5 51	5 55	5 55	5 55	5 55	5 56	5 56	5 56	5 56	5 56	5 56	S.	
17	R.	6 28	6 29	6 29	6 28	6 28	6 26	6 25	6 23	6 21	6 19	6 18	6 16	6 14	6 12	6 10	6 08	6 06	6 03	6 01	5 59	5 57	5 55	5 53	5 50	5 48	R.	17
	S.	5 36	5 38	5 41	5 43	5 45	5 46	5 47	5 48	5 49	5 50	5 51	5 52	5 52	5 53	5 53	5 54	5 54	5 54	5 54	5 55	5 55	5 56	5 56	5 56	5 56	S.	
18	R.	6 30	6 31	6 31	6 30	6 29	6 28	6 26	6 24	6 22	6 20	6 19	6 17	6 15	6 13	6 10	6 08	6 06	6 04	6 01	5 59	5 57	5 55	5 53	5 50	5 48	R.	18
	S.	5 34	5 37	5 40	5 42	5 43	5 45	5 46	5 47	5 48	5 49	5 50	5 51	5 51	5 52	5 52	5 53	5 53	5 54	5 54	5 55	5 55	5 56	5 56	5 56	5 56	S.	
19	R.	6 32	6 33	6 33	6 32	6 31	6 29	6 28	6 26	6 24	6 22	6 20	6 18	6 16	6 14	6 11	6 09	6 07	6 04	6 02	6 00	5 58	5 55	5 53	5 50	5 48	R.	19
	S.	5 32	5 35	5 38	5 40	5 42	5 43	5 45	5 46	5 47	5 48	5 49	5 50	5 50	5 51	5 51	5 52	5 53	5 53	5 54	5 55	5 55	5 55	5 56	5 56	5 56	S.	
20	R.	6 34	6 35	6 35	6 33	6 32	6 31	6 29	6 27	6 25	6 23	6 21	6 19	6 16	6 14	6 12	6 10	6 07	6 05	6 02	6 00	5 58	5 55	5 53	5 50	5 48	R.	20
	S.	5 30	5 33	5 36	5 38	5 40	5 42	5 43	5 45	5 46	5 47	5 48	5 49	5 49	5 50	5 51	5 52	5 52	5 53	5 53	5 54	5 55	5 55	5 56	5 56	5 56	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

South Latitude: 21° to 40°—June 22 to September 23.

[R = Local mean time of sun's visible rising. S = Local mean time of sun's visible setting.]

Lat. S.	Approx. date	JUNE.	JULY.					AUGUST.										SEPTEMBER.									Approx. date	Lat. S.
		22	3	12	19	24	28	2	5	9	12	16	19	22	25	28	30	2	5	8	10	13	16	18	21	23		
	Dec. N.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
21	R.	6 36	6 37	6 37	6 35	6 34	6 32	6 30	6 28	6 26	6 24	6 22	6 20	6 17	6 15	6 13	6 11	6 08	6 05	6 03	6 01	5 58	5 56	5 53	5 51	5 48	R.	21
	S.	5 28	5 31	5 34	5 36	5 38	5 40	5 42	5 43	5 44	5 46	5 47	5 48	5 48	5 49	5 50	5 51	5 51	5 52	5 53	5 54	5 54	5 55	5 55	5 56	5 56	S.	
22	R.	6 38	6 39	6 38	6 37	6 36	6 34	6 32	6 30	6 27	6 25	6 23	6 21	6 18	6 16	6 13	6 11	6 09	6 06	6 03	6 01	5 58	5 56	5 53	5 51	5 48	R.	22
	S.	5 26	5 29	5 32	5 35	5 37	5 39	5 40	5 42	5 43	5 45	5 46	5 47	5 47	5 48	5 49	5 50	5 51	5 52	5 52	5 53	5 54	5 55	5 55	5 56	5 56	S.	
23	R.	6 40	6 41	6 40	6 39	6 37	6 35	6 33	6 31	6 29	6 26	6 24	6 22	6 19	6 17	6 14	6 12	6 09	6 06	6 04	6 02	5 59	5 56	5 53	5 51	5 48	R.	23
	S.	5 24	5 27	5 30	5 33	5 35	5 37	5 39	5 40	5 42	5 43	5 45	5 46	5 46	5 47	5 48	5 49	5 50	5 51	5 52	5 53	5 54	5 55	5 55	5 56	5 56	S.	
24	R.	6 42	6 43	6 42	6 40	6 39	6 37	6 35	6 33	6 30	6 28	6 25	6 23	6 20	6 18	6 15	6 13	6 10	6 07	6 04	6 02	5 59	5 56	5 53	5 51	5 48	R.	24
	S.	5 22	5 25	5 28	5 31	5 34	5 36	5 37	5 39	5 40	5 42	5 43	5 44	5 45	5 46	5 48	5 49	5 50	5 51	5 51	5 52	5 53	5 54	5 55	5 56	5 56	S	
25	R.	6 44	6 45	6 44	6 42	6 41	6 39	6 37	6 34	6 32	6 29	6 27	6 24	6 21	6 19	6 16	6 13	6 11	6 08	6 05	6 02	6 00	5 57	5 54	5 51	5 48	R.	25
	S.	5 20	5 23	5 26	5 29	5 32	5 34	5 36	5 37	5 39	5 40	5 42	5 43	5 44	5 46	5 47	5 48	5 49	5 50	5 51	5 52	5 53	5 54	5 55	5 56	5 56	S.	
26	R.	6 46	6 47	6 46	6 44	6 42	6 40	6 38	6 35	6 33	6 30	6 28	6 25	6 22	6 19	6 16	6 14	6 11	6 08	6 05	6 03	6 00	5 57	5 54	5 51	5 48	R.	26
	S.	5 18	5 21	5 24	5 27	5 30	5 32	5 34	5 36	5 38	5 39	5 41	5 42	5 43	5 45	5 46	5 47	5 48	5 49	5 50	5 52	5 53	5 54	5 55	5 56	5 56	S.	
27	R.	6 48	6 49	6 48	6 46	6 44	6 42	6 40	6 37	6 34	6 31	6 29	6 26	6 23	6 20	6 17	6 15	6 12	6 09	6 06	6 03	6 00	5 57	5 54	5 51	5 48	R.	27
	S.	5 15	5 18	5 22	5 25	5 28	5 31	5 33	5 35	5 36	5 38	5 40	5 41	5 42	5 44	5 45	5 47	5 48	5 49	5 50	5 51	5 52	5 54	5 55	5 56	5 57	S.	
28	R.	6 50	6 51	6 50	6 48	6 46	6 44	6 41	6 38	6 36	6 33	6 30	6 27	6 24	6 21	6 18	6 15	6 12	6 09	6 06	6 03	6 00	5 57	5 54	5 51	5 48	R.	28
	S.	5 13	5 16	5 20	5 23	5 26	5 29	5 31	5 33	5 35	5 37	5 39	5 40	5 41	5 43	5 44	5 46	5 47	5 48	5 49	5 51	5 52	5 53	5 54	5 56	5 57	S.	
29	R.	6 53	6 53	6 52	6 50	6 48	6 46	6 43	6 40	6 37	6 34	6 31	6 28	6 25	6 22	6 19	6 16	6 13	6 10	6 07	6 04	6 01	5 57	5 54	5 51	5 48	R.	29
	S.	5 11	5 14	5 18	5 21	5 24	5 27	5 29	5 31	5 33	5 35	5 37	5 39	5 40	5 42	5 43	5 45	5 46	5 48	5 49	5 51	5 52	5 53	5 54	5 56	5 57	S.	
30	R.	6 55	6 55	6 54	6 52	6 50	6 47	6 45	6 42	6 39	6 36	6 33	6 30	6 26	6 23	6 20	6 17	6 14	6 10	6 07	6 04	6 01	5 57	5 54	5 51	5 48	R.	30
	S.	5 09	5 12	5 16	5 19	5 22	5 25	5 28	5 30	5 32	5 34	5 36	5 38	5 39	5 41	5 43	5 45	5 46	5 47	5 48	5 50	5 52	5 53	5 54	5 56	5 57	S.	
31	R.	6 57	6 58	6 57	6 54	6 52	6 49	6 46	6 43	6 40	6 37	6 34	6 31	6 27	6 24	6 21	6 18	6 15	6 11	6 08	6 05	6 01	5 58	5 54	5 51	5 48	R.	31
	S.	5 06	5 10	5 14	5 17	5 20	5 23	5 26	5 28	5 30	5 32	5 34	5 36	5 38	5 40	5 42	5 44	5 45	5 46	5 48	5 50	5 51	5 53	5 54	5 56	5 57	S.	
32	R.	7 00	7 00	6 59	6 56	6 54	6 51	6 48	6 45	6 42	6 38	6 35	6 32	6 28	6 25	6 22	6 19	6 15	6 12	6 08	6 05	6 02	5 58	5 54	5 51	5 48	R.	32
	S.	5 04	5 07	5 12	5 15	5 18	5 21	5 24	5 27	5 29	5 31	5 33	5 35	5 37	5 39	5 41	5 48	5 44	5 46	5 47	5 49	5 51	5 53	5 54	5 56	5 57	S.	
33	R.	7 02	7 03	7 01	6 59	6 56	6 53	6 50	6 47	6 43	6 40	6 37	6 33	6 30	6 26	6 23	6 20	6 16	6 12	6 09	6 06	6 02	5 58	5 55	5 51	5 48	R.	33
	S.	5 01	5 05	5 09	5 13	5 16	5 19	5 22	5 25	5 27	5 30	5 32	5 34	5 36	5 38	5 40	5 42	5 43	5 45	5 47	5 49	5 50	5 52	5 54	5 55	5 57	S.	
34	R.	7 05	7 05	7 03	7 01	6 58	6 55	6 52	6 48	6 45	6 41	6 38	6 35	6 31	6 27	6 24	6 20	6 17	6 13	6 09	6 06	6 02	5 58	5 55	5 51	5 48	R.	34
	S.	4 59	5 02	5 07	5 11	5 14	5 18	5 21	5 23	5 26	5 28	5 30	5 33	5 35	5 37	5 39	5 41	5 43	5 45	5 46	5 48	5 50	5 52	5 54	5 55	5 57	S.	
35	R.	7 07	7 08	7 06	7 03	7 00	6 57	6 54	6 50	6 47	6 43	6 40	6 36	6 32	6 29	6 25	6 21	6 18	6 14	6 10	6 07	6 03	5 59	5 55	5 51	5 48	R.	35
	S.	4 56	5 00	5 05	5 09	5 12	5 16	5 19	5 21	5 24	5 26	5 29	5 31	5 33	5 36	5 38	5 40	5 42	5 44	5 46	5 48	5 50	5 52	5 53	5 55	5 57	S.	
36	R.	7 10	7 10	7 08	7 05	7 02	6 59	6 56	6 52	6 48	6 45	6 41	6 37	6 33	6 30	6 26	6 22	6 18	6 14	6 10	6 07	6 03	5 59	5 55	5 51	5 48	R.	36
	S.	4 54	4 57	5 02	5 06	5 10	5 14	5 17	5 20	5 22	5 25	5 27	5 30	5 32	5 35	5 37	5 39	5 41	5 43	5 45	5 47	5 49	5 51	5 53	5 55	5 57	S.	
37	R.	7 13	7 13	7 11	7 08	7 05	7 01	6 58	6 54	6 50	6 46	6 43	6 39	6 35	6 31	6 27	6 23	6 19	6 15	6 11	6 08	6 04	6 00	5 56	5 52	5 48	R.	37
	S.	4 51	4 55	5 00	5 04	5 08	5 11	5 15	5 18	5 20	5 23	5 26	5 29	5 31	5 34	5 36	5 38	5 40	5 42	5 44	5 47	5 49	5 51	5 53	5 55	5 57	S.	
38	R.	7 16	7 16	7 13	7 10	7 07	7 03	7 00	6 56	6 52	6 48	6 44	6 40	6 36	6 32	6 28	6 24	6 20	6 16	6 12	6 08	6 04	6 00	5 56	5 52	5 47	R.	38
	S.	4 48	4 52	4 57	5 01	5 05	5 09	5 13	5 16	5 19	5 22	5 24	5 27	5 30	5 33	5 35	5 37	5 40	5 42	5 44	5 46	5 49	5 51	5 53	5 55	5 57	S.	
39	R.	7 19	7 19	7 16	7 13	7 10	7 06	7 02	6 58	6 54	6 50	6 46	6 42	6 37	6 33	6 29	6 25	6 21	6 17	6 13	6 09	6 04	6 00	5 56	5 52	5 47	R.	39
	S.	4 45	4 49	4 54	4 59	5 03	5 07	5 10	5 14	5 17	5 20	5 23	5 26	5 28	5 31	5 34	5 36	5 39	5 41	5 43	5 46	5 48	5 51	5 53	5 55	5 57	S.	
40	R.	7 22	7 22	7 19	7 15	7 12	7 08	7 04	7 00	6 56	6 51	6 47	6 43	6 39	6 34	6 30	6 26	6 22	6 18	6 13	6 09	6 05	6 00	5 56	5 52	5 47	R.	40
	S.	4 42	4 46	4 52	4 56	5 00	5 04	5 08	5 12	5 15	5 18	5 21	5 24	5 27	5 30	5 33	5 35	5 38	5 40	5 42	5 45	5 48	5 50	5 53	5 55	5 57	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

South Latitude: 41° to 60°—June 22 to September 23.

[R = Local mean time of sun's visible rising. S = Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	JUNE.	JULY.					AUGUST.										SEPTEMBER.									Approx. date.	Lat. S.
		22	3	12	19	24	28	2	5	9	12	16	19	22	25	28	30	2	5	8	10	13	16	18	21	23		
	Dec. N.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. N.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
41	R.	7 25	7 25	7 22	7 18	7 15	7 11	7 07	7 02	6 58	6 53	6 49	6 45	6 40	6 36	6 31	6 27	6 23	6 18	6 14	6 10	6 05	6 01	5 56	5 52	5 47	R.	41
	S.	4 39	4 43	4 49	4 53	4 58	5 02	5 06	5 09	5 13	5 16	5 19	5 22	5 25	5 28	5 31	5 34	5 37	5 39	5 42	5 45	5 47	5 50	5 52	5 55	5 57	S.	
42	R.	7 28	7 28	7 25	7 21	7 17	7 13	7 09	7 04	7 00	6 55	6 51	6 46	6 42	6 37	6 32	6 28	6 24	6 19	6 14	6 10	6 06	6 01	5 56	5 52	5 47	R.	42
	S.	4 36	4 40	4 46	4 51	4 55	5 00	5 04	5 07	5 11	5 14	5 18	5 21	5 24	5 27	5 30	5 33	5 36	5 39	5 41	5 44	5 47	5 50	5 52	5 55	5 57	S.	
43	R.	7 31	7 31	7 28	7 24	7 20	7 15	7 11	7 06	7 02	6 57	6 53	6 48	6 43	6 39	6 34	6 29	6 25	6 20	6 15	6 11	6 06	6 01	5 57	5 52	5 47	R.	43
	S.	4 32	4 37	4 43	4 48	4 53	4 57	5 01	5 05	5 09	5 12	5 16	5 19	5 22	5 26	5 29	5 32	5 35	5 38	5 41	5 44	5 46	5 49	5 52	5 55	5 57	S.	
44	R.	7 35	7 34	7 31	7 27	7 23	7 18	7 14	7 09	7 04	6 59	6 54	6 50	6 45	6 40	6 35	6 31	6 26	6 21	6 16	6 11	6 06	6 01	5 57	5 52	5 47	R.	44
	S.	4 29	4 33	4 40	4 45	4 50	4 54	4 59	5 03	5 07	5 10	5 14	5 18	5 21	5 24	5 27	5 31	5 34	5 37	5 40	5 43	5 46	5 49	5 52	5 55	5 58	S.	
45	R.	7 38	7 38	7 34	7 30	7 26	7 21	7 16	7 11	7 06	7 01	6 56	6 51	6 46	6 41	6 36	6 32	6 27	6 22	6 17	6 12	6 07	6 02	5 57	5 52	5 47	R.	45
	S.	4 25	4 30	4 36	4 42	4 47	4 52	4 56	5 00	5 04	5 08	5 12	5 16	5 19	5 23	5 26	5 30	5 33	5 36	5 39	5 43	5 46	5 49	5 52	5 55	5 58	S.	
46	R.	7 42	7 41	7 38	7 33	7 29	7 24	7 19	7 14	7 08	7 03	6 58	6 53	6 48	6 43	6 38	6 33	6 28	6 22	6 17	6 12	6 07	6 02	5 57	5 52	5 47	R.	46
	S.	4 22	4 26	4 33	4 38	4 44	4 49	4 54	4 58	5 02	5 06	5 10	5 14	5 18	5 21	5 25	5 29	5 32	5 35	5 38	5 42	5 45	5 49	5 52	5 55	5 58	S.	
47	R.	7 46	7 45	7 41	7 37	7 32	7 27	7 22	7 16	7 11	7 05	7 00	6 55	6 50	6 45	6 39	6 34	6 29	6 23	6 18	6 13	6 08	6 02	5 57	5 52	5 47	R.	47
	S.	4 18	4 22	4 29	4 35	4 41	4 46	4 51	4 55	5 00	5 04	5 08	5 12	5 16	5 20	5 23	5 27	5 31	5 34	5 38	5 42	5 45	5 48	5 51	5 55	5 58	S.	
48	R.	7 50	7 49	7 45	7 40	7 35	7 30	7 25	7 19	7 13	7 08	7 02	6 57	6 51	6 46	6 41	6 35	6 30	6 24	6 19	6 14	6 08	6 03	5 57	5 52	5 47	R.	48
	S.	4 14	4 18	4 25	4 31	4 37	4 43	4 48	4 53	4 57	5 02	5 06	5 10	5 14	5 18	5 22	5 26	5 30	5 33	5 37	5 41	5 44	5 48	5 51	5 55	5 58	S.	
49	R.	7 54	7 53	7 49	7 44	7 39	7 33	7 28	7 22	7 16	7 10	7 05	6 59	6 53	6 48	6 42	6 37	6 31	6 25	6 19	6 14	6 09	6 03	5 57	5 52	5 47	R.	49
	S.	4 09	4 14	4 21	4 28	4 34	4 39	4 45	4 50	4 54	4 59	5 04	5 08	5 12	5 17	5 21	5 25	5 28	5 32	5 36	5 40	5 44	5 47	5 51	5 55	5 58	S.	
50	R.	7 59	7 58	7 53	7 48	7 43	7 37	7 31	7 25	7 19	7 13	7 07	7 01	6 55	6 50	6 44	6 38	6 32	6 26	6 20	6 15	6 09	6 04	5 58	5 52	5 46	R.	50
	S.	4 05	4 10	4 17	4 24	4 30	4 36	4 42	4 47	4 52	4 57	5 01	5 06	5 10	5 15	5 19	5 23	5 27	5 31	5 35	5 39	5 43	5 47	5 51	5 55	5 58	S.	
51	R.	8 04	8 02	7 58	7 52	7 46	7 40	7 34	7 28	7 22	7 16	7 10	7 04	6 57	6 51	6 45	6 39	6 33	6 27	6 21	6 16	6 10	6 04	5 58	5 52	5 46	R.	51
	S.	4 00	4 05	4 13	4 20	4 26	4 32	4 38	4 44	4 49	4 54	4 59	5 04	5 08	5 13	5 17	5 22	5 26	5 30	5 34	5 38	5 42	5 46	5 50	5 54	5 58	S.	
52	R.	8 09	8 07	8 02	7 56	7 50	7 44	7 38	7 31	7 25	7 18	7 12	7 06	6 59	6 53	6 47	6 41	6 35	6 29	6 23	6 17	6 11	6 04	5 58	5 52	5 46	R.	52
	S.	3 55	4 00	4 08	4 15	4 22	4 28	4 34	4 40	4 46	4 51	4 56	5 01	5 06	5 11	5 16	5 20	5 25	5 29	5 33	5 38	5 42	5 46	5 50	5 54	5 58	S.	
53	R.	8 14	8 13	8 07	8 01	7 54	7 48	7 41	7 35	7 28	7 21	7 15	7 08	7 02	6 55	6 49	6 43	6 36	6 30	6 24	6 18	6 11	6 05	5 59	5 52	5 46	R.	53
	S.	3 49	3 55	4 03	4 11	4 18	4 25	4 31	4 37	4 43	4 48	4 54	4 59	5 04	5 09	5 14	5 19	5 23	5 28	5 32	5 37	5 41	5 46	5 50	5 54	5 58	S.	
54	R.	8 20	8 18	8 12	8 06	7 59	7 52	7 45	7 38	7 31	7 24	7 18	7 11	7 04	6 57	6 51	6 44	6 38	6 31	6 25	6 18	6 12	6 05	5 59	5 52	5 46	R.	54
	S.	3 44	3 49	3 58	4 06	4 14	4 21	4 27	4 33	4 39	4 45	4 51	4 57	5 02	5 07	5 12	5 17	5 22	5 27	5 31	5 36	5 41	5 45	5 50	5 54	5 59	S.	
55	R.	8 26	8 24	8 18	8 11	8 04	7 56	7 49	7 42	7 35	7 28	7 21	7 14	7 07	7 00	6 53	6 46	6 39	6 32	6 26	6 19	6 13	6 06	5 59	5 52	5 46	R.	55
	S.	3 38	3 44	3 53	4 01	4 09	4 16	4 23	4 30	4 36	4 42	4 48	4 54	4 59	5 05	5 10	5 15	5 20	5 25	5 30	5 35	5 40	5 45	5 50	5 54	5 59	S.	
56	R.	8 33	8 30	8 24	8 16	8 09	8 01	7 54	7 46	7 38	7 31	7 24	7 17	7 09	7 02	6 55	6 48	6 41	6 34	6 27	6 20	6 13	6 06	5 59	5 52	5 45	R.	56
	S.	3 31	3 37	3 47	3 55	4 03	4 11	4 19	4 26	4 32	4 39	4 45	4 51	4 56	5 02	5 08	5 13	5 19	5 24	5 29	5 34	5 39	5 44	5 49	5 54	5 59	S.	
57	R.	8 40	8 37	8 30	8 22	8 14	8 06	7 58	7 50	7 42	7 35	7 27	7 20	7 12	7 05	6 57	6 50	6 43	6 35	6 28	6 21	6 14	6 07	6 00	5 52	5 45	R.	57
	S.	3 24	3 30	3 41	3 50	3 58	4 06	4 14	4 21	4 28	4 35	4 41	4 48	4 54	5 00	5 05	5 11	5 17	5 22	5 27	5 33	5 38	5 44	5 49	5 54	5 59	S.	
58	R.	8 47	8 44	8 37	8 28	8 20	8 11	8 03	7 55	7 46	7 38	7 31	7 23	7 15	7 07	6 59	6 52	6 44	6 37	6 29	6 22	6 15	6 07	6 00	5 52	5 45	R.	58
	S.	3 16	3 23	3 34	3 43	3 52	4 01	4 09	4 17	4 24	4 31	4 38	4 45	4 51	4 57	5 03	5 09	5 15	5 21	5 26	5 32	5 38	5 43	5 49	5 54	5 59	S.	
59	R.	8 55	8 52	8 44	8 35	8 26	8 17	8 08	8 00	7 51	7 42	7 34	7 26	7 18	7 10	7 02	6 54	6 46	6 38	6 31	6 23	6 16	6 08	6 00	5 52	5 45	R.	59
	S.	3 08	3 15	3 27	3 37	3 47	3 56	4 04	4 12	4 20	4 27	4 34	4 41	4 48	4 55	5 01	5 07	5 13	5 19	5 25	5 31	5 37	5 43	5 48	5 54	6 00	S.	
60	R.	9 04	9 01	8 52	8 42	8 33	8 23	8 14	8 05	7 56	7 47	7 38	7 30	7 21	7 13	7 04	6 56	6 48	6 40	6 32	6 25	6 17	6 09	6 01	5 53	5 45	R.	60
	S.	2 59	3 06	3 19	3 30	3 40	3 49	3 58	4 07	4 15	4 23	4 30	4 38	4 45	4 52	4 58	5 05	5 11	5 17	5 23	5 30	5 36	5 42	5 48	5 54	6 00	S.	

Mean Time of Sun's Visible Rising and Setting.

South latitude: 0° to 20°—September 23 to December 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	SEPTEMBER.			OCTOBER.												NOVEMBER.							DECEMBER.			Approx. date.	Lat. S.
		23	26	28	1	4	6	9	11	14	17	19	22	25	28	31	3	6	10	14	17	22	27	3	11	22		
	Dec. S.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. S.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
0	R.	5 49	5 48	5 47	5 46	5 45	5 44	5 44	5 43	5 42	5 42	5 41	5 41	5 40	5 40	5 40	5 40	5 40	5 40	5 40	5 41	5 42	5 44	5 46	5 49	5 54	R.	0
	S.	5 56	5 55	5 55	5 54	5 53	5 52	5 52	5 51	5 50	5 50	5 49	5 49	5 48	5 48	5 48	5 48	5 48	5 48	5 48	5 49	5 50	5 52	5 54	5 57	6 02	S.	
1	R.	5 49	5 48	5 47	5 46	5 45	5 44	5 44	5 43	5 42	5 41	5 41	5 40	5 40	5 39	5 39	5 39	5 39	5 39	5 39	5 40	5 41	5 42	5 44	5 48	5 53	R.	1
	S.	5 56	5 55	5 55	5 54	5 53	5 52	5 52	5 51	5 50	5 50	5 50	5 49	5 49	5 49	5 49	5 49	5 49	5 49	5 50	5 51	5 52	5 53	5 55	5 59	6 04	S.	
2	R.	5 49	5 48	5 47	5 46	5 45	5 44	5 44	5 43	5 42	5 41	5 40	5 40	5 39	5 38	5 38	5 38	5 38	5 38	5 38	5 39	5 40	5 41	5 43	5 46	5 51	R.	2
	S.	5 56	5 55	5 55	5 54	5 53	5 52	5 52	5 51	5 51	5 51	5 50	5 50	5 49	5 49	5 50	5 50	5 50	5 50	5 51	5 52	5 53	5 55	5 57	6 00	6 05	S.	
3	R.	5 49	5 48	5 47	5 46	5 45	5 44	5 43	5 42	5 41	5 40	5 39	5 39	5 38	5 37	5 37	5 37	5 37	5 37	5 37	5 37	5 38	5 39	5 41	5 44	5 49	R.	3
	S.	5 56	5 55	5 55	5 54	5 54	5 53	5 52	5 51	5 51	5 51	5 51	5 51	5 50	5 50	5 51	5 51	5 51	5 51	5 52	5 53	5 55	5 56	5 58	6 02	6 07	S.	
4	R.	5 49	5 48	5 47	5 46	5 45	5 44	5 43	5 42	5 41	5 40	5 39	5 38	5 37	5 36	5 36	5 36	5 36	5 35	5 35	5 36	5 36	5 38	5 39	5 43	5 48	R.	4
	S.	5 56	5 55	5 55	5 54	5 54	5 53	5 53	5 52	5 52	5 52	5 52	5 51	5 51	5 51	5 52	5 52	5 52	5 52	5 53	5 55	5 56	5 58	6 00	6 04	6 09	S.	
5	R.	5 49	5 48	5 46	5 45	5 44	5 43	5 42	5 41	5 40	5 39	5 38	5 37	5 36	5 35	5 35	5 35	5 34	5 34	5 34	5 34	5 35	5 36	5 38	5 41	5 46	R.	5
	S.	5 56	5 55	5 55	5 54	5 54	5 53	5 53	5 53	5 53	5 53	5 53	5 52	5 52	5 52	5 53	5 53	5 53	5 54	5 55	5 56	5 58	5 59	6 02	6 05	6 11	S.	
6	R.	5 48	5 47	5 46	5 45	5 44	5 43	5 42	5 40	3 39	5 38	5 37	5 37	5 36	5 35	5 34	5 34	5 33	5 33	5 33	5 33	5 33	5 35	5 36	5 40	5 44	R.	6
	S.	5 56	5 55	5 55	5 54	5 54	5 54	5 54	5 53	5 53	5 53	5 53	5 53	5 53	5 53	5 54	5 54	5 54	5 55	5 56	5 57	5 59	6 01	6 03	6 07	6 12	S.	
7	R.	5 48	5 47	5 46	5 45	5 44	5 42	5 41	5 40	5 39	5 38	5 37	5 36	5 35	5 34	5 33	5 32	5 32	5 31	5 31	5 32	5 32	5 33	5 34	5 38	5 42	R.	7
	S.	5 56	5 55	5 55	5 55	5 55	5 54	5 54	5 54	5 54	5 54	5 54	5 54	5 54	5 54	5 55	5 55	5 56	5 56	5 57	5 59	6 01	6 03	6 05	6 09	6 14	S.	
8	R.	5 48	5 47	5 46	5 45	5 43	5 42	5 41	5 39	5 38	5 37	5 36	5 35	5 34	5 33	5 32	5 31	5 31	5 30	5 30	5 30	5 30	5 31	5 33	5 36	5 41	R.	8
	S.	5 56	5 55	5 55	5 55	5 55	5 55	5 55	5 54	5 54	5 54	5 55	5 55	5 55	5 55	5 56	5 56	5 57	5 58	5 59	6 00	6 02	6 04	6 07	6 11	6 16	S.	
9	R.	5 48	5 47	5 46	5 44	5 43	5 41	5 40	5 39	5 37	5 36	5 35	5 34	5 33	5 32	5 31	5 30	5 29	5 29	5 28	5 29	5 29	5 30	5 31	5 34	5 39	R.	9
	S.	5 56	5 56	5 56	5 55	5 55	5 55	5 55	5 55	5 55	5 55	5 56	5 56	5 56	5 56	5 57	5 57	5 58	5 59	6 00	6 02	6 04	6 06	6 09	6 13	6 18	S.	
10	R.	5 48	5 47	5 46	5 44	5 43	5 41	5 40	5 38	5 37	5 36	5 34	5 33	5 32	5 31	5 30	5 29	5 28	5 28	5 27	5 27	5 27	5 28	5 29	5 32	5 37	R.	10
	S.	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 57	5 58	5 58	5 59	6 00	6 01	6 03	6 05	6 07	6 10	6 14	6 19	S.	
11	R.	5 48	5 47	5 46	5 44	5 42	5 41	5 39	5 37	5 36	5 35	5 33	5 32	5 31	5 30	5 29	5 28	5 27	5 26	5 26	5 26	5 26	5 27	5 28	5 30	5 35	R.	11
	S.	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 56	5 57	5 57	5 57	5 57	5 58	5 59	5 59	6 00	6 01	6 03	6 05	6 07	6 09	6 12	6 16	6 21	S.	
12	R.	5 48	5 47	5 46	5 44	5 42	5 40	5 39	5 37	5 36	5 34	5 33	5 32	5 30	5 29	5 28	5 27	5 26	5 25	5 25	5 25	5 25	5 25	5 26	5 29	5 33	R.	12
	S.	5 56	5 56	5 56	5 56	5 56	5 56	5 57	5 57	5 57	5 57	5 58	5 58	5 58	5 59	6 00	6 00	6 01	6 02	6 04	6 06	6 08	6 10	6 13	6 18	6 23	S.	
13	R.	5 48	5 47	5 45	5 43	5 42	5 40	5 38	5 36	5 35	5 33	5 32	5 31	5 29	5 28	5 27	5 26	5 25	5 24	5 23	5 23	5 23	5 24	5 24	5 27	5 31	R.	13
	S.	5 56	5 56	5 56	5 56	5 57	5 57	5 57	5 57	5 58	5 58	5 59	5 59	5 59	6 00	6 01	6 02	6 03	6 04	6 05	6 07	6 10	6 12	6 15	6 20	6 25	S.	
14	R.	5 48	5 47	5 45	5 43	5 42	5 40	5 38	5 36	5 34	5 33	5 31	5 30	5 28	5 27	5 26	5 25	5 24	5 23	5 22	5 22	5 21	5 22	5 23	5 25	5 29	R.	14
	S.	5 56	5 56	5 56	5 56	5 57	5 57	5 58	5 58	5 58	5 59	5 59	6 00	6 00	6 01	6 02	6 03	6 04	6 05	6 07	6 09	6 11	6 14	6 17	6 22	6 27	S.	
15	R.	5 48	5 46	5 45	5 43	5 41	5 39	5 37	5 35	5 34	5 32	5 30	5 29	5 27	5 26	5 25	5 24	5 22	5 21	5 20	5 20	5 20	5 20	5 21	5 23	5 27	R.	15
	S.	5 56	5 56	5 57	5 57	5 57	5 57	5 58	5 58	5 59	5 59	6 00	6 01	6 01	6 02	6 03	6 04	6 05	6 06	6 08	6 10	6 13	6 15	6 19	6 24	6 29	S.	
16	R.	5 48	5 46	5 45	5 43	5 41	5 39	5 37	5 35	5 33	5 32	5 30	5 28	5 26	5 25	5 24	5 23	5 21	5 20	5 19	5 19	5 19	5 19	5 19	5 21	5 25	R.	16
	S.	5 56	5 56	5 57	5 57	5 58	5 58	5 59	5 59	5 59	6 00	6 01	6 01	6 02	6 03	6 04	6 05	6 06	6 08	6 10	6 12	6 14	6 17	6 20	6 25	6 31	S.	
17	R.	5 48	5 46	5 45	5 42	5 40	5 38	5 36	5 34	5 32	5 31	5 29	5 27	5 25	5 24	5 22	5 21	5 20	5 18	5 17	5 17	5 17	5 17	5 17	5 19	5 23	R.	17
	S.	5 56	5 56	5 57	5 57	5 58	5 58	5 59	5 59	6 00	6 01	6 02	6 02	6 03	6 04	6 05	6 06	6 08	6 09	6 11	6 14	6 16	6 19	6 22	6 27	6 33	S.	
18	R.	5 48	5 46	5 45	5 42	5 40	5 38	5 36	5 34	5 32	5 30	5 28	5 26	5 24	5 23	5 21	5 20	5 19	5 17	5 16	5 15	5 15	5 15	5 16	5 18	5 21	R.	18
	S.	5 56	5 56	5 57	5 57	5 58	5 58	5 59	6 00	6 01	6 01	6 02	6 03	6 04	6 05	6 06	6 07	6 09	6 11	6 13	6 15	6 18	6 20	6 24	6 29	6 35	S.	
19	R.	5 48	5 46	5 44	5 42	5 40	5 38	5 36	5 33	5 31	5 29	5 27	5 25	5 23	5 22	5 20	5 19	5 17	5 16	5 14	5 14	5 13	5 13	5 14	5 16	5 19	R.	19
	S.	5 56	5 56	5 57	5 58	5 59	5 59	6 00	6 00	6 01	6 02	6 03	6 04	6 05	6 06	6 07	6 09	6 10	6 12	6 14	6 17	6 19	6 22	6 26	6 31	6 37	S.	
20	R.	5 48	5 46	5 44	5 42	5 40	5 37	5 35	5 33	5 31	5 29	5 27	5 25	5 22	5 21	5 19	5 18	5 16	5 15	5 13	5 12	5 12	5 12	5 12	5 14	5 17	R.	20
	S.	5 56	5 56	5 57	5 58	5 59	5 59	6 00	6 01	6 02	6 03	6 04	6 05	6 06	6 07	6 08	6 10	6 12	6 14	6 16	6 18	6 21	6 24	6 28	6 33	6 39	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

South latitude: 21° to 40°—September 23 to December 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	SEPTEMBER. 23	26	28	OCTOBER. 1	4	6	9	11	14	17	19	22	25	28	31
	Dec. S.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
21	R.	5 48	5 46	5 44	5 41	5 39	5 37	5 35	5 32	5 30	5 28	5 26	5 24	5 21	5 19	5 18
	S.	5 56	5 57	5 58	5 58	5 59	6 00	6 01	6 01	6 03	6 04	6 05	6 06	6 07	6 08	6 10
22	R.	5 48	5 46	5 44	5 41	5 39	5 36	5 34	5 32	5 29	5 27	5 25	5 23	5 20	5 18	5 17
	S.	5 56	5 57	5 58	5 58	5 59	6 00	6 01	6 02	6 03	6 04	6 05	6 07	6 08	6 09	6 11
23	R.	5 48	5 46	5 44	5 41	5 39	5 36	5 34	5 31	5 29	5 27	5 24	5 22	5 19	5 17	5 15
	S.	5 56	5 57	5 58	5 59	6 00	6 01	6 02	6 03	6 04	6 05	6 06	6 08	6 09	6 10	6 12
24	R.	5 48	5 46	5 44	5 41	5 38	5 35	5 33	5 30	5 28	5 26	5 23	5 21	5 18	5 16	5 14
	S.	5 56	5 57	5 58	5 59	6 00	6 01	6 02	6 03	6 04	6 06	6 07	6 09	6 10	6 11	6 13
25	R.	5 48	5 46	5 43	5 40	5 38	5 35	5 33	5 30	5 27	5 25	5 22	5 20	5 17	5 15	5 13
	S.	5 56	5 57	5 58	5 59	6 01	6 02	6 03	6 04	6 05	6 07	6 08	6 10	6 11	6 13	6 15
26	R.	5 48	5 45	5 43	5 40	5 38	5 35	5 32	5 29	5 27	5 24	5 21	5 19	5 16	5 14	5 12
	S.	5 56	5 57	5 58	5 59	6 01	6 02	6 03	6 04	6 06	6 07	6 09	6 11	6 12	6 14	6 16
27	R.	5 48	5 45	5 43	5 40	5 37	5 34	5 32	5 29	5 26	5 23	5 20	5 18	5 15	5 13	5 10
	S.	5 57	5 58	5 59	6 00	6 01	6 02	6 04	6 05	6 07	6 08	6 10	6 12	6 13	6 15	6 17
28	R.	5 48	5 45	5 42	5 39	5 37	5 34	5 31	5 28	5 25	5 22	5 19	5 17	5 14	5 11	5 09
	S.	5 57	5 58	5 59	6 00	6 02	6 03	6 04	6 06	6 08	6 09	6 11	6 13	6 14	6 16	6 19
29	R.	5 48	5 45	5 42	5 39	5 36	5 33	5 30	5 27	5 24	5 21	5 18	5 16	5 13	5 10	5 07
	S.	5 57	5 58	5 59	6 00	6 02	6 03	6 05	6 07	6 09	6 10	6 12	6 14	6 16	6 18	6 20
30	R.	5 48	5 45	5 42	5 39	5 36	5 33	5 30	5 26	5 23	5 20	5 17	5 15	5 12	5 09	5 06
	S.	5 57	5 58	5 59	6 01	6 02	6 04	6 06	6 07	6 09	6 11	6 13	6 15	6 17	6 19	6 21
31	R.	5 48	5 45	5 42	5 39	5 36	5 32	5 29	5 26	5 22	5 19	5 16	5 13	5 10	5 07	5 05
	S.	5 57	5 58	6 00	6 01	6 03	6 04	6 06	6 08	6 10	6 12	6 14	6 16	6 18	6 20	6 23
32	R.	5 48	5 44	5 41	5 38	5 35	5 32	5 29	5 25	5 22	5 18	5 15	5 12	5 09	5 06	5 03
	S.	5 57	5 58	6 00	6 01	6 03	6 05	6 07	6 09	6 11	6 13	6 15	6 17	6 19	6 21	6 24
33	R.	5 48	5 44	5 41	5 38	5 35	5 31	5 28	5 24	5 21	5 17	5 14	5 11	5 08	5 05	5 02
	S.	5 57	5 58	6 00	6 02	6 04	6 06	6 08	6 10	6 12	6 14	6 16	6 18	6 21	6 23	6 26
34	R.	5 48	5 44	5 41	5 37	5 34	5 30	5 27	5 23	5 20	5 16	5 13	5 10	5 07	5 03	5 00
	S.	5 57	5 58	6 00	6 02	6 04	6 06	6 08	6 10	6 12	6 15	6 17	6 19	6 22	6 24	6 27
35	R.	5 48	5 44	5 41	5 37	5 34	5 30	5 26	5 23	5 19	5 15	5 12	5 09	5 05	5 02	4 59
	S.	5 57	5 58	6 01	6 03	6 05	6 07	6 09	6 11	6 13	6 16	6 18	6 21	6 23	6 26	6 29
36	R.	5 48	5 44	5 41	5 37	5 33	5 29	5 26	5 22	5 18	5 14	5 11	5 08	5 04	5 00	4 57
	S.	5 57	5 59	6 01	6 03	6 05	6 07	6 10	6 12	6 14	6 17	6 19	6 22	6 25	6 27	6 30
37	R.	5 48	5 44	5 40	5 36	5 33	5 28	5 25	5 21	5 17	5 13	5 10	5 06	5 02	4 59	4 55
	S.	5 57	5 59	6 01	6 03	6 06	6 08	6 11	6 13	6 15	6 18	6 21	6 23	6 26	6 29	6 32
38	R.	5 47	5 44	5 40	5 36	5 32	5 28	5 24	5 20	5 16	5 12	5 09	5 05	5 01	4 57	4 54
	S.	5 57	5 59	6 02	6 04	6 06	6 09	6 11	6 13	6 16	6 19	6 22	6 25	6 28	6 31	6 34
39	R.	5 47	5 43	5 39	5 35	5 31	5 27	5 23	5 19	5 15	5 11	5 07	5 03	4 59	4 55	4 52
	S.	5 57	5 59	6 02	6 04	6 07	6 09	6 12	6 14	6 17	6 20	6 23	6 26	6 29	6 32	6 36
40	R.	5 47	5 43	5 39	5 35	5 31	5 27	5 23	5 18	5 14	5 10	5 06	5 02	4 58	4 54	4 50
	S.	5 57	5 59	6 02	6 05	6 07	6 10	6 13	6 15	6 18	6 21	6 24	6 27	6 31	6 34	6 37

Lat. S.	Approx. date.	NOVEMBER. 3	6	10	14	17	22	27	DECEMBER. 3	11	22
	Dec. S.	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
21	R.	5 16	5 14	5 13	5 12	5 11	5 10	5 10	5 10	5 11	5 15
	S.	6 11	6 13	6 15	6 17	6 20	6 23	6 26	6 30	6 35	6 41
22	R.	5 15	5 13	5 11	5 10	5 09	5 08	5 08	5 08	5 09	5 13
	S.	6 12	6 14	6 16	6 19	6 21	6 24	6 28	6 32	6 37	6 43
23	R.	5 14	5 12	5 10	5 08	5 07	5 06	5 06	5 06	5 07	5 11
	S.	6 14	6 16	6 18	6 20	6 23	6 26	6 30	6 34	6 39	6 45
24	R.	5 12	5 10	5 08	5 07	5 06	5 05	5 04	5 04	5 05	5 09
	S.	6 15	6 17	6 19	6 22	6 25	6 28	6 31	6 36	6 41	6 47
25	R.	5 11	5 09	5 07	5 05	5 04	5 03	5 02	5 02	5 03	5 07
	S.	6 17	6 19	6 21	6 24	6 27	6 30	6 33	6 38	6 44	6 50
26	R.	5 10	5 07	5 05	5 03	5 02	5 01	5 00	5 00	5 01	5 05
	S.	6 18	6 20	6 22	6 25	6 28	6 31	6 35	6 40	6 46	6 52
27	R.	5 08	5 06	5 04	5 02	5 01	4 59	4 58	4 58	4 59	5 02
	S.	6 19	6 22	6 24	6 27	6 30	6 33	6 37	6 42	6 48	6 54
28	R.	5 07	5 04	5 02	5 00	4 59	4 57	4 56	4 56	4 57	5 00
	S.	6 21	6 23	6 25	6 28	6 31	6 35	6 39	6 44	6 50	6 56
29	R.	5 05	5 03	5 00	4 58	4 57	4 55	4 54	4 53	4 54	4 58
	S.	6 22	6 25	6 27	6 30	6 33	6 37	6 41	6 46	6 52	6 59
30	R.	5 04	5 01	4 59	4 57	4 55	4 53	4 52	4 51	4 52	4 55
	S.	6 24	6 26	6 29	6 32	6 35	6 39	6 43	6 48	6 55	7 01
31	R.	5 02	5 00	4 57	4 55	4 53	4 51	4 50	4 49	4 49	4 53
	S.	6 25	6 28	6 31	6 34	6 37	6 41	6 46	6 51	6 57	7 04
32	R.	5 01	4 58	4 55	4 53	4 51	4 49	4 48	4 46	4 47	4 50
	S.	6 27	6 30	6 33	6 36	6 39	6 43	6 48	6 53	7 00	7 06
33	R.	4 59	4 56	4 53	4 51	4 49	4 47	4 45	4 44	4 44	4 48
	S.	6 28	6 31	6 34	6 38	6 42	6 46	6 50	6 56	7 02	7 09
34	R.	4 57	4 54	4 51	4 49	4 47	4 45	4 43	4 41	4 42	4 45
	S.	6 30	6 33	6 36	6 40	6 44	6 48	6 53	6 58	7 04	7 11
35	R.	4 56	4 53	4 50	4 47	4 45	4 42	4 40	4 39	4 39	4 42
	S.	6 32	6 35	6 38	6 42	6 46	6 50	6 55	7 01	7 07	7 14
36	R.	4 54	4 51	4 48	4 45	4 42	4 40	4 38	4 36	4 36	4 39
	S.	6 33	6 37	6 40	6 44	6 48	6 53	6 58	7 03	7 10	7 17
37	R.	4 52	4 49	4 46	4 43	4 40	4 37	4 35	4 34	4 33	4 36
	S.	6 35	6 39	6 42	6 46	6 51	6 55	7 00	7 06	7 13	7 20
38	R.	4 50	4 47	4 44	4 41	4 38	4 35	4 33	4 31	4 30	4 33
	S.	6 37	6 41	6 44	6 48	6 53	6 58	7 03	7 09	7 16	7 23
39	R.	4 48	4 45	4 41	4 38	4 35	4 32	4 30	4 28	4 27	4 30
	S.	6 39	6 43	6 47	6 51	6 55	7 00	7 06	7 12	7 19	7 26
40	R.	4 47	4 43	4 39	4 36	4 33	4 30	4 27	4 25	4 24	4 27
	S.	6 41	6 45	6 49	6 53	6 58	7 03	7 09	7 15	7 22	7 29

Mean Time of Sun's Visible Rising and Setting.

South Latitude: 41° to 60°—September 23 to December 22.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	SEPTEMBER. 23	26	28	OCTOBER. 1	4	6	9	11	14	17	19	22	25	28	31	NOVEMBER. 3	6	10	14	17	22	27	DECEMBER. 3	11	22	Approx. date.	Lat. S.
	Dec. S.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	23° 27′	Dec. S.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
41	R.	5 47	5 43	5 39	5 35	5 31	5 26	5 22	5 17	5 13	5 09	5 05	5 01	4 56	4 52	4 48	4 45	4 41	4 37	4 33	4 30	4 27	4 24	4 22	4 21	4 24	R.	41
	S.	5 57	6 00	6 03	6 05	6 08	6 11	6 14	6 16	6 19	6 22	6 26	6 29	6 32	6 35	6 39	6 43	6 47	6 51	6 55	7 00	7 06	7 11	7 18	7 25	7 33	S.	
42	R.	5 47	5 43	5 39	5 34	5 30	5 25	5 21	5 17	5 12	5 08	5 04	4 59	4 55	4 50	4 46	4 43	4 39	4 35	4 31	4 28	4 24	4 21	4 19	4 18	4 20	R.	42
	S.	5 57	6 00	6 03	6 05	6 08	6 11	6 14	6 17	6 20	6 23	6 27	6 30	6 34	6 37	6 41	6 45	6 49	6 53	6 58	7 03	7 08	7 14	7 21	7 28	7 36	S.	
43	R.	5 47	5 42	5 38	5 34	5 29	5 25	5 20	5 16	5 11	5 07	5 02	4 58	4 53	4 49	4 44	4 40	4 36	4 32	4 28	4 25	4 21	4 18	4 15	4 14	4 17	R.	43
	S.	5 57	6 00	6 03	6 06	6 09	6 12	6 15	6 18	6 21	6 25	6 28	6 32	6 35	6 39	6 43	6 47	6 51	6 55	7 00	7 06	7 11	7 17	7 24	7 32	7 40	S.	
44	R.	5 47	5 42	5 38	5 33	5 29	5 24	5 19	5 15	5 10	5 06	5 01	4 56	4 52	4 47	4 42	4 38	4 34	4 29	4 25	4 22	4 18	4 15	4 12	4 10	4 13	R.	44
	S.	5 58	6 01	6 04	6 07	6 10	6 13	6 16	6 19	6 22	6 26	6 30	6 33	6 37	6 41	6 45	6 49	6 54	6 58	7 03	7 09	7 15	7 21	7 28	7 36	7 44	S.	
45	R.	5 47	5 42	5 37	5 33	5 28	5 23	5 18	5 13	5 09	5 04	4 59	4 55	4 50	4 45	4 40	4 36	4 31	4 27	4 22	4 18	4 15	4 11	4 08	4 06	4 09	R.	45
	S.	5 58	6 01	6 04	6 07	6 11	6 14	6 17	6 20	6 24	6 27	6 31	6 35	6 39	6 43	6 47	6 52	6 56	7 01	7 06	7 12	7 18	7 25	7 32	7 40	7 48	S.	
46	R.	5 47	5 42	5 37	5 32	5 27	5 22	5 17	5 12	5 08	5 03	4 58	4 53	4 48	4 43	4 38	4 34	4 29	4 24	4 19	4 15	4 11	4 07	4 04	4 02	4 05	R.	46
	S.	5 58	6 01	6 04	6 07	6 11	6 14	6 18	6 21	6 25	6 29	6 33	6 36	6 40	6 45	6 49	6 54	6 59	7 04	7 09	7 15	7 21	7 28	7 36	7 44	7 52	S.	
47	R.	5 47	5 42	5 37	5 32	5 27	5 21	5 16	5 11	5 06	5 01	4 56	4 51	4 46	4 41	4 36	4 31	4 26	4 21	4 16	4 12	4 08	4 04	4 00	3 58	4 00	R.	47
	S.	5 58	6 01	6 05	6 08	6 12	6 15	6 19	6 22	6 26	6 30	6 34	6 38	6 42	6 47	6 52	6 56	7 01	7 06	7 12	7 18	7 25	7 32	7 40	7 48	7 56	S.	
48	R.	5 47	5 41	5 36	5 31	5 26	5 21	5 15	5 10	5 05	5 00	4 54	4 49	4 44	4 39	4 33	4 28	4 23	4 18	4 13	4 09	4 04	4 00	3 56	3 54	3 56	R.	48
	S.	5 58	6 01	6 05	6 08	6 12	6 16	6 20	6 24	6 28	6 32	6 36	6 40	6 44	6 49	6 54	6 59	7 04	7 09	7 15	7 22	7 28	7 35	7 44	7 53	8 01	S.	
49	R.	5 47	5 41	5 36	5 30	5 25	5 20	5 14	5 09	5 03	4 58	4 52	4 47	4 42	4 36	4 31	4 26	4 20	4 15	4 10	4 05	4 01	3 56	3 52	3 49	3 51	R.	49
	S.	5 58	6 02	6 06	6 09	6 13	6 17	6 21	6 25	6 29	6 34	6 38	6 42	6 47	6 52	6 57	7 02	7 07	7 13	7 19	7 25	7 32	7 39	7 48	7 57	8 05	S.	
50	R.	5 46	5 41	5 36	5 30	5 25	5 19	5 13	5 07	5 02	4 56	4 51	4 45	4 40	4 34	4 28	4 23	4 17	4 12	4 07	4 02	3 57	3 52	3 47	3 44	3 46	R.	50
	S.	5 58	6 02	6 06	6 10	6 14	6 18	6 22	6 26	6 31	6 35	6 40	6 44	6 49	6 54	6 59	7 05	7 10	7 16	7 22	7 29	7 36	7 44	7 52	8 02	8 10	S.	
51	R.	5 46	5 41	5 35	5 29	5 24	5 18	5 12	5 06	5 00	4 55	4 49	4 43	4 37	4 31	4 26	4 20	4 14	4 08	4 03	3 58	3 52	3 47	3 43	3 39	3 41	R.	51
	S.	5 58	6 02	6 06	6 10	6 15	6 19	6 24	6 28	6 32	6 37	6 42	6 46	6 51	6 56	7 02	7 08	7 13	7 19	7 26	7 33	7 40	7 48	7 57	8 07	8 16	S.	
52	R.	5 46	5 40	5 35	5 29	5 23	5 17	5 11	5 04	4 59	4 53	4 47	4 41	4 35	4 29	4 23	4 17	4 11	4 05	3 59	3 53	3 48	3 42	3 37	3 34	3 35	R.	52
	S.	5 58	6 02	6 07	6 11	6 16	6 20	6 25	6 29	6 34	6 39	6 44	6 49	6 54	6 59	7 05	7 11	7 17	7 23	7 30	7 37	7 45	7 53	8 02	8 13	8 21	S.	
53	R.	5 46	5 40	5 34	5 28	5 22	5 15	5 09	5 03	4 57	4 51	4 45	4 39	4 32	4 26	4 20	4 14	4 07	4 01	3 55	3 49	3 43	3 37	3 32	3 28	3 29	R.	53
	S.	5 58	6 03	6 07	6 12	6 17	6 21	6 26	6 31	6 36	6 41	6 46	6 51	6 56	7 02	7 08	7 14	7 20	7 27	7 34	7 42	7 50	7 58	8 08	8 19	8 27	S.	
54	R.	5 46	5 40	5 34	5 27	5 21	5 14	5 08	5 01	4 55	4 49	4 43	4 36	4 30	4 23	4 17	4 10	4 04	3 57	3 50	3 44	3 38	3 32	3 26	3 22	3 23	R.	54
	S.	5 59	6 03	6 08	6 12	6 18	6 22	6 27	6 32	6 37	6 43	6 48	6 53	6 59	7 05	7 11	7 17	7 24	7 31	7 38	7 46	7 55	8 04	8 14	8 25	8 34	S.	
55	R.	5 46	5 39	5 33	5 26	5 20	5 13	5 07	5 00	4 53	4 47	4 40	4 34	4 27	4 20	4 13	4 07	4 00	3 53	3 46	3 39	3 33	3 26	3 20	3 15	3 16	R.	55
	S.	5 59	6 03	6 08	6 13	6 18	6 23	6 29	6 34	6 39	6 45	6 50	6 56	7 02	7 08	7 14	7 21	7 28	7 35	7 43	7 51	8 00	8 09	8 20	8 32	8 41	S.	
56	R.	5 45	5 39	5 33	5 26	5 19	5 12	5 05	4 58	4 51	4 45	4 38	4 31	4 24	4 17	4 10	4 03	3 55	3 48	3 41	3 34	3 27	3 20	3 13	3 08	3 08	R.	56
	S.	5 59	6 04	6 09	6 14	6 20	6 25	6 30	6 35	6 41	6 47	6 53	6 59	7 05	7 11	7 18	7 25	7 32	7 40	7 48	7 56	8 05	8 15	8 26	8 39	8 48	S.	
57	R.	5 45	5 38	5 32	5 25	5 18	5 11	5 04	4 56	4 49	4 42	4 35	4 28	4 20	4 13	4 06	3 58	3 51	3 43	3 36	3 28	3 21	3 13	3 06	3 00	3 00	R.	57
	S.	5 59	6 04	6 10	6 15	6 21	6 26	6 32	6 37	6 43	6 49	6 56	7 02	7 08	7 15	7 22	7 29	7 37	7 45	7 53	8 02	8 12	8 22	8 33	8 46	8 56	S.	
58	R.	5 45	5 38	5 31	5 24	5 17	5 09	5 02	4 54	4 47	4 40	4 32	4 25	4 17	4 09	4 02	3 54	3 46	3 38	3 30	3 22	3 14	3 06	2 58	2 51	2 51	R.	58
	S.	5 59	6 05	6 10	6 16	6 22	6 27	6 33	6 39	6 45	6 52	6 58	7 05	7 12	7 19	7 26	7 34	7 42	7 50	7 59	8 08	8 18	8 29	8 41	8 55	9 05	S.	
59	R.	5 45	5 37	5 30	5 23	5 15	5 08	5 00	4 52	4 45	4 37	4 29	4 21	4 13	4 05	3 57	3 49	3 41	3 32	3 24	3 16	3 07	2 58	2 50	2 42	2 42	R.	59
	S.	6 00	6 05	6 11	6 17	6 23	6 29	6 35	6 41	6 48	6 54	7 01	7 08	7 15	7 23	7 31	7 39	7 47	7 55	8 04	8 14	8 25	8 37	8 50	9 04	9 15	S.	
60	R.	5 45	5 37	5 30	5 22	5 14	5 06	4 58	4 50	4 43	4 35	4 27	4 18	4 10	4 01	3 53	3 44	3 35	3 27	3 18	3 09	3 00	2 51	2 41	2 31	2 31	R.	60
	S.	6 00	6 06	6 12	6 18	6 24	6 30	6 37	6 43	6 50	6 57	7 04	7 11	7 19	7 27	7 35	7 43	7 52	8 01	8 11	8 22	8 33	8 45	8 59	9 15	9 26	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

South Latitude: 0° to 20°—December 22 to March 21.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	DECEMBER.	JANUARY.						FEBRUARY.									MARCH.									Approx. date.	Lat. S.
		22	2	10	16	21	25	29	2	5	9	12	15	18	20	23	26	1	3	6	8	11	13	16	18	21		
	Dec. S.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. S.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
0	R.	5 54	6 00	6 04	6 06	6 07	6 08	6 09	6 10	6 10	6 10	6 10	6 10	6 10	6 10	6 10	6 09	6 09	6 08	6 08	6 07	6 06	6 06	6 05	6 04	6 04	R.	0
	S.	6 02	6 08	6 12	6 14	6 15	6 16	6 17	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 17	6 17	6 16	6 16	6 15	6 14	6 14	6 13	6 12	6 11	S.	
1	R.	5 53	5 58	6 02	6 04	6 06	6 07	6 08	6 09	6 09	6 09	6 09	6 10	6 10	6 09	6 09	6 09	6 08	6 08	6 08	6 07	6 06	6 06	6 05	6 04	6 04	R.	1
	S.	6 04	6 09	6 13	6 15	6 17	6 17	6 18	6 19	6 19	6 19	6 19	6 19	6 19	6 18	6 18	6 18	6 17	6 16	6 16	6 15	6 14	6 14	6 13	6 12	6 11	S.	
2	R.	5 51	5 57	6 01	6 03	6 04	6 06	6 07	6 08	6 08	6 08	6 08	6 09	6 09	6 09	6 09	6 08	6 08	6 08	6 08	6 07	6 06	6 06	6 05	6 04	6 04	R.	2
	S.	6 05	6 11	6 15	6 17	6 18	6 19	6 19	6 20	6 20	6 20	6 20	6 20	6 19	6 19	6 19	6 18	6 17	6 17	6 16	6 15	6 14	6 14	6 13	6 12	6 11	S.	
3	R.	5 49	5 55	5 59	6 01	6 03	6 04	6 06	6 07	6 07	6 07	6 07	6 08	6 08	6 08	6 08	6 08	6 08	6 07	6 07	6 07	6 06	6 06	6 05	6 04	6 04	R.	3
	S.	6 07	6 13	6 16	6 18	6 20	6 20	6 21	6 21	6 21	6 21	6 21	6 21	6 20	6 20	6 20	6 19	6 18	6 17	6 16	6 16	6 15	6 14	6 13	6 12	6 11	S.	
4	R.	5 48	5 53	5 57	6 00	6 01	6 03	6 04	6 05	6 06	6 06	6 06	6 07	6 07	6 07	6 07	6 07	6 07	6 07	6 07	6 07	6 06	6 06	6 05	6 04	6 04	R.	4
	S.	6 09	6 14	6 18	6 20	6 21	6 22	6 22	6 22	6 22	6 22	6 22	6 22	6 21	6 20	6 20	6 19	6 18	6 18	6 17	6 16	6 15	6 14	6 13	6 12	6 11	S.	
5	R.	5 46	5 52	5 56	5 58	6 00	6 01	6 03	6 04	6 05	6 05	6 05	6 06	6 06	6 06	6 06	6 06	6 06	6 06	6 06	6 06	6 05	6 05	6 04	6 04	6 04	R.	5
	S.	6 11	6 16	6 20	6 21	6 23	6 23	6 24	6 24	6 24	6 23	6 23	6 23	6 22	6 21	6 21	6 20	6 19	6 18	6 17	6 16	6 15	6 14	6 13	6 12	6 11	S.	
6	R.	5 44	5 50	5 54	5 57	5 58	6 00	6 02	6 03	6 04	6 04	6 04	6 05	6 06	6 06	6 06	6 06	6 06	6 06	6 06	6 06	6 05	6 05	6 04	6 04	6 03	R.	6
	S.	6 12	6 17	6 21	6 23	6 24	6 24	6 25	6 25	6 25	6 24	6 24	6 23	6 23	6 22	6 22	6 21	6 20	6 19	6 18	6 17	6 15	6 14	6 13	6 12	6 11	S.	
7	R.	5 42	5 48	5 52	5 55	5 57	5 59	6 00	6 01	6 02	6 03	6 03	6 04	6 05	6 05	6 05	6 05	6 05	6 05	6 05	6 05	6 05	6 05	6 04	6 04	6 03	R.	7
	S.	6 14	6 19	6 23	6 25	6 26	6 26	6 26	6 26	6 26	6 26	6 25	6 24	6 24	6 23	6 22	6 21	6 20	6 19	6 18	6 17	6 16	6 15	6 13	6 12	6 11	S.	
8	R.	5 41	5 46	5 50	5 53	5 55	5 57	5 59	6 00	6 01	6 02	6 02	6 03	6 04	6 04	6 04	6 04	6 05	6 05	6 05	6 05	6 04	6 05	6 04	6 04	6 03	R.	8
	S.	6 16	6 21	6 25	6 26	6 27	6 27	6 28	6 27	6 27	6 27	6 26	6 25	6 25	6 24	6 23	6 22	6 21	6 20	6 19	6 18	6 16	6 15	6 13	6 12	6 11	S.	
9	R.	5 39	5 45	5 49	5 52	5 54	5 56	5 57	5 59	6 00	6 01	6 01	6 02	6 03	6 03	6 03	6 04	6 04	6 04	6 04	6 04	6 04	6 04	6 04	6 04	6 03	R.	9
	S.	6 18	6 23	6 27	6 28	6 29	6 29	6 29	6 29	6 29	6 28	6 27	6 26	6 26	6 25	6 24	6 23	6 22	6 20	6 19	6 18	6 17	6 15	6 14	6 13	6 11	S.	
10	R.	5 37	5 43	5 47	5 50	5 52	5 54	5 56	5 58	5 59	6 00	6 00	6 01	6 02	6 02	6 02	6 03	6 03	6 04	6 04	6 04	6 04	6 04	6 04	6 04	6 03	R.	10
	S.	6 19	6 25	6 28	6 29	6 30	6 30	6 30	6 30	6 30	6 29	6 28	6 27	6 26	6 25	6 24	6 23	6 22	6 21	6 20	6 18	6 17	6 15	6 14	6 13	6 11	S.	
11	R.	5 35	5 41	5 46	5 49	5 51	5 53	5 55	5 56	5 58	5 59	5 59	6 00	6 01	6 01	6 02	6 02	6 03	6 03	6 03	6 04	6 04	6 04	6 04	6 04	6 03	R.	11
	S.	6 21	6 27	6 30	6 31	6 32	6 32	6 32	6 31	6 31	6 30	6 29	6 28	6 27	6 26	6 25	6 24	6 23	6 21	6 20	6 19	6 17	6 16	6 14	6 13	6 11	S.	
12	R.	5 33	5 39	5 44	5 47	5 49	5 52	5 54	5 55	5 57	5 58	5 58	5 59	6 00	6 01	6 01	6 02	6 02	6 03	6 03	6 03	6 03	6 04	6 04	6 04	6 03	R.	12
	S.	6 23	6 28	6 31	6 32	6 33	6 33	6 33	6 32	6 32	6 31	6 30	6 29	6 28	6 27	6 26	6 25	6 23	6 22	6 21	6 19	6 17	6 16	6 14	6 13	6 11	S.	
13	R.	5 31	5 37	5 42	5 46	5 48	5 50	5 52	5 54	5 55	5 56	5 57	5 58	5 59	6 00	6 00	6 01	6 01	6 02	6 02	6 03	6 03	6 03	6 03	6 03	6 03	R.	13
	S.	6 25	6 30	6 33	6 34	6 35	6 34	6 34	6 34	6 33	6 32	6 31	6 30	6 29	6 28	6 27	6 26	6 24	6 23	6 21	6 20	6 18	6 16	6 14	6 13	6 11	S.	
14	R.	5 29	5 35	5 41	5 44	5 46	5 49	5 51	5 53	5 54	5 55	5 56	5 57	5 58	5 59	6 00	6 00	6 01	6 01	6 02	6 03	6 03	6 03	6 03	6 03	6 03	R.	14
	S.	6 27	6 32	6 35	6 36	6 36	6 36	6 36	6 35	6 34	6 33	6 32	6 31	6 30	6 29	6 28	6 26	6 25	6 23	6 22	6 20	6 18	6 16	6 14	6 13	6 11	S.	
15	R.	5 27	5 33	5 39	5 42	5 45	5 47	5 49	5 51	5 53	5 54	5 55	5 56	5 57	5 58	5 59	6 00	6 00	6 01	6 01	6 02	6 02	6 03	6 03	6 03	6 03	R.	15
	S.	6 29	6 34	6 37	6 37	6 38	6 37	6 37	6 36	6 35	6 34	6 33	6 32	6 31	6 30	6 28	6 27	6 25	6 24	6 22	6 20	6 18	6 17	6 15	6 13	6 11	S.	
16	R.	5 25	5 32	5 37	5 41	5 43	5 46	5 48	5 50	5 52	5 53	5 54	5 55	5 56	5 57	5 58	5 59	6 00	6 00	6 01	6 02	6 02	6 03	6 03	6 03	6 03	R.	16
	S.	6 31	6 36	6 38	6 39	6 39	6 39	6 39	6 38	6 37	6 35	6 34	6 33	6 32	6 30	6 29	6 27	6 26	6 24	6 23	6 21	6 19	6 17	6 15	6 13	6 11	S.	
17	R.	5 23	5 30	5 35	5 39	5 41	5 44	5 46	5 48	5 50	5 52	5 53	5 54	5 55	5 56	5 57	5 58	5 59	6 00	6 00	6 01	6 01	6 02	6 03	6 03	6 03	R.	17
	S.	6 33	6 38	6 40	6 41	6 41	6 41	6 40	6 39	6 38	6 37	6 36	6 34	6 33	6 31	6 30	6 28	6 27	6 25	6 23	6 21	6 19	6 17	6 15	6 13	6 11	S.	
18	R.	5 21	5 28	5 34	5 37	5 40	5 42	5 45	5 47	5 49	5 51	5 52	5 53	5 54	5 55	5 56	5 57	5 58	5 59	6 00	6 01	6 01	6 02	6 03	6 03	6 03	R.	18
	S.	6 35	6 39	6 42	6 42	6 43	6 42	6 41	6 40	6 39	6 38	6 37	6 35	6 34	6 32	6 31	6 29	6 27	6 25	6 23	6 21	6 19	6 17	6 15	6 13	6 11	S.	
19	R.	5 19	5 26	5 32	5 35	5 38	5 41	5 44	5 46	5 48	5 49	5 51	5 52	5 53	5 54	5 55	5 57	5 58	5 59	6 00	6 01	6 01	6 02	6 02	6 03	6 03	R.	19
	S.	6 37	6 41	6 44	6 44	6 44	6 44	6 43	6 42	6 41	6 39	6 38	6 36	6 35	6 33	6 31	6 30	6 28	6 26	6 24	6 22	6 20	6 18	6 15	6 13	6 11	S.	
20	R.	5 17	5 24	5 30	5 34	5 37	5 39	5 42	5 44	5 46	5 48	5 50	5 51	5 52	5 54	5 55	5 56	5 57	5 58	5 59	6 00	6 01	6 02	6 02	6 03	6 03	R.	20
	S.	6 39	6 43	6 46	6 46	6 46	6 45	6 44	6 43	6 42	6 40	6 39	6 37	6 36	6 34	6 32	6 30	6 28	6 26	6 24	6 22	6 20	6 18	6 15	6 13	6 11	S.	

Mean Time of Sun's Visible Rising and Setting.

South Latitude: 21° to 40°—December 22 to March 21.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	DECEMBER. 22	JANUARY. 2	10	16	21	25	29	FEBRUARY. 2	5	9	12	15
°	Dec. S.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°
		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
21	R.	5 15	5 22	5 28	5 32	5 35	5 38	5 41	5 43	5 45	5 47	5 48	5 50
	S.	6 41	6 46	6 48	6 48	6 48	6 47	6 46	6 45	6 44	6 42	6 40	6 39
22	R.	5 13	5 20	5 26	5 30	5 33	5 36	5 39	5 41	5 44	5 46	5 47	5 49
	S.	6 43	6 48	6 50	6 50	6 49	6 48	6 47	6 46	6 45	6 43	6 41	6 40
23	R.	5 11	5 18	5 24	5 28	5 31	5 34	5 37	5 40	5 42	5 44	5 46	5 48
	S.	6 45	6 50	6 52	6 52	6 51	6 50	6 49	6 48	6 46	6 44	6 43	6 41
24	R.	5 09	5 16	5 22	5 26	5 30	5 33	5 36	5 38	5 41	5 43	5 45	5 47
	S.	6 47	6 52	6 54	6 53	6 53	6 52	6 51	6 49	6 48	6 46	6 44	6 42
25	R.	5 07	5 14	5 20	5 24	5 28	5 31	5 34	5 37	5 39	5 41	5 43	5 45
	S.	6 50	6 54	6 56	6 55	6 55	6 54	6 53	6 51	6 49	6 47	6 45	6 43
26	R.	5 05	5 12	5 18	5 22	5 26	5 29	5 32	5 35	5 38	5 40	5 42	5 44
	S.	6 52	6 56	6 58	6 57	6 56	6 55	6 54	6 52	6 51	6 48	6 46	6 44
27	R.	5 02	5 09	5 16	5 20	5 24	5 28	5 31	5 34	5 36	5 39	5 41	5 43
	S.	6 54	6 58	7 00	6 59	6 58	6 57	6 56	6 54	6 52	6 50	6 48	6 45
28	R.	5 00	5 07	5 14	5 18	5 22	5 26	5 29	5 32	5 35	5 37	5 39	5 42
	S.	6 56	7 00	7 02	7 01	7 00	6 59	6 57	6 55	6 53	6 51	6 49	6 47
29	R.	4 58	5 05	5 11	5 16	5 20	5 24	5 27	5 30	5 33	5 36	5 38	5 40
	S.	6 59	7 03	7 04	7 03	7 02	7 01	6 59	6 57	6 55	6 53	6 51	6 48
30	R.	4 55	5 02	5 09	5 14	5 18	5 22	5 26	5 29	5 32	5 34	5 37	5 39
	S.	7 01	7 05	7 06	7 05	7 04	7 02	7 01	6 59	6 57	6 54	6 52	6 49
31	R.	4 53	5 00	5 07	5 12	5 16	5 20	5 24	5 27	5 30	5 33	5 35	5 38
	S.	7 04	7 08	7 09	7 08	7 06	7 04	7 03	7 01	6 58	6 56	6 53	6 51
32	R.	4 50	4 57	5 04	5 10	5 14	5 18	5 22	5 25	5 28	5 31	5 34	5 37
	S.	7 06	7 10	7 11	7 10	7 08	7 06	7 05	7 03	7 00	6 57	6 55	6 52
33	R.	4 48	4 55	5 02	5 07	5 12	5 16	5 20	5 23	5 27	5 30	5 32	5 35
	S.	7 09	7 13	7 14	7 12	7 11	7 09	7 07	7 04	7 02	6 59	6 56	6 53
34	R.	4 45	4 52	4 59	5 05	5 10	5 14	5 18	5 21	5 25	5 28	5 31	5 34
	S.	7 11	7 15	7 16	7 15	7 13	7 11	7 09	7 06	7 03	7 00	6 58	6 55
35	R.	4 42	4 50	4 57	5 02	5 07	5 12	5 16	5 19	5 23	5 26	5 29	5 32
	S.	7 14	7 18	7 19	7 17	7 15	7 13	7 11	7 08	7 05	7 02	6 59	6 56
36	R.	4 39	4 47	4 54	5 00	5 05	5 09	5 14	5 17	5 21	5 25	5 28	5 31
	S.	7 17	7 21	7 21	7 20	7 18	7 15	7 13	7 10	7 07	7 04	7 01	6 58
37	R.	4 36	4 44	4 52	4 57	5 02	5 07	5 11	5 15	5 19	5 23	5 26	5 29
	S.	7 20	7 24	7 24	7 22	7 20	7 18	7 15	7 12	7 09	7 06	7 03	6 59
38	R.	4 33	4 41	4 49	4 55	5 00	5 05	5 09	5 13	5 17	5 21	5 24	5 28
	S.	7 23	7 27	7 27	7 25	7 23	7 20	7 17	7 14	7 11	7 08	7 04	7 01
39	R.	4 30	4 38	4 46	4 52	4 57	5 02	5 07	5 11	5 15	5 19	5 22	5 26
	S.	7 26	7 30	7 30	7 28	7 25	7 22	7 19	7 16	7 13	7 10	7 06	7 03
40	R.	4 27	4 35	4 43	4 49	4 55	5 00	5 05	5 09	5 13	5 17	5 21	5 24
	S.	7 29	7 33	7 33	7 30	7 28	7 25	7 22	7 18	7 15	7 11	7 08	7 04

Lat. S.	Approx. date.	FEBRUARY. 18	20	23	26	MARCH. 1	3	6	8	11	13	16	18	21	Approx. date.	Lat. S.
°	Dec. S.	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. S.	°
		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		
21	R.	5 51	5 53	5 54	5 55	5 56	5 58	5 59	6 00	6 00	6 01	6 02	6 03	6 03	R.	21
	S.	6 37	6 35	6 33	6 31	6 29	6 27	6 25	6 23	6 20	6 18	6 16	6 14	6 11	S.	
22	R.	5 50	5 52	5 53	5 54	5 56	5 57	5 58	6 00	6 00	6 01	6 02	6 03	6 03	R.	22
	S.	6 38	6 36	6 34	6 32	6 30	6 27	6 25	6 23	6 20	6 18	6 16	6 14	6 11	S.	
23	R.	5 49	5 51	5 53	5 54	5 55	5 57	5 58	5 59	6 00	6 01	6 02	6 03	6 03	R.	23
	S.	6 39	6 37	6 35	6 33	6 30	6 28	6 26	6 23	6 21	6 19	6 16	6 14	6 11	S.	
24	R.	5 48	5 50	5 52	5 53	5 55	5 56	5 57	5 59	6 00	6 01	6 02	6 03	6 03	R.	24
	S.	6 40	6 38	6 36	6 33	6 31	6 28	6 26	6 24	6 21	6 19	6 16	6 14	6 11	S.	
25	R.	5 47	5 49	5 51	5 52	5 54	5 55	5 57	5 58	5 59	6 00	6 01	6 02	6 03	R.	25
	S.	6 41	6 39	6 37	6 34	6 32	6 29	6 27	6 24	6 21	6 19	6 16	6 14	6 11	S.	
26	R.	5 46	5 48	5 50	5 51	5 53	5 55	5 56	5 58	5 59	6 00	6 01	6 02	6 03	R.	26
	S.	6 42	6 40	6 38	6 35	6 32	6 30	6 27	6 25	6 22	6 19	6 16	6 14	6 11	S.	
27	R.	5 45	5 47	5 49	5 50	5 52	5 54	5 56	5 57	5 58	6 00	6 01	6 02	6 03	R.	27
	S.	6 43	6 41	6 39	6 36	6 33	6 30	6 28	6 25	6 22	6 20	6 17	6 14	6 11	S.	
28	R.	5 44	5 46	5 48	5 49	5 51	5 53	5 55	5 57	5 58	5 59	6 00	6 02	6 03	R.	28
	S.	6 44	6 42	6 40	6 37	6 34	6 31	6 28	6 26	6 23	6 20	6 17	6 14	6 11	S.	
29	R.	5 43	5 45	5 47	5 48	5 50	5 52	5 54	5 56	5 58	5 59	6 00	6 02	6 03	R.	29
	S.	6 46	6 43	6 41	6 38	6 35	6 32	6 29	6 26	6 23	6 20	6 17	6 14	6 11	S.	
30	R.	5 42	5 44	5 46	5 48	5 50	5 52	5 54	5 56	5 57	5 59	6 00	6 02	6 03	R.	30
	S.	6 47	6 44	6 42	6 39	6 36	6 33	6 30	6 27	6 23	6 21	6 18	6 15	6 12	S.	
31	R.	5 40	5 42	5 45	5 47	5 49	5 51	5 53	5 55	5 57	5 58	6 00	6 02	6 03	R.	31
	S.	6 48	6 45	6 43	6 40	6 37	6 33	6 30	6 27	6 24	6 21	6 18	6 15	6 12	S.	
32	R.	5 39	5 41	5 44	5 46	5 48	5 51	5 53	5 55	5 56	5 58	5 59	6 01	6 03	R.	32
	S.	6 49	6 46	6 44	6 41	6 37	6 34	6 31	6 28	6 24	6 21	6 18	6 15	6 12	S.	
33	R.	5 38	5 40	5 54	5 45	5 47	5 50	5 52	5 54	5 56	5 58	5 59	6 01	6 03	R.	33
	S.	6 50	6 47	6 45	6 42	6 38	6 35	6 32	6 29	6 25	6 22	6 18	6 15	6 12	S.	
34	R.	5 37	5 39	5 42	5 44	5 47	5 49	5 51	5 53	5 55	5 57	5 59	6 01	6 03	R.	34
	S.	6 52	6 49	6 46	6 43	6 39	6 35	6 32	6 29	6 25	6 22	6 18	6 15	6 12	S.	
35	R.	5 35	5 38	5 41	5 43	5 46	5 48	5 50	5 53	5 55	5 57	5 59	6 01	6 03	R.	35
	S.	6 53	6 50	6 47	6 44	6 40	6 36	6 33	6 30	6 26	6 23	6 19	6 15	6 12	S.	
36	R.	5 34	5 37	5 40	5 42	5 45	5 47	5 50	5 52	5 54	5 57	5 59	6 01	6 03	R.	36
	S.	6 55	6 51	6 48	6 45	6 41	6 37	6 34	6 30	6 26	6 23	6 19	6 15	6 12	S.	
37	R.	5 32	5 35	5 38	5 41	5 44	5 46	5 49	5 51	5 54	5 56	5 58	6 01	6 03	R.	37
	S.	6 56	6 52	6 49	6 46	6 42	6 38	6 35	6 31	6 27	6 23	6 19	6 16	6 12	S.	
38	R.	5 31	5 34	5 37	5 40	5 43	5 46	5 48	5 51	5 53	5 56	5 58	6 00	6 02	R.	38
	S.	6 58	6 54	6 50	6 47	6 43	6 39	6 35	6 32	6 28	6 24	6 20	6 16	6 12	S.	
39	R.	5 29	5 32	5 36	5 39	5 42	5 45	5 47	5 50	5 52	5 55	5 58	6 00	6 02	R.	39
	S.	6 59	6 55	6 52	6 48	6 44	6 40	6 36	6 32	6 28	6 24	6 20	6 16	6 12	S.	
40	R.	5 28	5 31	5 35	5 38	5 41	5 44	5 47	5 50	5 52	5 55	5 57	6 00	6 02	R.	40
	S.	7 01	6 57	6 53	6 49	6 45	6 41	6 37	6 33	6 28	6 25	6 20	6 16	6 12	S.	

TABLE 10.

Mean Time of Sun's Visible Rising and Setting.

South Latitude: 41° to 60°—December 22 to March 21.

[R=Local mean time of sun's visible rising. S=Local mean time of sun's visible setting.]

Lat. S.	Approx. date.	DECEMBER.	JANUARY.						FEBRUARY.									MARCH.									Approx. date.	Lat. S.
		22	2	10	16	21	25	29	2	5	9	12	15	18	20	23	26	1	3	6	8	11	13	16	18	21		
	Dec. S.	23° 27′	23°	22°	21°	20°	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	9°	8°	7°	6°	5°	4°	3°	2°	1°	0°	Dec. S.	
°		h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.		°
41	R.	4 24	4 32	4 40	4 46	4 52	4 57	5 02	5 07	5 11	5 15	5 19	5 23	5 26	5 30	5 33	5 37	5 40	5 43	5 46	5 49	5 52	5 55	5 57	6 00	6 02	R.	41
	S.	7 33	7 36	7 36	7 33	7 31	7 27	7 24	7 21	7 17	7 13	7 10	7 06	7 02	6 58	6 54	6 50	6 46	6 42	6 38	6 34	6 29	6 25	6 21	6 17	6 12	S.	
42	R.	4 20	4 29	4 37	4 43	4 49	4 55	5 00	5 05	5 09	5 13	5 17	5 21	5 25	5 28	5 32	5 36	5 39	5 42	5 45	5 48	5 51	5 54	5 57	6 00	6 02	R.	42
	S.	7 36	7 39	7 39	7 36	7 33	7 30	7 27	7 23	7 19	7 15	7 12	7 08	7 04	6 59	6 55	6 51	6 47	6 42	6 38	6 34	6 29	6 25	6 21	6 17	6 12	S.	
43	R.	4 17	4 25	4 33	4 40	4 46	4 52	4 57	5 02	5 07	5 11	5 15	5 19	5 23	5 27	5 31	5 34	5 38	5 41	5 44	5 48	5 51	5 54	5 56	5 59	6 02	R.	43
	S.	7 40	7 43	7 42	7 39	7 36	7 33	7 29	7 25	7 22	7 18	7 14	7 09	7 05	7 01	6 57	6 52	6 48	6 43	6 39	6 35	6 30	6 26	6 21	6 17	6 12	S.	
44	R.	4 13	4 21	4 29	4 37	4 43	4 49	4 54	4 59	5 04	5 09	5 13	5 17	5 21	5 25	5 29	5 33	5 37	5 40	5 43	5 47	5 50	5 53	5 56	5 59	6 02	R.	44
	S.	7 44	7 47	7 46	7 43	7 39	7 36	7 32	7 28	7 24	7 20	7 16	7 11	7 07	7 02	6 58	6 53	6 49	6 44	6 40	6 36	6 31	6 26	6 22	6 17	6 13	S.	
45	R.	4 09	4 17	4 26	4 33	4 40	4 46	4 51	4 57	5 02	5 06	5 11	5 15	5 20	5 24	5 28	5 32	5 35	5 39	5 42	5 46	5 49	5 53	5 56	5 59	6 02	R.	45
	S.	7 48	7 51	7 50	7 46	7 43	7 39	7 35	7 31	7 27	7 22	7 18	7 13	7 09	7 04	7 00	6 55	6 50	6 46	6 41	6 37	6 32	6 27	6 22	6 18	6 13	S.	
46	R.	4 05	4 13	4 22	4 29	4 36	4 42	4 48	4 54	4 59	5 04	5 09	5 13	5 18	5 22	5 26	5 30	5 34	5 38	5 41	5 45	5 48	5 52	5 55	5 59	6 02	R.	46
	S.	7 52	7 55	7 54	7 50	7 46	7 42	7 38	7 34	7 29	7 24	7 20	7 15	7 10	7 05	7 01	6 56	6 51	6 47	6 42	6 37	6 32	6 27	6 22	6 18	6 13	S.	
47	R.	4 00	4 09	4 18	4 26	4 33	4 39	4 45	4 51	4 57	5 02	5 06	5 11	5 16	5 20	5 24	5 29	5 33	5 37	5 40	5 44	5 48	5 52	5 55	5 59	6 02	R.	47
	S.	7 56	7 59	7 57	7 54	7 50	7 45	7 41	7 36	7 32	7 27	7 22	7 17	7 12	7 07	7 03	6 58	6 53	6 48	6 43	6 38	6 33	6 28	6 23	6 18	6 13	S.	
48	R.	3 56	4 04	4 14	4 22	4 29	4 36	4 42	4 48	4 54	4 59	5 04	5 09	5 14	5 18	5 23	5 27	5 31	5 35	5 39	5 43	5 47	5 51	5 54	5 58	6 02	R.	48
	S.	8 01	8 03	8 01	7 57	7 53	7 49	7 44	7 39	7 35	7 30	7 25	7 19	7 14	7 09	7 05	6 59	6 54	6 49	6 44	6 39	6 33	6 28	6 23	6 18	6 13	S.	
49	R.	3 51	4 00	4 10	4 18	4 26	4 32	4 39	4 45	4 51	4 56	5 01	5 07	5 12	5 16	5 21	5 25	5 30	5 34	5 38	5 42	5 46	5 50	5 54	5 58	6 01	R.	49
	S.	8 05	8 08	8 06	8 01	7 57	7 52	7 48	7 43	7 38	7 32	7 27	7 22	7 17	7 11	7 06	7 01	6 56	6 50	6 45	6 40	6 34	6 29	6 24	6 19	6 13	S.	
50	R.	3 46	3 55	4 05	4 14	4 22	4 29	4 35	4 42	4 48	4 53	4 59	5 04	5 09	5 14	5 19	5 24	5 28	5 33	5 37	5 42	5 46	5 50	5 54	5 58	6 01	R.	50
	S	8 10	8 13	8 10	8 06	8 01	7 56	7 51	7 46	7 41	7 35	7 30	7 24	7 19	7 13	7 08	7 03	6 57	6 52	6 46	6 41	6 35	6 30	6 24	6 19	6 13	S.	
51	R.	3 41	3 50	4 01	4 09	4 17	4 25	4 32	4 38	4 44	4 50	4 56	5 02	5 07	5 12	5 17	5 22	5 27	5 31	5 36	5 41	5 45	5 49	5 53	5 57	6 01	R.	51
	S.	8 16	8 18	8 15	8 10	8 05	8 00	7 55	7 49	7 44	7 38	7 32	7 27	7 21	7 15	7 10	7 04	6 59	6 53	6 48	6 42	6 36	6 30	6 24	6 19	6 13	S.	
52	R.	3 35	3 44	3 55	4 04	4 13	4 21	4 28	4 35	4 41	4 47	4 53	4 59	5 05	5 10	5 15	5 20	5 25	5 30	5 35	5 40	5 44	5 49	5 53	5 57	6 01	R.	52
	S.	8 21	8 23	8 20	8 15	8 10	8 04	7 59	7 53	7 47	7 41	7 35	7 29	7 24	7 18	7 12	7 06	7 00	6 55	6 49	6 43	6 37	6 31	6 25	6 19	6 13	S.	
53	R.	3 29	3 38	3 50	3 59	4 08	4 16	4 24	4 31	4 38	4 44	4 50	4 56	5 02	5 08	5 13	5 18	5 23	5 28	5 33	5 38	5 43	5 48	5 52	5 57	6 01	R.	53
	S.	8 27	8 29	8 26	8 20	8 15	8 09	8 03	7 57	7 51	7 44	7 38	7 32	7 26	7 20	7 14	7 08	7 02	6 56	6 50	6 44	6 38	6 32	6 25	6 19	6 13	S.	
54	R.	3 23	3 32	3 44	3 54	4 03	4 11	4 19	4 27	4 34	4 41	4 47	4 53	4 59	5 05	5 11	5 16	5 22	5 27	5 32	5 37	5 42	5 47	5 52	5 57	6 01	R.	54
	S.	8 34	8 35	8 32	8 26	8 20	8 13	8 07	8 01	7 54	7 48	7 41	7 35	7 29	7 22	7 16	7 10	7 04	6 58	6 51	6 45	6 39	6 32	6 26	6 20	6 14	S.	
55	R.	3 16	3 25	3 38	3 48	3 57	4 06	4 15	4 23	4 30	4 37	4 44	4 50	4 57	5 03	5 09	5 14	5 20	5 25	5 31	5 36	5 41	5 46	5 51	5 56	6 01	R.	55
	S.	8 41	8 42	8 38	8 31	8 25	8 18	8 12	8 05	7 58	7 51	7 45	7 38	7 32	7 25	7 19	7 12	7 06	6 59	6 53	6 46	6 40	6 33	6 26	6 20	6 14	S.	
56	R.	3 08	3 18	3 31	3 42	3 52	4 01	4 10	4 18	4 26	4 33	4 40	4 47	4 54	5 00	5 06	5 12	5 18	5 24	5 29	5 35	5 40	5 46	5 51	5 56	6 01	R.	56
	S.	8 48	8 49	8 44	8 37	8 30	8 23	8 17	8 10	8 03	7 56	7 49	7 42	7 35	7 28	7 21	7 14	7 08	7 01	6 54	6 48	6 41	6 34	6 27	6 21	6 14	S.	
57	R.	3 00	3 11	3 24	3 35	3 45	3 55	4 04	4 13	4 21	4 29	4 36	4 43	4 50	4 57	5 03	5 10	5 16	5 22	5 28	5 34	5 39	5 45	5 50	5 55	6 00	R.	57
	S.	8 56	8 57	8 51	8 44	8 37	8 29	8 22	8 15	8 07	8 00	7 52	7 45	7 38	7 31	7 24	7 17	7 10	7 03	6 56	6 49	6 42	6 35	6 28	6 21	6 14	S.	
58	R.	2 51	3 02	3 16	3 28	3 39	3 49	3 59	4 08	4 16	4 24	4 32	4 40	4 47	4 54	5 01	5 07	5 14	5 20	5 26	5 32	5 38	5 44	5 49	5 55	6 00	R.	58
	S.	9 05	9 06	8 59	8 51	8 43	8 35	8 27	8 20	8 12	8 04	7 56	7 49	7 42	7 34	7 27	7 19	7 12	7 05	6 57	6 50	6 43	6 36	6 29	6 22	6 14	S.	
59	R.	2 42	2 53	3 08	3 20	3 32	3 43	3 53	4 02	4 11	4 19	4 28	4 36	4 43	4 50	4 58	5 05	5 11	5 18	5 24	5 31	5 37	5 43	5 48	5 54	6 00	R.	59
	S.	9 15	9 15	9 08	8 59	8 50	8 42	8 33	8 25	8 17	8 09	8 01	7 53	7 45	7 37	7 30	7 22	7 14	7 07	6 59	6 52	6 44	6 37	6 29	6 22	6 15	S.	
60	R.	2 31	2 42	2 59	3 13	3 25	3 36	3 47	3 57	4 06	4 15	4 23	4 32	4 40	4 47	4 55	5 02	5 09	5 16	5 22	5 29	5 35	5 42	5 48	5 54	6 00	R.	60
	S.	9 26	9 26	9 17	9 07	8 58	8 49	8 40	8 31	8 23	8 14	8 05	7 57	7 49	7 40	7 32	7 24	7 16	7 09	7 01	6 53	6 45	6 38	6 30	6 23	6 15	S.	

TABLE 11.

For reducing the Time of the Moon's passage over the Meridian of Greenwich to the Time of its passage over any other Meridian. The numbers taken from this Table are to be added to the Time at Greenwich in West Longitude, subtracted in East Longitude.

Longitude.	Daily variation of the moon's passing the meridian.														Longitude.
	40m	42m	44m	46m	48m	50m	52m	54m	56m	58m	60m	62m	64m	66m	
°	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	°
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	1	1	1	1	1	1	1	1	1	1	1	1	1	1	5
10	1	1	1	1	1	1	1	1	2	2	2	2	2	2	10
15	2	2	2	3	2	2	2	2	2	2	2	3	3	3	15
20	2	2	2	2	3	3	3	3	3	3	3	3	4	4	20
25	3	3	3	3	3	3	4	4	4	4	4	4	4	5	25
30	3	3	4	4	4	4	4	4	5	5	5	5	5	5	30
35	4	4	4	4	5	5	5	5	5	6	6	6	6	6	35
40	4	5	5	5	5	6	6	6	6	6	7	7	7	7	40
45	5	5	5	6	6	6	6	7	7	7	7	8	8	8	45
50	6	6	6	6	7	7	7	7	8	8	8	9	9	9	50
55	6	6	7	7	7	8	8	8	9	9	9	9	10	10	55
60	7	7	7	8	8	8	9	9	9	10	10	10	11	11	60
65	7	8	8	8	9	9	9	10	10	10	11	11	12	12	65
70	8	8	9	9	9	10	10	10	11	11	12	12	12	13	70
75	8	9	9	10	10	10	11	11	12	12	12	13	13	14	75
80	9	9	10	10	11	11	12	12	12	13	13	14	14	15	80
85	9	10	10	11	11	12	12	13	13	14	14	15	15	16	85
90	10	10	11	11	12	12	13	13	14	14	15	15	16	16	90
95	11	11	12	12	13	13	14	14	15	15	16	16	17	17	95
100	11	12	12	13	13	14	14	15	16	16	17	17	18	18	100
105	12	12	13	13	14	15	15	16	16	17	17	18	19	19	105
110	12	13	13	14	15	15	16	16	17	18	18	19	20	20	110
115	13	13	14	15	15	16	17	17	18	19	19	20	20	21	115
120	13	14	15	15	16	17	17	18	19	19	20	21	21	22	120
125	14	15	15	16	17	17	18	19	19	20	21	22	22	23	125
130	14	15	16	17	17	18	19	19	20	21	22	22	23	24	130
135	15	16	16	17	18	19	19	20	21	22	22	23	24	25	135
140	16	16	17	18	19	19	20	21	22	23	23	24	25	26	140
145	16	17	18	19	19	20	21	22	23	23	24	25	26	27	145
150	17	17	18	19	20	21	22	22	23	24	25	26	27	27	150
155	17	18	19	20	21	22	22	23	24	25	26	27	28	28	155
160	18	19	20	20	21	22	23	24	25	26	27	28	28	29	160
165	18	19	20	21	22	23	24	25	26	27	27	28	29	30	165
170	19	20	21	22	23	24	25	25	26	27	28	29	30	31	170
175	19	20	21	22	23	24	25	26	27	28	29	30	31	32	175
180	20	21	22	23	24	25	26	27	28	29	30	31	32	33	180
	40m	42m	44m	46m	48m	50m	52m	54m	56m	58m	60m	62m	64m	66m	

TABLE 12.

For finding the Variation of the Sun's Right Ascension or Declination, or of the Equation of Time, in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variation of the Moon's Declination or Right Ascension in seconds of time, the motion in one minute being given at the top, and the numbers in the side column being taken for seconds.

M.	Horary motion.																			M.
	1″	2″	3″	4″	5″	6″	7″	8″	9″	10″	11″	12″	13″	14″	15″	16″	17″	18″	19″	
1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	1	1	1	2
3	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	3
4	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	4
5	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	2	2	5
6	0	0	0	0	1	1	1	1	1	1	1	1	1	1	2	2	2	2	2	6
7	0	0	0	0	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	7
8	0	0	0	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	3	8
9	0	0	0	1	1	1	1	1	1	2	2	2	2	2	2	2	3	3	3	9
10	0	0	1	1	1	1	1	1	2	2	2	2	2	2	3	3	3	3	3	10
11	0	0	1	1	1	1	1	1	2	2	2	2	2	3	3	3	3	3	3	11
12	0	0	1	1	1	1	1	2	2	2	2	2	3	3	3	3	3	4	4	12
13	0	0	1	1	1	1	2	2	2	2	2	3	3	3	3	3	4	4	4	13
14	0	0	1	1	1	1	2	2	2	2	3	3	3	3	4	4	4	4	4	14
15	0	1	1	1	1	2	2	2	2	3	3	3	3	4	4	4	4	5	5	15
16	0	1	1	1	1	2	2	2	2	3	3	3	3	4	4	4	5	5	5	16
17	0	1	1	1	1	2	2	2	3	3	3	3	4	4	4	5	5	5	5	17
18	0	1	1	1	2	2	2	2	3	3	3	4	4	4	5	5	5	5	6	18
19	0	1	1	1	2	2	2	3	3	3	3	4	4	4	5	5	5	6	6	19
20	0	1	1	1	2	2	2	3	3	3	4	4	4	5	5	5	6	6	6	20
21	0	1	1	1	2	2	2	3	3	4	4	4	5	5	5	6	6	6	7	21
22	0	1	1	1	2	2	3	3	3	4	4	4	5	5	6	6	6	7	7	22
23	0	1	1	2	2	2	3	3	3	4	4	5	5	5	6	6	7	7	7	23
24	0	1	1	2	2	2	3	3	4	4	4	5	5	6	6	6	7	7	8	24
25	0	1	1	2	2	3	3	3	4	4	5	5	5	6	6	7	7	8	8	25
26	0	1	1	2	2	3	3	3	4	4	5	5	6	6	7	7	7	8	8	26
27	0	1	1	2	2	3	3	4	4	5	5	5	6	6	7	7	8	8	9	27
28	0	1	1	2	2	3	3	4	4	5	5	6	6	7	7	7	8	8	9	28
29	0	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	9	9	29
30	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	9	9	10	30
31	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	8	9	9	10	31
32	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	9	9	10	10	32
33	1	1	2	2	3	3	4	4	5	6	6	7	7	8	8	9	9	10	10	33
34	1	1	2	2	3	3	4	5	5	6	6	7	7	8	9	9	10	10	11	34
35	1	1	2	2	3	4	4	5	5	6	6	7	8	8	9	9	10	11	11	35
36	1	1	2	2	3	4	4	5	5	6	7	7	8	8	9	10	10	11	11	36
37	1	1	2	2	3	4	4	5	6	6	7	7	8	9	9	10	10	11	12	37
38	1	1	2	3	3	4	4	5	6	6	7	8	8	9	10	10	11	11	12	38
39	1	1	2	3	3	4	5	5	6	7	7	8	8	9	10	10	11	12	12	39
40	1	1	2	3	3	4	5	5	6	7	7	8	9	9	10	11	11	12	13	40
41	1	1	2	3	3	4	5	5	6	7	8	8	9	10	10	11	12	12	13	41
42	1	1	2	3	4	4	5	6	6	7	8	8	9	10	11	11	12	13	13	42
43	1	1	2	3	4	4	5	6	6	7	8	9	9	10	11	11	12	13	14	43
44	1	1	2	3	4	4	5	6	7	7	8	9	10	10	11	12	12	13	14	44
45	1	2	2	3	4	5	5	6	7	8	8	9	10	11	11	12	13	14	14	45
46	1	2	2	3	4	5	5	6	7	8	8	9	10	11	12	12	13	14	15	46
47	1	2	2	3	4	5	5	6	7	8	9	9	10	11	12	13	13	14	15	47
48	1	2	2	3	4	5	6	6	7	8	9	10	10	11	12	13	14	14	15	48
49	1	2	2	3	4	5	6	7	7	8	9	10	11	11	12	13	14	15	16	49
50	1	2	3	3	4	5	6	7	8	8	9	10	11	12	13	13	14	15	16	50
51	1	2	3	3	4	5	6	7	8	9	9	10	11	12	13	14	14	15	16	51
52	1	2	3	3	4	5	6	7	8	9	10	10	11	12	13	14	15	16	16	52
53	1	2	3	4	4	5	6	7	8	9	10	11	11	12	13	14	15	16	17	53
54	1	2	3	4	5	5	6	7	8	9	10	11	12	13	14	14	15	16	17	54
55	1	2	3	4	5	6	6	7	8	9	10	11	12	13	14	15	16	17	17	55
56	1	2	3	4	5	6	7	7	8	9	10	11	12	13	14	15	16	17	18	56
57	1	2	3	4	5	6	7	8	9	10	10	11	12	13	14	15	16	17	18	57
58	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	15	16	17	18	58
59	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	59
60	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	60

TABLE 12.

For finding the Variation of the Sun's Right Ascension or Declination, or of the Equation of Time, in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variation of the Moon's Declination or Right Ascension in seconds of time, the motion in one minute being given at the top, and the numbers in the side column being taken for seconds.

M.	Horary motion.																	M.
	20″	21″	22″	23″	24″	25″	26″	27″	28″	29″	30″	31″	32″	33″	34″	35″	36″	
1	0	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1
2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	2
3	1	1	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	3
4	1	1	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	4
5	2	2	2	2	2	2	2	2	2	2	3	3	3	3	3	3	3	5
6	2	2	2	2	2	3	3	3	3	3	3	3	3	3	3	4	4	6
7	2	2	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	7
8	3	3	3	3	3	3	3	4	4	4	4	4	4	4	5	5	5	8
9	3	3	3	3	4	4	4	4	4	4	5	5	5	5	5	5	5	9
10	3	4	4	4	4	4	4	5	5	5	5	5	5	6	6	6	6	10
11	4	4	4	4	4	5	5	5	5	5	6	6	6	6	6	6	7	11
12	4	4	4	5	5	5	5	5	6	6	6	6	6	7	7	7	7	12
13	4	5	5	5	5	5	6	6	6	6	7	7	7	7	7	8	8	13
14	5	5	5	5	6	6	6	6	7	7	7	7	7	8	8	8	8	14
15	5	5	6	6	6	6	7	7	7	7	8	8	8	8	9	9	9	15
16	5	6	6	6	6	7	7	7	7	8	8	8	9	9	9	9	10	16
17	6	6	6	7	7	7	7	8	8	8	9	9	9	9	10	10	10	17
18	6	6	7	7	7	8	8	8	8	9	9	9	10	10	10	11	11	18
19	6	7	7	7	8	8	8	9	9	9	10	10	10	10	11	11	11	19
20	7	7	7	8	8	8	9	9	9	10	10	10	11	11	11	12	12	20
21	7	7	8	8	8	9	9	9	10	10	11	11	11	12	12	12	13	21
22	7	8	8	8	9	9	10	10	10	11	11	11	12	12	12	13	13	22
23	8	8	8	9	9	10	10	10	11	11	12	12	12	13	13	13	14	23
24	8	8	9	9	10	10	10	11	11	12	12	12	13	13	14	14	14	24
25	8	9	9	10	10	10	11	11	12	12	13	13	13	14	14	15	15	25
26	9	9	10	10	10	11	11	12	12	13	13	13	14	14	15	15	16	26
27	9	9	10	10	11	11	12	12	13	13	14	14	14	15	15	16	16	27
28	9	10	10	11	11	12	12	13	13	14	14	14	15	15	16	16	17	28
29	10	10	11	11	12	12	13	13	14	14	15	15	15	16	16	17	17	29
30	10	11	11	12	12	13	13	14	14	15	15	16	16	17	17	18	18	30
31	10	11	11	12	12	13	13	14	14	15	16	16	17	17	18	18	19	31
32	11	11	12	12	13	13	14	14	15	15	16	17	17	18	18	19	19	32
33	11	12	12	13	13	14	14	15	15	16	17	17	18	18	19	19	20	33
34	11	12	12	13	14	14	15	15	16	16	17	18	18	19	19	20	20	34
35	12	12	13	13	14	15	15	16	16	17	18	18	19	19	20	20	21	35
36	12	13	13	14	14	15	16	16	17	17	18	19	19	20	20	21	22	36
37	12	13	14	14	15	15	16	17	17	18	19	19	20	20	21	22	22	37
38	13	13	14	15	15	16	16	17	18	18	19	20	20	21	22	22	23	38
39	13	14	14	15	16	16	17	18	18	19	20	20	21	21	22	23	23	39
40	13	14	15	15	16	17	17	18	19	19	20	21	21	22	23	23	24	40
41	14	14	15	16	16	17	18	18	19	20	21	21	22	23	23	24	25	41
42	14	15	15	16	17	18	18	19	20	20	21	22	22	23	24	25	25	42
43	14	15	16	16	17	18	19	19	20	21	22	22	23	24	24	25	26	43
44	15	15	16	17	18	18	19	20	21	21	22	23	23	24	25	26	26	44
45	15	16	17	17	18	19	20	20	21	22	23	23	24	25	26	26	27	45
46	15	16	17	18	18	19	20	21	21	22	23	24	25	25	26	27	28	46
47	16	16	17	18	19	20	20	21	22	23	24	24	25	26	27	27	28	47
48	16	17	18	18	19	20	21	22	22	23	24	25	26	26	27	28	29	48
49	16	17	18	19	20	20	21	22	23	24	25	25	26	27	28	29	29	49
50	17	18	18	19	20	21	22	23	23	24	25	26	27	28	28	29	30	50
51	17	18	19	20	20	21	22	23	24	25	26	26	27	28	29	30	31	51
52	17	18	19	20	21	22	23	23	24	25	26	27	28	29	29	30	31	52
53	18	19	19	20	21	22	23	24	25	26	27	27	28	29	30	31	32	53
54	18	19	20	21	22	23	23	24	25	26	27	28	29	30	31	32	32	54
55	18	19	20	21	22	23	24	25	26	27	28	28	29	30	31	32	33	55
56	19	20	21	21	22	23	24	25	26	27	28	29	30	31	32	33	34	56
57	19	20	21	22	23	24	25	26	27	28	29	29	30	31	32	33	34	57
58	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	58
59	20	21	22	23	24	25	26	27	28	29	30	30	31	32	33	34	35	59
60	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	60

TABLE 12.

For finding the Variation of the Sun's Right Ascension or Declination, or of the Equation of Time, in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variation of the Moon's Declination or Right Ascension in seconds of time, the motion in one minute being given at the top, and the numbers in the side column being taken for seconds.

M.	Horary motion.																	M.
	37″	38″	39″	40″	41″	42″	43″	44″	45″	46″	47″	48″	49″	50″	51″	52″	53″	
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
2	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	2	2	2
3	2	2	2	2	2	2	2	2	2	2	2	2	2	3	3	3	3	3
4	2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	4
5	3	3	3	3	3	4	4	4	4	4	4	4	4	4	4	4	4	5
6	4	4	4	4	4	4	4	4	5	5	5	5	5	5	5	5	5	6
7	4	4	5	5	5	5	5	5	5	5	5	6	6	6	6	6	6	7
8	5	5	5	5	5	6	6	6	6	6	6	6	7	7	7	7	7	8
9	6	6	6	6	6	6	6	7	7	7	7	7	7	8	8	8	8	9
10	6	6	7	7	7	7	7	7	8	8	8	8	8	8	9	9	9	10
11	7	7	7	7	8	8	8	8	8	8	9	9	9	9	9	10	10	11
12	7	8	8	8	8	8	9	9	9	9	9	10	10	10	10	10	11	12
13	8	8	8	9	9	9	9	10	10	10	10	10	11	11	11	11	11	13
14	9	9	9	9	10	10	10	10	11	11	11	11	11	12	12	12	12	14
15	9	10	10	10	10	11	11	11	11	12	12	12	12	13	13	13	13	15
16	10	10	10	11	11	11	11	12	12	12	13	13	13	13	14	14	14	16
17	10	11	11	11	12	12	12	12	13	13	13	14	14	14	14	15	15	17
18	11	11	12	12	12	13	13	13	14	14	14	14	15	15	15	16	16	18
19	12	12	12	13	13	13	14	14	14	15	15	15	16	16	16	16	17	19
20	12	13	13	13	14	14	14	15	15	15	16	16	16	17	17	17	18	20
21	13	13	14	14	14	15	15	15	16	16	16	17	17	18	18	18	19	21
22	14	14	14	15	15	15	16	16	17	17	17	18	18	18	19	19	19	22
23	14	15	15	15	16	16	16	17	17	18	18	18	19	19	20	20	20	23
24	15	15	16	16	16	17	17	18	18	18	19	19	20	20	20	21	21	24
25	15	16	16	17	17	18	18	18	19	19	20	20	20	21	21	22	22	25
26	16	16	17	17	18	18	19	19	20	20	20	21	21	22	22	23	23	26
27	17	17	18	18	18	19	19	20	20	21	21	22	22	23	23	23	24	27
28	17	18	18	19	19	20	20	21	21	21	22	22	23	23	24	24	25	28
29	18	18	19	19	20	20	21	21	22	22	23	23	24	24	25	25	26	29
30	19	19	20	20	21	21	22	22	23	23	24	24	25	25	26	26	27	30
31	19	20	20	21	21	22	22	23	23	24	24	25	25	26	26	27	27	31
32	20	20	21	21	22	22	23	23	24	25	25	26	26	27	27	28	28	32
33	20	21	21	22	23	23	24	24	25	25	26	26	27	28	28	29	29	33
34	21	22	22	23	23	24	24	25	26	26	27	27	28	28	29	29	30	34
35	22	22	23	23	24	25	25	26	26	27	27	28	29	29	30	30	31	35
36	22	23	23	24	25	25	26	26	27	28	28	29	29	30	31	31	32	36
37	23	23	24	25	25	26	27	27	28	28	29	30	30	31	31	32	33	37
38	23	24	25	25	26	27	27	28	29	29	30	30	31	32	32	33	34	38
39	24	25	25	26	27	27	28	29	29	30	31	31	32	33	33	34	34	39
40	25	25	26	27	27	28	29	29	30	31	31	32	33	33	34	35	35	40
41	25	26	27	27	28	29	29	30	31	31	32	33	33	34	35	36	36	41
42	26	27	27	28	29	29	30	31	32	32	33	34	34	35	36	36	37	42
43	27	27	28	29	29	30	31	32	32	33	34	34	35	36	37	37	38	43
44	27	28	29	29	30	31	32	32	33	34	34	35	36	37	37	38	39	44
45	28	29	29	30	31	32	32	33	34	35	35	36	37	38	38	39	40	45
46	28	29	30	31	31	32	33	34	35	35	36	37	38	38	39	40	41	46
47	29	30	31	31	32	33	34	34	35	36	37	38	38	39	40	41	42	47
48	30	30	31	32	33	34	34	35	36	37	38	38	39	40	41	42	42	48
49	30	31	32	33	33	34	35	36	37	38	38	39	40	41	42	42	43	49
50	31	32	33	33	34	35	36	37	38	38	39	40	41	42	43	43	44	50
51	31	32	33	34	35	36	37	37	38	39	40	41	42	43	43	44	45	51
52	32	33	34	35	36	36	37	38	39	40	41	42	42	43	44	45	46	52
53	33	34	34	35	36	37	38	39	40	41	42	42	43	44	45	46	47	53
54	33	34	35	36	37	38	39	40	41	41	42	43	44	45	46	47	48	54
55	34	35	36	37	38	39	39	40	41	42	43	44	45	46	47	48	49	55
56	35	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	49	56
57	35	36	37	38	39	40	41	42	43	44	45	46	47	48	48	49	50	57
58	36	37	38	39	40	41	42	43	44	44	45	46	47	48	49	50	51	58
59	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	59
60	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	60

TABLE 12.

For finding the Variation of the Sun's Right Ascension or Declination, or of the Equation of Time, in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variation of the Moon's Declination or Right Ascension in seconds of time, the motion in one minute being given at the top, and the numbers in the side column being taken for seconds.

M.	Horary motion.																	M.
	54″	55″	56″	57″	58″	59″	60″	61″	62″	63″	64″	65″	66″	67″	68″	69″	70″	
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	3
4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	5	5	5	4
5	5	5	5	5	5	5	5	5	5	5	5	5	6	6	6	6	6	5
6	5	6	6	6	6	6	6	6	6	6	6	7	7	7	7	7	7	6
7	6	6	7	7	7	7	7	7	7	7	7	8	8	8	8	8	8	7
8	7	7	7	8	8	8	8	8	8	8	9	9	9	9	9	9	9	8
9	8	8	8	9	9	9	9	9	9	9	10	10	10	10	10	10	11	9
10	9	9	9	10	10	10	10	10	10	11	11	11	11	11	11	12	12	10
11	10	10	10	10	11	11	11	11	11	12	12	12	12	12	12	13	13	11
12	11	11	11	11	12	12	12	12	12	13	13	13	13	13	14	14	14	12
13	12	12	12	12	13	13	13	13	13	14	14	14	14	15	15	15	15	13
14	13	13	13	13	14	14	14	14	14	15	15	15	15	16	16	16	16	14
15	14	14	14	14	15	15	15	15	16	16	16	16	17	17	17	17	18	15
16	14	15	15	15	15	16	16	16	17	17	17	17	18	18	18	18	19	16
17	15	16	16	16	16	17	17	17	18	18	18	18	19	19	19	20	20	17
18	16	17	17	17	17	18	18	18	19	19	19	20	20	20	20	21	21	18
19	17	17	18	18	18	19	19	19	20	20	20	21	21	21	22	22	22	19
20	18	18	19	19	19	20	20	20	21	21	21	22	22	22	23	23	23	20
21	19	19	20	20	20	21	21	21	22	22	22	23	23	23	24	24	25	21
22	20	20	21	21	21	22	22	22	23	23	23	24	24	25	25	25	26	22
23	21	21	21	22	22	23	23	23	24	24	25	25	25	26	26	26	27	23
24	22	22	22	23	23	24	24	24	25	25	26	26	26	27	27	28	28	24
25	23	23	23	24	24	25	25	25	26	26	27	27	28	28	28	29	29	25
26	23	24	24	25	25	26	26	26	27	27	28	28	29	29	29	30	30	26
27	24	25	25	26	26	27	27	27	28	28	29	29	30	30	31	31	32	27
28	25	26	26	27	27	28	28	28	29	29	30	30	31	31	32	32	33	28
29	26	27	27	28	28	29	29	29	30	30	31	31	32	32	33	33	34	29
30	27	28	28	29	29	30	30	31	31	32	32	33	33	34	34	35	35	30
31	28	28	29	29	30	30	31	32	32	33	33	34	34	35	35	36	36	31
32	29	29	30	30	31	31	32	33	33	34	34	35	35	36	36	37	37	32
33	30	30	31	31	32	32	33	34	34	35	35	36	36	37	37	38	39	33
34	31	31	32	32	33	33	34	35	35	36	36	37	37	38	39	39	40	34
35	32	32	33	33	34	34	35	36	36	37	37	38	39	39	40	40	41	35
36	32	33	34	34	35	35	36	37	37	38	38	39	40	40	41	41	42	36
37	33	34	35	35	36	36	37	38	38	39	39	40	41	41	42	43	43	37
38	34	35	35	36	37	37	38	39	39	40	41	41	42	42	43	44	44	38
39	35	36	36	37	38	38	39	40	40	41	42	42	43	44	44	45	46	39
40	36	37	37	38	39	39	40	41	41	42	43	43	44	45	45	46	47	40
41	37	38	38	39	40	40	41	42	42	43	44	44	45	46	46	47	48	41
42	38	39	39	40	41	41	42	43	43	44	45	46	46	47	48	48	49	42
43	39	39	40	41	42	42	43	44	44	45	46	47	47	48	49	49	50	43
44	40	40	41	42	43	43	44	45	45	46	47	48	48	49	50	51	51	44
45	41	41	42	43	44	44	45	46	47	47	48	49	50	50	51	52	53	45
46	41	42	43	44	44	45	46	47	48	48	49	50	51	51	52	53	54	46
47	42	43	44	45	45	46	47	48	49	49	50	51	52	52	53	54	55	47
48	43	44	45	46	46	47	48	49	50	50	51	52	53	54	54	55	56	48
49	44	45	46	47	47	48	49	50	51	51	52	53	54	55	56	56	57	49
50	45	46	47	48	48	49	50	51	52	53	53	54	55	56	57	58	58	50
51	46	47	48	48	49	50	51	52	53	54	54	55	56	57	58	59	60	51
52	47	48	49	49	50	51	52	53	54	55	55	56	57	58	59	60	61	52
53	48	49	49	50	51	52	53	54	55	56	57	57	58	59	60	61	62	53
54	49	50	50	51	52	53	54	55	56	57	58	59	59	60	61	62	63	54
55	50	50	51	52	53	54	55	56	57	58	59	60	61	61	62	63	64	55
56	50	51	52	53	54	55	56	57	58	59	60	61	62	63	63	64	65	56
57	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	57
58	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	58
59	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	59
60	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	60

6583—06——33

TABLE 12.

For finding the Variation of the Sun's Right Ascension or Declination, or of the Equation of Time, in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variation of the Moon's Declination or Right Ascension in seconds of time, the motion in one minute being given at the top, and the numbers in the side column being taken for seconds.

M.	Horary motion.																	M.
	71″	72″	73″	74″	75″	76″	77″	78″	79″	80″	81″	82″	83″	84″	85″	86″	87″	
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
2	2	2	2	2	3	3	3	3	3	3	3	3	3	3	3	3	3	2
3	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	3
4	5	5	5	5	5	5	5	5	5	5	5	5	6	6	6	6	6	4
5	6	6	6	6	6	6	6	7	7	7	7	7	7	7	7	7	7	5
6	7	7	7	7	8	8	8	8	8	8	8	8	8	8	9	9	9	6
7	8	8	9	9	9	9	9	9	9	9	9	10	10	10	10	10	10	7
8	9	10	10	10	10	10	10	10	11	11	11	11	11	11	11	11	12	8
9	11	11	11	11	11	11	12	12	12	12	12	12	12	13	13	13	13	9
10	12	12	12	12	13	13	13	13	13	13	14	14	14	14	14	14	15	10
11	13	13	13	14	14	14	14	14	14	15	15	15	15	15	16	16	16	11
12	14	14	15	15	15	15	15	16	16	16	16	16	17	17	17	17	17	12
13	15	16	16	16	16	16	17	17	17	17	18	18	18	18	18	19	19	13
14	17	17	17	17	18	18	18	18	18	19	19	19	19	20	20	20	20	14
15	18	18	18	19	19	19	19	20	20	20	20	21	21	21	21	22	22	15
16	19	19	19	20	20	20	21	21	21	21	22	22	22	22	23	23	23	16
17	20	20	21	21	21	22	22	22	22	23	23	23	24	24	24	24	25	17
18	21	22	22	22	23	23	23	23	24	24	24	25	25	25	26	26	26	18
19	22	23	23	23	24	24	24	25	25	25	26	26	26	27	27	27	28	19
20	24	24	24	25	25	25	26	26	26	27	27	27	28	28	28	29	29	20
21	25	25	26	26	26	27	27	27	28	28	28	29	29	29	30	30	30	21
22	26	26	27	27	28	28	28	29	29	29	30	30	30	31	31	32	32	22
23	27	28	28	28	29	29	30	30	30	31	31	31	32	32	33	33	33	23
24	28	29	29	30	30	30	31	31	32	32	32	33	33	34	34	34	34	24
25	30	30	30	31	31	32	32	33	33	33	34	34	35	35	35	36	36	25
26	31	31	32	32	33	33	33	34	34	35	35	36	36	36	37	37	38	26
27	32	32	33	33	34	34	35	35	36	36	36	37	37	38	38	39	39	27
28	33	34	34	35	35	35	36	36	37	37	38	38	39	39	40	40	41	28
29	34	35	35	36	36	37	37	38	38	39	39	40	40	41	41	42	42	29
30	36	36	37	37	38	38	39	39	40	40	41	41	42	42	43	43	44	30
31	37	37	38	38	39	39	40	40	41	41	42	42	43	43	44	44	45	31
32	38	38	39	39	40	41	41	42	42	43	43	44	44	45	45	46	46	32
33	39	40	40	41	41	42	42	43	43	44	45	45	46	46	47	47	48	33
34	40	41	41	42	43	43	44	44	45	45	46	46	47	48	48	49	49	34
35	41	42	43	43	44	44	45	46	46	47	47	48	48	49	50	50	51	35
36	43	43	44	44	45	46	46	47	47	48	49	49	50	50	51	52	52	36
37	44	44	45	46	46	47	47	48	49	49	50	51	51	52	52	53	54	37
38	45	46	46	47	48	48	49	49	50	51	51	52	53	53	54	54	55	38
39	46	47	47	48	49	49	50	51	51	52	53	53	54	55	55	56	57	39
40	47	48	49	49	50	51	51	52	53	53	54	55	55	56	57	57	58	40
41	49	49	50	51	51	52	53	53	54	55	55	56	57	57	58	59	59	41
42	50	50	51	52	53	53	54	55	55	56	57	57	58	59	60	60	61	42
43	51	52	52	53	54	54	55	56	57	57	58	59	59	60	61	62	62	43
44	52	53	54	54	55	56	56	57	58	59	59	60	61	62	62	63	64	44
45	53	54	55	56	56	57	58	59	59	60	61	62	62	63	64	65	65	45
46	54	55	56	57	58	58	59	60	61	61	62	63	64	64	65	66	67	46
47	56	56	57	58	59	60	60	61	62	63	63	64	65	66	67	67	68	47
48	57	58	58	59	60	61	62	62	63	64	65	66	66	67	68	69	70	48
49	58	59	60	60	61	62	63	64	65	65	66	67	68	69	69	70	71	49
50	59	60	61	62	63	63	64	65	66	67	68	68	69	70	71	72	73	50
51	60	61	62	63	64	65	65	66	67	68	69	70	71	71	72	73	74	51
52	62	62	63	64	65	66	67	68	68	69	70	71	72	73	74	75	75	52
53	63	64	64	65	66	67	68	69	70	71	72	72	73	74	75	76	77	53
54	64	65	66	67	68	68	69	70	71	72	73	74	75	76	77	77	78	54
55	65	66	67	68	69	70	71	72	72	73	74	75	76	77	78	79	80	55
56	66	67	68	69	70	71	72	73	74	75	76	77	77	78	79	80	81	56
57	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	57
58	69	70	71	72	73	73	74	75	76	77	78	79	80	81	82	83	84	58
59	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	59
60	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	60

TABLE 12.

For finding the Variation of the Sun's Right Ascension or Declination, or of the Equation of Time, in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variation of the Moon's Declination or Right Ascension, in seconds of time, the motion in one minute being given at the top and the numbers in the side column being taken for seconds.

M.	Horary motion.																	M.
	88″	89″	90″	91″	92″	93″	94″	95″	96″	97″	98″	99″	100″	101″	102″	103″	104″	
1	1	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	1
2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	2
3	4	4	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	3
4	6	6	6	6	6	6	6	6	6	6	7	7	7	7	7	7	7	4
5	7	7	8	8	8	8	8	8	8	8	8	8	8	8	9	9	9	5
6	9	9	9	9	9	9	9	10	10	10	10	10	10	10	10	10	10	6
7	10	10	11	11	11	11	11	11	11	11	11	12	12	12	12	12	12	7
8	12	12	12	12	12	12	13	13	13	13	13	13	13	13	14	14	14	8
9	13	13	14	14	14	14	14	14	14	15	15	15	15	15	15	15	16	9
10	15	15	15	15	15	16	16	16	16	16	16	17	17	17	17	17	17	10
11	16	16	17	17	17	17	17	17	18	18	18	18	18	19	19	19	19	11
12	18	18	18	18	18	19	19	19	19	19	20	20	20	20	20	21	21	12
13	19	19	20	20	20	20	20	21	21	21	21	21	22	22	22	22	23	13
14	21	21	21	21	21	22	22	22	22	23	23	23	23	24	24	24	24	14
15	22	22	23	23	23	23	24	24	24	24	25	25	25	25	26	26	26	15
16	23	24	24	24	25	25	25	25	26	26	26	26	27	27	27	27	28	16
17	25	25	26	26	26	26	27	27	27	27	28	28	28	29	29	29	29	17
18	26	27	27	27	28	28	28	29	29	29	29	30	30	30	31	31	31	18
19	28	28	29	29	29	29	30	30	30	31	31	31	32	32	32	33	33	19
20	29	30	30	30	31	31	31	32	32	32	33	33	33	34	34	34	35	20
21	31	31	32	32	32	33	33	33	34	34	34	35	35	35	36	36	36	21
22	32	33	33	33	34	34	34	35	35	36	36	36	37	37	37	38	38	22
23	34	34	35	35	35	36	36	36	37	37	38	38	38	39	39	39	40	23
24	35	36	36	36	37	37	38	38	38	39	39	40	40	40	41	41	42	24
25	37	37	38	38	38	39	39	40	40	40	41	41	42	42	43	43	43	25
26	38	39	39	39	40	40	41	41	42	42	42	43	43	44	44	45	45	26
27	40	40	41	41	41	42	42	43	43	44	44	45	45	45	46	46	47	27
28	41	42	42	42	43	43	44	44	45	45	46	46	47	47	48	48	49	28
29	43	43	44	44	44	45	45	46	46	47	47	48	48	49	49	50	50	29
30	44	45	45	46	46	47	47	48	48	49	49	50	50	51	51	52	52	30
31	45	46	47	47	48	48	49	49	50	50	51	51	52	52	53	53	54	31
32	47	47	48	49	49	50	50	51	51	52	52	53	53	54	54	55	55	32
33	48	49	50	50	51	51	52	52	53	53	54	54	55	56	56	57	57	33
34	50	50	51	52	52	53	53	54	54	55	56	56	57	57	58	58	59	34
35	51	52	53	53	54	54	55	55	56	57	57	58	58	59	60	60	61	35
36	53	53	54	55	55	56	56	57	58	58	59	59	60	61	61	62	62	36
37	54	55	56	56	57	57	58	59	59	60	60	61	62	62	63	64	64	37
38	56	56	57	58	58	59	60	60	61	61	62	63	63	64	65	65	66	38
39	57	58	59	59	60	60	61	62	62	63	64	64	65	66	66	67	68	39
40	59	59	60	61	61	62	63	63	64	65	65	66	67	67	68	69	69	40
41	60	61	62	62	63	64	64	65	66	66	67	68	68	69	70	70	71	41
42	62	62	63	64	64	65	66	67	67	68	69	69	70	71	71	72	73	42
43	63	64	65	65	66	67	67	68	69	70	70	71	72	72	73	74	75	43
44	65	65	66	67	67	68	69	70	70	71	72	73	73	74	75	76	76	44
45	66	67	68	68	69	70	71	71	72	73	74	74	75	76	77	77	78	45
46	67	68	69	70	71	71	72	73	74	74	75	76	77	77	78	79	80	46
47	69	70	71	71	72	73	74	74	75	76	77	78	78	79	80	81	81	47
48	70	71	72	73	74	74	75	76	77	78	78	79	80	81	82	82	83	48
49	72	73	74	74	75	76	77	78	78	79	80	81	82	82	83	84	85	49
50	73	74	75	76	77	78	78	79	80	81	82	83	83	84	85	86	87	50
51	75	76	77	77	78	79	80	81	82	82	83	84	85	86	87	88	88	51
52	76	77	78	79	80	81	81	82	83	84	85	86	87	88	88	89	90	52
53	78	79	80	80	81	82	83	84	85	86	87	87	88	89	90	91	92	53
54	79	80	81	82	83	84	85	86	86	87	88	89	90	91	92	93	94	54
55	81	82	83	83	84	85	86	87	88	89	90	91	92	93	94	94	95	55
56	82	83	84	85	86	87	88	89	90	91	91	92	93	94	95	96	97	56
57	84	85	86	86	87	88	89	90	91	92	93	94	95	96	97	98	99	57
58	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	58
59	87	88	89	90	90	91	92	93	94	95	96	97	98	99	100	101	102	59
60	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	60

TABLE 12.

For finding the Variation of the Sun's Right Ascension or Declination, or of the Equation of Time, in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variatior of the Moon's Declination or Right Ascension, in seconds of time, the motion in one minute being given at the top and the numbers in the side column being taken for seconds.

M.	Horary motion.														M.
	105″	106″	107″	108″	109″	110″	111″	112″	113″	114″	115″	116″	117″	118″	
1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	1
2	4	4	4	4	4	4	4	4	4	4	4	4	4	4	2
3	5	5	5	5	5	6	6	6	6	6	6	6	6	6	3
4	7	7	7	7	7	7	7	7	8	8	8	8	8	8	4
5	9	9	9	9	9	9	9	9	9	10	10	10	10	10	5
6	11	11	11	11	11	11	11	11	11	11	12	12	12	12	6
7	12	12	12	13	13	13	13	13	13	13	13	14	14	14	7
8	14	14	14	14	15	15	15	15	15	15	15	15	16	16	8
9	16	16	16	16	16	17	17	17	17	17	17	17	18	18	9
10	18	18	18	18	18	18	19	19	19	19	19	19	20	20	10
11	19	19	20	20	20	20	20	21	21	21	21	21	21	22	11
12	21	21	21	22	22	22	22	22	23	23	23	23	23	24	12
13	23	23	23	23	24	24	24	24	24	25	25	25	25	26	13
14	25	25	25	25	25	26	26	26	26	27	27	27	27	28	14
15	26	27	27	27	27	28	28	28	28	29	29	29	29	30	15
16	28	28	29	29	29	29	30	30	30	30	31	31	31	31	16
17	30	30	30	31	31	31	31	32	32	32	33	33	33	33	17
18	32	32	32	32	33	33	33	34	34	34	35	35	35	35	18
19	33	34	34	34	35	35	35	35	36	36	36	37	37	37	19
20	35	35	36	36	36	37	37	37	38	38	38	39	39	39	20
21	37	37	37	38	38	39	39	39	40	40	40	41	41	41	21
22	39	39	39	40	40	40	41	41	41	42	42	43	43	43	22
23	40	41	41	41	42	42	43	43	43	44	44	44	45	45	23
24	42	42	43	43	44	44	44	45	45	46	46	46	47	47	24
25	44	44	45	45	45	46	46	47	47	48	48	48	49	49	25
26	46	46	46	47	47	48	48	49	49	49	50	50	51	51	26
27	47	48	48	49	49	50	50	50	51	51	52	52	53	53	27
28	49	49	50	50	51	51	52	52	53	53	54	54	55	55	28
29	51	51	52	52	53	53	54	54	55	55	56	56	57	57	29
30	53	53	54	54	55	55	56	56	57	57	58	58	59	59	30
31	54	55	55	56	56	57	57	58	58	59	59	60	60	61	31
32	56	57	57	58	58	59	59	60	60	61	61	62	62	63	32
33	58	58	59	59	60	61	61	62	62	63	63	64	64	65	33
34	60	60	61	61	62	62	63	63	64	65	65	66	66	67	34
35	61	62	62	63	64	64	65	65	66	67	67	68	68	69	35
36	63	64	64	65	65	66	67	67	68	68	69	70	70	71	36
37	65	65	66	67	67	68	68	69	70	70	71	72	72	73	37
38	67	67	68	68	69	70	70	71	72	72	73	73	74	75	38
39	68	69	70	70	71	72	72	73	73	74	75	75	76	77	39
40	70	71	71	72	73	73	74	75	75	76	77	77	78	79	40
41	72	72	73	74	74	75	76	77	77	78	79	79	80	81	41
42	74	74	75	76	76	77	78	78	79	80	81	81	82	83	42
43	75	76	77	77	78	79	80	80	81	82	82	83	84	85	43
44	77	78	78	79	80	81	81	82	83	84	84	85	86	87	44
45	79	80	80	81	82	83	83	84	85	86	86	87	88	89	45
46	81	81	82	83	84	84	85	86	87	87	88	89	90	90	46
47	82	83	84	85	85	86	87	88	89	89	90	91	92	92	47
48	84	85	86	86	87	88	89	90	90	91	92	93	94	94	48
49	86	87	87	88	89	90	91	91	92	93	94	95	96	96	49
50	88	88	89	90	91	92	93	93	94	95	96	97	98	98	50
51	89	90	91	92	93	94	94	95	96	97	98	99	99	100	51
52	91	92	93	94	94	95	96	97	98	99	100	101	101	102	52
53	93	94	95	95	96	97	98	99	100	101	102	102	103	104	53
54	95	95	96	97	98	99	100	101	102	103	104	104	105	106	54
55	96	97	98	99	100	101	102	103	104	105	105	106	107	108	55
56	98	99	100	101	102	103	104	105	105	106	107	108	109	110	56
57	100	101	102	103	104	105	105	106	107	108	109	110	111	112	57
58	102	102	103	104	105	106	107	108	109	110	111	112	113	114	58
59	103	104	105	106	107	108	109	110	111	112	113	114	115	116	59
60	105	106	107	108	109	110	111	112	113	114	115	116	117	118	60

For finding the Variation of the Sun's Right Ascension or Declination, or of the Equation of Time, in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variation of the Moon's Declination or Right Ascension in seconds of time, the motion in one minute being given at the top, and the numbers in the side column being taken for seconds.

M.	Horary motion.														M.
	119″	120″	121″	122″	123″	124″	125″	126″	127″	128″	129″	130″	131″	132″	
1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	1
2	4	4	4	4	4	4	4	4	4	4	4	4	4	4	2
3	6	6	6	6	6	6	6	6	6	6	6	7	7	7	3
4	8	8	8	8	8	8	8	8	8	9	9	9	9	9	4
5	10	10	10	10	10	10	10	11	11	11	11	11	11	11	5
6	12	12	12	12	12	12	13	13	13	13	13	13	13	13	6
7	14	14	14	14	14	14	15	15	15	15	15	15	15	15	7
8	16	16	16	16	16	17	17	17	17	17	17	17	17	18	8
9	18	18	18	18	18	19	19	19	19	19	19	20	20	20	9
10	20	20	20	20	21	21	21	21	21	21	22	22	22	22	10
11	22	22	22	22	23	23	23	23	23	23	24	24	24	24	11
12	24	24	24	24	25	25	25	25	25	26	26	26	26	26	12
13	26	26	26	26	27	27	27	27	28	28	28	28	28	29	13
14	28	28	28	28	29	29	29	29	30	30	30	30	31	31	14
15	30	30	30	31	31	31	31	32	32	32	32	33	33	33	15
16	32	32	32	33	33	33	33	34	34	34	34	35	35	35	16
17	34	34	34	35	35	35	35	36	36	36	37	37	37	37	17
18	36	36	36	37	37	37	38	38	38	38	39	39	39	40	18
19	38	38	38	39	39	39	40	40	40	41	41	41	41	42	19
20	40	40	40	41	41	41	42	42	42	43	43	43	44	44	20
21	42	42	42	43	43	43	44	44	44	45	45	46	46	46	21
22	44	44	44	45	45	45	46	46	47	47	47	48	48	48	22
23	46	46	46	47	47	48	48	48	49	49	49	50	50	51	23
24	48	48	48	49	49	50	50	50	51	51	52	52	52	53	24
25	50	50	50	51	51	52	52	53	53	53	54	54	55	55	25
26	52	52	52	53	53	54	54	55	55	55	56	56	57	57	26
27	54	54	54	55	55	56	56	57	57	58	58	59	59	59	27
28	56	56	56	57	57	58	58	59	59	60	60	61	61	62	28
29	58	58	58	59	59	60	60	61	61	62	62	63	63	64	29
30	60	60	61	61	62	62	63	63	64	64	65	65	66	66	30
31	61	62	63	63	64	64	65	65	66	66	67	67	68	68	31
32	63	64	65	65	66	66	67	67	68	68	69	69	70	70	32
33	65	66	67	67	68	68	69	69	70	70	71	72	72	73	33
34	67	68	69	69	70	70	71	71	72	73	73	74	74	75	34
35	69	70	71	71	72	72	73	74	74	75	75	76	76	77	35
36	71	72	73	73	74	74	75	76	76	77	77	78	79	79	36
37	73	74	75	75	76	76	77	78	78	79	80	80	81	81	37
38	75	76	77	77	78	79	79	80	80	81	82	82	83	84	38
39	77	78	79	79	80	81	81	82	83	83	84	85	85	86	39
40	79	80	81	81	82	83	83	84	85	85	86	87	87	88	40
41	81	82	83	83	84	85	85	86	87	87	88	89	90	90	41
42	83	84	85	85	86	87	88	88	89	90	90	91	92	92	42
43	85	86	87	87	88	89	90	90	91	92	92	93	94	95	43
44	87	88	89	89	90	91	92	92	93	94	95	95	96	97	44
45	89	90	91	92	92	93	94	95	95	96	97	98	98	99	45
46	91	92	93	94	94	95	96	97	97	98	99	100	100	101	46
47	93	94	95	96	96	97	98	99	99	100	101	102	103	103	47
48	95	96	97	98	98	99	100	101	102	102	103	104	105	106	48
49	97	98	99	100	100	101	102	103	104	105	105	106	107	108	49
50	99	100	101	102	103	103	104	105	106	107	108	108	109	110	50
51	101	102	103	104	105	105	106	107	108	109	110	111	111	112	51
52	103	104	105	106	107	107	108	109	110	111	112	113	114	114	52
53	105	106	107	108	109	110	110	111	112	113	114	115	116	117	53
54	107	108	109	110	111	112	113	113	114	115	116	117	118	119	54
55	109	110	111	112	113	114	115	116	116	117	118	119	120	121	55
56	111	112	113	114	115	116	117	118	119	119	120	121	122	123	56
57	113	114	115	116	117	118	119	120	121	122	123	124	124	125	57
58	115	116	117	118	119	120	121	122	123	124	125	126	127	128	58
59	117	118	119	120	121	122	123	124	125	126	127	128	129	130	59
60	119	120	121	122	123	124	125	126	127	128	129	130	131	132	60

TABLE 12.

For finding the Variation of the Sun's Right Ascension or Declination, or of the Equation of Time, in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variation of the Moon's Declination or Right Ascension in seconds of time, the motion in one minute being given at the top, and the numbers in the side column being taken for seconds.

M.	Horary motion.														M.
	133″	134″	135″	136″	137″	138″	139″	140″	141″	142″	143″	144″	145″	146″	
1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	1
2	4	4	5	5	5	5	5	5	5	5	5	5	5	5	2
3	7	7	7	7	7	7	7	7	7	7	7	7	7	7	3
4	9	9	9	9	9	9	9	9	9	9	10	10	10	10	4
5	11	11	11	11	11	12	12	12	12	12	12	12	12	12	5
6	13	13	14	14	14	14	14	14	14	14	14	14	15	15	6
7	16	16	16	16	16	16	16	16	16	17	17	17	17	17	7
8	18	18	18	18	18	18	19	19	19	19	19	19	19	19	8
9	20	20	20	20	21	21	21	21	21	21	21	22	22	22	9
10	22	22	23	23	23	23	23	23	24	24	24	24	24	24	10
11	24	25	25	25	25	25	25	26	26	26	26	26	27	27	11
12	27	27	27	27	27	28	28	28	28	28	29	29	29	29	12
13	29	29	29	29	30	30	30	30	31	31	31	31	31	32	13
14	31	31	32	32	32	32	32	33	33	33	33	34	34	34	14
15	33	34	34	34	34	35	35	35	35	36	36	36	36	37	15
16	35	36	36	36	37	37	37	37	38	38	38	38	39	39	16
17	38	38	38	39	39	39	39	40	40	40	41	41	41	41	17
18	40	40	41	41	41	41	42	42	42	43	43	43	44	44	18
19	42	42	43	43	43	44	44	44	45	45	45	46	46	46	19
20	44	45	45	45	46	46	46	47	47	47	48	48	48	49	20
21	47	47	47	48	48	48	49	49	49	50	50	50	51	51	21
22	49	49	50	50	50	51	51	51	52	52	52	53	53	54	22
23	51	51	52	52	53	53	53	54	54	54	55	55	56	56	23
24	53	54	54	54	55	55	56	56	56	57	57	58	58	58	24
25	55	56	56	57	57	58	58	58	59	59	60	60	60	61	25
26	58	58	59	59	59	60	60	61	61	62	62	62	63	63	26
27	60	60	61	61	62	62	63	63	63	64	64	65	65	66	27
28	62	63	63	63	64	64	65	65	66	66	67	67	68	68	28
29	64	65	65	66	66	67	67	68	68	69	69	70	70	71	29
30	67	67	68	68	69	69	70	70	71	71	72	72	73	73	30
31	69	69	70	70	71	71	72	72	73	73	74	74	75	75	31
32	71	71	72	73	73	74	74	75	75	76	76	77	77	78	32
33	73	74	74	75	75	76	76	77	78	78	79	79	80	80	33
34	75	76	77	77	78	78	79	79	80	80	81	82	82	83	34
35	78	78	79	79	80	81	81	82	82	83	83	84	85	85	35
36	80	80	81	82	82	83	83	84	85	85	86	86	87	88	36
37	82	83	83	84	84	85	86	86	87	88	88	89	89	90	37
38	84	85	86	86	87	87	88	89	89	90	91	91	92	92	38
39	86	87	88	88	89	90	90	91	92	92	93	94	94	95	39
40	89	89	90	91	91	92	93	93	94	95	95	96	97	97	40
41	91	92	92	93	94	94	95	96	96	97	98	98	99	100	41
42	93	94	95	95	96	97	97	98	99	99	100	101	102	102	42
43	95	96	97	97	98	99	100	100	101	102	102	103	104	105	43
44	98	98	99	100	100	101	102	103	103	104	105	106	106	107	44
45	100	101	101	102	103	104	104	105	106	107	107	108	109	110	45
46	102	103	104	104	105	106	107	107	108	109	110	110	111	112	46
47	104	105	106	107	107	108	109	110	110	111	112	113	114	114	47
48	106	107	108	109	110	110	111	112	113	114	114	115	116	117	48
49	109	109	110	111	112	113	114	114	115	116	117	118	118	119	49
50	111	112	113	113	114	115	116	117	118	118	119	120	121	122	50
51	113	114	115	116	116	117	118	119	120	121	122	122	123	124	51
52	115	116	117	118	119	120	120	121	122	123	124	125	126	127	52
53	117	118	119	120	121	122	123	124	125	125	126	127	128	129	53
54	120	121	122	122	123	124	125	126	127	128	129	130	131	131	54
55	122	123	124	125	126	127	127	128	129	130	131	132	133	134	55
56	124	125	126	127	128	129	130	131	132	133	133	134	135	136	56
57	126	127	128	129	130	131	132	133	134	135	136	137	138	139	57
58	129	130	131	131	132	133	134	135	136	137	138	139	140	141	58
59	131	132	133	134	135	136	137	138	139	140	141	142	143	144	59
60	133	134	135	136	137	138	139	140	141	142	143	144	145	146	60

For finding the Variation of the Sun's Right Ascension, or Declination, or of the Equation of Time in any number of minutes of time, the Horary Motion being given at the top of the page in seconds, and the number of minutes of time in the side column. Also for finding the Variation of the Moon's Declination or Right Ascension in seconds of time, the motion in one minute being given at the top, and the numbers in the side column being taken for seconds.

M.	Horary motion.														M.
	147″	148″	149″	150″	151″	152″	153″	154″	155″	156″	157″	158″	159″	160″	
1	2	2	2	3	3	3	3	3	3	3	3	3	3	3	1
2	5	5	5	5	5	5	5	5	5	5	5	5	5	5	2
3	7	7	7	8	8	8	8	8	8	8	8	8	8	8	3
4	10	10	10	10	10	10	10	10	10	10	10	11	11	11	4
5	12	12	12	13	13	13	13	13	13	13	13	13	13	13	5
6	15	15	15	15	15	15	15	15	16	16	16	16	16	16	6
7	17	17	17	18	18	18	18	18	18	18	18	18	19	19	7
8	20	20	20	20	20	20	20	21	21	21	21	21	21	21	8
9	22	22	22	23	23	23	23	23	23	23	24	24	24	24	9
10	25	25	25	25	25	25	26	26	26	26	26	26	27	27	10
11	27	27	27	28	28	28	28	28	28	29	29	29	29	29	11
12	29	30	30	30	30	30	31	31	31	31	31	32	32	32	12
13	32	32	32	33	33	33	33	33	34	34	34	34	34	35	13
14	34	35	35	35	35	35	36	36	36	36	37	37	37	37	14
15	37	37	37	38	38	38	38	39	39	39	39	40	40	40	15
16	39	39	40	40	40	41	41	41	41	42	42	42	42	43	16
17	42	42	42	43	43	43	43	44	44	44	44	45	45	45	17
18	44	44	45	45	45	46	46	46	47	47	47	47	48	48	18
19	47	47	47	48	48	48	48	49	49	49	50	50	50	51	19
20	49	49	50	50	50	51	51	51	52	52	52	53	53	53	20
21	51	52	52	53	53	53	54	54	54	55	55	55	56	56	21
22	54	54	55	55	55	56	56	56	57	57	58	58	58	59	22
23	56	57	57	58	58	58	59	59	59	60	60	61	61	61	23
24	59	59	60	60	60	61	61	62	62	62	63	63	64	64	24
25	61	62	62	63	63	63	64	64	65	65	65	66	66	67	25
26	64	64	65	65	65	66	66	67	67	68	68	68	69	69	26
27	66	67	67	68	68	68	69	69	70	70	71	71	72	72	27
28	69	69	70	70	70	71	71	72	72	73	73	74	74	75	28
29	71	72	72	73	73	73	74	74	75	75	76	76	77	77	29
30	74	74	75	75	76	76	77	77	78	78	79	79	80	80	30
31	76	76	77	78	78	79	79	80	80	81	81	82	82	83	31
32	78	79	79	80	81	81	82	82	83	83	84	84	85	85	32
33	81	81	82	83	83	84	84	85	85	86	86	87	87	88	33
34	83	84	84	85	86	86	87	87	88	88	89	90	90	91	34
35	86	86	87	88	88	89	89	90	90	91	92	92	93	93	35
36	88	89	89	90	91	91	92	92	93	94	94	95	95	96	36
37	91	91	92	93	93	94	94	95	96	96	97	97	98	99	37
38	93	94	94	95	96	96	97	98	98	99	99	100	101	101	38
39	96	96	97	98	98	99	99	100	101	101	102	103	103	104	39
40	98	99	99	100	101	101	102	103	103	104	105	105	106	107	40
41	100	101	102	103	103	104	105	105	106	107	107	108	109	109	41
42	103	104	104	105	106	106	107	108	109	109	110	111	111	112	42
43	105	106	107	108	108	109	110	110	111	112	113	113	114	115	43
44	108	109	109	110	111	111	112	113	114	114	115	116	117	117	44
45	110	111	112	113	113	114	115	116	116	117	118	119	119	120	45
46	113	113	114	115	116	117	117	118	119	120	120	121	122	123	46
47	115	116	117	118	118	119	120	121	121	122	123	124	125	125	47
48	118	118	119	120	121	122	122	123	124	125	126	126	127	128	48
49	120	121	122	123	123	124	125	126	127	127	128	129	130	131	49
50	123	123	124	125	126	127	128	128	129	130	131	132	133	133	50
51	125	126	127	128	128	129	130	131	132	133	133	134	135	136	51
52	127	128	129	130	131	132	133	133	134	135	136	137	138	139	52
53	130	131	132	133	133	134	135	136	137	138	139	140	140	141	53
54	132	133	134	135	136	137	138	139	140	140	141	142	143	144	54
55	135	136	137	138	138	139	140	141	142	143	144	145	146	147	55
56	137	138	139	140	141	142	143	144	145	146	147	147	148	149	56
57	140	141	142	143	143	144	145	146	147	148	149	150	151	152	57
58	142	143	144	145	146	147	148	149	150	151	152	153	154	155	58
59	145	146	147	148	148	149	150	151	152	153	154	155	156	157	59
60	147	148	149	150	151	152	153	154	155	156	157	158	159	160	60

TABLE 13.

For finding the Sun's change of Right Ascension for any given number of hours.

Hourly variation.	Number of hours.												Hourly variation.
	1	2	3	4	5	6	7	8	9	10	11	12	
s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.
8.50	8.5	17.0	25.5	34.0	42.5	51.0	59.5	68.0	76.5	85.0	93.5	102.0	8.50
8.55	8.6	17.1	25.7	34.2	42.8	51.3	59.9	68.4	77.0	85.5	94.1	102.6	8.55
8.60	8.6	17.2	25.8	34.4	43.0	51.6	60.2	68.8	77.4	86.0	94.6	103.2	8.60
8.65	8.7	17.3	26.0	34.6	43.3	51.9	60.6	69.2	77.9	86.5	95.2	103.8	8.65
8.70	8.7	17.4	26.1	34.8	43.5	52.2	60.9	69.6	78.3	87.0	95.7	104.4	8.70
8.75	8.8	17.5	26.3	35.0	43.8	52.5	61.3	70.0	78.8	87.5	96.3	105.0	8.75
8.80	8.8	17.6	26.4	35.2	44.0	52.8	61.6	70.4	79.2	88.0	96.8	105.6	8.80
8.85	8.9	17.7	26.6	35.4	44.3	53.1	62.0	70.8	79.7	88.5	97.4	106.2	8.85
8.90	8.9	17.8	26.7	35.6	44.5	53.4	62.3	71.2	80.1	89.0	97.9	106.8	8.90
8.95	9.0	17.9	26.9	35.8	44.8	53.7	62.7	71.6	80.6	89.5	98.5	107.4	8.95
9.00	9.0	18.0	27.0	36.0	45.0	54.0	63.0	72.0	81.0	90.0	99.0	108.0	9.00
9.05	9.1	18.1	27.2	36.2	45.3	54.3	63.4	72.4	81.5	90.5	99.6	108.6	9.05
9.10	9.1	18.2	27.3	36.4	45.5	54.6	63.7	72.8	81.9	91.0	100.1	109.2	9.10
9.15	9.2	18.3	27.5	36.6	45.8	54.9	64.1	73.2	82.4	91.5	100.7	109.8	9.15
9.20	9.2	18.4	27.6	36.8	46.0	55.2	64.4	73.6	82.8	92.0	101.2	110.4	9.20
9.25	9.3	18.5	27.8	37.0	46.3	55.5	64.8	74.0	83.3	92.5	101.8	111.0	9.25
9.30	9.3	18.6	27.9	37.2	46.5	55.8	65.1	74.4	83.7	93.0	102.3	111.6	9.30
9.35	9.4	18.7	28.1	37.4	46.8	56.1	65.5	74.8	84.2	93.5	102.9	112.2	9.35
9.40	9.4	18.8	28.2	37.6	47.0	56.4	65.8	75.2	84.6	94.0	103.4	112.8	9.40
9.45	9.5	18.9	28.4	37.8	47.3	56.7	66.2	75.6	85.1	94.5	104.0	113.4	9.45
9.50	9.5	19.0	28.5	38.0	47.5	57.0	66.5	76.0	85.5	95.0	104.5	114.0	9.50
9.55	9.6	19.1	28.7	38.2	47.8	57.3	66.9	76.4	86.0	95.5	105.1	114.6	9.55
9.60	9.6	19.2	28.8	38.4	48.0	57.6	67.2	76.8	86.4	96.0	105.6	115.2	9.60
9.65	9.7	19.3	29.0	38.6	48.3	57.9	67.6	77.2	86.9	96.5	106.2	115.8	9.65
9.70	9.7	19.4	29.1	38.8	48.5	58.2	67.9	77.6	87.3	97.0	106.7	116.4	9.70
9.75	9.8	19.5	29.3	39.0	48.8	58.5	68.3	78.0	87.8	97.5	107.3	117.0	9.75
9.80	9.8	19.6	29.4	39.2	49.0	58.8	68.6	78.4	88.2	98.0	107.8	117.6	9.80
9.85	9.9	19.7	29.6	39.4	49.3	59.1	69.0	78.8	88.7	98.5	108.4	118.2	9.85
9.90	9.9	19.8	29.7	39.6	49.5	59.4	69.3	79.2	89.1	99.0	108.9	118.8	9.90
9.95	10.0	19.9	29.9	39.8	49.8	59.7	69.7	79.6	89.6	99.5	109.5	119.4	9.95
10.00	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0	110.0	120.0	10.00
10.05	10.1	20.1	30.2	40.2	50.3	60.3	70.4	80.4	90.5	100.5	110.6	120.6	10.05
10.10	10.1	20.2	30.3	40.4	50.5	60.6	70.7	80.8	90.9	101.0	111.1	121.2	10.10
10.15	10.2	20.3	30.5	40.6	50.8	60.9	71.1	81.2	91.4	101.5	111.7	121.8	10.15
10.20	10.2	20.4	30.6	40.8	51.0	61.2	71.4	81.6	91.8	102.0	112.2	122.4	10.20
10.25	10.3	20.5	30.8	41.0	51.3	61.5	71.8	82.0	92.3	102.5	112.8	123.0	10.25
10.30	10.3	20.6	30.9	41.2	51.5	61.8	72.1	82.4	92.7	103.0	113.3	123.6	10.30
10.35	10.4	20.7	31.1	41.4	51.8	62.1	72.5	82.8	93.2	103.5	113.9	124.2	10.35
10.40	10.4	20.8	31.2	41.6	52.0	62.4	72.8	83.2	93.6	104.0	114.4	124.8	10.40
10.45	10.5	20.9	31.4	41.8	52.3	62.7	73.2	83.6	94.1	104.5	115.0	125.4	10.45
10.50	10.5	21.0	31.5	42.0	52.5	63.0	73.5	84.0	94.5	105.0	115.5	126.0	10.50
10.55	10.6	21.1	31.7	42.2	52.8	63.3	73.9	84.4	95.0	105.5	116.1	126.6	10.55
10.60	10.6	21.2	31.8	42.4	53.0	63.6	74.2	84.8	95.4	106.0	116.6	127.2	10.60
10.65	10.7	21.3	32.0	42.6	53.3	63.9	74.6	85.2	95.9	106.5	117.2	127.8	10.65
10.70	10.7	21.4	32.1	42.8	53.5	64.2	74.9	85.6	96.3	107.0	117.7	128.4	10.70
10.75	10.8	21.5	32.3	43.0	53.8	64.5	75.3	86.0	96.8	107.5	118.3	129.0	10.75
10.80	10.8	21.6	32.4	43.2	54.0	64.8	75.6	86.4	97.2	108.0	118.8	129.6	10.80
10.85	10.9	21.7	32.6	43.4	54.3	65.1	76.0	86.8	97.7	108.5	119.4	130.2	10.85
10.90	10.9	21.8	32.7	43.6	54.5	65.4	76.3	87.2	98.1	109.0	119.9	130.8	10.90
10.95	11.0	21.9	32.9	43.8	54.8	65.7	76.7	87.6	98.6	109.5	120.5	131.4	10.95
11.00	11.0	22.0	33.0	44.0	55.0	66.0	77.0	88.0	99.0	110.0	121.0	132.0	11.00
11.05	11.1	22.1	33.2	44.2	55.3	66.3	77.4	88.4	99.5	110.5	121.6	132.6	11.05
11.10	11.1	22.2	33.3	44.4	55.5	66.6	77.7	88.8	99.9	111.0	122.1	133.2	11.10
11.15	11.2	22.3	33.5	44.6	55.8	66.9	78.1	89.2	100.4	111.5	122.7	133.8	11.15
11.20	11.2	22.4	33.6	44.8	56.0	67.2	78.4	89.6	100.8	112.0	123.2	134.4	11.20
11.25	11.3	22.5	33.8	45.0	56.3	67.5	78.8	90.0	101.3	112.5	123.8	135.0	11.25
11.30	11.3	22.6	33.9	45.2	56.5	67.8	79.1	90.4	101.7	113.0	124.3	135.6	11.30
11.35	11.4	22.7	34.1	45.4	56.8	68.1	79.5	90.8	102.2	113.5	124.9	136.2	11.35
11.40	11.4	22.8	34.2	45.6	57.0	68.4	79.8	91.2	102.6	114.0	125.4	136.8	11.40
11.45	11.5	22.9	34.4	45.8	57.3	68.7	80.2	91.6	103.1	114.5	126.0	137.4	11.45

TABLE 13.

For finding the Sun's change of Right Ascension for any given number of hours.

Hourly variation.	Number of hours. 13	14	15	16	17	18	19	20	21	22	23	24	Hourly variation.
s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.	s.
8.50	110.5	119.0	127.5	136.0	144.5	153.0	161.5	170.0	178.5	187.0	195.5	204.0	8.50
8.55	111.2	119.7	128.3	136.8	145.4	153.9	162.5	171.0	179.6	188.1	196.7	205.2	8.55
8.60	111.8	120.4	129.0	137.6	146.2	154.8	163.4	172.0	180.6	189.2	197.8	206.4	8.60
8.65	112.5	121.1	129.8	138.4	147.1	155.7	164.4	173.0	181.7	190.3	199.0	207.6	8.65
8.70	113.1	121.8	130.5	139.2	147.9	156.6	165.3	174.0	182.7	191.4	200.1	208.8	8.70
8.75	113.8	122.5	131.3	140.0	148.8	157.5	166.3	175.0	183.8	192.5	201.3	210.0	8.75
8.80	114.4	123.2	132.0	140.8	149.6	158.4	167.2	176.0	184.8	193.6	202.4	211.2	8.80
8.85	115.1	123.9	132.8	141.6	150.5	159.3	168.2	177.0	185.9	194.7	203.6	212.4	8.85
8.90	115.7	124.6	133.5	142.4	151.3	160.2	169.1	178.0	186.9	195.8	204.7	213.6	8.90
8.95	116.4	125.3	134.3	143.2	152.2	161.1	170.1	179.0	188.0	196.9	205.9	214.8	8.95
9.00	117.0	126.0	135.0	144.0	153.0	162.0	171.0	180.0	189.0	198.0	207.0	216.0	9.00
9.05	117.7	126.7	135.8	144.8	153.9	162.9	172.0	181.0	190.1	199.1	208.2	217.2	9.05
9.10	118.3	127.4	136.5	145.6	154.7	163.8	172.9	182.0	191.1	200.2	209.3	218.4	9.10
9.15	119.0	128.1	137.3	146.4	155.6	164.7	173.9	183.0	192.2	201.3	210.5	219.6	9.15
9.20	119.6	128.8	138.0	147.2	156.4	165.6	174.8	184.0	193.2	202.4	211.6	220.8	9.20
9.25	120.3	129.5	138.8	148.0	157.3	166.5	175.8	185.0	194.3	203.5	212.8	222.0	9.25
9.30	120.9	130.2	139.5	148.8	158.1	167.4	176.7	186.0	195.3	204.6	213.9	223.2	9.30
9.35	121.6	130.9	140.3	149.6	159.0	168.3	177.7	187.0	196.4	205.7	215.1	224.4	9.35
9.40	122.2	131.6	141.0	150.4	159.8	169.2	178.6	188.0	197.4	206.8	216.2	225.6	9.40
9.45	122.9	132.3	141.8	151.2	160.7	170.1	179.6	189.0	198.5	207.9	217.4	226.8	9.45
9.50	123.5	133.0	142.5	152.0	161.5	171.0	180.5	190.0	199.5	209.0	218.5	228.0	9.50
9.55	124.2	133.7	143.3	152.8	162.4	171.9	181.5	191.0	200.6	210.1	219.7	229.2	9.55
9.60	124.8	134.4	144.0	153.6	163.2	172.8	182.4	192.0	201.6	211.2	220.8	230.4	9.60
9.65	125.5	135.1	144.8	154.4	164.1	173.7	183.4	193.0	202.7	212.3	222.0	231.6	9.65
9.70	126.1	135.8	145.5	155.2	164.9	174.6	184.3	194.0	203.7	213.4	223.1	232.8	9.70
9.75	126.8	136.5	146.3	156.0	165.8	175.5	185.3	195.0	204.8	214.5	224.3	234.0	9.75
9.80	127.4	137.2	147.0	156.8	166.6	176.4	186.2	196.0	205.8	215.6	225.4	235.2	9.80
9.85	128.1	137.9	147.8	157.6	167.5	177.3	187.2	197.0	206.9	216.7	226.6	236.4	9.85
9.90	128.7	138.6	148.5	158.4	168.3	178.2	188.1	198.0	207.9	217.8	227.7	237.6	9.90
9.95	129.4	139.3	149.3	159.2	169.2	179.1	189.1	199.0	209.0	218.9	228.9	238.8	9.95
10.00	130.0	140.0	150.0	160.0	170.0	180.0	190.0	200.0	210.0	220.0	230.0	240.0	10.00
10.05	130.7	140.7	150.8	160.8	170.9	180.9	191.0	201.0	211.1	221.1	231.2	241.2	10.05
10.10	131.3	141.4	151.5	161.6	171.7	181.8	191.9	202.0	212.1	222.2	232.3	242.4	10.10
10.15	132.0	142.1	152.3	162.4	172.6	182.7	192.9	203.0	213.2	223.3	233.5	243.6	10.15
10.20	132.6	142.8	153.0	163.2	173.4	183.6	193.8	204.0	214.2	224.4	234.6	244.8	10.20
10.25	133.3	143.5	153.8	164.0	174.3	184.5	194.8	205.0	215.3	225.5	235.8	246.0	10.25
10.30	133.9	144.2	154.5	164.8	175.1	185.4	195.7	206.0	216.3	226.6	236.9	247.2	10.30
10.35	134.6	144.9	155.3	165.6	176.0	186.3	196.7	207.0	217.4	227.7	238.1	248.4	10.35
10.40	135.2	145.6	156.0	166.4	176.8	187.2	197.6	208.0	218.4	228.8	239.2	249.6	10.40
10.45	135.9	146.3	156.8	167.2	177.7	188.1	198.6	209.0	219.5	229.9	240.4	250.8	10.45
10.50	136.5	147.0	157.5	168.0	178.5	189.0	199.5	210.0	220.5	231.0	241.5	252.0	10.50
10.55	137.2	147.7	158.3	168.8	179.4	189.9	200.5	211.0	221.6	232.1	242.7	253.2	10.55
10.60	137.8	148.4	159.0	169.6	180.2	190.8	201.4	212.0	222.6	233.2	243.8	254.4	10.60
10.65	138.5	149.1	159.8	170.4	181.1	191.7	202.4	213.0	223.7	234.3	245.0	255.6	10.65
10.70	139.1	149.8	160.5	171.2	181.9	192.6	203.3	214.0	224.7	235.4	246.1	256.8	10.70
10.75	139.8	150.5	161.3	172.0	182.8	193.5	204.3	215.0	225.8	236.5	247.3	258.0	10.75
10.80	140.4	151.2	162.0	172.8	183.6	194.4	205.2	216.0	226.8	237.6	248.4	259.2	10.80
10.85	141.1	151.9	162.8	173.6	184.5	195.3	206.2	217.0	227.9	238.7	249.6	260.4	10.85
10.90	141.7	152.6	163.5	174.4	185.3	196.2	207.1	218.0	228.9	239.8	250.7	261.6	10.90
10.95	142.4	153.3	164.3	175.2	186.2	197.1	208.1	219.0	230.0	240.9	251.9	262.8	10.95
11.00	143.0	154.0	165.0	176.0	187.0	198.0	209.0	220.0	231.0	242.0	253.0	264.0	11.00
11.05	143.7	154.7	165.8	176.8	187.9	198.9	210.0	221.0	232.1	243.1	254.2	265.2	11.05
11.10	144.3	155.4	166.5	177.6	188.7	199.8	210.9	222.0	233.1	244.2	255.3	266.4	11.10
11.15	145.0	156.1	167.3	178.4	189.6	200.7	211.9	223.0	234.2	245.3	256.5	267.6	11.15
11.20	145.6	156.8	168.0	179.2	190.4	201.6	212.8	224.0	235.2	246.4	257.6	268.8	11.20
11.25	146.3	157.5	168.8	180.0	191.3	202.5	213.8	225.0	236.3	247.5	258.8	270.0	11.25
11.30	146.9	158.2	169.5	180.8	192.1	203.4	214.7	226.0	237.3	248.6	259.9	271.2	11.30
11.35	147.6	158.9	170.3	181.6	193.0	204.3	215.7	227.0	238.4	249.7	261.1	272.4	11.35
11.40	148.2	159.6	171.0	182.4	193.8	205.2	216.6	228.0	239.4	250.8	262.2	273.6	11.40
11.45	148.9	160.3	171.8	183.2	194.7	206.1	217.6	229.0	240.5	251.9	263.4	274.8	11.45

TABLES 14, 15, 16.

TABLE 14.

Dip of the Sea Horizon.

Height of the Eye.	Dip of the Horizon.
Feet.	′ ″
1	0 59
2	1 23
3	1 42
4	1 58
5	2 11
6	2 24
7	2 36
8	2 46
9	2 56
10	3 06
11	3 15
12	3 24
13	3 32
14	3 40
15	3 48
16	3 55
17	4 02
18	4 09
19	4 16
20	4 23
21	4 29
22	4 36
23	4 42
24	4 48
25	4 54
26	5 00
27	5 06
28	5 11
29	5 17
30	5 22
31	5 27
32	5 33
33	5 38
34	5 43
35	5 48
36	5 53
37	5 58
38	6 02
39	6 07
40	6 12
45	6 36
50	6 56
55	7 16
60	7 35
65	7 54
70	8 12
75	8 29
80	8 46
85	9 02
90	9 18
95	9 33
100	9 48

TABLE 15.

Dip of the Sea at different Distances from the Observer.

Dist. of Land in Sea Miles.	Height of the Eye above the Sea in Feet.							
	5	10	15	20	25	30	35	40
	′	′	′	′	′	′	′	′
¼	11	23	34	45	57	68	79	91
½	6	12	17	23	28	34	40	45
¾	4	8	12	15	19	23	27	30
1	3	6	9	12	15	17	20	23
1¼	3	5	7	10	12	14	16	19
1½	3	4	6	8	10	12	14	16
2	2	4	5	7	8	9	11	12
2½	2	3	4	6	7	8	9	10
3	2	3	4	5	6	7	8	9
3½	2	3	4	5	6	6	7	8
4	2	3	4	5	5	6	7	7
5	2	3	4	4	5	6	6	7
6	2	3	4	4	5	5	6	6

Note to Table 15.—The numbers of this Table below the black lines are the same as are given in Table 14, the visible horizon corresponding to those heights not being so far distant as the land.

TABLE 16.

The Sun's Parallax in Altitude.

Altitude.	Parallax.
°	″
0	9
10	9
20	8
30	8
40	7
50	6
55	5
60	4
65	4
70	3
75	2
80	2
85	1
90	0

TABLE 17.

Parallax in Altitude of a Planet.

Horizontal parallax of planet. / Altitude.	0°	10	20	30	35	40	43	46	49	52	55	58	61	64	67	70	72	74	76	78	80	82	84	86	88	90
35″	35	35	33	30	29	27	26	24	23	22	20	19	17	15	14	12	11	10	8	7	6	5	4	2	1	0
30″	30	30	28	26	25	23	22	21	20	18	17	16	15	13	12	10	9	8	7	6	5	4	3	2	1	0
28″	28	28	26	24	23	21	20	19	18	17	16	15	14	12	11	10	9	8	7	6	5	4	3	2	1	0
27″	27	27	25	23	22	21	20	19	18	17	15	14	13	12	11	9	8	7	7	6	5	4	3	2	1	0
26″	26	26	24	23	21	20	19	18	17	16	15	14	13	11	10	9	8	7	6	5	5	4	3	2	1	0
25″	25	25	23	22	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	3	2	1	0
24″	24	24	23	21	20	18	18	17	16	15	14	13	12	11	9	8	7	7	6	5	4	3	3	2	1	0
23″	23	23	22	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	6	5	4	3	2	2	1	0
22″	22	22	21	19	18	17	16	15	14	14	13	12	11	10	9	8	7	6	5	5	4	3	2	2	1	0
21″	21	21	20	18	17	16	15	15	14	13	12	11	10	9	8	7	6	6	5	4	4	3	2	1	1	0
20″	20	20	19	17	16	15	15	14	13	12	11	11	10	9	8	7	6	6	5	4	3	3	2	1	1	0
19″	19	19	18	16	16	15	14	13	12	12	11	10	9	8	7	6	6	5	5	4	3	3	2	1	1	0
18″	18	18	17	16	15	14	13	13	12	11	10	10	9	8	7	6	6	5	4	4	3	3	2	1	1	0
17″	17	17	16	15	14	13	12	12	11	10	10	9	8	7	7	6	5	5	4	4	3	2	2	1	1	0
16″	16	16	15	14	13	12	12	11	10	10	9	8	8	7	6	5	5	4	4	3	3	2	2	1	1	0
15″	15	15	14	13	12	11	11	10	10	9	9	8	7	7	6	5	5	4	4	3	3	2	2	1	1	0
14″	14	14	13	12	11	11	10	10	9	9	8	7	7	6	5	5	4	4	3	3	2	2	1	1	0	0
13″	13	13	12	11	11	10	10	9	9	8	7	7	6	6	5	4	4	4	3	3	2	2	1	1	0	0
12″	12	12	11	10	10	9	9	8	8	7	7	6	6	5	5	4	4	3	3	2	2	2	1	1	0	0
11″	11	11	10	10	9	8	8	8	7	7	6	6	5	5	4	4	3	3	3	2	2	2	1	1	0	0
10″	10	10	9	9	8	8	7	7	7	6	6	5	5	4	4	3	3	3	2	2	2	1	1	1	0	0
9″	9	9	8	8	7	7	7	6	6	6	5	5	4	4	4	3	3	2	2	2	2	1	1	1	0	0
8″	8	8	8	7	7	6	6	6	5	5	5	4	4	4	3	3	2	2	2	2	1	1	1	1	0	0
7″	7	7	7	6	6	5	5	5	5	4	4	4	3	3	3	2	2	2	2	1	1	1	1	0	0	0
6″	6	6	6	5	5	5	4	4	4	4	3	3	3	3	2	2	2	2	1	1	1	1	1	0	0	0
5″	5	5	5	4	4	4	4	3	3	3	3	3	2	2	2	2	2	1	1	1	1	1	1	0	0	0
4″	4	4	4	3	3	3	3	3	3	2	2	2	2	2	2	1	1	1	1	1	1	1	0	0	0	0
3″	3	3	3	3	2	2	2	2	2	2	2	2	1	1	1	1	1	1	1	1	1	0	0	0	0	0
2″	2	2	2	2	2	2	1	1	1	1	1	1	1	1	1	1	1	1	0	0	0	0	0	0	0	0
1″	1	1	1	1	1	1	1	1	1	1	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Altitude.	0°	10	20	30	35	40	43	46	49	52	55	58	61	64	67	70	72	74	76	78	80	82	84	86	88	90

TABLE 18.

Augmentation of the Moon's Semidiameter.

Apparent altitude of ☽.	☽'s Semidiameter. 14′ 30″	15′ 0″	15′ 30″	16′ 0″	16′ 30″	17′ 0″
°	″	″	″	″	″	″
0	0.1	0.1	0.1	0.1	0.2	0.2
2	0.6	0.6	0.7	0.7	0.8	0.8
4	1.0	1.1	1.2	1.3	1.4	1.5
6	1.5	1.6	1.7	1.9	2.0	2.1
8	2.0	2.1	2.3	2.4	2.6	2.7
10	2.4	2.6	2.8	3.0	3.2	3.4
12	2.9	3.1	3.3	3.6	3.8	4.0
14	3.4	3.6	3.9	4.1	4.4	4.7
16	3.8	4.1	4.4	4.7	5.0	5.3
18	4.3	4.6	4.9	5.2	5.6	5.9
20	4.7	5.1	5.4	5.8	6.1	6.5
22	5.2	5.5	5.9	6.3	6.7	7.1
24	5.6	6.0	6.4	6.8	7.3	7.7
26	6.0	6.5	6.9	7.4	7.8	8.3
28	6.5	6.9	7.4	7.9	8.4	8.9
30	6.9	7.3	7.9	8.4	8.9	9.5
32	7.3	7.8	8.3	8.9	9.4	10.0
34	7.7	8.2	8.8	9.4	10.0	10.6
36	8.1	8.6	9.2	9.8	10.5	11.1
38	8.4	9.0	9.7	10.3	10.9	11.6
40	8.8	9.4	10.1	10.7	11.4	12.1
42	9.2	9.8	10.5	11.2	11.9	12.6
44	9.5	10.2	10.9	11.6	12.3	13.1
46	9.8	10.5	11.3	12.0	12.8	13.6
48	10.2	10.9	11.6	12.4	13.2	14.0
50	10.5	11.2	12.0	12.8	13.6	14.4
52	10.8	11.5	12.3	13.1	14.0	14.9
54	11.1	11.8	12.7	13.5	14.4	15.3
56	11.3	12.1	13.0	13.8	14.7	15.6
58	11.6	12.4	13.3	14.1	15.1	16.0
60	11.8	12.7	13.5	14.4	15.4	16.3
62	12.1	12.9	13.8	14.7	15.7	16.6
64	12.3	13.2	14.1	15.0	16.0	16.9
66	12.5	13.4	14.3	15.2	16.2	17.2
68	12.7	13.6	14.5	15.5	16.5	17.5
70	12.9	13.8	14.7	15.7	16.7	17.7
72	13.0	13.9	14.9	15.9	16.9	17.9
74	13.1	14.1	15.0	16.0	17.1	18.1
76	13.3	14.2	15.2	16.2	17.2	18.3
78	13.4	14.3	15.3	16.3	17.4	18.4
80	13.5	14.4	15.4	16.4	17.5	18.6
82	13.5	14.5	15.5	16.5	17.6	18.7
84	13.6	14.6	15.6	16.6	17.6	18.7
86	13.6	14.6	15.6	16.6	17.7	18.8
88	13.7	14.6	15.6	16.7	17.7	18.8
90	13.7	14.6	15.6	16.7	17.7	18.8

TABLE 19.

Augmentation of the Moon's Horizontal Parallax.

Latitude of observation.	☽'s Hor. Parallax. 53′	57′	61′
°	″	″	″
0	0.0	0.0	0.0
2	0.0	0.0	0.0
4	0.1	0.1	0.1
6	0.1	0.1	0.1
8	0.2	0.2	0.2
10	0.3	0.3	0.4
12	0.5	0.5	0.5
14	0.6	0.7	0.7
16	0.8	0.9	0.9
18	1.0	1.1	1.1
20	1.2	1.3	1.4
22	1.5	1.6	1.7
24	1.7	1.9	2.0
26	2.0	2.2	2.3
28	2.3	2.5	2.6
30	2.6	2.8	3.0
32	2.9	3.1	3.4
34	3.3	3.5	3.8
36	3.6	3.9	4.1
38	4.0	4.3	4.6
40	4.3	4.6	5.0
42	4.7	5.0	5.4
44	5.0	5.4	5.8
46	5.4	5.8	6.2
48	5.8	6.2	6.6
50	6.1	6.6	7.1
52	6.5	7.0	7.5
54	6.8	7.4	7.9
56	7.2	7.7	8.3
58	7.5	8.1	8.6
60	7.8	8.4	9.0
62	8.1	8.8	9.4
64	8.4	9.1	9.7
66	8.7	9.4	10.0
68	9.0	9.7	10.3
70	9.2	9.9	10.6
72	9.5	10.2	10.9
74	9.7	10.4	11.1
76	9.8	10.6	11.3
78	10.0	10.8	11.5
80	10.1	10.9	11.7
82	10.3	11.0	11.8
84	10.3	11.1	11.9
86	10.4	11.2	12.0
88	10.4	11.2	12.0
90	10.5	11.3	12.0

TABLE 20A.

Mean Refraction.

[Barometer, 30 inches. Fahrenheit's Thermometer, 50°.]

Apparent Altitude.	Mean Refraction.	Apparent Altitude.	Mean Refraction.	Apparent Altitude.	Mean Refraction.	Apparent Altitude.	Mean Refraction.	Apparent Altitude.	Mean Refraction.
° ′	′ ″	° ′	′ ″	° ′	′ ″	° ′	′ ″	° ′	′ ″
		9 30	5 35.1	15 00	3 34.1	25 00	2 4.4	42 00	1 04.7
0 00	36 29.4	35	5 32.4	10	3 31.7	10	2 3.4	20	1 03.9
1 00	24 53.6	40	5 29.6	20	3 29.4	20	2 2.5	40	1 03.2
2 00	18 25.5	45	5 27.0	30	3 27.1	30	2 1.6	43 00	1 02.4
3 00	14 25.1	50	5 24.3	40	3 24.8	40	2 0.7	20	1 01.7
4 00	11 44.4	55	5 21.7	50	3 22.6	50	1 59.8	40	1 01.0
5 00	9 52.0	10 00	5 19.2	16 00	3 20.5	26 00	1 58.9	44 00	1 00.3
05	9 44.0	05	5 16.7	10	3 18.4	10	1 58.1	20	0 59.6
10	9 36.2	10	5 14.2	20	3 16.3	20	1 57.2	40	0 58.9
15	9 28.6	15	5 11.7	30	3 14.2	30	1 56.4	45 00	0 58.2
20	9 21.2	20	5 9.3	40	3 12.2	40	1 55.5	20	0 57.6
25	9 14.0	25	5 6.9	50	3 10.3	50	1 54.7	40	0 56.9
5 30	9 7.0	10 30	5 4.6	17 00	3 8.3	27 00	1 53.9	46 00	0 56.2
35	9 0.1	35	5 2.3	10	3 6.4	10	1 53.1	20	0 55.6
40	8 53.4	40	5 0.0	20	3 4.6	20	1 52.3	40	0 55.0
45	8 46.8	45	4 57.8	30	3 2.8	30	1 51.5	47 00	0 54.3
50	8 40.4	50	4 55.6	40	3 1.0	40	1 50.7	20	0 53.7
55	8 34.2	55	4 53.4	50	2 59.2	50	1 50.0	40	0 53.1
6 00	8 28.0	11 00	4 51.2	18 00	2 57.5	28 00	1 49.2	48 00	0 52.5
05	8 22.1	05	4 49.1	10	2 55.8	20	1 47.7	49 00	0 50.6
10	8 16.2	10	4 47.0	20	2 54.1	40	1 46.2	50 00	0 48.9
15	8 10.5	15	4 44.9	30	2 52.4	29 00	1 44.8	51 00	0 47.2
20	8 4.8	20	4 42.9	40	2 50.8	20	1 43.4	52 00	0 45.5
25	7 59.3	25	4 40.9	50	2 49.2	40	1 42.0	53 00	0 43.9
6 30	7 53.9	11 30	4 38.9	19 00	2 47.7	30 00	1 40.6	54 00	0 42.3
35	7 48.7	35	4 36.9	10	2 46.1	20	1 39.3	55 00	0 40.8
40	7 43.5	40	4 35.0	20	2 44.6	40	1 38.0	56 00	0 39.3
45	7 38.4	45	4 33.1	30	2 43.1	31 00	1 36.7	57 00	0 37.8
50	7 33.5	50	4 31.2	40	2 41.6	20	1 35.5	58 00	0 36.4
55	7 28.6	55	4 29.4	50	2 40.2	40	1 34.2	59 00	0 35.0
7 00	7 23.8	12 00	4 27.5	20 00	2 38.8	32 00	1 33.0	60 00	0 33.6
05	7 19.2	05	4 25.7	10	2 37.4	20	1 31.8	61 00	0 32.3
10	7 14.6	10	4 23.9	20	2 36.0	40	1 30.7	62 00	0 31.0
15	7 10.1	15	4 22.2	30	2 34.6	33 00	1 29.5	63 00	0 29.7
20	7 5.7	20	4 20.4	40	2 33.3	20	1 28.4	64 00	0 28.4
25	7 1.4	25	4 18.7	50	2 32.0	40	1 27.3	65 00	0 27.2
7 30	6 57.1	12 30	4 17.0	21 00	2 30.7	34 00	1 26.2	66 00	0 25.9
35	6 53.0	35	4 15.3	10	2 29.4	20	1 25.1	67 00	0 24.7
40	6 48.9	40	4 13.6	20	2 28.1	40	1 24.1	68 00	0 23.6
45	6 44.9	45	4 12.0	30	2 26.9	35 00	1 23.1	69 00	0 22.4
50	6 41.0	50	4 10.4	40	2 25.7	20	1 22.0	70 00	0 21.2
55	6 37.1	55	4 8.8	50	2 24.5	40	1 21.0	71 00	0 20.1
8 00	6 33.3	13 00	4 7.2	22 00	2 23.3	36 00	1 20.1	72 00	0 18.9
05	6 29.6	05	4 5.6	10	2 22.1	20	1 19.1	73 00	0 17.8
10	6 25.9	10	4 4.1	20	2 20.9	40	1 18.2	74 00	0 16.7
15	6 22.3	15	4 2.6	30	2 19.8	37 00	1 17.2	75 00	0 15.6
20	6 18.8	20	4 1.0	40	2 18.7	20	1 16.3	76 00	0 14.5
25	6 15.3	25	3 59.6	50	2 17.5	40	1 15.4	77 00	0 13.5
8 30	6 11.9	13 30	3 58.1	23 00	2 16.4	38 00	1 14.5	78 00	0 12.4
35	6 8.5	35	3 56.6	10	2 15.4	20	1 13.6	79 00	0 11.3
40	6 5.2	40	3 55.2	20	2 14.3	40	1 12.7	80 00	0 10.3
45	6 2.0	45	3 53.7	30	2 13.3	39 00	1 11.9	81 00	0 9.2
50	5 58.8	50	3 52.3	40	2 12.2	20	1 11.0	82 00	0 8.2
55	5 55.7	55	3 50.9	50	2 11.2	40	1 10.2	83 00	0 7.2
9 00	5 52.6	14 00	3 49.5	24 00	2 10.2	40 00	1 9.4	84 00	0 6.1
05	5 49.6	10	3 46.8	10	2 9.2	20	1 8.6	85 00	0 5.1
10	5 46.6	20	3 44.2	20	2 8.2	40	1 7.8	86 00	0 4.1
15	5 43.6	30	3 41.6	30	2 7.2	41 00	1 7.0	87 00	0 3.1
20	5 40.7	40	3 39.0	40	2 6.2	20	1 6.2	88 00	0 2.0
25	5 37.9	50	3 36.5	50	2 5.3	40	1 5.4	89 00	0 1.0
9 30	5 35.1	15 00	3 34.1	25 00	2 4.4	42 00	1 4.7	90 00	0 0.0

TABLE 20B.

Correction of the Sun's Apparent Altitude for Refraction and Parallax.

[Barometer, 30 inches. Fahrenheit's Thermometer, 50°.]

Apparent Altitude.	Mean Refraction and Parallax ☉.	Apparent Altitude.	Mean Refraction and Parallax ☉.	Apparent Altitude.	Mean Refraction and Parallax ☉.	Apparent Altitude.	Mean Refraction and Parallax ☉.	Apparent Altitude.	Mean Refraction and Parallax ☉.
° ′	′ ″	° ′	′ ″	° ′	′ ″	° ′	′ ″	° ′	′ ″
		9 30	5 26	15 00	3 25	25 00	1 56	42 00	0 58
0 00	36 20	35	5 23	10	3 24	10	1 55	20	0 57
1 00	24 45	40	5 21	20	3 21	20	1 55	40	0 56
2 00	18 17	45	5 18	30	3 19	30	1 54	43 00	0 55
3 00	14 16	50	5 15	40	3 17	40	1 53	20	0 55
4 00	11 35	55	5 13	50	3 15	50	1 52	40	0 54
5 00	9 43	10 00	5 10	16 00	3 13	26 00	1 51	44 00	0 53
05	9 35	05	5 8	10	3 10	10	1 50	20	0 53
10	9 27	10	5 5	20	3 8	20	1 49	40	0 52
15	9 20	15	5 3	30	3 6	30	1 48	45 00	0 52
20	9 12	20	5 0	40	3 4	40	1 48	20	0 52
25	9 5	25	4 58	50	3 2	50	1 47	40	0 51
5 30	8 58	10 30	4 56	17 00	3 0	27 00	1 46	46 00	0 50
35	8 51	35	4 53	10	2 58	10	1 45	20	0 50
40	8 44	40	4 51	20	2 57	20	1 44	40	0 49
45	8 38	45	4 49	30	2 55	30	1 44	47 00	0 48
50	8 31	50	4 47	40	2 53	40	1 43	20	0 48
55	8 25	55	4 44	50	2 51	50	1 42	40	0 47
6 00	8 19	11 00	4 42	18 00	2 50	28 00	1 41	48 00	0 47
05	8 13	05	4 40	10	2 48	20	1 40	49 00	0 45
10	8 7	10	4 38	20	2 46	40	1 38	50 00	0 43
15	8 2	15	4 36	30	2 44	29 00	1 37	51 00	0 41
20	7 56	20	4 34	40	2 43	20	1 35	52 00	0 40
25	7 50	25	4 32	50	2 41	40	1 34	53 00	0 39
6 30	7 45	11 30	4 30	19 00	2 40	30 00	1 33	54 00	0 37
35	7 40	35	4 28	10	2 38	20	1 31	55 00	0 36
40	7 35	40	4 26	20	2 37	40	1 30	56 00	0 34
45	7 29	45	4 24	30	2 35	31 00	1 29	57 00	0 33
50	7 25	50	4 22	40	2 34	20	1 28	58 00	0 32
55	7 20	55	4 20	50	2 32	40	1 26	59 00	0 31
7 00	7 15	12 00	4 19	20 00	2 31	32 00	1 25	60 00	0 30
05	7 10	05	4 17	10	2 29	20	1 24	61 00	0 28
10	7 6	10	4 15	20	2 28	40	1 23	62 00	0 27
15	7 1	15	4 13	30	2 27	33 00	1 22	63 00	0 26
20	6 57	20	4 11	40	2 25	20	1 20	64 00	0 24
25	6 52	25	4 10	50	2 24	40	1 19	65 00	0 23
7 30	6 48	12 30	4 8	21 00	2 23	34 00	1 18	66 00	0 22
35	6 44	35	4 6	10	2 21	20	1 17	67 00	0 21
40	6 40	40	4 5	20	2 20	40	1 16	68 00	0 21
45	6 36	45	4 3	30	2 19	35 00	1 15	69 00	0 19
50	6 32	50	4 1	40	2 18	20	1 15	70 00	0 18
55	6 28	55	4 0	50	2 17	40	1 14	71 00	0 17
8 00	6 24	13 00	3 58	22 00	2 15	36 00	1 13	72 00	0 16
05	6 21	05	3 57	10	2 14	20	1 12	73 00	0 16
10	6 17	10	3 55	20	2 13	40	1 11	74 00	0 15
15	6 13	15	3 54	30	2 12	37 00	1 10	75 00	0 14
20	6 10	20	3 52	40	2 11	20	1 9	76 00	0 13
25	6 6	25	3 51	50	2 10	40	1 8	77 00	0 12
8 30	6 3	13 30	3 49	23 00	2 8	38 00	1 8	78 00	0 10
35	6 0	35	3 48	10	2 7	20	1 7	79 00	0 9
40	5 56	40	3 46	20	2 6	40	1 6	80 00	0 8
45	5 53	45	3 45	30	2 5	39 00	1 5	81 00	0 7
50	5 50	50	3 43	40	2 4	20	1 4	82 00	0 6
55	5 47	55	3 42	50	2 3	40	1 3	83 00	0 6
9 00	5 44	14 00	3 41	24 00	2 2	40 00	1 2	84 00	0 5
05	5 41	10	3 38	10	2 1	20	1 2	85 00	0 4
10	5 38	20	3 35	20	2 0	40	1 1	86 00	0 3
15	5 35	30	3 33	30	1 59	41 00	1 0	87 00	0 2
20	5 32	40	3 30	40	1 58	20	0 59	88 00	0 2
25	5 29	50	3 28	50	1 57	40	0 58	89 00	0 1
9 30	5 26	15 00	3 25	25 00	1 56	42 00	0 58	90 00	0 0

TABLE 21.

Correction of the Mean Refraction for the Height of the Barometer.

Barom.	Mean refraction.																					Barom.
Subtract.	0′		1′		2′		3′		4′		5′		6′		7′		8′		9′		10′	Add.
	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	
	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	
27.50	0	2	5	7	10	12	15	17	20	23	25	28	30	33	35	38	40	43	45	48	51	
27.55	0	2	5	7	10	12	15	17	20	22	25	27	30	32	35	37	40	42	45	47	50	
27.60	0	2	5	7	10	12	14	17	19	22	24	27	29	31	34	36	39	41	44	46	49	
27.65	0	2	5	7	9	12	14	16	19	21	24	26	28	31	33	36	38	40	43	45	48	
27.70	0	2	5	7	9	11	14	16	18	21	23	25	28	30	32	35	37	39	42	44	47	
27.75	0	2	4	7	9	11	13	16	18	20	23	25	27	29	32	34	36	39	41	43	46	
27.80	0	2	4	7	9	11	13	15	18	20	22	24	27	29	31	33	35	38	40	42	45	
27.85	0	2	4	6	9	11	13	15	17	19	22	24	26	28	30	32	35	37	39	41	44	
27.90	0	2	4	6	8	10	13	15	17	19	21	23	25	27	30	32	34	36	38	40	43	
27.95	0	2	4	6	8	10	12	14	16	18	21	23	25	27	29	31	33	35	37	39	42	
28.00	0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	41	
28.05	0	2	4	6	8	10	12	14	16	18	20	22	24	25	27	29	31	33	35	37	39	
28.10	0	2	4	6	8	9	11	13	15	17	19	21	23	25	27	29	31	33	34	36	38	
28.15	0	2	4	6	7	9	11	13	15	17	19	20	22	24	26	28	30	32	34	36	37	
28.20	0	2	4	5	7	9	11	13	14	16	18	20	22	24	25	27	29	31	33	35	36	
28.25	0	2	3	5	7	9	10	12	14	16	18	19	21	23	25	26	28	30	32	34	35	
28.30	0	2	3	5	7	8	10	12	14	15	17	19	21	22	24	26	27	29	31	33	34	
28.35	0	2	3	5	7	8	10	12	13	15	17	18	20	22	23	25	27	28	30	32	33	
28.40	0	2	3	5	6	8	10	11	13	14	16	18	19	21	23	24	26	27	29	31	32	
28.45	0	2	3	5	6	8	9	11	12	14	16	17	19	20	22	23	25	27	28	30	31	
28.50	0	1	3	4	6	7	9	10	12	14	15	17	18	20	21	23	24	26	27	29	30	31.50
28.55	0	1	3	4	6	7	9	10	12	13	15	16	17	19	20	22	23	25	26	28	29	31.45
28.60	0	1	3	4	6	7	8	10	11	13	14	15	17	18	20	21	23	24	25	27	28	31.40
28.65	0	1	3	4	5	7	8	9	11	12	14	15	16	18	19	20	22	23	25	26	27	31.35
28.70	0	1	3	4	5	6	8	9	10	12	13	14	16	17	18	20	21	22	24	25	26	31.30
28.75	0	1	2	4	5	6	7	9	10	11	13	14	15	16	18	19	20	21	23	24	25	31.25
28.80	0	1	2	4	5	6	7	8	10	11	12	13	14	16	17	18	19	21	22	23	24	31.20
28.85	0	1	2	3	5	6	7	8	9	10	12	13	14	15	16	17	19	20	21	22	23	31.15
28.90	0	1	2	3	4	5	7	8	9	10	11	12	13	14	16	17	18	19	20	21	22	31.10
28.95	0	1	2	3	4	5	6	7	8	9	11	12	13	14	15	16	17	18	19	20	21	31.05
29.00	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	31.00
29.05	0	1	2	3	4	5	6	7	8	9	10	11	11	12	13	14	15	16	17	18	19	30.95
29.10	0	1	2	3	4	4	5	6	7	8	9	10	11	12	13	14	15	15	16	17	18	30.90
29.15	0	1	2	3	3	4	5	6	7	8	9	9	10	11	12	13	14	15	15	16	17	30.85
29.20	0	1	2	2	3	4	5	6	6	7	8	9	10	10	11	12	13	14	15	15	16	30.80
29.25	0	1	1	2	3	4	4	5	6	7	8	8	9	10	11	11	12	13	14	14	15	30.75
29.30	0	1	1	2	3	3	4	5	6	6	7	8	8	9	10	11	11	12	13	13	14	30.70
29.35	0	1	1	2	3	3	4	5	5	6	7	7	8	9	9	10	10	11	12	13	13	30.65
29.40	0	1	1	2	2	3	4	4	5	5	6	7	7	8	8	9	10	10	11	12	12	30.60
29.45	0	1	1	2	2	3	3	4	4	5	6	6	7	7	8	8	9	9	10	11	11	30.55
29.50	0	0	1	1	2	2	3	3	4	5	5	6	6	7	7	8	8	9	9	10	10	30.50
29.55	0	0	1	1	2	2	3	3	4	4	5	5	5	6	6	7	7	8	8	9	9	30.45
29.60	0	0	1	1	2	2	2	3	3	4	4	4	5	5	6	6	6	7	7	8	8	30.40
29.65	0	0	1	1	1	2	2	2	3	3	4	4	4	5	5	5	6	6	6	7	7	30.35
29.70	0	0	1	1	1	1	2	2	2	3	3	3	4	4	4	5	5	5	5	6	6	30.30
29.75	0	0	0	1	1	1	1	2	2	2	3	3	3	3	4	4	4	4	5	5	5	30.25
29.80	0	0	0	1	1	1	1	1	2	2	2	2	2	3	3	3	3	3	4	4	4	30.20
29.85	0	0	0	0	1	1	1	1	1	1	2	2	2	2	2	2	2	3	3	3	3	30.15
29.90	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	2	2	2	2	2	2	30.10
29.95	0	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	30.05
30.00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30.00
Subtract.	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	Add.
	0′		1′		2′		3′		4′		5′		6′		7′		8′		9′		10′	
Barom.	Mean refraction.																					Barom.

TABLE 22.

Correction of the Mean Refraction for the Height of the Thermometer.

Ther.	Mean refraction.																					Ther.
	0′		1′		2′		3′		4′		5′		6′		7′		8′		9′		10′	
Add.	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0′	30″	0″	30″	0″	30″	0″	30″	0″	Add.
°	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	°
—10	0	4	8	12	16	20	24	28	33	37	41	46	50	55	60	65	70	75	80	85	90	—10
— 8	0	4	8	12	15	19	23	27	31	36	40	44	48	53	58	62	67	72	77	82	87	— 8
— 6	0	4	7	11	15	19	22	26	30	34	38	42	47	51	55	60	64	69	74	79	84	— 6
— 4	0	4	7	11	14	18	22	25	29	33	37	41	45	49	53	57	62	66	71	76	80	— 4
— 2	0	3	7	10	14	17	21	24	28	31	35	39	43	47	51	55	59	64	68	72	77	— 2
0	0	3	7	10	13	16	20	23	27	30	34	37	41	45	49	53	57	61	65	69	74	0
2	0	3	6	9	12	16	19	22	25	29	32	36	39	43	47	50	54	58	62	66	70	2
4	0	3	6	9	12	15	18	21	24	28	31	34	37	41	44	48	52	55	59	63	67	4
6	0	3	6	8	11	14	17	20	23	26	29	32	36	39	42	46	49	53	56	60	64	6
8	0	3	5	8	11	14	16	19	22	25	28	31	34	37	40	43	47	50	54	57	61	8
10	0	3	5	8	10	13	15	18	21	24	26	29	32	35	38	41	44	48	51	54	58	10
11	0	2	5	7	10	13	15	18	20	23	26	28	31	34	37	40	43	46	49	53	56	11
12	0	2	5	7	10	12	15	17	20	22	25	28	30	33	36	39	42	45	48	51	54	12
13	0	2	5	7	9	12	14	17	19	22	24	27	30	32	35	38	41	44	47	50	53	13
14	0	2	5	7	9	11	14	16	19	21	24	26	29	31	34	37	40	42	45	48	51	14
15	0	2	4	7	9	11	13	16	18	20	23	25	28	30	33	36	38	41	44	47	50	15
16	0	2	4	6	9	11	13	15	18	20	22	25	27	29	32	35	37	40	43	45	48	16
17	0	2	4	6	8	10	13	15	17	19	21	24	26	29	31	33	36	39	41	44	47	17
18	0	2	4	6	8	10	12	14	16	19	21	23	25	28	30	32	35	37	40	43	45	18
19	0	2	4	6	8	10	12	14	16	18	20	22	24	27	29	31	34	36	39	41	44	19
20	0	2	4	6	8	9	11	13	15	17	19	22	24	26	28	30	33	35	37	40	42	20
21	0	2	4	5	7	9	11	13	15	17	19	21	23	25	27	29	31	34	36	38	41	21
22	0	2	3	5	7	9	11	12	14	16	18	20	22	24	26	28	30	32	35	37	39	22
23	0	2	3	5	7	8	10	12	14	15	17	19	21	23	25	27	29	31	33	36	38	23
24	0	2	3	5	6	8	10	11	13	15	17	18	20	22	24	26	28	30	32	34	36	24
25	0	2	3	5	6	8	9	11	13	14	16	18	19	21	23	25	27	29	31	33	35	25
26	0	1	3	4	6	7	9	11	12	14	15	17	19	20	22	24	26	28	29	31	33	26
27	0	1	3	4	6	7	9	10	12	13	15	16	18	19	21	23	25	26	28	30	32	27
28	0	1	3	4	5	7	8	10	11	12	14	15	17	19	20	22	23	25	27	29	30	28
29	0	1	3	4	5	6	8	9	11	12	13	15	16	18	19	21	22	24	26	27	29	29
30	0	1	2	4	5	6	7	9	10	11	13	14	15	17	18	20	21	23	24	26	28	30
31	0	1	2	3	5	6	7	8	9	11	12	13	15	16	17	19	20	22	23	25	26	31
32	0	1	2	3	4	6	7	8	9	10	11	13	14	15	16	18	19	20	22	23	25	32
33	0	1	2	3	4	5	6	7	8	10	11	12	13	14	15	17	18	19	21	22	23	33
34	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	16	17	18	19	21	22	34
35	0	1	2	3	4	5	6	6	7	8	9	10	11	13	14	15	16	17	18	19	20	35
36	0	1	2	3	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	36
37	0	1	2	2	3	4	5	6	6	7	8	9	10	11	12	13	14	15	16	17	18	37
38	0	1	1	2	3	4	4	5	6	7	7	8	9	10	11	12	13	13	14	15	16	38
39	0	1	1	2	3	3	4	5	5	6	7	8	8	9	10	11	11	12	13	14	15	39
40	0	1	1	2	2	3	4	4	5	6	6	7	8	8	9	10	10	11	12	13	13	40
41	0	1	1	2	2	3	3	4	4	5	6	6	7	7	8	9	9	10	11	11	12	41
42	0	0	1	1	2	2	3	3	4	4	5	5	6	7	7	8	8	9	9	10	11	42
43	0	0	1	1	2	2	3	3	3	4	4	5	5	6	6	7	7	8	8	9	9	43
44	0	0	1	1	1	2	2	3	3	3	4	4	4	5	5	6	6	7	7	8	8	44
45	0	0	1	1	1	1	2	2	2	3	3	3	4	4	4	5	5	6	6	6	7	45
46	0	0	0	1	1	1	1	2	2	2	2	2	3	3	4	4	4	4	5	5	5	46
47	0	0	0	1	1	1	1	1	1	2	2	2	2	2	3	3	3	3	4	4	4	47
48	0	0	0	0	0	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	3	48
49	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	49
50	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	50
Add.	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	Add.
	0′		1′		2′		3′		4′		5′		6′		7′		8′		9′		10′	
Ther.	Mean refraction.																					Ther.

TABLE 22.

Correction of the Mean Refraction for the Height of the Thermometer.

Ther. Subt.	Mean refraction.																					Ther. Subt.
	0′		1′		2′		3′		4′		5′		6′		7′		8′		9′		10′	
	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	
°	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	°
50	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	50
51	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	51
52	0	0	0	0	0	1	1	1	1	1	1	1	1	2	2	2	2	2	2	2	3	52
53	0	0	0	1	1	1	1	1	1	2	2	2	2	2	2	3	3	3	3	4	4	53
54	0	0	0	1	1	1	1	2.	2	2	2	3	3	3	3	4	4	4	5	5	5	54
55	0	0	1	1	1	1	2	2	2	3	3	3	4	4	4	5	5	5	6	6	6	55
56	0	0	1	1	1	2	2	2	3	3	4	4	4	5	5	6	6	6	7	7	8	56
57	0	0	1	1	2	2	2	3	3	4	4	5	5	6	6	6	7	8	8	8	9	57
58	0	0	1	1	2	2	3	3	4	4	5	5	6	6	7	7	8	9	9	10	10	58
59	0	1	1	2	2	3	3	4	4	5	5	6	6	7	8	8	9	10	10	11	12	59
60	0	1	1	2	2	3	3	4	5	5	6	7	7	8	9	9	10	11	11	12	13	60
61	0	1	1	2	3	3	4	4	5	6	7	7	8	9	9	10	11	12	12	13	14	61
62	0	1	1	2	3	3	4	5	6	6	7	8	9	9	10	11	12	13	14	15	15	62
63	0	1	1	2	3	4	5	5	6	7	8	8	9	10	11	12	13	14	15	16	17	63
64	0	1	2	2	3	4	5	6	7	7	8	9	10	11	12	13	14	15	16	17	18	64
65	0	1	2	3	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	65
66	0	1	2	3	4	5	6	6	7	8	9	10	11	12	14	15	16	17	18	19	20	66
67	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	16	17	18	19	20	22	67
68	0	1	2	3	4	5	6	7	8	9	11	11	13	14	15	16	18	19	20	22	23	68
69	0	1	2	3	4	5	7	8	9	10	11	12	13	15	16	17	19	20	21	23	24	69
70	0	1	2	3	5	6	7	8	9	10	12	12	14	16	17	18	20	21	22	24	25	70
71	0	1	2	4	5	6	7	8	10	11	12	13	15	16	18	19	20	22	23	25	27	71
72	0	1	2	4	5	6	8	9	10	11	13	14	16	17	18	20	21	23	25	26	28	72
73	0	1	3	4	5	7	8	9	11	12	13	14	16	18	19	21	22	24	26	27	29	73
74	0	1	3	4	5	7	8	10	11	12	14	15	17	18	20	22	23	25	27	28	30	74
75	0	1	3	4	6	7	8	10	11	13	14	16	18	19	21	22	24	26	28	29	31	75
76	0	1	3	4	6	7	9	10	12	13	15	16	18	20	22	23	25	27	29	31	32	76
77	0	1	3	5	6	8	9	11	12	14	16	17	19	21	22	24	26	28	30	32	34	77
78	0	2	3	5	6	8	9	11	13	14	16	18	20	21	23	25	27	29	31	33	35	78
79	0	2	3	5	6	8	10	11	13	15	17	18	20	22	24	26	28	30	32	34	36	79
80	0	2	3	5	7	8	10	12	14	15	17	19	21	23	25	27	29	31	33	35	37	80
81	0	2	3	5	7	9	10	12	14	16	18	20	21	24	26	28	30	32	34	36	38	81
82	0	2	4	5	7	9	11	13	14	16	18	20	22	24	26	28	31	33	35	37	40	82
83	0	2	4	5	7	9	11	13	15	17	19	21	23	25	27	29	31	34	36	38	41	83
84	0	2	4	6	8	9	11	13	15	17	19	21	23	26	28	30	32	35	37	39	42	84
85	0	2	4	6	8	10	12	14	16	18	20	22	24	26	29	31	33	36	38	40	43	85
86	0	2	4	6	8	10	12	14	16	18	20	23	25	27	29	32	34	37	39	42	44	86
87	0	2	4	6	8	10	12	14	17	19	21	23	25	28	30	32	35	38	40	43	45	87
88	0	2	4	6	8	10	13	15	17	19	21	24	26	28	31	33	36	38	41	44	46	88
89	0	2	4	6	9	11	13	15	17	20	22	24	27	29	32	34	37	39	42	45	48	89
90	0	2	4	7	9	11	13	16	18	20	23	25	27	30	32	35	38	40	43	46	49	90
91	0	2	4	7	9	11	14	16	18	21	23	25	28	31	33	36	39	41	44	47	50	91
92	0	2	5	7	9	11	14	16	19	21	24	26	29	31	34	37	39	42	45	48	51	92
93	0	2	5	7	9	12	14	17.	19	22	24	27	29	32	35	37	40	43	46	49	52	93
94	0	2	5	7	10	12	14	17	19	22	25	27	30	33	35	38	41	44	47	50	53	94
95	0	2	5	7	10	12	15	17	20	22	25	28	30	33	36	39	42	45	48	51	54	95
96	0	2	5	7	10	12	15	18	20	23	26	28	31	34	37	40	43	46	49	52	55	96
97	0	3	5	8	10	13	15	18	21	23	26	29	32	35	38	41	44	47	50	53	56	97
98	0	3	5	8	10	13	16	18	21	24	27	29	32	35	38	41	44	48	51	54	58	98
99	0	3	5	8	11	13	16	19	21	24	27	30	33	36	39	42	45	49	52	55	59	99
100	0	3	5	8	11	13	16	19	22	25	28	31	34	37	40	43	46	50	53	56	60	100
Subt.	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	30″	0″	Subt.
	0′		1′		2′		3′		4′		5′		6′		7′		8′		9′		10′	
Ther.	Mean refraction.																					Ther.

6583—06——34

TABLE 23.

Correction of the Moon's Altitude for parallax and refraction corresponding to a mean value of the horizontal parallax, 57′ 30″.

Moon's alt.	Corr.	Moon's alt.	Corr.	Moon's alt.	Corr.	Moon's alt.	Corr.
°	′	°	′	°	′	°	′
10	51	31	48	51	35	71	18
11	52	32	47	52	35	72	17
12	52	33	47	53	34	73	17
13	52	34	46	54	33	74	16
14	52	35	46	55	32	75	15
15	52	36	45	56	32	76	14
16	52	37	45	57	31	77	13
17	52	38	44	58	30	78	12
18	52	39	44	59	29	79	11
19	52	40	43	60	28	80	10
20	51						
21	51	41	42	61	27	81	9
22	51	42	42	62	26	82	8
23	51	43	41	63	26	83	7
24	50	44	40	64	25	84	6
25	50	45	40	65	24	85	5
26	50	46	39	66	23	86	4
27	49	47	38	67	22	87	3
28	49	48	38	68	21	88	2
29	49	49	37	69	20	89	1
30	48	50	36	70	19	90	0

TABLE 24.

Correction of the Moon's Apparent Altitude for Parallax and Refraction.

[Barometer, 30 inches.—Fahrenheit's Thermometer, 50°.]

Moon's app. alt.	Horizontal parallax.								Seconds of parallax.	Correction for seconds of parallax.—Add.					Corr. for minutes of alt.
	54′	55′	56′	57′	58′	59′	60′	61′		0″	2″	4″	6″	8″	
° ′	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″	″	″	″	″	″	
5 0	43 56	44 56	45 56	46 56	47 56	48 55	49 55	50 55	0	0	2	4	6	8	
10	44 11	45 11	46 11	47 11	48 11	49 10	50 10	51 10	10	10	12	14	16	18	
20	25	25	25	25	25	24	24	24	20	20	22	24	26	28	
30	39	39	38	38	38	38	37	37	30	30	32	34	36	38	
40	52	51	51	51	51	51	51	51	40	40	42	44	46	48	
50	45 4	46 3	47 3	48 3	49 3	50 3	51 3	52 3	50	50	52	54	56	58	
6 0	45 15	46 15	47 14	48 14	49 14	50 13	51 13	52 13	0	0	2	4	6	8	
10	26	26	25	25	25	25	25	25	10	10	12	14	16	18	
20	36	36	36	35	35	34	34	34	20	20	22	24	26	28	
30	46	46	45	45	45	44	44	44	30	30	32	34	36	38	
40	55	55	55	54	54	54	53	53	40	40	42	44	46	48	
50	46 4	47 3	48 3	49 3	50 3	51 2	52 1	53 1	50	50	52	54	56	58	
7 0	46 12	47 12	48 12	49 12	50 12	51 11	52 11	53 10	0	0	2	4	6	8	
10	21	20	20	20	19	18	18	18	10	10	12	14	16	18	
20	29	28	28	27	27	26	25	25	20	20	22	24	26	28	
30	36	36	35	35	34	34	34	33	30	30	32	34	36	38	
40	43	42	42	41	41	40	40	40	40	40	42	44	46	48	
50	50	49	48	48	48	47	46	46	50	50	52	54	56	58	Add.
8 0	46 56	47 56	48 55	49 54	50 54	51 54	52 53	53 53	0	0	2	4	6	8	1′ 1″
10	47 2	48 2	49 1	50 0	51 0	59	59	58	10	10	12	14	16	18	2 1
20	8	7	7	6	6	52 5	53 4	54 4	20	20	22	24	26	28	3 2
30	13	13	12	11	11	10	10	9	30	30	32	34	36	38	4 2
40	19	18	17	17	16	16	15	14	40	40	42	44	46	48	5 3
50	24	23	22	22	21	20	19	19	50	50	52	54	56	58	6 4
9 0	47 28	48 27	49 26	50 26	51 25	52 24	53 24	54 23	0	0	2	4	6	8	7 4
10	33	32	31	30	30	29	28	27	10	10	12	14	16	18	8 5
20	37	36	35	34	34	33	32	32	20	20	22	24	26	28	9 5
30	41	41	40	39	38	37	37	36	30	30	32	34	36	38	
40	45	44	43	43	42	41	40	39	40	40	42	44	46	48	
50	49	48	47	46	46	45	44	44	50	49	51	53	55	57	

TABLE 24.

Correction of the Moon's Apparent Altitude for Parallax and Refraction.

[Barometer 30 inches.—Fahrenheit's Thermometer 50°.]

Moon's app. alt.	Horizontal parallax.								Seconds of parallax.	Correction for seconds of parallax.—Add.					Corr. for minutes of alt.
	54′	55′	56′	57′	58′	59′	60′	61′		0″	2″	4″	6″	8″	
° ′	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″	″	″	″	″	″	Add.
10 0	47 53	48 52	49 51	50 50	51 50	52 48	53 48	54 47	0	0	2	4	6	8	1′ 0″
10	56	55	54	53	52	51	50	50	10	10	12	14	16	18	2 1
20	59	58	57	56	55	55	54	53	20	20	22	24	26	28	3 1
30	48 2	49 1	50 0	59	58	57	56	55	30	29	31	33	35	37	4 1
40	5	4	2	51 2	52 1	53 0	59	58	40	39	41	43	45	47	5 2
50	7	6	5	4	4	2	54 1	55 0	50	49	51	53	55	57	6 2
11 0	48 10	49 9	50 8	51 7	52 7	53 5	54 4	55 3	0	0	2	4	6	8	7 2
10	12	11	10	9	9	7	6	5	10	10	12	14	16	18	8 2
20	15	14	12	12	11	9	8	7	20	20	22	24	26	28	9 3
30	17	16	14	13	13	11	10	9	30	29	31	33	35	37	
40	19	18	17	15	15	13	12	11	40	39	41	43	45	47	
50	21	20	18	17	17	15	14	13	50	49	51	53	55	57	
12 0	48 22	49 21	50 19	51 18	52 17	53 17	54 15	55 14	0	0	2	4	6	8	
10	24	23	21	20	19	18	16	15	10	10	12	14	16	18	
20	26	25	23	22	21	20	18	17	20	20	22	24	25	27	
30	27	26	24	23	22	20	19	18	30	29	31	33	35	37	
40	28	27	25	24	23	21	20	19	40	39	41	43	45	47	
50	29	28	26	25	24	22	21	20	50	49	51	53	55	57	
13 0	48 30	49 29	50 27	51 26	52 25	53 23	54 22	55 20	0	0	2	4	6	8	1 0
10	31	30	28	27	26	24	22	21	10	10	12	14	16	18	2 0
20	32	31	29	27	26	24	23	21	20	19	21	23	25	27	3 0
30	33	32	30	28	27	25	23	22	30	29	31	33	35	37	4 0
40	34	32	30	29	28	26	24	22	40	39	41	43	45	47	5 0
50	35	33	31	30	28	26	25	23	50	49	51	53	55	57	6 0
14 0	48 35	49 33	50 31	51 30	52 28	53 26	54 25	55 23	0	0	2	4	6	8	7 0
10	35	34	32	30	28	26	25	23	10	10	12	14	16	18	8 0
20	36	34	32	30	29	27	25	24	20	19	21	23	25	27	9 0
30	36	34	32	30	29	27	25	23	30	29	31	33	35	37	
40	36	34	32	30	29	27	25	23	40	39	41	43	45	47	
50	36	34	32	30	29	27	25	23	50	49	51	53	55	57	
15 0	48 36	49 35	50 33	51 31	52 29	53 27	54 25	55 23	0	0	2	4	6	8	
10	36	35	32	30	28	26	24	22	10	10	12	14	16	18	
20	36	35	32	30	28	26	24	22	20	19	21	23	25	27	
30	36	34	31	29	28	25	23	21	30	29	31	33	35	37	
40	36	34	31	29	27	25	23	21	40	39	41	43	45	47	
50	35	33	30	28	26	24	21	19	50	49	51	53	55	57	
16 0	48 35	49 32	50 29	51 27	52 25	53 23	54 20	55 18	0	0	2	4	6	8	
10	34	32	29	27	25	23	20	18	10	10	12	13	15	17	
20	34	32	29	27	25	22	20	17	20	19	21	23	25	27	
30	33	31	28	26	24	21	19	16	30	29	31	33	35	36	
40	33	31	28	25	23	21	18	16	40	38	40	42	44	46	
50	32	30	27	24	22	20	17	15	50	48	50	52	54	56	Sub.
17 0	48 31	49 29	50 26	51 23	52 21	53 18	54 16	55 13	0	0	2	4	6	8	1′ 0″
10	30	28	25	22	20	17	14	12	10	10	12	13	15	17	2 0
20	28	26	23	20	18	15	12	10	20	19	21	23	25	27	3 0
30	27	25	22	19	17	14	11	9	30	29	31	33	34	36	4 0
40	26	24	21	18	16	13	10	7	40	38	40	42	44	46	5 1
50	26	23	20	17	15	12	9	6	50	48	50	52	53	55	6 1
18 0	48 24	49 21	50 18	51 15	52 13	53 10	54 7	55 4	0	0	2	4	6	8	7 1
10	23	20	17	14	12	9	6	3	10	10	11	13	15	17	8 1
20	22	19	16	13	11	8	5	2	20	19	21	23	25	27	9 1
30	21	18	15	12	10	6	3	0	30	29	30	32	34	36	
40	20	17	14	10	8	4	1	54 58	40	38	40	42	44	46	
50	18	15	12	9	6	2	53 59	56	50	48	50	51	53	55	
19 0	48 16	49 13	50 10	51 7	52 4	53 0	53 57	54 55	0	0	2	4	6	8	
10	15	12	8	5	2	52 59	55	53	10	10	11	13	15	17	
20	13	10	6	3	0	57	53	51	20	19	21	23	25	27	
30	12	8	5	2	51 58	55	51	49	30	29	30	32	34	36	
40	10	6	3	0	56	53	49	47	40	38	40	42	44	46	
50	9	5	2	50 58	55	51	48	45	50	48	50	51	53	55	

TABLE 24.

Correction of the Moon's Apparent Altitude for Parallax and Refraction.

[Barometer 30 inches.—Fahrenheit's Thermometer 50°.]

Moon's app. alt.	Horizontal parallax. 54′	55′	56′	57′	58′	59′	60′	61′	Seconds of parallax.	Correction for seconds of parallax.—Add. 0″	2″	4″	6″	8″	Corr. for minutes of alt.
° ′	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″	″	″	″	″	″	Sub.
20 0	48 6	49 3	49 59	50 56	51 52	52 49	53 45	54 42	0	0	2	4	6	8	1′ 0″
10	5	2	58	55	51	47	43	40	10	9	11	13	15	17	2 0
20	3	0	56	52	49	45	41	37	20	19	21	23	24	26	3 1
30	1	48 58	53	50	46	42	38	35	30	28	30	32	34	36	4 1
40	59	56	52	48	44	40	36	33	40	38	39	41	43	45	5 1
50	57	54	50	46	42	38	34	30	50	47	49	51	53	54	6 1
21 0	47 55	48 51	49 47	50 43	51 39	52 35	53 31	54 28	0	0	2	4	6	7	7 1
10	53	49	45	41	37	33	29	26	10	9	11	13	15	17	8 1
20	51	47	43	39	35	31	27	23	20	19	21	22	24	26	9 2
30	48	44	40	36	32	28	24	20	30	28	30	32	34	35	
40	46	42	38	33	29	25	21	17	40	37	39	41	43	45	
50	43	39	35	31	27	22	18	14	50	47	49	50	52	54	
22 0	47 42	48 37	49 33	50 29	51 25	52 20	53 16	54 11	0	0	2	4	6	7	
10	40	35	30	26	22	17	13	8	10	9	11	13	15	17	
20	37	32	27	23	19	14	10	5	20	19	20	22	24	26	
30	34	30	25	20	16	11	7	3	30	28	30	31	33	35	
40	32	27	22	18	13	9	4	0	40	37	39	41	43	45	
50	29	25	20	15	11	6	1	53 57	50	46	48	50	52	54	
23 0	47 27	48 22	49 17	50 13	51 8	52 3	52 58	53 54	0	0	2	4	6	7	
10	25	20	15	10	5	0	55	51	10	9	11	13	15	17	
20	22	17	12	7	2	51 57	52	48	20	18	20	22	24	26	
30	19	14	9	4	0	54	49	45	30	28	29	31	33	35	
40	16	11	6	1	50 57	51	46	42	40	37	39	40	42	44	
50	13	8	3	49 58	54	48	43	38	50	46	48	50	51	53	
24 0	47 10	48 5	49 0	49 55	50 50	51 45	52 40	53 35	0	0	2	4	5	7	1 0
10	8	3	48 57	52	47	42	37	32	10	9	11	13	15	16	2 1
20	5	0	54	49	44	39	33	28	20	18	20	22	24	26	3 1
30	2	47 57	51	46	41	35	30	24	30	27	29	30	32	34	4 1
40	46 59	54	48	43	38	32	27	21	40	36	38	40	42	44	5 2
50	56	51	45	40	35	29	23	18	50	46	47	49	51	53	6 2
25 0	46 53	47 48	48 42	49 37	50 31	51 26	52 20	53 14	0	0	2	4	5	7	7 2
10	50	45	39	33	28	22	16	10	10	9	11	13	14	16	8 2
20	46	41	35	29	24	18	12	6	20	18	20	22	24	25	9 3
30	43	38	32	26	20	14	8	3	30	27	29	31	33	34	
40	40	34	28	23	17	11	5	52 59	40	36	38	40	42	43	
50	37	31	25	19	14	7	1	56	50	45	47	49	51	52	
26 0	46 34	47 28	48 22	49 16	50 10	51 4	51 58	52 52	0	0	2	4	5	7	
10	31	25	19	13	7	1	54	48	10	9	11	13	14	16	
20	27	21	15	9	3	50 57	50	44	20	18	20	22	23	25	
30	24	18	12	6	49 59	53	46	40	30	27	29	31	32	34	
40	20	14	8	2	55	49	42	36	40	36	38	39	41	43	
50	17	11	4	48 58	51	45	38	32	50	45	47	48	50	52	
27 0	46 14	47 7	48 1	48 54	49 48	50 41	51 35	52 28	0	0	2	4	5	7	1 0
10	11	4	47 58	51	44	37	31	24	10	9	11	12	14	16	2 1
20	7	1	54	47	40	33	27	20	20	18	20	21	23	25	3 1
30	3	46 57	50	43	36	29	23	16	30	27	28	30	32	34	4 1
40	45 59	53	46	39	32	25	19	12	40	36	37	39	41	43	5 2
50	56	49	42	35	28	21	15	8	50	44	46	48	50	52	6 2
28 0	45 53	46 46	47 38	48 31	49 24	50 17	51 11	52 4	0	0	2	4	5	7	7 3
10	49	42	34	27	20	13	6	51 59	10	9	11	12	14	16	8 3
20	45	38	30	23	16	9	2	55	20	18	19	21	23	25	9 3
30	41	34	26	19	12	5	50 57	50	30	26	28	30	32	33	
40	37	30	23	15	8	1	54	46	40	35	37	39	41	42	
50	34	26	19	11	4	49 57	49	42	50	44	46	48	49	51	
29 0	45 30	46 22	47 15	48 7	49 0	49 53	50 45	51 38	0	0	2	4	5	7	
10	26	18	11	3	48 56	49	40	34	10	9	10	12	14	16	
20	22	14	7	47 59	52	44	36	29	20	17	19	21	23	24	
30	18	10	2	55	47	39	31	24	30	26	28	30	31	33	
40	14	6	46 58	51	43	35	27	20	40	35	37	38	40	42	
50	11	3	55	47	39	31	23	15	50	44	45	47	49	51	

TABLE 24.

Correction of the Moon's Apparent Altitude for Parallax and Refraction.

[Barometer 30 inches.—Fahrenheit's Thermometer 50°.]

Moon's app. alt.	Horizontal parallax. 54′	55′	56′	57′	58′	59′	60′	61′	Seconds of parallax.	Correction for seconds of parallax.—Add. 0″	2″	4″	6″	8″	Corr. for minutes of alt.	
° ′	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″	″	″	″	″	″	Sub.	
30 0	45 6	45 57	46 50	47 42	48 34	49 26	50 18	51 10	0	0	2	3	5	7	1′	0″
10	2	54	46	38	30	22	13	6	10	9	10	12	14	16	2	1
20	44 58	50	42	34	26	18	9	1	20	17	19	21	23	24	3	1
30	54	46	37	29	21	13	4	50 56	30	26	28	29	31	33	4	2
40	50	42	33	25	17	8	0	52	40	35	36	38	40	42	5	2
50	45	38	29	21	12	4	49 55	47	50	43	45	47	49	50	6	3
31 0	44 41	45 33	46 24	47 16	48 7	48 59	49 50	50 42	0	0	2	3	5	7	7	3
10	37	29	20	12	2	54	45	37	10	9	10	12	14	15	8	4
20	33	24	15	7	47 58	49	40	32	20	17	19	21	22	24	9	4
30	28	20	11	2	54	45	36	27	30	26	27	29	31	32		
40	24	16	7	46 58	49	40	31	22	40	34	36	38	39	41		
50	20	11	2	53	44	35	26	17	50	43	44	46	48	50		
32 0	44 15	45 7	45 58	46 49	47 40	48 31	49 22	50 13	0	0	2	3	5	7		
10	11	3	53	44	35	26	17	8	10	8	10	12	14	15		
20	7	44 58	48	39	30	21	11	2	20	17	19	20	22	24		
30	3	53	44	34	25	16	6	49 57	30	25	27	29	30	32		
40	43 58	48	39	29	20	11	1	52	40	34	35	37	39	41		
50	54	44	34	24	15	6	48 56	47	50	42	44	46	47	49		
33 0	43 48	44 39	45 29	46 19	47 10	48 0	48 50	49 41	0	0	2	3	5	7	1	0
10	44	34	25	15	5	47 55	45	36	10	8	10	12	13	15	2	1
20	40	30	20	10	0	50	40	31	20	17	18	20	22	23	3	1
30	35	25	15	5	46 55	45	35	25	30	25	27	28	30	32	4	2
40	30	20	10	0	50	40	30	20	40	33	35	37	38	40	5	2
50	25	15	5	45 55	45	35	24	14	50	42	43	45	47	48	6	3
34 0	43 21	44 11	45 0	45 50	46 40	47 30	48 19	49 9	0	0	2	3	5	7	7	3
10	16	6	44 55	45	34	24	14	3	10	8	10	12	13	15	8	4
20	11	1	50	40	29	19	9	48 58	20	17	18	20	21	23	9	4
30	6	43 56	45	35	24	13	3	52	30	25	26	28	30	31		
40	1	51	40	30	19	8	47 58	47	40	33	35	36	38	40		
50	42 56	46	35	24	14	3	52	42	50	41	43	44	46	48		
35 0	42 52	43 41	44 30	45 19	46 9	46 58	47 47	48 36	0	0	2	3	5	7		
10	47	36	25	14	3	52	41	30	10	8	10	11	13	15		
20	42	31	20	9	45 58	47	36	25	20	16	18	20	21	23		
30	37	26	15	3	52	41	30	19	30	24	26	28	29	31		
40	32	21	10	44 58	47	36	25	14	40	33	34	36	38	39		
50	27	16	4	53	42	30	19	8	50	41	42	44	46	47		
36 0	42 22	43 11	43 59	44 48	45 37	46 25	47 14	48 2	0	0	2	3	5	6		
10	17	5	54	42	31	19	8	47 56	10	8	10	11	13	14	1	1
20	12	0	48	37	25	14	2	50	20	16	18	19	21	23	2	1
30	7	42 55	43	31	20	8	46 56	44	30	24	26	27	29	31	3	2
40	1	50	38	26	14	2	50	39	40	32	34	35	37	39	4	2
50	41 56	44	32	20	8	45 56	44	33	50	40	42	43	45	47	5	3
37 0	41 51	42 39	43 27	44 15	45 3	45 51	46 39	47 27	0	0	2	3	5	6	6	3
10	46	34	21	9	44 57	45	33	21	10	8	10	11	13	14	7	4
20	41	29	16	4	52	40	27	15	20	16	17	19	21	22	8	4
30	35	23	11	43 58	46	34	21	9	30	24	25	27	29	30	9	5
40	30	18	5	53	40	28	15	3	40	32	33	35	37	38		
50	25	12	42 59	47	34	22	9	46 57	50	40	41	43	45	46		
38 0	41 19	42 7	42 54	43 41	44 29	45 16	46 3	46 51	0	0	2	3	5	6		
10	14	2	49	36	23	10	45 57	45	10	8	9	11	13	14		
20	8	41 56	43	30	17	4	51	38	20	16	17	19	20	22		
30	3	51	38	24	12	44 58	45	32	30	23	25	27	28	30		
40	40 58	45	32	18	6	52	39	26	40	31	33	35	36	38		
50	52	39	26	13	0	46	33	20	50	39	41	42	44	46		
39 0	40 47	41 33	42 20	43 7	43 54	44 40	45 27	46 13	0	0	2	3	5	6		
10	42	28	15	1	48	34	21	7	10	8	9	11	12	14	1	1
20	36	23	9	42 55	42	28	15	1	20	15	17	19	20	22	2	1
30	30	17	3	49	36	22	8	45 54	30	23	25	26	28	29	3	2
40	25	11	41 57	43	30	16	2	48	40	31	32	34	36	37	4	2
50	19	5	51	37	23	9	44 55	42	50	39	40	42	43	45	5	3

TABLE 24.

Correction of the Moon's Apparent Altitude for Parallax and Refraction.

[Barometer 30 inches.—Fahrenheit's Thermometer 50°.]

Moon's app. alt.	Horizontal parallax. 54′	55′	56′	57′	58′	59′	60′	61′	Seconds of parallax.	Correction for seconds of parallax.—Add. 0″	2″	4″	6″	8″	Corr. for minutes of alt.
° ′	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″	″	″	″	″	″	Sub.
40 0	40 14	41 0	41 46	42 32	43 18	44 4	44 50	45 36	0	0	2	3	5	6	6′ 3″
10	8	40 54	39	25	11	43 57	43	29	10	8	9	11	12	14	7 4
20	2	48	33	19	5	50	36	22	20	15	17	18	20	21	8 5
30	39 56	42	28	13	42 59	44	30	16	30	23	24	26	27	29	9 5
40	50	36	22	7	53	38	24	9	40	30	32	34	35	37	
50	45	30	16	1	47	32	18	3	50	38	40	41	43	44	
41 0	39 39	40 24	41 10	41 55	42 41	43 26	44 11	44 56	0	0	2	3	5	6	
10	33	18	4	49	34	19	4	49	10	8	9	11	12	14	
20	27	12	40 58	43	28	13	43 58	43	20	15	17	18	20	21	
30	21	6	51	36	22	7	51	37	30	23	24	26	27	29	
40	16	0	45	30	16	0	45	30	40	30	32	33	35	36	
50	10	39 54	39	24	9	42 53	38	23	50	38	39	41	42	44	
42 0	39 4	39 48	40 33	41 17	42 2	42 47	43 31	44 16	0	0	1	3	4	6	
10	38 58	42	27	11	41 56	41	25	10	10	7	9	10	12	13	1 1
20	52	36	21	5	50	34	18	3	20	15	16	18	19	21	2 1
30	46	30	14	40 58	43	27	11	43 56	30	22	24	25	27	28	3 2
40	40	24	8	52	36	21	5	49	40	30	31	33	34	36	4 2
50	34	18	2	46	30	14	42 58	42	50	37	38	40	41	43	5 3
43 0	38 28	39 12	39 56	40 40	41 24	42 8	42 52	43 36	0	0	1	3	4	6	6 4
10	22	6	50	34	18	1	45	29	10	7	9	10	12	13	7 4
20	16	38 59	43	27	11	41 54	38	22	20	15	16	18	19	20	8 5
30	10	53	37	20	5	48	31	15	30	22	23	25	26	28	9 5
40	4	47	30	14	40 58	41	24	8	40	29	31	32	34	35	
50	37 57	41	24	7	51	34	17	1	50	37	38	39	41	42	
44 0	37 51	38 35	39 18	40 1	40 44	41 27	42 10	42 54	0	0	1	3	4	6	
10	45	28	11	39 54	37	20	3	46	10	7	9	10	11	13	
20	38	21	4	47	30	13	41 56	39	20	14	16	17	19	20	
30	32	15	38 58	41	24	7	49	32	30	21	23	24	26	27	
40	26	9	51	34	17	0	42	25	40	29	30	31	33	34	
50	20	2	44	27	10	40 53	35	18	50	36	37	39	40	41	
45 0	37 14	37 56	38 38	39 21	40 3	40 46	41 28	42 11	0	0	1	3	4	6	1 1
10	7	49	31	14	39 56	39	21	3	10	7	8	10	11	13	2 1
20	0	43	25	7	49	32	14	41 56	20	14	15	17	18	20	3 2
30	36 54	37	18	1	43	25	7	49	30	21	23	24	25	27	4 3
40	48	30	11	38 54	36	18	0	42	40	28	30	31	32	34	5 3
50	41	23	4	47	29	11	40 52	34	50	35	37	38	39	41	6 4
46 0	36 35	37 17	37 58	38 40	39 22	40 4	40 45	41 27	0	0	1	3	4	6	7 5
10	29	10	51	33	15	39 57	38	20	10	7	8	10	11	12	8 5
20	22	3	44	26	8	49	31	12	20	14	15	17	18	19	9 6
30	16	36 57	38	20	1	42	24	5	30	21	22	23	25	26	
40	9	50	32	13	38 54	35	17	40 58	40	28	29	30	32	33	
50	2	43	25	6	47	28	9	50	50	35	36	37	39	40	
47 0	35 56	36 37	37 18	37 59	38 40	39 21	40 2	40 43	0	0	1	3	4	5	
10	49	30	11	52	34	14	39 55	36	10	7	8	10	11	12	
20	42	23	4	45	26	6	47	28	20	14	15	16	18	19	
30	36	17	36 57	38	19	38 59	40	21	30	20	22	23	24	26	
40	30	10	50	31	12	52	32	13	40	27	29	30	31	33	
50	23	3	43	24	5	45	25	5	50	34	35	37	38	39	
48 0	35 16	35 56	36 36	37 17	37 57	38 37	39 17	39 58	0	0	1	3	4	5	1 1
10	10	50	30	10	50	30	10	50	10	7	8	9	11	12	2 1
20	3	43	23	2	43	22	2	42	20	13	15	16	17	19	3 2
30	34 56	36	16	36 55	35	15	38 55	34	30	20	21	23	24	25	4 3
40	49	29	9	48	28	8	48	27	40	27	28	29	31	32	5 3
50	42	22	1	41	21	0	40	19	50	33	35	36	37	39	6 4
49 0	34 35	35 15	35 54	36 34	37 13	37 53	38 32	39 11	0	0	1	3	4	5	7 5
10	29	8	47	27	6	46	25	4	10	7	8	9	10	12	8 5
20	22	1	40	20	36 59	38	17	38 56	20	13	14	16	17	18	9 6
30	15	34 54	33	12	51	30	9	48	30	20	21	22	23	25	
40	8	47	26	5	44	23	2	41	40	26	27	29	30	31	
50	1	40	19	35 58	36	15	37 54	33	50	33	34	35	36	38	

TABLE 24.

Correction of the Moon's Apparent Altitude for Parallax and Refraction.

[Barometer 30 inches.—Fahrenheit's Thermometer 50°.]

Moon's app. alt.	Horizontal parallax. 54′	55′	56′	57′	58′	59′	60′	61′	Seconds of parallax.	Correction for seconds of parallax.—Add. 0″	2″	4″	6″	8″	Corr. for minutes of alt.
° ′	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″	″	″	″	″	″	
50 0	33 54	34 33	35 11	35 50	36 29	37 8	37 46	38 25	0	0	1	3	4	5	
10	47	26	4	43	21	0	38	17	10	6	8	9	10	12	
20	40	19	34 57	36	14	36 53	31	9	20	13	14	15	17	18	
30	33	11	49	28	6	45	23	1	30	19	20	22	23	24	
40	26	4	42	20	35 58	37	15	37 53	40	26	27	28	29	31	
50	19	33 57	35	13	51	29	7	45	50	32	33	35	36	37	Sub.
51 0	33 12	33 50	34 28	35 6	35 44	36 22	36 59	37 37	0	0	1	3	4	5	1′ 1″
10	5	43	21	34 58	36	14	51	29	10	6	8	9	10	11	2 1
20	32 58	36	13	50	28	6	43	21	20	13	14	15	16	18	3 2
30	51	29	6	43	21	35 58	36	13	30	19	20	21	23	24	4 3
40	44	22	33 59	36	14	50	28	5	40	25	26	28	29	30	5 4
50	37	14	51	28	6	42	20	36 57	50	31	33	34	35	36	6 4
52 0	32 30	33 7	33 44	34 21	34 58	35 35	36 12	36 49	0	0	1	2	4	5	7 5
10	23	0	36	13	50	27	4	41	10	6	7	9	10	11	8 6
20	15	32 52	29	6	43	19	35 56	33	20	12	13	15	16	17	9 6
30	8	45	21	33 58	35	11	48	24	30	18	20	21	22	23	
40	1	38	14	50	27	3	40	16	40	24	26	27	28	29	
50	31 54	31	7	43	19	34 55	32	8	50	31	32	33	34	35	
53 0	31 47	32 23	32 59	33 35	34 11	34 47	35 24	36 0	0	0	1	2	4	5	
10	39	15	51	27	3	39	15	35 51	10	6	7	8	10	11	
20	32	8	44	20	33 56	31	7	43	20	12	13	14	16	17	
30	25	0	36	12	48	23	34 59	35	30	18	19	20	22	23	
40	17	31 53	28	4	40	15	51	27	40	24	25	26	28	29	
50	10	46	21	32 57	32	7	43	19	50	30	31	32	34	35	
54 0	31 3	31 38	32 13	32 49	33 24	33 59	34 35	35 10	0	0	1	2	4	5	
10	30 55	30	5	41	16	51	26	1	10	6	7	8	9	11	
20	48	22	31 57	33	8	43	18	34 53	20	12	13	14	15	16	
30	40	15	49	25	0	35	10	45	30	18	19	20	21	22	
40	33	8	42	17	32 52	27	1	37	40	23	25	26	27	28	
50	26	0	35	9	44	19	33 53	28	50	29	30	32	33	34	
55 0	30 18	30 52	31 27	32 1	32 36	33 10	33 45	34 19	0	0	1	2	3	5	
10	10	45	19	31 53	28	2	36	11	10	6	7	8	9	10	
20	3	38	12	46	20	32 54	28	3	20	11	13	14	15	16	
30	29 55	30	4	38	12	46	20	33 54	30	17	18	19	20	22	
40	48	22	30 56	30	4	37	11	45	40	23	24	25	26	27	
50	40	14	48	22	31 55	29	3	37	50	28	30	31	32	33	
56 0	29 33	30 7	30 40	31 14	31 47	32 21	32 55	33 28	0	0	1	2	3	4	
10	25	29 59	32	6	39	13	46	20	10	6	7	8	9	10	
20	18	51	24	30 58	31	4	37	11	20	11	12	13	14	16	
30	10	43	16	50	23	31 56	29	2	30	17	18	19	20	21	1 1
40	3	36	9	42	15	48	21	32 54	40	22	23	24	25	27	2 2
50	28 55	28	1	34	7	40	12	45	50	28	29	30	31	32	3 2
57 0	28 47	29 20	29 53	30 25	30 58	31 31	32 3	32 36	0	0	1	2	3	4	4 3
10	39	12	45	17	50	22	31 55	27	10	5	6	7	9	10	5 4
20	32	5	37	9	42	14	47	19	20	11	12	13	14	15	6 5
30	24	28 57	29	1	33	6	38	10	30	16	17	18	19	21	7 5
40	17	49	21	29 53	25	30 57	29	1	40	22	23	24	25	26	8 6
50	9	41	13	45	17	49	21	31 52	50	27	28	29	30	31	9 7
58 0	28 1	28 33	29 5	29 37	30 9	30 41	31 12	31 44	0	0	1	2	3	4	
10	27 53	25	28 57	28	0	32	4	35	10	5	6	7	8	9	
20	45	17	49	20	29 52	23	30 55	26	20	10	12	13	14	15	
30	38	9	41	12	44	15	46	17	30	16	17	18	19	20	
40	30	1	33	4	35	6	38	9	40	21	22	23	24	25	
50	22	27 53	24	28 55	27	29 58	29	0	50	26	27	28	29	30	
59 0	27 14	27 45	28 16	28 47	29 18	29 49	30 20	30 51	0	0	1	2	3	4	
10	6	37	7	38	9	40	11	42	10	5	6	7	8	9	
20	26 58	29	27 59	30	1	31	2	33	20	10	11	12	13	14	
30	51	21	51	22	28 53	23	29 54	24	30	15	16	17	18	19	
40	43	13	43	14	44	14	45	15	40	20	21	22	23	24	
50	35	5	35	5	36	6	36	6	50	25	26	27	29	30	

TABLE 24.

Correction of the Moon's Apparent Altitude for Parallax and Refraction.

[Barometer 30 inches.—Fahrenheit's Thermometer 50°.]

Moon's app. alt.	Horizontal parallax. 54′	55′	56′	57′	58′	59′	60′	61′	Seconds of parallax.	Correction for seconds of parallax.—Add. 0″	2″	4″	6″	8″	Corr. for minutes of alt.
° ′	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″	″	″	″	″	″	
60 0	26 26	26 57	27 27	27 57	28 27	28 57	29 27	29 57	0	0	1	2	3	4	
10	19	49	19	49	19	49	18	48	10	5	6	7	8	9	
20	11	41	11	40	10	40	9	39	20	10	11	12	13	14	
30	3	32	2	31	1	31	0	30	30	15	16	17	18	19	
40	25 55	24	26 53	23	27 53	22	28 51	21	40	20	21	22	23	24	
50	47	16	45	14	44	13	42	12	50	25	26	27	28	29	
61 0	25 39	26 8	26 37	27 6	27 36	28 5	28 34	29 3	0	0	1	2	3	4	
10	31	0	29	26 58	27	27 56	25	28 54	10	5	6	7	8	9	
20	23	25 52	20	49	18	47	16	45	20	10	11	12	12	13	
30	15	43	12	40	10	38	7	35	30	14	15	16	17	18	
40	7	35	4	32	1	29	27 58	26	40	19	20	21	22	23	
50	24 59	27	25 55	24	26 52	20	49	17	50	24	25	26	27	28	
62 0	24 50	25 19	25 47	26 15	26 43	27 11	27 40	28 8	0	0	1	2	3	4	
10	42	10	38	6	34	2	30	27 58	10	5	6	6	7	8	
20	34	2	29	25 57	25	26 53	21	49	20	9	10	11	12	12	
30	26	24 54	21	49	17	45	12	40	30	14	15	16	17	18	
40	18	46	13	41	8	36	3	31	40	19	19	20	21	22	
50	10	37	4	32	25 59	27	26 54	21	50	23	24	25	26	27	
63 0	24 2	24 29	24 56	25 23	25 51	26 18	26 45	27 12	0	0	1	2	3	4	
10	23 54	21	48	15	42	9	36	3	10	4	5	6	7	8	
20	46	13	39	6	33	0	27	26 54	20	9	10	11	12	13	
30	37	4	31	24 58	24	25 51	18	45	30	13	14	15	16	17	
40	29	23 55	22	49	15	42	8	35	40	18	19	20	21	22	
50	20	47	13	40	6	33	25 59	26	50	22	23	24	25	26	
64 0	23 12	23 39	24 5	24 32	24 58	25 24	25 50	26 17	0	0	1	2	3	3	
10	4	31	23 57	23	49	15	41	8	10	4	5	6	7	8	
20	22 56	22	48	14	40	6	32	25 58	20	9	10	10	11	12	
30	47	13	39	5	31	24 57	22	48	30	13	14	15	16	16	
40	39	5	30	23 56	22	48	13	39	40	17	18	19	20	21	
50	31	22 57	22	48	13	39	4	30	50	22	23	23	24	25	
65 0	22 23	22 48	23 13	23 39	24 4	24 30	24 55	25 21	0	0	1	2	2	3	Sub.
10	14	40	5	30	23 55	20	46	11	10	4	5	6	7	7	1′ 1″
20	6	31	22 56	21	46	11	36	1	20	8	9	10	11	12	2 2
30	21 58	23	48	13	37	2	27	24 52	30	13	13	14	15	16	3 3
40	49	14	39	4	28	23 53	18	43	40	17	18	18	19	20	4 4
50	41	6	30	22 55	19	44	8	33	50	21	22	23	23	24	5 5
66 0	21 32	21 57	22 21	22 46	23 10	23 35	23 59	24 23	0	0	1	2	2	3	6 5
10	24	48	12	37	1	25	49	14	10	4	5	6	7	7	7 6
20	15	39	3	28	22 52	15	40	4	20	8	9	10	11	11	8 7
30	7	31	21 55	19	43	6	31	23 55	30	12	13	14	15	16	9 8
40	20 59	22	46	10	34	22 57	21	45	40	16	17	18	19	20	
50	50	14	37	1	25	48	12	36	50	20	21	22	23	24	
67 0	20 41	21 5	21 28	21 52	22 15	22 39	23 2	23 26	0	0	1	2	2	3	
10	33	20 56	19	43	6	29	22 52	16	10	4	5	5	6	7	
20	25	48	11	34	21 57	20	43	7	20	8	8	9	10	11	
30	16	39	2	25	48	11	34	22 57	30	12	12	13	14	15	
40	8	30	20 53	16	39	2	24	47	40	15	16	17	18	18	
50	19 59	21	44	7	30	21 52	15	37	50	19	20	21	22	22	
68 0	19 50	20 13	20 35	20 58	21 21	21 43	22 5	22 28	0	0	1	1	2	3	
10	42	4	27	49	12	34	21 56	19	10	4	4	5	6	7	
20	33	19 56	18	40	2	24	47	9	20	7	8	9	9	10	
30	25	47	9	31	20 53	15	37	21 59	30	11	12	13	13	14	
40	16	38	0	22	44	5	27	49	40	15	16	16	17	18	
50	7	29	19 51	13	34	20 56	17	39	50	18	19	20	21	21	
69 0	18 59	19 21	19 42	20 4	20 25	20 47	21 8	21 30	0	0	1	1	2	3	
10	50	12	33	19 55	16	37	20 59	20	10	4	4	5	6	6	
20	42	3	24	45	7	28	49	10	20	7	8	8	9	10	
30	33	18 54	15	36	19 57	18	39	0	30	11	11	12	13	13	
40	24	45	6	27	48	9	29	20 50	40	14	15	15	16	17	
50	16	37	18 57	18	39	0	20	41	50	18	18	19	20	20	

TABLE 24.

Correction of the Moon's Apparent Altitude for Parallax and Refraction.

[Barometer 30 inches.—Fahrenheit's Thermometer 50°.]

Moon's app. alt.	Horizontal parallax. 54′	55′	56′	57′	58′	59′	60′	61′	Seconds of parallax.	Correction for seconds of parallax.—Add. 0″	2″	4″	6″	8″	Corr. for minutes of alt.
° ′	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″	″	″	″	″	″	
70 0	18 7	18 28	18 48	19 9	19 30	19 50	20 11	20 31	0	0	1	1	2	3	
10	17 58	19	39	0	20	41	1	21	10	3	4	5	5	6	
20	50	10	30	18 50	11	31	19 51	11	20	7	7	8	9	9	
30	41	1	21	41	1	21	41	1	30	10	11	11	12	13	
40	32	17 53	12	32	18 52	12	32	19 52	40	13	14	15	15	16	
50	24	44	3	23	43	3	22	42	50	17	17	18	19	19	
71 0	17 15	17 35	17 54	18 14	18 34	18 53	19 12	19 32	0	0	1	1	2	3	
10	6	26	45	5	24	43	3	22	10	3	4	4	5	6	
20	16 57	17	36	17 55	14	33	18 53	12	20	6	7	8	8	9	
30	48	8	27	46	5	24	43	2	30	10	10	11	12	12	
40	40	16 59	18	37	17 56	15	34	18 52	40	13	13	14	15	15	
50	31	50	9	28	47	5	24	42	50	16	17	17	18	19	
72 0	16 22	16 41	17 0	17 18	17 37	17 55	18 14	18 32	0	0	1	1	2	2	
10	13	32	16 50	9	27	46	4	22	10	3	4	4	5	5	
20	5	23	41	16 59	18	36	17 54	12	20	6	7	7	8	8	
30	15 57	14	32	50	9	27	45	3	30	9	10	10	11	11	
40	48	5	23	41	16 59	17	35	17 53	40	12	13	13	14	14	
50	39	15 56	14	32	50	7	25	43	50	15	16	16	17	18	
73 0	15 30	15 47	16 5	16 22	16 40	16 58	17 15	17 33	0	0	1	1	2	2	
10	21	38	15 56	13	30	48	5	23	10	3	3	4	5	5	
20	12	29	47	4	21	39	16 56	13	20	6	6	7	7	8	
30	3	20	37	15 55	12	29	46	3	30	9	9	10	10	11	
40	14 54	11	28	45	2	19	36	16 53	40	11	12	13	13	14	
50	45	2	19	35	15 52	9	26	42	50	14	15	15	16	17	
74 0	14 36	14 53	15 9	15 26	15 42	15 59	16 16	16 32	0	0	1	1	2	2	Sub.
10	28	44	0	17	33	49	6	22	10	3	3	4	4	5	1′ 1″
20	19	35	14 51	8	24	40	15 56	12	20	5	6	6	7	8	2 2
30	10	26	42	14 58	14	30	46	2	30	8	9	9	10	11	3 3
40	1	17	33	49	5	20	36	15 52	40	11	11	12	12	13	4 4
50	13 52	8	23	39	14 55	10	26	42	50	13	14	14	15	16	5 5
75 0	13 43	13 59	14 14	14 29	14 45	15 1	15 16	15 32	0	0	1	1	2	2	6 6
10	34	50	5	20	36	14 52	7	22	10	3	3	4	4	5	7 7
20	25	41	13 56	11	27	42	14 57	12	20	5	6	6	7	7	8 8
30	16	32	46	1	17	32	47	2	30	8	8	9	9	10	9 9
40	7	22	37	13 52	7	22	37	14 51	40	10	11	11	12	12	
50	12 58	13	28	42	13 57	12	27	41	50	13	13	14	14	15	
76 0	12 49	13 4	13 18	13 33	13 47	14 2	14 17	14 31	0	0	0	1	1	2	
10	41	12 55	9	24	38	13 53	7	21	10	2	3	3	4	4	
20	32	46	0	14	28	43	13 57	11	20	5	5	6	6	7	
30	23	37	12 51	5	19	33	47	1	30	7	8	8	8	9	
40	14	27	41	12 55	9	23	36	13 50	40	9	10	10	11	11	
50	5	18	32	45	12 59	13	26	40	50	12	12	13	13	14	
77 0	11 56	12 9	12 22	12 36	12 49	13 3	13 16	13 30	0	0	0	1	1	2	
10	47	0	13	27	40	12 53	7	20	10	2	3	3	4	4	
20	38	11 51	4	17	30	43	12 57	10	20	4	5	5	6	6	
30	29	42	11 55	8	21	33	47	0	30	7	7	7	8	8	
40	19	32	45	11 58	11	23	36	12 49	40	9	9	9	10	10	
50	10	23	35	48	1	13	26	39	50	11	11	12	12	13	
78 0	11 1	11 14	11 26	11 39	11 52	12 4	12 16	12 29	0	0	0	1	1	2	
10	10 52	5	17	30	42	11 54	6	19	10	2	2	3	3	4	
20	43	10 55	8	20	32	44	11 56	8	20	4	4	5	5	6	
30	34	46	10 58	10	22	34	46	11 58	30	6	6	7	7	8	
40	25	37	48	0	12	24	36	48	40	8	8	9	9	10	
50	16	28	39	10 51	3	15	26	38	50	10	10	11	11	12	
79 0	10 7	10 19	10 30	10 42	10 53	11 5	11 16	11 28	0	0	0	1	1	1	
10	9 58	9	21	32	43	10 55	6	17	10	2	2	3	3	3	
20	49	0	11	22	33	44	10 56	7	20	4	4	4	5	5	
30	40	9 50	1	12	23	34	45	10 56	30	6	6	6	7	7	
40	31	41	9 52	3	13	24	35	46	40	7	8	8	8	9	
50	22	32	43	9 54	4	15	25	36	50	9	10	10	10	11	

TABLE 24.

Correction of the Moon's Apparent Altitude for Parallax and Refraction.

[Barometer 30 inches.—Fahrenheit's Thermometer 50°.]

Moon's app. alt.	Horizontal parallax. 54′	55′	56′	57′	58′	59′	60′	61′	Seconds of parallax.	Correction for seconds of parallax.—Add. 0″	2″	4″	6″	8″	Corr. for minutes of alt.
° ′	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″	″	″	″	″	″	
80 0	9 13	9 23	9 34	9 44	9 55	10 5	10 15	10 26	0	0	0	1	1	1	
10	3	14	24	34	45	9 55	5	15	10	2	2	2	3	3	
20	8 54	4	14	24	35	45	9 55	5	20	3	4	4	4	5	
30	45	8 55	5	15	25	35	45	9 54	30	5	5	6	6	6	
40	36	46	8 55	5	15	25	35	44	40	7	7	7	8	8	
50	27	37	46	8 56	6	15	25	34	50	8	9	9	9	10	
81 0	8 18	8 27	8 37	8 46	8 56	9 5	9 14	9 24	0	0	0	1	1	1	
10	9	18	27	36	46	8 55	4	13	10	1	2	2	2	3	
20	7 59	8	17	26	36	45	8 54	3	20	3	3	4	4	4	
30	50	7 59	8	17	26	35	44	8 52	30	4	5	5	5	6	
40	41	50	7 59	8	17	25	34	42	40	6	6	6	7	7	
50	32	41	49	7 58	7	15	24	32	50	7	8	8	8	9	
82 0	7 23	7 31	7 40	7 48	7 57	8 5	8 13	8 22	0	0	0	1	1	1	
10	14	22	30	38	47	7 55	3	11	10	1	2	2	2	2	
20	4	12	20	28	37	45	7 52	0	20	3	3	3	3	4	
30	6 55	3	11	19	27	35	42	7 50	30	4	4	5	5	5	
40	46	6 54	2	10	17	25	32	40	40	5	6	6	6	6	
50	37	45	6 52	0	7	15	22	30	50	7	7	7	7	8	
83 0	6 28	6 35	6 43	6 50	6 57	7 5	7 12	7 20	0	0	0	0	1	1	Sub.
10	19	26	33	40	47	6 54	2	9	10	1	1	2	2	2	1′ 1″
20	9	16	23	30	37	44	6 51	6 58	20	2	3	3	3	3	2 2
30	0	7	13	20	27	34	41	48	30	3	4	4	4	4	3 3
40	5 51	5 58	4	11	18	24	31	38	40	5	5	5	5	6	4 4
50	42	49	5 55	1	8	14	21	27	50	6	6	6	6	7	5 5
84 0	5 33	5 39	5 45	5 52	5 58	6 4	6 10	6 17	0	0	0	0	1	1	6 6
10	23	30	36	42	48	5 54	0	6	10	1	1	1	2	2	7 7
20	14	20	26	32	38	44	5 50	5 55	20	2	2	2	3	3	8 8
30	5	10	16	22	28	34	39	45	30	3	3	3	3	4	9 9
40	4 56	1	7	13	18	24	29	35	40	4	4	4	4	5	
50	47	4 52	4 58	3	8	14	19	25	50	5	5	5	5	6	
85 0	4 37	4 43	4 48	4 53	4 58	5 4	5 9	5 14	0	0	0	0	0	1	
10	28	33	38	43	48	4 53	4 58	3	10	1	1	1	1	1	
20	18	24	28	33	38	43	48	4 53	20	2	2	2	2	2	
30	9	14	19	23	28	33	38	43	30	2	3	3	3	3	
40	0	5	10	14	19	23	28	33	40	3	3	4	4	4	
50	3 51	3 56	0	5	9	13	18	22	50	4	4	4	5	5	
86 0	3 42	3 46	3 50	3 55	3 59	4 3	4 7	4 11	0	0	0	0	0	1	
10	33	37	41	45	49	3 53	3 57	1	10	1	1	1	1	1	
20	23	27	31	35	39	43	46	3 50	20	1	1	2	2	2	
30	14	18	21	25	29	33	36	40	30	2	2	2	2	2	
40	5	9	12	16	19	23	26	30	40	3	3	3	3	3	
50	2 56	2 59	3	6	9	13	16	19	50	3	3	3	4	4	
87 0	2 47	2 50	2 53	2 56	2 59	3 2	3 5	3 9	0	0	0	0	0	0	
10	37	40	43	46	49	2 52	2 55	2 58	10	0	1	1	1	1	
20	28	31	33	36	39	42	45	47	20	1	1	1	1	1	
30	19	21	24	26	29	32	34	37	30	1	1	2	2	2	
40	10	12	15	17	19	22	24	27	40	2	2	2	2	2	
50	1	3	5	7	9	12	14	16	50	2	2	2	3	3	
88 0	1 51	1 53	1 55	1 57	1 59	2 2	2 4	2 6	0	0	0	0	0	0	
10	42	43	45	47	49	1 51	1 53	1 55	10	0	0	0	0	0	
20	32	34	36	38	39	41	43	44	20	1	1	1	1	1	
30	23	25	26	28	29	31	32	34	30	1	1	1	1	1	
40	14	15	16	19	20	21	22	24	40	1	1	1	1	1	
50	5	6	7	9	10	11	12	13	50	1	1	1	2	2	
89 0	0 56	0 57	0 58	0 59	1 0	1 1	1 2	1 3	0	0	0	0	0	0	
10	46	47	48	49	0 50	0 51	0 51	0 52	10	0	0	0	0	0	
20	37	37	38	39	40	40	41	42	20	0	0	0	0	0	
30	28	28	28	29	30	30	31	31	30	0	0	0	0	0	
40	19	19	19	19	20	20	21	21	40	0	0	0	0	0	
50	9	10	10	10	10	10	10	10	50	1	1	1	1	1	

TABLE 25.

Table showing the variation of the altitude of an object arising from a change of 100 seconds in the declination. Unmarked quantities in the Table are positive. If the change move the body toward the elevated pole, apply the correction to the altitude with the signs in the Table; otherwise, change the signs.

Declination.	Altitude.	Latitude of same name as declination.								Latitude of different name from declination.							Altitude.	Declination.
		70°	60°	50°	40°	30°	20°	10°	0°	10°	20°	30°	40°	50°	60°	70°		
°	°	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	°	°
	0	94	87	76	64	50	34	17	0	17	34	50	64	76	87	94	0	
	10	95	88	78	65	51	35	18	0	18	35	51	65	78	88	95	10	
	20	100	92	82	68	53	36	18	0	18	36	53	68	82	92	100	20	
	30		100	88	74	57	39	20	0	20	39	57	74	88	100		30	
0	40			100	84	65	45	22	0	22	45	65	84	100			40	0
	50				100	78	53	27	0	27	53	78	100				50	
	60					100	68	35	0	35	68	100					60	
	70						100	51	0	51	100						70	
	0	94	87	77	64	50	34	17	0	17	34	50	64	77	87	94	0	
	10	95	87	77	65	50	34	17	− 1	18	35	51	66	78	88	96	10	
	20	99	91	81	67	52	35	17	− 1	19	37	54	69	83	93	101	20	
	30	107	98	87	73	56	38	18	− 2	22	41	59	76	90	102		30	
2	40		111	98	82	63	42	20	− 2	25	47	68	86	102			40	2
	50			116	97	74	50	24	− 3	30	57	81	103				50	
	60				124	95	64	30	− 5	40	73	103					60	
	70					139	92	43	− 8	59	108						70	
	0	94	87	77	64	50	34	17	0	17	34	50	64	77	87	94	0	
	10	94	87	77	64	50	34	16	− 1	19	36	52	67	79	89	97	10	
	20	98	90	79	66	51	34	16	− 3	21	39	56	71	84	95	103	20	
	30	105	96	85	70	54	36	16	− 4	24	44	62	78	93	104		30	
4	40		107	94	78	59	39	17	− 6	29	51	71	90	106			40	4
	50			111	92	70	45	19	− 8	35	62	86	109				50	
	60				117	88	56	23	−12	47	81	112					60	
	70					127	81	32	−19	70	119						70	
	0	94	87	77	65	50	34	17	0	17	34	50	65	77	87	94	0	
	10	94	87	76	64	49	33	16	− 2	20	37	53	67	80	90	98	10	
	20	97	89	78	65	50	33	15	− 4	22	40	57	73	86	96	104	20	
	30	103	94	83	69	52	34	14	− 6	26	46	64	81	95	107		30	
6	40		105	92	76	57	36	14	− 9	32	54	74	93	109			40	6
	50			107	88	66	41	15	−13	40	66	91	113				50	
	60				111	82	51	17	−18	53	87	119					60	
	70					118	72	22	−29	80	129						70	
	0	95	87	77	65	50	35	18	0	18	35	50	65	77	87	95	0	
	10	94	86	76	63	49	33	15	− 3	20	38	54	68	81	91	99	10	
	20	96	88	77	64	49	32	14	− 5	24	40	59	74	87	98	106	20	
	30	101	93	81	67	50	32	12	− 8	28	48	66	83	97	109		30	
8	40		102	89	73	54	33	11	−12	35	57	78	97	113			40	8
	50			104	84	62	37	11	−17	44	70	95	118				50	
	60				105	77	45	11	−24	59	93	125					60	
	70					109	62	13	−39	90	140						70	
	0	95	88	78	65	51	35	18	0	18	35	51	65	78	88	95	0	
	10	94	86	75	63	48	32	15	− 3	21	38	55	69	82	92	100	10	
	20	95	87	76	63	48	31	12	− 6	25	43	60	76	89	100		20	
	30	100	91	80	65	49	30	10	−10	30	50	69	86	100			30	
10	40		100	87	70	51	31	8	−15	38	60	81	100				40	10
	50			100	81	58	33	6	−21	48	75	100					50	
	60				100	71	39	5	−31	66	100						60	
	70					100	53	3	−48	100							70	
	0	96	89	78	66	51	35	18	0	18	35	51	66	78	89	96	0	
	10	94	86	76	63	48	32	14	− 4	22	39	56	70	83	94	101	10	
	20	94	86	76	62	47	29	11	− 8	27	45	62	78	91	102		20	
	30	99	90	78	64	47	28	8	−12	33	53	71	88	103			30	
12	40	108	98	84	68	49	28	5	−18	41	63	85	104				40	12
	50		112	97	77	54	29	2	−25	53	80	105					50	
	60			120	95	65	33	−1	−37	72	107						60	
	70				134	91	44	−6	−58	110							70	
Declination.	Altitude.	70°	60°	50°	40°	30°	20°	10°	0°	10°	20°	30°	40°	50°	60°	70°	Altitude.	Declination.
		Latitude of same name as declination.								Latitude of different name from declination.								

TABLE 25.

Table showing the variation of the altitude of an object arising from a change of 100 seconds in the declination. Unmarked quantities in the Table are positive. If the change move the body toward the elevated pole, apply the correction to the altitude with the signs in the Table; otherwise, change the signs.

Declination.	Altitude.	Latitude of same name as declination.								Latitude of different name from declination.							Altitude.	Declination.
		70°	60°	50°	40°	30°	20°	10°	0°	10°	20°	30°	40°	50°	60°	70°		
°	°	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	°	°
	0	97	89	79	66	52	35	18	0	18	35	52	66	79	89	97	0	
	10	94	86	76	63	48	31	14	− 4	23	40	57	72	85	95	103	10	
	20	94	86	75	61	46	27	10	− 9	28	45	64	80	93	104		20	
	30	97	89	77	62	45	26	6	− 14	35	55	74	91	106			30	
14	40	106	96	82	66	46	25	2	− 21	44	67	88	107				40	14
	50		109	93	73	50	25	− 2	− 30	58	85	110					50	
	60			115	89	60	27	− 7	− 43	79	114						60	
	70				125	82	35	−16	− 69	121							70	
	0	98	90	80	67	52	36	18	0	18	36	52	67	80	90	98	0	
	10	94	86	76	63	48	31	13	− 5	23	41	58	73	86	97	104	10	
	20	94	85	74	61	45	27	9	− 10	30	48	66	82	95	106		20	
	30	96	87	75	61	44	25	4	− 17	37	58	77	94	109			30	
16	40	104	94	80	63	44	22	0	− 24	48	70	92	111				40	16
	50		106	90	70	47	21	− 6	− 34	62	90	115					50	
	60			110	84	54	21	−14	− 50	86	121						60	
	70				117	73	25	−26	− 79	132							70	
	0	99	91	81	68	53	36	18	0	18	36	53	68	81	91	99	0	
	10	95	87	76	63	48	31	13	− 6	24	42	59	74	88	98	106	10	
	20	93	85	74	60	44	26	8	− 12	31	50	68	84	98	109		20	
	30	95	86	74	59	42	23	2	− 19	40	60	79	97	112			30	
18	40	102	92	78	61	41	20	− 3	− 27	51	74	96	116				40	18
	50		103	87	66	43	17	−10	− 39	67	95	121					50	
	60			105	79	49	16	−20	− 56	93	128						60	
	70				108	64	16	−36	− 89	143							70	
	0	100	92	82	68	53	36	18	0	18	36	53	68	82	92	100	0	
	10	95	87	76	63	48	31	12	− 6	25	43	60	76	89	100		10	
	20	93	85	74	60	43	25	6	− 13	33	52	70	86	100			20	
	30	94	85	73	58	40	21	0	− 21	42	63	82	100				30	
20	40	100	90	76	59	39	17	− 6	− 31	55	78	100					40	20
	50		100	83	63	39	13	−15	− 43	72	100						50	
	60			100	74	43	10	−26	− 63	100							60	
	70				100	56	6	−46	−100								70	
	0		93	83	69	54	37	19	0	19	37	54	69	83	93	101	0	
	10	96	88	77	63	48	30	12	− 7	26	45	62	78	91	102		10	
	20	93	85	73	59	43	25	5	− 15	35	54	72	88	103			20	
	30	94	85	72	57	39	19	− 2	− 23	45	66	86	103				30	
22	40	98	88	74	57	36	14	− 9	− 34	58	82	104					40	22
	50	110	97	80	60	36	9	−19	− 48	77	106						50	
	60		117	95	68	38	4	−33	− 70	107							60	
	70			131	92	47	− 3	−56	−111								70	
	0		95	84	70	55	37	19	0	19	37	55	70	84	95	103	0	
	10	97	88	77	64	48	30	11	− 8	27	46	63	79	93	104		10	
	20	93	85	73	59	42	24	4	− 16	36	56	74	91	105			20	
	30	93	84	71	56	38	18	− 4	− 26	48	69	89	107				30	
24	40	97	86	72	54	34	12	−12	− 37	62	86	109					40	24
	50	107	93	77	56	32	5	−23	− 53	83	111						50	
	60		112	91	64	32	− 2	−39	− 77	115							60	
	70			123	83	38	−13	−67	−122								70	
	0		96	85	72	56	38	19	0	19	38	56	72	85	96	105	0	
	10	98	89	78	64	48	30	11	− 9	28	47	65	81	95	106		10	
	20	95	85	73	59	41	23	3	− 18	38	58	77	94	108			20	
	30	93	83	70	54	36	16	− 6	− 28	50	72	92	111				30	
26	40	96	85	70	52	32	9	−16	− 41	66	91	114					40	26
	50	105	92	74	53	28	1	−28	− 58	88	117						50	
	60		108	86	58	27	− 8	−46	− 84	123							60	
	70			115	75	29	−23	−78	−134								70	
Declination.	Altitude.	70°	60°	50°	40°	30°	20°	10°	0°	10°	20°	30°	40°	50°	60°	70°	Altitude.	Declination.
		Latitude of same name as declination.								Latitude of different name from declination.								

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Lati-tude.	Declination of the same name as the latitude; upper transit; reduction additive.												Lati-tude.
	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	
°	″	″	″	″	″	″	″	″	″	″	″	″	°
0					28.1	22.4	18.7	16.0	14.0	12.4	11.1	10.1	0
1						28.0	22.4	18.6	16.0	13.9	12.4	11.1	1
2							28.0	22.3	18.6	15.9	13.9	12.3	2
3								27.9	22.3	18.5	15.8	13.8	3
4	28.1								27.8	22.2	18.5	15.8	4
5	22.4	28.0								27.7	22.1	18.4	5
6	18.7	22.4	28.0								27.6	22.0	6
7	16.0	18.6	22.3	27.9								27.4	7
8	14.0	16.0	18.6	22.3	27.8								8
9	12.4	13.9	15.9	18.5	22.2	27.7							9
10	11.1	12.4	13.9	15.8	18.5	22.1	27.6						10
11	10.1	11.1	12.3	13.8	15.8	18.4	22.0	27.4					11
12	9.2	10.1	11.1	12.3	13.8	15.7	18.3	21.9	27.3				12
13	8.5	9.2	10.0	11.0	12.2	13.7	15.6	18.2	21.7	27.1			13
14	7.9	8.5	9.2	10.0	10.9	12.1	13.6	15.5	18.0	21.6	26.9		14
15	7.3	7.8	8.4	9.1	9.9	10.9	12.1	13.5	15.4	17.9	21.4	26.7	15
16	6.8	7.3	7.8	8.4	9.1	9.8	10.8	12.0	13.4	15.3	17.8	21.3	16
17	6.4	6.8	7.2	7.8	8.3	9.0	9.8	10.7	11.9	13.3	15.2	17.6	17
18	6.0	6.4	6.8	7.2	7.7	8.3	8.9	9.7	10.6	11.8	13.2	15.0	18
19	5.7	6.0	6.3	6.7	7.2	7.6	8.2	8.9	9.6	10.6	11.7	13.1	19
20	5.4	5.7	6.0	6.3	6.7	7.1	7.6	8.1	8.8	9.5	10.5	11.6	20
21	5.1	5.4	5.6	5.9	6.3	6.6	7.0	7.5	8.1	8.7	9.5	10.4	21
22	4.9	5.1	5.3	5.6	5.9	6.2	6.6	7.0	7.5	8.0	8.6	9.4	22
23	4.6	4.8	5.0	5.3	5.5	5.8	6.1	6.5	6.9	7.4	7.9	8.5	23
24	4.4	4.6	4.8	5.0	5.2	5.5	5.8	6.1	6.4	6.8	7.3	7.8	24
25	4.2	4.4	4.6	4.7	5.0	5.2	5.4	5.7	6.0	6.4	6.8	7.2	25
26	4.0	4.2	4.3	4.5	4.7	4.9	5.1	5.4	5.7	6.0	6.3	6.7	26
27	3.9	4.0	4.1	4.3	4.5	4.7	4.9	5.1	5.3	5.6	5.9	6.2	27
28	3.7	3.8	4.0	4.1	4.3	4.4	4.6	4.8	5.0	5.3	5.5	5.8	28
29	3.5	3.7	3.8	3.9	4.1	4.2	4.4	4.6	4.7	5.0	5.2	5.5	29
30	3.4	3.5	3.6	3.7	3.9	4.0	4.2	4.3	4.5	4.7	4.9	5.1	30
31	3.3	3.4	3.5	3.6	3.7	3.8	4.0	4.1	4.3	4.4	4.6	4.8	31
32	3.1	3.2	3.3	3.4	3.5	3.7	3.8	3.9	4.1	4.2	4.4	4.6	32
33	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.9	4.0	4.2	4.3	33
34	2.9	3.0	3.1	3.2	3.2	3.3	3.4	3.6	3.7	3.8	3.9	4.1	34
35	2.8	2.9	3.0	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.9	35
36	2.7	2.8	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	36
37	2.6	2.7	2.7	2.8	2.9	2.9	3.0	3.1	3.2	3.3	3.4	3.5	37
38	2.5	2.6	2.6	2.7	2.8	2.8	2.9	3.0	3.0	3.2	3.2	3.3	38
39	2.4	2.5	2.5	2.6	2.7	2.7	2.8	2.9	2.9	3.0	3.1	3.2	39
40	2.3	2.4	2.4	2.5	2.6	2.6	2.7	2.7	2.8	2.9	3.0	3.0	40
41	2.3	2.3	2.4	2.4	2.5	2.5	2.6	2.6	2.7	2.8	2.8	2.9	41
42	2.2	2.2	2.3	2.3	2.4	2.4	2.5	2.5	2.6	2.6	2.7	2.8	42
43	2.1	2.1	2.2	2.2	2.3	2.3	2.4	2.4	2.5	2.5	2.6	2.7	43
44	2.0	2.1	2.1	2.1	2.2	2.2	2.3	2.3	2.4	2.4	2.5	2.5	44
45	2.0	2.0	2.0	2.1	2.1	2.2	2.2	2.2	2.3	2.3	2.4	2.4	45
46	1.9	1.9	2.0	2.0	2.0	2.1	2.1	2.2	2.2	2.2	2.3	2.3	46
47	1.8	1.9	1.9	1.9	2.0	2.0	2.0	2.1	2.1	2.1	2.2	2.2	47
48	1.8	1.8	1.8	1.9	1.9	1.9	2.0	2.0	2.0	2.1	2.1	2.1	48
49	1.7	1.7	1.8	1.8	1.8	1.8	1.9	1.9	1.9	2.0	2.0	2.1	49
50	1.6	1.7	1.7	1.7	1.8	1.8	1.8	1.8	1.9	1.9	1.9	2.0	50
51	1.6	1.6	1.6	1.7	1.7	1.7	1.7	1.8	1.8	1.8	1.9	1.9	51
52	1.5	1.6	1.6	1.6	1.6	1.6	1.7	1.7	1.7	1.8	1.8	1.8	52
53	1.5	1.5	1.5	1.5	1.6	1.6	1.6	1.6	1.7	1.7	1.7	1.7	53
54	1.4	1.4	1.5	1.5	1.5	1.5	1.5	1.6	1.6	1.6	1.6	1.7	54
55	1.4	1.4	1.4	1.4	1.5	1.5	1.5	1.5	1.5	1.6	1.6	1.6	55
56	1.3	1.3	1.4	1.4	1.4	1.4	1.4	1.4	1.5	1.5	1.5	1.5	56
57	1.3	1.3	1.3	1.3	1.3	1.4	1.4	1.4	1.4	1.4	1.4	1.5	57
58	1.2	1.2	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.4	1.4	1.4	58
59	1.2	1.2	1.2	1.2	1.2	1.3	1.3	1.3	1.3	1.3	1.3	1.3	59
60	1.1	1.1	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.3	1.3	60
	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	
	Declination of the same name as the latitude; upper transit; reduction additive.												

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Latitude.	Declination of the same name as the latitude; upper transit; reduction additive.													Latitude.
	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	24°	
°	"	"	"	"	"	"	"	"	"	"	"	"	"	°
0	9.2	8.5	7.9	7.3	6.8	6.4	6.0	5.7	5.4	5.1	4.9	4.6	4.4	0
1	10.1	9.2	8.5	7.8	7.3	6.8	6.4	6.0	5.7	5.4	5.1	4.8	4.6	1
2	11.1	10.0	9.2	8.4	7.8	7.2	6.8	6.3	6.0	5.6	5.3	5.0	4.8	2
3	12.3	11.0	10.0	9.1	8.4	7.8	7.2	6.7	6.3	5.9	5.6	5.3	5.0	3
4	13.8	12.2	10.9	9.9	9.1	8.3	7.7	7.2	6.7	6.3	5.9	5.5	5.2	4
5	15.7	13.7	12.1	10.9	9.8	9.0	8.3	7.6	7.1	6.6	6.2	5.8	5.5	5
6	18.3	15.6	13.6	12.1	10.8	9.8	8.9	8.2	7.6	7.0	6.6	6.1	5.8	6
7	21.9	18.2	15.5	13.5	12.0	10.7	9.7	8.9	8.1	7.5	7.0	6.5	6.1	7
8	27.3	21.7	18.0	15.4	13.4	11.9	10.6	9.6	8.8	8.1	7.5	6.9	6.4	8
9		27.1	21.6	17.9	15.3	13.3	11.8	10.6	9.5	8.7	8.0	7.4	6.8	9
10			26.9	21.4	17.8	15.2	13.2	11.7	10.5	9.5	8.6	7.9	7.3	10
11				26.7	21.3	17.6	15.0	13.1	11.6	10.4	9.4	8.5	7.8	11
12					26.5	21.1	17.5	14.9	13.0	11.5	10.3	9.3	8.4	12
13						26.2	20.9	17.3	14.8	12.8	11.3	10.1	9.2	13
14							26.0	20.7	17.1	14.6	12.7	11.2	10.0	14
15								25.7	20.4	16.9	14.4	12.5	11.1	15
16	26.5								25.4	20.2	16.7	14.3	12.4	16
17	21.1	26.2								25.1	20.0	16.5	14.1	17
18	17.5	20.9	26.0								24.8	19.7	16.3	18
19	14.9	17.3	20.7	25.7								24.5	19.5	19
20	13.0	14.8	17.1	20.4	25.4								24.2	20
21	11.5	12.8	14.6	16.9	20.2	25.1								21
22	10.3	11.3	12.7	14.4	16.7	20.0	24.8							22
23	9.3	10.1	11.2	12.5	14.3	16.5	19.7	24.5						23
24	8.4	9.2	10.0	11.1	12.4	14.1	16.3	19.5	24.2					24
25	7.7	8.3	9.0	9.9	10.9	12.2	13.9	16.1	19.2	23.8				25
26	7.1	7.6	8.2	8.9	9.8	10.8	12.1	13.7	15.9	18.9	23.5			26
27	6.6	7.0	7.5	8.1	8.8	9.6	10.6	11.9	13.5	15.6	18.6	23.1		27
28	6.2	6.5	7.0	7.4	8.0	8.7	9.5	10.5	11.7	13.3	15.4	18.3	22.7	28
29	5.7	6.1	6.4	6.9	7.3	7.9	8.6	9.4	10.3	11.5	13.1	15.1	18.0	29
30	5.4	5.7	6.0	6.4	6.8	7.2	7.8	8.4	9.2	10.1	11.3	12.8	14.9	30
31	5.1	5.3	5.6	5.9	6.3	6.7	7.1	7.7	8.3	9.0	10.0	11.1	12.6	31
32	4.8	5.0	5.2	5.5	5.8	6.2	6.5	7.0	7.5	8.1	8.9	9.8	10.9	32
33	4.5	4.7	4.9	5.1	5.4	5.7	6.1	6.4	6.9	7.4	8.0	8.7	9.6	33
34	4.3	4.4	4.6	4.8	5.1	5.3	5.6	5.9	6.3	6.8	7.3	7.8	8.6	34
35	4.0	4.2	4.4	4.5	4.7	5.0	5.2	5.5	5.8	6.2	6.6	7.1	7.7	35
36	3.8	4.0	4.1	4.3	4.5	4.7	4.9	5.1	5.4	5.7	6.1	6.5	7.0	36
37	3.6	3.8	3.9	4.0	4.2	4.4	4.6	4.8	5.0	5.3	5.6	6.0	6.4	37
38	3.4	3.6	3.7	3.8	4.0	4.1	4.3	4.5	4.7	4.9	5.2	5.5	5.8	38
39	3.3	3.4	3.5	3.6	3.8	3.9	4.0	4.2	4.4	4.6	4.8	5.1	5.4	39
40	3.1	3.2	3.3	3.4	3.6	3.7	3.8	4.0	4.1	4.3	4.5	4.7	5.0	40
41	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.9	4.0	4.2	4.4	4.6	41
42	2.9	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.7	3.8	4.0	4.1	4.3	42
43	2.7	2.8	2.9	3.0	3.0	3.1	3.2	3.3	3.5	3.6	3.7	3.9	4.0	43
44	2.6	2.7	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.8	44
45	2.5	2.6	2.6	2.7	2.8	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	45
46	2.4	2.4	2.5	2.6	2.6	2.7	2.8	2.8	2.9	3.0	3.1	3.2	3.3	46
47	2.3	2.3	2.4	2.4	2.5	2.6	2.6	2.7	2.8	2.9	2.9	3.0	3.1	47
48	2.2	2.2	2.3	2.3	2.4	2.4	2.5	2.6	2.6	2.7	2.8	2.9	3.0	48
49	2.1	2.1	2.2	2.2	2.3	2.3	2.4	2.4	2.5	2.6	2.6	2.7	2.8	49
50	2.0	2.0	2.1	2.1	2.2	2.2	2.3	2.3	2.4	2.4	2.5	2.6	2.6	50
51	1.9	2.0	2.0	2.0	2.1	2.1	2.2	2.2	2.3	2.3	2.4	2.4	2.5	51
52	1.8	1.9	1.9	1.9	2.0	2.0	2.1	2.1	2.1	2.2	2.2	2.3	2.4	52
53	1.8	1.8	1.8	1.9	1.9	1.9	2.0	2.0	2.0	2.1	2.1	2.2	2.2	53
54	1.7	1.7	1.7	1.8	1.8	1.8	1.9	1.9	1.9	2.0	2.0	2.1	2.1	54
55	1.6	1.6	1.7	1.7	1.7	1.8	1.8	1.8	1.9	1.9	1.9	2.0	2.0	55
56	1.5	1.6	1.6	1.6	1.6	1.7	1.7	1.7	1.8	1.8	1.8	1.9	1.9	56
57	1.5	1.5	1.5	1.5	1.6	1.6	1.6	1.6	1.7	1.7	1.7	1.8	1.8	57
58	1.4	1.4	1.5	1.5	1.5	1.5	1.5	1.6	1.6	1.6	1.6	1.7	1.7	58
59	1.4	1.4	1.4	1.4	1.4	1.5	1.5	1.5	1.5	1.5	1.6	1.6	1.6	59
60	1.3	1.3	1.3	1.3	1.4	1.4	1.4	1.4	1.4	1.5	1.5	1.5	1.5	60
	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	24°	
	Declination of the same name as the latitude; upper transit; reduction additive.													

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Latitude.	Declination of the same name as the latitude; upper transit; reduction additive.													Latitude.
	25°	26°	27°	28°	29°	30°	31°	32°	33°	34°	35°	36°	37°	
°	"	"	"	"	"	"	"	"	"	"	"	"	"	°
0	4.2	4.0	3.9	3.7	3.5	3.4	3.3	3.1	3.0	2.9	2.8	2.7	2.6	0
1	4.4	4.2	4.0	3.8	3.7	3.5	3.4	3.2	3.1	3.0	2.9	2.8	2.7	1
2	4.6	4.3	4.1	4.0	3.8	3.6	3.5	3.3	3.2	3.1	3.0	2.8	2.7	2
3	4.7	4.5	4.3	4.1	3.9	3.7	3.6	3.4	3.3	3.2	3.0	2.9	2.8	3
4	5.0	4.7	4.5	4.3	4.1	3.9	3.7	3.5	3.4	3.3	3.1	3.0	2.9	4
5	5.2	4.9	4.7	4.4	4.2	4.0	3.8	3.7	3.5	3.3	3.2	3.1	3.0	5
6	5.4	5.1	4.9	4.6	4.4	4.2	4.0	3.8	3.6	3.5	3.3	3.2	3.0	6
7	5.7	5.4	5.1	4.8	4.6	4.3	4.1	3.9	3.7	3.6	3.4	3.3	3.1	7
8	6.0	5.7	5.3	5.0	4.8	4.5	4.3	4.1	3.9	3.7	3.5	3.4	3.2	8
9	6.4	6.0	5.6	5.3	5.0	4.7	4.4	4.2	4.0	3.8	3.6	3.5	3.3	9
10	6.8	6.3	5.9	5.5	5.2	4.9	4.6	4.4	4.2	3.9	3.8	3.6	3.4	10
11	7.2	6.7	6.2	5.8	5.5	5.1	4.8	4.6	4.3	4.1	3.9	3.7	3.5	11
12	7.7	7.1	6.6	6.2	5.8	5.4	5.1	4.8	4.5	4.3	4.0	3.8	3.6	12
13	8.3	7.6	7.1	6.5	6.1	5.7	5.3	5.0	4.7	4.4	4.2	4.0	3.8	13
14	9.1	8.2	7.6	7.0	6.4	6.0	5.6	5.2	4.9	4.6	4.4	4.1	3.9	14
15	9.9	8.9	8.1	7.4	6.9	6.4	5.9	5.5	5.2	4.8	4.5	4.3	4.0	15
16	10.9	9.8	8.8	8.0	7.3	6.8	6.3	5.8	5.4	5.1	4.8	4.5	4.2	16
17	12.2	10.8	9.6	8.7	7.9	7.2	6.7	6.2	5.7	5.3	5.0	4.7	4.4	17
18	13.9	12.1	10.6	9.5	8.6	7.8	7.1	6.6	6.1	5.6	5.2	4.9	4.6	18
19	16.1	13.7	11.9	10.5	9.4	8.4	7.7	7.0	6.4	6.0	5.5	5.1	4.8	19
20	19.2	15.9	13.5	11.7	10.3	9.2	8.3	7.5	6.9	6.3	5.8	5.4	5.0	20
21	23.8	18.9	15.6	13.3	11.5	10.2	9.1	8.2	7.4	6.8	6.2	5.7	5.3	21
22		23.5	18.6	15.4	13.1	11.3	10.0	8.9	8.0	7.3	6.6	6.1	5.6	22
23			23.1	18.3	15.1	12.8	11.1	9.8	8.7	7.9	7.1	6.5	6.0	23
24				22.7	18.0	14.9	12.6	10.9	9.6	8.6	7.7	7.0	6.4	24
25					22.3	17.7	14.6	12.4	10.7	9.4	8.4	7.5	6.8	25
26						21.9	17.4	14.3	12.1	10.5	9.2	8.2	7.4	26
27							21.5	17.0	14.0	11.9	10.3	9.1	8.1	27
28								21.1	16.7	13.8	11.7	10.1	8.9	28
29	22.3								20.6	16.3	13.5	11.4	9.9	29
30	17.7	21.9								20.2	16.0	13.2	11.1	30
31	14.6	17.4	21.5								19.8	15.6	12.9	31
32	12.4	14.3	17.0	21.1								19.3	15.3	32
33	10.7	12.1	14.0	16.7	20.6								18.9	33
34	9.4	10.5	11.9	13.8	16.3	20.2								34
35	8.4	9.2	10.3	11.7	13.5	16.0	19.8							35
36	7.5	8.2	9.1	10.1	11.4	13.2	15.6	19.3						36
37	6.8	7.4	8.1	8.9	9.9	11.1	12.9	15.3	18.9					37
38	6.2	6.7	7.2	7.9	8.7	9.6	10.9	12.6	14.9	18.4				38
39	5.7	6.1	6.5	7.1	7.7	8.5	9.4	10.6	12.2	14.5	17.9			39
40	5.3	5.6	6.0	6.4	6.9	7.5	8.2	9.2	10.4	11.9	14.1	17.4		40
41	4.9	5.2	5.5	5.8	6.2	6.7	7.3	8.0	8.9	10.1	11.6	13.8	17.0	41
42	4.5	4.8	5.0	5.3	5.7	6.1	6.6	7.1	7.8	8.7	9.8	11.3	13.4	42
43	4.2	4.4	4.6	4.9	5.2	5.5	5.9	6.4	6.9	7.6	8.5	9.5	11.0	43
44	3.9	4.1	4.3	4.5	4.8	5.1	5.4	5.8	6.2	6.7	7.4	8.2	9.3	44
45	3.7	3.8	4.0	4.2	4.4	4.7	4.9	5.2	5.6	6.0	6.6	7.2	8.0	45
46	3.5	3.6	3.7	3.9	4.1	4.3	4.5	4.8	5.1	5.4	5.9	6.4	7.0	46
47	3.3	3.4	3.5	3.6	3.8	4.0	4.2	4.4	4.6	4.9	5.3	5.7	6.2	47
48	3.1	3.2	3.3	3.4	3.5	3.7	3.9	4.0	4.3	4.5	4.8	5.1	5.5	48
49	2.9	3.0	3.1	3.2	3.3	3.4	3.6	3.7	3.9	4.1	4.4	4.6	5.0	49
50	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.5	3.6	3.8	4.0	4.2	4.5	50
51	2.6	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.4	3.5	3.7	3.9	4.1	51
52	2.4	2.5	2.6	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.4	3.6	3.7	52
53	2.3	2.3	2.4	2.5	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.3	3.4	53
54	2.2	2.2	2.3	2.3	2.4	2.5	2.5	2.6	2.7	2.8	2.9	3.0	3.2	54
55	2.0	2.1	2.1	2.2	2.3	2.3	2.4	2.4	2.5	2.6	2.7	2.8	2.9	55
56	1.9	2.0	2.0	2.1	2.1	2.2	2.2	2.3	2.4	2.4	2.5	2.6	2.7	56
57	1.8	1.9	1.9	2.0	2.0	2.0	2.1	2.2	2.2	2.3	2.3	2.4	2.5	57
58	1.7	1.8	1.8	1.8	1.9	1.9	2.0	2.0	2.1	2.1	2.2	2.3	2.3	58
59	1.6	1.7	1.7	1.7	1.8	1.8	1.9	1.9	1.9	2.0	2.0	2.1	2.2	59
60	1.6	1.6	1.6	1.6	1.7	1.7	1.7	1.8	1.8	1.9	1.9	2.0	2.0	60
	25°	26°	27°	28°	29°	30°	31°	32°	33°	34°	35°	36°	37°	
	Declination of the same name as the latitude; upper transit; reduction additive.													

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Latitude.	Declination of the same name as the latitude; upper transit; reduction additive.													Latitude.
	38°	39°	40°	41°	42°	43°	44°	45°	46°	47°	48°	49°	50°	
°	"	"	"	"	"	"	"	"	"	"	"	"	"	°
0	2.5	2.4	2.3	2.3	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.7	1.7	0
1	2.6	2.5	2.4	2.3	2.2	2.2	2.1	2.0	1.9	1.9	1.8	1.7	1.7	1
2	2.6	2.5	2.4	2.4	2.3	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.7	2
3	2.7	2.6	2.5	2.4	2.3	2.2	2.2	2.1	2.0	1.9	1.9	1.8	1.7	3
4	2.8	2.7	2.6	2.5	2.4	2.3	2.2	2.1	2.0	2.0	1.9	1.8	1.8	4
5	2.8	2.7	2.6	2.5	2.4	2.3	2.2	2.2	2.1	2.0	1.9	1.9	1.8	5
6	2.9	2.8	2.7	2.6	2.5	2.4	2.3	2.2	2.1	2.0	2.0	1.9	1.8	6
7	3.0	2.9	2.7	2.6	2.5	2.4	2.3	2.2	2.2	2.1	2.0	1.9	1.8	7
8	3.1	2.9	2.8	2.7	2.6	2.5	2.4	2.3	2.2	2.1	2.0	1.9	1.9	8
9	3.2	3.0	2.9	2.8	2.7	2.5	2.4	2.3	2.2	2.2	2.1	2.0	1.9	9
10	3.3	3.1	3.0	2.8	2.7	2.6	2.5	2.4	2.3	2.2	2.1	2.0	1.9	10
11	3.4	3.2	3.1	2.9	2.8	2.7	2.6	2.4	2.3	2.2	2.1	2.1	2.0	11
12	3.5	3.3	3.1	3.0	2.9	2.7	2.6	2.5	2.4	2.3	2.2	2.1	2.0	12
13	3.6	3.4	3.2	3.1	2.9	2.8	2.7	2.6	2.4	2.3	2.2	2.1	2.0	13
14	3.7	3.5	3.3	3.2	3.0	2.9	2.7	2.6	2.5	2.4	2.3	2.2	2.1	14
15	3.8	3.6	3.4	3.3	3.1	3.0	2.8	2.7	2.6	2.4	2.3	2.2	2.1	15
16	4.0	3.8	3.6	3.4	3.2	3.0	2.9	2.8	2.6	2.5	2.4	2.3	2.2	16
17	4.1	3.9	3.7	3.5	3.3	3.1	3.0	2.8	2.7	2.6	2.4	2.3	2.2	17
18	4.3	4.1	3.8	3.6	3.4	3.2	3.1	2.9	2.8	2.6	2.5	2.4	2.3	18
19	4.5	4.2	4.0	3.7	3.5	3.3	3.2	3.0	2.8	2.7	2.6	2.4	2.3	19
20	4.7	4.4	4.1	3.9	3.7	3.5	3.3	3.1	2.9	2.8	2.6	2.5	2.4	20
21	4.9	4.6	4.3	4.0	3.8	3.6	3.4	3.2	3.0	2.9	2.7	2.6	2.4	21
22	5.2	4.8	4.5	4.2	4.0	3.7	3.5	3.3	3.1	2.9	2.8	2.6	2.5	22
23	5.5	5.1	4.7	4.4	4.1	3.9	3.6	3.4	3.2	3.0	2.9	2.7	2.6	23
24	5.8	5.4	5.0	4.6	4.3	4.0	3.8	3.5	3.3	3.1	3.0	2.8	2.6	24
25	6.2	5.7	5.3	4.9	4.5	4.2	3.9	3.7	3.5	3.3	3.1	2.9	2.7	25
26	6.7	6.1	5.6	5.2	4.8	4.4	4.1	3.8	3.6	3.4	3.2	3.0	2.8	26
27	7.2	6.5	6.0	5.5	5.0	4.6	4.3	4.0	3.7	3.5	3.3	3.1	2.9	27
28	7.9	7.1	6.4	5.8	5.3	4.9	4.5	4.2	3.9	3.6	3.4	3.2	3.0	28
29	8.7	7.7	6.9	6.2	5.7	5.2	4.8	4.4	4.1	3.8	3.5	3.3	3.1	29
30	9.6	8.5	7.5	6.7	6.1	5.5	5.1	4.7	4.3	4.0	3.7	3.4	3.2	30
31	10.9	9.4	8.2	7.3	6.6	5.9	5.4	4.9	4.5	4.2	3.9	3.6	3.3	31
32	12.6	10.6	9.2	8.0	7.1	6.4	5.8	5.2	4.8	4.4	4.0	3.7	3.5	32
33	14.9	12.2	10.4	8.9	7.8	6.9	6.2	5.6	5.1	4.6	4.3	3.9	3.6	33
34	18.4	14.5	11.9	10.1	8.7	7.6	6.7	6.0	5.4	4.9	4.5	4.1	3.8	34
35		17.9	14.1	11.6	9.8	8.5	7.4	6.6	5.9	5.3	4.8	4.4	4.0	35
36			17.4	13.8	11.3	9.5	8.2	7.2	6.4	5.7	5.1	4.6	4.2	36
37				17.0	13.4	11.0	9.3	8.0	7.0	6.2	5.5	5.0	4.5	37
38					16.5	13.0	10.7	9.0	7.7	6.8	6.0	5.3	4.8	38
39						16.0	12.6	10.3	8.7	7.5	6.5	5.8	5.1	39
40							15.5	12.2	10.0	8.4	7.2	6.3	5.6	40
41								15.0	11.8	9.7	8.1	7.0	6.1	41
42	16.5								14.5	11.4	9.3	7.9	6.7	42
43	13.0	16.0								14.0	11.0	9.0	7.6	43
44	10.7	12.6	15.5								13.6	10.6	8.7	44
45	9.0	10.3	12.2	15.0								13.1	10.2	45
46	7.7	8.7	10.0	11.8	14.5								12.6	46
47	6.8	7.5	8.4	9.7	11.4	14.0								47
48	6.0	6.5	7.2	8.1	9.3	11.0	13.6							48
49	5.3	5.8	6.3	7.0	7.9	9.0	10.6	13.1						49
50	4.8	5.1	5.6	6.1	6.7	7.6	8.7	10.2	12.6					50
51	4.3	4.6	5.0	5.4	5.9	6.5	7.3	8.4	9.9	12.1				51
52	3.9	4.2	4.5	4.8	5.2	5.7	6.3	7.0	8.0	9.5	11.6			52
53	3.6	3.8	4.0	4.3	4.6	5.0	5.4	6.0	6.7	7.7	9.1	11.1		53
54	3.3	3.5	3.7	3.9	4.1	4.4	4.8	5.2	5.8	6.5	7.4	8.7	10.6	54
55	3.0	3.2	3.3	3.5	3.7	4.0	4.3	4.6	5.0	5.5	6.2	7.1	8.3	55
56	2.8	2.9	3.1	3.2	3.4	3.6	3.8	4.1	4.4	4.8	5.3	5.9	6.8	56
57	2.6	2.7	2.8	2.9	3.1	3.2	3.4	3.6	3.9	4.2	4.6	5.0	5.6	57
58	2.4	2.5	2.6	2.7	2.8	2.9	3.1	3.3	3.5	3.7	4.0	4.4	4.8	58
59	2.2	2.3	2.4	2.5	2.6	2.7	2.8	3.0	3.1	3.3	3.6	3.8	4.2	59
60	2.1	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	3.0	3.2	3.4	3.6	60
	38°	39°	40°	41°	42°	43°	44°	45°	46°	47°	48°	49°	50°	
	Declination of the same name as the latitude; upper transit; reduction additive.													

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Latitude.	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°	61°	62°	63°	Latitude.
	Declination of the same name as the latitude; upper transit; reduction additive.													
°	"	"	"	"	"	"	"	"	"	"	"	"	"	°
0	1.6	1.5	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.0	1.0	0
1	1.6	1.6	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.2	1.1	1.1	1.0	1
2	1.6	1.6	1.5	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.0	2
3	1.7	1.6	1.5	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.0	3
4	1.7	1.6	1.6	1.5	1.5	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.0	4
5	1.7	1.7	1.6	1.5	1.5	1.4	1.4	1.3	1.3	1.2	1.1	1.1	1.1	5
6	1.7	1.7	1.6	1.5	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	6
7	1.8	1.7	1.6	1.6	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	7
8	1.8	1.7	1.7	1.6	1.5	1.5	1.4	1.4	1.3	1.2	1.2	1.1	1.1	8
9	1.8	1.8	1.7	1.6	1.6	1.5	1.4	1.4	1.3	1.3	1.2	1.1	1.1	9
10	1.9	1.8	1.7	1.6	1.6	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	10
11	1.9	1.8	1.7	1.7	1.6	1.5	1.5	1.4	1.3	1.3	1.2	1.2	1.1	11
12	1.9	1.8	1.8	1.7	1.6	1.6	1.5	1.4	1.4	1.3	1.2	1.2	1.1	12
13	2.0	1.9	1.8	1.7	1.6	1.6	1.5	1.4	1.4	1.3	1.3	1.2	1.1	13
14	2.0	1.9	1.8	1.7	1.7	1.6	1.5	1.5	1.4	1.3	1.3	1.2	1.2	14
15	2.0	1.9	1.9	1.8	1.7	1.6	1.5	1.5	1.4	1.3	1.3	1.2	1.2	15
16	2.1	2.0	1.9	1.8	1.7	1.6	1.6	1.5	1.4	1.4	1.3	1.2	1.2	16
17	2.1	2.0	1.9	1.8	1.8	1.7	1.6	1.5	1.5	1.4	1.3	1.3	1.2	17
18	2.2	2.1	2.0	1.9	1.8	1.7	1.6	1.5	1.5	1.4	1.3	1.3	1.2	18
19	2.2	2.1	2.0	1.9	1.8	1.7	1.6	1.6	1.5	1.4	1.4	1.3	1.2	19
20	2.3	2.1	2.0	1.9	1.9	1.8	1.7	1.6	1.5	1.4	1.4	1.3	1.2	20
21	2.3	2.2	2.1	2.0	1.9	1.8	1.7	1.6	1.5	1.5	1.4	1.3	1.2	21
22	2.4	2.2	2.1	2.0	1.9	1.8	1.7	1.6	1.6	1.5	1.4	1.3	1.3	22
23	2.4	2.3	2.2	2.1	2.0	1.9	1.8	1.7	1.6	1.5	1.4	1.4	1.3	23
24	2.5	2.4	2.2	2.1	2.0	1.9	1.8	1.7	1.6	1.5	1.5	1.4	1.3	24
25	2.6	2.4	2.3	2.2	2.0	1.9	1.8	1.7	1.6	1.6	1.5	1.4	1.3	25
26	2.6	2.5	2.3	2.2	2.1	2.0	1.9	1.8	1.7	1.6	1.5	1.4	1.3	26
27	2.7	2.6	2.4	2.3	2.1	2.0	1.9	1.8	1.7	1.6	1.5	1.4	1.4	27
28	2.8	2.6	2.5	2.3	2.2	2.1	2.0	1.8	1.7	1.6	1.5	1.5	1.4	28
29	2.9	2.7	2.5	2.4	2.3	2.1	2.0	1.9	1.8	1.7	1.6	1.5	1.4	29
30	3.0	2.8	2.6	2.5	2.3	2.2	2.0	1.9	1.8	1.7	1.6	1.5	1.4	30
31	3.1	2.9	2.7	2.5	2.4	2.2	2.1	2.0	1.9	1.7	1.6	1.5	1.4	31
32	3.2	3.0	2.8	2.6	2.4	2.3	2.2	2.0	1.9	1.8	1.7	1.6	1.5	32
33	3.4	3.1	2.9	2.7	2.5	2.4	2.2	2.1	1.9	1.8	1.7	1.6	1.5	33
34	3.5	3.2	3.0	2.8	2.6	2.4	2.3	2.1	2.0	1.9	1.7	1.6	1.5	34
35	3.7	3.4	3.1	2.9	2.7	2.5	2.3	2.2	2.0	1.9	1.8	1.7	1.6	35
36	3.9	3.6	3.3	3.0	2.8	2.6	2.4	2.3	2.1	2.0	1.8	1.7	1.6	36
37	4.1	3.7	3.4	3.2	2.9	2.7	2.5	2.3	2.2	2.0	1.9	1.7	1.6	37
38	4.3	3.9	3.6	3.3	3.0	2.8	2.6	2.4	2.2	2.1	1.9	1.8	1.7	38
39	4.6	4.2	3.8	3.5	3.2	2.9	2.7	2.5	2.3	2.1	2.0	1.8	1.7	39
40	5.0	4.5	4.0	3.7	3.3	3.1	2.8	2.6	2.4	2.2	2.0	1.9	1.8	40
41	5.4	4.8	4.3	3.9	3.5	3.2	2.9	2.7	2.5	2.3	2.1	1.9	1.8	41
42	5.9	5.2	4.6	4.1	3.7	3.4	3.1	2.8	2.6	2.4	2.2	2.0	1.9	42
43	6.5	5.7	5.0	4.4	4.0	3.6	3.2	2.9	2.7	2.5	2.3	2.1	1.9	43
44	7.3	6.3	5.4	4.8	4.3	3.8	3.4	3.1	2.8	2.6	2.3	2.2	2.0	44
45	8.4	7.0	6.0	5.2	4.6	4.1	3.6	3.3	3.0	2.7	2.4	2.2	2.0	45
46	9.9	8.0	6.7	5.8	5.0	4.4	3.9	3.5	3.1	2.8	2.6	2.3	2.1	46
47	12.1	9.5	7.7	6.5	5.5	4.8	4.2	3.7	3.3	3.0	2.7	2.4	2.2	47
48		11.6	9.1	7.4	6.2	5.3	4.6	4.0	3.6	3.2	2.8	2.6	2.3	48
49			11.1	8.7	7.1	5.9	5.0	4.4	3.8	3.4	3.0	2.7	2.4	49
50				10.6	8.3	6.8	5.6	4.8	4.2	3.6	3.2	2.9	2.6	50
51					10.2	7.9	6.4	5.4	4.6	4.0	3.5	3.0	2.7	51
52						9.7	7.6	6.1	5.1	4.3	3.8	3.3	2.9	52
53							9.2	7.2	5.9	4.9	4.1	3.6	3.1	53
54								8.8	6.8	5.5	4.6	3.9	3.4	54
55	10.2								8.3	6.5	5.3	4.3	3.7	55
56	7.9	9.7								7.9	6.1	5.0	4.1	56
57	6.4	7.6	9.2								7.4	5.8	4.7	57
58	5.4	6.1	7.2	8.8								7.0	5.4	58
59	4.6	5.1	5.9	6.8	8.3								6.6	59
60	4.0	4.3	4.9	5.5	6.5	7.9								60
	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°	61°	62°	63°	
	Declination of the same name as the latitude; upper transit; reduction additive.													

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Latitude.	Declination of a different name from the latitude; upper transit; reduction additive.												Latitude.
	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	
°	"	"	"	"	"	"	"	"	"	"	"	"	°
0					28.1	22.4	18.7	16.0	14.0	12.4	11.1	10.1	0
1				28.1	22.4	18.7	16.0	14.0	12.4	11.2	10.1	9.3	1
2			28.1	22.4	18.7	16.0	14.0	12.5	11.2	10.2	9.3	8.6	2
3		28.1	22.4	18.7	16.0	14.0	12.5	11.2	10.2	9.3	8.6	8.0	3
4	28.1	22.4	18.7	16.0	14.0	12.5	11.2	10.2	9.3	8.6	8.0	7.4	4
5	22.4	18.7	16.0	14.0	12.5	11.2	10.2	9.3	8.6	8.0	7.4	7.0	5
6	18.7	16.0	14.0	12.5	11.2	10.2	9.3	8.6	8.0	7.5	7.0	6.6	6
7	16.0	14.0	12.4	11.2	10.2	9.3	8.6	8.0	7.5	7.0	6.6	6.2	7
8	14.0	12.4	11.2	10.2	9.3	8.6	8.0	7.5	7.0	6.6	6.2	5.9	8
9	12.4	11.2	10.2	9.3	8.6	8.0	7.5	7.0	6.6	6.2	5.9	5.6	9
10	11.1	10.1	9.3	8.6	8.0	7.4	7.0	6.6	6.2	5.9	5.6	5.3	10
11	10.1	9.3	8.6	8.0	7.4	7.0	6.6	6.2	5.9	5.6	5.3	5.1	11
12	9.2	8.5	7.9	7.4	7.0	6.5	6.2	5.9	5.6	5.3	5.0	4.8	12
13	8.5	7.9	7.4	6.9	6.5	6.2	5.8	5.6	5.3	5.0	4.8	4.6	13
14	7.9	7.4	6.9	6.5	6.2	5.8	5.5	5.3	5.0	4.8	4.6	4.4	14
15	7.3	6.9	6.5	6.1	5.8	5.5	5.3	5.0	4.8	4.6	4.4	4.2	15
16	6.8	6.5	6.1	5.8	5.5	5.2	5.0	4.8	4.6	4.4	4.2	4.1	16
17	6.4	6.1	5.8	5.5	5.2	5.0	4.8	4.6	4.4	4.2	4.1	3.9	17
18	6.0	5.7	5.5	5.2	5.0	4.8	4.6	4.4	4.2	4.1	3.9	3.8	18
19	5.7	5.4	5.2	4.9	4.7	4.5	4.4	4.2	4.0	3.9	3.8	3.6	19
20	5.4	5.1	4.9	4.7	4.5	4.3	4.2	4.0	3.9	3.8	3.6	3.5	20
21	5.1	4.9	4.7	4.5	4.3	4.2	4.0	3.9	3.7	3.6	3.5	3.4	21
22	4.9	4.7	4.5	4.3	4.1	4.0	3.9	3.7	3.6	3.5	3.4	3.3	22
23	4.6	4.4	4.3	4.1	4.0	3.8	3.7	3.6	3.5	3.4	3.3	3.2	23
24	4.4	4.2	4.1	3.9	3.8	3.7	3.6	3.5	3.4	3.3	3.2	3.1	24
25	4.2	4.1	3.9	3.8	3.7	3.5	3.4	3.3	3.2	3.1	3.1	3.0	25
26	4.0	3.9	3.8	3.6	3.5	3.4	3.3	3.2	3.1	3.0	3.0	2.9	26
27	3.9	3.7	3.6	3.5	3.4	3.3	3.2	3.1	3.0	2.9	2.9	2.8	27
28	3.7	3.6	3.5	3.4	3.3	3.2	3.1	3.0	2.9	2.8	2.8	2.7	28
29	3.5	3.4	3.3	3.2	3.1	3.1	3.0	2.9	2.8	2.8	2.7	2.6	29
30	3.4	3.3	3.2	3.1	3.0	3.0	2.9	2.8	2.7	2.7	2.6	2.5	30
31	3.3	3.2	3.1	3.0	2.9	2.9	2.8	2.7	2.6	2.6	2.5	2.5	31
32	3.2	3.1	3.0	2.9	2.8	2.8	2.7	2.6	2.6	2.5	2.5	2.4	32
33	3.0	2.9	2.9	2.8	2.7	2.7	2.6	2.5	2.5	2.4	2.4	2.3	33
34	2.9	2.8	2.8	2.7	2.6	2.6	2.5	2.5	2.4	2.4	2.3	2.3	34
35	2.8	2.7	2.7	2.6	2.5	2.5	2.4	2.4	2.3	2.3	2.2	2.2	35
36	2.7	2.6	2.6	2.5	2.5	2.4	2.4	2.3	2.3	2.2	2.2	2.1	36
37	2.6	2.5	2.5	2.4	2.4	2.3	2.3	2.2	2.2	2.2	2.1	2.1	37
38	2.5	2.5	2.4	2.4	2.3	2.3	2.2	2.2	2.1	2.1	2.1	2.0	38
39	2.4	2.4	2.3	2.3	2.2	2.2	2.1	2.1	2.1	2.0	2.0	2.0	39
40	2.3	2.3	2.2	2.2	2.2	2.1	2.1	2.0	2.0	2.0	1.9	1.9	40
41	2.3	2.2	2.2	2.1	2.1	2.1	2.0	2.0	1.9	1.9	1.9	1.8	41
42	2.2	2.1	2.1	2.1	2.0	2.0	2.0	1.9	1.9	1.9	1.8	1.8	42
43	2.1	2.1	2.0	2.0	2.0	1.9	1.9	1.9	1.8	1.8	1.8	1.7	43
44	2.0	2.0	2.0	1.9	1.9	1.9	1.8	1.8	1.8	1.7	1.7	1.7	44
45	2.0	1.9	1.9	1.9	1.8	1.8	1.8	1.7	1.7	1.7	1.7	1.6	45
46	1.9	1.9	1.8	1.8	1.8	1.7	1.7	1.7	1.7	1.6	1.6	1.6	46
47	1.8	1.8	1.8	1.7	1.7	1.7	1.7	1.6	1.6	1.6	1.6	1.6	47
48	1.8	1.7	1.7	1.7	1.7	1.6	1.6	1.6	1.6	1.6	1.5	1.5	48
49	1.7	1.7	1.7	1.6	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.5	49
50	1.6	1.6	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.5	1.4	1.4	50
51	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	51
52	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	1.4	1.4	1.3	52
53	1.5	1.5	1.4	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.3	53
54	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.3	1.3	1.3	54
55	1.4	1.4	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.2	55
56	1.3	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.2	56
57	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1.1	57
58	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	1.1	58
59	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	59
60	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.0	1 0	1.0	1.0	60
	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	
	Declination of a different name from the latitude; upper transit; reduction additive.												

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Latitude.	Declination of a different name from the latitude; upper transit; reduction additive.													Latitude.
	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	24°	
°	″	″	″	″	″	″	″	″	″	″	″	″	″	°
0	9.2	8.5	7.9	7.3	6.8	6.4	6.0	5.7	5.4	5.1	4.9	4.6	4.4	0
1	8.5	7.9	7.4	6.9	6.5	6.1	5.7	5.4	5.1	4.9	4.7	4.4	4.2	1
2	7.9	7.4	6.9	6.5	6.1	5.8	5.5	5.2	4.9	4.7	4.5	4.3	4.1	2
3	7.4	6.9	6.5	6.1	5.8	5.5	5.2	4.9	4.7	4.5	4.3	4.1	3.9	3
4	7.0	6.5	6.2	5.8	5.5	5.2	5.0	4.7	4.5	4.3	4.1	4.0	3.8	4
5	6.5	6.2	5.8	5.5	5.2	5.0	4.8	4.5	4.3	4.2	4.0	3.8	3.7	5
6	6.2	5.8	5.5	5.3	5.0	4.8	4.6	4.4	4.2	4.0	3.9	3.7	3.6	6
7	5.9	5.6	5.3	5.0	4.8	4.6	4.4	4.2	4.0	3.9	3.7	3.6	3.5	7
8	5.6	5.3	5.0	4.8	4.6	4.4	4.2	4.0	3.9	3.7	3.6	3.5	3.4	8
9	5.3	5.0	4.8	4.6	4.4	4.2	4.1	3.9	3.8	3.6	3.5	3.4	3.3	9
10	5.0	4.8	4.6	4.4	4.2	4.1	3.9	3.8	3.6	3.5	3.4	3.3	3.2	10
11	4.8	4.6	4.4	4.2	4.1	3.9	3.8	3.6	3.5	3.4	3.3	3.2	3.1	11
12	4.6	4.4	4.3	4.1	3.9	3.8	3.7	3.5	3.4	3.3	3.2	3.1	3.0	12
13	4.4	4.3	4.1	3.9	3.8	3.7	3.5	3.4	3.3	3.2	3.1	3.0	2.9	13
14	4.2	4.1	3.9	3.8	3.7	3.5	3.4	3.3	3.2	3.1	3.0	2.9	2.8	14
15	4.1	3.9	3.8	3.7	3.5	3.4	3.3	3.2	3.1	3.0	2.9	2.8	2.8	15
16	3.9	3.8	3.7	3.5	3.4	3.3	3.2	3.1	3.0	2.9	2.8	2.8	2.7	16
17	3.8	3.7	3.5	3.4	3.3	3.2	3.1	3.0	2.9	2.8	2.8	2.7	2.6	17
18	3.7	3.5	3.4	3.3	3.2	3.1	3.0	2.9	2.9	2.8	2.7	2.6	2.5	18
19	3.5	3.4	3.3	3.2	3.1	3.0	2.9	2.9	2.8	2.7	2.6	2.6	2.5	19
20	3.4	3.3	3.2	3.1	3.0	2.9	2.9	2.8	2.7	2.6	2.6	2.5	2.4	20
21	3.3	3.2	3.1	3.0	2.9	2.8	2.8	2.7	2.6	2.6	2.5	2.4	2.4	21
22	3.2	3.1	3.0	2.9	2.8	2.8	2.7	2.6	2.6	2.5	2.4	2.4	2.3	22
23	3.1	3.0	2.9	2.8	2.8	2.7	2.6	2.6	2.5	2.4	2.4	2.3	2.3	23
24	3.0	2.9	2.8	2.8	2.7	2.6	2.5	2.5	2.4	2.4	2.3	2.3	2.2	24
25	2.9	2.8	2.7	2.7	2.6	2.5	2.5	2.4	2.4	2.3	2.3	2.2	2.2	25
26	2.8	2.7	2.7	2.6	2.5	2.5	2.4	2.4	2.3	2.3	2.2	2.1	2.1	26
27	2.7	2.7	2.6	2.5	2.5	2.4	2.4	2.3	2.2	2.2	2.1	2.1	2.1	27
28	2.6	2.6	2.5	2.5	2.4	2.3	2.3	2.2	2.2	2.1	2.1	2.1	2.0	28
29	2.6	2.5	2.4	2.4	2.3	2.3	2.2	2.2	2.1	2.1	2.0	2.0	2.0	29
30	2.5	2.4	2.4	2.3	2.3	2.2	2.2	2.1	2.1	2.0	2.0	2.0	1.9	30
31	2.4	2.4	2.3	2.3	2.2	2.2	2.1	2.1	2.0	2.0	2.0	1.9	1.9	31
32	2.3	2.3	2.2	2.2	2.2	2.1	2.1	2.0	2.0	1.9	1.9	1.9	1.8	32
33	2.3	2.2	2.2	2.1	2.1	2.1	2.0	2.0	1.9	1.9	1.9	1.8	1.8	33
34	2.2	2.2	2.1	2.1	2.0	2.0	2.0	1.9	1.9	1.9	1.8	1.8	1.8	34
35	2.2	2.1	2.1	2.0	2.0	2.0	1.9	1.9	1.8	1.8	1.8	1.7	1.7	35
36	2.1	2.1	2.0	2.0	1.9	1.9	1.9	1.8	1.8	1.8	1.7	1.7	1.7	36
37	2.0	2.0	2.0	1.9	1.9	1.9	1.8	1.8	1.8	1.7	1.7	1.7	1.6	37
38	2.0	1.9	1.9	1.9	1.8	1.8	1.8	1.8	1.7	1.7	1.7	1.6	1.6	38
39	1.9	1.9	1.9	1.8	1.8	1.8	1.7	1.7	1.7	1.6	1.6	1.6	1.6	39
40	1.9	1.8	1.8	1.8	1.7	1.7	1.7	1.7	1.6	1.6	1.6	1.6	1.5	40
41	1.8	1.8	1.8	1.7	1.7	1.7	1.6	1.6	1.6	1.6	1.5	1.5	1.5	41
42	1.8	1.7	1.7	1.7	1.7	1.6	1.6	1.6	1.6	1.5	1.5	1.5	1.5	42
43	1.7	1.7	1.7	1.6	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.4	1.4	43
44	1.7	1.6	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	44
45	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	1.4	45
46	1.6	1.6	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	1.4	1.3	1.3	46
47	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.3	47
48	1.5	1.5	1.4	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.3	48
49	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.3	1.3	1.2	1.2	49
50	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.2	50
51	1.4	1.3	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.2	51
52	1.3	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.1	1.1	52
53	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1	53
54	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	1.1	1.1	54
55	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	55
56	1.2	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.0	1.0	1.0	56
57	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.0	1.0	1.0	1.0	1.0	1.0	57
58	1.1	1.1	1.1	1.1	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	58
59	1.1	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.9	0.9	59
60	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.9	0.9	0.9	0.9	0.9	0.9	60
	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	24°	
	Declination of a different name from the latitude; upper transit; reduction additive.													

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Latitude.	Declination of a different name from the latitude; upper transit; reduction additive.													Latitude.
	25°	26°	27°	28°	29°	30°	31°	32°	33°	34°	35°	36°	37°	
°	″	″	″	″	″	″	″	″	″	″	″	″	″	°
0	4.2	4.0	3.9	3.7	3.5	3.4	3.3	3.1	3.0	2.9	2.8	2.7	2.6	0
1	4.1	3.9	3.7	3.6	3.4	3.3	3.2	3.1	2.9	2.8	2.7	2.6	2.6	1
2	3.9	3.8	3.6	3.5	3.3	3.2	3.1	3.0	2.9	2.8	2.7	2.6	2.5	2
3	3.8	3.6	3.5	3.4	3.2	3.1	3.0	2.9	2.8	2.7	2.6	2.5	2.4	3
4	3.7	3.5	3.4	3.3	3.2	3.0	2.9	2.8	2.7	2.6	2.6	2.5	2.4	4
5	3.6	3.4	3.3	3.2	3.1	3.0	2.9	2.8	2.7	2.6	2.5	2.4	2.3	5
6	3.4	3.3	3.2	3.1	3.0	2.9	2.8	2.7	2.6	2.5	2.4	2.4	2.3	6
7	3.3	3.2	3.1	3.0	2.9	2.8	2.7	2.6	2.5	2.5	2.4	2.3	2.2	7
8	3.2	3.1	3.0	2.9	2.8	2.7	2.7	2.6	2.5	2.4	2.3	2.3	2.2	8
9	3.1	3.0	2.9	2.9	2.8	2.7	2.6	2.5	2.4	2.4	2.3	2.2	2.2	9
10	3.1	3.0	2.9	2.8	2.7	2.6	2.5	2.5	2.4	2.3	2.2	2.2	2.1	10
11	3.0	2.9	2.8	2.7	2.6	2.5	2.5	2.4	2.3	2.3	2.2	2.1	2.1	11
12	2.9	2.8	2.7	2.6	2.6	2.5	2.4	2.3	2.3	2.2	2.2	2.1	2.0	12
13	2.8	2.7	2.7	2.6	2.5	2.4	2.4	2.3	2.2	2.2	2.1	2.1	2.0	13
14	2.7	2.7	2.6	2.5	2.4	2.4	2.3	2.3	2.2	2.1	2.1	2.0	2.0	14
15	2.7	2.6	2.5	2.5	2.4	2.3	2.3	2.2	2.1	2.1	2.0	2.0	1.9	15
16	2.6	2.5	2.5	2.4	2.3	2.3	2.2	2.2	2.1	2.0	2.0	1.9	1.9	16
17	2.5	2.5	2.4	2.3	2.3	2.2	2.2	2.1	2.1	2.0	2.0	1.9	1.9	17
18	2.5	2.4	2.4	2.3	2.2	2.2	2.1	2.1	2.0	2.0	1.9	1.9	1.8	18
19	2.4	2.4	2.3	2.2	2.2	2.1	2.1	2.0	2.0	1.9	1.9	1.8	1.8	19
20	2.4	2.3	2.3	2.2	2.1	2.1	2.0	2.0	1.9	1.9	1.9	1.8	1.8	20
21	2.3	2.3	2.2	2.1	2.1	2.0	2.0	2.0	1.9	1.9	1.8	1.8	1.7	21
22	2.3	2.2	2.2	2.1	2.1	2.0	2.0	1.9	1.9	1.8	1.8	1.7	1.7	22
23	2.2	2.2	2.1	2.1	2.0	2.0	1.9	1.9	1.8	1.8	1.8	1.7	1.7	23
24	2.2	2.1	2.1	2.0	2.0	1.9	1.9	1.8	1.8	1.8	1.7	1.7	1.6	24
25	2.1	2.1	2.0	2.0	1.9	1.9	1.8	1.8	1.8	1.7	1.7	1.6	1.6	25
26	2.1	2.0	2.0	1.9	1.9	1.9	1.8	1.8	1.7	1.7	1.7	1.6	1.6	26
27	2.0	2.0	1.9	1.9	1.9	1.8	1.8	1.7	1.7	1.7	1.6	1.6	1.6	27
28	2.0	1.9	1.9	1.9	1.8	1.8	1.7	1.7	1.7	1.6	1.6	1.6	1.5	28
29	1.9	1.9	1.9	1.8	1.8	1.7	1.7	1.7	1.6	1.6	1.6	1.5	1.5	29
30	1.9	1.8	1.8	1.8	1.7	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.5	30
31	1.8	1.8	1.8	1.7	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.5	1.5	31
32	1.8	1.8	1.7	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.4	32
33	1.8	1.7	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.4	1.4	33
34	1.7	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.4	1.4	1.4	34
35	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	35
36	1.6	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	1.3	36
37	1.6	1.6	1.6	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	1.3	1.3	37
38	1.6	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	1.3	1.3	1.3	38
39	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.3	39
40	1.5	1.5	1.5	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.3	1.2	40
41	1.5	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.3	1.2	1.2	41
42	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	42
43	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	43
44	1.4	1.4	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.2	44
45	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1.1	45
46	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1	46
47	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	1.1	47
48	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	1.1	1.1		48
49	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	1.1	1.1			49
50	1.2	1.2	1.2	1.1	1.1	1.1	1.1	1.1	1.1	1.1				50
51	1.2	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.0					51
52	1.1	1.1	1.1	1.1	1.1	1.1	1.0	1.0						52
53	1.1	1.1	1.1	1.1	1.0	1.0	1.0							53
54	1.1	1.0	1.0	1.0	1.0	1.0								54
55	1.0	1.0	1.0	1.0	1.0									55
56	1.0	1.0	1.0	1.0										56
57	1.0	1.0	1.0											57
58	1.0	0.9												58
59	0.9												0.8	59
60												0.8	0.8	60
	25°	26°	27°	28°	29°	30°	31°	32°	33°	34°	35°	36°	37°	
	Declination of the same name as the latitude; lower transit; reduction subtractive.													

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Lati-tude.	38°	39°	40°	41°	42°	43°	44°	45°	46°	47°	48°	49°	50°	Lati-tude.
	Declination of a different name from the latitude; upper transit; reduction additive.													
°	"	"	"	"	"	"	"	"	"	"	"	"	"	°
0	2.5	2.4	2.3	2.3	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.7	1.7	0
1	2.5	2.4	2.3	2.2	2.1	2.1	2.0	1.9	1.9	1.8	1.7	1.7	1.6	1
2	2.4	2.3	2.3	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.7	1.7	1.6	2
3	2.4	2.3	2.2	2.1	2.1	2.0	1.9	1.9	1.8	1.8	1.7	1.7	1.6	3
4	2.3	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.7	1.7	1.6	1.6	4
5	2.3	2.2	2.1	2.1	2.0	1.9	1.9	1.8	1.8	1.7	1.6	1.6	1.5	5
6	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.7	1.7	1.6	1.6	1.5	6
7	2.2	2.1	2.0	2.0	1.9	1.9	1.8	1.8	1.7	1.6	1.6	1.5	1.5	7
8	2.1	2.1	2.0	1.9	1.9	1.8	1.8	1.7	1.7	1.6	1.6	1.5	1.5	8
9	2.1	2.0	2.0	1.9	1.9	1.8	1.8	1.7	1.6	1.6	1.6	1.5	1.5	9
10	2.1	2.0	1.9	1.9	1.8	1.8	1.7	1.7	1.6	1.6	1.5	1.5	1.4	10
11	2.0	2.0	1.9	1.8	1.8	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.4	11
12	2.0	1.9	1.9	1.8	1.8	1.7	1.7	1.6	1.6	1.5	1.5	1.4	1.4	12
13	1.9	1.9	1.8	1.8	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.4	1.4	13
14	1.9	1.9	1.8	1.8	1.7	1.7	1.6	1.6	1.5	1.5	1.4	1.4	1.4	14
15	1.9	1.8	1.8	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.4	1.4	1.4	15
16	1.8	1.8	1.7	1.7	1.7	1.6	1.6	1.5	1.5	1.4	1.4	1.4	1.3	16
17	1.8	1.8	1.7	1.7	1.6	1.6	1.5	1.5	1.5	1.4	1.4	1.4	1.3	17
18	1.8	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.4	1.4	1.4	1.3	1.3	18
19	1.7	1.7	1.7	1.6	1.6	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	19
20	1.7	1.7	1.6	1.6	1.6	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	20
21	1.7	1.6	1.6	1.6	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	21
22	1.7	1.6	1.6	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.2	22
23	1.6	1.6	1.6	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.2	23
24	1.6	1.6	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.2	1.2	24
25	1.6	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.2	25
26	1.6	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.2	26
27	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.2	1.2	27
28	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.1	28
29	1.5	1.4	1.4	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.1	29
30	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.1	1.1	30
31	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.1	1.1	31
32	1.4	1.4	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.1	1.1	1.1	32
33	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	33
34	1.4	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	34
35	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1		35
36	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1			36
37	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1				37
38	1.3	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1					38
39	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1						39
40	1.2	1.2	1.2	1.2	1.1	1.1	1.1							40
41	1.2	1.2	1.2	1.1	1.1	1.1								41
42	1.2	1.2	1.1	1.1	1.1									42
43	1.2	1.1	1.1	1.1										43
44	1.1	1.1	1.1											44
45	1.1	1.1												45
46	1.1												0.9	46
47												0.9	0.9	47
48											0.9	0.9	0.9	48
49										0.9	0.9	0.9	0.8	49
50									0.9	0.9	0.9	0.8	0.8	50
51								0.9	0.9	0.9	0.8	0.8	0.8	51
52							0.9	0.9	0.9	0.8	0.8	0.8	0.8	52
53						0.9	0.9	0.8	0.8	0.8	0.8	0.8	0.8	53
54					0.9	0.9	0.8	0.8	0.8	0.8	0.8	0.8	0.8	54
55				0.9	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.7	55
56			0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	56
57		0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	57
58	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	58
59	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	59
60	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	60
	38°	39°	40°	41°	42°	43°	44°	45°	46°	47°	48°	49°	50°	
	Declination of the same name as the latitude; lower transit; reduction subtractive.													

TABLE 26.

Variation of Altitude in one minute from meridian passage.

Latitude.	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°	61°	62°	63°	Latitude.
	Declination of a different name from the latitude; upper transit; reduction additive.													
°	"	"	"	"	"	"	"	"	"	"	"	"	"	°
0	1.6	1.5	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.0	1.0	0
1	1.6	1.5	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.0	1.0	1
2	1.5	1.5	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.1	1.1	1.0	1.0	2
3	1.5	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.1	1.0	1.0	3
4	1.5	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.1	1.0	1.0	4
5	1.5	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.1	1.1	1.0	1.0	1.0	5
6	1.5	1.4	1.4	1.3	1.3	1.2	1.2	1.2	1.1	1.1	1.0	1.0	1.0	6
7	1.4	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.1	1.0	1.0	0.9	7
8	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.1	1.1	1.1	1.0	1.0	0.9	8
9	1.4	1.4	1.3	1.3	1.2	1.2	1.2	1.1	1.1	1.0	1.0	1.0	0.9	9
10	1.4	1.4	1.3	1.3	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	10
11	1.4	1.3	1.3	1.3	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	11
12	1.4	1.3	1.3	1.2	1.2	1.2	1.1	1.1	1.1	1.0	1.0	0.9	0.9	12
13	1.3	1.3	1.3	1.2	1.2	1.2	1.1	1.1	1.0	1.0	1.0	0.9	0.9	13
14	1.3	1.3	1.3	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	14
15	1.3	1.3	1.2	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	15
16	1.3	1.3	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	0.9	16
17	1.3	1.2	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	0.9	17
18	1.3	1.2	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	0.9	18
19	1.2	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	1.0	0.9	0.9	0.9	19
20	1.2	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	0.9	0.8	20
21	1.2	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	0.9	0.8	21
22	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	1.0	0.9	0.9	0.9		22
23	1.2	1.2	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9	0.9			23
24	1.2	1.1	1.1	1.1	1.1	1.0	1.0	1.0	0.9	0.9				24
25	1.2	1.1	1.1	1.1	1.0	1.0	1.0	1.0	0.9					25
26	1.1	1.1	1.1	1.1	1.0	1.0	1.0	0.9						26
27	1.1	1.1	1.1	1.0	1.0	1.0	1.0							27
28	1.1	1.1	1.1	1.0	1.0	1.0								28
29	1.1	1.1	1.0	1.0	1.0									29
30	1.1	1.1	1.0	1.0										30
31	1.1	1.0	1.0											31
32	1.1	1.0												32
33	1.1												0.8	33
34												0.8	0.7	34
35											0.8	0.8	0.7	35
36										0.8	0.8	0.8	0.7	36
37									0.8	0.8	0.8	0.7	0.7	37
38								0.8	0.8	0.8	0.8	0.7	0.7	38
39							0.8	0.8	0.8	0.8	0.8	0.7	0.7	39
40						0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	40
41					0.9	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	41
42				0.9	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	42
43			0.9	0.9	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	43
44		0.9	0.9	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	44
45	0.9	0.9	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	45
46	0.9	0.9	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	46
47	0.9	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.6	47
48	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.6	48
49	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	49
50	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	50
51	0.8	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	51
52	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	0.6	52
53	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	0.6	0.6	53
54	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	0.6	0.6	0.6	54
55	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	0.6	0.6	0.6	55
56	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	0.6	0.6	0.6	0.6	56
57	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	0.6	0.6	0.6	0.6	0.6	57
58	0.7	0.7	0.7	0.7	0.7	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	58
59	0.7	0.7	0.7	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.5	59
60	0.7	0.7	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.5	60
	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°	61°	62°	63°	
	Declination of the same name as the latitude; lower transit; reduction subtractive.													

TABLE 27.

Reduction to be applied to Altitudes near the Meridian.

Var. 1 min. (Table 26.)	Time from meridian passage.													Var. 1 min. (Table 26.)
	m. s. 0 30	m. s. 1 0	m. s. 1 30	m. s. 2 0	m. s. 2 30	m. s. 3 0	m. s. 3 30	m. s. 4 0	m. s. 4 30	m. s. 5 0	m. s. 5 30	m. s. 6 0	m. s. 6 30	
″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″
0.1	0 0	0 0	0 0	0 0	0 1	0 1	0 1	0 2	0 2	0 2	0 3	0 4	0 4	0.1
0.2	0 0	0 0	0 0	0 1	0 1	0 2	0 3	0 3	0 4	0 5	0 6	0 7	0 8	0.2
0.3	0 0	0 0	0 1	0 1	0 2	0 3	0 4	0 5	0 6	0 7	0 9	0 11	0 13	0.3
0.4	0 0	0 0	0 1	0 2	0 2	0 4	0 5	0 6	0 8	0 10	0 12	0 14	0 17	0.4
0.5	0 0	0 0	0 1	0 2	0 3	0 4	0 6	0 8	0 10	0 12	0 15	0 18	0 21	0.5
0.6	0 0	0 1	0 1	0 2	0 4	0 5	0 7	0 10	0 12	0 15	0 18	0 22	0 25	0.6
0.7	0 0	0 1	0 2	0 3	0 4	0 6	0 9	0 11	0 14	0 17	0 21	0 25	0 30	0.7
0.8	0 0	0 1	0 2	0 3	0 5	0 7	0 10	0 13	0 16	0 20	0 24	0 29	0 34	0.8
0.9	0 0	0 1	0 2	0 4	0 6	0 8	0 11	0 14	0 18	0 22	0 27	0 32	0 38	0.9
1.0	0 0	0 1	0 2	0 4	0 6	0 9	0 12	0 16	0 20	0 25	0 30	0 36	0 42	1.0
2.0	0 0	0 2	0 4	0 8	0 12	0 18	0 24	0 32	0 41	0 50	1 0	1 12	1 24	2.0
3.0	0 1	0 3	0 7	0 12	0 19	0 27	0 37	0 48	1 1	1 15	1 31	1 48	2 6	3.0
4.0	0 1	0 4	0 9	0 16	0 25	0 36	0 49	1 4	1 21	1 40	2 1	2 24	2 49	4.0
5.0	0 1	0 5	0 11	0 20	0 31	0 45	1 1	1 20	1 41	2 5	2 31	3 0	3 31	5.0
6.0	0 1	0 6	0 13	0 24	0 37	0 54	1 13	1 36	2 1	2 30	3 1	3 36	4 13	6.0
7.0	0 2	0 7	0 16	0 28	0 44	1 3	1 26	1 52	2 22	2 55	3 32	4 12	4 56	7.0
8.0	0 2	0 8	0 18	0 32	0 50	1 12	1 38	2 8	2 42	3 20	4 2	4 48	5 38	8.0
9.0	0 2	0 9	0 20	0 36	0 56	1 21	1 50	2 24	3 2	3 45	4 32	5 24	6 20	9.0
10.0	0 2	0 10	0 22	0 40	1 2	1 30	2 3	2 40	3 23	4 10	5 2	6 0	7 2	10.0
11.0	0 3	0 11	0 25	0 44	1 9	1 39	2 15	2 56	3 43	4 35	5 32	6 36	7 45	11.0
12.0	0 3	0 12	0 27	0 48	1 15	1 48	2 27	3 12	4 3	5 0	6 3	7 12	8 27	12.0
13.0	0 3	0 13	0 29	0 52	1 21	1 57	2 39	3 28	4 23	5 25	6 33	7 48	9 9	13.0
14.0	0 3	0 14	0 31	0 56	1 27	2 6	2 51	3 44	4 43	5 50	7 4	8 24	9 51	14.0
15.0	0 4	0 15	0 34	1 0	1 34	2 15	3 4	4 0	5 3	6 15	7 34	9 0	10 34	15.0
16.0	0 4	0 16	0 36	1 4	1 40	2 24	3 16	4 16	5 24	6 40	8 4	9 36	11 16	16.0
17.0	0 4	0 17	0 38	1 8	1 46	2 33	3 28	4 32	5 44	7 5	8 34	10 12	11 58	17.0
18.0	0 4	0 18	0 40	1 12	1 52	2 42	3 40	4 48	6 4	7 30	9 4	10 48	12 40	18.0
19.0	0 5	0 19	0 43	1 16	1 59	2 51	3 53	5 4	6 25	7 55	9 35	11 24	13 23	19.0
20.0	0 5	0 20	0 45	1 20	2 5	3 0	4 5	5 20	6 45	8 20	10 5	12 0	14 5	20.0
21.0	0 5	0 21	0 47	1 24	2 11	3 9	4 17	5 36	7 5	8 45	10 35	12 36	14 47	21.0
22.0	0 5	0 22	0 49	1 28	2 17	3 18	4 30	5 52	7 25	9 10	11 5	13 12	15 29	22.0
23.0	0 6	0 23	0 52	1 32	2 24	3 27	4 42	6 8	7 46	9 35	11 36	13 48	16 12	23.0
24.0	0 6	0 24	0 54	1 36	2 30	3 36	4 54	6 24	8 6	10 0	12 6	14 24	16 54	24.0
25.0	0 6	0 25	0 56	1 40	2 36	3 45	5 6	6 40	8 26	10 25	12 36	15 0		25.0
26.0	0 6	0 26	0 58	1 44	2 42	3 54	5 18	6 56	8 46	10 50	13 6			26.0
27.0	0 7	0 27	1 1	1 48	2 49	4 3	5 30	7 12	9 7	11 15				27.0
28.0	0 7	0 28	1 3	1 52	2 55	4 12	5 43	7 28	9 27	11 40				28.0

TABLE 27.

Reduction to be applied to Altitudes near the Meridian.

Var. 1 min. (Table 26.)	Time from meridian passage.													Var. 1 min. (Table 26.)
	m. s. 7 0	m. s. 7 30	m. s. 8 0	m. s. 8 30	m. s. 9 0	m. s. 9 30	m. s. 10 0	m. s. 10 30	m. s. 11 0	m. s. 11 30	m. s. 12 0	m. s. 12 30	m. s. 13 0	
″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	′ ″	″
0.1	0 5	0 6	0 6	0 7	0 8	0 9	0 10	0 11	0 12	0 13	0 14	0 16	0 17	0.1
0.2	0 10	0 11	0 13	0 14	0 16	0 18	0 20	0 22	0 24	0 26	0 29	0 31	0 34	0.2
0.3	0 15	0 17	0 19	0 22	0 24	0 27	0 30	0 33	0 36	0 40	0 43	0 47	0 51	0.3
0.4	0 20	0 23	0 26	0 29	0 32	0 36	0 40	0 44	0 48	0 53	0 58	1 2	1 8	0.4
0.5	0 24	0 28	0 32	0 36	0 40	0 45	0 50	0 55	1 0	1 6	1 12	1 18	1 24	0.5
0.6	0 29	0 34	0 38	0 43	0 49	0 54	1 0	1 6	1 13	1 19	1 26	1 34	1 41	0.6
0.7	0 34	0 39	0 45	0 51	0 57	1 3	1 10	1 17	1 25	1 33	1 41	1 49	1 58	0.7
0.8	0 39	0 45	0 51	0 58	1 5	1 12	1 20	1 28	1 37	1 46	1 55	2 5	2 15	0.8
0.9	0 44	0 51	0 57	1 5	1 13	1 21	1 30	1 39	1 49	1 59	2 10	2 21	2 32	0.9
1.0	0 49	0 56	1 4	1 12	1 21	1 30	1 40	1 50	2 1	2 12	2 24	2 36	2 49	1.0
2.0	1 38	1 52	2 8	2 24	2 42	3 0	3 20	3 40	4 2	4 24	4 48	5 12	5 38	2.0
3.0	2 27	2 49	3 12	3 37	4 3	4 30	5 0	5 31	6 3	6 37	7 12	7 49	8 27	3.0
4.0	3 16	3 45	4 16	4 49	5 24	6 1	6 40	7 21	8 4	8 49	9 36	10 25	11 16	4.0
5.0	4 5	4 41	5 20	6 1	6 45	7 31	8 20	9 11	10 5	11 1	12 0	13 1	14 5	5.0
6.0	4 54	5 37	6 24	7 14	8 6	9 1	10 0	11 1	12 6	13 13	14 24	15 37	16 54	6.0
7.0	5 43	6 34	7 28	8 26	9 27	10 32	11 40	12 52	14 7	15 26	16 48	18 14	19 43	7.0
8.0	6 32	7 30	8 32	9 38	10 48	12 2	13 20	14 42	16 8	17 38	19 12	20 50	22 32	8.0
9.0	7 21	8 26	9 36	10 50	12 9	13 32	15 0	16 32	18 9	19 50	21 36	23 26	25 21	9.0
10.0	8 10	9 22	10 40	12 2	13 30	15 2	16 40	18 22	20 10	22 2	24 0	26 2	28 10	10.0
11.0	8 59	10 19	11 44	13 15	14 51	16 33	18 20	20 13	22 11	24 15	26 24	28 39		11.0
12.0	9 48	11 15	12 48	14 27	16 12	18 3	20 0	22 3	24 12	26 27	28 48			12.0
13.0	10 37	12 11	13 52	15 39	17 33	19 33	21 40	23 53	26 13	28 39				13.0
14.0	11 26	13 7	14 56	16 51	18 54	21 3	23 20	25 43	28 14					14.0
15.0	12 15	14 4	16 0	18 14	20 15	22 34	25 0	27 34						15.0
16.0	13 4	15 0	17 4	19 16	21 36	24 4	26 40							16.0
17.0	13 53	15 56	18 8	20 28	22 57	25 34								17.0
18.0	14 42	16 52	19 12	21 40	24 18									18.0
19.0	15 31	17 49	20 16											19.0
20.0	16 20	18 45												20.0
21.0	17 9													21.0

TABLE 27.

Reduction to be applied to Altitudes near the Meridian

Var. 1 min. (Table 26.)	Time from meridian passage. m. s. 13 30	m. s. 14 0	m. s. 14 30	m. s. 15 0	m. s. 15 30	m. s. 16 0	m. s. 16 30	m. s. 17 0	m. s. 17 30	m. s. 18 0	m. s. 18 30	m. s. 19 0	m. s. 19 30	Var. 1 min. (Table 26.)
"	' "	' "	' "	' "	' "	' "	' "	' "	' "	' "	' "	' "	' "	"
0.1	0 18	0 20	0 21	0 22	0 24	0 26	0 27	0 29	0 31	0 32	0 34	0 36	0 38	0.1
0.2	0 36	0 39	0 42	0 45	0 48	0 51	0 54	0 58	1 1	1 5	1 8	1 12	1 16	0.2
0.3	0 55	0 59	1 3	1 7	1 12	1 17	1 22	1 27	1 32	1 37	1 43	1 48	1 54	0.3
0.4	1 13	1 18	1 24	1 30	1 36	1 42	1 49	1 56	2 2	2 10	2 17	2 24	2 32	0.4
0.5	1 31	1 38	1 45	1 52	2 0	2 8	2 16	2 24	2 33	2 42	2 51	3 1	3 10	0.5
0.6	1 49	1 58	2 6	2 15	2 24	2 34	2 43	2 53	3 4	3 14	3 25	3 37	3 48	0.6
0.7	2 8	2 17	2 27	2 37	2 48	2 59	3 11	3 22	3 34	3 47	4 0	4 13	4 26	0.7
0.8	2 26	2 37	2 48	3 0	3 12	3 25	3 38	3 51	4 5	4 19	4 34	4 49	5 4	0.8
0.9	2 44	2 56	3 9	3 22	3 36	3 50	4 5	4 20	4 36	4 52	5 8	5 25	5 42	0.9
1.0	3 2	3 16	3 30	3 45	4 0	4 16	4 32	4 49	5 6	5 24	5 42	6 1	6 20	1.0
2.0	6 4	6 32	7 0	7 30	8 0	8 32	9 4	9 38	10 12	10 48	11 24	12 2	12 40	2.0
3.0	9 7	9 48	10 30	11 15	12 1	12 48	13 38	14 27	15 19	16 12	17 7	18 3	19 1	3.0
4.0	12 9	13 14	14 1	15 0	16 1	17 4	18 9	19 16	20 25	21 36	22 49	24 4	25 21	4.0
5.0	15 11	16 20	17 31	18 45	20 1	21 20	22 41	24 5	25 31	27 0	28 31			5.0
6.0	18 13	19 36	21 2	22 30	24 1	25 36	27 13							6.0
7.0	21 16	22 52	24 32	26 15	28 1									7.0
8.0	24 18	26 8	28 2											8.0
9.0	27 20													9.0

Var. 1 min. (Table 26.)	Time from meridian passage. m. s. 20 0	m. s. 20 30	m. s. 21 0	m. s. 21 30	m. s. 22 0	m. s. 22 30	m. s. 23 0	m. s. 23 30	m. s. 24 0	m. s. 24 30	m. s. 25 0	m. s. 25 30	m. s. 26 0	Var. 1 min. (Table 26.)
"	' "	' "	' "	' "	' "	' "	' "	' "	' "	' "	' "	' "	' "	"
0.1	0 40	0 42	0 44	0 46	0 48	0 51	0 53	0 55	0 58	1 0	1 2	1 6	1 8	0.1
0.2	1 20	1 24	1 28	1 32	1 37	1 41	1 46	1 50	1 55	2 0	2 5	2 10	2 15	0.2
0.3	2 0	2 6	2 12	2 19	2 25	2 32	2 39	2 46	2 53	3 0	3 7	3 15	3 23	0.3
0.4	2 40	2 48	2 56	3 5	3 14	3 22	3 32	3 41	3 50	4 0	4 10	4 20	4 30	0.4
0.5	3 20	3 30	3 41	3 51	4 2	4 13	4 24	4 36	4 48	5 0	5 12	5 25	5 38	0.5
0.6	4 0	4 12	4 25	4 37	4 50	5 4	5 17	5 31	5 46	6 0	6 15	6 30	6 46	0.6
0.7	4 40	4 54	5 9	5 24	5 39	5 54	6 10	6 27	6 43	7 0	7 17	7 35	7 53	0.7
0.8	5 20	5 36	5 53	6 10	6 27	6 45	7 3	7 22	7 41	8 0	8 20	8 40	9 1	0.8
0.9	6 0	6 18	6 37	6 56	7 16	7 36	7 56	8 17	8 38	9 0	9 22	9 45	10 8	0.9
1.0	6 40	7 0	7 21	7 42	8 4	8 26	8 49	9 12	9 36	10 0	10 25	10 50	11 16	1.0
2.0	13 20	14 0	14 42	15 24	16 8	16 52	17 38	18 24	19 12	20 0	20 50	21 40	22 32	2.0
3.0	20 0	21 0	22 3	23 7	24 12	25 19	26 27	27 37	28 48	30 0				3.0
4.0	26 40	28 1	29 24											4.0

TABLE 28A.

For finding the Latitude of a place by Altitudes of Polaris.

[A=1st correction. Argument, the star's hour angle (or 24h—the star's hour angle).]

m.	0h		1h		2h		3h		4h		5h		m.
	° ′ ″	″	° ′ ″	″	° ′ ″	″	° ′ ″	″	° ′ ″	″	° ′ ″	″	
0	−1 12 00.0	.0	−1 09 32.8	4.9	−1 02 21.4	9.5	−0 50 54.9	13.3	−0 36 00.0	16.3	−0 18 38.2	18.2	60
1	11 59.9	.1	09 27.9	5.0	02 11.9	9.5	50 41.6	13.4	35 43.7	16.4	18 20.0	18.2	59
2	11 59.8	.1	09 22.9	5.0	02 02.4	9.6	50 28.2	13.5	35 27.3	16.4	18 01.8	18.3	58
3	11 59.6	.3	09 17.9	5.2	01 52.8	9.7	50 14.7	13.5	35 10.9	16.4	17 43.5	18.3	57
4	11 59.3	.4	09 12.7	5.3	01 43.1	9.7	50 01.2	13.6	34 54.5	16.4	17 25.2	18.3	56
5	−1 11 58.9	.4	−1 09 07.4	5.3	−1 01 33.4	9.8	−0 49 47.6	13.7	−0 34 38.1	16.5	−0 17 06.9	18.3	55
6	11 58.5	.5	09 02.1	5.4	01 23.6	9.9	49 33.9	13.7	34 21.6	16.6	16 48.6	18.3	54
7	11 58.0	.6	08 56.7	5.4	01 13.7	10.0	49 20.2	13.7	34 05.0	16.6	16 30.3	18.4	53
8	11 57.4	.7	08 51.3	5.5	01 03.7	10.0	49 06.5	13.8	33 48.4	16.7	16 11.9	18.4	52
9	11 56.7	.8	08 45.8	5.6	00 53.7	10.1	48 52.7	13.9	33 31.7	16.7	15 53.5	18.4	51
10	−1 11 55.9	.9	−1 08 40.2	5.8	−1 00 43.6	10.2	−0 48 38.8	14.0	−0 33 15.0	16.8	−0 15 35.1	18.4	50
11	11 55.0	.9	08 34.4	5.8	00 33.4	10.2	48 24.8	14.0	32 58.2	16.8	15 16.7	18.4	49
12	11 54.1	1.0	08 28.6	5.9	00 23.2	10.3	48 10.8	14.0	32 41.4	16.8	14 58.3	18.4	48
13	11 53.1	1.1	08 22.7	5.9	00 12.9	10.3	47 56.8	14.1	32 24.6	16.8	14 39.9	18.4	47
14	11 52.0	1.2	08 16.8	6.0	00 02.6	10.5	47 42.7	14.1	32 07.8	16.9	14 21.5	18.5	46
15	−1 11 50.8	1.3	−1 08 10.8	6.1	−0 59 52.1	10.5	−0 47 28.6	14.2	−0 31 50.9	16.9	−0 14 03.0	18.5	45
16	11 49.5	1.4	08 04.7	6.2	59 41.6	10.6	47 14.4	14.2	31 34.0	16.9	13 44.5	18.5	44
17	11 48.1	1.4	07 58.5	6.2	59 31.0	10.6	47 00.2	14.3	31 27.1	17.0	13 26.0	18.5	43
18	11 46.7	1.5	07 52.3	6.3	59 20.4	10.7	46 45.9	14.4	31 10.1	17.1	13 07.5	18.6	42
19	11 45.2	1.6	07 46.0	6.4	59 09.7	10.8	46 31.5	14.4	30 53.0	17.0	12 48.9	18.6	41
20	−1 11 43.6	1.7	−1 07 39.6	6.5	−0 58 58.9	10.9	−0 46 17.1	14.5	−0 30 36.0	17.1	−0 12 30.3	18.6	40
21	11 41.9	1.8	07 33.1	6.6	58 48.0	10.9	46 02.6	14.5	30 18.9	17.2	12 11.7	18.6	39
22	11 40.1	1.8	07 26.5	6.6	58 37.1	10.9	45 48.1	14.6	30 01.7	17.2	11 53.1	18.6	38
23	11 38.3	2.0	07 19.9	6.8	58 26.2	11.1	45 33.5	14.6	29 44.5	17.2	11 34.5	18.6	37
24	11 36.3	2.0	07 13.1	6.8	58 15.1	11.1	45 18.9	14.7	29 17.3	17.2	11 15.9	18.7	36
25	−1 11 34.3	2.1	−1 07 06.3	6.8	−0 58 04.0	11.2	−0 45 04.2	14.8	−0 29 00.1	17.3	−0 10 57.2	18.6	35
26	11 32.2	2.2	06 59.5	7.0	57 52.8	11.2	44 49.4	14.8	28 42.8	17.3	10 38.6	18.6	34
27	11 30.0	2.2	06 52.5	7.0	57 41.6	11.3	44 34.6	14.8	28 25.5	17.3	10 20.0	18.6	33
28	11 27.8	2.3	06 45.5	7.1	57 30.3	11.4	44 19.8	14.9	28 08.2	17.4	10 01.4	18.7	32
29	11 25.5	2.4	06 38.4	7.2	57 18.9	11.4	44 04.9	14.9	27 50.8	17.4	09 42.7	18.7	31
30	−1 11 23.1	2.5	−1 06 31.2	7.2	−0 57 07.5	11.5	−0 43 50.0	15.0	−0 27 33.4	17.4	−0 09 24.0	18.7	30
31	11 20.6	2.6	06 24.0	7.3	56 56.0	11.6	43 35.0	15.0	27 16.0	17.5	09 05.3	18.7	29
32	11 18.0	2.7	06 16.7	7.4	56 44.4	11.6	43 20.0	15.0	26 58.5	17.5	08 46.6	18.7	28
33	11 15.3	2.7	06 09.3	7.5	56 32.8	11.7	43 05.0	15.1	26 41.0	17.5	08 27.9	18.7	27
34	11 12.6	2.9	06 01.8	7.6	56 21.1	11.8	42 49.9	15.2	26 23.5	17.6	08 09.1	18.7	26
35	−1 11 09.7	2.9	−1 05 54.2	7.6	−0 56 09.3	11.8	−0 42 34.7	15.2	−0 26 05.9	17.6	−0 07 50.4	18.7	25
36	11 06.8	3.0	05 46.6	7.7	55 57.5	11.9	42 19.5	15.3	25 48.3	17.6	07 31.7	18.7	24
37	11 03.8	3.0	05 38.9	7.8	55 45.6	12.0	42 04.2	15.3	25 30.7	17.6	07 12.9	18.8	23
38	11 00.8	3.2	05 31.1	7.8	55 33.6	12.0	41 48.9	15.3	25 13.1	17.7	06 54.1	18.8	22
39	10 57.6	3.2	05 23.3	8.0	55 21.6	12.1	41 33.6	15.4	24 55.4	17.7	06 35.3	18.7	21
40	−1 10 54.4	3.3	−1 05 15.3	8.0	−0 55 09.5	12.1	−0 41 18.2	15.5	−0 24 37.7	17.7	−0 06 16.6	18.8	20
41	10 51.1	3.4	05 07.3	8.0	54 57.4	12.2	41 02.7	15.5	24 20.0	17.8	05 57.8	18.8	19
42	10 47.7	3.5	04 59.3	8.2	54 45.2	12.3	40 47.2	15.6	24 02.2	17.8	05 39.0	18.8	18
43	10 44.2	3.5	04 51.1	8.2	54 32.9	12.3	40 31.6	15.6	23 44.4	17.8	05 20.2	18.8	17
44	10 40.7	3.7	04 42.9	8.3	54 20.6	12.4	40 16.0	15.7	23 26.6	17.8	05 01.4	18.8	16
45	−1 10 37.0	3.7	−1 04 34.6	8.4	−0 54 08.2	12.5	−0 40 00.3	15.7	−0 23 08.8	17.9	−0 04 42.6	18.8	15
46	10 33.3	3.8	04 26.2	8.4	53 55.7	12.5	39 44.6	15.7	22 50.9	17.9	04 23.8	18.8	14
47	10 29.5	3.9	04 17.8	8.5	53 43.2	12.6	39 28.9	15.8	22 33.0	17.9	04 05.0	18.8	13
48	10 25.6	3.9	04 09.3	8.6	53 30.6	12.6	39 13.1	15.8	22 15.1	17.9	03 46.2	18.8	12
49	10 21.7	4.1	04 00.7	8.7	53 18.0	12.7	38 57.3	15.9	21 57.2	18.0	03 27.4	18.9	11
50	−1 10 17.6	4.1	−1 03 52.0	8.7	−0 53 05.3	12.8	−0 38 41.4	15.9	−0 21 39.2	18.0	−0 03 08.5	18.8	10
51	10 13.5	4.2	03 43.3	8.8	52 52.5	12.8	38 25.5	16.0	21 21.2	18.0	02 49.7	18.8	9
52	10 09.3	4.3	03 34.5	8.9	52 39.7	12.9	38 09.5	16.0	21 03.2	18.0	02 30.9	18.9	8
53	10 05.0	4.3	03 25.6	9.0	52 26.8	13.0	37 53.5	16.1	20 45.2	18.1	02 12.0	18.8	7
54	10 00.7	4.5	03 16.6	9.0	52 13.8	13.0	37 37.4	16.1	20 27.1	18.1	01 53.2	18.8	6
55	−1 09 56.2	4.5	−1 03 07.6	9.0	−0 52 00.8	13.0	−0 37 21.3	16.2	−0 20 09.0	18.1	−0 01 34.4	18.9	5
56	09 51.7	4.6	02 58.6	9.2	51 47.8	13.1	37 05.1	16.2	19 50.9	18.1	01 15.5	18.8	4
57	09 47.1	4.7	02 49.4	9.2	51 34.7	13.2	36 48.9	16.3	19 32.8	18.2	00 56.7	18.9	3
58	09 42.4	4.7	02 40.2	9.4	51 21.5	13.3	36 32.6	16.3	19 14.6	18.2	00 37.8	18.9	2
59	09 37.7	4.9	02 30.8	9.4	51 08.2	13.3	36 16.3	16.3	18 56.4	18.2	00 18.9	18.9	1
60	−1 09 32.8		−1 02 21.4		−0 50 54.9		−0 36 00.0		−0 18 38.2		−0 00 00.0		0
m.	11h		10h		9h		8h		7h		6h		m.

Change the sign to + when the argument is found at the bottom.

TABLE 28B.

For finding the Latitude of a place by Altitudes of Polaris.

[B=the 2d correction. This correction is always additive.]

Star's hour angle.	Star's altitude. 10°	15°	16°	17°	18°	19°	20°	21°	22°	23°	Star's hour angle.
h. m.	″	″	″	″	″	″	″	″	″	″	h. m.
0 00	0.0 .0	0.0 .0	0.0 .0	0.0 .0	0.0 .0	0.0 .0	0.0 .0	0.0 .0	0.0 .0	0.0 .0	12 00
10	0.0 .1	0.0 .1	0.0 .1	0.0 .1	0.0 .1	0.0 .1	0.0 .1	0.0 .1	0.0 .1	0.0 .1	11 50
20	0.1 .1	0.1 .1	0.1 .1	0.1 .1	0.1 .1	0.1 .1	0.1 .2	0.1 .2	0.1 .2	0.1 .2	40
30	0.2 .1	0.2 .1	0.2 .2	0.2 .2	0.2 .2	0.2 .3	0.3 .2	0.3 .2	0.3 .3	0.3 .3	30
40	0.3 .1	0.3 .2	0.4 .2	0.4 .2	0.4 .3	0.5 .3	0.5 .3	0.5 .3	0.6 .3	0.6 .3	20
50	0.4 .1	0.5 .3	0.6 .3	0.6 .3	0.7 .3	0.8 .3	0.8 .3	0.8 .3	0.9 .3	0.9 .4	10
1 00	0.5	0.8	0.9	0.9	1.0	1.1	1.1	1.1	1.2	1.3	00
10	.2 0.7 .2	.3 1.1 .3	.3 1.2 .3	.3 1.2 .4	.3 1.3 .4	.3 1.4 .4	.3 1.4 .5	.4 1.5 .5	.4 1.6 .5	.4 1.7 .5	10 50
20	0.9 .2	1.4 .4	1.5 .3	1.6 .4	1.7 .4	1.8 .5	1.9 .5	2.0 .5	2.1 .6	2.2 .6	40
30	1.1 .3	1.8 .4	1.8 .5	2.0 .4	2.1 .5	2.3 .5	2.4 .5	2.5 .6	2.7 .5	2.8 .6	30
40	1.4 .3	2.2 .4	2.3 .5	2.4 .5	2.6 .5	2.8 .5	2.9 .6	3.1 .6	3.2 .6	3.4 .6	20
50	1.7 .3	2.6 .4	2.8 .4	2.9 .5	3.1 .5	3.3 .6	3.5 .6	3.7 .7	3.8 .7	4.0 .7	10
2 00	2.0	3.0	3.2	3.4	3.6	3.9	4.1	4.4	4.5	4.7	00
10	.3 2.3 .3	.5 3.5 .5	.5 3.7 .6	.5 3.9 .6	.6 4.2 .7	.6 4.5 .6	.7 4.8 .6	.6 5.0 .7	.8 5.3 .7	.8 5.5 .8	9 50
20	2.6 .3	4.0 .5	4.3 .5	4.5 .6	4.9 .6	5.1 .7	5.4 .7	5.7 .7	6.0 .8	6.3 .8	40
30	2.9 .4	4.5 .5	4.8 .5	5.1 .6	5.5 .6	5.8 .6	6.1 .7	6.4 .8	6.8 .7	7.1 .8	30
40	3.3 .3	5.0 .5	5.3 .6	5.7 .6	6.1 .6	6.4 .7	6.8 .7	7.2 .7	7.5 .8	7.9 .8	20
50	3.6 .4	5.5 .5	5.9 .6	6.3 .6	6.7 .7	7.1 .7	7.5 .8	7.9 .8	8.3 .8	8.7 .8	10
3 00	4.0	6.0	6.5	6.9	7.4	7.8	8.3	8.7	9.1	9.5	00
10	.3 4.3 .4	.6 6.6 .5	.5 7.0 .6	.6 7.5 .6	.6 8.0 .6	.6 8.4 .7	.6 8.9 .7	.7 9.4 .8	.8 9.9 .8	.9 10.4 .9	8 50
20	4.7 .3	7.1 .5	7.6 .6	8.1 .5	8.6 .6	9.1 .7	9.6 .8	10.2 .7	10.7 .8	11.3 .8	40
30	5.0 .3	7.6 .5	8.2 .5	8.6 .6	9.2 .7	9.8 .6	10.4 .6	10.9 .7	11.5 .7	12.1 .8	30
40	5.3 .4	8.1 .5	8.7 .5	9.2 .6	9.9 .6	10.4 .7	11.0 .7	11.6 .7	12.2 .8	12.9 .8	20
50	5.7 .3	8.6 .5	9.2 .5	9.8 .6	10.5 .5	11.1 .6	11.7 .6	12.3 .7	13.0 .7	13.7 .7	10
4 00	6.0	9.1	9.7	10.4	11.0	11.7	12.3	13.0	13.7	14.4	00
10	.3 6.3 .3	.5 9.6 .4	.5 10.2 .5	.5 10.9 .4	.6 11.6 .5	.5 12.2 .6	.7 13.0 .6	.6 13.6 .7	.6 14.3 .6	.6 15.0 .7	7 50
20	6.6 .2	10.0 .4	10.7 .4	11.3 .4	12.1 .4	12.8 .5	13.6 .4	14.3 .5	14.9 .7	15.7 .6	40
30	6.8 .2	10.4 .4	11.1 .3	11.7 .4	12.5 .5	13.3 .5	14.0 .5	14.8 .5	15.6 .5	16.3 .6	30
40	7.0 .3	10.8 .3	11.4 .4	12.1 .4	13.0 .4	13.8 .4	14.5 .5	15.3 .5	16.1 .5	16.9 .6	20
50	7.3 .2	11.1 .3	11.8 .3	12.5 .4	13.4 .3	14.2 .3	15.0 .4	15.8 .4	16.6 .5	17.5 .4	10
5 00	7.5	11.4	12.1	12.9	13.7	14.5	15.4	16.2	17.1	17.9	00
10	.1 7.6 .2	.2 11.6 .1	.3 12.4 .2	.3 13.2 .2	.3 14.0 .2	.3 14.8 .3	.3 15.7 .3	.3 16.5 .3	.3 17.4 .3	.4 18.3 .3	6 50
20	7.8 .1	11.7 .2	12.6 .1	13.4 .2	14.2 .2	15.1 .2	16.0 .2	16.8 .3	17.7 .3	18.6 .3	40
30	7.9 .0	11.9 .1	12.7 .2	13.6 .1	14.4 .2	15.3 .2	16.2 .2	17.1 .2	18.0 .1	18.9 .1	30
40	7.9 .0	12.0 .1	12.9 .1	13.7 .1	14.6 .1	15.5 .1	16.4 .1	17.3 .0	18.1 .1	19.0 .1	20
50	7.9 .0	12.1 .1	13.0 .0	13.8 .1	14.7 .0	15.6 .0	16.5 .0	17.3 .0	18.2 .1	19.1 .1	10
6 00	7.9	12.2	13.0	13.9	14.7	15.6	16.5	17.3	18.3	19.2	6 00

TABLE 28C.

[C=the 3d correction. Hor. Arg., the star's declination. Vert. Arg., B=the 2d correction.]

B.	88° 47′				88° 48′						88° 49′		
	20″	30″	40″	50″	0″	10″	20″	30″	40″	50″	0″	10″	20″
″	″	″	″	″	″	″	″	″	″	″	″	″	″
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	+0.2	+0.1	+0.1	+0.0	0.0	−0.0	−0.1	−0.1	−0.2	−0.2	−0.3	−0.4	−0.4
20	0.4	0.3	0.2	0.1	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8
30	0.6	0.5	0.3	0.1	0.0	0.1	0.3	0.5	0.6	0.7	0.8	1.1	1.2
40	0.8	0.6	0.4	0.2	0.0	0.2	0.4	0.6	0.8	1.0	1.2	1.5	1.6
50	+1.0	+0.7	+0.5	+0.2	0.0	−0.2	−0.5	−0.9	−1.0	−1.2	−1.5	−1.7	−2.1

NOTE.—Below 15° B is nearly proportional to the altitude.

TABLE 28B.

For finding the Latitude of a place by Altitudes of Polaris.

[B=the 2d correction. This correction is always additive.]

Star's hour angle.	24°		25°		26°		27°		28°	
h. m.	″		″		″		″		″	
0 00	0.0		0.0		0.0		0.0		0.0	
10	0.0	.0	0.0	.0	0.0	.0	0.0	.0	0.0	.0
20	0.1	.1	0.1	.1	0.2	.2	0.2	.2	0.2	.2
30	0.3	.2	0.3	.2	0.4	.2	0.4	.2	0.4	.2
40	0.6	.3	0.6	.3	0.7	.3	0.7	.3	0.7	.3
50	1.0	.4	1.0	.4	1.1	.4	1.1	.4	1.1	.4
1 00	1.4	.4	1.4	.4	1.5	.4	1.5	.4	1.6	.5
10	1.8	.4	1.9	.5	2.0	.5	2.1	.6	2.2	.6
20	2.3	.5	2.4	.5	2.5	.5	2.7	.6	2.8	.6
30	2.9	.6	3.1	.7	3.2	.7	3.4	.7	3.5	.7
40	3.6	.7	3.8	.7	4.0	.8	4.1	.7	4.3	.8
50	4.3	.7	4.5	.7	4.7	.7	4.9	.8	5.1	.8
2 00	5.0	.7	5.3	.8	5.5	.8	5.8	.9	6.0	.9
10	5.8	.8	6.1	.8	6.4	.9	6.7	.9	7.0	1.0
20	6.6	.8	7.0	.9	7.3	.9	7.6	.9	7.9	.9
30	7.5	.9	7.9	.9	8.2	.9	8.5	.9	8.9	1.0
40	8.3	.8	8.7	.8	9.1	.9	9.5	1.0	10.0	1.1
50	9.2	.9	9.6	.9	10.0	.9	10.5	1.0	11.0	1.0
3 00	10.0	.8	10.5	.9	11.0	1.0	11.5	1.0	12.0	1.0
10	10.9	.9	11.4	.9	12.0	1.0	12.5	1.0	13.0	1.0
20	11.8	.9	12.4	1.0	13.0	1.0	13.5	1.0	14.1	1.1
30	12.6	.8	13.3	.9	13.9	.9	14.5	1.0	15.1	1.0
40	13.5	.9	14.2	.9	14.8	.9	15.5	1.0	16.1	1.0
50	14.3	.8	15.0	.8	15.7	.9	16.4	.9	17.1	1.0
4 00	15.1	.8	15.8	.8	16.5	.8	17.3	.9	18.1	1.0
10	15.9	.8	16.6	.8	17.3	.8	18.1	.8	19.0	.9
20	16.6	.7	17.3	.7	18.1	.8	19.0	.9	19.8	.8
30	17.2	.6	18.0	.7	18.8	.7	19.7	.7	20.5	.7
40	17.8	.6	18.6	.6	19.5	.7	20.3	.6	21.2	.7
50	18.3	.5	19.2	.6	20.1	.6	21.0	.7	21.9	.7
5 00	18.8	.5	19.7	.5	20.6	.5	21.5	.5	22.4	.5
10	19.2	.4	20.1	.4	21.1	.5	22.0	.5	22.9	.5
20	19.5	.3	20.5	.4	21.4	.3	22.4	.4	23.3	.4
30	19.8	.3	20.7	.2	21.7	.3	22.6	.2	23.6	.3
40	20.0	.2	20.9	.2	21.9	.2	22.8	.2	23.9	.3
50	20.1	.1	21.0	.1	22.0	.1	23.0	.2	24.0	.1
6 00	20.2	.1	21.1	.1	22.0	.0	23.1	.1	24.1	.1

Star's hour angle.	29°		30°		31°		32°		33°		Star's hour angle.
h. m.	″		″		″		″		″		h. m.
0 00	0.0		0.0		0.0		0.0		0.0		12 00
10	0.0	.0	0.0	.0	0.0	.0	0.0	.0	0.0	.0	11 50
20	0.2	.2	0.2	.2	0.2	.2	0.2	.2	0.2	.2	40
30	0.4	.2	0.4	.2	0.5	.3	0.5	.3	0.5	.3	30
40	0.7	.3	0.8	.4	0.8	.3	0.8	.3	0.9	.4	20
50	1.1	.4	1.2	.4	1.3	.5	1.3	.5	1.4	.5	10
1 00	1.7	.6	1.7	.5	1.8	.5	1.9	.6	1.9	.5	00
10	2.3	.6	2.3	.6	2.4	.6	2.5	.6	2.6	.7	10 50
20	2.9	.6	3.0	.7	3.2	.8	3.3	.8	3.4	.8	40
30	3.6	.7	3.8	.8	4.0	.8	4.1	.8	4.3	.9	30
40	4.5	.9	4.7	.9	4.9	.9	5.0	.9	5.3	1.0	20
50	5.3	.8	5.6	.9	5.8	.9	6.0	1.0	6.2	.9	10
2 00	6.2	.9	6.5	.9	6.8	1.0	7.0	1.0	7.3	1.1	00
10	7.2	1.0	7.5	1.0	7.9	1.1	8.2	1.2	8.5	1.2	9 50
20	8.3	1.1	8.6	1.1	8.9	1.0	9.3	1.1	9.6	1.1	40
30	9.3	1.0	9.6	1.0	10.0	1.1	10.4	1.1	10.8	1.2	30
40	10.4	1.1	10.8	1.2	11.2	1.2	11.6	1.2	12.0	1.2	20
50	11.4	1.0	11.9	1.1	12.4	1.2	12.9	1.3	13.3	1.3	10
3 00	12.5	1.1	13.0	1.1	13.6	1.2	14.1	1.2	14.6	1.3	00
10	13.6	1.1	14.2	1.2	14.7	1.1	15.4	1.3	16.0	1.4	8 50
20	14.7	1.1	15.3	1.1	15.9	1.2	16.6	1.2	17.3	1.3	40
30	15.8	1.1	16.4	1.1	17.1	1.2	17.8	1.2	18.5	1.2	30
40	16.8	1.0	17.5	1.1	18.2	1.1	19.0	1.2	19.7	1.2	20
50	17.8	1.0	18.5	1.0	19.4	1.2	20.1	1.1	20.9	1.2	10
4 00	18.8	1.0	19.6	1.1	20.4	1.0	21.2	1.1	22.0	1.1	00
10	19.7	.9	20.6	1.0	21.4	1.0	22.3	1.1	23.1	1.1	7 50
20	20.6	.9	21.5	.9	22.4	1.0	23.2	.9	24.1	1.0	40
30	21.4	.8	22.3	.8	23.2	.8	24.1	.9	25.1	1.0	30
40	22.1	.7	23.0	.7	24.0	.8	24.9	.8	25.9	.8	20
50	22.8	.7	23.7	.7	24.6	.6	25.7	.8	26.7	.8	10
5 00	23.4	.6	24.4	.7	25.3	.7	26.4	.7	27.4	.7	00
10	23.9	.5	24.9	.5	25.8	.5	27.0	.6	28.0	.6	6 50
20	24.3	.4	25.4	.5	26.2	.4	27.4	.4	28.5	.5	40
30	24.6	.3	25.7	.3	26.6	.4	27.8	.4	28.8	.3	30
40	24.9	.3	25.9	.2	26.9	.3	28.0	.2	29.1	.3	20
50	25.0	.1	26.0	.1	27.0	.1	28.2	.2	29.3	.2	10
6 00	25.1	.1	26.1	.1	27.1	.1	28.3	.1	29.4	.1	6 00

TABLE 28C.

[C=the 3d correction. Hor. Arg., the star's declination. Vert. Arg., B=the 2d correction.]

B.	88° 47′				88° 48′						88° 49′		
	20″	30″	40″	50″	0″	10″	20″	30″	40″	50″	0″	10″	20″
″	″	″	″	″	″	″	″	″	″	″	″	″	″
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	+0.2	+0.1	+0.1	+0.0	0.0	−0.0	−0.1	−0.1	−0.2	−0.2	−0.3	−0.4	−0.4
20	0.4	0.3	0.2	0.1	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8
30	0.6	0.5	0.3	0.1	0.0	0.1	0.3	0.5	0.6	0.7	0.8	1.1	1.2
40	0.8	0.6	0.4	0.2	0.0	0.2	0.4	0.6	0.8	1.0	1.2	1.5	1.6
50	+1.0	+0.7	+0.5	+0.2	0.0	−0.2	−0.5	−0.7	−1.0	−1.2	−1.5	−1.7	−2.1

TABLE 28B.

For finding the Latitude of a place by Altitudes of Polaris.

[B = the 2d correction. This correction is always additive.]

Star's hour angle.	34°	diff	35°	diff	36°	diff	37°	diff	38°	diff	39°	diff	40°	diff	41°	diff	42°	diff	43°	diff	Star's hour angle.
h. m.	"		"		"		"		"		"		"		"		"		"		h. m.
0 00	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	12 00
10	0.1	.1	0.1	.1	0.1	.1	0.1	.2	0.1	.2	0.1	.2	0.1	.2	0.1	.2	0.1	.2	0.1	.2	11 50
20	0.2	.3	0.2	.3	0.2	.3	0.3	.3	0.3	.3	0.3	.3	0.3	.3	0.3	.4	0.3	.4	0.3	.4	40
30	0.5	.4	0.5	.5	0.5	.5	0.6	.4	0.6	.5	0.6	.5	0.6	.5	0.7	.5	0.7	.5	0.7	.6	30
40	0.9	.6	1.0	.5	1.0	.5	1.0	.6	1.1	.5	1.1	.6	1.1	.7	1.2	.7	1.2	.7	1.3	.6	20
50	1.5	.5	1.5	.6	1.5	.7	1.6	.7	1.6	.7	1.7	.7	1.8	.7	1.9	.8	1.9	.9	1.9	.9	10
1 00	2.0	.8	2.1	.7	2.2	.8	2.3	.8	2.3	.9	2.4	.9	2.5	.9	2.7	.9	2.8	.9	2.8	1.0	00
10	2.8	.8	2.8	.9	3.0	.8	3.1	.9	3.2	.9	3.3	1.0	3.4	1.1	3.6	1.0	3.7	1.1	3.8	1.1	10 50
20	3.6	.9	3.7	.9	3.8	1.0	4.0	1.0	4.1	1.1	4.3	1.0	4.5	1.1	4.6	1.2	4.8	1.2	4.9	1.3	40
30	4.5	.9	4.6	1.0	4.8	1.0	5.0	1.1	5.2	1.1	5.3	1.3	5.6	1.2	5.8	1.2	6.0	1.3	6.2	1.3	30
40	5.4	1.1	5.6	1.1	5.8	1.2	6.1	1.2	6.3	1.2	6.6	1.2	6.8	1.3	7.0	1.3	7.3	1.4	7.5	1.5	20
50	6.5	1.1	6.7	1.2	7.0	1.2	7.3	1.2	7.5	1.3	7.8	1.4	8.1	1.4	8.3	1.5	8.7	1.5	9.0	1.5	10
2 00	7.6	1.2	7.9	1.3	8.2	1.3	8.5	1.3	8.8	1.4	9.2	1.4	9.5	1.4	9.8	1.5	10.2	1.5	10.5	1.6	00
10	8.8	1.2	9.2	1.3	9.5	1.3	9.8	1.4	10.2	1.5	10.6	1.5	10.9	1.6	11.3	1.7	11.7	1.7	12.1	1.8	9 50
20	10.0	1.3	10.5	1.2	10.8	1.3	11.2	1.4	11.7	1.4	12.1	1.5	12.5	1.6	13.0	1.6	13.4	1.7	13.9	1.9	40
30	11.3	1.3	11.7	1.4	12.1	1.5	12.6	1.5	13.1	1.5	13.6	1.5	14.1	1.6	14.6	1.6	15.1	1.7	15.6	1.8	30
40	12.6	1.3	13.1	1.3	13.6	1.4	14.1	1.5	14.6	1.5	15.1	1.6	15.7	1.6	16.2	1.8	16.8	1.7	17.4	1.9	20
50	13.9	1.3	14.4	1.5	15.0	1.4	15.6	1.4	16.1	1.6	16.7	1.6	17.3	1.7	18.0	1.7	18.5	1.8	19.3	1.8	10
3 00	15.2	1.4	15.9	1.4	16.4	1.5	17.0	1.5	17.7	1.5	18.3	1.6	19.0	1.7	19.7	1.7	20.3	1.8	21.1	1.8	00
10	16.6	1.3	17.3	1.3	17.9	1.4	18.5	1.5	19.2	1.5	19.9	1.6	20.7	1.6	21.4	1.7	22.1	1.8	22.9	1.9	8 50
20	17.9	1.3	18.6	1.3	19.3	1.4	20.0	1.5	20.7	1.6	21.5	1.6	22.3	1.6	23.1	1.6	23.9	1.7	24.8	1.7	40
30	19.2	1.3	19.9	1.3	20.7	1.3	21.5	1.3	22.3	1.4	23.1	1.5	23.9	1.5	24.7	1.7	25.6	1.7	26.5	1.8	30
40	20.5	1.2	21.2	1.3	22.0	1.4	22.8	1.4	23.7	1.4	24.6	1.5	25.4	1.6	26.4	1.5	27.3	1.7	28.3	1.7	20
50	21.7	1.1	22.5	1.2	23.4	1.2	24.2	1.4	25.1	1.4	26.1	1.4	27.0	1.4	27.9	1.6	29.0	1.5	30.0	1.7	10
4 00	22.8	1.2	23.7	1.2	24.6	1.2	25.6	1.2	26.5	1.3	27.5	1.3	28.4	1.5	29.5	1.4	30.5	1.6	31.7	1.5	00
10	24.0	1.0	24.9	1.1	25.8	1.2	26.8	1.2	27.8	1.2	28.8	1.3	29.9	1.3	30.9	1.4	32.1	1.4	33.2	1.5	7 50
20	25.0	1.1	26.0	1.1	27.0	1.0	28.0	1.1	29.0	1.1	30.1	1.2	31.2	1.2	32.3	1.2	33.5	1.2	34.7	1.3	40
30	26.1	.9	27.1	.8	28.0	1.0	29.1	1.0	30.1	1.1	31.3	1.0	32.4	1.1	33.5	1.2	34.7	1.3	36.0	1.3	30
40	27.0	.8	27.9	.9	29.0	.9	30.1	.9	31.2	1.0	32.3	1.0	33.5	.9	34.7	1.1	36.0	1.0	37.3	1.1	20
50	27.8	.6	28.8	.8	29.9	.8	31.0	.8	32.2	.8	33.3	.9	34.4	.9	35.8	.9	37.0	1.0	38.4	1.0	10
5 00	28.4	.7	29.6	.6	30.7	.6	31.8	.7	33.0	.7	34.2	.7	35.3	.8	36.7	.8	38.0	.8	39.4	.8	00
10	29.1	.5	30.2	.5	31.3	.5	32.5	.5	33.7	.6	34.9	.7	36.1	.7	37.5	.7	38.8	.7	40.2	.7	6 50
20	29.6	.4	30.7	.4	31.8	.5	33.0	.5	34.3	.4	35.6	.4	36.8	.5	38.2	.4	39.5	.5	40.9	.6	40
30	30.0	.3	31.1	.3	32.3	.3	33.5	.4	34.7	.4	36.0	.4	37.3	.3	38.6	.4	40.0	.4	41.5	.4	30
40	30.3	.2	31.4	.2	32.6	.2	33.9	.1	35.1	.1	36.4	.1	37.6	.2	39.0	.3	40.4	.3	41.9	.2	20
50	30.5	.0	31.6	.1	32.8	.1	34.0	.1	35.2	.1	36.5	.1	37.8	.1	39.3	.1	40.7	.1	42.1	.1	10
6 00	30.5		31.7		32.9		34.1		35.3		36.6		37.9		39.4		40.8		42.2		6 00

TABLE 28C.

[C = the 3d correction. Hor. Arg., the star's declination. Vert. Arg., B = the 2d correction.]

B.	88° 47′				88° 48′						88° 49′		
	20″	30″	40″	50″	0″	10″	20″	30″	40″	50″	0″	10″	20″
"	"	"	"	"	"	"	"	"	"	"	"	"	"
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	+0.2	+0.1	+0.1	+0.0	0.0	−0.0	−0.1	−0.1	−0.2	−0.2	−0.3	−0.4	−0.4
20	0.4	0.3	0.2	0.1	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8
30	0.6	0.5	0.3	0.1	0.0	0.1	0.3	0.5	0.6	0.7	0.8	1.1	1.2
40	0.8	0.6	0.4	0.2	0.0	0.2	0.4	0.6	0.8	1.0	1.2	1.5	1.6
50	+1.0	+0.7	+0.5	+0.2	0.0	−0.2	−0.5	−0.7	−1.0	−1.2	−1.5	−1.7	−2.1

TABLE 28B.

For finding the Latitude of a place by Altitudes of Polaris.

[B=the 2d correction. This correction is always additive.]

Star's hour angle.	Star's altitude. 44°		45°		46°		47°		48°		49°		50°		51°		52°		Star's hour angle.
h. m.	″		″		″		″		″		″		″		″		″		h. m.
0 00	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	0.0	.1	12 00
10	0.1	.2	0.1	.2	0.1	.2	0.1	.2	0.1	.3	0.1	.3	0.1	.3	0.1	.3	0.1	.3	11 50
20	0.3	.4	0.3	.4	0.3	.5	0.3	.5	0.4	.5	0.4	.5	0.4	.5	0.4	.6	0.4	.6	40
30	0.7	.6	0.7	.7	0.8	.6	0.8	.7	0.9	.6	0.9	.7	0.9	.7	1.0	.7	1.0	.8	30
40	1.3	.7	1.4	.7	1.4	.8	1.5	.8	1.5	.8	1.6	.8	1.6	.9	1.7	.9	1.8	1.0	20
50	2.0	.9	2.1	.9	2.2	1.0	2.3	.9	2.3	1.1	2.4	1.1	2.5	1.1	2.6	1.1	2.8	1.1	10
1 00	2.9	1.1	3.0	1.1	3.2	1.0	3.2	1.2	3.4	1.1	3.5	1.2	3.6	1.3	3.7	1.3	3.9	1.4	00
10	4.0	1.1	4.1	1.2	4.2	1.3	4.4	1.3	4.5	1.4	4.7	1.4	4.9	1.4	5.0	1.6	5.3	1.5	10 50
20	5.1	1.3	5.3	1.3	5.5	1.4	5.7	1.4	5.9	1.5	6.1	1.5	6.3	1.6	6.6	1.6	6.8	1.7	40
30	6.4	1.4	6.6	1.5	6.9	1.4	7.1	1.6	7.4	1.6	7.6	1.7	7.9	1.7	8.2	1.8	8.5	1.8	30
40	7.8	1.5	8.1	1.5	8.3	1.7	8.7	1.7	9.0	1.7	9.3	1.8	9.6	1.9	10.0	1.9	10.3	2.0	20
50	9.3	1.6	9.6	1.7	10.0	1.7	10.4	1.8	10.7	1.9	11.1	1.9	11.5	2.0	11.9	2.0	12.3	2.2	10
2 00	10.9	1.7	11.3	1.7	11.7	1.8	12.2	1.8	12.6	1.9	13.0	2.0	13.5	2.1	13.9	2.2	14.5	2.2	00
10	12.6	1.7	13.0	1.9	13.5	1.9	14.0	2.0	14.5	2.0	15.0	2.1	15.6	2.1	16.1	2.3	16.7	2.3	9 50
20	14.3	1.9	14.9	1.9	15.4	1.9	16.0	2.0	16.5	2.1	17.1	2.2	17.7	2.3	18.4	2.3	19.0	2.5	40
30	16.2	1.9	16.8	1.9	17.3	2.1	18.0	2.0	18.6	2.1	19.3	2.2	20.0	2.3	20.7	2.4	21.5	2.4	30
40	18.1	1.8	18.7	2.0	19.4	2.0	20.0	2.1	20.7	2.2	21.5	2.2	22.3	2.3	23.1	2.4	23.9	2.5	20
50	19.9	2.0	20.7	1.9	21.4	2.0	22.1	2.1	22.9	2.2	23.7	2.3	24.6	2.4	25.5	2.4	26.4	2.5	10
3 00	21.9	1.8	22.6	2.0	23.4	2.0	24.2	2.2	25.1	2.2	26.0	2.3	27.0	2.3	27.9	2.5	28.9	2.6	00
10	23.7	1.9	24.6	2.0	25.4	2.1	26.4	2.1	27.3	2.2	28.3	2.2	29.3	2.4	30.4	2.4	31.5	2.5	8 50
20	25.6	1.9	26.6	1.9	27.5	2.0	28.5	2.0	29.5	2.1	30.5	2.2	31.7	2.2	32.8	2.4	34.0	2.5	40
30	27.5	1.8	28.5	1.9	29.5	1.9	30.5	2.1	31.6	2.1	32.7	2.2	33.9	2.3	35.2	2.3	36.5	2.4	30
40	29.3	1.8	30.4	1.8	31.4	1.9	32.6	1.9	33.7	2.0	34.9	2.1	36.2	2.1	37.5	2.3	38.9	2.3	20
50	31.1	1.6	32.2	1.7	33.3	1.9	34.5	1.9	35.7	2.0	37.0	2.0	38.3	2.1	39.8	2.1	41.2	2.2	10
4 00	32.7	1.6	33.9	1.7	35.2	1.7	36.4	1.8	37.7	1.8	39.0	2.0	40.4	2.1	41.9	2.1	43.4	2.1	00
10	34.3	1.6	35.6	1.6	36.9	1.6	38.2	1.7	39.5	1.8	41.0	1.8	42.5	1.8	44.0	1.9	45.5	2.0	7 50
20	35.9	1.4	37.2	1.4	38.5	1.5	39.9	1.5	41.3	1.5	42.8	1.6	44.3	1.7	45.9	1.8	47.5	1.9	40
30	37.3	1.3	38.6	1.3	40.0	1.4	41.4	1.4	42.8	1.6	44.4	1.5	46.0	1.6	47.7	1.6	49.4	1.7	30
40	38.6	1.2	39.9	1.2	41.4	1.2	42.8	1.3	44.4	1.3	45.9	1.4	47.6	1.4	49.3	1.5	51.1	1.6	20
50	39.8	.9	41.1	1.1	42.6	1.1	44.1	1.2	45.7	1.2	47.3	1.3	49.0	1.3	50.8	1.3	52.7	1.3	10
5 00	40.7	.9	42.2	.9	43.7	.9	45.3	1.0	46.9	1.0	48.6	1.1	50.3	1.2	52.1	1.1	54.0	1.2	00
10	41.6	.8	43.1	.8	44.6	.8	46.3	.8	47.9	.8	49.7	.8	51.5	.9	53.2	1.0	55.2	.9	6 50
20	42.4	.5	43.9	.6	45.4	.7	47.1	.6	48.7	.7	50.5	.7	52.4	.7	54.2	.7	56.1	.8	40
30	42.9	.4	44.5	.4	46.1	.4	47.7	.4	49.4	.5	51.2	.5	53.1	.5	54.9	.6	56.9	.6	30
40	43.3	.3	44.9	.2	46.5	.2	48.1	.3	49.9	.2	51.7	.2	53.6	.3	55.5	.2	57.5	.3	20
50	43.6	.1	45.1	.2	46.7	.1	48.4	.1	50.1	.1	51.9	.2	53.9	.1	55.7	.2	57.8	.1	10
6 00	43.7		45.3		46.8		48.5		50.2		52.1		54.0		55.9		57.9		6 00

TABLE 28C.

[C=the 3d correction. Hor. Arg., the star's declination. Vert. Arg., B=the 2d correction.]

B.	88° 47′				88° 48′						88° 49′		
	20″	30″	40″	50″	0″	10″	20″	30″	40″	50″	0″	10″	20″
″	″	″	″	″	″	″	″	″	″	″	″	″	″
30	+0.6	+0.5	+0.3	+0.1	0.0	−0.1	−0.3	−0.5	−0.6	−0.7	−0.8	−1.1	−1.2
40	0.9	0.6	0.4	0.2	0.0	0.2	0.4	0.6	0.9	1.0	1.2	1.4	1.6
50	1.0	0.7	0.5	0.2	0.0	0.2	0.5	0.7	1.0	1.2	1.5	1.7	2.0
60	1.2	0.9	0.6	0.2	0.0	0.2	0.6	0.9	1.2	1.5	1.8	2.1	2.5
70	1.5	1.1	0.7	0.4	0.0	0.4	0.7	1.1	1.5	1.8	2.1	2.5	2.8
80	+1.6	+1.2	+0.8	+0.4	0.0	−0.4	−0.8	−1.2	−1.6	−2.1	−2.5	−2.8	−3.3

TABLE 28B.

For finding the Latitude of a place by Altitudes of Polaris.

[B=the 2d correction. This correction is always additive.]

Star's hour angle.	Star's altitude. 53°		54°		55°		56°		57°		58°		59°		60°		Star's hour angle.
h. m.	′ ″		′ ″		′ ″		′ ″		′ ″		′ ″		′ ″		′ ″		h. m.
0 00	0 0.0	0.1	0 0.0	0.1	0 0.0	0.1	0 0.0	0.2	0 0.0	0.2	0 0.0	0.2	0 0.0	0.2	0 0.0	0.2	12 00
10	0.1	0.4	0.1	0.4	0.1	0.4	0.2	0.3	0.2	0.3	0.2	0.4	0.2	0.4	0.2	0.4	11 50
20	0.5	0.5	0.5	0.5	0.5	0.6	0.5	0.6	0.5	0.7	0.6	0.6	0.6	0.7	0.6	0.7	40
30	1.0	0.8	1.0	0.8	1.1	0.8	1.1	0.9	1.2	0.9	1.2	1.0	1.3	0.9	1.3	1.0	30
40	1.8	1.0	1.8	1.1	1.9	1.1	2.0	1.1	2.1	1.1	2.2	1.2	2.2	1.3	2.3	1.3	20
50	2.8	1.2	2.9	1.3	3.0	1.3	3.1	1.4	3.2	1.5	3.4	1.5	3.5	1.5	3.6	1.7	10
1 00	4.0	1.4	4.2	1.4	4.3	1.5	4.5	1.6	4.7	1.6	4.9	1.7	5.0	1.8	5.3	1.8	00
10	0 5.4	1.6	0 5.6	1.7	0 5.8	1.7	0 6.1	1.8	0 6.3	1.9	0 6.6	1.8	0 6.8	2.0	0 7.1	2.0	10 50
20	7.0	1.8	7.3	1.8	7.5	2.0	7.9	1.9	8.2	2.0	8.4	2.2	8.8	2.2	9.1	2.4	40
30	8.8	1.9	9.1	2.0	9.5	2.0	9.8	2.1	10.2	2.3	10.6	2.4	11.0	2.4	11.5	2.5	30
40	10.7	2.1	11.1	2.2	11.5	2.3	11.9	2.4	12.5	2.3	13.0	2.5	13.4	2.6	14.0	2.7	20
50	12.8	2.2	13.3	2.3	13.8	2.3	14.3	2.5	14.8	2.6	15.5	2.6	16.0	2.8	16.7	2.9	10
2 00	15.0	2.3	15.6	2.4	16.1	2.5	16.8	2.5	17.4	2.7	18.1	2.7	18.8	2.9	19.6	3.0	00
10	0 17.3	2.4	0 18.0	2.5	0 18.6	2.7	0 19.3	2.8	0 20.1	2.8	0 20.8	3.0	0 21.7	3.1	0 22.6	3.2	9 50
20	19.7	2.5	20.5	2.6	21.3	2.7	22.1	2.8	22.9	2.9	23.8	3.0	24.8	3.1	25.8	3.3	40
30	22.2	2.6	23.1	2.6	24.0	2.7	24.9	2.8	25.8	3.0	26.8	3.1	27.9	3.2	29.1	3.3	30
40	24.8	2.6	25.7	2.7	26.7	2.8	27.7	2.9	28.8	3.0	29.9	3.1	31.1	3.2	32.4	3.4	20
50	27.4	2.7	28.4	2.7	29.5	2.8	30.6	2.9	31.8	3.0	33.0	3.2	34.3	3.3	35.8	3.4	10
3 00	30.1	2.5	31.1	2.7	32.3	2.8	33.5	3.0	34.8	3.1	36.2	3.2	37.6	3.3	39.2	3.4	00
10	0 32.6	2.6	0 33.8	2.7	0 35.1	2.8	0 36.5	2.9	0 37.9	3.0	0 39.4	3.1	0 40.9	3.3	0 42.6	3.4	8 50
20	35.2	2.6	36.5	2.7	37.9	2.8	39.4	2.8	40.9	2.9	42.5	3.1	44.2	3.2	46.0	3.3	40
30	37.8	2.5	39.2	2.6	40.7	2.6	42.2	2.8	43.8	2.9	45.6	3.0	47.4	3.1	49.3	3.3	30
40	40.3	2.4	41.8	2.5	43.3	2.6	45.0	2.7	46.7	2.9	48.6	2.9	50.5	3.0	52.6	3.1	20
50	42.7	2.3	44.3	2.4	45.9	2.5	47.7	2.6	49.6	2.6	51.5	2.8	53.5	2.9	55.7	3.1	10
4 00	45.0	2.2	46.7	2.3	48.4	2.4	50.3	2.5	52.2	2.6	54.3	2.6	56.4	2.8	58.8	2.8	00
10	0 47.2	2.1	0 49.0	2.1	0 50.8	2.3	0 52.8	2.3	0 54.8	2.4	0 56.9	2.5	0 59.2	2.7	1 1.6	2.8	7 50
20	49.3	2.0	51.1	2.0	53.1	2.1	55.1	2.2	57.2	2.3	59.4	2.4	1 1.9	2.4	1 4.4	2.5	40
30	51.3	1.8	53.1	1.9	55.2	1.9	57.3	1.9	59.5	2.1	1 1.8	2.1	1 4.3	2.2	1 6.9	2.3	30
40	53.1	1.5	55.0	1.6	57.1	1.7	59.2	1.8	1 1.6	1.8	1 3.9	2.0	1 6.5	2.0	1 9.2	2.1	20
50	54.6	1.5	56.6	1.5	58.8	1.5	1 1.0	1.6	1 3.4	1.6	1 5.9	1.7	1 8.5	1.8	1 11.3	1.8	10
5 00	56.1	1.2	58.1	1.3	1 0.3	1.3	1 2.6	1.3	1 5.0	1.4	1 7.6	1.4	1 10.3	1.5	1 13.1	1.6	00
10	0 57.3	0.9	0 59.4	1.0	1 1.6	1.1	1 3.9	1.1	1 6.4	1.2	1 9.0	1.2	1 11.8	1.3	1 14.7	1.4	6 50
20	58.2	0.8	1 0.4	0.8	1 2.7	0.8	1 5.0	0.9	1 7.6	0.9	1 10.2	1.0	1 13.1	0.9	1 16.1	0.9	40
30	59.0	0.6	1 1.2	0.6	1 3.5	0.7	1 5.9	0.7	1 8.5	0.7	1 11.2	0.6	1 14.0	0.8	1 17.0	0.8	30
40	59.6	0.3	1 1.8	0.3	1 4.2	0.3	1 6.6	0.4	1 9.2	0.4	1 11.8	0.4	1 14.8	0.4	1 17.8	0.4	20
50	59.9	0.1	1 2.1	0.2	1 4.5	0.2	1 7.0	0.1	1 9.6	0.1	1 12.2	0.2	1 15.2	0.2	1 18.2	0.2	10
6 00	1 0.0		1 2.3		1 4.7		1 7.1		1 9.7		1 12.4		1 15.4		1 18.4		6 00

TABLE 28C.

[C = the 3d correction. Hor. Arg., the star's declination. Vert. Arg., B = the 2d correction.]

B.	88° 47′ 20″	88° 47′ 30″	88° 47′ 40″	88° 47′ 50″	88° 48′ 0″	88° 48′ 10″	88° 48′ 20″	88° 48′ 30″	88° 48′ 40″	88° 48′ 50″	88° 49′ 0″	88° 49′ 10″	88° 49′ 20″
″	″	″	″	″	″	″	″	″	″	″	″	″	″
30	+0.6	+0.5	+0.3	+0.1	0.0	−0.1	−0.3	−0.5	−0.6	−0.7	−0.8	−1.1	−1.2
40	0.9	0.6	0.4	0.2	0.0	0.2	0.4	0.6	0.9	1.0	1.2	1.4	1.6
50	1.0	0.7	0.5	0.2	0.0	0.2	0.5	0.7	1.0	1.2	1.5	1.7	2.0
60	1.2	0.9	0.6	0.2	0.0	0.2	0.6	0.9	1.2	1.5	1.8	2.1	2.5
70	1.5	1.1	0.7	0.4	0.0	0.4	0.7	1.1	1.5	1.8	2.1	2.5	2.8
80	+1.6	+1.2	+0.8	+0.4	0.0	−0.4	−0.8	−1.2	−1.6	−2.1	−2.5	−2.8	−3.3

TABLE 28D.

For finding the Latitude of a place by Altitudes of Polaris.

[D=the 4th correction. (D has the same sign as A when the Dec. <88° 48′, the opposite sign when the Dec. >88° 48′.)]

[Vertical Argument, A = the 1st correction. Horizontal Argument, the star's declination.]

A.	Declination, 88° 47′								88° 48′						Proportional parts.			
	20″	25″	30″	35″	40″	45″	50″	55″	0″	5″	10″	15″	20″	25″	1″	2″	3″	4″
′	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	1.1	1.0	0.8	0.7	0.6	0.4	0.2	0.1	0.0	0.1	0.2	0.4	0.6	0.7	0.0	0.0	0.1	0.1
4	2.2	1.9	1.7	1.4	1.1	0.8	0.6	0.3	0.0	0.3	0.6	0.8	1.1	1.4	0.1	0.1	0.2	0.2
6	3.3	2.9	2.5	2.1	1.7	1.2	0.8	0.4	0.0	0.4	0.8	1.2	1.7	2.1	0.1	0.2	0.2	0.3
8	4.4	3.9	3.3	2.8	2.2	1.7	1.1	0.6	0.0	0.6	1.1	1.7	2.2	2.8	0.1	0.2	0.3	0.4
10	5.6	4.9	4.2	3.4	2.8	2.1	1.4	0.7	0.0	0.7	1.4	2.1	2.8	3.4	0.1	0.3	0.4	0.6
12	6.7	5.8	5.0	4.2	3.3	2.5	1.7	0.8	0.0	0.8	1.7	2.5	3.3	4.1	0.2	0.3	0.5	0.6
14	7.8	6.8	5.8	4.9	3.9	2.9	1.9	1.0	0.0	1.0	1.9	2.9	3.9	4.9	0.2	0.4	0.6	0.8
16	8.9	7.8	6.7	5.5	4.4	3.3	2.2	1.1	0.0	1.1	2.2	3.3	4.4	5.5	0.2	0.4	0.7	0.9
18	10.0	8.8	7.5	6.2	5.0	3.8	2.5	1.2	0.0	1.2	2.5	3.8	5.0	6.2	0.2	0.5	0.7	1.0
20	11.1	9.7	8.3	6.9	5.5	4.2	2.8	1.4	0.0	1.4	2.8	4.2	5.5	6.9	0.3	0.6	0.8	1.1
22	12.2	10.7	9.2	7.7	6.1	4.6	3.0	1.6	0.0	1.6	3.0	4.6	6.1	7.7	0.3	0.6	0.9	1.3
24	13.3	11.7	10.0	8.3	6.7	5.0	3.3	1.7	0.0	1.7	3.3	5.0	6.7	8.3	0.3	0.7	1.0	1.4
26	14.4	12.7	10.8	9.0	7.2	5.4	3.6	1.8	0.0	1.8	3.6	5.4	7.2	9.0	0.4	0.7	1.1	1.4
28	15.6	13.6	11.7	9.7	7.8	5.8	3.9	1.9	0.0	1.9	3.9	5.8	7.8	9.7	0.4	0.8	1.1	1.5
30	16.7	14.6	12.5	10.4	8.3	6.2	4.2	2.1	0.0	2.1	4.2	6.2	8.3	10.4	0.4	0.8	1.3	1.7
32	17.8	15.6	13.3	11.1	8.9	6.7	4.4	2.2	0.0	2.2	4.4	6.7	8.9	11.1	0.4	0.9	1.3	1.8
34	18.9	16.6	14.2	11.8	9.4	7.1	4.7	2.3	0.0	2.3	4.7	7.1	9.4	11.8	0.5	0.9	1.4	1.9
36	20.0	17.5	15.0	12.5	10.0	7.5	5.0	2.5	0.0	2.5	5.0	7.5	10.0	12.5	0.5	1.0	1.5	2.0
38	21.1	18.4	15.8	13.2	10.6	7.9	5.3	2.7	0.0	2.7	5.3	7.9	10.6	13.2	0.5	1.1	1.6	2.1
40	22.2	19.4	16.7	13.9	11.1	8.3	5.6	2.8	0.0	2.8	5.6	8.3	11.1	13.9	0.6	1.1	1.7	2.2
42	23.3	20.4	17.6	14.6	11.7	8.8	5.8	2.9	0.0	2.9	5.8	8.8	11.7	14.6	0.6	1.2	1.7	2.3
44	24.4	21.4	18.3	15.3	12.2	9.2	6.1	3.0	0.0	3.0	6.1	9.2	12.2	15.3	0.6	1.2	1.8	2.4
46	25.6	22.3	19.2	16.0	12.8	9.6	6.4	3.2	0.0	3.2	6.4	9.6	12.8	16.0	0.6	1.3	1.9	2.6
48	26.7	23.3	20.0	16.7	13.3	10.0	6.7	3.3	0.0	3.3	6.7	10.0	13.3	16.7	0.7	1.3	2.0	2.6
50	27.8	24.3	20.8	17.3	13.9	10.4	6.9	3.4	0.0	3.4	6.9	10.4	13.9	17.3	0.7	1.4	2.1	2.8
52	28.9	25.3	21.7	18.0	14.4	10.8	7.2	3.6	0.0	3.6	7.2	10.8	14.4	18.0	0.7	1.4	2.2	2.9
54	30.0	26.2	22.5	18.8	15.0	11.2	7.5	3.8	0.0	3.8	7.5	11.2	15.0	18.8	0.7	1.5	2.2	3.0
56	31.1	27.2	23.3	19.4	15.6	11.7	7.8	3.9	0.0	3.9	7.8	11.7	15.6	19.4	0.8	1.6	2.3	3.1
58	32.2	28.2	24.2	20.1	16.1	12.1	8.0	4.0	0.0	4.0	8.0	12.1	16.1	20.1	0.8	1.6	2.4	3.2
60	33.3	29.2	25.0	20.8	16.7	12.5	8.3	4.2	0.0	4.2	8.3	12.5	16.7	20.8	0.8	1.7	2.5	3.3
62	34.4	30.1	25.8	21.5	17.2	12.9	8.6	4.3	0.0	4.3	8.6	12.9	17.2	21.5	0.9	1.7	2.6	3.4
64	35.6	31.1	26.7	22.2	17.8	13.3	8.9	4.4	0.0	4.4	8.9	13.3	17.8	22.2	0.9	1.8	2.7	3.6
66	36.7	32.1	27.5	22.9	18.3	13.8	9.2	4.6	0.0	4.6	9.2	13.8	18.3	22.9	0.9	1.8	2.8	3.7
68	37.8	33.0	28.3	23.6	18.9	14.2	9.4	4.7	0.0	4.7	9.4	14.2	18.9	23.6	0.9	1.9	2.8	3.8
70	38.9	34.0	29.2	24.3	19.4	14.6	9.7	4.9	0.0	4.9	9.7	14.6	19.4	24.3	1.0	1.9	2.9	3.9
72	40.0	35.0	30.0	25.0	20.0	15.0	10.0	5.0	0.0	5.0	10.0	15.0	20.0	25.0	1.0	2.0	3.0	4.0

Proportional parts.

′ ″	″	″	″	″	″	″	″	″	″	″	″	″	″	″
0 20	0.2	0.2	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1
0 40	0.4	0.3	0.3	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2
1 00	0.6	0.5	0.4	0.4	0.3	0.2	0.1	0.1	0.0	0.1	0.1	0.2	0.3	0.4
1 20	0.7	0.7	0.5	0.5	0.4	0.2	0.1	0.1	0.0	0.1	0.1	0.2	0.4	0.5
1 40	0.9	0.8	0.7	0.6	0.5	0.3	0.2	0.1	0.0	0.1	0.2	0.3	0.5	0.6
2 00	1.1	1.0	0.8	0.7	0.6	0.4	0.2	0.1	0.0	0.1	0.2	0.4	0.6	0.7

TABLE 28D.

For finding the Latitude of a place by Altitudes of Polaris.

[D=the 4th correction. (D has the same sign as A when the Dec. <88° 48′, the opposite sign when the Dec. >88° 48′.)]

[Vertical Argument A=the 1st correction. Horizontal Argument, the star's declination.]

A.	Declination, 88° 48′						88° 49′					Proportional parts.			
	30″	35″	40″	45″	50″	55″	0″	5″	10″	15″	20″	1″	2″	3″	4″
′	″	″	″	″	″	″	″	″	″	″	″	″	″	″	″
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0.8	1.0	1.1	1.2	1.4	1.6	1.7	1.8	1.9	2.1	2.2	0.0	0.1	0.1	0.1
4	1.7	1.9	2.2	2.5	2.8	3.1	3.3	3.6	3.9	4.2	4.4	0.1	0.1	0.1	0.2
6	2.5	2.9	3.3	3.8	4.2	4.6	5.0	5.3	5.8	6.2	6.7	0.1	0.2	0.2	0.3
8	3.3	3.9	4.4	5.0	5.6	6.1	6.7	7.2	7.8	8.3	8.9	0.1	0.2	0.3	0.4
10	4.2	4.9	5.6	6.2	6.9	7.6	8.3	9.0	9.7	10.4	11.1	0.1	0.3	0.4	0.6
12	5.0	5.8	6.7	7.5	8.3	9.2	10.0	10.8	11.7	12.5	13.3	0.2	0.3	0.5	0.7
14	5.8	6.8	7.8	8.8	9.8	10.8	11.8	12.7	13.7	14.6	15.6	0.2	0.4	0.6	0.8
16	6.7	7.8	8.9	10.0	11.1	12.2	13.3	14.4	15.6	16.7	17.8	0.2	0.4	0.7	0.9
18	7.5	8.8	10.0	11.2	12.5	13.8	15.0	16.2	17.5	18.8	20.0	0.2	0.5	0.7	1.0
20	8.3	9.7	11.1	12.5	13.9	15.3	16.7	18.1	19.4	20.9	22.2	0.3	0.6	0.8	1.1
22	9.2	10.7	12.2	13.8	15.3	16.8	18.3	19.8	21.4	22.9	24.4	0.3	0.6	1.0	1.3
24	10.0	11.7	13.3	15.0	16.7	18.4	20.0	21.7	23.3	25.0	26.7	0.3	0.7	1.0	1.4
26	10.8	12.7	14.4	16.2	18.0	19.9	21.7	23.5	25.3	27.1	28.9	0.4	0.7	1.1	1.4
28	11.7	13.6	15.6	17.5	19.4	21.4	23.3	25.3	27.2	29.2	31.1	0.4	0.8	1.2	1.6
30	12.5	14.6	16.7	18.8	20.8	22.9	25.0	27.1	29.2	31.2	33.3	0.4	0.8	1.2	1.6
32	13.3	15.6	17.8	20.0	22.2	24.4	26.7	28.9	31.1	33.3	35.5	0.4	0.9	1.3	1.8
34	14.2	16.6	18.9	21.2	23.6	26.0	28.4	30.7	33.1	35.4	37.8	0.5	0.9	1.4	1.9
36	15.0	17.5	20.0	22.5	25.0	27.5	30.0	32.5	35.0	37.5	40.0	0.5	1.0	1.5	2.0
38	15.8	18.4	21.1	23.8	26.4	29.0	31.6	34.2	37.0	39.6	42.2	0.5	1.1	1.6	2.2
40	16.7	19.4	22.2	25.0	27.8	30.6	33.3	36.1	38.9	41.7	44.4	0.6	1.1	1.7	2.2
42	17.6	20.4	23.3	26.2	29.2	32.1	35.0	37.9	40.8	43.8	46.7	0.6	1.2	1.8	2.4
44	18.3	21.4	24.4	27.5	30.6	33.7	36.8	39.8	42.8	45.9	48.9	0.6	1.2	1.8	2.4
46	19.2	22.3	25.6	28.8	32.0	35.1	38.3	41.5	44.8	47.9	51.1	0.6	1.3	1.9	2.6
48	20.0	23.3	26.7	30.0	33.3	36.7	40.0	43.3	46.7	50.0	53.3	0.7	1.3	2.0	2.7
50	20.8	24.3	27.8	31.2	34.7	38.2	41.7	45.1	48.6	52.1	55.5	0.7	1.4	2.1	2.8
52	21.7	25.3	28.9	32.5	36.1	39.7	43.3	46.9	50.5	54.2	57.8	0.7	1.4	2.2	2.9
54	22.5	26.2	30.0	33.8	37.5	41.2	45.0	48.7	52.5	56.2	60.0	0.7	1.5	2.2	3.0
56	23.3	27.2	31.1	35.0	38.9	42.8	46.7	50.5	54.4	58.3	62.2	0.8	1.6	2.3	3.1
58	24.2	28.2	32.2	36.2	40.3	44.3	48.3	52.3	56.4	60.4	64.4	0.8	1.6	2.4	3.2
60	25.0	29.2	33.3	37.5	41.7	45.9	50.0	54.2	58.3	62.5	66.7	0.8	1.7	2.5	3.3
62	25.8	30.1	34.4	38.8	43.0	47.3	51.7	56.0	60.3	64.6	68.9	0.9	1.7	2.6	3.4
64	26.7	31.1	35.6	40.0	44.4	48.9	53.3	57.8	62.2	66.7	71.1	0.9	1.8	2.7	3.6
66	27.5	32.1	36.7	41.2	45.8	50.4	55.0	59.6	64.2	68.8	73.3	0.9	1.8	2.7	3.6
68	28.3	33.0	37.8	42.5	47.2	52.0	56.7	61.3	66.1	70.9	75.5	0.9	1.9	2.8	3.8
70	29.2	34.0	38.9	43.8	48.6	53.5	58.3	63.1	68.0	72.9	77.7	1.0	1.9	2.9	3.9
72	30.0	35.0	40.0	45.0	50.0	55.0	60.0	65.0	70.0	75.0	80.0	1.0	2.0	3.0	4.0

	Proportional parts.										
′ ″	″	″	″	″	″	″	″	″	″	″	″
0 20	0.1	0.1	0.1	0.2	0.2	0.3	0.3	0.3	0.3	0.3	0.4
0 40	0.2	0.3	0.4	0.4	0.5	0.5	0.6	0.6	0.6	0.7	0.7
1 00	0.4	0.5	0.6	0.6	0.7	0.8	0.8	0.9	0.9	1.0	1.1
1 20	0.5	0.7	0.7	0.8	0.9	1.1	1.1	1.2	1.3	1.4	1.5
1 40	0.6	0.8	0.9	1.0	1.1	1.3	1.4	1.5	1.6	1.7	1.8
2 00	0.8	1.0	1.1	1.2	1.4	1.6	1.7	1.8	1.9	2.1	2.2

TABLE 29.

Conversion Tables for Nautical and Statute Miles.

Nautical miles into statute miles.

1 nautical mile or knot = 6,080 feet.
1 statute mile = 5,280 feet.

Statute miles into nautical miles.

1 statute mile = 5,280 feet.
1 nautical mile or knot = 6,080 feet.

Nautical miles.	Statute miles.	Nautical miles.	Statute miles.	Nautical miles.	Statute miles.	Statute miles.	Nautical miles.	Statute miles.	Nautical miles.	Statute miles.	Nautical miles.
1.00	1.151	8.75	10.075	16.50	18.999	1.00	0.868	9.00	7.815	17.00	14.763
1.25	1.439	9.00	10.363	16.75	19.287	1.25	1.085	9.25	8.032	17.25	14.980
1.50	1.727	9.25	10.651	17.00	19.575	1.50	1.302	9.50	8.249	17.50	15.197
1.75	2.015	9.50	10.939	17.25	19.863	1.75	1.519	9.75	8.467	17.75	15.414
2.00	2.303	9.75	11.227	17.50	20.151	2.00	1.736	10.00	8.684	18.00	15.632
2.25	2.590	10.00	11.515	17.75	20.439	2.25	1.953	10.25	8.901	18.25	15.849
2.50	2.878	10.25	11.803	18.00	20.727	2.50	2.170	10.50	9.118	18.50	16.066
2.75	3.166	10.50	12.090	18.25	21.015	2.75	2.387	10.75	9.335	18.75	16.283
3.00	3.454	10.75	12.378	18.50	21.303	3.00	2.604	11.00	9.552	19.00	16.500
3.25	3.742	11.00	12.666	18.75	21.590	3.25	2.821	11.25	9.769	19.25	16.717
3.50	4.030	11.25	12.954	19.00	21.878	3.50	3.038	11.50	9.986	19.50	16.934
3.75	4.318	11.50	13.242	19.25	22.166	3.75	3.256	11.75	10.203	19.75	17.151
4.00	4.606	11.75	13.530	19.50	22.454	4.00	3.473	12.00	10.420	20.00	17.369
4.25	4.893	12.00	13.818	19.75	22.742	4.25	3.690	12.25	10.638	20.25	17.586
4.50	5.181	12.25	14.106	20.00	23.030	4.50	3.907	12.50	10.855	20.50	17.803
4.75	5.469	12.50	14.393	20.25	23.318	4.75	4.124	12.75	11.072	20.75	18.020
5.00	5.757	12.75	14.681	20.50	23.606	5.00	4.341	13.00	11.289	21.00	18.237
5.25	6.045	13.00	14.969	20.75	23.893	5.25	4.559	13.25	11.507	21.25	18.454
5.50	6.333	13.25	15.257	21.00	24.181	5.50	4.776	13.50	11.724	21.50	18.671
5.75	6.621	13.50	15.545	21.25	24.469	5.75	4.994	13.75	11.941	21.75	18.888
6.00	6.909	13.75	15.833	21.50	24.757	6.00	5.211	14.00	12.158	22.00	19.105
6.25	7.196	14.00	16.121	21.75	25.045	6.25	5.428	14.25	12.376	22.25	19.322
6.50	7.484	14.25	16.409	22.00	25.333	6.50	5.645	14.50	12.593	22.50	19.539
6.75	7.772	14.50	16.696	22.25	25.621	6.75	5.862	14.75	12.810	22.75	19.756
7.00	8.060	14.75	16.984	22.50	25.909	7.00	6.079	15.00	13.027	23.00	19.973
7.25	8.348	15.00	17.272	22.75	26.196	7.25	6.296	15.25	13.244	23.25	20.191
7.50	8.636	15.25	17.560	23.00	26.484	7.50	6.513	15.50	13.461	23.50	20.408
7.75	8.924	15.50	17.848	23.50	27.060	7.75	6.730	15.75	13.678	23.75	20.625
8.00	9.212	15.75	18.136	24.00	27.636	8.00	6.947	16.00	13.895	24.00	20.842
8.25	9.500	16.00	18.424	24.50	28.212	8.25	7.164	16.25	14.112	24.25	21.060
8.50	9.787	16.25	18.712	25.00	28.787	8.50	7.381	16.50	14.329	24.50	21.277
						8.75	7.598	16.75	14.546	25.00	21.711

TABLE 30.

Conversion Tables for Metric and English Linear Measure.

Metric to English.

Meters.	Feet.	Yards.	Statute miles.	Nautical miles.
1	3. 280 833 3	1. 093 611 1	0. 000 621 369	0. 000 539 593
2	6. 561 666 7	2. 187 222 2	. 001 242 738	. 001 079 185
3	9. 842 500 0	3. 280 833 3	. 001 864 106	. 001 618 778
4	13. 123 333 3	4. 374 444 4	. 002 485 475	. 002 158 370
5	16. 404 166 7	5. 468 055 6	. 003 106 844	. 002 697 963
6	19. 685 000 0	6. 561 666 7	. 003 728 213	. 003 237 556
7	22. 965 833 3	7. 655 277 8	. 004 349 582	. 003 777 148
8	26. 246 666 7	8. 748 888 9	. 004 970 950	. 004 316 741
9	29. 527 500 0	9. 842 500 0	. 005 592 319	. 004 856 333

English to metric.

No.	Feet to meters.	Yards to meters.	Statute miles to meters.	Nautical miles to meters.
1	0. 304 800 6	0. 914 401 8	1, 609. 35	1, 853. 25
2	0. 609 601 2	1. 828 803 7	3, 218. 70	3, 706. 50
3	0. 914 401 8	2. 743 205 5	4, 828. 05	5, 559. 75
4	1. 219 202 4	3. 657 607 3	6, 437. 40	7, 413. 00
5	1. 524 003 0	4. 572 009 1	8, 046. 75	9, 266. 25
6	1. 828 803 7	5. 486 411 0	9, 656. 10	11, 119. 50
7	2. 133 604 3	6. 400 812 8	11, 265. 45	12, 972. 75
8	2. 438 404 9	7. 315 214 6	12, 874. 80	14, 826. 00
9	2. 743 205 5	8. 229 616 5	14, 484. 15	16, 679. 25

TABLE 31.

Conversion Tables for Thermometer Scales.

[F°=Fahrenheit temperature; C°=Centigrade temperature; R°=Réaumur temperature.]

Equivalent temperatures—Fahr., Cent., Réau

$R° = \frac{4}{5} C° = \frac{4}{9} (F° - 32°)$.
$C° = \frac{5}{4} R° = \frac{5}{9} (F° - 32°)$.

F°.	C°.	R°.	F°.	C°.	R°.
1	−17.2	−13.8	51	+10.6	+ 8.4
2	16.7	13.3	52	11.1	8.9
3	16.1	12.9	53	11.7	9.3
4	15.6	12.4	54	12.2	9.8
5	15.0	12.0	55	12.8	10.2
6	14.4	11.6	56	13.3	10.7
7	13.9	11.1	57	13.9	11.1
8	13.3	10.7	58	14.4	11.6
9	12.8	10.2	59	15.0	12.0
10	12.2	9.8	60	15.6	12.4
11	11.7	9.3	61	16.1	12.9
12	11.1	8.9	62	16.7	13.3
13	10.6	8.4	63	17.2	13.8
14	10.0	8.0	64	17.8	14.2
15	9.4	7.6	65	18.3	14.7
16	8.9	7.1	66	18.9	15.1
17	8.3	6.7	67	19.4	15.6
18	7.8	6.2	68	20.0	16.0
19	7.2	5.8	69	20.6	16.4
20	6.7	5.3	70	21.1	16.9
21	6.1	4.9	71	21.7	17.3
22	5.6	4.4	72	22.2	17.8
23	5.0	4.0	73	22.8	18.2
24	4.4	3.6	74	23.3	18.7
25	3.9	3.1	75	23.9	19.1
26	3.3	2.7	76	24.4	19.6
27	2.8	2.2	77	25.0	20.0
28	2.2	1.8	78	25.6	20.4
29	1.7	1.3	79	26.1	20.9
30	1.1	0.9	80	26.7	21.3
31	− 0.6	− 0.4	81	27.2	21.8
32	0.0	0.0	82	27.8	22.2
33	+ 0.6	+ 0.4	83	28.3	22.7
34	1.1	0.9	84	28.9	23.1
35	1.7	1.3	85	29.4	23.6
36	2.2	1.8	86	30.0	24.0
37	2.8	2.2	87	30.6	24.4
38	3.3	2.7	88	31.1	24.9
39	3.9	3.1	89	31.7	25.3
40	4.4	3.6	90	32.2	25.8
41	5.0	4.0	91	32.8	26.2
42	5.6	4.4	92	33.3	26.7
43	6.1	4.9	93	33.9	27.1
44	6.7	5.3	94	34.4	27.6
45	7.2	5.8	95	35.0	28.0
46	7.8	6.2	96	35.6	28.4
47	8.3	6.7	97	36.1	28.9
48	8.9	7.1	98	36.7	29.3
49	9.4	7.6	99	37.2	29.8
50	+10.0	+ 8.0	100	+37.8	+30.2

Equivalent temperatures—Centigrade and Fahrenheit.

$F° = \frac{9}{5} C° + 32°$.

C°.	F°.	C°.	F°.	C°.	F°.	C°.	F°.	C°.	F°.
−10	14.0	0	32.0	10	50.0	20	68.0	30	86.0
− 9	15.8	1	33.8	11	51.8	21	69.8	31	87.8
− 8	17.6	2	35.6	12	53.6	22	71.6	32	89.6
− 7	19.4	3	37.4	13	55.4	23	73.4	33	91.4
− 6	21.2	4	39.2	14	57.2	24	75.2	34	93.2
− 5	23.0	5	41.0	15	59.0	25	77.0	35	95.0
− 4	24.8	6	42.8	16	60.8	26	78.8	36	96.8
− 3	26.6	7	44.6	17	62.6	27	80.6	37	98.6
− 2	28.4	8	46.4	18	64.4	28	82.4	38	100.4
− 1	30.2	9	48.2	19	66.2	29	84.2	39	102.2

Equivalent temperatures—Réaumur and Fahrenheit.

$F° = \frac{9}{4} R° + 32°$.

R°.	F°.	R°.	F°.	R°.	F°.	R°.	F°.
−10	9.5	0	32.0	10	54.5	20	77.0
− 9	11.8	1	34.2	11	56.8	21	79.2
− 8	14.0	2	36.5	12	59.0	22	81.5
− 7	16.2	3	38.8	13	61.2	23	83.8
− 6	18.5	4	41.0	14	63.5	24	86.0
− 5	20.8	5	43.2	15	65.8	25	88.2
− 4	23.0	6	45.5	16	68.0	26	90.5
− 3	25.2	7	47.8	17	70.2	27	92.8
− 2	27.5	8	50.0	18	72.5	28	95.0
− 1	29.8	9	52.2	19	74.8	29	97.2

TABLE 32.

To obtain the True Force and Direction of the Wind from its Apparent Force and Direction on a Moving Vessel.

Apparent force of the wind (Beaufort scale).	Speed of vessel, knots.	Apparent direction of the wind (points off the bow).																																	
		0		1		2		3		4		5		6		7		8		9		10		11		12		13		14		15		16	
		True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.	True direction, points off the bow.	True force, Beaufort scale.
0	10	16	1	16	1	15	1	15	1	15	1	15	1	15	2	15	2	15	2	15	2	15	2	15	2	15	2	15	2	15	2	16	2	16	2
	15	16	2	16	2	16	2	15	2	15	2	15	2	15	3	15	3	15	3	15	3	15	3	15	3	15	3	16	3	16	3	16	3	16	3
	20	16	3	16	3	16	3	16	4	15	4	15	4	15	4	15	4	15	4	15	4	15	4	15	4	16	4	16	5	16	5	16	5	16	5
1	10	16	0	14	0	13	0	12	1	12	1	12	1	12	2	13	2	13	2	13	2	14	3	14	3	14	3	15	3	15	3	16	3	16	3
	15	16	1	15	1	14	2	14	2	14	2	14	2	14	3	14	3	14	3	14	3	14	4	14	4	15	4	15	4	15	4	16	4	16	4
	20	16	2	15	2	15	3	15	3	14	3	14	3	14	4	14	4	14	4	14	4	15	5	15	5	15	5	15	5	15	5	16	5	16	5
2	10	0	0	6	0	7	0	8	1	9	1	10	2	10	2	11	3	12	3	12	3	13	3	13	4	14	4	14	4	15	4	15	4	16	4
	15	16	0	13	0	12	1	12	1	12	2	12	2	12	3	12	3	13	4	13	4	13	4	14	5	14	5	15	5	15	5	16	5	16	5
	20	16	1	15	2	14	2	13	2	13	3	13	3	13	4	13	4	13	5	14	5	14	5	14	6	15	6	15	6	15	6	16	6	16	6
3	10	0	1	3	1	5	1	6	2	8	2	8	2	9	3	10	3	11	4	12	4	12	4	13	5	14	5	14	5	15	5	15	5	16	5
	15	0	0	8	0	8	1	9	1	10	2	10	3	11	3	11	4	12	4	12	5	13	5	13	6	14	6	14	6	15	6	15	6	16	6
	20	16	0	13	1	12	1	12	2	12	3	12	3	12	4	12	5	13	5	13	6	13	6	14	6	14	7	15	7	15	7	16	7	16	7
4	10	0	2	2	2	4	2	6	2	7	3	8	3	9	4	10	4	10	4	11	5	12	5	13	5	13	6	14	6	15	6	15	6	16	6
	15	0	1	4	1	6	1	7	2	8	3	9	3	10	4	11	5	11	5	12	6	12	6	13	6	14	7	14	7	15	7	15	7	16	7
	20	.....	0	9	0	9	1	10	2	10	3	10	4	11	4	12	5	12	5	12	6	13	7	14	7	14	7	14	8	15	8	16	8	16	8
5	10	0	3	2	3	3	3	5	3	6	4	7	4	8	5	9	5	10	5	11	6	12	6	12	6	13	7	14	7	15	7	15	7	16	7
	15	0	2	3	2	5	2	6	3	7	3	8	4	9	5	10	5	11	6	12	6	12	7	13	7	14	7	14	7	15	8	15	8	16	8
	20	0	0	5	1	7	2	8	3	9	3	10	3	10	5	11	6	12	6	12	7	13	7	13	8	14	8	14	8	15	8	15	8	16	8
6	10	0	4	2	4	3	4	4	4	6	5	7	5	8	6	9	6	10	6	11	7	11	7	12	7	13	7	14	7	14	8	15	8	16	8
	15	0	3	2	3	4	3	5	4	7	4	8	5	9	6	10	6	10	7	11	7	12	7	13	8	13	8	14	8	15	8	15	8	16	8
	20	0	2	3	2	5	2	7	3	8	4	9	5	10	6	10	7	11	7	12	7	12	8	13	8	14	8	14	9	14	9	15	9	16	9
7	10	0	5	1	5	3	5	4	6	5	6	6	6	7	7	8	7	9	7	10	7	11	8	12	8	13	8	14	8	14	8	15	8	16	8
	15	0	4	2	4	3	4	5	5	6	5	7	6	8	6	9	7	10	7	11	8	12	8	12	8	13	9	14	9	15	9	15	9	16	9
	20	0	3	2	3	4	4	6	4	7	5	8	6	9	7	10	7	11	8	11	8	12	9	13	9	13	9	14	9	15	10	15	10	16	10
8	10	0	6	1	6	3	7	4	7	5	7	6	7	7	8	8	8	9	8	10	8	11	9	12	9	13	9	14	9	14	9	15	9	16	9
	15	0	5	2	6	3	6	4	6	6	7	7	7	8	8	9	8	10	8	11	9	11	9	12	9	13	10	14	10	15	10	15	10	16	10
	20	0	4	2	5	4	5	5	6	6	6	8	7	9	8	9	8	10	9	11	9	12	10	13	10	13	10	14	10	15	10	15	11	16	11
9	10	0	8	1	8	2	8	4	8	5	8	6	8	7	9	8	9	9	9	10	9	11	10	12	10	13	10	13	10	14	10	15	10	16	10
	15	0	7	1	7	3	7	4	7	5	8	6	8	8	8	9	9	10	9	10	10	11	10	12	10	13	10	14	11	14	11	15	11	16	11
	20	0	6	2	6	3	6	5	7	6	7	7	8	8	8	9	8	10	9	11	10	12	10	12	10	13	11	14	11	15	11	15	11	16	11
10	10	0	9	1	9	2	9	4	9	5	9	6	9	7	10	8	10	9	10	10	10	11	11	12	11	13	11	13	11	14	11	15	11	16	11
	15	0	8	1	8	3	8	4	8	5	9	6	9	7	9	8	10	9	10	10	11	11	11	12	11	13	11	14	11	14	11	15	11	16	11
	20	0	7	2	7	3	8	4	8	6	8	7	9	8	9	9	10	10	10	11	11	11	11	12	11	13	12	14	12	15	12	16	12	16	12
11	10	0	10	1	10	2	10	4	10	5	10	6	10	7	11	8	11	9	11	10	11	11	11	12	11	12	12	13	12	14	12	15	12	16	12
	15	0	9	1	9	3	9	4	10	5	10	6	10	7	11	8	11	9	11	10	11	11	12	12	12	13	12	14	12	14	12	15	12	16	12
	20	0	9	1	9	3	9	4	9	5	10	7	10	8	10	9	11	10	11	10	12	11	12	12	12	13	12	14	12	14	12	15	12	16	12
12	10	0	11	1	11	2	11	3	11	4	11	6	12	7	12	8	12	9	12	10	12	11	12	12	12	12	12	13	12	14	12	15	12	16	12
	15	0	11	1	11	2	11	4	11	5	11	6	11	7	12	8	12	9	12	10	12	11	12	12	12	13	12	13	12	14	12	15	12	16	12
	20	0	10	1	10	3	10	4	11	5	11	6	11	7	12	8	12	9	12	10	12	11	12	12	12	13	12	14	12	14	12	15	12	16	12

TABLE 33.

Distance by Vertical Angle.

Dist., knots.	Heights in feet. 40	45	50	55	60	65	70	75	80	85	90	95	100	110	120	130	140	150
	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′
0.1	3 46	4 14	4 42	5 10	5 38	6 06	6 34	7 02	7 30	7 58	8 25	8 53	9 20	10 15	11 10	12 04	12 58	13 52
.2	1 53	2 07	2 21	2 35	2 49	3 04	3 18	3 32	3 46	4 00	4 14	4 28	4 42	5 10	5 38	6 06	6 34	7 02
.3	1 15	1 25	1 34	1 44	1 53	2 02	2 12	2 21	2 31	2 40	2 49	2 59	3 08	3 27	3 46	4 05	4 23	4 42
.4	0 57	1 04	1 11	1 18	1 25	1 32	1 39	1 46	1 53	2 00	2 07	2 14	2 21	2 35	2 49	3 04	3 18	3 32
0.5	0 45	0 51	0 57	1 02	1 08	1 14	1 19	1 25	1 30	1 36	1 42	1 47	1 53	2 04	2 16	2 27	2 38	2 49
.6	0 38	0 42	0 47	0 52	0 57	1 01	1 06	1 11	1 15	1 20	1 25	1 30	1 34	1 44	1 53	2 02	2 12	2 21
.7	0 32	0 36	0 40	0 44	0 48	0 53	0 57	1 01	1 05	1 09	1 13	1 17	1 21	1 29	1 37	1 45	1 53	2 01
.8	0 28	0 32	0 35	0 39	0 42	0 46	0 49	0 53	0 57	1 00	1 04	1 07	1 11	1 18	1 25	1 32	1 39	1 46
.9	0 25	0 28	0 31	0 35	0 38	0 41	0 44	0 47	0 50	0 53	0 57	1 00	1 03	1 09	1 15	1 22	1 28	1 34
1.0	0 23	0 25	0 28	0 31	0 34	0 37	0 40	0 42	0 45	0 48	0 51	0 54	0 57	1 02	1 08	1 14	1 19	1 25
.1	0 21	0 23	0 26	0 28	0 31	0 33	0 36	0 39	0 41	0 44	0 46	0 49	0 51	0 57	1 02	1 07	1 12	1 17
.2	0 19	0 21	0 24	0 26	0 28	0 31	0 33	0 35	0 38	0 40	0 42	0 45	0 47	0 52	0 57	1 01	1 06	1 11
.3	0 17	0 20	0 22	0 24	0 26	0 28	0 30	0 33	0 35	0 37	0 39	0 41	0 44	0 48	0 52	0 57	1 01	1 05
.4	0 16	0 18	0 20	0 22	0 24	0 26	0 28	0 30	0 32	0 34	0 36	0 38	0 40	0 44	0 48	0 53	0 57	1 01
1.5	0 15	0 17	0 19	0 21	0 23	0 25	0 26	0 28	0 30	0 32	0 34	0 36	0 38	0 41	0 45	0 49	0 53	0 57
.6	0 14	0 16	0 18	0 19	0 21	0 23	0 25	0 27	0 28	0 30	0 32	0 34	0 35	0 39	0 42	0 46	0 49	0 53
.7	0 13	0 15	0 17	0 18	0 20	0 22	0 23	0 25	0 27	0 28	0 30	0 32	0 33	0 37	0 40	0 43	0 47	0 50
.8	0 13	0 14	0 16	0 17	0 19	0 20	0 22	0 24	0 25	0 27	0 28	0 30	0 31	0 35	0 38	0 41	0 44	0 47
.9	0 12	0 13	0 15	0 16	0 18	0 19	0 21	0 22	0 24	0 25	0 27	0 28	0 30	0 33	0 36	0 39	0 42	0 45
2.0	0 11	0 13	0 14	0 16	0 17	0 18	0 20	0 21	0 23	0 24	0 25	0 27	0 28	0 31	0 34	0 37	0 40	0 42
.1	0 11	0 13	0 14	0 15	0 16	0 18	0 19	0 20	0 22	0 23	0 24	0 26	0 27	0 30	0 32	0 35	0 38	0 40
.2	0 10	0 12	0 13	0 14	0 15	0 17	0 18	0 19	0 21	0 22	0 23	0 24	0 26	0 28	0 31	0 33	0 36	0 39
.3	0 10	0 12	0 12	0 14	0 14	0 16	0 17	0 18	0 20	0 21	0 22	0 23	0 25	0 27	0 30	0 32	0 34	0 37
.4	0 10	0 11	0 12	0 13	0 14	0 15	0 17	0 18	0 19	0 20	0 21	0 22	0 24	0 26	0 28	0 31	0 33	0 35
2.5	0 9	0 11	0 11	0 12	0 13	0 15	0 16	0 17	0 18	0 19	0 20	0 21	0 23	0 25	0 27	0 29	0 32	0 34
.6	0 9	0 10	0 11	0 12	0 13	0 14	0 15	0 16	0 17	0 18	0 20	0 21	0 22	0 24	0 26	0 28	0 30	0 33
.7	0 9	0 10	0 10	0 11	0 12	0 14	0 15	0 16	0 17	0 18	0 19	0 20	0 21	0 23	0 25	0 27	0 29	0 31
.8	0 8	0 9	0 10	0 11	0 12	0 13	0 14	0 15	0 16	0 17	0 18	0 19	0 20	0 22	0 24	0 26	0 28	0 30
.9	0 8	0 9	0 10	0 10	0 11	0 13	0 14	0 15	0 16	0 17	0 18	0 19	0 20	0 21	0 23	0 25	0 27	0 29
3.0	0 8	0 9	0 9	0 10	0 10	0 12	0 13	0 14	0 15	0 16	0 17	0 18	0 19	0 21	0 23	0 25	0 26	0 28
.2							0 12	0 13	0 14	0 15	0 16	0 17	0 18	0 19	0 21	0 23	0 25	0 27
.4							0 12	0 12	0 13	0 14	0 15	0 16	0 17	0 18	0 20	0 22	0 23	0 25
.6							0 11	0 12	0 13	0 13	0 14	0 15	0 16	0 17	0 19	0 20	0 22	0 24
.8							0 10	0 11	0 12	0 13	0 13	0 14	0 15	0 16	0 18	0 19	0 21	0 22
4.0							0 10	0 11	0 11	0 12	0 13	0 13	0 14	0 16	0 17	0 18	0 20	0 21
.2										0 11	0 12	0 13	0 14	0 15	0 16	0 17	0 19	0 20
.4										0 11	0 12	0 12	0 13	0 14	0 15	0 17	0 18	0 19
.6										0 10	0 11	0 12	0 13	0 14	0 15	0 16	0 17	0 18
.8										0 10	0 11	0 11	0 12	0 13	0 14	0 15	0 16	0 18
5.0										0 10	0 10	0 11	0 11	0 12	0 14	0 15	0 16	0 17

TABLE 33.

Distance by Vertical Angle.

Dist., knots.	160	170	180	190	200	300	400	500	600	700	800	900	1,000	1,200	1,400	1,600	1,800	2,000
	Heights in feet.																	
	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′
0.1	14 45	15 37	16 29	17 21	18 13	26 16												
.2	7 30	7 58	8 25	8 53	9 20	13 52	18 13	22 21	26 16	29 56								
.3	5 01	5 19	5 38	5 57	6 15	9 20	12 22	15 20	18 13	21 00	23 41	26 16	28 44					
.4	3 46	4 00	4 14	4 28	4 42	7 02	9 20	11 37	13 52	16 03	18 13	20 18	22 21	26 16	29 56			
0.5	3 01	3 12	3 23	3 35	3 46	5 38	7 30	9 20	11 10	12 58	14 45	16 30	18 13	21 32	24 44	27 46	30 38	
.6	2 31	2 40	2 49	2 59	3 08	4 42	6 15	7 48	9 20	10 52	12 22	13 52	15 20	18 13	21 00	23 41	26 16	28 44
.7	2 09	2 17	2 25	2 33	2 41	4 02	5 22	6 42	8 01	9 20	10 39	11 56	13 13	15 45	18 13	20 36	22 56	25 10
.8	1 53	2 00	2 07	2 14	2 21	3 32	4 42	5 52	7 02	8 11	9 20	10 29	11 37	13 52	16 03	18 13	20 18	22 21
.9	1 40	1 47	1 53	1 59	2 06	3 08	4 11	5 13	6 15	7 17	8 19	9 20	10 21	12 22	14 21	16 18	18 13	20 05
1.0	1 30	1 36	1 42	1 47	1 53	2 49	3 46	4 42	5 38	6 34	7 30	8 25	9 20	11 10	12 58	14 45	16 29	18 13
.1	1 22	1 27	1 33	1 38	1 43	2 34	3 25	4 17	5 08	5 59	6 49	7 40	8 30	10 10	11 49	13 27	15 04	16 39
.2	1 15	1 20	1 25	1 30	1 34	2 21	3 08	3 55	4 42	5 29	6 15	7 02	7 48	9 20	10 52	12 22	13 52	15 20
.3	1 10	1 14	1 18	1 23	1 27	2 10	2 54	3 37	4 20	5 04	5 47	6 30	7 13	8 38	10 03	11 27	12 50	14 12
.4	1 05	1 09	1 13	1 17	1 21	2 01	2 41	3 22	4 02	4 42	5 22	6 02	6 42	8 01	9 20	10 39	11 56	13 13
1.5	1 00	1 04	1 08	1 12	1 15	1 53	2 31	3 08	3 46	4 23	5 01	5 38	6 15	7 30	8 44	9 57	11 10	12 22
.6	0 57	1 00	1 04	1 07	1 11	1 46	2 21	2 57	3 32	4 07	4 42	5 17	5 52	7 02	8 11	9 20	10 29	11 37
.7	0 53	0 57	1 00	1 03	1 07	1 40	2 13	2 46	3 19	3 52	4 26	4 59	5 32	6 38	7 43	8 48	9 53	10 57
.8	0 50	0 53	0 57	1 00	1 03	1 34	2 06	2 37	3 08	3 40	4 11	4 42	5 13	6 15	7 17	8 19	9 20	10 21
.9	0 48	0 51	0 54	0 57	1 00	1 29	1 59	2 29	2 58	3 28	3 58	4 27	4 57	5 56	6 55	7 54	8 52	9 50
2.0	0 45	0 48	0 51	0 54	0 57	1 25	1 53	2 21	2 49	3 18	3 46	4 14	4 42	5 38	6 34	7 30	8 25	9 20
.1	0 43	0 46	0 48	0 51	0 54	1 21	1 48	2 15	2 41	3 08	3 35	4 02	4 29	5 22	6 15	7 08	8 01	8 53
.2	0 41	0 44	0 46	0 49	0 51	1 17	1 43	2 08	2 34	3 00	3 25	3 51	4 17	5 08	5 59	6 49	7 40	8 30
.3	0 39	0 42	0 44	0 47	0 49	1 14	1 38	2 03	2 27	2 52	3 16	3 41	4 05	4 55	5 44	6 32	7 21	8 09
.4	0 38	0 40	0 42	0 45	0 47	1 11	1 34	1 58	2 21	2 45	3 08	3 32	3 55	4 42	5 29	6 15	7 02	7 48
2.5	0 36	0 38	0 41	0 43	0 45	1 08	1 30	1 53	2 16	2 38	3 01	3 23	3 46	4 31	5 16	6 01	6 45	7 30
.6	0 35	0 37	0 39	0 41	0 44	1 05	1 27	1 49	2 10	2 32	2 54	3 16	3 37	4 20	5 04	5 47	6 30	7 13
.7	0 34	0 36	0 38	0 40	0 42	1 03	1 24	1 45	2 06	2 27	2 47	3 08	3 29	4 11	4 53	5 34	6 15	6 57
.8	0 32	0 34	0 36	0 38	0 40	1 01	1 21	1 41	2 01	2 21	2 41	3 02	3 22	4 02	4 42	5 22	6 02	6 42
.9	0 31	0 33	0 35	0 37	0 39	0 58	1 18	1 37	1 57	2 16	2 36	2 55	3 15	3 54	4 32	5 11	5 50	6 28
3.0	0 30	0 32	0 34	0 36	0 38	0 57	1 15	1 34	1 53	2 12	2 31	2 49	3 08	3 46	4 23	5 01	5 38	6 15
.2	0 28	0 30	0 32	0 34	0 35	0 53	1 11	1 28	1 46	2 04	2 21	2 39	2 57	3 32	4 07	4 42	5 17	5 52
.4	0 27	0 28	0 30	0 32	0 33	0 50	1 07	1 23	1 40	1 56	2 13	2 30	2 46	3 19	3 52	4 26	4 59	5 32
.6	0 25	0 27	0 28	0 30	0 31	0 47	1 03	1 19	1 34	1 50	2 06	2 21	2 37	3 08	3 40	4 11	4 42	5 13
.8	0 24	0 25	0 27	0 28	0 30	0 45	1 00	1 14	1 29	1 44	1 59	2 14	2 29	2 58	3 28	3 58	4 27	4 57
4.0	0 23	0 24	0 25	0 27	0 28	0 42	0 57	1 11	1 25	1 39	1 53	2 07	2 21	2 49	3 18	3 46	4 14	4 42
.2	0 22	0 23	0 24	0 26	0 27	0 40	0 54	1 07	1 21	1 34	1 48	2 01	2 15	2 41	3 08	3 35	4 02	4 29
.4	0 21	0 22	0 23	0 24	0 26	0 39	0 51	1 04	1 17	1 30	1 43	1 56	2 08	2 34	3 00	3 25	3 51	4 17
.6	0 20	0 21	0 22	0 23	0 25	0 37	0 49	1 01	1 14	1 26	1 38	1 51	2 03	2 27	2 52	3 16	3 41	4 05
.8	0 19	0 20	0 21	0 22	0 24	0 35	0 47	0 59	1 11	1 22	1 34	1 46	1 58	2 21	2 45	3 08	3 32	3 55
5.0	0 18	0 19	0 20	0 21	0 23	0 34	0 45	0 57	1 08	1 19	1 30	1 42	1 53	2 16	2 38	3 01	3 23	3 46

TABLE 34.

For finding the distance of an object by an angle, measured from an elevated position, between the object and the horizon beyond.

Dist., yards.	Height of the Eye Above the Level of the Sea, in Feet.											Dist., yards.
	20	30	40	50	60	70	80	90	100	110	120	
	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	° ′	
100	3 44	5 37	7 29	9 21	11 11	13 00	14 47	16 34	18 16	19 58	21 37	100
200	1 50	2 46	3 43	4 39	5 35	6 31	7 27	8 23	9 18	10 13	11 08	200
300	1 12	1 49	2 26	3 04	3 41	4 19	4 56	5 33	6 11	6 48	7 25	300
400	52	1 21	1 48	2 16	2 44	3 12	3 40	4 08	4 36	5 04	5 32	400
500	41	1 03	1 25	1 48	2 10	2 32	2 54	3 17	3 39	4 01	4 24	500
600	34	52	1 10	1 29	1 47	2 05	2 24	2 42	3 01	3 20	3 38	600
700	28	44	1 01	1 15	1 31	1 46	2 01	2 18	2 34	2 50	3 05	700
800	24	38	51	1 05	1 18	1 32	1 46	2 00	2 13	2 27	2 41	800
900	21	33	45	57	1 09	1 22	1 33	1 45	1 57	2 10	2 22	900
1,000	18	29	40	50	1 01	1 12	1 23	1 34	1 45	1 56	2 07	1,000
1,100	16	26	35	45	55	1 05	1 15	1 24	1 34	1 44	1 54	1,100
1,200	15	23	32	41	50	59	1 08	1 17	1 26	1 35	1 44	1,200
1,300	13	21	29	37	45	53	1 02	1 10	1 18	1 27	1 35	1,300
1,400	12	19	27	34	41	49	57	1 04	1 12	1 20	1 27	1,400
1,500	11	18	24	31	38	45	52	59	1 07	1 14	1 21	1,500
1,600	10	16	22	29	35	42	48	55	1 02	1 08	1 15	1,600
1,700		15	21	27	33	39	45	51	58	1 04	1 10	1,700
1,800		14	19	25	31	36	42	48	54	1 00	1 06	1,800
1,900		13	18	23	29	34	39	45	50	56	1 02	1,900
2,000		12	17	22	27	32	37	42	47	53	58	2,000
2,100		11	16	20	25	30	35	40	45	50	55	2,100
2,200		10	15	19	24	28	33	38	42	47	52	2,200
2,300			14	18	22	27	31	36	40	45	49	2,300
2,400			13	17	21	25	29	34	38	42	47	2,400
2,500			12	16	20	24	28	32	36	40	44	2,500
2,600			11	15	19	23	26	30	34	38	42	2,600
2,700			11	14	18	22	25	29	33	36	40	2,700
2,800			10	14	17	20	24	28	31	35	38	2,800
2,900				13	16	19	23	26	30	33	37	2,900
3,000				12	15	19	22	25	28	32	35	3,000
3,100				12	15	18	21	24	27	30	34	3,100
3,200				11	14	17	20	23	26	29	32	3,200
3,300				10	13	16	19	22	25	28	31	3,300
3,400					13	15	18	21	24	27	30	3,400
3,500					12	15	17	20	23	26	29	3,500
3,600					12	14	17	19	22	25	27	3,600
3,700					11	13	16	19	21	24	26	3,700
3,800					11	13	15	18	20	23	25	3,800
3,900					10	12	15	17	20	22	25	3,900
4,000						12	14	16	19	21	24	4,000
4,100						11	14	16	18	20	23	4,100
4,200						11	13	15	17	20	22	4,200
4,300						10	13	15	17	19	21	4,300
4,400							12	14	16	18	21	4,400
4,500							12	14	16	18	20	4,500
4,600							11	13	15	17	19	4,600
4,700							11	13	15	17	19	4,700
4,800							10	12	14	16	18	4,800
4,900								12	14	15	17	4,900
5,000								11	13	15	17	5,000

TABLE 35.

Speed in knots per hour developed by a vessel traversing a measured nautical mile in any given number of minutes and seconds.

Sec.	Number of minutes.												Sec.
	1	2	3	4	5	6	7	8	9	10	11	12	
	Knots.	*Knots.*	*Knots.*	*Knots.*	*Knots.*	*Knots.*	*Knots.*	*Knots.*	*Knots.*	*Knots.*	*Knots.*	*Knots.*	
0	60.000	30.000	20.000	15.000	12.000	10.000	8.571	7.500	6.666	6.000	5.455	5.000	0
1	59.016	29.752	19.890	14.938	11.960	9.972	8.551	7.484	6.654	5.990	5.446	4.993	1
2	58.065	29.508	19.780	14.876	11.920	9.944	8.530	7.468	6.642	5.980	5.438	4.986	2
3	57.143	29.268	19.672	14.815	11.880	9.917	8.510	7.453	6.629	5.970	5.429	4.979	3
4	56.250	29.032	19.565	14.754	11.841	9.890	8.490	7.438	6.617	5.960	5.421	4.972	4
5	55.385	28.800	19.460	14.694	11.803	9.863	8.470	7.422	6.605	5.950	5.413	4.965	5
6	54.545	28.571	19.355	14.634	11.764	9.836	8.450	7.407	6.593	5.940	5.405	4.958	6
7	53.731	28.346	19.251	14.575	11.726	9.809	8.430	7.392	6.581	5.930	5.397	4.951	7
8	52.941	28.125	19.149	14.516	11.688	9.783	8.411	7.377	6.569	5.921	5.389	4.945	8
9	52.174	27.907	19.048	14.458	11.650	9.756	8.392	7.362	6.557	5.911	5.381	4.938	9
10	51.429	27.692	18.947	14.400	11.613	9.729	8.372	7.346	6.545	5.902	5.373	4.932	10
11	50.704	27.481	18.848	14.342	11.575	9.703	8.353	7.331	6.533	5.892	5.365	4.924	11
12	50.000	27.273	18.750	14.286	11.538	9.677	8.334	7.317	6.521	5.882	5.357	4.918	12
13	49.315	27.068	18.652	14.229	11.501	9.651	8.315	7.302	6.509	5.872	5.349	4.911	13
14	48.649	26.866	18.556	14.173	11.465	9.625	8.295	7.287	6.498	5.863	5.341	4.904	14
15	48.000	26.667	18.461	14.118	11.428	9.600	8.276	7.272	6.486	5.853	5.333	4.897	15
16	47.368	26.471	18.367	14.063	11.392	9.574	8.257	7.258	6.474	5.844	5.325	4.891	16
17	46.753	26.277	18.274	14.008	11.356	9.549	8.238	7.243	6.463	5.834	5.317	4.884	17
18	46.154	26.087	18.182	13.953	11.321	9.524	8.219	7.229	6.451	5.825	5.309	4.878	18
19	45.570	25.899	18.090	13.900	11.285	9.499	8.200	7.214	6.440	5.815	5.301	4.871	19
20	45.000	25.714	18.000	13.846	11.250	9.473	8.181	7.200	6.428	5.806	5.294	4.865	20
21	44.444	25.532	17.910	13.793	11.214	9.448	8.163	7.185	6.417	5.797	5.286	4.858	21
22	43.902	25.352	17.822	13.740	11.180	9.424	8.144	7.171	6.405	5.787	5.278	4.851	22
23	43.373	25.175	17.734	13.688	11.146	9.399	8.126	7.157	6.394	5.778	5.270	4.845	23
24	42.857	25.000	17.647	13.636	11.111	9.375	8.108	7.142	6.383	5.769	5.263	4.838	24
25	42.353	24.828	17.560	13.584	11.077	9.350	8.090	7.128	6.371	5.760	5.255	4.832	25
26	41.860	24.658	17.475	13.533	11.043	9.326	8.071	7.114	6.360	5.750	5.247	4.825	26
27	41.379	24.490	17.391	13.483	11.009	9.302	8.053	7.100	6.349	5.741	5.240	4.819	27
28	40.909	24.324	17.307	13.433	10.975	9.278	8.035	7.086	6.338	5.732	5.232	4.812	28
29	40.449	24.161	17.225	13.383	10.942	9.254	8.017	7.072	6.327	5.723	5.224	4.806	29
30	40.000	24.000	17.143	13.333	10.909	9.230	8.000	7.059	6.315	5.714	5.217	4.800	30
31	39.560	23.841	17.061	13.284	10.876	9.207	7.982	7.045	6.304	5.705	5.210	4.793	31
32	39.130	23.684	16.981	13.235	10.843	9.183	7.964	7.031	6.293	5.696	5.202	4.787	32
33	38.710	23.529	16.901	13.186	10.810	9.160	7.947	7.017	6.282	5.687	5.195	4.780	33
34	38.298	23.377	16.822	13.138	10.778	9.137	7.929	7.004	6.271	5.678	5.187	4.774	34
35	37.895	23.226	16.744	13.091	10.746	9.113	7.912	6.990	6.260	5.669	5.179	4.768	35
36	37.500	28.077	16.667	13.043	10.714	9.090	7.895	6.977	6.250	5.660	5.172	4.761	36
37	37.113	22.930	16.590	12.996	10.682	9.068	7.877	6.963	6.239	5.651	5.164	4.755	37
38	36.735	22.785	16.514	12.950	10.651	9.045	7.860	6.950	6.228	5.642	5.157	4.749	38
39	36.364	22.642	16.438	12.903	10.619	9.022	7.843	6.936	6.217	5.633	5.150	4.743	39
40	36.000	22.500	16.363	12.857	10.588	9.000	7.826	6.923	6.207	5.625	5.143	4.737	40
41	35.644	22.360	16.289	12.811	10.557	8.977	7.809	6.909	6.196	5.616	5.135	4.731	41
42	35.294	22.222	16.216	12.766	10.526	8.955	7.792	6.896	6.185	5.607	5.128	4.724	42
43	34.951	22.086	16.143	12.721	10.495	8.933	7.775	6.883	6.174	5.598	5.121	4.718	43
44	34.615	21.951	16.071	12.676	10.465	8.911	7.758	6.870	6.164	5.590	5.114	4.712	44
45	34.286	21.818	16.000	12.631	10.434	8.889	7.741	6.857	6.153	5.581	5.106	4.706	45
46	33.962	21.687	15.929	12.587	10.404	8.867	7.725	6.844	6.143	5.572	5.099	4.700	46
47	33.645	21.557	15.859	12.543	10.375	8.845	7.708	6.831	6.132	5.564	5.091	4.693	47
48	33.333	21.429	15.789	12.500	10.345	8.823	7.692	6.818	6.122	5.555	5.084	4.687	48
49	33.028	21.302	15.721	12.456	10.315	8.801	7.675	6.805	6.112	5.547	5.077	4.681	49
50	32.727	21.176	15.652	12.413	10.286	8.780	7.659	6.792	6.101	5.538	5.070	4.675	50
51	32.432	21.053	15.584	12.371	10.256	8.759	7.643	6.779	6.091	5.530	5.063	4.669	51
52	32.143	20.930	15.517	12.329	10.227	8.737	7.627	6.766	6.081	5.521	5.056	4.663	52
53	31.858	20.809	15.450	12.287	10.198	8.716	7.611	6.754	6.071	5.513	5.049	4.657	53
54	31.579	20.690	15.384	12.245	10.169	8.695	7.595	6.741	6.060	5.504	5.042	4.651	54
55	31.304	20.571	15.319	12.203	10.140	8.675	7.579	6.739	6.050	5.496	5.035	4.645	55
56	31.034	20.455	15.254	12.162	10.112	8.654	7.563	6.716	6.040	5.487	5.028	4.639	56
57	30.769	20.339	15.190	12.121	10.084	8.633	7.547	6.704	6.030	5.479	5.020	4.633	57
58	30.508	20.225	15.126	12.080	10.055	8.612	7.531	6.691	6.020	5.471	5.013	4.627	58
59	30.252	20.112	15.062	12.040	10.027	8.591	7.515	6.679	6.010	5.463	5.006	4.621	59
Sec.	1	2	3	4	5	6	7	8	9	10	11	12	Sec.

TABLE 36.

Reduction of Local Mean Time to Standard Meridian Time, and the reverse.

[If local meridian is east of standard meridian, subtract from local mean time, or add to standard meridian time. If local meridian is west of standard meridian, add to local mean time, or subtract from standard meridian time.]

Difference of longitude between local meridian and standard meridian.	Reduction to be applied to local mean time.	Difference of longitude between local meridian and standard meridian.	Reduction to be applied to local mean time.
° ′ ° ′	*Minutes.*	° ′ ° ′	*Minutes.*
0 00 to 0 07	0	7 23 to 7 37	30
0 08 to 0 22	1	7 38 to 7 52	31
0 23 to 0 37	2	7 53 to 8 07	32
0 38 to 0 52	3	8 08 to 8 22	33
0 53 to 1 07	4	8 23 to 8 37	34
1 08 to 1 22	5	8 38 to 8 52	35
1 23 to 1 37	6	8 53 to 9 07	36
1 38 to 1 52	7	9 08 to 9 22	37
1 53 to 2 07	8	9 23 to 9 37	38
2 08 to 2 22	9	9 38 to 9 52	39
2 23 to 2 37	10	9 53 to 10 07	40
2 38 to 2 52	11	10 08 to 10 22	41
2 53 to 3 07	12	10 23 to 10 37	42
3 08 to 3 22	13	10 38 to 10 52	43
3 23 to 3 37	14	10 53 to 11 07	44
3 38 to 3 52	15	11 08 to 11 22	45
3 53 to 4 07	16	11 23 to 11 37	46
4 08 to 4 22	17	11 38 to 11 52	47
4 23 to 4 37	18	11 53 to 12 07	48
4 38 to 4 52	19	12 08 to 12 22	49
4 53 to 5 07	20	12 23 to 12 37	50
5 08 to 5 22	21	12 38 to 12 52	51
5 23 to 5 37	22	12 53 to 13 07	52
5 38 to 5 52	23	13 08 to 13 22	53
5 53 to 6 07	24	13 23 to 13 37	54
6 08 to 6 22	25	13 38 to 13 52	55
6 23 to 6 37	26	13 53 to 14 07	56
6 38 to 6 52	27	14 08 to 14 22	57
6 53 to 7 07	28	14 23 to 14 37	58
7 08 to 7 22	29	14 38 to 14 52	59

TABLE 37.

Log. A and Log. B.

[For Computing the Equation of Equal Altitudes. For Noon, A−; for Midnight, A+; for Noon or Midnight, B+. Argument=Elapsed Time.]

Elapsed time.	0h		1h		2h		3h		4h		5h	
	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.
m.												
0	9.4059	9.4059	9.4072	9.4034	9.4109	9.3959	9.4172	9.3828	9.4260	9.3635	9.4374	9.3369
1	.4059	.4059	.4072	.4034	.4110	.3957	.4173	.3825	.4261	.3631	.4376	.3364
2	.4059	.4059	.4073	.4033	.4111	.3955	.4174	.3822	.4263	.3627	.4378	.3358
3	.4059	.4059	.4073	.4032	.4112	.3953	.4175	.3820	.4265	.3624	.4380	.3353
4	.4059	.4059	.4074	.4031	.4113	.3952	.4177	.3817	.4266	.3620	.4383	.3348
5	9.4059	9.4059	9.4074	9.4030	9.4113	9.3950	9.4178	9.3814	9.4268	9.3616	9.4385	9.3343
6	.4060	.4059	.4074	.4029	.4114	.3948	.4179	.3811	.4270	.3612	.4387	.3337
7	.4060	.4059	.4075	.4028	.4115	.3946	.4181	.3809	.4272	.3608	.4389	.3332
8	.4060	.4059	.4075	.4027	.4116	.3944	.4182	.3806	.4273	.3604	.4391	.3327
9	.4060	.4059	.4076	.4026	.4117	.3943	.4183	.3803	.4275	.3600	.4393	.3221
10	9.4060	9.4059	9.4076	9.4025	9.4118	9.3941	9.4184	9.3800	9.4277	9.3596	9.4396	9.3316
11	.4060	.4059	.4077	.4024	.4119	.3939	.4186	.3797	.4279	.3592	.4398	.3311
12	.4060	.4058	.4077	.4023	.4120	.3937	.4187	.3794	.4280	.3588	.4400	.3305
13	.4060	.4058	.4078	.4022	.4121	.3935	.4188	.3792	.4282	.3584	.4402	.3300
14	.4060	.4058	.4078	.4021	.4121	.3933	.4190	.3789	.4284	.3580	.4405	.3294
15	9.4060	9.4058	9.4079	9.4020	9.4122	9.3931	9.4191	9.3786	9.4286	9.3576	9.4407	9.3289
16	.4060	.4058	.4079	.4019	.4123	.3929	.4193	.3783	.4288	.3572	.4409	.3283
17	.4060	.4057	.4080	.4018	.4124	.3927	.4194	.3780	.4289	.3568	.4411	.3278
18	.4061	.4057	.4080	.4017	.4125	.3925	.4195	.3777	.4291	.3564	.4414	.3272
19	.4061	.4057	.4081	.4016	.4126	.3923	.4197	.3774	.4293	.3559	.4416	.3266
20	9.4061	9.4057	9.4081	9.4015	9.4127	9.3921	9.4198	9.3771	9.4295	9.3555	9.4418	9.3261
21	.4061	.4056	.4082	.4014	.4128	.3919	.4199	.3768	.4297	.3551	.4420	.3255
22	.4061	.4056	.4083	.4013	.4129	.3917	.4201	.3765	.4299	.3547	.4423	.3249
23	.4061	.4056	.4083	.4012	.4130	.3915	.4202	.3762	.4300	.3542	.4425	.3244
24	.4061	.4055	.4084	.4010	.4131	.3913	.4204	.3759	.4302	.3538	.4427	.3238
25	9.4062	9.4055	9.4084	9.4009	9.4132	9.3911	9.4205	9.3756	9.4304	9.3534	9.4430	9.3232
26	.4062	.4055	.4085	.4008	.4133	.3909	.4207	.3752	.4306	.3530	.4432	.3226
27	.4062	.4054	.4086	.4007	.4134	.3907	.4208	.3749	.4308	.3525	.4434	.3220
28	.4062	.4054	.4086	.4006	.4135	.3905	.4209	.3746	.4310	.3521	.4437	.3214
29	.4062	.4054	.4087	.4004	.4136	.3903	.4211	.3743	.4312	.3516	.4439	.3208
30	9.4062	9.4053	9.4087	9.4003	9.4137	9.3900	9.4212	9.3740	9.4314	9.3512	9.4441	9.3203
31	.4063	.4053	.4088	.4002	.4138	.3898	.4214	.3737	.4315	.3508	.4444	.3197
32	.4063	.4052	.4089	.4001	.4139	.3896	.4215	.3733	.4317	.3503	.4446	.3191
33	.4063	.4052	.4089	.3999	.4140	.3894	.4217	.3730	.4319	.3499	.4448	.3185
34	.4063	.4051	.4090	.3998	.4141	.3892	.4218	.3727	.4321	.3494	.4451	.3178
35	9.4064	9.4051	9.4091	9.3997	9.4142	9.3889	9.4220	9.3723	9.4323	9.3490	9.4453	9.3172
36	.4064	.4050	.4091	.3995	.4144	.3887	.4221	.3720	.4325	.3485	.4456	.3166
37	.4064	.4050	.4092	.3994	.4145	.3885	.4223	.3717	.4327	.3480	.4458	.3160
38	.4064	.4049	.4093	.3993	.4146	.3882	.4224	.3713	.4329	.3476	.4460	.3154
39	.4065	.4049	.4093	.3991	.4147	.3880	.4226	.3710	.4331	.3471	.4463	.3148
40	9.4065	9.4048	9.4094	9.3990	9.4148	9.3878	9.4227	9.3707	9.4333	9.3467	9.4465	9.3142
41	.4065	.4048	.4095	.3988	.4149	.3875	.4229	.3703	.4335	.3462	.4468	.3135
42	.4065	.4047	.4095	.3987	.4150	.3873	.4231	.3700	.4337	.3457	.4470	.3129
43	.4066	.4047	.4096	.3985	.4151	.3871	.4232	.3696	.4339	.3453	.4473	.3123
44	.4066	.4046	.4097	.3984	.4152	.3868	.4234	.3693	.4341	.3448	.4475	.3116
45	9.4066	9.4045	9.4097	9.3982	9.4154	9.3866	9.4235	9.3690	9.4343	9.3443	9.4477	9.3110
46	.4067	.4045	.4098	.3981	.4155	.3863	.4237	.3686	.4345	.3438	.4480	.3103
47	.4067	.4044	.4099	.3979	.4156	.3861	.4238	.3683	.4347	.3433	.4482	.3097
48	.4067	.4043	.4100	.3978	.4157	.3859	.4240	.3679	.4349	.3429	.4485	.3091
49	.4068	.4043	.4100	.3976	.4158	.3856	.4242	.3675	.4351	.3424	.4487	.3084
50	9.4068	9.4042	9.4101	9.3975	9.4159	9.3854	9.4243	9.3672	9.4353	9.3419	9.4490	9.3078
51	.4068	.4041	.4102	.3973	.4161	.3851	.4245	.3668	.4355	.3414	.4492	.3071
52	.4069	.4041	.4103	.3972	.4162	.3849	.4246	.3665	.4357	.3409	.4494	.3064
53	.4069	.4040	.4103	.3970	.4163	.3846	.4248	.3661	.4359	.3404	.4497	.3058
54	.4069	.4039	.4104	.3969	.4164	.3843	.4250	.3657	.4361	.3399	.4500	.3051
55	9.4070	9.4038	9.4105	9.3967	9.4165	9.3841	9.4251	9.3654	9.4363	9.3394	9.4503	9.3044
56	.4070	.4038	.4106	.3965	.4167	.3838	.4253	.3650	.4366	.3389	.4505	.3038
57	.4071	.4037	.4107	.3964	.4168	.3836	.4255	.3646	.4368	.3384	.4508	.3031
58	.4071	.4036	.4107	.3962	.4169	.3833	.4256	.3643	.4370	.3379	.4510	.3024
59	.4071	.4035	.4108	.3960	.4170	.3830	.4258	.3639	.4372	.3374	.4513	.3017
60	9.4072	9.4034	9.4109	9.3959	9.4172	9.3828	9.4260	9.3635	9.4374	9.3369	9.4515	9.3010

TABLE 37.

Log. A and Log. B.

[For Computing the Equation of Equal Altitudes. For Noon, A−; for Midnight, A+; for Noon or Midnight, B+. Argument=Elapsed Time.]

Elapsed time.	6h		7h		8h		9h		10h		11h	
	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.
m.												
0	9.4515	9.3010	9.4685	9.2530	9.4884	9.1874	9.5115	9.0943	9.5379	8.9509	9.5680	8.6837
1	.4518	.3003	.4688	.2520	.4888	.1861	.5119	.0925	.5384	.9478	5685	.6770
2	.4521	.2996	.4691	.2511	.4892	.1848	.5123	.0906	.5389	.9447	5691	.6701
3	.4523	.2989	.4694	.2502	.4895	.1835	.5127	.0887	.5393	.9416	.5696	.6632
4	.4526	.2982	.4697	.2492	.4899	.1822	.5132	.0867	.5398	.9384	.5701	.6560
5	9.4528	9.2975	9.4701	9.2483	9.4902	9.1809	9.5136	9.0848	9.5403	8.9352	9.5707	8.6488
6	.4531	.2968	.4704	.2473	.4906	.1796	.5140	.0828	.5408	.9320	.5712	.6414
7	.4534	.2961	.4707	.2463	.4910	.1782	.5144	.0809	.5412	.9287	.5718	.6339
8	.4536	.2954	.4710	.2454	.4913	.1769	.5148	.0789	.5417	.9254	.5723	.6262
9	.4539	.2947	.4713	.2444	.4917	.1756	.5153	.0769	.5422	.9221	.5728	.6183
10	9.4542	9.2940	9.4716	9.2434	9.4921	9.1742	9.5157	9.0749	9.5427	8.9187	9.5734	8.6103
11	.4544	.2932	.4719	.2425	.4924	.1728	.5161	.0729	.5432	.9153	.5739	.6021
12	.4547	.2925	.4723	.2415	.4928	.1715	.5165	.0708	.5436	.9118	.5745	.5937
13	.4550	.2918	.4726	.2405	.4932	.1701	.5169	.0688	.5441	.9083	.5750	.5852
14	.4552	.2911	.4729	.2395	.4935	.1687	.5174	.0667	.5446	.9048	.5756	.5764
15	9.4555	9.2903	9.4732	9.2385	9.4939	9.1673	9.5178	9.0646	9.5451	8.9013	9.5761	8.5674
16	.4558	.2896	.4735	.2375	.4943	.1659	.5182	.0625	.5456	.8977	.5767	.5583
17	.4561	.2888	.4738	.2365	.4946	.1645	.5186	.0604	.5461	.8940	.5772	.5488
18	.4563	.2881	.4742	.2355	.4950	.1630	.5191	.0583	.5466	.8903	.5778	.5392
19	.4566	.2873	.4745	.2344	.4954	.1616	.5195	.0561	.5470	.8866	.5783	.5293
20	9.4569	9.2866	9.4748	9.2334	9.4958	9.1602	9.5199	9.0540	9.5475	8.8829	9.5789	8.5192
21	.4572	.2858	.4751	.2324	.4961	.1587	.5204	.0518	.5480	.8791	.5794	.5088
22	.4574	.2850	.4755	.2313	.4965	.1573	.5208	.0496	.5485	.8752	.5800	.4981
23	.4577	.2843	.4758	.2303	.4969	.1558	.5212	.0474	.5490	.8713	.5806	.4871
24	.4580	.2835	.4761	.2292	.4973	.1543	.5217	.0452	.5495	.8674	.5811	.4758
25	9.4583	9.2827	9.4764	9.2282	9.4977	9.1528	9.5221	9.0429	9.5500	8.8634	9.5817	8.4641
26	.4585	.2819	.4768	.2271	.4980	.1513	.5225	.0406	.5505	.8594	.5822	.4521
27	.4588	.2812	.4771	.2261	.4984	.1498	.5230	.0383	.5510	.8553	.5828	.4397
28	.4591	.2804	.4774	.2250	.4988	.1483	.5234	.0360	.5515	.8512	.5834	.4270
29	.4594	.2796	.4778	.2239	.4992	.1468	.5238	.0337	.5520	.8470	.5839	.4138
30	9.4597	9.2788	9.4781	9.2228	9.4996	9.1453	9.5243	9.0314	9.5525	8.8427	9.5845	8.4001
31	.4600	.2780	.4784	.2217	.5000	.1437	.5247	.0290	.5530	.8384	.5851	.3860
32	.4602	.2772	.4788	.2206	.5003	.1422	.5252	.0266	.5535	.8341	.5856	.3713
33	.4605	.2764	.4791	.2195	.5007	.1406	.5256	.0242	.5540	.8297	.5862	.3561
34	.4608	.2756	.4794	.2184	.5011	.1390	5261	.0218	.5545	.8253	.5868	.3403
35	9.4611	9.2747	9.4798	9.2173	9.5015	9.1375	9.5265	9.0194	9.5550	8.8208	9.5874	8.3239
36	.4614	.2739	.4801	.2162	.5019	.1359	.5269	.0169	.5555	.8162	.5879	.3067
37	.4617	.2731	.4804	.2151	.5023	.1343	.5274	.0144	.5560	.8115	.5885	.2888
38	.4620	.2723	.4808	.2140	.5027	.1327	.5278	.0119	.5565	.8068	.5891	.2701
39	.4622	.2714	.4811	.2128	.5031	.1310	.5283	.0094	.5570	.8020	.5897	.2505
40	9.4625	9.2706	9.4815	9.2117	9.5035	9.1294	9.5287	9.0069	9.5576	8.7972	9.5902	8.2299
41	.4628	.2698	.4818	.2105	.5038	.1278	.5292	.0043	.5581	.7923	.5908	.2082
42	.4631	.2689	.4821	.2094	.5042	.1261	.5296	.0017	.5586	.7873	.5914	.1853
43	.4634	.2681	.4825	.2082	.5046	.1244	.5301	8.9991	.5591	.7823	.5920	.1611
44	.4637	.2672	.4828	.2070	.5050	.1228	.5305	.9965	.5596	.7772	.5926	.1354
45	9.4640	9.2664	9.4832	9.2059	9.5054	9.1211	9.5310	8.9938	9.5601	8.7720	9.5931	8.1080
46	.4643	.2655	.4835	.2047	.5058	.1194	.5315	.9911	.5606	.7668	.5937	.0786
47	.4646	.2646	.4839	.2035	.5062	.1177	.5319	.9884	.5612	.7614	.5943	.0470
48	.4649	.2638	.4842	.2023	.5066	.1159	.5324	.9857	.5617	.7560	.5949	.0128
49	.4652	.2629	.4846	.2011	.5070	.1142	.5328	.9830	.5622	.7505	.5955	7.9756
50	9.4655	9.2620	9.4849	9.1999	9.5074	9.1125	9.5333	8.9802	9.5627	8.7449	9.5961	7.9348
51	.4658	.2611	.4853	.1987	.5078	.1107	.5337	.9774	.5632	.7392	.5967	.8897
52	.4661	.2602	.4856	.1974	.5082	.1089	.5342	.9745	.5638	.7335	.5973	.8391
53	.4664	.2593	.4860	.1962	.5086	.1072	.5347	.9717	.5643	.7276	.5979	.7817
54	.4667	.2584	.4863	.1950	.5091	.1054	.5351	.9688	.5648	.7217	.5985	.7154
55	9.4670	9.2575	9.4867	9.1937	9.5095	9.1036	9.5356	8.9659	9.5654	8.7156	9.5991	7.6368
56	.4673	.2566	.4870	.1925	.5099	.1017	.5361	.9630	.5659	.7094	.5997	.5405
57	.4676	.2557	.4874	.1912	.5103	.0999	.5365	.9600	.5664	.7032	.6003	.4162
58	.4679	.2548	.4877	.1900	.5107	.0981	.5370	.9570	.5669	.6968	.6009	.2407
59	.4682	.2539	.4881	.1887	.5111	.0962	.5375	.9540	.5675	.6903	.6015	6.9591
60	9.4685	9.2530	9.4884	9.1874	9.5115	9.0943	9.5379	8.9509	9.5680	8.6837	9.6021	*Inf.*

TABLE 37.

Log. A and Log. B.

[For Computing the Equation of Equal Altitudes. For Noon, A −; for Midnight, A +; for Noon or Midnight, B −. Argument = Elapsed Time.]

Elapsed time.	12h		13h		14h		15h		16h		17h	
	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.
m.												
0	9.6021	Inf.	9.6406	8.7563	9.6841	9.0971	9.7333	9.3162	9.7895	9.4884	9.8539	9.6383
1	.6027	6.9603	.6412	.7641	.6848	.1014	.7342	.3194	.7905	.4911	.8550	.6407
2	.6033	7.2431	.6419	.7718	.6856	.1057	.7351	.3225	.7915	.4937	.8562	.6431
3	.6039	.4198	.6426	.7794	.6864	.1099	.7360	.3256	.7925	.4963	.8573	.6455
4	.6045	.5453	.6433	.7868	.6872	.1141	.7369	.3287	.7935	.4990	.8585	.6478
5	9.6051	7.6428	9.6440	8.7942	9.6879	9.1183	9.7378	9.3319	9.7945	9.5016	9.8597	9.6502
6	.6057	.7226	.6447	.8015	.6887	.1224	.7386	.3350	.7955	.5042	.8608	.6526
7	.6063	.7902	.6454	.8087	.6895	.1265	.7395	.3380	.7965	.5068	.8620	.6550
8	.6069	.8488	.6461	.8158	.6903	.1306	.7404	.3411	.7975	.5094	.8632	.6573
9	.6075	.9005	.6467	.8227	.6911	.1347	.7413	.3442	.7986	.5120	.8644	.6597
10	9.6082	7.9469	9.6474	8.8296	9.6919	9.1387	9.7422	9.3472	9.7996	9.5146	9.8655	9.6621
11	.6088	.9889	.6481	.8364	.6926	.1428	.7431	.3503	.8006	.5171	.8667	.6644
12	.6094	8.0273	.6488	.8432	.6934	.1468	.7440	.3533	.8016	.5197	.8679	.6668
13	.6100	.0627	.6495	.8498	.6942	.1507	.7449	.3563	.8027	.5223	.8691	.6691
14	.6106	.0955	.6502	.8564	.6950	.1547	.7458	.3593	.8037	.5248	.8703	.6715
15	9.6112	8.1260	9.6509	8.8628	9.6958	9.1586	9.7467	9.3623	9.8047	9.5274	9.8715	9.6738
16	.6119	.1547	.6516	.8692	.6966	.1625	.7476	.3653	.8058	.5300	.8727	.6762
17	.6125	.1816	.6523	.8756	.6974	.1664	.7485	.3683	.8068	.5325	.8739	.6785
18	.6131	.2071	.6530	.8818	.6982	.1703	.7494	.3713	.8078	.5351	.8751	.6809
19	.6137	.2312	.6538	.8880	.6990	.1741	.7503	.3742	.8089	.5376	.8763	.6832
20	9.6144	8.2541	9.6545	8.8941	9.6998	9.1779	9.7512	9.3772	9.8099	9.5401	9.8775	9.6856
21	.6150	.2759	.6552	.9002	.7006	.1817	.7522	.3801	.8110	.5427	.8787	.6879
22	.6156	.2967	.6559	.9062	.7014	.1855	.7531	.3831	.8120	.5452	.8799	.6903
23	.6163	.3166	.6566	.9121	.7022	.1893	.7540	.3860	.8131	.5477	.8812	.6926
24	.6169	.3357	.6573	.9180	.7030	.1930	.7549	.3889	.8141	.5502	.8824	.6949
25	9.6175	8.3540	9.6580	8.9238	9.7038	9.1967	9.7558	9.3918	9.8152	9.5528	9.8836	9.6973
26	.6182	.3717	.6588	.9295	.7047	.2004	.7568	.3947	.8162	.5553	.8848	.6996
27	.6188	.3887	.6595	.9352	.7055	.2041	.7577	.3976	.8173	.5578	.8861	.7019
28	.6194	.4051	.6602	.9408	.7063	.2078	.7586	.4005	.8184	.5603	.8873	.7043
29	.6201	.4210	.6609	.9464	.7071	.2114	.7595	.4033	.8194	.5628	.8885	.7066
30	9.6207	8.4363	9.6616	8.9519	9.7079	9.2150	9.7605	9.4062	9.8205	9.5653	9.8898	9.7089
31	.6214	.4512	.6624	.9573	.7088	.2186	.7614	.4090	.8216	.5677	.8910	.7112
32	.6220	.4657	.6631	.9627	.7096	.2222	.7624	.4119	.8227	.5702	.8923	.7136
33	.6226	.4796	.6638	.9681	.7104	.2258	.7633	.4147	.8237	.5727	.8935	.7159
34	.6233	.4932	.6645	.9734	.7112	.2293	.7642	.4175	.8248	.5752	.8948	.7182
35	9.6239	8.5064	9.6653	8.9787	9.7121	9.2329	9.7652	9.4204	9.8259	9.5777	9.8961	9.7205
36	.6246	.5192	.6660	.9839	.7129	.2364	.7661	.4232	.8270	.5801	.8973	.7228
37	.6252	.5318	.6667	.9891	.7137	.2399	.7671	.4260	.8281	.5826	.8986	.7251
38	.6259	.5440	.6675	.9942	.7146	.2434	.7680	.4288	.8292	.5850	.8999	.7275
39	.6265	.5559	.6682	.9993	.7154	.2468	.7690	.4316	.8303	.5875	.9011	.7298
40	9.6272	8.5675	9.6690	9.0043	9.7162	9.2503	9.7699	9.4343	9.8314	9.5900	9.9024	9.7321
41	.6279	.5788	.6697	.0093	.7171	.2537	.7709	.4371	.8325	.5924	.9037	.7344
42	.6285	.5899	.6704	.0142	.7179	.2571	.7718	.4399	.8336	.5948	.9050	.7367
43	.6292	.6008	.6712	.0191	.7187	.2605	.7728	.4426	.8347	.5973	.9063	.7390
44	.6298	.6114	.6719	.0240	.7196	.2639	.7738	.4454	.8358	.5997	.9075	.7413
45	9.6305	8.6218	9.6727	9.0288	9.7204	9.2673	9.7747	9.4481	9.8369	9.6022	9.9088	9.7436
46	.6311	.6320	.6734	.0336	.7213	.2706	.7757	.4509	.8380	.6046	.9101	.7459
47	.6318	.6419	.6742	.0384	.7221	.2740	.7767	.4536	.8391	.6070	.9114	.7482
48	.6325	.6517	.6749	.0431	.7230	.2773	.7776	.4563	.8402	.6094	.9127	.7505
49	.6331	.6613	.6757	.0478	.7238	.2806	.7786	.4590	.8414	.6119	.9140	.7529
50	9.6338	8.6707	9.6764	9.0524	9.7247	9.2839	9.7796	9.4617	9.8425	9.6143	9.9154	9.7552
51	.6345	.6799	.6772	.0570	.7256	.2872	.7806	.4644	.8436	.6167	.9167	.7575
52	.6351	.6890	.6779	.0616	.7264	.2905	.7815	.4671	.8447	.6191	.9180	.7598
53	.6358	.6979	.6787	.0662	.7273	.2937	.7825	.4698	.8459	.6215	.9193	.7621
54	.6365	.7067	.6795	.0707	.7281	.2970	.7835	.4725	.8470	.6239	.9206	.7644
55	9.6372	8.7153	9.6802	9.0752	9.7290	9.3002	9.7845	9.4752	9.8481	9.6263	9.9220	9.7667
56	.6378	.7237	.6810	.0796	.7299	.3034	.7855	.4778	.8493	.6287	.9233	.7690
57	.6385	.7321	.6818	.0840	.7307	.3066	.7865	.4805	.8504	.6311	.9246	.7713
58	.6392	.7402	.6825	.0884	.7316	.3098	.7875	.4831	.8516	.6335	.9260	.7736
59	.6399	.7483	.6833	.0928	.7324	.3130	.7885	.4858	.8527	.6359	.9273	.7759
60	9.6406	8.7563	9.6841	9.0971	9.7333	9.3162	9.7895	9.4884	9.8539	9.6383	9.9287	9.7782

TABLE 37.

Log. A and Log. B.

[For Computing the Equation of Equal Altitudes. For Noon, A −; for Midnight, A +; for Noon or Midnight, B −. Argument = Elapsed Time.]

Elapsed time.	18h		19h		20h		21h		22h		23h	
	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.	Log. A.	Log. B.
m. 0	9.9287	9.7782	0.0172	9.9167	0.1249	0.0625	0.2623	0.2279	0.4523	0.4372	0.7689	0.7652
1	.9300	.7804	.0188	.9190	.1269	.0650	.2649	.2309	.4562	.4414	.7765	.7729
2	.9314	.7827	.0204	.9213	.1290	.0676	.2676	.2339	.4601	.4455	.7842	.7807
3	.9327	.7850	.0221	.9237	.1310	.0701	.2702	.2370	.4640	.4497	.7920	.7886
4	.9341	.7873	.0237	.9260	.1330	.0727	.2729	.2401	.4680	.4540	.8000	.7967
5	9.9355	9.7896	0.0253	9.9284	0.1351	0.0753	0.2756	0.2431	0.4720	0.4582	0.8081	0.8049
6	.9368	.7919	.0270	.9307	.1371	.0779	.2783	.2462	.4761	.4625	.8163	.8133
7	.9382	.7942	.0286	.9331	.1392	.0805	.2810	.2493	.4801	.4668	.8247	.8218
8	.9396	.7965	.0303	.9355	.1412	.0830	.2838	.2524	.4842	.4711	.8333	.8305
9	.9410	.7988	.0319	.9378	.1433	.0856	.2865	.2556	.4884	.4755	.8420	.8393
10	9.9424	9.8011	0.0336	9.9402	0.1454	0.0882	0.2893	0.2587	0.4926	0.4799	0.8508	0.8483
11	.9437	.8034	.0353	.9426	.1475	.0909	.2921	.2619	.4968	.4844	.8599	.8574
12	.9451	.8057	.0370	.9449	.1496	.0935	.2949	.2650	.5010	.4889	.8691	.8667
13	.9465	.8080	.0386	.9473	.1517	.0961	.2977	.2682	.5053	.4934	.8786	.8763
14	.9479	.8103	.0403	.9497	.1538	.0987	.3005	.2714	.5097	.4980	.8882	.8860
15	9.9493	9.8126	0.0420	9.9520	0.1559	0.1013	0.3034	0.2746	0.5140	0.5026	0.8980	0.8959
16	.9508	.8149	.0437	.9544	.1581	.1040	.3063	.2778	.5184	.5072	.9080	.9060
17	.9522	.8172	.0454	.9568	.1602	.1066	.3091	.2811	.5229	.5118	.9183	.9164
18	.9536	.8195	.0472	.9592	.1623	.1093	.3120	.2843	.5274	.5165	.9288	.9270
19	.9550	.8218	.0489	.9616	.1645	.1119	.3150	.2876	.5319	.5213	.9396	.9378
20	9.9564	9.8241	0.0506	9.9640	0.1667	0.1146	0.3179	0.2909	0.5365	0.5261	0.9506	0.9489
21	.9579	.8264	.0523	.9664	.1689	.1173	.3208	.2942	.5411	.5309	.9618	.9603
22	.9593	.8287	.0541	.9687	.1711	.1200	.3238	.2975	.5458	.5358	.9734	.9719
23	.9607	.8310	.0558	.9711	.1733	.1226	.3268	.3008	.5505	.5407	.9853	.9839
24	.9622	.8333	.0576	.9735	.1755	.1253	.3298	.3041	.5553	.5457	.9975	.9961
25	9.9636	9.8356	0.0593	9.9760	0.1777	0.1280	0.3328	0.3075	0.5601	0.5507	1.0100	1.0087
26	.9651	.8379	.0611	.9784	.1799	.1308	.3359	.3109	.5649	.5557	.0228	.0216
27	.9665	.8402	.0628	.9808	.1821	.1335	.3389	.3143	.5698	.5608	.0361	.0350
28	.9680	.8425	.0646	.9832	.1844	.1362	.3420	.3177	.5748	.5660	.0497	.0487
29	.9695	.8448	.0664	.9856	.1867	.1389	.3451	.3211	.5798	.5712	.0638	.0628
30	9.9709	9.8471	0.0682	9.9880	0.1889	0.1417	0.3482	0.3245	0.5848	0.5764	1.0783	1.0774
31	.9724	.8494	.0700	.9904	.1912	.1444	.3514	.3280	.5899	.5817	.0934	.0925
32	.9739	.8517	.0718	.9929	.1935	.1472	.3545	.3315	.5951	.5871	.1089	.1081
33	.9754	.8540	.0736	.9953	.1958	.1499	.3577	.3350	.6003	.5925	.1250	.1242
34	.9769	.8563	.0754	.9977	.1981	.1527	.3609	.3385	.6056	.5979	.1416	.1409
35	9.9784	9.8586	0.0772	0.0002	0.2004	0.1555	0.3641	0.3420	0.6110	0.6034	1.1590	1.1583
36	.9798	.8609	.0790	.0026	.2028	.1582	.3674	.3456	.6164	.6090	.1770	.1764
37	.9813	.8632	.0809	.0051	.2051	.1610	.3706	.3491	.6218	.6147	.1958	.1952
38	.9829	.8655	.0827	.0075	.2075	.1638	.3739	.3527	.6273	.6204	.2154	.2149
39	.9844	.8678	.0845	.0100	.2098	.1667	.3772	.3563	.6329	.6261	.2359	.2354
40	9.9859	9.8701	0.0864	0.0124	0.2122	0.1695	0.3805	0.3599	0.6386	0.6319	1.2573	1.2569
41	.9874	.8724	.0883	.0149	.2146	.1723	.3839	.3636	.6443	.6378	.2799	.2795
42	.9889	.8748	.0901	.0173	.2170	.1751	.3873	.3673	.6501	.6438	.3037	.3033
43	.9904	.8771	.0920	.0198	.2194	.1780	.3907	.3710	.6560	.6498	.3288	.3285
44	.9920	.8794	.0939	.0223	.2218	.1808	.3941	.3747	.6619	.6559	.3554	.3552
45	9.9935	9.8817	0.0958	0.0248	0.2243	0.1837	0.3975	0.3784	0.6679	0.6621	1.3837	1.3835
46	.9951	.8840	.0976	.0272	.2267	.1866	.4010	.3822	.6740	.6684	.4140	.4138
47	.9966	.8863	.0995	.0297	.2292	.1895	.4045	.3859	.6802	.6747	.4465	.4463
48	.9982	.8887	.1015	.0322	.2316	.1924	.4080	.3897	.6865	.6811	.4815	.4814
49	.9998	.8910	.1034	.0347	.2341	.1953	.4115	.3936	.6928	.6876	.5196	.5195
50	0.0013	9.8933	0.1053	0.0372	0.2366	0.1982	0.4151	0.3974	0.6993	0.6942	1.5613	1.5612
51	.0029	.8956	.1072	.0397	.2391	.2011	.4187	.4013	.7058	.7008	.6074	.6073
52	.0044	.8980	.1092	.0422	.2416	.2040	.4223	.4052	.7124	.7076	.6588	.6587
53	.0060	.9003	.1111	.0447	.2442	.2070	.4260	.4091	.7191	.7144	.7171	.7171
54	.0076	.9026	.1131	.0473	.2467	.2099	.4297	.4130	.7259	.7214	.7844	.7843
55	0.0092	9.9050	0.1150	0.0498	0.2493	0.2129	0.4334	0.4170	0.7328	0.7284	1.8638	1.8638
56	.0108	.9073	.1170	.0523	.2518	.2159	.4371	.4210	.7398	.7355	.9610	.9610
57	.0124	.9096	.1190	.0548	.2544	.2189	.4408	.4250	.7469	.7428	2.0863	2.0863
58	.0140	.9120	.1209	.0574	.2570	.2219	.4446	.4291	.7541	.7501	.2627	.2627
59	.0156	.9143	.1229	.0599	.2596	.2249	.4485	.4331	.7615	.7576	2.5640	2.5640
60	0.0172	9.9167	0.1249	0.0625	0.2623	0.2279	0.4523	0.4372	0.7689	0.7652	*Inf.*	*Inf.*

TABLE 38.

Error in Longitude due to one minute Error of Latitude.

Sun's altitude.	Polar distance.	Latitude. 0°	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	75°	Polar distance.	Sun's altitude.
°	°	′	′	′	′	′	′	′	′	′	′	′	′	′	′	′	′	°	°
10	110	.4	.4	.4	.5	.5	.6	.7	.8	1.0	1.3	1.8	2.9					110	10
20		.4	.4	.5	.6	.7	.8	1.0	1.2	1.6	2.6								20
30		.4	.5	.6	.7	.9	1.1	1.5	2.3										30
40		.5	.6	.8	1.0	1.3													40
50		.7	.9	1.2															50
60		.9																	60
10	105	.3	.3	.3	.3	.4	.4	.5	.6	.8	.9	1.2	1.8	3.0				105	10
20		.3	.3	.4	.4	.5	.6	.7	.9	1.2	1.6	2.7							20
30		.3	.4	.5	.6	.7	.8	1.1	1.5	2.4									30
40		.4	.5	.6	.7	1.0	1.3												40
50		.4	.6	.8	1.2														50
60		.6	.9																60
15	100	.2	.2	.2	.3	.3	.4	.4	.5	.6	.8	1.1	1.6	2.9				100	15
20		.2	.2	.3	.3	.4	.5	.5	.7	.9	1.1	1.6	2.7						20
30		.2	.3	.3	.4	.5	.6	.8	1.1	1.5	2.4								30
40		.2	.3	.4	.6	.7	.9	1.3	2.1										40
50		.3	.4	.6	.8	1.2													50
60		.3	.6	.9															60
15	95	.1	.1	.1	.2	.2	.3	.3	.4	.5	.6	.8	1.1	1.7	3.0			95	15
20		.1	.1	.2	.2	.3	.3	.4	.5	.6	.8	1.1	1.6	2.8					20
30		.1	.2	.2	.3	.4	.5	.6	.8	1.0	1.5	2.5							30
40		.1	.2	.3	.4	.5	.7	.9	1.3	2.1									40
50		.1	.3	.4	.6	.8	1.1												50
60		.2	.3	.6	.9														60
20	90	.0	.0	.1	.1	.1	.2	.2	.3	.4	.6	.7	1.1	1.6	3.0			90	20
30		.0	.1	.1	.2	.2	.3	.4	.5	.7	1.0	1.5	2.7						30
40		.0	.1	.2	.3	.3	.5	.6	.9	1.3	2.2								40
50		.0	.1	.2	.4	.5	.8	1.1											50
60		.0	.2	.3	.5	.9													60
70		.0	.2	.6	1.1														70
20	85	.1*	.1*	.0	.0	.0	.1	.1	.2	.3	.3	.5	.7	1.0	1.6	3.1		85	20
30		.1*	.0	.0	.1	.1	.2	.2	.4	.5	.7	1.0	1.5	2.7					30
40		.1*	.0	.0	.1	.2	.3	.4	.6	.9	1.3	2.3							40
50		.1*	.0	.1	.2	.3	.5	.7	1.1										50
60		.2*	.0	.1	.3	.5	.9												60
70		.3*	.0	.2	.6	1.1													70
20	80	.2*	.2*	.1*	.1*	.1*	.0	.0	.0	.1	.1	.2	.4	.5	.9	1.5	3.1	80	20
30		.2*	.2*	.1*	.0	.0	.1	.1	.2	.3	.4	.6	.9	1.5	2.8				30
40		.2*	.2*	.1*	.0	.1	.2	.3	.4	.6	.9	1.3	2.4						40
50		.3*	.2*	.1*	.1	.2	.3	.5	.7	1.1									50
60		.4*	.2*	.0	.1	.3	.5	.9											60
70		.6*	.3*	.0	.2	.6	1.2												70
20	75	.3*	.3*	.2*	.2*	.2*	.1*	.1*	.1*	.1*	.0	.0	.1	.2	.3	.6	1.2	75	20
30		.3*	.3*	.2*	.2*	.1*	.1*	.0	.1	.1	.2	.4	.6	.9	1.5	3.0			30
40		.4*	.3*	.2*	.1*	.1*	.0	.1	.2	.4	.5	.8	1.3	2.5					40
50		.4*	.3*	.2*	.1*	.0	.1	.3	.5	.7	1.1								50
60		.6*	.4*	.2*	.1*	.1	.3	.5	.9										60
70		1.2*	.6*	.3*	.0	.2	.6	1.2											70
20	70	.4*	.4*	.3*	.3*	.3*	.3*	.2*	.2*	.2*	.2*	.2*	.2*	.2*	.2*	.2*	.2*	70	20
30		.4*	.4*	.3*	.3*	.2*	.2*	.1*	.1*	.0	.0	.1	.2	.6	.8	1.5	3.1		30
40		.5*	.4*	.3*	.3*	.2*	.1*	.0	.1	.2	.3	.5	.8	1.3	2.6				40
50		.6*	.5*	.3*	.2*	.2*	.0	.1	.3	.4	.7	1.1							50
60		.9*	.6*	.4*	.3*	.1*	.1	.2	.5	.9									60
70			1.2*	.6*	.3*	.1*	.2	.6	1.2										70
Sun's altitude.	Polar distance.	0°	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	75°	Polar distance.	Sun's altitude.
		Latitude.																	

TABLE 39.

Amplitudes.

Latitude.	Declination. 0°.0	0°.5	1°.0	1°.5	2°.0	2°.5	3°.0	3°.5	4°.0	4°.5	5°.0	5°.5	6°.0	Latitude.
°	°	°	°	°	°	°	°	°	°	°	°	°	°	°
0	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	5.5	6.0	0
10	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.1	4.6	5.1	5.6	6.1	10
15	0.0	0.5	1.0	1.5	2.1	2.6	3.1	3.6	4.2	4.7	5.2	5.7	6.2	15
20	0.0	0.5	1.1	1.6	2.1	2.7	3.2	3.7	4.3	4.8	5.3	5.8	6.4	20
25	0.0	0.5	1.1	1.6	2.2	2.8	3.3	3.8	4.4	5.0	5.5	6.0	6.6	25
30	0.0	0.6	1.2	1.7	2.3	2.9	3.4	4.0	4.6	5.2	5.8	6.3	6.9	30
32	0.0	0.6	1.2	1.8	2.4	2.9	3.5	4.1	4.7	5.3	5.9	6.5	7.0	32
34	0.0	0.6	1.2	1.8	2.4	3.0	3.6	4.2	4.8	5.4	6.0	6.6	7.2	34
36	0.0	0.6	1.2	1.8	2.5	3.1	3.7	4.3	4.9	5.6	6.1	6.8	7.4	36
38	0.0	0.6	1.3	1.9	2.5	3.2	3.8	4.4	5.1	5.7	6.3	7.0	7.6	38
40	0.0	0.7	1.3	2.0	2.6	3.3	3.9	4.6	5.2	5.9	6.5	7.2	7.8	40
42	0.0	0.7	1.3	2.0	2.7	3.4	4.0	4.7	5.4	6.1	6.7	7.4	8.0	42
44	0.0	0.7	1.4	2.1	2.8	3.5	4.2	4.9	5.6	6.3	6.9	7.6	8.3	44
46	0.0	0.7	1.4	2.2	2.9	3.6	4.3	5.0	5.8	6.5	7.2	7.9	8.6	46
48	0.0	0.7	1.5	2.2	3.0	3.7	4.5	5.2	6.0	6.7	7.5	8.2	9.0	48
50	0.0	0.8	1.5	2.3	3.1	3.9	4.7	5.4	6.2	7.0	7.8	8.6	9.3	50
51	0.0	0.8	1.6	2.4	3.2	4.0	4.8	5.6	6.4	7.2	8.0	8.8	9.5	51
52	0.0	0.8	1.6	2.4	3.3	4.1	4.9	5.7	6.5	7.3	8.1	9.0	9.7	52
53	0.0	0.8	1.6	2.5	3.3	4.2	5.0	5.8	6.7	7.5	8.3	9.2	10.0	53
54	0.0	0.9	1.7	2.5	3.4	4.3	5.1	6.0	6.8	7.7	8.5	9.4	0.2	54
55	0.0	0.9	1.7	2.6	3.5	4.4	5.2	6.1	7.0	7.9	8.7	9.6	10.5	55
56	0.0	0.9	1.8	2.7	3.6	4.5	5.4	6.3	7.2	8.1	9.0	9.9	0.8	56
57	0.0	0.9	1.8	2.7	3.7	4.6	5.5	6.4	7.4	8.3	9.2	10.1	1.1	57
58	0.0	0.9	1.9	2.8	3.8	4.7	5.7	6.6	7.6	8.5	9.5	0.4	1.4	58
59	0.0	1.0	1.9	2.9	3.9	4.9	5.8	6.8	7.8	8.8	9.7	0.7	1.7	59
60	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0	11.0	12.1	60
61	0.0	1.0	2.1	3.1	4.1	5.2	6.2	7.2	8.3	9.3	0.3	1.4	2.5	61
62	0.0	1.1	2.1	3.2	4.3	5.3	6.4	7.5	8.5	9.6	0.7	1.8	2.9	62
63	0.0	1.1	2.2	3.3	4.5	5.5	6.6	7.7	8.8	9.9	1.1	2.2	3.4	63
64	0.0	1.1	2.3	3.4	4.6	5.7	6.9	8.0	9.2	10.3	1.5	2.6	3.9	64
65.0	0.0	1.2	2.4	3.5	4.8	5.9	7.1	8.3	9.5	10.7	11.9	13.1	14.4	65.0
5.5	0.0	1.2	2.4	3.6	4.8	6.0	7.2	8.5	9.7	0.9	2.1	3.4	4.6	5.5
6.0	0.0	1.2	2.5	3.7	4.9	6.1	7.4	8.6	9.9	1.1	2.4	3.6	4.9	6.0
6.5	0.0	1.2	2.5	3.8	5.0	6.3	7.5	8.8	10.1	1.3	2.6	3.9	5.2	6.5
7.0	0.0	1.3	2.6	3.8	5.1	6.4	7.7	9.0	0.3	1.6	2.9	4.2	5.5	7.0
67.5	0.0	1.3	2.6	3.9	5.2	6.5	7.9	9.2	10.5	11.8	13.2	14.5	15.9	67.5
8.0	0.0	1.3	2.7	4.0	5.3	6.7	8.0	9.4	0.7	2.1	3.5	4.8	6.2	8.0
8.5	0.0	1.4	2.7	4.1	5.4	6.8	8.2	9.6	1.0	2.4	3.8	5.2	6.6	8.5
9.0	0.0	1.4	2.8	4.2	5.5	7.0	8.4	9.8	1.2	2.6	4.1	5.5	7.0	9.0
9.5	0.0	1.4	2.9	4.3	5.7	7.2	8.6	10.0	1.5	2.9	4.4	5.9	7.4	9.5
70.0	0.0	1.5	2.9	4.4	5.8	7.3	8.8	10.3	11.8	13.3	14.8	16.3	17.8	70.0
0.5	0.0	1.5	3.0	4.5	6.0	7.5	9.0	0.5	2.1	3.6	5.1	6.7	8.2	0.5
1.0	0.0	1.5	3.1	4.6	6.2	7.7	9.3	0.8	2.4	3.9	5.5	7.1	8.7	1.0
1.5	0.0	1.6	3.2	4.7	6.3	7.9	9.5	1.1	2.7	4.3	5.9	7.8	9.2	1.5
2.0	0.0	1.6	3.2	4.9	6.5	8.1	9.8	1.4	3.0	4.7	6.4	8.1	9.8	2.0
72.5	0.0	1.7	3.3	5.0	6.7	8.3	10.0	11.7	13.4	15.1	16.9	18.6	20.3	72.5
3.0	0.0	1.7	3.4	5.1	6.9	8.6	0.3	2.0	3.8	5.5	7.4	9.1	0.9	3.0
3.5	0.0	1.8	3.5	5.2	7.1	8.8	0.6	2.4	4.2	6.0	7.9	9.7	1.6	3.5
4.0	0.0	1.8	3.6	5.4	7.3	9.1	0.9	2.8	4.6	6.5	8.4	20.3	2.3	4.0
4.5	0.0	1.9	3.7	5.6	7.5	9.4	1.3	3.2	5.1	7.1	9.0	1.0	3.0	4.5
75.0	0.0	1.9	3.8	5.8	7.7	9.7	11.7	13.6	15.6	17.7	19.7	21.7	23.8	75.0
5.5	0.0	2.0	3.9	6.0	8.0	10.0	2.1	4.1	6.2	8.3	20.4	2.5	4.7	5.5
6.0	0.0	2.1	4.0	6.2	8.3	0.4	2.5	4.6	6.8	8.9	1.1	3.3	5.6	6.0
6.5	0.0	2.1	4.2	6.4	8.6	0.8	3.0	5.2	7.4	9.6	1.9	4.2	6.6	6.5
7.0	0.0	2.2	4.4	6.6	8.9	1.2	3.5	5.8	8.1	20.4	2.8	5.2	7.7	7.0

TABLE 39.

Amplitudes.

Latitude.	Declination. 6°.0	6°.5	7°.0	7°.5	8°.0	8°.5	9°.0	9°.5	10°.0	10°.5	11°.0	11°.5	12°.0	Latitude.
°	°	°	°	°	°	°	°	°	°	°	°	°	°	°
0	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5	10.0	10.5	11.0	11.5	12.0	0
10	6.1	6.6	7.1	7.6	8.1	8.6	9.1	9.7	0.1	0.7	1.2	1.7	2.2	10
15	6.2	6.7	7.2	7.8	8.3	8.8	9.3	9.8	0.4	0.9	1.4	1.9	2.5	15
20	6.4	6.9	7.4	8.0	8.5	9.1	9.6	10.1	0.7	1.2	1.7	2.3	2.8	20
25	6.6	7.1	7.7	8.3	8.8	9.4	9.9	0.5	1.1	1.6	2.2	2.8	3.3	25
30	6.9	7.5	8.1	8.7	9.3	9.8	10.4	11.0	11.5	12.1	12.7	13.3	13.9	30
32	7.0	7.7	8.3	8.8	9.5	10.0	0.6	1.2	1.8	2.4	3.0	3.6	4.2	32
34	7.2	7.8	8.5	9.0	9.7	0.3	0.8	1.5	2.1	2.7	3.3	3.9	4.5	34
36	7.4	8.0	8.7	9.3	9.9	0.5	1.1	1.8	2.4	3.0	3.6	4.3	4.9	36
38	7.6	8.2	8.9	9.5	10.2	0.8	1.4	2.1	2.7	3.4	4.0	4.7	5.3	38
40	7.8	8.5	9.1	9.8	10.5	11.1	11.7	12.4	13.1	13.8	14.4	15.1	15.7	40
42	8.0	8.8	9.4	10.1	0.8	1.5	2.1	2.8	3.5	4.2	4.8	5.6	6.2	42
44	8.3	9.1	9.7	0.5	1.1	1.9	2.5	3.3	4.0	4.7	5.3	6.1	6.8	44
46	8.6	9.4	10.1	0.8	1.5	2.3	3.0	3.8	4.5	5.2	5.9	6.7	7.4	46
48	9.0	9.7	0.5	1.2	2.0	2.8	3.5	4.3	5.0	5.8	6.6	7.3	8.1	48
50	9.3	10.1	10.9	11.7	12.5	13.3	14.1	14.9	15.7	16.5	17.3	18.1	18.9	50
51	9.5	0.4	1.2	2.0	2.8	3.6	4.4	5.2	6.0	6.8	7.7	8.5	9.3	51
52	9.7	0.6	1.4	2.2	3.1	3.9	4.7	5.6	6.4	7.2	8.1	8.9	9.7	52
53	10.0	0.8	1.7	2.5	3.4	4.2	5.1	5.9	6.8	7.6	8.5	9.4	20.2	53
54	0.2	1.1	2.0	2.8	3.7	4.6	5.4	6.3	7.2	8.1	8.9	9.8	0.7	54
55	10.5	11.4	12.3	13.1	14.0	14.9	15.8	16.7	17.6	18.5	19.4	20.3	21.2	55
56	0.8	1.7	2.6	3.5	4.4	5.3	6.2	7.2	8.1	9.0	9.9	0.9	1.8	56
57	1.1	2.0	2.9	3.9	4.8	5.8	6.7	7.7	8.6	9.6	20.5	1.5	2.4	57
58	1.4	2.3	3.3	4.3	5.2	6.2	7.2	8.2	9.1	20.1	1.1	2.1	3.1	58
59	1.7	2.7	3.7	4.7	5.7	6.7	7.7	8.7	9.7	0.7	1.7	2.8	3.8	59
60	12.1	13.1	14.1	15.1	16.2	17.2	18.2	19.3	20.3	21.4	22.4	23.5	24.6	60
61	2.5	3.5	4.6	5.6	6.7	7.8	8.8	9.9	1.0	2.1	3.1	4.3	5.4	61
62	2.9	3.9	5.1	6.1	7.3	8.4	9.4	20.6	1.7	2.9	3.9	5.2	6.3	62
63	3.4	4.4	5.6	6.7	7.9	9.0	20.1	1.3	2.5	3.7	4.8	6.1	7.2	63
64	3.9	5.0	6.2	7.3	8.5	9.7	0.9	2.1	3.3	4.6	5.7	7.1	8.3	64
65.0	14.4	15.5	16.8	18.0	19.3	20.5	21.7	23.0	24.2	25.6	26.8	28.2	29.5	65.0
5.5	4.6	5.8	7.1	8.3	9.6	0.9	2.2	3.5	4.7	6.1	7.4	8.7	30.1	5.5
6.0	4.9	6.2	7.4	8.7	20.0	1.3	2.6	3.9	5.3	6.6	8.0	9.3	0.7	6.0
6.5	5.2	6.5	7.8	9.1	0.4	1.8	3.1	4.4	5.8	7.2	8.6	30.0	1.4	6.5
7.0	5.5	6.8	8.2	9.5	0.9	2.2	3.6	5.0	6.4	7.8	9.2	0.7	2.1	7.0
67.5	15.9	17.2	18.6	19.9	21.3	22.7	24.1	25.5	27.0	28.4	29.9	31.4	32.9	67.5
8.0	6.2	7.6	9.0	20.4	1.8	3.2	4.7	6.1	7.6	9.1	30.6	2.2	3.7	8.0
8.5	6.6	8.0	9.4	0.9	2.3	3.8	5.3	6.8	8.3	9.8	1.4	3.0	4.6	8.5
9.0	7.0	8.4	9.9	1.4	2.8	4.4	5.9	7.4	9.0	30.6	2.2	3.8	5.5	9.0
9.5	7.4	8.9	20.4	1.9	3.4	5.0	6.5	8.1	9.7	1.4	3.0	4.7	6.4	9.5
70.0	17.8	19.3	20.9	22.4	24.0	25.6	27.2	28.8	30.5	32.2	33.9	35.7	37.4	70.0
0.5	8.2	9.8	1.4	3.0	4.6	6.3	7.9	9.6	1.3	3.1	4.9	6.7	8.5	0.5
1.0	8.7	20.3	2.0	3.6	5.3	7.0	8.7	30.5	2.2	4.0	5.9	7.8	9.7	1.0
1.5	9.2	0.9	2.6	4.3	6.0	7.8	9.5	1.4	3.2	5.0	7.0	8.9	40.9	1.5
2.0	9.8	1.5	3.2	5.0	6.8	8.6	30.4	2.3	4.2	6.1	8.1	40.2	2.3	2.0
72.5	20.3	22.1	23.9	25.7	27.6	29.5	31.4	33.3	35.3	37.3	39.4	41.5	43.7	72.5
3.0	0.9	2.8	4.6	6.5	8.4	30.4	2.4	4.4	6.5	8.6	40.8	3.0	5.3	3.0
3.5	1.6	3.5	5.4	7.4	9.3	1.4	3.4	5.5	7.7	9.9	2.2	4.6	7.0	3.5
4.0	2.3	4.3	6.2	8.3	30.3	2.5	4.6	6.8	9.1	41.4	3.8	6.3	8.9	4.0
4.5	3.0	5.1	7.1	9.3	1.4	3.6	5.8	8.2	40.5	3.0	5.6	8.2	51.1	4.5
75.0	23.8	26.0	28.1	30.3	32.5	34.8	37.2	39.6	42.1	44.8	47.5	50.4	53.5	75.0
5.5	4.7	6.9	9.1	1.4	3.8	6.2	8.7	41.2	3.9	6.7	9.6	2.8	6.2	5.5
6.0	5.6	7.9	30.2	2.6	5.1	7.7	40.3	3.0	5.9	8.9	52.1	5.5	9.3	6.0
6.5	6.6	9.0	1.4	4.0	6.6	9.3	2.1	5.0	8.1	51.3	4.8	8.7	63.0	6.5
7.0	7.7	30.2	2.8	5.5	8.2	41.1	4.1	7.2	50.5	4.1	8.0	62.4	7.6	7.0

TABLE 39.

Amplitudes.

Latitude.	Declination. 12°.0	12°.5	13°.0	13°.5	14°.0	14°.5	15°.0	15°.5	16°.0	16°.5	17°.0	17°.5	18°.0	Latitude.
°	°	°	°	°	°	°	°	°	°	°	°	°	°	°
0	12.0	12.5	13.0	13.5	14.0	14.5	15.0	15.5	16.0	16.5	17.0	17.5	18.0	0
10	2.2	2.7	3.2	3.7	4.2	4.7	5.3	5.8	6.3	6.8	7.3	7.9	8.3	10
15	2.5	2.9	3.5	4.0	4.5	5.0	5.6	6.1	6.6	7.1	7.7	8.2	8.7	15
20	2.8	3.3	3.8	4.4	4.9	5.5	6.0	6.5	7.1	7.6	8.1	8.7	9.2	20
25	3.3	3.8	4.4	4.9	5.5	6.1	6.6	7.1	7.7	8.3	8.8	9.4	9.9	25
30	13.9	14.5	15.0	15.6	16.2	16.8	17.4	18.0	18.6	19.2	19.7	20.3	20.9	30
32	4.2	4.8	5.3	6.0	6.6	7.2	7.8	8.4	9.0	9.6	20.2	0.8	1.4	32
34	4.5	5.1	5.7	6.4	7.0	7.6	8.2	8.8	9.5	20.0	0.7	1.3	1.9	34
36	4.9	5.5	6.1	6.8	7.4	8.0	8.7	9.3	20.0	0.5	1.2	1.8	2.5	36
38	5.3	6.0	6.6	7.2	7.9	8.5	9.2	9.8	0.5	1.1	1.8	2.4	3.1	38
40	15.7	16.4	17.1	17.8	18.4	19.1	19.7	20.4	21.1	21.8	22.4	23.1	23.8	40
41	6.0	6.7	7.3	8.0	8.7	9.4	20.0	0.8	1.4	2.1	2.8	3.5	4.2	41
42	6.2	6.9	7.6	8.3	9.0	9.7	0.4	1.1	1.8	2.5	3.2	3.9	4.6	42
43	6.5	7.2	7.9	8.6	9.3	20.0	0.7	1.4	2.2	2.9	3.6	4.3	5.0	43
44	6.8	7.5	8.2	8.9	9.6	0.4	1.1	1.8	2.6	3.3	4.0	4.7	5.4	44
45	17.1	17.8	18.5	19.3	20.0	20.7	21.5	22.2	23.0	23.7	24.4	25.2	25.9	45
46	7.4	8.2	8.9	9.6	0.4	1.1	1.9	2.6	3.4	4.1	4.9	5.7	6.4	46
47	7.7	8.5	9.3	20.0	0.8	1.5	2.3	3.1	3.8	4.6	5.4	6.2	6.9	47
48	8.1	8.9	9.7	0.4	1.2	2.0	2.8	3.6	4.3	5.1	5.9	6.7	7.5	48
49	8.5	9.3	20.1	0.8	1.6	2.4	3.2	4.1	4.9	5.7	6.5	7.3	8.1	49
50	18.9	19.7	20.5	21.3	22.1	22.9	23.7	24.6	25.4	26.2	27.0	27.9	28.7	50
51	9.3	20.1	0.9	1.8	2.6	3.5	4.3	5.1	6.0	6.8	7.6	8.5	9.4	51
52	9.7	0.6	1.4	2.3	3.1	4.0	4.9	5.7	6.6	7.5	8.3	9.2	30.1	52
53	20.2	1.1	1.9	2.8	3.7	4.6	5.5	6.4	7.3	8.2	9.0	30.0	0.9	53
54	0.7	1.6	2.5	3.4	4.3	5.2	6.1	7.1	8.0	8.9	9.8	0.8	1.7	54
55	21.2	22.2	23.1	24.0	24.9	25.9	26.8	27.8	28.7	29.7	30.6	31.6	32.6	55
56	1.8	2.8	3.7	4.7	5.6	6.6	7.6	8.6	9.5	30.5	1.5	2.5	3.6	56
57	2.4	3.4	4.4	5.4	6.4	7.4	8.4	9.4	30.4	1.4	2.5	3.5	4.6	57
58	3.1	4.1	5.1	6.1	7.2	8.2	9.2	30.3	1.3	2.4	3.5	4.6	5.7	58
59	3.8	4.8	5.9	6.9	8.0	9.1	30.2	1.3	2.3	3.5	4.6	5.7	6.9	59
60	24.6	25.6	26.7	27.8	28.9	30.1	31.2	32.3	33.4	34.6	35.8	36.9	38.2	60
61	5.4	6.5	7.6	8.8	9.9	1.1	2.2	3.5	4.6	5.8	7.1	8.3	9.6	61
62	6.3	7.5	8.6	9.8	31.0	2.2	3.4	4.7	5.9	7.2	8.5	9.8	41.2	62
63	7.2	8.5	9.7	31.0	2.2	3.5	4.7	6.1	7.4	8.7	40.1	41.5	2.9	63
64	8.3	9.6	30.9	2.2	3.5	4.8	6.2	7.6	9.0	40.4	1.8	3.3	4.8	64
65.0	29.5	30.8	32.2	33.5	34.9	36.3	37.8	39.2	40.7	42.2	43.8	45.4	47.0	65.0
5.5	30.1	1.5	2.9	4.3	5.7	7.1	8.6	40.1	1.6	3.2	4.8	6.5	8.2	5.5
6.0	0.7	2.2	3.6	5.0	6.5	8.0	9.5	1.1	2.7	4.3	5.9	7.7	9.4	6.0
6.5	1.4	2.9	4.3	5.8	7.3	8.9	40.5	2.1	3.8	5.4	7.1	8.9	50.8	6.5
7.0	2.1	3.6	5.1	6.7	8.2	9.8	1.5	3.2	4.9	6.6	8.4	50.3	2.3	7.0
67.5	32.9	34.4	36.0	37.6	39.2	40.8	42.6	44.3	46.1	47.9	49.8	51.8	53.9	67.5
8.0	3.7	5.3	6.9	8.6	40.2	1.9	3.7	5.5	7.4	9.3	51.3	3.4	5.6	8.0
8.5	4.6	6.2	7.9	9.6	1.3	3.1	4.9	6.8	8.8	50.8	2.9	5.1	7.5	8.5
9.0	5.5	7.2	8.9	40.7	2.5	4.3	6.2	8.2	50.3	2.4	4.6	7.0	9.6	9.0
9.5	6.4	8.2	40.0	1.8	3.7	5.6	7.6	9.7	1.9	4.2	6.5	9.1	61.9	9.5
70.0	37.4	39.3	41.1	43.0	45.0	47.0	49.2	51.4	53.7	56.1	58.7	61.5	64.6	70.0
0.5	8.5	40.4	2.4	4.4	6.4	8.6	50.8	3.2	5.7	8.3	61.1	4.3	7.8	0.5
1.0	9.7	1.7	3.7	5.8	8.0	50.3	2.6	5.2	7.9	60.7	3.9	7.5	71.7	1.0
1.5	40.9	3.0	5.1	7.4	9.7	2.1	4.6	7.4	60.3	3.5	7.1	71.4	6.9	1.5
2.0	2.3	4.4	6.7	9.1	51.5	4.1	6.9	9.9	3.1	6.8	71.1	6.7	90.0	2.0
72.5	43.7	46.0	48.4	50.9	53.6	56.4	59.4	62.7	66.4	70.9	76.5	90.0		72.5
3.0	5.3	7.7	50.3	3.0	5.9	8.9	62.2	6.1	70.6	6.3	90.0			3.0
3.5	7.0	9.6	2.3	5.3	8.4	61.8	5.6	70.3	6.1	90.0				3.5
4.0	8.9	51.7	4.7	7.9	61.4	5.3	9.8	75.9	90.0					4.0
4.5	51.1	4.1	7.3	60.9	4.9	9.5	75.5	90.0						4.5

TABLE 39.

Amplitudes.

Latitude.	Declination. 18°.0	18°.5	19°.0	19°.5	20°.0	20°.5	21°.0	21°.5	22°.0	22°.5	23°.0	23°.5	24°.0	Latitude.
°	°	°	°	°	°	°	°	°	°	°	°	°	°	°
0	18.0	18.5	19.0	19.5	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	0
10	8.3	8.8	9.3	9.8	0.3	0.8	1.3	1.8	2.3	2.9	3.4	3.9	4.4	10
15	8.7	9.2	9.7	20.2	0.7	1.3	1.8	2.3	2.8	3.3	3.9	4.4	4.9	15
20	9.2	9.7	20.3	0.8	1.4	1.9	2.4	3.0	3.5	4.0	4.6	5.1	5.7	20
25	9.9	20.5	1.1	1.6	2.2	2.7	3.3	3.9	4.4	5.0	5.5	6.1	6.7	25
30	20.9	21.5	22.1	22.7	23.3	23.8	24.4	25.0	25.6	26.2	26.8	27.4	28.0	30
32	1.4	2.0	2.6	3.2	3.8	4.4	5.0	5.6	6.2	6.8	7.4	8.0	8.7	32
34	1.9	2.5	3.1	3.8	4.4	5.0	5.6	6.2	6.9	7.5	8.1	8.7	9.4	34
36	2.5	3.1	3.7	4.4	5.0	5.7	6.3	6.9	7.6	8.2	8.9	9.5	30.2	36
38	3.1	3.8	4.4	5.1	5.7	6.4	7.0	7.7	8.4	9.1	9.7	30.4	1.1	38
40	23.9	24.4	25.1	25.8	26.5	27.2	27.9	28.6	29.3	30.0	30.7	31.3	32.1	40
41	4.2	4.8	5.5	6.2	6.9	7.7	8.3	9.1	9.8	0.5	1.2	1.8	2.6	41
42	4.6	5.3	6.0	6.7	7.4	8.1	8.8	9.6	30.3	1.0	1.7	2.4	3.2	42
43	5.0	5.7	6.4	7.2	7.9	8.6	9.3	30.1	0.8	1.6	2.3	3.0	3.8	43
44	5.4	6.2	6.9	7.7	8.4	9.1	9.8	0.6	1.4	2.2	2.9	3.6	4.4	44
45	25.9	26.7	27.4	28.2	28.9	29.7	30.4	31.2	32.0	32.8	33.5	34.3	35.1	45
46	6.4	7.2	7.9	8.7	9.5	30.3	1.0	1.8	2.6	3.4	4.2	5.0	5.8	46
47	6.9	7.7	8.5	9.3	30.1	0.9	1.7	2.5	3.3	4.1	4.9	5.7	6.6	47
48	7.5	8.3	9.1	9.9	0.7	1.6	2.4	3.2	4.0	4.9	5.7	6.5	7.4	48
49	8.1	8.9	9.7	30.6	1.4	2.3	3.1	4.0	4.8	5.7	6.5	7.4	8.3	49
50	28.7	29.6	30.4	31.3	32.1	33.0	33.9	34.8	35.6	36.5	37.4	38.3	39.2	50
51	9.4	30.3	1.1	2.0	2.9	3.8	4.7	5.6	6.5	7.4	8.4	9.3	40.2	51
52	30.1	1.0	1.9	2.8	3.7	4.7	5.6	6.5	7.5	8.4	9.4	40.3	1.3	52
53	0.9	1.8	2.7	3.7	4.6	5.6	6.6	7.5	8.5	9.5	40.5	1.4	2.5	53
54	1.7	2.7	3.6	4.6	5.6	6.6	7.6	8.6	9.6	40.6	1.7	2.6	3.8	54
55	32.6	33.6	34.6	35.6	36.6	37.6	38.7	39.7	40.8	41.9	42.9	44.0	45.2	55
56	3.6	4.6	5.6	6.7	7.7	8.8	9.8	41.0	2.1	3.2	4.3	5.4	6.7	56
57	4.6	5.6	6.7	7.8	8.9	40.0	41.1	2.3	3.5	4.6	5.8	7.0	8.3	57
58	5.7	6.8	7.9	9.1	40.2	1.4	2.5	3.8	5.0	6.2	7.5	8.8	50.1	58
59	6.9	8.0	9.2	40.4	1.6	2.8	4.1	5.4	6.7	8.0	9.3	50.7	2.2	59
60.0	38.2	39.4	40.6	41.9	43.2	44.5	45.8	47.2	48.6	49.9	51.4	52.9	54.4	60.0
0.5	8.9	40.1	1.4	2.7	4.0	5.4	6.7	8.1	9.6	51.0	2.5	4.1	5.7	0.5
1.0	9.6	0.9	2.2	3.5	4.9	6.3	7.7	9.1	50.6	2.1	3.7	5.3	7.0	1.0
1.5	40.4	1.7	3.0	4.4	5.8	7.3	8.7	50.2	1.7	3.3	5.0	6.7	8.5	1.5
2.0	1.2	2.5	3.9	5.3	6.8	8.3	9.8	1.3	2.9	4.6	6.3	8.1	60.0	2.0
62.5	42.0	43.4	44.9	46.3	47.8	49.4	51.0	52.6	54.2	56.0	57.8	59.7	61.7	62.5
3.0	2.9	4.3	5.9	7.4	8.9	50.5	2.2	3.9	5.6	7.5	9.4	61.4	3.6	3.0
3.5	3.8	5.3	6.9	8.5	50.1	1.7	3.5	5.3	7.1	9.1	61.1	3.4	5.7	3.5
4.0	4.8	6.4	8.0	9.7	1.3	3.0	4.9	6.7	8.7	60.7	3.0	5.5	8.1	4.0
4.5	5.9	7.5	9.2	50.9	2.6	4.5	6.4	8.4	60.5	2.8	5.2	7.8	70.9	4.5
65.0	47.0	48.7	50.4	52.2	54.0	56.0	58.0	60.2	62.5	64.9	67.6	70.6	74.4	65.0
5.5	8.2	50.0	1.8	3.6	5.6	7.6	9.8	2.2	4.7	7.3	70.4	4.1	8.9	5.5
6.0	9.4	1.3	3.2	5.1	7.3	9.4	61.8	4.4	7.1	70.2	3.8	8.6	90.0	6.0
6.5	50.8	2.7	4.7	6.8	9.1	61.4	4.0	6.8	70.0	3.7	8.4	90.0		6.5
7.0	2.3	4.3	6.4	8.7	61.1	3.7	6.5	9.8	3.5	8.3	90.0			7.0
67.5	53.9	56.0	58.3	60.7	63.4	66.2	69.5	73.3	78.2	90.0				67.5
8.0	5.6	7.9	60.3	3.0	5.9	9.2	73.0	8.1	90.0					8.0
8.5	7.5	60.0	2.6	5.6	8.9	72.8	7.9	90.0						8.5
9.0	9.6	2.3	5.3	8.7	72.7	7.7	90.0							9.0
9.5	61.9	5.0	8.4	72.4	7.6	90.0								9.5
70.0	64.6	69.1	72.2	77.4	90.0									70.0
0.5	7.8	71.9	7.2	90.0										0.5
1.0	71.7	7.1	90.0											1.0
1.5	6.9	90.0												1.5
2.0	90.0													2.0

TABLE 39.

Amplitudes.

Latitude.	Declination. 24°.0	24°.5	25°.0	25°.5	26°.0	26°.5	27°.0	27°.5	28°.0	28°.5	29°.0	29°.5	30°.0	Latitude.
°	°	°	°	°	°	°	°	°	°	°	°	°	°	°
0	24.0	24.5	25.0	25.5	26.0	26.5	27.0	27.5	28.0	28.5	29.0	29.5	30.0	0
4	4.1	4.6	5.1	5.6	6.1	6.6	7.1	7.6	8.1	8.6	9.1	9.6	0.1	4
8	4.3	4.8	5.3	5.8	6.3	6.8	7.3	7.8	8.3	8.8	9.3	9.8	0.3	8
12	4.6	5.1	5.6	6.1	6.6	7.1	7.6	8.1	8.7	9.2	9.7	30.2	0.7	12
16	5.0	5.6	6.1	6.6	7.1	7.6	8.2	8.7	9.2	9.8	30.3	0.8	1.3	16
20	25.7	26.2	26.7	27.3	27.8	28.3	28.9	29.4	30.0	30.5	31.1	31.6	32.1	20
22	6.0	6.6	7.1	7.7	8.2	8.8	9.3	9.9	0.4	1.0	1.5	2.1	2.6	22
24	6.4	7.0	7.6	8.1	8.7	9.2	9.8	30.4	0.9	1.5	2.0	2.6	3.2	24
26	6.9	7.5	8.1	8.6	9.2	9.7	30.3	0.9	1.5	2.1	2.6	3.2	3.8	26
28	7.4	8.0	8.6	9.2	9.8	30.3	0.9	1.5	2.1	2.7	3.3	3.9	4.5	28
30	28.0	28.6	29.2	29.8	30.4	31.0	31.6	32.2	32.8	33.4	34.0	34.7	35.3	30
31	8.3	8.9	9.5	30.1	0.8	1.4	2.0	2.6	3.2	3.8	4.5	5.1	5.7	31
32	8.7	9.3	9.9	0.5	1.1	1.7	2.4	3.0	3.6	4.2	4.9	5.5	6.1	32
33	9.0	9.6	30.2	0.9	1.5	2.1	2.8	3.4	4.0	4.7	5.3	6.0	6.6	33
34	9.4	30.0	0.6	31.3	1.9	2.6	3.2	3.8	4.5	5.1	5.8	6.4	7.1	34
35	29.8	30.4	31.1	31.7	32.3	33.0	33.6	34.3	35.0	35.6	36.3	36.9	37.6	35
36	30.2	0.8	1.5	2.1	2.8	3.5	4.1	4.8	5.5	6.1	6.8	7.5	8.2	36
37	0.6	1.3	1.9	2.6	3.3	4.0	4.6	5.3	6.0	6.7	7.4	8.1	8.8	37
38	1.1	1.7	2.4	3.1	3.8	4.5	5.2	5.9	6.6	7.3	8.0	8.7	9.4	38
39	1.6	2.2	2.9	3.6	4.3	5.0	5.7	6.5	7.2	7.9	8.6	9.3	40.0	39
40	32.1	32.8	33.5	34.2	34.9	35.6	36.3	37.1	37.8	38.5	39.3	40.0	40.7	40
41	2.6	3.3	4.1	4.8	5.5	6.2	7.0	7.7	8.5	9.2	40.0	0.7	1.5	41
42	3.2	3.9	4.7	5.4	6.1	6.9	7.7	8.4	9.2	9.9	0.7	1.5	2.3	42
43	3.8	4.5	5.3	6.1	6.8	7.6	8.4	9.2	9.9	40.7	1.5	2.3	3.1	43
44	4.4	5.2	6.0	6.8	7.5	8.3	9.1	40.0	40.7	1.6	2.4	3.2	4.0	44
45	35.1	35.9	36.7	37.5	38.3	39.1	39.9	40.8	41.6	42.5	43.3	44.1	45.0	45
46	5.8	6.6	7.5	8.3	9.1	40.0	40.8	1.7	2.5	3.4	4.3	5.1	6.0	46
47	6.6	7.4	8.3	9.1	40.0	0.9	1.7	2.6	3.5	4.4	5.3	6.2	7.1	47
48	7.4	8.3	9.2	40.0	0.9	1.8	2.7	3.6	4.6	5.5	6.4	7.4	8.3	48
49	8.3	9.2	40.1	1.0	1.9	2.8	3.8	4.7	5.7	6.7	7.6	8.6	9.6	49
50	39.2	40.2	41.1	42.0	43.0	43.9	44.9	45.9	46.9	47.9	48.9	50.0	51.1	50
51	40.2	1.2	2.2	3.2	4.1	5.1	6.2	7.2	8.2	9.3	50.4	1.5	2.6	51
52	1.3	2.3	3.3	4.4	5.4	6.4	7.5	8.6	9.7	50.8	2.0	3.1	4.3	52
53	2.5	3.5	4.6	5.7	6.7	7.8	9.0	50.1	51.3	2.5	3.7	4.9	6.2	53
54	3.8	4.9	6.0	7.1	8.2	9.4	50.6	1.8	3.0	4.3	5.6	6.9	8.3	54
55.0	45.2	46.3	47.5	48.6	49.8	51.1	52.3	53.6	54.9	56.3	57.7	59.1	60.7	55.0
5.5	5.9	7.1	8.3	9.5	50.7	2.0	3.3	4.6	6.0	7.4	8.9	60.4	2.0	5.5
6.0	6.7	7.9	9.1	50.4	1.6	2.9	4.3	5.7	7.1	8.6	60.1	1.7	3.4	6.0
6.5	7.5	8.8	50.0	1.3	2.6	3.9	5.4	6.8	8.3	9.9	1.5	3.2	5.0	6.5
7.0	8.3	9.6	0.9	2.2	3.6	5.0	6.5	8.0	9.5	61.2	2.9	4.7	6.6	7.0
57.5	49.2	50.5	51.9	53.2	54.7	56.2	57.7	59.3	60.9	62.6	64.5	66.4	68.5	57.5
8.0	50.1	1.5	2.9	4.3	5.8	7.4	8.9	60.6	2.4	4.2	6.2	8.3	70.7	8.0
8.5	1.1	2.5	4.0	5.5	7.0	8.6	60.3	2.1	3.9	6.0	8.1	70.4	3.1	8.5
9.0	2.2	3.6	5.1	6.7	8.3	60.0	1.8	3.7	5.7	7.9	70.3	3.0	6.2	9.0
9.5	3.3	4.8	6.4	8.0	9.7	1.5	3.4	5.5	7.7	70.1	2.8	5.9	80.1	9.5
60.0	54.4	56.0	57.7	59.4	61.2	63.2	65.2	67.4	69.9	72.6	75.8	80.0	90.0	60.0
0.5	5.7	7.4	9.1	61.0	2.9	5.0	7.2	9.6	72.4	5.8	9.9	90.0		0.5
1.0	7.0	8.8	60.7	2.6	4.7	7.0	9.5	72.3	5.5	9.8	90.0			1.0
1.5	8.5	60.3	2.3	4.4	6.7	9.2	72.0	5.4	9.7	90.0				1.5
2.0	60.0	2.0	4.2	6.5	9.0	71.9	5.2	9.6	90.0					2.0
62.5	61.7	63.9	66.2	68.8	71.7	75.1	9.5	90.0						62.5
3.0	3.6	6.0	8.6	71.5	4.9	9.4	90.0							3.0
3.5	5.7	8.3	71.3	4.8	9.3	90.0								3.5
4.0	8.1	71.1	4.6	9.2	90.0									4.0
4.5	70.9	4.4	9.0	90.0										4.5

TABLE 40.

Correction of the Amplitude as observed on the Apparent Horizon.

Latitude.	Declination. 0°	5°	10°	12°	14°	16°	18°	20°	22°	24°	26°	28°	30°	Latitude.
°	°	°	°	°	°	°	°	°	°	°	°	°	°	°
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
5	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	5
10	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	.1	10
15	.2	.2	.2	.2	.2	.2	.2	.2	.2	.2	.2	.2	.2	15
20	.2	.2	.2	.2	.2	.2	.3	.3	.3	.3	.3	.3	.3	20
24	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.4	0.4	24
28	.3	.4	.4	.4	.4	.4	.4	.4	.4	.4	.4	.4	.4	28
32	.4	.4	.4	.4	.4	.4	.4	.5	.5	.5	.5	.5	.5	32
36	.5	.5	.5	.5	.5	.5	.5	.5	.6	.6	.6	.6	.6	36
38	.5	.5	.5	.5	.6	.6	.6	.6	.6	.6	.6	.7	.7	38
40	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.7	40
42	.6	.6	.6	.6	.6	.7	.7	.7	.7	.7	.8	.8	.8	42
44	.6	.6	.7	.7	.7	.7	.7	.7	.8	.8	.8	.9	.9	44
46	.7	.7	.7	.7	.7	.8	.8	.8	.8	.9	.9	.9	1.0	46
48	.7	.8	.8	.8	.8	.8	.8	.9	.9	1.0	1.0	1.0	.1	48
50	0.8	0.8	0.8	0.8	0.9	0.9	0.9	0.9	1.0	1.1	1.1	1.1	1.3	50
52	.8	.9	.9	.9	.9	1.0	1.0	1.0	.1	.2	.2	.3	.5	52
54	.9	.9	1.0	1.0	1.0	.1	.1	.1	.2	.3	.4	.5	.8	54
56	1.0	1.0	.1	.1	.1	.2	.2	.2	.3	.5	.6	.8	2.2	56
58	.1	.1	.2	.2	.2	.3	.3	.4	.5	.7	.9	2.3	3.2	58
60	1.2	1.2	1.3	1.3	1.3	1.4	1.5	1.6	1.7	2.0	2.4	3.4		60
62	.3	.3	.4	.4	.4	.6	.7	.8	2.1	.5	3.5			62
64	.4	.4	.5	.5	.6	.8	.9	2.2	.6	3.7				64
66	.5	.5	.7	.7	.9	2.0	2.3	.8	3.8					66
68	.6	.7	.9	2.0	2.2	.4	.9	4.0						68
70	1.8	1.9	2.1	2.3	2.6	3.1	4.3							70
72	2.0	2.1	.5	.8	3.3	4.6								72
74	.2	.5	3.0	3.5	4.8									74
76	.6	3.0	.8	5.2										76
78	3.1	.6	5.7											78
80	3.8	4.4												80

TABLE 41.

Natural Sines and Cosines.

Prop. parts		0°		1°		2°		3°		4°			Prop. parts
29	M.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine	N. cos.		2
0	0	00000	100000	01745	99985	03490	99939	05234	99863	06976	99756	60	2
0	1	00029	100000	01774	99984	03519	99938	05263	99861	07005	99754	59	2
1	2	00058	100000	01803	99984	03548	99937	05292	99860	07034	99752	58	2
1	3	00087	100000	01832	99983	03577	99936	05321	99858	07063	99750	57	2
2	4	00116	100000	01862	99983	03606	99935	05350	99857	07092	99748	56	2
2	5	00145	100000	01891	99982	03635	99934	05379	99855	07121	99746	55	2
3	6	00175	100000	01920	99982	03664	99933	05408	99854	07150	99744	54	2
3	7	00204	100000	01949	99981	03693	99932	05437	99852	07179	99742	53	2
4	8	00233	100000	01978	99980	03723	99931	05466	99851	07208	99740	52	2
4	9	00262	100000	02007	99980	03752	99930	05495	99849	07237	99738	51	2
5	10	00291	100000	02036	99979	03781	99929	05524	99847	07266	99736	50	2
5	11	00320	99999	02065	99979	03810	99927	05553	99846	07295	99734	49	2
6	12	00349	99999	02094	99978	03839	99926	05582	99844	07324	99731	48	2
6	13	00378	99999	02123	99977	03868	99925	05611	99842	07353	99729	47	2
7	14	00407	99999	02152	99977	03897	99924	05640	99841	07382	99727	46	2
7	15	00436	99999	02181	99976	03926	99923	05669	99839	07411	99725	45	2
8	16	00465	99999	02211	99976	03955	99922	05698	99838	07440	99723	44	1
8	17	00495	99999	02240	99975	03984	99921	05727	99836	07469	99721	43	1
9	18	00524	99999	02269	99974	04013	99919	05756	99834	07498	99719	42	1
9	19	00553	99998	02298	99974	04042	99918	05785	99833	07527	99716	41	1
10	20	00582	99998	02327	99973	04071	99917	05814	99831	07556	99714	40	1
10	21	00611	99998	02356	99972	04100	99916	05844	99829	07585	99712	39	1
11	22	00640	99998	02385	99972	04129	99915	05873	99827	07614	99710	38	1
11	23	00669	99998	02414	99971	04159	99913	05902	99826	07643	99708	37	1
12	24	00698	99998	02443	99970	04188	99912	05931	99824	07672	99705	36	1
12	25	00727	99997	02472	99969	04217	99911	05960	99822	07701	99703	35	1
13	26	00756	99997	02501	99969	04246	99910	05989	99821	07730	99701	34	1
13	27	00785	99997	02530	99968	04275	99909	06018	99819	07759	99699	33	1
14	28	00814	99997	02560	99967	04304	99907	06047	99817	07788	99696	32	1
14	29	00844	99996	02589	99966	04333	99906	06076	99815	07817	99694	31	1
15	30	00873	99996	02618	99966	04362	99905	06105	99813	07846	99692	30	1
15	31	00902	99996	02647	99965	04391	99904	06134	99812	07875	99689	29	1
15	32	00931	99996	02676	99964	04420	99902	06163	99810	07904	99687	28	1
16	33	00960	99995	02705	99963	04449	99901	06192	99808	07933	99685	27	1
16	34	00989	99995	02734	99963	04478	99900	06221	99806	07962	99683	26	1
17	35	01018	99995	02763	99962	04507	99898	06250	99804	07991	99680	25	1
17	36	01047	99995	02792	99961	04536	99897	06279	99803	08020	99678	24	1
18	37	01076	99994	02821	99960	04565	99896	06308	99801	08049	99676	23	1
18	38	01105	99994	02850	99959	04594	99894	06337	99799	08078	99673	22	1
19	39	01134	99994	02879	99959	04623	99893	06366	99797	08107	99671	21	1
19	40	01164	99993	02908	99958	04653	99892	06395	99795	08136	99668	20	1
20	41	01193	99993	02938	99957	04682	99890	06424	99793	08165	99666	19	1
20	42	01222	99993	02967	99956	04711	99889	06453	99792	08194	99664	18	1
21	43	01251	99992	02996	99955	04740	99888	06482	99790	08223	99661	17	1
21	44	01280	99992	03025	99954	04769	99886	06511	99788	08252	99659	16	1
22	45	01309	99991	03054	99953	04798	99885	06540	99786	08281	99657	15	1
22	46	01338	99991	03083	99952	04827	99883	06569	99784	08310	99654	14	0
23	47	01367	99991	03112	99952	04856	99882	06598	99782	08339	99652	13	0
23	48	01396	99990	03141	99951	04885	99881	06627	99780	08368	99649	12	0
24	49	01425	99990	03170	99950	04914	99879	06656	99778	08397	99647	11	0
24	50	01454	99989	03199	99949	04943	99878	06685	99776	08426	99644	10	0
25	51	01483	99989	03228	99948	04972	99876	06714	99774	08455	99642	9	0
25	52	01513	99989	03257	99947	05001	99875	06743	99772	08484	99639	8	0
26	53	01542	99988	03286	99946	05030	99873	06773	99770	08513	99637	7	0
26	54	01571	99988	03316	99945	05059	99872	06802	99768	08542	99635	6	0
27	55	01600	99987	03345	99944	05088	99870	06831	99766	08571	99632	5	0
27	56	01629	99987	03374	99943	05117	99869	06860	99764	08600	99630	4	0
28	57	01658	99986	03403	99942	05146	99867	06889	99762	08629	99627	3	0
28	58	01687	99986	03432	99941	05175	99866	06918	99760	08658	99625	2	0
29	59	01716	99985	03461	99940	05205	99864	06947	99758	08687	99622	1	0
29	60	01745	99985	03490	99939	05234	99863	06976	99756	08716	99619	0	0
		N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	M.	Prop. parts
		89°		88°		87°		86°		85°			

TABLE 41.

Natural Sines and Cosines.

Prop. parts		5°		6°		7°		8°		9°			Prop. parts
29	M.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.		4
0	0	08716	99619	10453	99452	12187	99255	13917	99027	15643	98769	60	4
0	1	08745	99617	10482	99449	12216	99251	13946	99023	15672	98764	59	4
1	2	08774	99614	10511	99446	12245	99248	13975	99019	15701	98760	58	4
1	3	08803	99612	10540	99443	12274	99244	14004	99015	15730	98755	57	4
2	4	08831	99609	10569	99440	12302	99240	14033	99011	15758	98751	56	4
2	5	08860	99607	10597	99437	12331	99237	14061	99006	15787	98746	55	4
3	6	08889	99604	10626	99434	12360	99233	14090	99002	15816	98741	54	4
3	7	08918	99602	10655	99431	12389	99230	14119	98998	15845	98737	53	4
4	8	08947	99599	10684	99428	12418	99226	14148	98994	15873	98732	52	3
4	9	08976	99596	10713	99424	12447	99222	14177	98990	15902	98728	51	3
5	10	09005	99594	10742	99421	12476	99219	14205	98986	15931	98723	50	3
5	11	09034	99591	10771	99418	12504	99215	14234	98982	15959	98718	49	3
6	12	09063	99588	10800	99415	12533	99211	14263	98978	15988	98714	48	3
6	13	09092	99586	10829	99412	12562	99208	14292	98973	16017	98709	47	3
7	14	09121	99583	10858	99409	12591	99204	14320	98969	16046	98704	46	3
7	15	09150	99580	10887	99406	12620	99200	14349	98965	16074	98700	45	3
8	16	09179	99578	10916	99402	12649	99197	14378	98961	16103	98695	44	3
8	17	09208	99575	10945	99399	12678	99193	14407	98957	16132	98690	43	3
9	18	09237	99572	10973	99396	12706	99189	14436	98953	16160	98686	42	3
9	19	09266	99570	11002	99393	12735	99186	14464	98948	16189	98681	41	3
10	20	09295	99567	11031	99390	12764	99182	14493	98944	16218	98676	40	3
10	21	09324	99564	11060	99386	12793	99178	14522	98940	16246	98671	39	3
11	22	09353	99562	11089	99383	12822	99175	14551	98936	16275	98667	38	3
11	23	09382	99559	11118	99380	12851	99171	14580	98931	16304	98662	37	2
12	24	09411	99556	11147	99377	12880	99167	14608	98927	16333	98657	36	2
12	25	09440	99553	11176	99374	12908	99163	14637	98923	16361	98652	35	2
13	26	09469	99551	11205	99370	12937	99160	14666	98919	16390	98648	34	2
13	27	09498	99548	11234	99367	12966	99156	14695	98914	16419	98643	33	2
14	28	09527	99545	11263	99364	12995	99152	14723	98910	16447	98638	32	2
14	29	09556	99542	11291	99360	13024	99148	14752	98906	16476	98633	31	2
15	30	09585	99540	11320	99357	13053	99144	14781	98902	16505	98629	30	2
15	31	09614	99537	11349	99354	13081	99141	14810	98897	16533	98624	29	2
15	32	09642	99534	11378	99351	13110	99137	14838	98893	16562	98619	28	2
16	33	09671	99531	11407	99347	13139	99133	14867	98889	16591	98614	27	2
16	34	09700	99528	11436	99344	13168	99129	14896	98884	16620	98609	26	2
17	35	09729	99526	11465	99341	13197	99125	14925	98880	16648	98604	25	2
17	36	09758	99523	11494	99337	13226	99122	14954	98876	16677	98600	24	2
18	37	09787	99520	11523	99334	13254	99118	14982	98871	16706	98595	23	2
18	38	09816	99517	11552	99331	13283	99114	15011	98867	16734	98590	22	1
19	39	09845	99514	11580	99327	13312	99110	15040	98863	16763	98585	21	1
19	40	09874	99511	11609	99324	13341	99106	15069	98858	16792	98580	20	1
20	41	09903	99508	11638	99320	13370	99102	15097	98854	16820	98575	19	1
20	42	09932	99506	11667	99317	13399	99098	15126	98849	16849	98570	18	1
21	43	09961	99503	11696	99314	13427	99094	15155	98845	16878	98565	17	1
21	44	09990	99500	11725	99310	13456	99091	15184	98841	16906	98561	16	1
22	45	10019	99497	11754	99307	13485	99087	15212	98836	16935	98556	15	1
22	46	10048	99494	11783	99303	13514	99083	15241	98832	16964	98551	14	1
23	47	10077	99491	11812	99300	13543	99079	15270	98827	16992	98546	13	1
23	48	10106	99488	11840	99297	13572	99075	15299	98823	17021	98541	12	1
24	49	10135	99485	11869	99293	13600	99071	15327	98818	17050	98536	11	1
24	50	10164	99482	11898	99290	13629	99067	15356	98814	17078	98531	10	1
25	51	10192	99479	11927	99286	13658	99063	15385	98809	17107	98526	9	1
25	52	10221	99476	11956	99283	13687	99059	15414	98805	17136	98521	8	1
26	53	10250	99473	11985	99279	13716	99055	15442	98800	17164	98516	7	0
26	54	10279	99470	12014	99276	13744	99051	15471	98796	17193	98511	6	0
27	55	10308	99467	12043	99272	13773	99047	15500	98791	17222	98506	5	0
27	56	10337	99464	12071	99269	13802	99043	15529	98787	17250	98501	4	0
28	57	10366	99461	12100	99265	13831	99039	15557	98782	17279	98496	3	0
28	58	10395	99458	12129	99262	13860	99035	15586	98778	17308	98491	2	0
29	59	10424	99455	12158	99258	13889	99031	15615	98773	17336	98486	1	0
29	60	10453	99452	12187	99255	13917	99027	15643	98769	17365	98481	0	0
Prop. parts		N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	M.	
		84°		83°		82°		81°		80°			

TABLE 41.

Natural Sines and Cosines.

Prop. parts 28	M.	10° N. sine.	10° N. cos.	11° N. sine.	11° N. cos.	12° N. sine.	12° N. cos.	13° N. sine.	13° N. cos.	14° N. sine.	14° N. cos.		Prop. parts 6
0	0	17365	98481	19081	98163	20791	97815	22495	97437	24192	97030	60	6
0	1	17393	98476	19109	98157	20820	97809	22523	97430	24220	97023	59	6
1	2	17422	98471	19138	98152	20848	97803	22552	97424	24249	97015	58	6
1	3	17451	98466	19167	98146	20877	97797	22580	97417	24277	97008	57	6
2	4	17479	98461	19195	98140	20905	97791	22608	97411	24305	97001	56	6
2	5	17508	98455	19224	98135	20933	97784	22637	97404	24333	96994	55	6
3	6	17537	98450	19252	98129	20962	97778	22665	97398	24362	96987	54	5
3	7	17565	98445	19281	98124	20990	97772	22693	97391	24390	96980	53	5
4	8	17594	98440	19309	98118	21019	97766	22722	97384	24418	96973	52	5
4	9	17623	98435	19338	98112	21047	97760	22750	97378	24446	96966	51	5
5	10	17651	98430	19366	98107	21076	97754	22778	97371	24474	96959	50	5
5	11	17680	98425	19395	98101	21104	97748	22807	97365	24503	96952	49	5
6	12	17708	98420	19423	98096	21132	97742	22835	97358	24531	96945	48	5
6	13	17737	98414	19452	98090	21161	97735	22863	97351	24559	96937	47	5
7	14	17766	98409	19481	98084	21189	97729	22892	97345	24587	96930	46	5
7	15	17794	98404	19509	98079	21218	97723	22920	97338	24615	96923	45	5
7	16	17823	98399	19538	98073	21246	97717	22948	97331	24644	96916	44	4
8	17	17852	98394	19566	98067	21275	97711	22977	97325	24672	96909	43	4
8	18	17880	98389	19595	98061	21303	97705	23005	97318	24700	96902	42	4
9	19	17909	98383	19623	98056	21331	97698	23033	97311	24728	96894	41	4
9	20	17937	98378	19652	98050	21360	97692	23062	97304	24756	96887	40	4
10	21	17966	98373	19680	98044	21388	97686	23090	97298	24784	96880	39	4
10	22	17995	98368	19709	98039	21417	97680	23118	97291	24813	96873	38	4
11	23	18023	98362	19737	98033	21445	97673	23146	97284	24841	96866	37	4
11	24	18052	98357	19766	98027	21474	97667	23175	97278	24869	96858	36	4
12	25	18081	98352	19794	98021	21502	97661	23203	97271	24897	96851	35	4
12	26	18109	98347	19823	98016	21530	97655	23231	97264	24925	96844	34	3
13	27	18138	98341	19851	98010	21559	97648	23260	97257	24954	96837	33	3
13	28	18166	98336	19880	98004	21587	97642	23288	97251	24982	96829	32	3
14	29	18195	98331	19908	97998	21616	97636	23316	97244	25010	96822	31	3
14	30	18224	98325	19937	97992	21644	97630	23345	97237	25038	96815	30	3
14	31	18252	98320	19965	97987	21672	97623	23373	97230	25066	96807	29	3
15	32	18281	98315	19994	97981	21701	97617	23401	97223	25094	96800	28	3
15	33	18309	98310	20022	97975	21729	97611	23429	97217	25122	96793	27	3
16	34	18338	98304	20051	97969	21758	97604	23458	97210	25151	96786	26	3
16	35	18367	98299	20079	97963	21786	97598	23486	97203	25179	96778	25	3
17	36	18395	98294	20108	97958	21814	97592	23514	97196	25207	96771	24	2
17	37	18424	98288	20136	97952	21843	97585	23542	97189	25235	96764	23	2
18	38	18452	98283	20165	97946	21871	97579	23571	97182	25263	96756	22	2
18	39	18481	98277	20193	97940	21899	97573	23599	97176	25291	96749	21	2
19	40	18509	98272	20222	97934	21928	97566	23627	97169	25320	96742	20	2
19	41	18538	98267	20250	97928	21956	97560	23656	97162	25348	96734	19	2
20	42	18567	98261	20279	97922	21985	97553	23684	97155	25376	96727	18	2
20	43	18595	98256	20307	97916	22013	97547	23712	97148	25404	96719	17	2
21	44	18624	98250	20336	97910	22041	97541	23740	97141	25432	96712	16	2
21	45	18652	98245	20364	97905	22070	97534	23769	97134	25460	96705	15	2
21	46	18681	98240	20393	97899	22098	97528	23797	97127	25488	96697	14	1
22	47	18710	98234	20421	97893	22126	97521	23825	97120	25516	96690	13	1
22	48	18738	98229	20450	97887	22155	97515	23853	97113	25545	96682	12	1
23	49	18767	98223	20478	97881	22183	97508	23882	97106	25573	96675	11	1
23	50	18795	98218	20507	97875	22212	97502	23910	97100	25601	96667	10	1
24	51	18824	98212	20535	97869	22240	97496	23938	97093	25629	96660	9	1
24	52	18852	98207	20563	97863	22268	97489	23966	97086	25657	96653	8	1
25	53	18881	98201	20592	97857	22297	97483	23995	97079	25685	96645	7	1
25	54	18910	98196	20620	97851	22325	97476	24023	97072	25713	96638	6	1
26	55	18938	98190	20649	97845	22353	97470	24051	97065	25741	96630	5	1
26	56	18967	98185	20677	97839	22382	97463	24079	97058	25769	96623	4	0
27	57	18995	98179	20706	97833	22410	97457	24108	97051	25798	96615	3	0
27	58	19024	98174	20734	97827	22438	97450	24136	97044	25826	96608	2	0
28	59	19052	98168	20763	97821	22467	97444	24164	97037	25854	96600	1	0
28	60	19081	98163	20791	97815	22495	97437	24192	97030	25882	96593	0	0
		N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	M.	
		79°		78°		77°		76°		75°			

TABLE 41.

Natural Sines and Cosines.

Prop. parts 27		15°		16°		17°		18°		19°			Prop. parts 9
	M.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.		
0	0	25882	96593	27564	96126	29237	95630	30902	95106	32557	94552	60	9
0	1	25910	96585	27592	96118	29265	95622	30929	95097	32584	94542	59	9
1	2	25938	96578	27620	96110	29293	95613	30957	95088	32612	94533	58	9
1	3	25966	96570	27648	96102	29321	95605	30985	95079	32639	94523	57	9
2	4	25994	96562	27676	96094	29348	95596	31012	95070	32667	94514	56	8
2	5	26022	96555	27704	96086	29376	95588	31040	95061	32694	94504	55	8
3	6	26050	96547	27731	96078	29404	95579	31068	95052	32722	94495	54	8
3	7	26079	96540	27759	96070	29432	95571	31095	95043	32749	94485	53	8
4	8	26107	96532	27787	96062	29460	95562	31123	95033	32777	94476	52	8
4	9	26135	96524	27815	96054	29487	95554	31151	95024	32804	94466	51	8
5	10	26163	96517	27843	96046	29515	95545	31178	95015	32832	94457	50	8
5	11	26191	96509	27871	96037	29543	95536	31206	95006	32859	94447	49	7
5	12	26219	96502	27899	96029	29571	95528	31233	94997	32887	94438	48	7
6	13	26247	96494	27927	96021	29599	95519	31261	94988	32914	94428	47	7
6	14	26275	96486	27955	96013	29626	95511	31289	94979	32942	94418	46	7
7	15	26303	96479	27983	96005	29654	95502	31316	94970	32969	94409	45	7
7	16	26331	96471	28011	95997	29682	95493	31344	94961	32997	94399	44	7
8	17	26359	96463	28039	95989	29710	95485	31372	94952	33024	94390	43	6
8	18	26387	96456	28067	95981	29737	95476	31399	94943	33051	94380	42	6
9	19	26415	96448	28095	95972	29765	95467	31427	94933	33079	94370	41	6
9	20	26443	96440	28123	95964	29793	95459	31454	94924	33106	94361	40	6
9	21	26471	96433	28150	95956	29821	95450	31482	94915	33134	94351	39	6
10	22	26500	96425	28178	95948	29849	95441	31510	94906	33161	94342	38	6
10	23	26528	96417	28206	95940	29876	95433	31537	94897	33189	94332	37	6
11	24	26556	96410	28234	95931	29904	95424	31565	94888	33216	94322	36	5
11	25	26584	96402	28262	95923	29932	95415	31593	94878	33244	94313	35	5
12	26	26612	96394	28290	95915	29960	95407	31620	94869	33271	94303	34	5
12	27	26640	96386	28318	95907	29987	95398	31648	94860	33298	94293	33	5
13	28	26668	96379	28346	95898	30015	95389	31675	94851	33326	94284	32	5
13	29	26696	96371	28374	95890	30043	95380	31703	94842	33353	94274	31	5
14	30	26724	96363	28402	95882	30071	95372	31730	94832	33381	94264	30	5
14	31	26752	96355	28429	95874	30098	95363	31758	94823	33408	94254	29	4
14	32	26780	96347	28457	95865	30126	95354	31786	94814	33436	94245	28	4
15	33	26808	96340	28485	95857	30154	95345	31813	94805	33463	94235	27	4
15	34	26836	96332	28513	95849	30182	95337	31841	94795	33490	94225	26	4
16	35	26864	96324	28541	95841	30209	95328	31868	94786	33518	94215	25	4
16	36	26892	96316	28569	95832	30237	95319	31896	94777	33545	94206	24	4
17	37	26920	96308	28597	95824	30265	95310	31923	94768	33573	94196	23	3
17	38	26948	96301	28625	95816	30292	95301	31951	94758	33600	94186	22	3
18	39	26976	96293	28652	95807	30320	95293	31979	94749	33627	94176	21	3
18	40	27004	96285	28680	95799	30348	95284	32006	94740	33655	94167	20	3
18	41	27032	96277	28708	95791	30376	95275	32034	94730	33682	94157	19	3
19	42	27060	96269	28736	95782	30403	95266	32061	94721	33710	94147	18	3
19	43	27088	96261	28764	95774	30431	95257	32089	94712	33737	94137	17	3
20	44	27116	96253	28792	95766	30459	95248	32116	94702	33764	94127	16	2
20	45	27144	96246	28820	95757	30486	95240	32144	94693	33792	94118	15	2
21	46	27172	96238	28847	95749	30514	95231	32171	94684	33819	94108	14	2
21	47	27200	96230	28875	95740	30542	95222	32199	94674	33846	94098	13	2
22	48	27228	96222	28903	95732	30570	95213	32227	94665	33874	94088	12	2
22	49	27256	96214	28931	95724	30597	95204	32254	94656	33901	94078	11	2
23	50	27284	96206	28959	95715	30625	95195	32282	94646	33929	94068	10	2
23	51	27312	96198	28987	95707	30653	95186	32309	94637	33956	94058	9	1
23	52	27340	96190	29015	95698	30680	95177	32337	94627	33983	94049	8	1
24	53	27368	96182	29042	95690	30708	95168	32364	94618	34011	94039	7	1
24	54	27396	96174	29070	95681	30736	95159	32392	94609	34038	94029	6	1
25	55	27424	96166	29098	95673	30763	95150	32419	94599	34065	94019	5	1
25	56	27452	96158	29126	95664	30791	95142	32447	94590	34093	94009	4	1
26	57	27480	96150	29154	95656	30819	95133	32474	94580	34120	93999	3	0
26	58	27508	96142	29182	95647	30846	95124	32502	94571	34147	93989	2	0
27	59	27536	96134	29209	95639	30874	95115	32529	94561	34175	93979	1	0
27	60	27564	96126	29237	95630	30902	95106	32557	94552	34202	93969	0	0
		N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	M.	
		74°		73°		72°		71°		70°			

TABLE 41.

Natural Sines and Cosines.

Prop. parts		20°		21°		22°		23°		24°			Prop. parts
27	M.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.		11
0	0	34202	93969	35837	93358	37461	92718	39073	92050	40674	91355	60	11
0	1	34229	93959	35864	93348	37488	92707	39100	92039	40700	91343	59	11
1	2	34257	93949	35891	93337	37515	92697	39127	92028	40727	91331	58	11
1	3	34284	93939	35918	93327	37542	92686	39153	92016	40753	91319	57	10
2	4	34311	93929	35945	93316	37569	92675	39180	92005	40780	91307	56	10
2	5	34339	93919	35973	93306	37595	92664	39207	91994	40806	91295	55	10
3	6	34366	93909	36000	93295	37622	92653	39234	91982	40833	91283	54	10
3	7	34393	93899	36027	93285	37649	92642	39260	91971	40860	91272	53	10
4	8	34421	93889	36054	93274	37676	92631	39287	91959	40886	91260	52	10
4	9	34448	93879	36081	93264	37703	92620	39314	91948	40913	91248	51	9
5	10	34475	93869	36108	93253	37730	92609	39341	91936	40939	91236	50	9
5	11	34503	93859	36135	93243	37757	92598	39367	91925	40966	91224	49	9
5	12	34530	93849	36162	93232	37784	92587	39394	91914	40992	91212	48	9
6	13	34557	93839	36190	93222	37811	92576	39421	91902	41019	91200	47	9
6	14	34584	93829	36217	93211	37838	92565	39448	91891	41045	91188	46	8
7	15	34612	93819	36244	93201	37865	92554	39474	91879	41072	91176	45	8
7	16	34639	93809	36271	93190	37892	92543	39501	91868	41098	91164	44	8
8	17	34666	93799	36298	93180	37919	92532	39528	91856	41125	91152	43	8
8	18	34694	93789	36325	93169	37946	92521	39555	91845	41151	91140	42	8
9	19	34721	93779	36352	93159	37973	92510	39581	91833	41178	91128	41	8
9	20	34748	93769	36379	93148	37999	92499	39608	91822	41204	91116	40	7
9	21	34775	93759	36406	93137	38026	92488	39635	91810	41231	91104	39	7
10	22	34803	93748	36434	93127	38053	92477	39661	91799	41257	91092	38	7
10	23	34830	93738	36461	93116	38080	92466	39688	91787	41284	91080	37	7
11	24	34857	93728	36488	93106	38107	92455	39715	91775	41310	91068	36	7
11	25	34884	93718	36515	93095	38134	92444	39741	91764	41337	91056	35	6
12	26	34912	93708	36542	93084	38161	92432	39768	91752	41363	91044	34	6
12	27	34939	93698	36569	93074	38188	92421	39795	91741	41390	91032	33	6
13	28	34966	93688	36596	93063	38215	92410	39822	91729	41416	91020	32	6
13	29	34993	93677	36623	93052	38241	92399	39848	91718	41443	91008	31	6
14	30	35021	93667	36650	93042	38268	92388	39875	91706	41469	90996	30	6
14	31	35048	93657	36677	93031	38295	92377	39902	91694	41496	90984	29	5
14	32	35075	93647	36704	93020	38322	92366	39928	91683	41522	90972	28	5
15	33	35102	93637	36731	93010	38349	92355	39955	91671	41549	90960	27	5
15	34	35130	93626	36758	92999	38376	92343	39982	91660	41575	90948	26	5
16	35	35157	93616	36785	92988	38403	92332	40008	91648	41602	90936	25	5
16	36	35184	93606	36812	92978	38430	92321	40035	91636	41628	90924	24	4
17	37	35211	93596	36839	92967	38456	92310	40062	91625	41655	90911	23	4
17	38	35239	93585	36867	92956	38483	92299	40088	91613	41681	90899	22	4
18	39	35266	93575	36894	92945	38510	92287	40115	91601	41707	90887	21	4
18	40	35293	93565	36921	92935	38537	92276	40141	91590	41734	90875	20	4
18	41	35320	93555	36948	92924	38564	92265	40168	91578	41760	90863	19	3
19	42	35347	93544	36975	92913	38591	92254	40195	91566	41787	90851	18	3
19	43	35375	93534	37002	92902	38617	92243	40221	91555	41813	90839	17	3
20	44	35402	93524	37029	92892	38644	92231	40248	91543	41840	90826	16	3
20	45	35429	93514	37056	92881	38671	92220	40275	91531	41866	90814	15	3
21	46	35456	93503	37083	92870	38698	92209	40301	91519	41892	90802	14	3
21	47	35484	93493	37110	92859	38725	92198	40328	91508	41919	90790	13	2
22	48	35511	93483	37137	92849	38752	92186	40355	91496	41945	90778	12	2
22	49	35538	93472	37164	92838	38778	92175	40381	91484	41972	90766	11	2
23	50	35565	93462	37191	92827	38805	92164	40408	91472	41998	90753	10	2
23	51	35592	93452	37218	92816	38832	92152	40434	91461	42024	90741	9	2
23	52	35619	93441	37245	92805	38859	92141	40461	91449	42051	90729	8	1
24	53	35647	93431	37272	92794	38886	92130	40488	91437	42077	90717	7	1
24	54	35674	93420	37299	92784	38912	92119	40514	91425	42104	90704	6	1
25	55	35701	93410	37326	92773	38939	92107	40541	91414	42130	90692	5	1
25	56	35728	93400	37353	92762	38966	92096	40567	91402	42156	90680	4	1
26	57	35755	93389	37380	92751	38993	92085	40594	91390	42183	90668	3	1
26	58	35782	93379	37407	92740	39020	92073	40621	91378	42209	90655	2	0
27	59	35810	93368	37434	92729	39046	92062	40647	91366	42235	90643	1	0
27	60	35837	93358	37461	92718	39073	92050	40674	91355	42262	90631	0	0
		N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	M.	
		69°		68°		67°		66°		65°			

TABLE 41.

Natural Sines and Cosines.

Prop. parts 26	M.	25° N. sine.	25° N. cos.	26° N. sine.	26° N. cos.	27° N. sine.	27° N. cos.	28° N. sine.	28° N. cos.	29° N. sine.	29° N. cos.	M.	Prop. parts 14
0	0	42262	90631	43837	89879	45399	89101	46947	88295	48481	87462	60	14
0	1	42288	90618	43863	89867	45425	89087	46973	88281	48506	87448	59	14
1	2	42315	90606	43889	89854	45451	89074	46999	88267	48532	87434	58	14
1	3	42341	90594	43916	89841	45477	89061	47024	88254	48557	87420	57	13
2	4	42367	90582	43942	89828	45503	89048	47050	88240	48583	87406	56	13
2	5	42394	90569	43968	89816	45529	89035	47076	88226	48608	87391	55	13
3	6	42420	90557	43994	89803	45554	89021	47101	88213	48634	87377	54	13
3	7	42446	90545	44020	89790	45580	89008	47127	88199	48659	87363	53	12
3	8	42473	90532	44046	89777	45606	88995	47153	88185	48684	87349	52	12
4	9	42499	90520	44072	89764	45632	88981	47178	88172	48710	87335	51	12
4	10	42525	90507	44098	89752	45658	88968	47204	88158	48735	87321	50	12
5	11	42552	90495	44124	89739	45684	88955	47229	88144	48761	87306	49	11
5	12	42578	90483	44151	89726	45710	88942	47255	88130	48786	87292	48	11
6	13	42604	90470	44177	89713	45736	88928	47281	88117	48811	87278	47	11
6	14	42631	90458	44203	89700	45762	88915	47306	88103	48837	87264	46	11
7	15	42657	90446	44229	89687	45787	88902	47332	88089	48862	87250	45	11
7	16	42683	90433	44255	89674	45813	88888	47358	88075	48888	87235	44	10
7	17	42709	90421	44281	89662	45839	88875	47383	88062	48913	87221	43	10
8	18	42736	90408	44307	89649	45865	88862	47409	88048	48938	87207	42	10
8	19	42762	90396	44333	89636	45891	88848	47434	88034	48964	87193	41	10
9	20	42788	90383	44359	89623	45917	88835	47460	88020	48989	87178	40	9
9	21	42815	90371	44385	89610	45942	88822	47486	88006	49014	87164	39	9
10	22	42841	90358	44411	89597	45968	88808	47511	87993	49040	87150	38	9
10	23	42867	90346	44437	89584	45994	88795	47537	87979	49065	87136	37	9
10	24	42894	90334	44464	89571	46020	88782	47562	87965	49090	87121	36	8
11	25	42920	90321	44490	89558	46046	88768	47588	87951	49116	87107	35	8
11	26	42946	90309	44516	89545	46072	88755	47614	87937	49141	87093	34	8
12	27	42972	90296	44542	89532	46097	88741	47639	87923	49166	87079	33	8
12	28	42999	90284	44568	89519	46123	88728	47665	87909	49192	87064	32	7
13	29	43025	90271	44594	89506	46149	88715	47690	87896	49217	87050	31	7
13	30	43051	90259	44620	89493	46175	88701	47716	87882	49242	87036	30	7
13	31	43077	90246	44646	89480	46201	88688	47741	87868	49268	87021	29	7
14	32	43104	90233	44672	89467	46226	88674	47767	87854	49293	87007	28	7
14	33	43130	90221	44698	89454	46252	88661	47793	87840	49318	86993	27	6
15	34	43156	90208	44724	89441	46278	88647	47818	87826	49344	86978	26	6
15	35	43182	90196	44750	89428	46304	88634	47844	87812	49369	86964	25	6
16	36	43209	90183	44776	89415	46330	88620	47869	87798	49394	86949	24	6
16	37	43235	90171	44802	89402	46355	88607	47895	87784	49419	86935	23	5
16	38	43261	90158	44828	89389	46381	88593	47920	87770	49445	86921	22	5
17	39	43287	90146	44854	89376	46407	88580	47946	87756	49470	86906	21	5
17	40	43313	90133	44880	89363	46433	88566	47971	87743	49495	86892	20	5
18	41	43340	90120	44906	89350	46458	88553	47997	87729	49521	86878	19	4
18	42	43366	90108	44932	89337	46484	88539	48022	87715	49546	86863	18	4
19	43	43392	90095	44958	89324	46510	88526	48048	87701	49571	86849	17	4
19	44	43418	90082	44984	89311	46536	88512	48073	87687	49596	86834	16	4
20	45	43445	90070	45010	89298	46561	88499	48099	87673	49622	86820	15	4
20	46	43471	90057	45036	89285	46587	88485	48124	87659	49647	86805	14	3
20	47	43497	90045	45062	89272	46613	88472	48150	87645	49672	86791	13	3
21	48	43523	90032	45088	89259	46639	88458	48175	87631	49697	86777	12	3
21	49	43549	90019	45114	89245	46664	88445	48201	87617	49723	86762	11	3
22	50	43575	90007	45140	89232	46690	88431	48226	87603	49748	86748	10	2
22	51	43602	89994	45166	89219	46716	88417	48252	87589	49773	86733	9	2
23	52	43628	89981	45192	89206	46742	88404	48277	87575	49798	86719	8	2
23	53	43654	89968	45218	89193	46767	88390	48303	87561	49824	86704	7	2
23	54	43680	89956	45243	89180	46793	88377	48328	87546	49849	86690	6	1
24	55	43706	89943	45269	89167	46819	88363	48354	87532	49874	86675	5	1
24	56	43733	89930	45295	89153	46844	88349	48379	87518	49899	86661	4	1
25	57	43759	89918	45321	89140	46870	88336	48405	87504	49924	86646	3	1
25	58	43785	89905	45347	89127	46896	88322	48430	87490	49950	86632	2	0
26	59	43811	89892	45373	89114	46921	88308	48456	87476	49975	86617	1	0
26	60	43837	89879	45399	89101	46947	88295	48481	87462	50000	86603	0	0
		N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	M.	
	M.	64°		63°		62°		61°		60°			

TABLE 41.

Natural Sines and Cosines.

Prop. parts.		30°		31°		32°		33°		34°			Prop. parts.
25	M.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.		16
0	0	50000	86603	51504	85717	52992	84805	54464	83867	55919	82904	60	16
0	1	50025	86588	51529	85702	53017	84789	54488	83851	55943	82887	59	16
1	2	50050	86573	51554	85687	53041	84774	54513	83835	55968	82871	58	15
1	3	50076	86559	51579	85672	53066	84759	54537	83819	55992	82855	57	15
2	4	50101	86544	51604	85657	53091	84743	54561	83804	56016	82839	56	15
2	5	50126	86530	51628	85642	53115	84728	54586	83788	56040	82822	55	15
3	6	50151	86515	51653	85627	53140	84712	54610	83772	56064	82806	54	14
3	7	50176	86501	51678	85612	53164	84697	54635	83756	56088	82790	53	14
3	8	50201	86486	51703	85597	53189	84681	54659	83740	56112	82773	52	14
4	9	50227	86471	51728	85582	53214	84666	54683	83724	56136	82757	51	14
4	10	50252	86457	51753	85567	53238	84650	54708	83708	56160	82741	50	13
5	11	50277	86442	51778	85551	53263	84635	54732	83692	56184	82724	49	13
5	12	50302	86427	51803	85536	53288	84619	54756	83676	56208	82708	48	13
5	13	50327	86413	51828	85521	53312	84604	54781	83660	56232	82692	47	13
6	14	50352	86398	51852	85506	53337	84588	54805	83645	56256	82675	46	12
6	15	50377	86384	51877	85491	53361	84573	54829	83629	56280	82659	45	12
7	16	50403	86369	51902	85476	53386	84557	54854	83613	56305	82643	44	12
7	17	50428	86354	51927	85461	53411	84542	54878	83597	56329	82626	43	11
8	18	50453	86340	51952	85446	53435	84526	54902	83581	56353	82610	42	11
8	19	50478	86325	51977	85431	53460	84511	54927	83565	56377	82593	41	11
8	20	50503	86310	52002	85416	53484	84495	54951	83549	56401	82577	40	11
9	21	50528	86295	52026	85401	53509	84480	54975	83533	56425	82561	39	10
9	22	50553	86281	52051	85385	53534	84464	54999	83517	56449	82544	38	10
10	23	50578	86266	52076	85370	53558	84448	55024	83501	56473	82528	37	10
10	24	50603	86251	52101	85355	53583	84433	55048	83485	56497	82511	36	10
10	25	50628	86237	52126	85340	53607	84417	55072	83469	56521	82495	35	9
11	26	50654	86222	52151	85325	53632	84402	55097	83453	56545	82478	34	9
11	27	50679	86207	52175	85310	53656	84386	55121	83437	56569	82462	33	9
12	28	50704	86192	52200	85294	53681	84370	55145	83421	56593	82446	32	9
12	29	50729	86178	52225	85279	53705	84355	55169	83405	56617	82429	31	8
13	30	50754	86163	52250	85264	53730	84339	55194	83389	56641	82413	30	8
13	31	50779	86148	52275	85249	53754	84324	55218	83373	56665	82396	29	8
13	32	50804	86133	52299	85234	53779	84308	55242	83356	56689	82380	28	7
14	33	50829	86119	52324	85218	53804	84292	55266	83340	56713	82363	27	7
14	34	50854	86104	52349	85203	53828	84277	55291	83324	56736	82347	26	7
15	35	50879	86089	52374	85188	53853	84261	55315	83308	56760	82330	25	7
15	36	50904	86074	52399	85173	53877	84245	55339	83292	56784	82314	24	6
15	37	50929	86059	52423	85157	53902	84230	55363	83276	56808	82297	23	6
16	38	50954	86045	52448	85142	53926	84214	55388	83260	56832	82281	22	6
16	39	50979	86030	52473	85127	53951	84198	55412	83244	56856	82264	21	6
17	40	51004	86015	52498	85112	53975	84182	55436	83228	56880	82248	20	5
17	41	51029	86000	52522	85096	54000	84167	55460	83212	56904	82231	19	5
18	42	51054	85985	52547	85081	54024	84151	55484	83195	56928	82214	18	5
18	43	51079	85970	52572	85066	54049	84135	55509	83179	56952	82198	17	5
18	44	51104	85956	52597	85051	54073	84120	55533	83163	56976	82181	16	4
19	45	51129	85941	52621	85035	54097	84104	55557	83147	57000	82165	15	4
19	46	51154	85926	52646	85020	54122	84088	55581	83131	57024	82148	14	4
20	47	51179	85911	52671	85005	54146	84072	55605	83115	57047	82132	13	3
20	48	51204	85896	52696	84989	54171	84057	55630	83098	57071	82115	12	3
20	49	51229	85881	52720	84974	54195	84041	55654	83082	57095	82098	11	3
21	50	51254	85866	52745	84959	54220	84025	55678	83066	57119	82082	10	3
21	51	51279	85851	52770	84943	54244	84009	55702	83050	57143	82065	9	2
22	52	51304	85836	52794	84928	54260	83994	55726	83034	57167	82048	8	2
22	53	51329	85821	52819	84913	54293	83978	55750	83017	57191	82032	7	2
23	54	51354	85806	52844	84897	54317	83962	55775	83001	57215	82015	6	2
23	55	51379	85792	52869	84882	54342	83946	55799	82985	57238	81999	5	1
23	56	51404	85777	52893	84866	54366	83930	55823	82969	57262	81982	4	1
24	57	51429	85762	52918	84851	54391	83915	55847	82953	57286	81965	3	1
24	58	51454	85747	52943	84836	54415	83899	55871	82936	57310	81949	2	1
25	59	51479	85732	52967	84820	54440	83883	55895	82920	57334	81932	1	0
25	60	51504	85717	52992	84805	54464	83867	55919	82904	57358	81915	0	0
		N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	M.	
		59°		58°		57°		56°		55°			

TABLE 41.

Natural Sines and Cosines.

Prop. parts		35°		36°		37°		38°		39°			Prop. parts
23	M.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.		18
0	0	57358	81915	58779	80902	60182	79864	61566	78801	62932	77715	60	18
0	1	57381	81899	58802	80885	60205	79846	61589	78783	62955	77696	59	18
1	2	57405	81882	58826	80867	60228	79829	61612	78765	62977	77678	58	17
1	3	57429	81865	58849	80850	60251	79811	61635	78747	63000	77660	57	17
2	4	57453	81848	58873	80833	60274	79793	61658	78729	63022	77641	56	17
2	5	57477	81832	58896	80816	60298	79776	61681	78711	63045	77623	55	17
2	6	57501	81815	58920	80799	60321	79758	61704	78694	63068	77605	54	16
3	7	57524	81798	58943	80782	60344	79741	61726	78676	63090	77586	53	16
3	8	57548	81782	58967	80765	60367	79723	61749	78658	63113	77568	52	16
3	9	57572	81765	58990	80748	60390	79706	61772	78640	63135	77550	51	15
4	10	57596	81748	59014	80730	60414	79688	61795	78622	63158	77531	50	15
4	11	57619	81731	59037	80713	60437	79671	61818	78604	63180	77513	49	15
5	12	57643	81714	59061	80696	60460	79653	61841	78586	63203	77494	48	14
5	13	57667	81698	59084	80679	60483	79635	61864	78568	63225	77476	47	14
5	14	57691	81681	59108	80662	60506	79618	61887	78550	63248	77458	46	14
6	15	57715	81664	59131	80644	60529	79600	61909	78532	63271	77439	45	14
6	16	57738	81647	59154	80627	60553	79583	61932	78514	63293	77421	44	13
7	17	57762	81631	59178	80610	60576	79565	61955	78496	63316	77402	43	13
7	18	57786	81614	59201	80593	60599	79547	61978	78478	63338	77384	42	13
7	19	57810	81597	59225	80576	60622	79530	62001	78460	63361	77366	41	12
8	20	57833	81580	59248	80558	60645	79512	62024	78442	63383	77347	40	12
8	21	57857	81563	59272	80541	60668	79494	62046	78424	63406	77329	39	12
8	22	57881	81546	59295	80524	60691	79477	62069	78405	63428	77310	38	11
9	23	57904	81530	59318	80507	60714	79459	62092	78387	63451	77292	37	11
9	24	57928	81513	59342	80489	60738	79441	62115	78369	63473	77273	36	11
10	25	57952	81496	59365	80472	60761	79424	62138	78351	63496	77255	35	11
10	26	57976	81479	59389	80455	60784	79406	62160	78333	63518	77236	34	10
10	27	57999	81462	59412	80438	60807	79388	62183	78315	63540	77218	33	10
11	28	58023	81445	59436	80420	60830	79371	62206	78297	63563	77199	32	10
11	29	58047	81428	59459	80403	60853	79353	62229	78279	63585	77181	31	9
12	30	58070	81412	59482	80386	60876	79335	62251	78261	63608	77162	30	9
12	31	58094	81395	59506	80368	60899	79318	62274	78243	63630	77144	29	9
12	32	58118	81378	59529	80351	60922	79300	62297	78225	63653	77125	28	8
13	33	58141	81361	59552	80334	60945	79282	62320	78206	63675	77107	27	8
13	34	58165	81344	59576	80316	60968	79264	62342	78188	63698	77088	26	8
13	35	58189	81327	59599	80299	60991	79247	62365	78170	63720	77070	25	8
14	36	58212	81310	59622	80282	61015	79229	62388	78152	63742	77051	24	7
14	37	58236	81293	59646	80264	61038	79211	62411	78134	63765	77033	23	7
15	38	58260	81276	59669	80247	61061	79193	62433	78116	63787	77014	22	7
15	39	58283	81259	59693	80230	61084	79176	62456	78098	63810	76996	21	6
15	40	58307	81242	59716	80212	61107	79158	62479	78079	63832	76977	20	6
16	41	58330	81225	59739	80195	61130	79140	62502	78061	63854	76959	19	6
16	42	58354	81208	59763	80178	61153	79122	62524	78043	63877	76940	18	5
16	43	58378	81191	59786	80160	61176	79105	62547	78025	63899	76921	17	5
17	44	58401	81174	59809	80143	61199	79087	62570	78007	63922	76903	16	5
17	45	58425	81157	59832	80125	61222	79069	62592	77988	63944	76884	15	5
18	46	58449	81140	59856	80108	61245	79051	62615	77970	63966	76866	14	4
18	47	58472	81123	59879	80091	61268	79033	62638	77952	63989	76847	13	4
18	48	58496	81106	59902	80073	61291	79016	62660	77934	64011	76828	12	4
19	49	58519	81089	59926	80056	61314	78998	62683	77916	64033	76810	11	3
19	50	58543	81072	59949	80038	61337	78980	62706	77897	64056	76791	10	3
20	51	58567	81055	59972	80021	61360	78962	62728	77879	64078	76772	9	3
20	52	58590	81038	59995	80003	61383	78944	62751	77861	64100	76754	8	2
20	53	58614	81021	60019	79986	61406	78926	62774	77843	64123	76735	7	2
21	54	58637	81004	60042	79968	61429	78908	62796	77824	64145	76717	6	2
21	55	58661	80987	60065	79951	61451	78891	62819	77806	64167	76698	5	2
21	56	58684	80970	60089	79934	61474	78873	62842	77788	64190	76679	4	1
22	57	58708	80953	60112	79916	61497	78855	62864	77769	64212	76661	3	1
22	58	58731	80936	60135	79899	61520	78837	62887	77751	64234	76642	2	1
23	59	58755	80919	60158	79881	61543	78819	62909	77733	64256	76623	1	0
23	60	58779	80902	60182	79864	61566	78801	62932	77715	64279	76604	0	0
		N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	M.	
		54°		53°		52°		51°		50°			

TABLE 41.

Natural Sines and Cosines.

Prop. parts		40°		41°		42°		43°		44°			Prop. parts
22	M.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.		19
0	0	64279	76604	65606	75471	66913	74314	68200	73135	69466	71934	60	19
0	1	64301	76586	65628	75452	66935	74295	68221	73116	69487	71914	59	19
1	2	64323	76567	65650	75433	66956	74276	68242	73096	69508	71894	58	18
1	3	64346	76548	65672	75414	66978	74256	68264	73076	69529	71873	57	18
1	4	64368	76530	65694	75395	66999	74237	68285	73056	69549	71853	56	18
2	5	64390	76511	65716	75375	67021	74217	68306	73036	69570	71833	55	17
2	6	64412	76492	65738	75356	67043	74198	68327	73016	69591	71813	54	17
3	7	64435	76473	65759	75337	67064	74178	68349	72996	69612	71792	53	17
3	8	64457	76455	65781	75318	67086	74159	68370	72976	69633	71772	52	16
3	9	64479	76436	65803	75299	67107	74139	68391	72957	69654	71752	51	16
4	10	64501	76417	65825	75280	67129	74120	68412	72937	69675	71732	50	16
4	11	64524	76398	65847	75261	67151	74100	68434	72917	69696	71711	49	16
4	12	64546	76380	65869	75241	67172	74080	68455	72897	69717	71691	48	15
5	13	64568	76361	65891	75222	67194	74061	68476	72877	69737	71671	47	15
5	14	64590	76342	65913	75203	67215	74041	68497	72857	69758	71650	46	15
6	15	64612	76323	65935	75184	67237	74022	68518	72837	69779	71630	45	14
6	16	64635	76304	65956	75165	67258	74002	68539	72817	69800	71610	44	14
6	17	64657	76286	65978	75146	67280	73983	68561	72797	69821	71590	43	14
7	18	64679	76267	66000	75126	67301	73963	68582	72777	69842	71569	42	13
7	19	64701	76248	66022	75107	67323	73944	68603	72757	69862	71549	41	13
7	20	64723	76229	66044	75088	67344	73924	68624	72737	69883	71529	40	13
8	21	64746	76210	66066	75069	67366	73904	68645	72717	69904	71508	39	12
8	22	64768	76192	66088	75050	67387	73885	68666	72697	69925	71488	38	12
8	23	64790	76173	66109	75030	67409	73865	68688	72677	69946	71468	37	12
9	24	64812	76154	66131	75011	67430	73846	68709	72657	69966	71447	36	11
9	25	64834	76135	66153	74992	67452	73826	68730	72637	69987	71427	35	11
10	26	64856	76116	66175	74973	67473	73806	68751	72617	70008	71407	34	11
10	27	64878	76097	66197	74953	67495	73787	68772	72597	70029	71386	33	10
10	28	64901	76078	66218	74934	67516	73767	68793	72577	70049	71366	32	10
11	29	64923	76059	66240	74915	67538	73747	68814	72557	70070	71345	31	10
11	30	64945	76041	66262	74896	67559	73728	68835	72537	70091	71325	30	10
11	31	64967	76022	66284	74876	67580	73708	68857	72517	70112	71305	29	9
12	32	64989	76003	66306	74857	67602	73688	68878	72497	70132	71284	28	9
12	33	65011	75984	66327	74838	67623	73669	68899	72477	70153	71264	27	9
12	34	65033	75965	66349	74818	67645	73649	68920	72457	70174	71243	26	8
13	35	65055	75946	66371	74799	67666	73629	68941	72437	70195	71223	25	8
13	36	65077	75927	66393	74780	67688	73610	68962	72417	70215	71203	24	8
14	37	65100	75908	66414	74760	67709	73590	68983	72397	70236	71182	23	7
14	38	65122	75889	66436	74741	67730	73570	69004	72377	70257	71162	22	7
14	39	65144	75870	66458	74722	67752	73551	69025	72357	70277	71141	21	7
15	40	65166	75851	66480	74703	67773	73531	69046	72337	70298	71121	20	6
15	41	65188	75832	66501	74683	67795	73511	69067	72317	70319	71100	19	6
15	42	65210	75813	66523	74664	67816	73491	69088	72297	70339	71080	18	6
16	43	65232	75794	66545	74644	67837	73472	69109	72277	70360	71059	17	5
16	44	65254	75775	66566	74625	67859	73452	69130	72257	70381	71039	16	5
17	45	65276	75756	66588	74606	67880	73432	69151	72236	70401	71019	15	5
17	46	65298	75738	66610	74586	67901	73413	69172	72216	70422	70998	14	4
17	47	65320	75719	66632	74567	67923	73393	69193	72196	70443	70978	13	4
18	48	65342	75700	66653	74548	67944	73373	69214	72176	70463	70957	12	4
18	49	65364	75680	66675	74528	67965	73353	69235	72156	70484	70937	11	3
18	50	65386	75661	66697	74509	67987	73333	69256	72136	70505	70916	10	3
19	51	65408	75642	66718	74489	68008	73314	69277	72116	70525	70896	9	3
19	52	65430	75623	66740	74470	68029	73294	69298	72095	70546	70875	8	3
19	53	65452	75604	66762	74451	68051	73274	69319	72075	70567	70855	7	2
20	54	65474	75585	66783	74431	68072	73254	69340	72055	70587	70834	6	2
20	55	65496	75566	66805	74412	68093	73234	69361	72035	70608	70813	5	2
21	56	65518	75547	66827	74392	68115	73215	69382	72015	70628	70793	4	1
21	57	65540	75528	66848	74373	68136	73195	69403	71995	70649	70772	3	1
21	58	65562	75509	66870	74353	68157	73175	69424	71974	70670	70752	2	1
22	59	65584	75490	66891	74334	68179	73155	69445	71954	70690	70731	1	0
22	60	65606	75471	66913	74314	68200	73135	69466	71934	70711	70711	0	0
Prop.		N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N. cos.	N. sine.	N.cos.	N. sine.	M.	Prop.
		49°		48°		47°		46°		45°			

TABLE 42.

Logarithms of Numbers.

No. 1——100. Log. 0.00000——2.00000.

No.	Log.	No.	Log.	No.	Log.	No.	Log.	No.	Log.
1	0.00000	21	1.32222	41	1.61278	61	1.78533	81	1.90849
2	0.30103	22	1.34242	42	1.62325	62	1.79239	82	1.91381
3	0.47712	23	1.36173	43	1.63347	63	1.79934	83	1.91908
4	0.60206	24	1.38021	44	1.64345	64	1.80618	84	1.92428
5	0.69897	25	1.39794	45	1.65321	65	1.81291	85	1.92942
6	0.77815	26	1.41497	46	1.66276	66	1.81954	86	1.93450
7	0.84510	27	1.43136	47	1.67210	67	1.82607	87	1.93952
8	0.90309	28	1.44716	48	1.68124	68	1.83251	88	1.94448
9	0.95424	29	1.46240	49	1.69020	69	1.83885	89	1.94939
10	1.00000	30	1.47712	50	1.69897	70	1.84510	90	1.95424
11	1.04139	31	1.49136	51	1.70757	71	1.85126	91	1.95904
12	1.07918	32	1.50515	52	1.71600	72	1.85733	92	1.96379
13	1.11394	33	1.51851	53	1.72428	73	1.86332	93	1.96848
14	1.14613	34	1.53148	54	1.73239	74	1.86923	94	1.97313
15	1.17609	35	1.54407	55	1.74036	75	1.87506	95	1.97772
16	1.20412	36	1.55630	56	1.74819	76	1.88081	96	1.98227
17	1.23045	37	1.56820	57	1.75587	77	1.88649	97	1.98677
18	1.25527	38	1.57978	58	1.76343	78	1.89209	98	1.99123
19	1.27875	39	1.59106	59	1.77085	79	1.89763	99	1.99564
20	1.30103	40	1.60206	60	1.77815	80	1.90309	100	2.00000

TABLE 42.

Logarithms of Numbers.

No. 100——1600. Log. 00000——20412.

No.	0	1	2	3	4	5	6	7	8	9
100	00000	00043	00087	00130	00173	00217	00260	00303	00346	00389
101	00432	00475	00518	00561	00604	00647	00689	00732	00775	00817
102	00860	00903	00945	00988	01030	01072	01115	01157	01199	01242
103	01284	01326	01368	01410	01452	01494	01536	01578	01620	01662
104	01703	01745	01787	01828	01870	01912	01953	01995	02036	02078
105	02119	02160	02202	02243	02284	02325	02366	02407	02449	02490
106	02531	02572	02612	02653	02694	02735	02776	02816	02857	02898
107	02938	02979	03019	03060	03100	03141	03181	03222	03262	03302
108	03342	03383	03423	03463	03503	03543	03583	03623	03663	03703
109	03743	03782	03822	03862	03902	03941	03981	04021	04060	04100
110	04139	04179	04218	04258	04297	04336	04376	04415	04454	04493
111	04532	04571	04610	04650	04689	04727	04766	04805	04844	04883
112	04922	04961	04999	05038	05077	05115	05154	05192	05231	05269
113	05308	05346	05385	05423	05461	05500	05538	05576	05614	05652
114	05690	05729	05767	05805	05843	05881	05918	05956	05994	06032
115	06070	06108	06145	06183	06221	06258	06296	06333	06371	06408
116	06446	06483	06521	06558	06595	06633	06670	06707	06744	06781
117	06819	06856	06893	06930	06967	07004	07041	07078	07115	07151
118	07188	07225	07262	07298	07335	07372	07408	07445	07482	07518
119	07555	07591	07628	07664	07700	07737	07773	07809	07846	07882
120	07918	07954	07990	08027	08063	08099	08135	08171	08207	08243
121	08279	08314	08350	08386	08422	08458	08493	08529	08565	08600
122	08636	08672	08707	08743	08778	08814	08849	08884	08920	08955
123	08991	09026	09061	09096	09132	09167	09202	09237	09272	09307
124	09342	09377	09412	09447	09482	09517	09552	09587	09621	09656
125	09691	09726	09760	09795	09830	09864	09899	09934	09968	10003
126	10037	10072	10106	10140	10175	10209	10243	10278	10312	10346
127	10380	10415	10449	10483	10517	10551	10585	10619	10653	10687
128	10721	10755	10789	10823	10857	10890	10924	10958	10992	11025
129	11059	11093	11126	11160	11193	11227	11261	11294	11327	11361
130	11394	11428	11461	11494	11528	11561	11594	11628	11661	11694
131	11727	11760	11793	11826	11860	11893	11926	11959	11992	12024
132	12057	12090	12123	12156	12189	12222	12254	12287	12320	12352
133	12385	12418	12450	12483	12516	12548	12581	12613	12646	12678
134	12710	12743	12775	12808	12840	12872	12905	12937	12969	13001
135	13033	13066	13098	13130	13162	13194	13226	13258	13290	13322
136	13354	13386	13418	13450	13481	13513	13545	13577	13609	13640
137	13672	13704	13735	13767	13799	13830	13862	13893	13925	13956
138	13988	14019	14051	14082	14114	14145	14176	14208	14239	14270
139	14301	14333	14364	14395	14426	14457	14489	14520	14551	14582
140	14613	14644	14675	14706	14737	14768	14799	14829	14860	14891
141	14922	14953	14983	15014	15045	15076	15106	15137	15168	15198
142	15229	15259	15290	15320	15351	15381	15412	15442	15473	15503
143	15534	15564	15594	15625	15655	15685	15715	15746	15776	15806
144	15836	15866	15897	15927	15957	15987	16017	16047	16077	16107
145	16137	16167	16197	16227	16256	16286	16316	16346	16376	16406
146	16435	16465	16495	16524	16554	16584	16613	16643	16673	16702
147	16732	16761	16791	16820	16850	16879	16909	16938	16967	16997
148	17026	17056	17085	17114	17143	17173	17202	17231	17260	17289
149	17319	17348	17377	17406	17435	17464	17493	17522	17551	17580
150	17609	17638	17667	17696	17725	17754	17782	17811	17840	17869
151	17898	17926	17955	17984	18013	18041	18070	18099	18127	18156
152	18184	18213	18241	18270	18298	18327	18355	18384	18412	18441
153	18469	18498	18526	18554	18583	18611	18639	18667	18696	18724
154	18752	18780	18808	18837	18865	18893	18921	18949	18977	19005
155	19033	19061	19089	19117	19145	19173	19201	19229	19257	19285
156	19312	19340	19368	19396	19424	19451	19479	19507	19535	19562
157	19590	19618	19645	19673	19700	19728	19756	19783	19811	19838
158	19866	19893	19921	19948	19976	20003	20030	20058	20085	20112
159	20140	20167	20194	20222	20249	20276	20303	20330	20358	20385
No.	0	1	2	3	4	5	6	7	8	9

	43	42
1	4	4
2	9	8
3	13	13
4	17	17
5	22	21
6	26	25
7	30	29
8	34	34
9	39	38
	41	**40**
1	4	4
2	8	8
3	12	12
4	16	16
5	21	20
6	25	24
7	29	28
8	33	32
9	37	36
	39	**38**
1	4	4
2	8	8
3	12	11
4	16	15
5	20	19
6	23	23
7	27	27
8	31	30
9	35	34
	37	**36**
1	4	4
2	7	7
3	11	11
4	15	14
5	19	18
6	22	22
7	26	25
8	30	29
9	33	32
	35	**34**
1	4	3
2	7	7
3	11	10
4	14	14
5	18	17
6	21	20
7	25	24
8	28	27
9	32	31
	33	**32**
1	3	3
2	7	6
3	10	10
4	13	13
5	17	16
6	20	19
7	23	22
8	26	26
9	30	29

TABLE 42.

Logarithms of Numbers.

No. 1600——2200. Log. 20412——34242.

No.	0	1	2	3	4	5	6	7	8	9
160	20412	20439	20466	20493	20520	20548	20575	20602	20629	20656
161	20683	20710	20737	20763	20790	20817	20844	20871	20898	20925
162	20952	20978	21005	21032	21059	21085	21112	21139	21165	21192
163	21219	21245	21272	21299	21325	21352	21378	21405	21431	21458
164	21484	21511	21537	21564	21590	21617	21643	21669	21696	21722
165	21748	21775	21801	21827	21854	21880	21906	21932	21958	21985
166	22011	22037	22063	22089	22115	22141	22167	22194	22220	22246
167	22272	22298	22324	22350	22376	22401	22427	22453	22479	22505
168	22531	22557	22583	22608	22634	22660	22686	22712	22737	22763
169	22789	22814	22840	22866	22891	22917	22943	22968	22994	23019
170	23045	23070	23096	23121	23147	23172	23198	23223	23249	23274
171	23300	23325	23350	23376	23401	23426	23452	23477	23502	23528
172	23553	23578	23603	23629	23654	23679	23704	23729	23754	23779
173	23805	23830	23855	23880	23905	23930	23955	23980	24005	24030
174	24055	24080	24105	24130	24155	24180	24204	24229	24254	24279
175	24304	24329	24353	24378	24403	24428	24452	24477	24502	24527
176	24551	24576	24601	24625	24650	24674	24699	24724	24748	24773
177	24797	24822	24846	24871	24895	24920	24944	24969	24993	25018
178	25042	25066	25091	25115	25139	25164	25188	25212	25237	25261
179	25285	25310	25334	25358	25382	25406	25431	25455	25479	25503
180	25527	25551	25575	25600	25624	25648	25672	25696	25720	25744
181	25768	25792	25816	25840	25864	25888	25912	25935	25959	25983
182	26007	26031	26055	26079	26102	26126	26150	26174	26198	26221
183	26245	26269	26293	26316	26340	26364	26387	26411	26435	26458
184	26482	26505	26529	26553	26576	26600	26623	26647	26670	26694
185	26717	26741	26764	26788	26811	26834	26858	26881	26905	26928
186	26951	26975	26998	27021	27045	27068	27091	27114	27138	27161
187	27184	27207	27231	27254	27277	27300	27323	27346	27370	27393
188	27416	27439	27462	27485	27508	27531	27554	27577	27600	27623
189	27646	27669	27692	27715	27738	27761	27784	27807	27830	27852
190	27875	27898	27921	27944	27967	27989	28012	28035	28058	28081
191	28103	28126	28149	28171	28194	28217	28240	28262	28285	28307
192	28330	28353	28375	28398	28421	28443	28466	28488	28511	28533
193	28556	28578	28601	28623	28646	28668	28691	28713	28735	28758
194	28780	28803	28825	28847	28870	28892	28914	28937	28959	28981
195	29003	29026	29048	29070	29092	29115	29137	29159	29181	29203
196	29226	29248	29270	29292	29314	29336	29358	29380	29403	29425
197	29447	29469	29491	29513	29535	29557	29579	29601	29623	29645
198	29667	29688	29710	29732	29754	29776	29798	29820	29842	29863
199	29885	29907	29929	29951	29973	29994	30016	30038	30060	30081
200	30103	30125	30146	30168	30190	30211	30233	30255	30276	30298
201	30320	30341	30363	30384	30406	30428	30449	30471	30492	30514
202	30535	30557	30578	30600	30621	30643	30664	30685	30707	30728
203	30750	30771	30792	30814	30835	30856	30878	30899	30920	30942
204	30963	30984	31006	31027	31048	31069	31091	31112	31133	31154
205	31175	31197	31218	31239	31260	31281	31302	31323	31345	31366
206	31387	31408	31429	31450	31471	31492	31513	31534	31555	31576
207	31597	31618	31639	31660	31681	31702	31723	31744	31765	31785
208	31806	31827	31848	31869	31890	31911	31931	31952	31973	31994
209	32015	32035	32056	32077	32098	32118	32139	32160	32181	32201
210	32222	32243	32263	32284	32305	32325	32346	32366	32387	32408
211	32428	32449	32469	32490	32510	32531	32552	32572	32593	32613
212	32634	32654	32675	32695	32715	32736	32756	32777	32797	32818
213	32838	32858	32879	32899	32919	32940	32960	32980	33001	33021
214	33041	33062	33082	33102	33122	33143	33163	33183	33203	33224
215	33244	33264	33284	33304	33325	33345	33365	33385	33405	33425
216	33445	33465	33486	33506	33526	33546	33566	33586	33606	33626
217	33646	33666	33686	33706	33726	33746	33766	33786	33806	33826
218	33846	33866	33885	33905	33925	33945	33965	33985	34005	34025
219	34044	34064	34084	34104	34124	34143	34163	34183	34203	34223
No.	0	1	2	3	4	5	6	7	8	9

	31	30	29	28	27	26	25	24	23	22	21	20
1	3	3	3	3	3	3	3	2	2	2	2	2
2	6	6	6	6	5	5	5	5	5	4	4	4
3	9	9	9	8	8	8	8	7	7	7	6	6
4	12	12	12	11	11	10	10	10	9	9	8	8
5	16	15	15	14	14	13	13	12	12	11	11	10
6	19	18	17	17	16	16	15	14	14	13	13	12
7	22	21	20	20	19	18	18	17	16	15	15	14
8	25	24	23	22	22	21	20	19	18	18	17	16
9	28	27	26	25	24	23	23	22	21	20	19	18

6583—06——38

TABLE 42.

Logarithms of Numbers.

No. 2200——2800. Log. 34242——44716.

No.	0	1	2	3	4	5	6	7	8	9
220	34242	34262	34282	34301	34321	34341	34361	34380	34400	34420
221	34439	34459	34479	34498	34518	34537	34557	34577	34596	34616
222	34635	34655	34674	34694	34713	34733	34753	34772	34792	34811
223	34830	34850	34869	34889	34908	34928	34947	34967	34986	35005
224	35025	35044	35064	35083	35102	35122	35141	35160	35180	35199
225	35218	35238	35257	35276	35295	35315	35334	35353	35372	35392
226	35411	35430	35449	35468	35488	35507	35526	35545	35564	35583
227	35603	35622	35641	35660	35679	35698	35717	35736	35755	35774
228	35793	35813	35832	35851	35870	35889	35908	35927	35946	35965
229	35984	36003	36021	36040	36059	36078	36097	36116	36135	36154
230	36173	36192	36211	36229	36248	36267	36286	36305	36324	36342
231	36361	36380	36399	36418	36436	36455	36474	36493	36511	36530
232	36549	36568	36586	36605	36624	36642	36661	36680	36698	36717
233	36736	36754	36773	36791	36810	36829	36847	36866	36884	36903
234	36922	36940	36959	36977	36996	37014	37033	37051	37070	37088
235	37107	37125	37144	37162	37181	37199	37218	37236	37254	37273
236	37291	37310	37328	37346	37365	37383	37401	37420	37438	37457
237	37475	37493	37511	37530	37548	37566	37585	37603	37621	37639
238	37658	37676	37694	37712	37731	37749	37767	37785	37803	37822
239	37840	37858	37876	37894	37912	37931	37949	37967	37985	38003
240	38021	38039	38057	38075	38093	38112	38130	38148	38166	38184
241	38202	38220	38238	38256	38274	38292	38310	38328	38346	38364
242	38382	38399	38417	38435	38453	38471	38489	38507	38525	38543
243	38561	38578	38596	38614	38632	38650	38668	38686	38703	38721
244	38739	38757	38775	38792	38810	38828	38846	38863	38881	38899
245	38917	38934	38952	38970	38987	39005	39023	39041	39058	39076
246	39094	39111	39129	39146	39164	39182	39199	39217	39235	39252
247	39270	39287	39305	39322	39340	39358	39375	39393	39410	39428
248	39445	39463	39480	39498	39515	39533	39550	39568	39585	39602
249	39620	39637	39655	39672	39690	39707	39724	39742	39759	39777
250	39794	39811	39829	39846	39863	39881	39898	39915	39933	39950
251	39967	39985	40002	40019	40037	40054	40071	40088	40106	40123
252	40140	40157	40175	40192	40209	40226	40243	40261	40278	40295
253	40312	40329	40346	40364	40381	40398	40415	40432	40449	40466
254	40483	40500	40518	40535	40552	40569	40586	40603	40620	40637
255	40654	40671	40688	40705	40722	40739	40756	40773	40790	40807
256	40824	40841	40858	40875	40892	40909	40926	40943	40960	40976
257	40993	41010	41027	41044	41061	41078	41095	41111	41128	41145
258	41162	41179	41196	41212	41229	41246	41263	41280	41296	41313
259	41330	41347	41363	41380	41397	41414	41430	41447	41464	41481
260	41497	41514	41531	41547	41564	41581	41597	41614	41631	41647
261	41664	41681	41697	41714	41731	41747	41764	41780	41797	41814
262	41830	41847	41863	41880	41896	41913	41929	41946	41963	41979
263	41996	42012	42029	42045	42062	42078	42095	42111	42127	42144
264	42160	42177	42193	42210	42226	42243	42259	42275	42292	42308
265	42325	42341	42357	42374	42390	42406	42423	42439	42455	42472
266	42488	42504	42521	42537	42553	42570	42586	42602	42619	42635
267	42651	42667	42684	42700	42716	42732	42749	42765	42781	42797
268	42813	42830	42846	42862	42878	42894	42911	42927	42943	42959
269	42975	42991	43008	43024	43040	43056	43072	43088	43104	43120
270	43136	43152	43169	43185	43201	43217	43233	43249	43265	43281
271	43297	43313	43329	43345	43361	43377	43393	43409	43425	43441
272	43457	43473	43489	43505	43521	43537	43553	43569	43584	43600
273	43616	43632	43648	43664	43680	43696	43712	43727	43743	43759
274	43775	43791	43807	43823	43838	43854	43870	43886	43902	43917
275	43933	43949	43965	43981	43996	44012	44028	44044	44059	44075
276	44091	44107	44122	44138	44154	44170	44185	44201	44217	44232
277	44248	44264	44279	44295	44311	44326	44342	44358	44373	44389
278	44404	44420	44436	44451	44467	44483	44498	44514	44529	44545
279	44560	44576	44592	44607	44623	44638	44654	44669	44685	44700
No.	0	1	2	3	4	5	6	7	8	9

	20	19	18	17	16	15
1	2	2	2	2	2	2
2	4	4	4	3	3	3
3	6	6	5	5	5	5
4	8	8	7	7	6	6
5	10	10	9	9	8	8
6	12	11	11	10	10	9
7	14	13	13	12	11	11
8	16	15	14	14	13	12
9	18	17	16	15	14	14

Logarithms of Numbers.

No. 2800——3400. Log. 44716——53148.

No.	0	1	2	3	4	5	6	7	8	9
280	44716	44731	44747	44762	44778	44793	44809	44824	44840	44855
281	44871	44886	44902	44917	44932	44948	44963	44979	44994	45010
282	45025	45040	45056	45071	45086	45102	45117	45133	45148	45163
283	45179	45194	45209	45225	45240	45255	45271	45286	45301	45317
284	45332	45347	45362	45378	45393	45408	45423	45439	45454	45469
285	45484	45500	45515	45530	45545	45561	45576	45591	45606	45621
286	45637	45652	45667	45682	45697	45712	45728	45743	45758	45773
287	45788	45803	45818	45834	45849	45864	45879	45894	45909	45924
288	45939	45954	45969	45984	46000	46015	46030	46045	46060	46075
289	46090	46105	46120	46135	46150	46165	46180	46195	46210	46225
290	46240	46255	46270	46285	46300	46315	46330	46345	46359	46374
291	46389	46404	46419	46434	46449	46464	46479	46494	46509	46523
292	46538	46553	46568	46583	46598	46613	46627	46642	46657	46672
293	46687	46702	46716	46731	46746	46761	46776	46790	46805	46820
294	46835	46850	46864	46879	46894	46909	46923	46938	46953	46967
295	46982	46997	47012	47026	47041	47056	47070	47085	47100	47114
296	47129	47144	47159	47173	47188	47202	47217	47232	47246	47261
297	47276	47290	47305	47319	47334	47349	47363	47378	47392	47407
298	47422	47436	47451	47465	47480	47494	47509	47524	47538	47553
299	47567	47582	47596	47611	47625	47640	47654	47669	47683	47698
300	47712	47727	47741	47756	47770	47784	47799	47813	47828	47842
301	47857	47871	47885	47900	47914	47929	47943	47958	47972	47986
302	48001	48015	48029	48044	48058	48073	48087	48101	48116	48130
303	48144	48159	48173	48187	48202	48216	48230	48244	48259	48273
304	48287	48302	48316	48330	48344	48359	48373	48387	48401	48416
305	48430	48444	48458	48473	48487	48501	48515	48530	48544	48558
306	48572	48586	48601	48615	48629	48643	48657	48671	48686	48700
307	48714	48728	48742	48756	48770	48785	48799	48813	48827	48841
308	48855	48869	48883	48897	48911	48926	48940	48954	48968	48982
309	48996	49010	49024	49038	49052	49066	49080	49094	49108	49122
310	49136	49150	49164	49178	49192	49206	49220	49234	49248	49262
311	49276	49290	49304	49318	49332	49346	49360	49374	49388	49402
312	49415	49429	49443	49457	49471	49485	49499	49513	49527	49541
313	49554	49568	49582	49596	49610	49624	49638	49651	49665	49679
314	49693	49707	49721	49734	49748	49762	49776	49790	49803	49817
315	49831	49845	49859	49872	49886	49900	49914	49927	49941	49955
316	49969	49982	49996	50010	50024	50037	50051	50065	50079	50092
317	50106	50120	50133	50147	50161	50174	50188	50202	50215	50229
318	50243	50256	50270	50284	50297	50311	50325	50338	50352	50365
319	50379	50393	50406	50420	50433	50447	50461	50474	50488	50501
320	50515	50529	50542	50556	50569	50583	50596	50610	50623	50637
321	50651	50664	50678	50691	50705	50718	50732	50745	50759	50772
322	50786	50799	50813	50826	50840	50853	50866	50880	50893	50907
323	50920	50934	50947	50961	50974	50987	51001	51014	51028	51041
324	51055	51068	51081	51095	51108	51121	51135	51148	51162	51175
325	51188	51202	51215	51228	51242	51255	51268	51282	51295	51308
326	51322	51335	51348	51362	51375	51388	51402	51415	51428	51441
327	51455	51468	51481	51495	51508	51521	51534	51548	51561	51574
328	51587	51601	51614	51627	51640	51654	51667	51680	51693	51706
329	51720	51733	51746	51759	51772	51786	51799	51812	51825	51838
330	51851	51865	51878	51891	51904	51917	51930	51943	51957	51970
331	51983	51996	52009	52022	52035	52048	52061	52075	52088	52101
332	52114	52127	52140	52153	52166	52179	52192	52205	52218	52231
333	52244	52257	52270	52284	52297	52310	52323	52336	52349	52362
334	52375	52388	52401	52414	52427	52440	52453	52466	52479	52492
335	52504	52517	52530	52543	52556	52569	52582	52595	52608	52621
336	52634	52647	52660	52673	52686	52699	52711	52724	52737	52750
337	52763	52776	52789	52802	52815	52827	52840	52853	52866	52879
338	52892	52905	52917	52930	52943	52956	52969	52982	52994	53007
339	53020	53033	53046	53058	53071	53084	53097	53110	53122	53135
No.	0	1	2	3	4	5	6	7	8	9

	16	15	14	13	12
1	2	2	1	1	1
2	3	3	3	3	2
3	5	5	4	4	4
4	6	6	6	5	5
5	8	8	7	7	6
6	10	9	8	8	7
7	11	11	10	9	8
8	13	12	11	10	10
9	14	14	13	12	11

TABLE 42.

Logarithms of Numbers.

No. 3400——4000. Log. 53148——60206.

No.	0	1	2	3	4	5	6	7	8	9
340	53148	53161	53173	53186	53199	53212	53224	53237	53250	53263
341	53275	53288	53301	53314	53326	53339	53352	53364	53377	53390
342	53403	53415	53428	53441	53453	53466	53479	53491	53504	53517
343	53529	53542	53555	53567	53580	53593	53605	53618	53631	53643
344	53656	53668	53681	53694	53706	53719	53732	53744	53757	53769
345	53782	53794	53807	53820	53832	53845	53857	53870	53882	53895
346	53908	53920	53933	53945	53958	53970	53983	53995	54008	54020
347	54033	54045	54058	54070	54083	54095	54108	54120	54133	54145
348	54158	54170	54183	54195	54208	54220	54233	54245	54258	54270
349	54283	54295	54307	54320	54332	54345	54357	54370	54382	54394
350	54407	54419	54432	54444	54456	54469	54481	54494	54506	54518
351	54531	54543	54555	54568	54580	54593	54605	54617	54630	54642
352	54654	54667	54679	54691	54704	54716	54728	54741	54753	54765
353	54777	54790	54802	54814	54827	54839	54851	54864	54876	54888
354	54900	54913	54925	54937	54949	54962	54974	54986	54998	55011
355	55023	55035	55047	55060	55072	55084	55096	55108	55121	55133
356	55145	55157	55169	55182	55194	55206	55218	55230	55242	55255
357	55267	55279	55291	55303	55315	55328	55340	55352	55364	55376
358	55388	55400	55413	55425	55437	55449	55461	55473	55485	55497
359	55509	55522	55534	55546	55558	55570	55582	55594	55606	55618
360	55630	55642	55654	55666	55678	55691	55703	55715	55727	55739
361	55751	55763	55775	55787	55799	55811	55823	55835	55847	55859
362	55871	55883	55895	55907	55919	55931	55943	55955	55967	55979
363	55991	56003	56015	56027	56038	56050	56062	56074	56086	56098
364	56110	56122	56134	56146	56158	56170	56182	56194	56205	56217
365	56229	56241	56253	56265	56277	56289	56301	56312	56324	56336
366	56348	56360	56372	56384	56396	56407	56419	56431	56443	56455
367	56467	56478	56490	56502	56514	56526	56538	56549	56561	56573
368	56585	56597	56608	56620	56632	56644	56656	56667	56679	56691
369	56703	56714	56726	56738	56750	56761	56773	56785	56797	56808
370	56820	56832	56844	56855	56867	56879	56891	56902	56914	56926
371	56937	56949	56961	56972	56984	56996	57008	57019	57031	57043
372	57054	57066	57078	57089	57101	57113	57124	57136	57148	57159
373	57171	57183	57194	57206	57217	57229	57241	57252	57264	57276
374	57287	57299	57310	57322	57334	57345	57357	57368	57380	57392
375	57403	57415	57426	57438	57449	57461	57473	57484	57496	57507
376	57519	57530	57542	57553	57565	57576	57588	57600	57611	57623
377	57634	57646	57657	57669	57680	57692	57703	57715	57726	57738
378	57749	57761	57772	57784	57795	57807	57818	57830	57841	57852
379	57864	57875	57887	57898	57910	57921	57933	57944	57955	57967
380	57978	57990	58001	58013	58024	58035	58047	58058	58070	58081
381	58092	58104	58115	58127	58138	58149	58161	58172	58184	58195
382	58206	58218	58229	58240	58252	58263	58274	58286	58297	58309
383	58320	58331	58343	58354	58365	58377	58388	58399	58410	58422
384	58433	58444	58456	58467	58478	58490	58501	58512	58524	58535
385	58546	58557	58569	58580	58591	58602	58614	58625	58636	58647
386	58659	58670	58681	58692	58704	58715	58726	58737	58749	58760
387	58771	58782	58794	58805	58816	58827	58838	58850	58861	58872
388	58883	58894	58906	58917	58928	58939	58950	58961	58973	58984
389	58995	59006	59017	59028	59040	59051	59062	59073	59084	59095
390	59106	59118	59129	59140	59151	59162	59173	59184	59195	59207
391	59218	59229	59240	59251	59262	59273	59284	59295	59306	59318
392	59329	59340	59351	59362	59373	59384	59395	59406	59417	59428
393	59439	59450	59461	59472	59483	59494	59506	59517	59528	59539
394	59550	59561	59572	59583	59594	59605	59616	59627	59638	59649
395	59660	59671	59682	59693	59704	59715	59726	59737	59748	59759
396	59770	59780	59791	59802	59813	59824	59835	59846	59857	59868
397	59879	59890	59901	59912	59923	59934	59945	59956	59966	59977
398	59988	59999	60010	60021	60032	60043	60054	60065	60076	60086
399	60097	60108	60119	60130	60141	60152	60163	60173	60184	60195
No.	0	1	2	3	4	5	6	7	8	9

	13	12	11	10
1	1	1	1	1
2	3	2	2	2
3	4	4	3	3
4	5	5	4	4
5	7	6	6	5
6	8	7	7	6
7	9	8	8	7
8	10	10	9	8
9	12	11	10	9

Logarithms of Numbers.

No. 4000——4600. Log. 60206——66276.

No.	0	1	2	3	4	5	6	7	8	9
400	60206	60217	60228	60239	60249	60260	60271	60282	60293	60304
401	60314	60325	60336	60347	60358	60369	60379	60390	60401	60412
402	60423	60433	60444	60455	60466	60477	60487	60498	60509	60520
403	60531	60541	60552	60563	60574	60584	60595	60606	60617	60627
404	60638	60649	60660	60670	60681	60692	60703	60713	60724	60735
405	60746	60756	60767	60778	60788	60799	60810	60821	60831	60842
406	60853	60863	60874	60885	60895	60906	60917	60927	60938	60949
407	60959	60970	60981	60991	61002	61013	61023	61034	61045	61055
408	61066	61077	61087	61098	61109	61119	61130	61140	61151	61162
409	61172	61183	61194	61204	61215	61225	61236	61247	61257	61268
410	61278	61289	61300	61310	61321	61331	61342	61352	61363	61374
411	61384	61395	61405	61416	61426	61437	61448	61458	61469	61479
412	61490	61500	61511	61521	61532	61542	61553	61563	61574	61584
413	61595	61606	61616	61627	61637	61648	61658	61669	61679	61690
414	61700	61711	61721	61731	61742	61752	61763	61773	61784	61794
415	61805	61815	61826	61836	61847	61857	61868	61878	61888	61899
416	61909	61920	61930	61941	61951	61962	61972	61982	61993	62003
417	62014	62024	62034	62045	62055	62066	62076	62086	62097	62107
418	62118	62128	62138	62149	62159	62170	62180	62190	62201	62211
419	62221	62232	62242	62252	62263	62273	62284	62294	62304	62315
420	62325	62335	62346	62356	62366	62377	62387	62397	62408	62418
421	62428	62439	62449	62459	62469	62480	62490	62500	62511	62521
422	62531	62542	62552	62562	62572	62583	62593	62603	62613	62624
423	62634	62644	62655	62665	62675	62685	62696	62706	62716	62726
424	62737	62747	62757	62767	62778	62788	62798	62808	62818	62829
425	62839	62849	62859	62870	62880	62890	62900	62910	62921	62931
426	62941	62951	62961	62972	62982	62992	63002	63012	63022	63033
427	63043	63053	63063	63073	63083	63094	63104	63114	63124	63134
428	63144	63155	63165	63175	63185	63195	63205	63215	63225	63236
429	63246	63256	63266	63276	63286	63296	63306	63317	63327	63337
430	63347	63357	63367	63377	63387	63397	63407	63417	63428	63438
431	63448	63458	63468	63478	63488	63498	63508	63518	63528	63538
432	63548	63558	63568	63579	63589	63599	63609	63619	63629	63639
433	63649	63659	63669	63679	63689	63699	63709	63719	63729	63739
434	63749	63759	63769	63779	63789	63799	63809	63819	63829	63839
435	63849	63859	63869	63879	63889	63899	63909	63919	63929	63939
436	63949	63959	63969	63979	63988	63998	64008	64018	64028	64038
437	64048	64058	64068	64078	64088	64098	64108	64118	64128	64137
438	64147	64157	64167	64177	64187	64197	64207	64217	64227	64237
439	64246	64256	64266	64276	64286	64296	64306	64316	64326	64335
440	64345	64355	64365	64375	64385	64395	64404	64414	64424	64434
441	64444	64454	64464	64473	64483	64493	64503	64513	64523	64532
442	64542	64552	64562	64572	64582	64591	64601	64611	64621	64631
443	64640	64650	64660	64670	64680	64689	64699	64709	64719	64729
444	64738	64748	64758	64768	64777	64787	64797	64807	64816	64826
445	64836	64846	64856	64865	64875	64885	64895	64904	64914	64924
446	64933	64943	64953	64963	64972	64982	64992	65002	65011	65021
447	65031	65040	65050	65060	65070	65079	65089	65099	65108	65118
448	65128	65137	65147	65157	65167	65176	65186	65196	65205	65215
449	65225	65234	65244	65254	65263	65273	65283	65292	65302	65312
450	65321	65331	65341	65350	65360	65369	65379	65389	65398	65408
451	65418	65427	65437	65447	65456	65466	65475	65485	65495	65504
452	65514	65523	65533	65543	65552	65562	65571	65581	65591	65600
453	65610	65619	65629	65639	65648	65658	65667	65677	65686	65696
454	65706	65715	65725	65734	65744	65753	65763	65772	65782	65792
455	65801	65811	65820	65830	65839	65849	65858	65868	65877	65887
456	65896	65906	65916	65925	65935	65944	65954	65963	65973	65982
457	65992	66001	66011	66020	66030	66039	66049	66058	66068	66077
458	66087	66096	66106	66115	66124	66134	66143	66153	66162	66172
459	66181	66191	66200	66210	66219	66229	66238	66247	66257	66266
No.	0	1	2	3	4	5	6	7	8	9

	11
1	1
2	2
3	3
4	4
5	6
6	7
7	8
8	9
9	10

	10
1	1
2	2
3	3
4	4
5	5
6	6
7	7
8	8
9	9

	9
1	1
2	2
3	3
4	4
5	5
6	5
7	6
8	7
9	8

TABLE 42.

Logarithms of Numbers.

No. 4600——5200. Log. 66276——71600.

No.	0	1	2	3	4	5	6	7	8	9
460	66276	66285	66295	66304	66314	66323	66332	66342	66351	66361
461	66370	66380	66389	66398	66408	66417	66427	66436	66445	66455
462	66464	66474	66483	66492	66502	66511	66521	66530	66539	66549
463	66558	66567	66577	66586	66596	66605	66614	66624	66633	66642
464	66652	66661	66671	66680	66689	66699	66708	66717	66727	66736
465	66745	66755	66764	66773	66783	66792	66801	66811	66820	66829
466	66839	66848	66857	66867	66876	66885	66894	66904	66913	66922
467	66932	66941	66950	66960	66969	66978	66987	66997	67006	67015
468	67025	67034	67043	67052	67062	67071	67080	67089	67099	67108
469	67117	67127	67136	67145	67154	67164	67173	67182	67191	67201
470	67210	67219	67228	67237	67247	67256	67265	67274	67284	67293
471	67302	67311	67321	67330	67339	67348	67357	67367	67376	67385
472	67394	67403	67413	67422	67431	67440	67449	67459	67468	67477
473	67486	67495	67504	67514	67523	67532	67541	67550	67560	67569
474	67578	67587	67596	67605	67614	67624	67633	67642	67651	67660
475	67669	67679	67688	67697	67706	67715	67724	67733	67742	67752
476	67761	67770	67779	67788	67797	67806	67815	67825	67834	67843
477	67852	67861	67870	67879	67888	67897	67906	67916	67925	67934
478	67943	67952	67961	67970	67979	67988	67997	68006	68015	68024
479	68034	68043	68052	68061	68070	68079	68088	68097	68106	68115
480	68124	68133	68142	68151	68160	68169	68178	68187	68196	68205
481	68215	68224	68233	68242	68251	68260	68269	68278	68287	68296
482	68305	68314	68323	68332	68341	68350	68359	68368	68377	68386
483	68395	68404	68413	68422	68431	68440	68449	68458	68467	68476
484	68485	68494	68502	68511	68520	68529	68538	68547	68556	68565
485	68574	68583	68592	68601	68610	68619	68628	68637	68646	68655
486	68664	68673	68681	68690	68699	68708	68717	68726	68735	68744
487	68753	68762	68771	68780	68789	68797	68806	68815	68824	68833
488	68842	68851	68860	68869	68878	68886	68895	68904	68913	68922
489	68931	68940	68949	68958	68966	68975	68984	68993	69002	69011
490	69020	69028	69037	69046	69055	69064	69073	69082	69090	69099
491	69108	69117	69126	69135	69144	69152	69161	69170	69179	69188
492	69197	69205	69214	69223	69232	69241	69249	69258	69267	69276
493	69285	69294	69302	69311	69320	69329	69338	69346	69355	69364
494	69373	69381	69390	69399	69408	69417	69425	69434	69443	69452
495	69461	69469	69478	69487	69496	69504	69513	69522	69531	69539
496	69548	69557	69566	69574	69583	69592	69601	69609	69618	69627
497	69636	69644	69653	69662	69671	69679	69688	69697	69705	69714
498	69723	69732	69740	69749	69758	69767	69775	69784	69793	69801
499	69810	69819	69827	69836	69845	69854	69862	69871	69880	69888
500	69897	69906	69914	69923	69932	69940	69949	69958	69966	69975
501	69984	69992	70001	70010	70018	70027	70036	70044	70053	70062
502	70070	70079	70088	70096	70105	70114	70122	70131	70140	70148
503	70157	70165	70174	70183	70191	70200	70209	70217	70226	70234
504	70243	70252	70260	70269	70278	70286	70295	70303	70312	70321
505	70329	70338	70346	70355	70364	70372	70381	70389	70398	70406
506	70415	70424	70432	70441	70449	70458	70467	70475	70484	70492
507	70501	70509	70518	70526	70535	70544	70552	70561	70569	70578
508	70586	70595	70603	70612	70621	70629	70638	70646	70655	70663
509	70672	70680	70689	70697	70706	70714	70723	70731	70740	70749
510	70757	70766	70774	70783	70791	70800	70808	70817	70825	70834
511	70842	70851	70859	70868	70876	70885	70893	70902	70910	70919
512	70927	70935	70944	70952	70961	70969	70978	70986	70995	71003
513	71012	71020	71029	71037	71046	71054	71063	71071	71079	71088
514	71096	71105	71113	71122	71130	71139	71147	71155	71164	71172
515	71181	71189	71198	71206	71214	71223	71231	71240	71248	71257
516	71265	71273	71282	71290	71299	71307	71315	71324	71332	71341
517	71349	71357	71366	71374	71383	71391	71399	71408	71416	71425
518	71433	71441	71450	71458	71466	71475	71483	71492	71500	71508
519	71517	71525	71533	71542	71550	71559	71567	71575	71584	71592
No.	0	1	2	3	4	5	6	7	8	9

	10
1	1
2	2
3	3
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7	7
8	8
9	9

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1	1
2	2
3	3
4	4
5	5
6	5
7	6
8	7
9	8

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1	1
2	2
3	2
4	3
5	4
6	5
7	6
8	6
9	7

Logarithms of Numbers.

No. 5200——5800. Log. 71600——76343.

No.	0	1	2	3	4	5	6	7	8	9
520	71600	71609	71617	71625	71634	71642	71650	71659	71667	71675
521	71684	71692	71700	71709	71717	71725	71734	71742	71750	71759
522	71767	71775	71784	71792	71800	71809	71817	71825	71834	71842
523	71850	71858	71867	71875	71883	71892	71900	71908	71917	71925
524	71933	71941	71950	71958	71966	71975	71983	71991	71999	72008
525	72016	72024	72032	72041	72049	72057	72066	72074	72082	72090
526	72099	72107	72115	72123	72132	72140	72148	72156	72165	72173
527	72181	72189	72198	72206	72214	72222	72230	72239	72247	72255
528	72263	72272	72280	72288	72296	72304	72313	72321	72329	72337
529	72346	72354	72362	72370	72378	72387	72395	72403	72411	72419
530	72428	72436	72444	72452	72460	72469	72477	72485	72493	72501
531	72509	72518	72526	72534	72542	72550	72558	72567	72575	72583
532	72591	72599	72607	72616	72624	72632	72640	72648	72656	72665
533	72673	72681	72689	72697	72705	72713	72722	72730	72738	72746
534	72754	72762	72770	72779	72787	72795	72803	72811	72819	72827
535	72835	72843	72852	72860	72868	72876	72884	72892	72900	72908
536	72916	72925	72933	72941	72949	72957	72965	72973	72981	72989
537	72997	73006	73014	73022	73030	73038	73046	73054	73062	73070
538	73078	73086	73094	73102	73111	73119	73127	73135	73143	73151
539	73159	73167	73175	73183	73191	73199	73207	73215	73223	73231
540	73239	73247	73255	73263	73272	73280	73288	73296	73304	73312
541	73320	73328	73336	73344	73352	73360	73368	73376	73384	73392
542	73400	73408	73416	73424	73432	73440	73448	73456	73464	73472
543	73480	73488	73496	73504	73512	73520	73528	73536	73544	73552
544	73560	73568	73576	73584	73592	73600	73608	73616	73624	73632
545	73640	73648	73656	73664	73672	73679	73687	73695	73703	73711
546	73719	73727	73735	73743	73751	73759	73767	73775	73783	73791
547	73799	73807	73815	73823	73830	73838	73846	73854	73862	73870
548	73878	73886	73894	73902	73910	73918	73926	73933	73941	73949
549	73957	73965	73973	73981	73989	73997	74005	74013	74020	74028
550	74036	74044	74052	74060	74068	74076	74084	74092	74099	74107
551	74115	74123	74131	74139	74147	74155	74162	74170	74178	74186
552	74194	74202	74210	74218	74225	74233	74241	74249	74257	74265
553	74273	74280	74288	74296	74304	74312	74320	74327	74335	74343
554	74351	74359	74367	74374	74382	74390	74398	74406	74414	74421
555	74429	74437	74445	74453	74461	74468	74476	74484	74492	74500
556	74507	74515	74523	74531	74539	74547	74554	74562	74570	74578
557	74586	74593	74601	74609	74617	74624	74632	74640	74648	74656
558	74663	74671	74679	74687	74695	74702	74710	74718	74726	74733
559	74741	74749	74757	74764	74772	74780	74788	74796	74803	74811
560	74819	74827	74834	74842	74850	74858	74865	74873	74881	74889
561	74896	74904	74912	74920	74927	74935	74943	74950	74958	74966
562	74974	74981	74989	74997	75005	75012	75020	75028	75035	75043
563	75051	75059	75066	75074	75082	75089	75097	75105	75113	75120
564	75128	75136	75143	75151	75159	75166	75174	75182	75189	75197
565	75205	75213	75220	75228	75236	75243	75251	75259	75266	75274
566	75282	75289	75297	75305	75312	75320	75328	75335	75343	75351
567	75358	75366	75374	75381	75389	75397	75404	75412	75420	75427
568	75435	75442	75450	75458	75465	75473	75481	75488	75496	75504
569	75511	75519	75526	75534	75542	75549	75557	75565	75572	75580
570	75587	75595	75603	75610	75618	75626	75633	75641	75648	75656
571	75664	75671	75679	75686	75694	75702	75709	75717	75724	75732
572	75740	75747	75755	75762	75770	75778	75785	75793	75800	75808
573	75815	75823	75831	75838	75846	75853	75861	75868	75876	75884
574	75891	75899	75906	75914	75921	75929	75937	75944	75952	75959
575	75967	75974	75982	75989	75997	76005	76012	76020	76027	76035
576	76042	76050	76057	76065	76072	76080	76087	76095	76103	76110
577	76118	76125	76133	76140	76148	76155	76163	76170	76178	76185
578	76193	76200	76208	76215	76223	76230	76238	76245	76253	76260
579	76268	76275	76283	76290	76298	76305	76313	76320	76328	76335
No.	0	1	2	3	4	5	6	7	8	9

Proportional parts:

	9	8	7
1	1	1	1
2	2	2	1
3	3	2	2
4	4	3	3
5	5	4	4
6	5	5	4
7	6	6	5
8	7	6	6
9	8	7	6

TABLE 42.

Logarithms of Numbers.

No. 5800——6400. Log. 76343——80618.

No.	0	1	2	3	4	5	6	7	8	9
580	76343	76350	76358	76365	76373	76380	76388	76395	76403	76410
581	76418	76425	76433	76440	76448	76455	76462	76470	76477	76485
582	76492	76500	76507	76515	76522	76530	76537	76545	76552	76559
583	76567	76574	76582	76589	76597	76604	76612	76619	76626	76634
584	76641	76649	76656	76664	76671	76678	76686	76693	76701	76708
585	76716	76723	76730	76738	76745	76753	76760	76768	76775	76782
586	76790	76797	76805	76812	76819	76827	76834	76842	76849	76856
587	76864	76871	76879	76886	76893	76901	76908	76916	76923	76930
588	76938	76945	76953	76960	76967	76975	76982	76989	76997	77004
589	77012	77019	77026	77034	77041	77048	77056	77063	77070	77078
590	77085	77093	77100	77107	77115	77122	77129	77137	77144	77151
591	77159	77166	77173	77181	77188	77195	77203	77210	77217	77225
592	77232	77240	77247	77254	77262	77269	77276	77283	77291	77298
593	77305	77313	77320	77327	77335	77342	77349	77357	77364	77371
594	77379	77386	77393	77401	77408	77415	77422	77430	77437	77444
595	77452	77459	77466	77474	77481	77488	77495	77503	77510	77517
596	77525	77532	77539	77546	77554	77561	77568	77576	77583	77590
597	77597	77605	77612	77619	77627	77634	77641	77648	77656	77663
598	77670	77677	77685	77692	77699	77706	77714	77721	77728	77735
599	77743	77750	77757	77764	77772	77779	77786	77793	77801	77808
600	77815	77822	77830	77837	77844	77851	77859	77866	77873	77880
601	77887	77895	77902	77909	77916	77924	77931	77938	77945	77952
602	77960	77967	77974	77981	77988	77996	78003	78010	78017	78025
603	78032	78039	78046	78053	78061	78068	78075	78082	78089	78097
604	78104	78111	78118	78125	78132	78140	78147	78154	78161	78168
605	78176	78183	78190	78197	78204	78211	78219	78226	78233	78240
606	78247	78254	78262	78269	78276	78283	78290	78297	78305	78312
607	78319	78326	78333	78340	78347	78355	78362	78369	78376	78383
608	78390	78398	78405	78412	78419	78426	78433	78440	78447	78455
609	78462	78469	78476	78483	78490	78497	78504	78512	78519	78526
610	78533	78540	78547	78554	78561	78569	78576	78583	78590	78597
611	78604	78611	78618	78625	78633	78640	78647	78654	78661	78668
612	78675	78682	78689	78696	78704	78711	78718	78725	78732	78739
613	78746	78753	78760	78767	78774	78781	78789	78796	78803	78810
614	78817	78824	78831	78838	78845	78852	78859	78866	78873	78880
615	78888	78895	78902	78909	78916	78923	78930	78937	78944	78951
616	78958	78965	78972	78979	78986	78993	79000	79007	79014	79021
617	79029	79036	79043	79050	79057	79064	79071	79078	79085	79092
618	79099	79106	79113	79120	79127	79134	79141	79148	79155	79162
619	79169	79176	79183	79190	79197	79204	79211	79218	79225	79232
620	79239	79246	79253	79260	79267	79274	79281	79288	79295	79302
621	79309	79316	79323	79330	79337	79344	79351	79358	79365	79372
622	79379	79386	79393	79400	79407	79414	79421	79428	79435	79442
623	79449	79456	79463	79470	79477	79484	79491	79498	79505	79511
624	79518	79525	79532	79539	79546	79553	79560	79567	79574	79581
625	79588	79595	79602	79609	79616	79623	79630	79637	79644	79650
626	79657	79664	79671	79678	79685	79692	79699	79706	79713	79720
627	79727	79734	79741	79748	79754	79761	79768	79775	79782	79789
628	79796	79803	79810	79817	79824	79831	79837	79844	79851	79858
629	79865	79872	79879	79886	79893	79900	79906	79913	79920	79927
630	79934	79941	79948	79955	79962	79969	79975	79982	79989	79996
631	80003	80010	80017	80024	80030	80037	80044	80051	80058	80065
632	80072	80079	80085	80092	80099	80106	80113	80120	80127	80134
633	80140	80147	80154	80161	80168	80175	80182	80188	80195	80202
634	80209	80216	80223	80229	80236	80243	80250	80257	80264	80271
635	80277	80284	80291	80298	80305	80312	80318	80325	80332	80339
636	80346	80353	80359	80366	80373	80380	80387	80393	80400	80407
637	80414	80421	80428	80434	80441	80448	80455	80462	80468	80475
638	80482	80489	80496	80502	80509	80516	80523	80530	80536	80543
639	80550	80557	80564	80570	80577	80584	80591	80598	80604	80611
No.	0	1	2	3	4	5	6	7	8	9

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1	1
2	2
3	2
4	3
5	4
6	5
7	6
8	6
9	7

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2	1
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6	4
7	5
8	6
9	6

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1	1
2	1
3	2
4	2
5	3
6	4
7	4
8	5
9	5

TABLE 42.

Logarithms of Numbers.

No. 6400——7000. Log. 80618——84510.

No.	0	1	2	3	4	5	6	7	8	9
640	80618	80625	80632	80638	80645	80652	80659	80665	80672	80679
641	80686	80693	80699	80706	80713	80720	80726	80733	80740	80747
642	80754	80760	80767	80774	80781	80787	80794	80801	80808	80814
643	80821	80828	80835	80841	80848	80855	80862	80868	80875	80882
644	80889	80895	80902	80909	80916	80922	80929	80936	80943	80949
645	80956	80963	80969	80976	80983	80990	80996	81003	81010	81017
646	81023	81030	81037	81043	81050	81057	81064	81070	81077	81084
647	81090	81097	81104	81111	81117	81124	81131	81137	81144	81151
648	81158	81164	81171	81178	81184	81191	81198	81204	81211	81218
649	81224	81231	81238	81245	81251	81258	81265	81271	81278	81285
650	81291	81298	81305	81311	81318	81325	81331	81338	81345	81351
651	81358	81365	81371	81378	81385	81391	81398	81405	81411	81418
652	81425	81431	81438	81445	81451	81458	81465	81471	81478	81485
653	81491	81498	81505	81511	81518	81525	81531	81538	81544	81551
654	81558	81564	81571	81578	81584	81591	81598	81604	81611	81617
655	81624	81631	81637	81644	81651	81657	81664	81671	81677	81684
656	81690	81697	81704	81710	81717	81723	81730	81737	81743	81750
657	81757	81763	81770	81776	81783	81790	81796	81803	81809	81816
658	81823	81829	81836	81842	81849	81856	81862	81869	81875	81882
659	81889	81895	81902	81908	81915	81921	81928	81935	81941	81948
660	81954	81961	81968	81974	81981	81987	81994	82000	82007	82014
661	82020	82027	82033	82040	82046	82053	82060	82066	82073	82079
662	82086	82092	82099	82105	82112	82119	82125	82132	82138	82145
663	82151	82158	82164	82171	82178	82184	82191	82197	82204	82210
664	82217	82223	82230	82236	82243	82249	82256	82263	82269	82276
665	82282	82289	82295	82302	82308	82315	82321	82328	82334	82341
666	82347	82354	82360	82367	82373	82380	82387	82393	82400	82406
667	82413	82419	82426	82432	82439	82445	82452	82458	82465	82471
668	82478	82484	82491	82497	82504	82510	82517	82523	82530	82536
669	82543	82549	82556	82562	82569	82575	82582	82588	82595	82601
670	82607	82614	82620	82627	82633	82640	82646	82653	82659	82666
671	82672	82679	82685	82692	82698	82705	82711	82718	82724	82730
672	82737	82743	82750	82756	82763	82769	82776	82782	82789	82795
673	82802	82808	82814	82821	82827	82834	82840	82847	82853	82860
674	82866	82872	82879	82885	82892	82898	82905	82911	82918	82924
675	82930	82937	82943	82950	82956	82963	82969	82975	82982	82988
676	82995	83001	83008	83014	83020	83027	83033	83040	83046	83052
677	83059	83065	83072	83078	83085	83091	83097	83104	83110	83117
678	83123	83129	83136	83142	83149	83155	83161	83168	83174	83181
679	83187	83193	83200	83206	83213	83219	83225	83232	83238	83245
680	83251	83257	83264	83270	83276	83283	83289	83296	83302	83308
681	83315	83321	83327	83334	83340	83347	83353	83359	83366	83372
682	83378	83385	83391	83398	83404	83410	83417	83423	83429	83436
683	83442	83448	83455	83461	83467	83474	83480	83487	83493	83499
684	83506	83512	83518	83525	83531	83537	83544	83550	83556	83563
685	83569	83575	83582	83588	83594	83601	83607	83613	83620	83626
686	83632	83639	83645	83651	83658	83664	83670	83677	83683	83689
687	83696	83702	83708	83715	83721	83727	83734	83740	83746	83753
688	83759	83765	83771	83778	83784	83790	83797	83803	83809	83816
689	83822	83828	83835	83841	83847	83853	83860	83866	83872	83879
690	83885	83891	83897	83904	83910	83916	83923	83929	83935	83942
691	83948	83954	83960	83967	83973	83979	83985	83992	83998	84004
692	84011	84017	84023	84029	84036	84042	84048	84055	84061	84067
693	84073	84080	84086	84092	84098	84105	84111	84117	84123	84130
694	84136	84142	84148	84155	84161	84167	84173	84180	84186	84192
695	84198	84205	84211	84217	84223	84230	84236	84242	84248	84255
696	84261	84267	84273	84280	84286	84292	84298	84305	84311	84317
697	84323	84330	84336	84342	84348	84354	84361	84367	84373	84379
698	84386	84392	84398	84404	84410	84417	84423	84429	84435	84442
699	84448	84454	84460	84466	84473	84479	84485	84491	84497	84504
No.	0	1	2	3	4	5	6	7	8	9

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1	1
2	1
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TABLE 42.

Logarithms of Numbers.

No. 7000——7600. Log. 84510——88081.

No.	0	1	2	3	4	5	6	7	8	9
700	84510	84516	84522	84528	84535	84541	84547	84553	84559	84566
701	84572	84578	84584	84590	84597	84603	84609	84615	84621	84628
702	84634	84640	84646	84652	84658	84665	84671	84677	84683	84689
703	84696	84702	84708	84714	84720	84726	84733	84739	84745	84751
704	84757	84763	84770	84776	84782	84788	84794	84800	84807	84813
705	84819	84825	84831	84837	84844	84850	84856	84862	84868	84874
706	84880	84887	84893	84899	84905	84911	84917	84924	84930	84936
707	84942	84948	84954	84960	84967	84973	84979	84985	84991	84997
708	85003	85009	85016	85022	85028	85034	85040	85046	85052	85058
709	85065	85071	85077	85083	85089	85095	85101	85107	85114	85120
710	85126	85132	85138	85144	85150	85156	85163	85169	85175	85181
711	85187	85193	85199	85205	85211	85217	85224	85230	85236	85242
712	85248	85254	85260	85266	85272	85278	85285	85291	85297	85303
713	85309	85315	85321	85327	85333	85339	85345	85352	85358	85364
714	85370	85376	85382	85388	85394	85400	85406	85412	85418	85425
715	85431	85437	85443	85449	85455	85461	85467	85473	85479	85485
716	85491	85497	85503	85509	85516	85522	85528	85534	85540	85546
717	85552	85558	85564	85570	85576	85582	85588	85594	85600	85606
718	85612	85618	85625	85631	85637	85643	85649	85655	85661	85667
719	85673	85679	85685	85691	85697	85703	85709	85715	85721	85727
720	85733	85739	85745	85751	85757	85763	85769	85775	85781	85788
721	85794	85800	85806	85812	85818	85824	85830	85836	85842	85848
722	85854	85860	85866	85872	85878	85884	85890	85896	85902	85908
723	85914	85920	85926	85932	85938	85944	85950	85956	85962	85968
724	85974	85980	85986	85992	85998	86004	86010	86016	86022	86028
725	86034	86040	86046	86052	86058	86064	86070	86076	86082	86088
726	86094	86100	86106	86112	86118	86124	86130	86136	86141	86147
727	86153	86159	86165	86171	86177	86183	86189	86195	86201	86207
728	86213	86219	86225	86231	86237	86243	86249	86255	86261	86267
729	86273	86279	86285	86291	86297	86303	86308	86314	86320	86326
730	86332	86338	86344	86350	86356	86362	86368	86374	86380	86386
731	86392	86398	86404	86410	86415	86421	86427	86433	86439	86445
732	86451	86457	86463	86469	86475	86481	86487	86493	86499	86504
733	86510	86516	86522	86528	86534	86540	86546	86552	86558	86564
734	86570	86576	86581	86587	86593	86599	86605	86611	86617	86623
735	86629	86635	86641	86646	86652	86658	86664	86670	86676	86682
736	86688	86694	86700	86705	86711	86717	86723	86729	86735	86741
737	86747	86753	86759	86764	86770	86776	86782	86788	86794	86800
738	86806	86812	86817	86823	86829	86835	86841	86847	86853	86859
739	86864	86870	86876	86882	86888	86894	86900	86906	86911	86917
740	86923	86929	86935	86941	86947	86953	86958	86964	86970	86976
741	86982	86988	86994	86999	87005	87011	87017	87023	87029	87035
742	87040	87046	87052	87058	87064	87070	87075	87081	87087	87093
743	87099	87105	87111	87116	87122	87128	87134	87140	87146	87151
744	87157	87163	87169	87175	87181	87186	87192	87198	87204	87210
745	87216	87221	87227	87233	87239	87245	87251	87256	87262	87268
746	87274	87280	87286	87291	87297	87303	87309	87315	87320	87326
747	87332	87338	87344	87349	87355	87361	87367	87373	87379	87384
748	87390	87396	87402	87408	87413	87419	87425	87431	87437	87442
749	87448	87454	87460	87466	87471	87477	87483	87489	87495	87500
750	87506	87512	87518	87523	87529	87535	87541	87547	87552	87558
751	87564	87570	87576	87581	87587	87593	87599	87604	87610	87616
752	87622	87628	87633	87639	87645	87651	87656	87662	87668	87674
753	87679	87685	87691	87697	87703	87708	87714	87720	87726	87731
754	87737	87743	87749	87754	87760	87766	87772	87777	87783	87789
755	87795	87800	87806	87812	87818	87823	87829	87835	87841	87846
756	87852	87858	87864	87869	87875	87881	87887	87892	87898	87904
757	87910	87915	87921	87927	87933	87938	87944	87950	87955	87961
758	87967	87973	87978	87984	87990	87996	88001	88007	88013	88018
759	88024	88030	88036	88041	88047	88053	88058	88064	88070	88076
No.	0	1	2	3	4	5	6	7	8	9

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1	1
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4	2
5	3
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7	4
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1	1
2	1
3	2
4	2
5	3
6	3
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TABLE 42.

Logarithms of Numbers.

No. 7600——8200. Log. 88081——91381.

No.	0	1	2	3	4	5	6	7	8	9
760	88081	88087	88093	88098	88104	88110	88116	88121	88127	88133
761	88138	88144	88150	88156	88161	88167	88173	88178	88184	88190
762	88195	88201	88207	88213	88218	88224	88230	88235	88241	88247
763	88252	88258	88264	88270	88275	88281	88287	88292	88298	88304
764	88309	88315	88321	88326	88332	88338	88343	88349	88355	88360
765	88366	88372	88377	88383	88389	88395	88400	88406	88412	88417
766	88423	88429	88434	88440	88446	88451	88457	88463	88468	88474
767	88480	88485	88491	88497	88502	88508	88513	88519	88525	88530
768	88536	88542	88547	88553	88559	88564	88570	88576	88581	88587
769	88593	88598	88604	88610	88615	88621	88627	88632	88638	88643
770	88649	88655	88660	88666	88672	88677	88683	88689	88694	88700
771	88705	88711	88717	88722	88728	88734	88739	88745	88750	88756
772	88762	88767	88773	88779	88784	88790	88795	88801	88807	88812
773	88818	88824	88829	88835	88840	88846	88852	88857	88863	88868
774	88874	88880	88885	88891	88897	88902	88908	88913	88919	88925
775	88930	88936	88941	88947	88953	88958	88964	88969	88975	88981
776	88986	88992	88997	89003	89009	89014	89020	89025	89031	89037
777	89042	89048	89053	89059	89064	89070	89076	89081	89087	89092
778	89098	89104	89109	89115	89120	89126	89131	89137	89143	89148
779	89154	89159	89165	89170	89176	89182	89187	89193	89198	89204
780	89209	89215	89221	89226	89232	89237	89243	89248	89254	89260
781	89265	89271	89276	89282	89287	89293	89298	89304	89310	89315
782	89321	89326	89332	89337	89343	89348	89354	89360	89365	89371
783	89376	89382	89387	89393	89398	89404	89409	89415	89421	89426
784	89432	89437	89443	89448	89454	89459	89465	89470	89476	89481
785	89487	89492	89498	89504	89509	89515	89520	89526	89531	89537
786	89542	89548	89553	89559	89564	89570	89575	89581	89586	89592
787	89597	89603	89609	89614	89620	89625	89631	89636	89642	89647
788	89653	89658	89664	89669	89675	89680	89686	89691	89697	89702
789	89708	89713	89719	89724	89730	89735	89741	89746	89752	89757
790	89763	89768	89774	89779	89785	89790	89796	89801	89807	89812
791	89818	89823	89829	89834	89840	89845	89851	89856	89862	89867
792	89873	89878	89883	89889	89894	89900	89905	89911	89916	89922
793	89927	89933	89938	89944	89949	89955	89960	89966	89971	89977
794	89982	89988	89993	89998	90004	90009	90015	90020	90026	90031
795	90037	90042	90048	90053	90059	90064	90069	90075	90080	90086
796	90091	90097	90102	90108	90113	90119	90124	90129	90135	90140
797	90146	90151	90157	90162	90168	90173	90179	90184	90189	90195
798	90200	90206	90211	90217	90222	90227	90233	90238	90244	90249
799	90255	90260	90266	90271	90276	90282	90287	90293	90298	90304
800	90309	90314	90320	90325	90331	90336	90342	90347	90352	90358
801	90363	90369	90374	90380	90385	90390	90396	90401	90407	90412
802	90417	90423	90428	90434	90439	90445	90450	90455	90461	90466
803	90472	90477	90482	90488	90493	90499	90504	90509	90515	90520
804	90526	90531	90536	90542	90547	90553	90558	90563	90569	90574
805	90580	90585	90590	90596	90601	90607	90612	90617	90623	90628
806	90634	90639	90644	90650	90655	90660	90666	90671	90677	90682
807	90687	90693	90698	90703	90709	90714	90720	90725	90730	90736
808	90741	90747	90752	90757	90763	90768	90773	90779	90784	90789
809	90795	90800	90806	90811	90816	90822	90827	90832	90838	90843
810	90849	90854	90859	90865	90870	90875	90881	90886	90891	90897
811	90902	90907	90913	90918	90924	90929	90934	90940	90945	90950
812	90956	90961	90966	90972	90977	90982	90988	90993	90998	91004
813	91009	91014	91020	91025	91030	91036	91041	91046	91052	91057
814	91062	91068	91073	91078	91084	91089	91094	91100	91105	91110
815	91116	91121	91126	91132	91137	91142	91148	91153	91158	91164
816	91169	91174	91180	91185	91190	91196	91201	91206	91212	91217
817	91222	91228	91233	91238	91243	91249	91254	91259	91265	91270
818	91275	91281	91286	91291	91297	91302	91307	91312	91318	91323
819	91328	91334	91339	91344	91350	91355	91360	91365	91371	91376
No.	0	1	2	3	4	5	6	7	8	9

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TABLE 42.

Logarithms of Numbers.

No. 8200——8800. Log. 91381——94448

No.	0	1	2	3	4	5	6	7	8	9
820	91381	91387	91392	91397	91403	91408	91413	91418	91424	91429
821	91434	91440	91445	91450	91455	91461	91466	91471	91477	91482
822	91487	91492	91498	91503	91508	91514	91519	91524	91529	91535
823	91540	91545	91551	91556	91561	91566	91572	91577	91582	91587
824	91593	91598	91603	91609	91614	91619	91624	91630	91635	91640
825	91645	91651	91656	91661	91666	91672	91677	91682	91687	91693
826	91698	91703	91709	91714	91719	91724	91730	91735	91740	91745
827	91751	91756	91761	91766	91772	91777	91782	91787	91793	91798
828	91803	91808	91814	91819	91824	91829	91834	91840	91845	91850
829	91855	91861	91866	91871	91876	91882	91887	91892	91897	91903
830	91908	91913	91918	91924	91929	91934	91939	91944	91950	91955
831	91960	91965	91971	91976	91981	91986	91991	91997	92002	92007
832	92012	92018	92023	92028	92033	92038	92044	92049	92054	92059
833	92065	92070	92075	92080	92085	92091	92096	92101	92106	92111
834	92117	92122	92127	92132	92137	92143	92148	92153	92158	92163
835	92169	92174	92179	92184	92189	92195	92200	92205	92210	92215
836	92221	92226	92231	92236	92241	92247	92252	92257	92262	92267
837	92273	92278	92283	92288	92293	92298	92304	92309	92314	92319
838	92324	92330	92335	92340	92345	92350	92355	92361	92366	92371
839	92376	92381	92387	92392	92397	92402	92407	92412	92418	92423
840	92428	92433	92438	92443	92449	92454	92459	92464	92469	92474
841	92480	92485	92490	92495	92500	92505	92511	92516	92521	92526
842	92531	92536	92542	92547	92552	92557	92562	92567	92572	92578
843	92583	92588	92593	92598	92603	92609	92614	92619	92624	92629
844	92634	92639	92645	92650	92655	92660	92665	92670	92675	92681
845	92686	92691	92696	92701	92706	92711	92716	92722	92727	92732
846	92737	92742	92747	92752	92758	92763	92768	92773	92778	92783
847	92788	92793	92799	92804	92809	92814	92819	92824	92829	92834
848	92840	92845	92850	92855	92860	92865	92870	92875	92881	92886
849	92891	92896	92901	92906	92911	92916	92921	92927	92932	92937
850	92942	92947	92952	92957	92962	92967	92973	92978	92983	92988
851	92993	92998	93003	93008	93013	93018	93024	93029	93034	93039
852	93044	93049	93054	93059	93064	93069	93075	93080	93085	93090
853	93095	93100	93105	93110	93115	93120	93125	93131	93136	93141
854	93146	93151	93156	93161	93166	93171	93176	93181	93186	93192
855	93197	93202	93207	93212	93217	93222	93227	93232	93237	93242
856	93247	93252	93258	93263	93268	93273	93278	93283	93288	93293
857	93298	93303	93308	93313	93318	93323	93328	93334	93339	93344
858	93349	93354	93359	93364	93369	93374	93379	93384	93389	93394
859	93399	93404	93409	93414	93420	93425	93430	93435	93440	93445
860	93450	93455	93460	93465	93470	93475	93480	93485	93490	93495
861	93500	93505	93510	93515	93520	93526	93531	93536	93541	93546
862	93551	93556	93561	93566	93571	93576	93581	93586	93591	93596
863	93601	93606	93611	93616	93621	93626	93631	93636	93641	93646
864	93651	93656	93661	93666	93671	93676	93682	93687	93692	93697
865	93702	93707	93712	93717	93722	93727	93732	93737	93742	93747
866	93752	93757	93762	93767	93772	93777	93782	93787	93792	93797
867	93802	93807	93812	93817	93822	93827	93832	93837	93842	93847
868	93852	93857	93862	93867	93872	93877	93882	93887	93892	93897
869	93902	93907	93912	93917	93922	93927	93932	93937	93942	93947
870	93952	93957	93962	93967	93972	93977	93982	93987	93992	93997
871	94002	94007	94012	94017	94022	94027	94032	94037	94042	94047
872	94052	94057	94062	94067	94072	94077	94082	94086	94091	94096
873	94101	94106	94111	94116	94121	94126	94131	94136	94141	94146
874	94151	94156	94161	94166	94171	94176	94181	94186	94191	94196
875	94201	94206	94211	94216	94221	94226	94231	94236	94240	94245
876	94250	94255	94260	94265	94270	94275	94280	94285	94290	94295
877	94300	94305	94310	94315	94320	94325	94330	94335	94340	94345
878	94349	94354	94359	94364	94369	94374	94379	94384	94389	94394
879	94399	94404	94409	94414	94419	94424	94429	94433	94438	94443
No.	0	1	2	3	4	5	6	7	8	9

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1	1
2	1
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6	4
7	4
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9	5

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2	1
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4	2
5	3
6	3
7	4
8	4
9	5

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1	0
2	1
3	1
4	2
5	2
6	2
7	3
8	3
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TABLE 42.

Logarithms of Numbers.

No. 8800——9400. Log. 94448——97313.

No.	0	1	2	3	4	5	6	7	8	9
880	94448	94453	94458	94463	94468	94473	94478	94483	94488	94493
881	94498	94503	94507	94512	94517	94522	94527	94532	94537	94542
882	94547	94552	94557	94562	94567	94571	94576	94581	94586	94591
883	94596	94601	94606	94611	94616	94621	94626	94630	94635	94640
884	94645	94650	94655	94660	94665	94670	94675	94680	94685	94689
885	94694	94699	94704	94709	94714	94719	94724	94729	94734	94738
886	94743	94748	94753	94758	94763	94768	94773	94778	94783	94787
887	94792	94797	94802	94807	94812	94817	94822	94827	94832	94836
888	94841	94846	94851	94856	94861	94866	94871	94876	94880	94885
889	94890	94895	94900	94905	94910	94915	94919	94924	94929	94934
890	94939	94944	94949	94954	94959	94963	94968	94973	94978	94983
891	94988	94993	94998	95002	95007	95012	95017	95022	95027	95032
892	95036	95041	95046	95051	95056	95061	95066	95071	95075	95080
893	95085	95090	95095	95100	95105	95109	95114	95119	95124	95129
894	95134	95139	95143	95148	95153	95158	95163	95168	95173	95177
895	95182	95187	95192	95197	95202	95207	95211	95216	95221	95226
896	95231	95236	95240	95245	95250	95255	95260	95265	95270	95274
897	95279	95284	95289	95294	95299	95303	95308	95313	95318	95323
898	95328	95332	95337	95342	95347	95352	95357	95361	95366	95371
899	95376	95381	95386	95390	95395	95400	95405	95410	95415	95419
900	95424	95429	95434	95439	95444	95448	95453	95458	95463	95468
901	95472	95477	95482	95487	95492	95497	95501	95506	95511	95516
902	95521	95525	95530	95535	95540	95545	95550	95554	95559	95564
903	95569	95574	95578	95583	95588	95593	95598	95602	95607	95612
904	95617	95622	95626	95631	95636	95641	95646	95650	95655	95660
905	95665	95670	95674	95679	95684	95689	95694	95698	95703	95708
906	95713	95718	95722	95727	95732	95737	95742	95746	95751	95756
907	95761	95766	95770	95775	95780	95785	95789	95794	95799	95804
908	95809	95813	95818	95823	95828	95832	95837	95842	95847	95852
909	95856	95861	95866	95871	95875	95880	95885	95890	95895	95899
910	95904	95909	95914	95918	95923	95928	95933	95938	95942	95947
911	95952	95957	95961	95966	95971	95976	95980	95985	95990	95995
912	95999	96004	96009	96014	96019	96023	96028	96033	96038	96042
913	96047	96052	96057	96061	96066	96071	96076	96080	96085	96090
914	96095	96099	96104	96109	96114	96118	96123	96128	96133	96137
915	96142	96147	96152	96156	96161	96166	96171	96175	96180	96185
916	96190	96194	96199	96204	96209	96213	96218	96223	96227	96232
917	96237	96242	96246	96251	96256	96261	96265	96270	96275	96280
918	96284	96289	96294	96298	96303	96308	96313	96317	96322	96327
919	96332	96336	96341	96346	96350	96355	96360	96365	96369	96374
920	96379	96384	96388	96393	96398	96402	96407	96412	96417	96421
921	96426	96431	96435	96440	96445	96450	96454	96459	96464	96468
922	96473	96478	96483	96487	96492	96497	96501	96506	96511	96515
923	96520	96525	96530	96534	96539	96544	96548	96553	96558	96562
924	96567	96572	96577	96581	96586	96591	96595	96600	96605	96609
925	96614	96619	96624	96628	96633	96638	96642	96647	96652	96656
926	96661	96666	96670	96675	96680	96685	96689	96694	96699	96703
927	96708	96713	96717	96722	96727	96731	96736	96741	96745	96750
928	96755	96759	96764	96769	96774	96778	96783	96788	96792	96797
929	96802	96806	96811	96816	96820	96825	96830	96834	96839	96844
930	96848	96853	96858	96862	96867	96872	96876	96881	96886	96890
931	96895	96900	96904	96909	96914	96918	96923	96928	96932	96937
932	96942	96946	96951	96956	96960	96965	96970	96974	96979	96984
933	96988	96993	96997	97002	97007	97011	97016	97021	97025	97030
934	97035	97039	97044	97049	97053	97058	97063	97067	97072	97077
935	97081	97086	97090	97095	97100	97104	97109	97114	97118	97123
936	97128	97132	97137	97142	97146	97151	97155	97160	97165	97169
937	97174	97179	97183	97188	97192	97197	97202	97206	97211	97216
938	97220	97225	97230	97234	97239	97243	97248	97253	97257	97262
939	97267	97271	97276	97280	97285	97290	97294	97299	97304	97308
No.	0	1	2	3	4	5	6	7	8	9

	5
1	1
2	1
3	2
4	2
5	3
6	3
7	4
8	4
9	5

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1	0
2	1
3	1
4	2
5	2
6	2
7	3
8	3
9	4

TABLE 42.

Logarithms of Numbers.

No. 9400——10000. Log. 97313——99996.

No.	0	1	2	3	4	5	6	7	8	9
940	97313	97317	97322	97327	97331	97336	97340	97345	97350	97354
941	97359	97364	97368	97373	97377	97382	97387	97391	97396	97400
942	97405	97410	97414	97419	97424	97428	97433	97437	97442	97447
943	97451	97456	97460	97465	97470	97474	97479	97483	97488	97493
944	97497	97502	97506	97511	97516	97520	97525	97529	97534	97539
945	97543	97548	97552	97557	97562	97566	97571	97575	97580	97585
946	97589	97594	97598	97603	97607	97612	97617	97621	97626	97630
947	97635	97640	97644	97649	97653	97658	97663	97667	97672	97676
948	97681	97685	97690	97695	97699	97704	97708	97713	97717	97722
949	97727	97731	97736	97740	97745	97749	97754	97759	97763	97768
950	97772	97777	97782	97786	97791	97795	97800	97804	97809	97813
951	97818	97823	97827	97832	97836	97841	97845	97850	97855	97859
952	97864	97868	97873	97877	97882	97886	97891	97896	97900	97905
953	97909	97914	97918	97923	97928	97932	97937	97941	97946	97950
954	97955	97959	97964	97968	97973	97978	97982	97987	97991	97996
955	98000	98005	98009	98014	98019	98023	98028	98032	98037	98041
956	98046	98050	98055	98059	98064	98068	98073	98078	98082	98087
957	98091	98096	98100	98105	98109	98114	98118	98123	98127	98132
958	98137	98141	98146	98150	98155	98159	98164	98168	98173	98177
959	98182	98186	98191	98195	98200	98204	98209	98214	98218	98223
960	98227	98232	98236	98241	98245	98250	98254	98259	98263	98268
961	98272	98277	98281	98286	98290	98295	98299	98304	98308	98313
962	98318	98322	98327	98331	98336	98340	98345	98349	98354	98358
963	98363	98367	98372	98376	98381	98385	98390	98394	98399	98403
964	98408	98412	98417	98421	98426	98430	98435	98439	98444	98448
965	98453	98457	98462	98466	98471	98475	98480	98484	98489	98493
966	98498	98502	98507	98511	98516	98520	98525	98529	98534	98538
967	98543	98547	98552	98556	98561	98565	98570	98574	98579	98583
968	98588	98592	98597	98601	98605	98610	98614	98619	98623	98628
969	98632	98637	98641	98646	98650	98655	98659	98664	98668	98673
970	98677	98682	98686	98691	98695	98700	98704	98709	98713	98717
971	98722	98726	98731	98735	98740	98744	98749	98753	98758	98762
972	98767	98771	98776	98780	98784	98789	98793	98798	98802	98807
973	98811	98816	98820	98825	98829	98834	98838	98843	98847	98851
974	98856	98860	98865	98869	98874	98878	98883	98887	98892	98896
975	98900	98905	98909	98914	98918	98923	98927	98932	98936	98941
976	98945	98949	98954	98958	98963	98967	98972	98976	98981	98985
977	98989	98994	98998	99003	99007	99012	99016	99021	99025	99029
978	99034	99038	99043	99047	99052	99056	99061	99065	99069	99074
979	99078	99083	99087	99092	99096	99100	99105	99109	99114	99118
980	99123	99127	99131	99136	99140	99145	99149	99154	99158	99162
981	99167	99171	99176	99180	99185	99189	99193	99198	99202	99207
982	99211	99216	99220	99224	99229	99233	99238	99242	99247	99251
983	99255	99260	99264	99269	99273	99277	99282	99286	99291	99295
984	99300	99304	99308	99313	99317	99322	99326	99330	99335	99339
985	99344	99348	99352	99357	99361	99366	99370	99374	99379	99383
986	99388	99392	99396	99401	99405	99410	99414	99419	99423	99427
987	99432	99436	99441	99445	99449	99454	99458	99463	99467	99471
988	99476	99480	99484	99489	99493	99498	99502	99506	99511	99515
989	99520	99524	99528	99533	99537	99542	99546	99550	99555	99559
990	99564	99568	99572	99577	99581	99585	99590	99594	99599	99603
991	99607	99612	99616	99621	99625	99629	99634	99638	99642	99647
992	99651	99656	99660	99664	99669	99673	99677	99682	99686	99691
993	99695	99699	99704	99708	99712	99717	99721	99726	99730	99734
994	99739	99743	99747	99752	99756	99760	99765	99769	99774	99778
995	99782	99787	99791	99795	99800	99804	99808	99813	99817	99822
996	99826	99830	99835	99839	99843	99848	99852	99856	99861	99865
997	99870	99874	99878	99883	99887	99891	99896	99900	99904	99909
998	99913	99917	99922	99926	99930	99935	99939	99944	99948	99952
999	99957	99961	99965	99970	99974	99978	99983	99987	99991	99996
No.	0	1	2	3	4	5	6	7	8	9

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1	1
2	1
3	2
4	2
5	3
6	3
7	4
8	4
9	5

	4
1	0
2	1
3	1
4	2
5	2
6	2
7	3
8	3
9	4

TABLE 43.

Logarithmic Sines, Tangents, and Secants to every Point and Quarter Point of the Compass.

Points.	Sine.	Cosine.	Tangent.	Cotangent.	Secant.	Cosecant.	
0	Inf. neg.	10.00000	Inf. neg.	Infinite.	10.00000	Infinite.	8
¼	8.69080	9.99948	8.69132	11.30868	10.00052	11.30920	7¾
½	8.99130	9.99790	8.99340	11.00660	10.00210	11.00870	7½
¾	9.16652	9.99527	9.17125	10.82875	10.00473	10.83348	7¼
1	9.29024	9.99157	9.29866	10.70134	10.00843	10.70976	7
1¼	9.38557	9.98679	9.39879	10.60121	10.01321	10.61443	6¾
1½	9.46282	9.98088	9.48194	10.51806	10.01912	10.53718	6½
1¾	9.52749	9.97384	9.55365	10.44635	10.02616	10.47251	6¼
2	9.58284	9.96562	9.61722	10.38278	10.03438	10.41716	6
2¼	9.63099	9.95616	9.67483	10.32517	10.04384	10.36901	5¾
2½	9.67339	9.94543	9.72796	10.27204	10.05457	10.32661	5½
2¾	9.71105	9.93335	9.77770	10.22230	10.06665	10.28895	5¼
3	9.74474	9.91985	9.82489	10.17511	10.08015	10.25526	5
3¼	9.77503	9.90483	9.87020	10.12980	10.09517	10.22497	4¾
3½	9.80236	9.88819	9.91417	10.08583	10.11181	10.19764	4½
3¾	9.82708	9.86979	9.95729	10.04271	10.13021	10.17292	4¼
4	9.84949	9.84949	10.00000	10.00000	10.15051	10.15051	4
	Cosine.	Sine.	Cotangent.	Tangent.	Cosecant.	Secant.	Points.

TABLE 44.

Log. Sines, Tangents, and Secants.

0° 179°

M.	Hour A. M.	Hour P. M.	Sine.	Diff. 1′.	Cosecant.	Tangent.	Diff. 1′.	Cotangent.	Secant.	Cosine.	M.
0	12 0 0	0 0 0	Inf. neg.		Infinite.	Inf. neg.		Infinite.	10. 00000	10. 00000	60
1	11 59 52	0 8	6. 46373	30103	13. 53627	6. 46373	30103	13. 53627	00000	00000	59
2	59 44	0 16	76476	17609	23524	76476	17609	23524	00000	00000	58
3	59 36	0 24	94085	12494	05915	94085	12494	05915	00000	00000	57
4	59 28	0 32	7. 06579	9691	12. 93421	7. 06579	9691	12. 93421	00000	00000	56
5	11 59 20	0 0 40	7. 16270	7918	12. 83730	7. 16270	7918	12. 83730	10. 00000	10. 00000	55
6	59 12	0 48	24188	6694	75812	24188	6694	75812	00000	00000	54
7	59 4	0 56	30882	5800	69118	30882	5800	69118	00000	00000	53
8	58 56	1 4	36682	5115	63318	36682	5115	63318	00000	00000	52
9	58 48	1 12	41797	4576	58203	41797	4576	58203	00000	00000	51
10	11 58 40	0 1 20	7. 46373	4139	12. 53627	7. 46373	4139	12. 53627	10. 00000	10. 00000	50
11	58 32	1 28	50512	3779	49488	50512	3779	49488	00000	00000	49
12	58 24	1 36	54291	3476	45709	54291	3476	45709	00000	00000	48
13	58 16	1 44	57767	3218	42233	57767	3219	42233	00000	00000	47
14	58 8	1 52	60985	2997	39015	60986	2996	39014	00000	00000	46
15	11 58 0	0 2 0	7. 63982	2802	12. 36018	7. 63982	2803	12. 36018	10. 00000	10. 00000	45
16	57 52	2 8	66784	2633	33216	66785	2633	33215	00000	00000	44
17	57 44	2 16	69417	2483	30583	69418	2482	30582	00001	9. 99999	43
18	57 36	2 24	71900	2348	28100	71900	2348	28100	00001	99999	42
19	57 28	2 32	74248	2227	25752	74248	2228	25752	00001	99999	41
20	11 57 20	0 2 40	7. 76475	2119	12. 23525	7. 76476	2119	12. 23524	10. 00001	9. 99999	40
21	57 12	2 48	78594	2021	21406	78595	2020	21405	00001	99999	39
22	57 4	2 56	80615	1930	19385	80615	1931	19385	00001	99999	38
23	56 56	3 4	82545	1848	17455	82546	1848	17454	00001	99999	37
24	56 48	3 12	84393	1773	15607	84394	1773	15606	00001	99999	36
25	11 56 40	0 3 20	7. 86166	1704	12. 13834	7. 86167	1704	12. 13833	10. 00001	9. 99999	35
26	56 32	3 28	87870	1639	12130	87871	1639	12129	00001	99999	34
27	56 24	3 36	89509	1579	10491	89510	1579	10490	00001	99999	33
28	56 16	3 44	91088	1524	08912	91089	1524	08911	00001	99999	32
29	56 8	3 52	92612	1472	07388	92613	1473	07387	00002	99998	31
30	11 56 0	0 4 0	7. 94084	1424	12. 05916	7. 94086	1424	12. 05914	10. 00002	9. 99998	30
31	55 52	4 8	95508	1379	04492	95510	1379	04490	00002	99998	29
32	55 44	4 16	96887	1336	03113	96889	1336	03111	00002	99998	28
33	55 36	4 24	98223	1297	01777	98225	1297	01775	00002	99998	27
34	55 28	4 32	99520	1259	00480	99522	1259	00478	00002	99998	26
35	11 55 20	0 4 40	8. 00779	1223	11. 99221	8. 00781	1223	11. 99219	10. 00002	9. 99998	25
36	55 12	4 48	02002	1190	97998	02004	1190	97996	00002	99998	24
37	55 4	4 56	03192	1158	96808	03194	1159	96806	00003	99997	23
38	54 56	5 4	04350	1128	95650	04353	1128	95647	00003	99997	22
39	54 48	5 12	05478	1100	94522	05481	1100	94519	00003	99997	21
40	11 54 40	0 5 20	8. 06578	1072	11. 93422	8. 06581	1072	11. 93419	10. 00003	9. 99997	20
41	54 32	5 28	07650	1046	92350	07653	1047	92347	00003	99997	19
42	54 24	5 36	08696	1022	91304	08700	1022	91300	00003	99997	18
43	54 16	5 44	09718	999	90282	09722	998	90278	00003	99997	17
44	54 8	5 52	10717	976	89283	10720	976	89280	00004	99996	16
45	11 54 0	0 6 0	8. 11693	954	11. 88307	8. 11696	955	11. 88304	10. 00004	9. 99996	15
46	53 52	6 8	12647	934	87353	12651	934	87349	00004	99996	14
47	53 44	6 16	13581	914	86419	13585	915	86415	00004	99996	13
48	53 36	6 24	14495	896	85505	14500	895	85500	00004	99996	12
49	53 28	6 32	15391	877	84609	15395	878	84605	00004	99996	11
50	11 53 20	0 6 40	8. 16268	860	11. 83732	8. 16273	860	11. 83727	10. 00005	9. 99995	10
51	53 12	6 48	17128	843	82872	17133	843	82867	00005	99995	9
52	53 4	6 56	17971	827	82029	17976	828	82024	00005	99995	8
53	52 56	7 4	18798	812	81202	18804	812	81196	00005	99995	7
54	52 48	7 12	19610	797	80390	19616	797	80384	00005	99995	6
55	11 52 40	0 7 20	8. 20407	782	11. 79593	8. 20413	782	11. 79587	10. 00006	9. 99994	5
56	52 32	7 28	21189	769	78811	21195	769	78805	00006	99994	4
57	52 24	7 36	21958	755	78042	21964	756	78036	00006	99994	3
58	52 16	7 44	22713	743	77287	22720	742	77280	00006	99994	2
59	52 8	7 52	23456	730	76544	23462	730	76538	00006	99994	1
60	52 0	8 0	24186	717	75814	24192	718	75808	00007	99993	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff. 1′.	Secant.	Cotangent.	Diff. 1′.	Tangent.	Cosecant.	Sine.	M.

90° 89°

TABLE 44.

Log. Sines, Tangents, and Secants.

1° | 178°

M.	Hour A. M.	Hour P. M.	Sine.	Diff. 1′.	Cosecant.	Tangent.	Diff. 1′.	Cotangent.	Secant.	Cosine.	M.
0	11 52 0	0 8 0	8.24186	717	11.75814	8.24192	718	11.75808	10.00007	9.99993	60
1	51 52	8 8	24903	706	75097	24910	706	75090	00007	99993	59
2	51 44	8 16	25609	695	74391	25616	696	74384	00007	99993	58
3	51 36	8 24	26304	684	73696	26312	684	73688	00007	99993	57
4	51 28	8 32	26988	673	73012	26996	673	73004	00008	99992	56
5	11 51 20	0 8 40	8.27661	663	11.72339	8.27669	663	11.72331	10.00008	9.99992	55
6	51 12	8 48	28324	653	71676	28332	654	71668	00008	99992	54
7	51 4	8 56	28977	644	71023	28986	643	71014	00008	99992	53
8	50 56	9 4	29621	634	70379	29629	634	70371	00008	99992	52
9	50 48	9 12	30255	624	69745	30263	625	69737	00009	99991	51
10	11 50 40	0 9 20	8.30879	616	11.69121	8.30888	617	11.69112	10.00009	9.99991	50
11	50 32	9 28	31495	608	68505	31505	607	68495	00009	99991	49
12	50 24	9 36	32103	599	67897	32112	599	67888	00010	99990	48
13	50 16	9 44	32702	590	67298	32711	591	67289	00010	99990	47
14	50 8	9 52	33292	583	66708	33302	584	66698	00010	99990	46
15	11 50 0	0 10 0	8.33875	575	11.66125	8.33886	575	11.66114	10.00010	9.99990	45
16	49 52	10 8	34450	568	65550	34461	568	65539	00011	99989	44
17	49 44	10 16	35018	560	64982	35029	561	64971	00011	99989	43
18	49 36	10 24	35578	553	64422	35590	553	64410	00011	99989	42
19	49 28	10 32	36131	547	63869	36143	546	63857	00011	99989	41
20	11 49 20	0 10 40	8.36678	539	11.63322	8.36689	540	11.63311	10.00012	9.99988	40
21	49 12	10 48	37217	533	62783	37229	533	62771	00012	99988	39
22	49 4	10 56	37750	526	62250	37762	527	62238	00012	99988	38
23	48 56	11 4	38276	520	61724	38289	520	61711	00013	99987	37
24	48 48	11 12	38796	514	61204	38809	514	61191	00013	99987	36
25	11 48 40	0 11 20	8.39310	508	11.60690	8.39323	509	11.60677	10.00013	9.99987	35
26	48 32	11 28	39818	502	60182	39832	502	60168	00014	99986	34
27	48 24	11 36	40320	496	59680	40334	496	59666	00014	99986	33
28	48 16	11 44	40816	491	59184	40830	491	59170	00014	99986	32
29	48 8	11 52	41307	485	58693	41321	486	58679	00015	99985	31
30	11 48 0	0 12 0	8.41792	480	11.58208	8.41807	480	11.58193	10.00015	9.99985	30
31	47 52	12 8	42272	474	57728	42287	475	57713	00015	99985	29
32	47 44	12 16	42746	470	57254	42762	470	57238	00016	99984	28
33	47 36	12 24	43216	464	56784	43232	464	56768	00016	99984	27
34	47 28	12 32	43680	459	56320	43696	460	56304	00016	99984	26
35	11 47 20	0 12 40	8.44139	455	11.55861	8.44156	455	11.55844	10.00017	9.99983	25
36	47 12	12 48	44594	450	55406	44611	450	55389	00017	99983	24
37	47 4	12 56	45044	445	54956	45061	446	54939	00017	99983	23
38	46 56	13 4	45489	441	54511	45507	441	54493	00018	99982	22
39	46 48	13 12	45930	436	54070	45948	437	54052	00018	99982	21
40	11 46 40	0 13 20	8.46366	433	11.53634	8.46385	432	11.53615	10.00018	9.99982	20
41	46 32	13 28	46799	427	53201	46817	428	53183	00019	99981	19
42	46 24	13 36	47226	424	52774	47245	424	52755	00019	99981	18
43	46 16	13 44	47650	419	52350	47669	420	52331	00019	99981	17
44	46 8	13 52	48069	416	51931	48089	416	51911	00020	99980	16
45	11 46 0	0 14 0	8.48485	411	11.51515	8.48505	412	11.51495	10.00020	9.99980	15
46	45 52	14 8	48896	408	51104	48917	408	51083	00021	99979	14
47	45 44	14 16	49304	404	50696	49325	404	50675	00021	99979	13
48	45 36	14 24	49708	400	50292	49729	401	50271	00021	99979	12
49	45 28	14 32	50108	396	49892	50130	397	49870	00022	99978	11
50	11 45 20	0 14 40	8.50504	393	11.49496	8.50527	393	11.49473	10.00022	9.99978	10
51	45 12	14 48	50897	390	49103	50920	390	49080	00023	99977	9
52	45 4	14 56	51287	386	48713	51310	386	48690	00023	99977	8
53	44 56	15 4	51673	382	48327	51696	383	48304	00023	99977	7
54	44 48	15 12	52055	379	47945	52079	380	47921	00024	99976	6
55	11 44 40	0 15 20	8.52434	376	11.47566	8.52459	376	11.47541	10.00024	9.99976	5
56	44 32	15 28	52810	373	47190	52835	373	47165	00025	99975	4
57	44 24	15 36	53183	369	46817	53208	370	46792	00025	99975	3
58	44 16	15 44	53552	367	46448	53578	367	46422	00026	99974	2
59	44 8	15 52	53919	363	46081	53945	363	46055	00026	99974	1
60	44 0	16 0	54282	360	45718	54308	361	45692	00026	99974	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff. 1′.	Secant.	Cotangent.	Diff. 1′.	Tangent.	Cosecant.	Sine.	M.

91° | 88°

6583—06——39

TABLE 44.

Log. Sines, Tangents, and Secants.

2° 177°

M.	Hour A. M.	Hour P. M.	Sine.	Diff. 1′.	Cosecant.	Tangent.	Diff. 1′.	Cotangent.	Secant.	Cosine.	M.
0	11 44 0	0 16 0	8.54282	360	11.45718	8.54308	361	11.45692	10.00026	9.99974	60
1	43 52	16 8	54642	357	45358	54669	358	45331	00027	99973	59
2	43 44	16 16	54999	355	45001	55027	355	44973	00027	99973	58
3	43 36	16 24	55354	351	44646	55382	352	44618	00028	99972	57
4	43 28	16 32	55705	349	44295	55734	349	44266	00028	99972	56
5	11 43 20	0 16 40	8.56054	346	11.43946	8.56083	346	11.43917	10.00029	9.99971	55
6	43 12	16 48	56400	343	43600	56429	344	43571	00029	99971	54
7	43 4	16 56	56743	341	43257	56773	341	43227	00030	99970	53
8	42 56	17 4	57084	337	42916	57114	338	42886	00030	99970	52
9	42 48	17 12	57421	336	42579	57452	336	42548	00031	99969	51
10	11 42 40	0 17 20	8.57757	332	11.42243	8.57788	333	11.42212	10.00031	9.99969	50
11	42 32	17 28	58089	330	41911	58121	330	41879	00032	99968	49
12	42 24	17 36	58419	328	41581	58451	328	41549	00032	99968	48
13	42 16	17 44	58747	325	41253	58779	326	41221	00033	99967	47
14	42 8	17 52	59072	323	40928	59105	323	40895	00033	99967	46
15	11 42 0	0 18 0	8.59395	320	11.40605	8.59428	321	11.40572	10.00033	9.99967	45
16	41 52	18 8	59715	318	40285	59749	319	40251	00034	99966	44
17	41 44	18 16	60033	316	39967	60068	316	39932	00034	99966	43
18	41 36	18 24	60349	313	39651	60384	314	39616	00035	99965	42
19	41 28	18 32	60662	311	39338	60698	311	39302	00036	99964	41
20	11 41 20	0 18 40	8.60973	309	11.39027	8.61009	310	11.38991	10.00036	9.99964	40
21	41 12	18 48	61282	307	38718	61319	307	38681	00037	99963	39
22	41 4	18 56	61589	305	38411	61626	305	38374	00037	99963	38
23	40 56	19 4	61894	302	38106	61931	303	38069	00038	99962	37
24	40 48	19 12	62196	301	37804	62234	301	37766	00038	99962	36
25	11 40 40	0 19 20	8.62497	298	11.37503	8.62535	299	11.37465	10.00039	9.99961	35
26	40 32	19 28	62795	296	37205	62834	297	37166	00039	99961	34
27	40 24	19 36	63091	294	36909	63131	295	36869	00040	99960	33
28	40 16	19 44	63385	293	36615	63426	292	36574	00040	99960	32
29	40 8	19 52	63678	290	36322	63718	291	36282	00041	99959	31
30	11 40 0	0 20 0	8.63968	288	11.36032	8.64009	289	11.35991	10.00041	9.99959	30
31	39 52	20 8	64256	287	35744	64298	287	35702	00042	99958	29
32	39 44	20 16	64543	284	35457	64585	285	35415	00042	99958	28
33	39 36	20 24	64827	283	35173	64870	284	35130	00043	99957	27
34	39 28	20 32	65110	281	34890	65154	281	34846	00044	99956	26
35	11 39 20	0 20 40	8.65391	279	11.34609	8.65435	280	11.34565	10.00044	9.99956	25
36	39 12	20 48	65670	277	34330	65715	278	34285	00045	99955	24
37	39 4	20 56	65947	276	34053	65993	276	34007	00045	99955	23
38	38 56	21 4	66223	274	33777	66269	274	33731	00046	99954	22
39	38 48	21 12	66497	272	33503	66543	273	33457	00046	99954	21
40	11 38 40	0 21 20	8.66769	270	11.33231	8.66816	271	11.33184	10.00047	9.99953	20
41	38 32	21 28	67039	269	32961	67087	269	32913	00048	99952	19
42	38 24	21 36	67308	267	32692	67356	268	32644	00048	99952	18
43	38 16	21 44	67575	266	32425	67624	266	32376	00049	99951	17
44	38 8	21 52	67841	263	32159	67890	264	32110	00049	99951	16
45	11 38 0	0 22 0	8.68104	263	11.31896	8.68154	263	11.31846	10.00050	9.99950	15
46	37 52	22 8	68367	260	31633	68417	261	31583	00051	99949	14
47	37 44	22 16	68627	259	31373	68678	260	31322	00051	99949	13
48	37 36	22 24	68886	258	31114	68938	258	31062	00052	99948	12
49	37 28	22 32	69144	256	30856	69196	257	30804	00052	99948	11
50	11 37 20	0 22 40	8.69400	254	11.30600	8.69453	255	11.30547	10.00053	9.99947	10
51	37 12	22 48	69654	253	30346	69708	254	30292	00054	99946	9
52	37 4	22 56	69907	252	30093	69962	252	30038	00054	99946	8
53	36 56	23 4	70159	250	29841	70214	251	29786	00055	99945	7
54	36 48	23 12	70409	249	29591	70465	249	29535	00056	99944	6
55	11 36 40	0 23 20	8.70658	247	11.29342	8.70714	248	11.29286	10.00056	9.99944	5
56	36 32	23 28	70905	246	29095	70962	246	29038	00057	99943	4
57	36 24	23 36	71151	244	28849	71208	245	28792	00058	99942	3
58	36 16	23 44	71395	243	28605	71453	244	28547	00058	99942	2
59	36 8	23 52	71638	242	28362	71697	243	28303	00059	99941	1
60	36 0	24 0	71880	240	28120	71940	241	28060	00060	99940	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff. 1′.	Secant.	Cotangent.	Diff. 1′.	Tangent.	Cosecant.	Sine.	M.

92° 87°

TABLE 44.

Log. Sines, Tangents, and Secants.

3° | 176°

M.	Hour A. M.	Hour P. M.	Sine.	Diff. 1′.	Cosecant.	Tangent.	Diff. 1′.	Cotangent.	Secant.	Cosine.	M.
0	11 36 0	0 24 0	8. 71880	240	11. 28120	8. 71940	241	11. 28060	10. 00060	9. 99940	60
1	35 52	24 8	72120	239	27880	72181	239	27819	00060	99940	59
2	35 44	24 16	72359	238	27641	72420	239	27580	00061	99939	58
3	35 36	24 24	72597	237	27403	72659	237	27341	00062	99938	57
4	35 28	24 32	72834	235	27166	72896	236	27104	00062	99938	56
5	11 35 20	0 24 40	8. 73069	234	11. 26931	8. 73132	234	11. 26868	10. 00063	9. 99937	55
6	35 12	24 48	73303	232	26697	73366	234	26634	00064	99936	54
7	35 4	24 56	73535	232	26465	73600	232	26400	00064	99936	53
8	34 56	25 4	73767	230	26233	73832	231	26168	00065	99935	52
9	34 48	25 12	73997	229	26003	74063	229	25937	00066	99934	51
10	11 34 40	0 25 20	8. 74226	228	11. 25774	8. 74292	229	11. 25708	10. 00066	9. 99934	50
11	34 32	25 28	74454	226	25546	74521	227	25479	00067	99933	49
12	34 24	25 36	74680	226	25320	74748	226	25252	00068	99932	48
13	34 16	25 44	74906	224	25094	74974	225	25026	00068	99932	47
14	34 8	25 52	75130	223	24870	75199	224	24801	00069	99931	46
15	11 34 0	0 26 0	8. 75353	222	11. 24647	8. 75423	222	11. 24577	10. 00070	9. 99930	45
16	33 52	26 8	75575	220	24425	75645	222	24355	00071	99929	44
17	33 44	26 16	75795	220	24205	75867	220	24133	00071	99929	43
18	33 36	26 24	76015	219	23985	76087	219	23913	00072	99928	42
19	33 28	26 32	76234	217	23766	76306	219	23694	00073	99927	41
20	11 33 20	0 26 40	8. 76451	216	11. 23549	8. 76525	217	11. 23475	10. 00074	9. 99926	40
21	33 12	26 48	76667	216	23333	76742	216	23258	00074	99926	39
22	33 4	26 56	76883	214	23117	76958	215	23042	00075	99925	38
23	32 56	27 4	77097	213	22903	77173	214	22827	00076	99924	37
24	32 48	27 12	77310	212	22690	77387	213	22613	00077	99923	36
25	11 32 40	0 27 20	8. 77522	211	11. 22478	8. 77600	211	11. 22400	10. 00077	9. 99923	35
26	32 32	27 28	77733	210	22267	77811	211	22189	00078	99922	34
27	32 24	27 36	77943	209	22057	78022	210	21978	00079	99921	33
28	32 16	27 44	78152	208	21848	78232	209	21768	00080	99920	32
29	32 8	27 52	78360	208	21640	78441	208	21559	00080	99920	31
30	11 32 0	0 28 0	8. 78568	206	11. 21432	8. 78649	206	11. 21351	10. 00081	9. 99919	30
31	31 52	28 8	78774	205	21226	78855	206	21145	00082	99918	29
32	31 44	28 16	78979	204	21021	79061	205	20939	00083	99917	28
33	31 36	28 24	79183	203	20817	79266	204	20734	00083	99917	27
34	31 28	28 32	79386	202	20614	79470	203	20530	00084	99916	26
35	11 31 20	0 28 40	8. 79588	201	11. 20412	8. 79673	202	11. 20327	10. 00085	9. 99915	25
36	31 12	28 48	79789	201	20211	79875	201	20125	00086	99914	24
37	31 4	28 56	79990	199	20010	80076	201	19924	00087	99913	23
38	30 56	29 4	80189	199	19811	80277	199	19723	00087	99913	22
39	30 48	29 12	80388	197	19612	80476	198	19524	00088	99912	21
40	11 30 40	0 29 20	8. 80585	197	11. 19415	8. 80674	198	11. 19326	10. 00089	9. 99911	20
41	30 32	29 28	80782	196	19218	80872	196	19128	00090	99910	19
42	30 24	29 36	80978	195	19022	81068	196	18932	00091	99909	18
43	30 16	29 44	81173	194	18827	81264	195	18736	00091	99909	17
44	30 8	29 52	81367	193	18633	81459	194	18541	00092	99908	16
45	11 30 0	0 30 0	8. 81560	192	11. 18440	8. 81653	193	11. 18347	10. 00093	9. 99907	15
46	29 52	30 8	81752	192	18248	81846	192	18154	00094	99906	14
47	29 44	30 16	81944	190	18056	82038	192	17962	00095	99905	13
48	29 36	30 24	82134	190	17866	82230	190	17770	00096	99904	12
49	29 28	30 32	82324	189	17676	82420	190	17580	00096	99904	11
50	11 29 20	0 30 40	8. 82513	188	11. 17487	8. 82610	189	11. 17390	10. 00097	9. 99903	10
51	29 12	30 48	82701	187	17299	82799	188	17201	00098	99902	9
52	29 4	30 56	82888	187	17112	82987	188	17013	00099	99901	8
53	28 56	31 4	83075	186	16925	83175	186	16825	00100	99900	7
54	28 48	31 12	83261	185	16739	83361	186	16639	00101	99899	6
55	11 28 40	0 31 20	8. 83446	184	11. 16554	8. 83547	185	11. 16453	10. 00102	9. 99898	5
56	28 32	31 28	83630	183	16370	83732	184	16268	00102	99898	4
57	28 24	31 36	83813	183	16187	83916	184	16084	00103	99897	3
58	28 16	31 44	83996	181	16004	84100	182	15900	00104	99896	2
59	28 8	31 52	84177	181	15823	84282	182	15718	00105	99895	1
60	28 0	32 0	84358	181	15642	84464	182	15536	00106	99894	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff. 1′.	Secant.	Cotangent.	Diff. 1′.	Tangent.	Cosecant.	Sine	M.

93° | 86°

TABLE 44.

Log. Sines, Tangents, and Secants.

4° | 175°

M.	Hour A. M.	Hour P. M.	Sine.	Diff. 1′.	Cosecant.	Tangent.	Diff. 1′.	Cotangent.	Secant.	Cosine.	M.
0	11 28 0	0 32 0	8. 84358	181	11. 15642	8. 84464	182	11. 15536	10. 00106	9. 99894	60
1	27 52	32 8	84539	179	15461	84646	180	15354	00107	99893	59
2	27 44	32 16	84718	179	15282	84826	180	15174	00108	99892	58
3	27 36	32 24	84897	178	15103	85006	179	14994	00109	99891	57
4	27 28	32 32	85075	177	14925	85185	178	14815	00109	99891	56
5	11 27 20	0 32 40	8. 85252	177	11. 14748	8. 85363	177	11. 14637	10. 00110	9. 99890	55
6	27 12	32 48	85429	176	14571	85540	177	14460	00111	99889	54
7	27 4	32 56	85605	175	14395	85717	176	14283	00112	99888	53
8	26 56	33 4	85780	175	14220	85893	176	14107	00113	99887	52
9	26 48	33 12	85955	173	14045	86069	174	13931	00114	99886	51
10	11 26 40	0 33 20	8. 86128	173	11. 13872	8. 86243	174	11. 13757	10. 00115	9. 99885	50
11	26 32	33 28	86301	173	13699	86417	174	13583	00116	99884	49
12	26 24	33 36	86474	171	13526	86591	172	13409	00117	99883	48
13	26 16	33 44	86645	171	13355	86763	172	13237	00118	99882	47
14	26 8	33 52	86816	171	13184	86935	171	13065	00119	99881	46
15	11 26 0	0 34 0	8. 86987	169	11. 13013	8. 87106	171	11. 12894	10. 00120	9. 99880	45
16	25 52	34 8	87156	169	12844	87277	170	12723	00121	99879	44
17	25 44	34 16	87325	169	12675	87447	169	12553	00121	99879	43
18	25 36	34 24	87494	167	12506	87616	169	12384	00122	99878	42
19	25 28	34 32	87661	168	12339	87785	168	12215	00123	99877	41
20	11 25 20	0 34 40	8. 87829	166	11. 12171	8. 87953	167	11. 12047	10. 00124	9. 99876	40
21	25 12	34 48	87995	166	12005	88120	167	11880	00125	99875	39
22	25 4	34 56	88161	165	11839	88287	166	11713	00126	99874	38
23	24 56	35 4	88326	164	11674	88453	165	11547	00127	99873	37
24	24 48	35 12	88490	164	11510	88618	165	11382	00128	99872	36
25	11 24 40	0 35 20	8. 88654	163	11. 11346	8. 88783	165	11. 11217	10. 00129	9. 99871	35
26	24 32	35 28	88817	163	11183	88948	163	11052	00130	99870	34
27	24 24	35 36	88980	162	11020	89111	163	10889	00131	99869	33
28	24 16	35 44	89142	162	10858	89274	163	10726	00132	99868	32
29	24 8	35 52	89304	160	10696	89437	161	10563	00133	99867	31
30	11 24 0	0 36 0	8. 89464	161	11. 10536	8. 89598	162	11. 10402	10. 00134	9. 99866	30
31	23 52	36 8	89625	159	10375	89760	160	10240	00135	99865	29
32	23 44	36 16	89784	159	10216	89920	160	10080	00136	99864	28
33	23 36	36 24	89943	159	10057	90080	160	09920	00137	99863	27
34	23 28	36 32	90102	158	09898	90240	159	09760	00138	99862	26
35	11 23 20	0 36 40	8. 90260	157	11. 09740	8. 90399	158	11. 09601	10. 00139	9. 99861	25
36	23 12	36 48	90417	157	09583	90557	158	09443	00140	99860	24
37	23 4	36 56	90574	156	09426	90715	157	09285	00141	99859	23
38	22 56	37 4	90730	155	09270	90872	157	09128	00142	99858	22
39	22 48	37 12	90885	155	09115	91029	156	08971	00143	99857	21
40	11 22 40	0 37 20	8. 91040	155	11. 08960	8. 91185	155	11. 08815	10. 00144	9. 99856	20
41	22 32	37 28	91195	154	08805	91340	155	08660	00145	99855	19
42	22 24	37 36	91349	153	08651	91495	155	08505	00146	99854	18
43	22 16	37 44	91502	153	08498	91650	153	08350	00147	99853	17
44	22 8	37 52	91655	152	08345	91803	154	08197	00148	99852	16
45	11 22 0	0 38 0	8. 91807	152	11. 08193	8. 91957	153	11. 08043	10. 00149	9. 99851	15
46	21 52	38 8	91959	151	08041	92110	152	07890	00150	99850	14
47	21 44	38 16	92110	151	07890	92262	152	07738	00152	99848	13
48	21 36	38 24	92261	150	07739	92414	151	07586	00153	99847	12
49	21 28	38 32	92411	150	07589	92565	151	07435	00154	99846	11
50	11 21 20	0 38 40	8. 92561	149	11. 07439	8. 92716	150	11. 07284	10. 00155	9. 99845	10
51	21 12	38 48	92710	149	07290	92866	150	07134	00156	99844	9
52	21 4	38 56	92859	148	07141	93016	149	06984	00157	99843	8
53	20 56	39 4	93007	147	06993	93165	148	06835	00158	99842	7
54	20 48	39 12	93154	147	06846	93313	149	06687	00159	99841	6
55	11 20 40	0 39 20	8. 93301	147	11. 06699	8. 93462	147	11. 06538	10. 00160	9. 99840	5
56	20 32	39 28	93448	146	06552	93609	147	06391	00161	99839	4
57	20 24	39 36	93594	146	06406	93756	147	06244	00162	99838	3
58	20 16	39 44	93740	145	06260	93903	146	06097	00163	99837	2
59	20 8	39 52	93885	145	06115	94049	146	05951	00164	99836	1
60	20 0	40 0	94030	144	05970	94195	145	05805	00166	99834	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff. 1′.	Secant.	Cotangent.	Diff. 1′.	Tangent.	Cosecant.	Sine.	M.

94° | 85°

TABLE 44.

Log. Sines, Tangents, and Secants.

5° | A | A | B | B | C | C | 174°

M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
			A		A	B		B	C		C	
0	11 20 00	0 40 00	8.94030	0	11.05970	8.94195	0	11.05805	10.00166	0	9.99834	60
1	19 52	40 08	94174	2	05826	94340	2	05660	00167	0	99833	59
2	19 44	40 16	94317	4	05683	94485	4	05515	00168	0	99832	58
3	19 36	40 24	94461	7	05539	94630	7	05370	00169	0	99831	57
4	19 28	40 32	94603	9	05397	94773	9	05227	00170	0	99830	56
5	11 19 20	0 40 40	8.94746	11	11.05254	8.94917	11	11.05083	10.00171	0	9.99829	55
6	19 12	40 48	94887	13	05113	95060	13	04940	00172	0	99828	54
7	19 04	40 56	95029	15	04971	95202	15	04798	00173	0	99827	53
8	18 56	41 04	95170	18	04830	95344	18	04656	00175	0	99825	52
9	18 48	41 12	95310	20	04690	95486	20	04514	00176	0	99824	51
10	11 18 40	0 41 20	8.95450	22	11.04550	8.95627	22	11.04373	10.00177	0	9.99823	50
11	18 32	41 28	95589	24	04411	95767	24	04233	00178	0	99822	49
12	18 24	41 36	95728	26	04272	95908	27	04092	00179	0	99821	48
13	18 16	41 44	95867	29	04133	96047	29	03953	00180	0	99820	47
14	18 08	41 52	96005	31	03995	96187	31	03813	00181	0	99819	46
15	11 18 00	0 42 00	8.96143	33	11.03857	8.96325	33	11.03675	10.00183	0	9.99817	45
16	17 52	42 08	96280	35	03720	96464	35	03536	00184	0	99816	44
17	17 44	42 16	96417	37	03583	96602	38	03398	00185	0	99815	43
18	17 36	42 24	96553	39	03447	96739	40	03261	00186	0	99814	42
19	17 28	42 32	96689	42	03311	96877	42	03123	00187	0	99813	41
20	11 17 20	0 42 40	8.96825	44	11.03175	8.97013	44	11.02987	10.00188	0	9.99812	40
21	17 12	42 48	96960	46	03040	97150	46	02850	00190	0	99810	39
22	17 04	42 56	97095	48	02905	97285	49	02715	00191	0	99809	38
23	16 56	43 04	97229	50	02771	97421	51	02579	00192	0	99808	37
24	16 48	43 12	97363	53	02637	97556	53	02444	00193	0	99807	36
25	11 16 40	0 43 20	8.97496	55	11.02504	8.97691	55	11.02309	10.00194	1	9.99806	35
26	16 32	43 28	97629	57	02371	97825	58	02175	00196	1	99804	34
27	16 24	43 36	97762	59	02238	97959	60	02041	00197	1	99803	33
28	16 16	43 44	97894	61	02106	98092	62	01908	00198	1	99802	32
29	16 08	43 52	98026	64	01974	98225	64	01775	00199	1	99801	31
30	11 16 00	0 44 00	8.98157	66	11.01843	8.98358	66	11.01642	10.00200	1	9.99800	30
31	15 52	44 08	98288	68	01712	98490	69	01510	00202	1	99798	29
32	15 44	44 16	98419	70	01581	98622	71	01378	00203	1	99797	28
33	15 36	44 24	98549	72	01451	98753	73	01247	00204	1	99796	27
34	15 28	44 32	98679	75	01321	98884	75	01116	00205	1	99795	26
35	11 15 20	0 44 40	8.98808	77	11.01192	8.99015	77	11.00985	10.00207	1	9.99793	25
36	15 12	44 48	98937	79	01063	99145	80	00855	00208	1	99792	24
37	15 04	44 56	99066	81	00934	99275	82	00725	00209	1	99791	23
38	14 56	45 04	99194	83	00806	99405	84	00595	00210	1	99790	22
39	14 48	45 12	99322	86	00678	99534	86	00466	00212	1	99788	21
40	11 14 40	0 45 20	8.99450	88	11.00550	8.99662	89	11.00338	10.00213	1	9.99787	20
41	14 32	45 28	99577	90	00423	99791	91	00209	00214	1	99786	19
42	14 24	45 36	99704	92	00296	99919	93	00081	00215	1	99785	18
43	14 16	45 44	99830	94	00170	9.00046	95	10.99954	00217	1	99783	17
44	14 08	45 52	99956	96	00044	00174	97	99826	00218	1	99782	16
45	11 14 00	0 46 00	9.00082	99	10.99918	9.00301	100	10.99699	10.00219	1	9.99781	15
46	13 52	46 08	00207	101	99793	00427	102	99573	00220	1	99780	14
47	13 44	46 16	00332	103	99668	00553	104	99447	00222	1	99778	13
48	13 36	46 24	00456	105	99544	00679	106	99321	00223	1	99777	12
49	13 28	46 32	00581	107	99419	00805	108	99195	00224	1	99776	11
50	11 13 20	0 46 40	9.00704	110	10.99296	9.00930	111	10.99070	10.00225	1	9.99775	10
51	13 12	46 48	00828	112	99172	01055	113	98945	00227	1	99773	9
52	13 04	46 56	00951	114	99049	01179	115	98821	00228	1	99772	8
53	12 56	47 04	01074	116	98926	01303	117	98697	00229	1	99771	7
54	12 48	47 12	01196	118	98804	01427	120	98573	00231	1	99769	6
55	11 12 40	0 47 20	9.01318	121	10.98682	9.01550	122	10.98450	10.00232	1	99768	5
56	12 32	47 28	01440	123	98560	01673	124	98327	00233	1	99767	4
57	12 24	47 36	01561	125	98439	01796	126	98204	00235	1	99765	3
58	12 16	47 44	01682	127	98318	01918	128	98082	00236	1	99764	2
59	12 08	47 52	01803	129	98197	02040	131	97960	00237	1	99763	1
60	12 00	48 00	01923	132	98077	02162	133	97838	00239	1	99761	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
			A		A	B		B	C		C	

95° | 84°

Seconds of time	1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols. A	16	33	49	66	82	99	115
Prop. parts of cols. B	17	33	50	66	83	100	116
Prop. parts of cols. C	0	0	0	1	1	1	1

TABLE 44.

Log. Sines, Tangents, and Secants.

6°			A		A	B		B	C		C	173°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	11 12 00	0 48 00	9.01923	0	10.98077	9.02162	0	10.97838	10.00239	0	9.99761	60
1	11 52	48 08	02043	2	97957	02283	2	97717	00240	0	99760	59
2	11 44	48 16	02163	4	97837	02404	4	97596	00241	0	99759	58
3	11 36	48 24	02283	6	97717	02525	6	97475	00243	0	99757	57
4	11 28	48 32	02402	7	97598	02645	8	97355	00244	0	99756	56
5	11 11 20	0 48 40	9.02520	9	10.97480	9.02766	9	10.97234	10.00245	0	9.99755	55
6	11 12	48 48	02639	11	97361	02885	11	97115	00247	0	99753	54
7	11 04	48 56	02757	13	97243	03005	13	96995	00248	0	99752	53
8	10 56	49 04	02874	15	97126	03124	15	96876	00249	0	99751	52
9	10 48	49 12	02992	17	97008	03242	17	96758	00251	0	99749	51
10	11 10 40	0 49 20	9.03109	19	10.96891	9.03361	19	10.96639	10.00252	0	9.99748	50
11	10 32	49 28	03226	20	96774	03479	21	96521	00253	0	99747	49
12	10 24	49 36	03342	22	96658	03597	23	96403	00255	0	99745	48
13	10 16	49 44	03458	24	96542	03714	24	96286	00256	0	99744	47
14	10 08	49 52	03574	26	96426	03832	26	96168	00258	0	99742	46
15	11 10 00	0 50 00	9.03690	28	10.96310	9.03948	28	10.96052	10.00259	0	9.99741	45
16	9 52	50 08	03805	30	96195	04065	30	95935	00260	0	99740	44
17	9 44	50 16	03920	31	96080	04181	32	95819	00262	0	99738	43
18	9 36	50 24	04034	33	95966	04297	34	95703	00263	0	99737	42
19	9 28	50 32	04149	35	95851	04413	36	95587	00264	0	99736	41
20	11 9 20	0 50 40	9.04262	37	10.95738	9.04528	38	10.95472	10.00266	0	9.99734	40
21	9 12	50 48	04376	39	95624	04643	39	95357	00267	1	99733	39
22	9 04	50 56	04490	41	95510	04758	41	95242	00269	1	99731	38
23	8 56	51 04	04603	43	95397	04873	43	95127	00270	1	99730	37
24	8 48	51 12	04715	44	95285	04987	45	95013	00272	1	99728	36
25	11 8 40	0 51 20	9.04828	46	10.95172	9.05101	47	10.94899	10.00273	1	9.99727	35
26	8 32	51 28	04940	48	95060	05214	49	94786	00274	1	99726	34
27	8 24	51 36	05052	50	94948	05328	51	94672	00276	1	99724	33
28	8 16	51 44	05164	52	94836	05441	53	94559	00277	1	99723	32
29	8 08	51 52	05275	54	94725	05553	54	94447	00279	1	99721	31
30	11 8 00	0 52 00	9.05386	56	10.94614	9.05666	56	10.94334	10.00280	1	9.99720	30
31	7 52	52 08	05497	57	94503	05778	58	94222	00282	1	99718	29
32	7 44	52 16	05607	59	94393	05890	60	94110	00283	1	99717	28
33	7 36	52 24	05717	61	94283	06002	62	93998	00284	1	99716	27
34	7 28	52 32	05827	63	94173	06113	64	93887	00286	1	99714	26
35	11 7 20	0 52 40	9.05937	65	10.94063	9.06224	66	10.93776	10.00287	1	9.99713	25
36	7 12	52 48	06046	67	93954	06335	68	93665	00289	1	99711	24
37	7 04	52 56	06155	69	93845	06445	69	93555	00290	1	99710	23
38	6 56	53 04	06264	70	93736	06556	71	93444	00292	1	99708	22
39	6 48	53 12	06372	72	93628	06666	73	93334	00293	1	99707	21
40	11 6 40	0 53 20	9.06481	74	10.93519	9.06775	75	10.93225	10.00295	1	9.99705	20
41	6 32	53 28	06589	76	93411	06885	77	93115	00296	1	99704	19
42	6 24	53 36	06696	78	93304	06994	79	93006	00298	1	99702	18
43	6 16	53 44	06804	80	93196	07103	81	92897	00299	1	99701	17
44	6 08	53 52	06911	81	93089	07211	83	92789	00301	1	99699	16
45	11 6 00	0 54 00	9.07018	83	10.92982	9.07320	84	10.92680	10.00302	1	9.99698	15
46	5 52	54 08	07124	85	92876	07428	86	92572	00304	1	99696	14
47	5 44	54 16	07231	87	92769	07536	88	92464	00305	1	99695	13
48	5 36	54 24	07337	89	92663	07643	90	92357	00307	1	99693	12
49	5 28	54 32	07442	91	92558	07751	92	92249	00308	1	99692	11
50	11 5 20	0 54 40	9.07548	93	10.92452	9.07858	94	10.92142	10.00310	1	9.99690	10
51	5 12	54 48	07653	94	92347	07964	96	92036	00311	1	99689	9
52	5 04	54 56	07758	96	92242	08071	98	91929	00313	1	99687	8
53	4 56	55 04	07863	98	92137	08177	99	91823	00314	1	99686	7
54	4 48	55 12	07968	100	92032	08283	101	91717	00316	1	99684	6
55	11 4 40	0 55 20	9.08072	102	10.91928	9.08389	103	10.91611	10.00317	1	9.99683	5
56	4 32	55 28	08176	104	91824	08495	105	91505	00319	1	99681	4
57	4 24	55 36	08280	106	91720	08600	107	91400	00320	1	99680	3
58	4 16	55 44	08383	107	91617	08705	109	91295	00322	1	99678	2
59	4 08	55 52	08486	109	91514	08810	111	91190	00323	1	99677	1
60	4 00	56 00	08589	111	91411	08914	113	91086	00325	1	99675	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
96°			A		A	B		B	C		C	83°

Seconds of time		1^s	2^s	3^s	4^s	5^s	6^s	7^s
Prop. parts of cols.	A	14	28	42	56	69	83	97
	B	14	28	42	56	70	84	98
	C	0	0	1	1	1	1	1

TABLE 44.

Log. Sines, Tangents, and Secants.

7°			A		A	B		B	C		C	172°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	11 4 0	0 56 0	9.08589	0	10.91411	9.08914	0	10.91086	10.00325	0	9.99675	60
1	3 52	56 8	08692	2	91308	09019	2	90981	00326	0	99674	59
2	3 44	56 16	08795	3	91205	09123	3	90877	00328	0	99672	58
3	3 36	56 24	08897	5	91103	09227	5	90773	00330	0	99670	57
4	3 28	56 32	08999	6	91001	09330	7	90670	00331	0	99669	56
5	11 3 20	0 56 40	9.09101	8	10.90899	9.09434	8	10.90566	10.00333	0	9.99667	55
6	3 12	56 48	09202	10	90798	09537	10	90463	00334	0	99666	54
7	3 4	56 56	09304	11	90696	09640	11	90360	00336	0	99664	53
8	2 56	57 4	09405	13	90595	09742	13	90258	00337	0	99663	52
9	2 48	57 12	09506	14	90494	09845	15	90155	00339	0	99661	51
10	11 2 40	0 57 20	9.09606	16	10.90394	9.09947	16	10.90053	10.00341	0	9.99659	50
11	2 32	57 28	09707	18	90293	10049	18	89951	00342	0	99658	49
12	2 24	57 36	09807	19	90193	10150	20	89850	00344	0	99656	48
13	2 16	57 44	09907	21	90093	10252	21	89748	00345	0	99655	47
14	2 8	57 52	10006	22	89994	10353	23	89647	00347	0	99653	46
15	11 2 0	0 58 0	9.10106	24	10.89894	9.10454	24	10.89546	10.00349	0	9.99651	45
16	1 52	58 8	10205	26	89795	10555	26	89445	00350	0	99650	44
17	1 44	58 16	10304	27	89696	10656	28	89344	00352	0	99648	43
18	1 36	58 24	10402	29	89598	10756	29	89244	00353	1	99647	42
19	1 28	58 32	10501	30	89499	10856	31	89144	00355	1	99645	41
20	11 1 20	0 58 40	9.10599	32	10.89401	9.10956	33	10.89044	10.00357	1	9.99643	40
21	1 12	58 48	10697	34	89303	11056	34	88944	00358	1	99642	39
22	1 4	58 56	10795	35	89205	11155	36	88845	00360	1	99640	38
23	0 56	59 4	10893	37	89107	11254	37	88746	00362	1	99638	37
24	0 48	59 12	10990	38	89010	11353	39	88647	00363	1	99637	36
25	11 0 40	0 59 20	9.11087	40	10.88913	9.11452	41	10.88548	10.00365	1	9.99635	35
26	0 32	59 28	11184	42	88816	11551	42	88449	00367	1	99633	34
27	0 24	59 36	11281	43	88719	11649	44	88351	00368	1	99632	33
28	0 16	59 44	11377	45	88623	11747	46	88253	00370	1	99630	32
29	0 8	59 52	11474	46	88526	11845	47	88155	00371	1	99629	31
30	11 0 0	1 0 0	9.11570	48	10.88430	9.11943	49	10.88057	10.00373	1	9.99627	30
31	10 59 52	0 8	11666	50	88334	12040	51	87960	00375	1	99625	29
32	59 44	0 16	11761	51	88239	12138	52	87862	00376	1	99624	28
33	59 36	0 24	11857	53	88143	12235	54	87765	00378	1	99622	27
34	59 28	0 32	11952	54	88048	12332	55	87668	00380	1	99620	26
35	10 59 20	1 0 40	9.12047	56	10.87953	9.12428	57	10.87572	10.00382	1	9.99618	25
36	59 12	0 48	12142	58	87858	12525	59	87475	00383	1	99617	24
37	59 4	0 56	12236	59	87764	12621	60	87379	00385	1	99615	23
38	58 56	1 4	12331	61	87669	12717	62	87283	00387	1	99613	22
39	58 48	1 12	12425	62	87575	12813	64	87187	00388	1	99612	21
40	10 58 40	1 1 20	9.12519	64	10.87481	9.12909	65	10.87091	10.00390	1	9.99610	20
41	58 32	1 28	12612	66	87388	13004	67	86996	00392	1	99608	19
42	58 24	1 36	12706	67	87294	13099	68	86901	00393	1	99607	18
43	58 16	1 44	12799	69	87201	13194	70	86806	00395	1	99605	17
44	58 8	1 52	12892	70	87108	13289	72	86711	00397	1	99603	16
45	10 58 0	1 2 0	9.12985	72	10.87015	9.13384	73	10.86616	10.00399	1	9.99601	15
46	57 52	2 8	13078	74	86922	13478	75	86522	00400	1	99600	14
47	57 44	2 16	13171	75	86829	13573	77	86427	00402	1	99598	13
48	57 36	2 24	13263	77	86737	13667	78	86333	00404	1	99596	12
49	57 28	2 32	13355	78	86645	13761	80	86239	00405	1	99595	11
50	10 57 20	1 2 40	9.13447	80	10.86553	9.13854	81	10.86146	10.00407	1	9.99593	10
51	57 12	2 48	13539	82	86461	13948	83	86052	00409	1	99591	9
52	57 4	2 56	13630	83	86370	14041	85	85959	00411	1	99589	8
53	56 56	3 4	13722	85	86278	14134	86	85866	00412	1	99588	7
54	56 48	3 12	13813	87	86187	14227	88	85773	00414	2	99586	6
55	10 56 40	1 3 20	9.13904	88	10.86096	9.14320	90	10.85680	10.00416	2	9.99584	5
56	56 32	3 28	13994	90	86006	14412	91	85588	00418	2	99582	4
57	56 24	3 36	14085	91	85915	14504	93	85496	00419	2	99581	3
58	56 16	3 44	14175	93	85825	14597	95	85403	00421	2	99579	2
59	56 8	3 52	14266	95	85734	14688	96	85312	00423	2	99577	1
60	56 0	4 0	14356	96	85644	14780	98	85220	00425	2	99575	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
97°			A		A	B		B	C		C	82°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	12	24	36	48	60	72	84
	B	12	24	37	49	61	73	86
	C	0	0	1	1	1	1	1

TABLE 44.

Log. Sines, Tangents, and Secants.

8°			A		A	B		B	C		C	171°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	10 56 0	1 4 0	9. 14356	0	10. 85644	9. 14780	0	10. 85220	10. 00425	0	9. 99575	60
1	55 52	4 8	14445	1	85555	14872	1	85128	00426	0	99574	59
2	55 44	4 16	14535	3	85465	14963	3	85037	00428	0	99572	58
3	55 36	4 24	14624	4	85376	15054	4	84946	00430	0	99570	57
4	55 28	4 32	14714	6	85286	15145	6	84855	00432	0	99568	56
5	10 55 20	1 4 40	9. 14803	7	10. 85197	9. 15236	7	10. 84764	10. 00434	0	9. 99566	55
6	55 12	4 48	14891	8	85109	15327	9	84673	00435	0	99565	54
7	55 4	4 56	14980	10	85020	15417	10	84583	00437	0	99563	53
8	54 56	5 4	15069	11	84931	15508	12	84492	00439	0	99561	52
9	54 48	5 12	15157	13	84843	15598	13	84402	00441	0	99559	51
10	10 54 40	1 5 20	9. 15245	14	10. 84755	9. 15688	14	10. 84312	10. 00443	0	9. 99557	50
11	54 32	5 28	15333	16	84667	15777	16	84223	00444	0	99556	49
12	54 24	5 36	15421	17	84579	15867	17	84133	00446	0	99554	48
13	54 16	5 44	15508	18	84492	15956	19	84044	00448	0	99552	47
14	54 8	5 52	15596	20	84404	16046	20	83954	00450	0	99550	46
15	10 54 0	1 6 0	9. 15683	21	10. 84317	9. 16135	22	10. 83865	10. 00452	0	9. 99548	45
16	53 52	6 8	15770	23	84230	16224	23	83776	00454	1	99546	44
17	53 44	6 16	15857	24	84143	16312	25	83688	00455	1	99545	43
18	53 36	6 24	15944	25	84056	16401	26	83599	00457	1	99543	42
19	53 28	6 32	16030	27	83970	16489	27	83511	00459	1	99541	41
20	10 53 20	1 6 40	9. 16116	28	10. 83884	9. 16577	29	10. 83423	10. 00461	1	9. 99539	40
21	53 12	6 48	16203	30	83797	16665	30	83335	00463	1	99537	39
22	53 4	6 56	16289	31	83711	16753	32	83247	00465	1	99535	38
23	52 56	7 4	16374	32	83626	16841	33	83159	00467	1	99533	37
24	52 48	7 12	16460	34	83540	16928	35	83072	00468	1	99532	36
25	10 52 40	1 7 20	9. 16545	35	10. 83455	9. 17016	36	10. 82984	10. 00470	1	9. 99530	35
26	52 32	7 28	16631	37	83369	17103	37	82897	00472	1	99528	34
27	52 24	7 36	16716	38	83284	17190	39	82810	00474	1	99526	33
28	52 16	7 44	16801	39	83199	17277	40	82723	00476	1	99524	32
29	52 8	7 52	16886	41	83114	17363	42	82637	00478	1	99522	31
30	10 52 0	1 8 0	9. 16970	42	10. 83030	9. 17450	43	10. 82550	10. 00480	1	9. 99520	30
31	51 52	8 8	17055	44	82945	17536	45	82464	00482	1	99518	29
32	51 44	8 16	17139	45	82861	17622	46	82378	00483	1	99517	28
33	51 36	8 24	17223	47	82777	17708	48	82292	00485	1	99515	27
34	51 28	8 32	17307	48	82693	17794	49	82206	00487	1	99513	26
35	10 51 20	1 8 40	9. 17391	49	10. 82609	9. 17880	50	10. 82120	10. 00489	1	9. 99511	25
36	51 12	8 48	17474	51	82526	17965	52	82035	00491	1	99509	24
37	51 4	8 56	17558	52	82442	18051	53	81949	00493	1	99507	23
38	50 56	9 4	17641	54	82359	18136	55	81864	00495	1	99505	22
39	50 48	9 12	17724	55	82276	18221	56	81779	00497	1	99503	21
40	10 50 40	1 9 20	9. 17807	56	10. 82193	9. 18306	58	10. 81694	10. 00499	1	9. 99501	20
41	50 32	9 28	17890	58	82110	18391	59	81609	00501	1	99499	19
42	50 24	9 36	17973	59	82027	18475	61	81525	00503	1	99497	18
43	50 16	9 44	18055	61	81945	18560	62	81440	00505	1	99495	17
44	50 8	9 52	18137	62	81863	18644	63	81356	00506	1	99494	16
45	10 50 0	1 10 0	9. 18220	63	10. 81780	9. 18728	65	10. 81272	10. 00508	1	9. 99492	15
46	49 52	10 8	18302	65	81698	18812	66	81188	00510	1	99490	14
47	49 44	10 16	18383	66	81617	18896	68	81104	00512	1	99488	13
48	49 36	10 24	18465	68	81535	18979	69	81021	00514	2	99486	12
49	49 28	10 32	18547	69	81453	19063	71	80937	00516	2	99484	11
50	10 49 20	1 10 40	9. 18628	71	10. 81372	9. 19146	72	10. 80854	10. 00518	2	9. 99482	10
51	49 12	10 48	18709	72	81291	19229	74	80771	00520	2	99480	9
52	49 4	10 56	18790	73	81210	19312	75	80688	00522	2	99478	8
53	48 56	11 4	18871	75	81129	19395	76	80605	00524	2	99476	7
54	48 48	11 12	18952	76	81048	19478	78	80522	00526	2	99474	6
55	10 48 40	1 11 20	9. 19033	78	10. 80967	9. 19561	79	10. 80439	10. 00528	2	9. 99472	5
56	48 32	11 28	19113	79	80887	19643	81	80357	00530	2	99470	4
57	48 24	11 36	19193	80	80807	19725	82	80275	00532	2	99468	3
58	48 16	11 44	19273	82	80727	19807	84	80193	00534	2	99466	2
59	48 8	11 52	19353	83	80647	19889	85	80111	00536	2	99464	1
60	48 0	12 0	19433	85	80567	19971	87	80029	00538	2	99462	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
98°			A		A	B		B	C		C	81°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	11	21	32	42	53	63	74
	B	11	22	32	43	54	65	76
	C	0	0	1	1	1	1	2

TABLE 44.

Log. Sines, Tangents, and Secants.

9°			A		A	B		B	C		C	170°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	10 48 0	1 12 0	9.19433	0	10.80567	9.19971	0	10.80029	10.00538	0	9.99462	60
1	47 52	12 8	19513	1	80487	20053	1	79947	00540	0	99460	59
2	47 44	12 16	19592	3	80408	20134	3	79865	00542	0	99458	58
3	47 36	12 24	19672	4	80328	20216	4	79784	00544	0	99456	57
4	47 28	12 32	19751	5	80249	20297	5	79703	00546	0	99454	56
5	10 47 20	1 12 40	9.19830	6	10.80170	9.20378	6	10.79622	10.00548	0	9.99452	55
6	47 12	12 48	19909	8	80091	20459	8	79541	00550	0	99450	54
7	47 4	12 56	19988	9	80012	20540	9	79460	00552	0	99448	53
8	46 56	13 4	20067	10	79933	20621	10	79379	00554	0	99446	52
9	46 48	13 12	20145	11	79855	20701	12	79299	00556	0	99444	51
10	10 46 40	1 13 20	9.20223	13	10.79777	9.20782	13	10.79218	10.00558	0	9.99442	50
11	46 32	13 28	20302	14	79698	20862	14	79138	00560	0	99440	49
12	46 24	13 36	20380	15	79620	20942	16	79058	00562	0	99438	48
13	46 16	13 44	20458	16	79542	21022	17	78978	00564	0	99436	47
14	46 8	13 52	20535	18	79465	21102	18	78898	00566	0	99434	46
15	10 46 0	1 14 0	9.20613	19	10.79387	9.21182	19	10.78818	10.00568	1	9.99432	45
16	45 52	14 8	20691	20	79309	21261	21	78739	00571	1	99429	44
17	45 44	14 16	20768	21	79232	21341	22	78659	00573	1	99427	43
18	45 36	14 24	20845	23	79155	21420	23	78580	00575	1	99425	42
19	45 28	14 32	20922	24	79078	21499	25	78501	00577	1	99423	41
20	10 45 20	1 14 40	9.20999	25	10.79001	9.21578	26	10.78422	10.00579	1	9.99421	40
21	45 12	14 48	21076	26	78924	21657	27	78343	00581	1	99419	39
22	45 4	14 56	21153	28	78847	21736	28	78264	00583	1	99417	38
23	44 56	15 4	21229	29	78771	21814	30	78186	00585	1	99415	37
24	44 48	15 12	21306	30	78694	21893	31	78107	00587	1	99413	36
25	10 44 40	1 15 20	9.21382	31	10.78618	9.21971	32	10.78029	10.00589	1	9.99411	35
26	44 32	15 28	21458	33	78542	22049	34	77951	00591	1	99409	34
27	44 24	15 36	21534	34	78466	22127	35	77873	00593	1	99407	33
28	44 16	15 44	21610	35	78390	22205	36	77795	00596	1	99404	32
29	44 8	15 52	21685	37	78315	22283	38	77717	00598	1	99402	31
30	10 44 0	1 16 0	9.21761	38	10.78239	9.22361	39	10.77639	10.00600	1	9.99400	30
31	43 52	16 8	21836	39	78164	22438	40	77562	00602	1	99398	29
32	43 44	16 16	21912	40	78088	22516	41	77484	00604	1	99396	28
33	43 36	16 24	21987	42	78013	22593	43	77407	00606	1	99394	27
34	43 28	16 32	22062	43	77938	22670	44	77330	00608	1	99392	26
35	10 43 20	1 16 40	9.22137	44	10.77863	9.22747	45	10.77253	10.00610	1	9.99390	25
36	43 12	16 48	22211	45	77789	22824	47	77176	00612	1	99388	24
37	43 4	16 56	22286	47	77714	22901	48	77099	00615	1	99385	23
38	42 56	17 4	22361	48	77639	22977	49	77023	00617	1	99383	22
39	42 48	17 12	22435	49	77565	23054	50	76946	00619	1	99381	21
40	10 42 40	1 17 20	9.22509	50	10.77491	9.23130	52	10.76870	10.00621	1	9.99379	20
41	42 32	17 28	22583	52	77417	23206	53	76794	00623	1	99377	19
42	42 24	17 36	22657	53	77343	23283	54	76717	00625	1	99375	18
43	42 16	17 44	22731	54	77269	23359	56	76641	00628	2	99372	17
44	42 8	17 52	22805	55	77195	23435	57	76565	00630	2	99370	16
45	10 42 0	1 18 0	9.22878	57	10.77122	9.23510	58	10.76490	10.00632	2	9.99368	15
46	41 52	18 8	22952	58	77048	23586	60	76414	00634	2	99366	14
47	41 44	18 16	23025	59	76975	23661	61	76339	00636	2	99364	13
48	41 36	18 24	23098	60	76902	23737	62	76263	00638	2	99362	12
49	41 28	18 32	23171	62	76829	23812	63	76188	00641	2	99359	11
50	10 41 20	1 18 40	9.23244	63	10.76756	9.23887	65	10.76113	10.00643	2	9.99357	10
51	41 12	18 48	23317	64	76683	23962	66	76038	00645	2	99355	9
52	41 4	18 56	23390	65	76610	24037	67	75963	00647	2	99353	8
53	40 56	19 4	23462	67	76538	24112	69	75888	00649	2	99351	7
54	40 48	19 12	23535	68	76465	24186	70	75814	00652	2	99348	6
55	10 40 40	1 19 20	9.23607	69	10.76393	9.24261	71	10.75739	10.00654	2	9.99346	5
56	40 32	19 28	23679	71	76321	24335	73	75665	00656	2	99344	4
57	40 24	19 36	23752	72	76248	24410	74	75590	00658	2	99342	3
58	40 16	19 44	23823	73	76177	24484	75	75516	00660	2	99340	2
59	40 8	19 52	23895	74	76105	24558	76	75442	00663	2	99337	1
60	40 0	20 0	23967	76	76033	24632	78	75368	00665	2	99335	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
99°			A		A	B		B	C		C	80°

Seconds of time	1^s	2^s	3^s	4^s	5^s	6^s	7^s
Prop. parts of cols. A	9	19	28	38	47	57	66
Prop. parts of cols. B	10	19	29	39	49	58	68
Prop. parts of cols. C	0	1	1	1	1	2	2

TABLE 44.

Log. Sines, Tangents, and Secants.

10°			A		A	B		B	C		C	169°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	10 40 0	1 20 0	9.23967	0	10.76033	9.24632	0	10.75368	10.00665	0	9.99335	60
1	39 52	20 8	24039	1	75961	24706	1	75294	00667	0	99333	59
2	39 44	20 16	24110	2	75890	24779	2	75221	00669	0	99331	58
3	39 36	20 24	24181	3	75819	24853	4	75147	00672	0	99328	57
4	39 28	20 32	24253	5	75747	24926	5	75074	00674	0	99326	56
5	10 39 20	1 20 40	9.24324	6	10.75676	9.25000	6	10.75000	10.00676	0	9.99324	55
6	39 12	20 48	24395	7	75605	25073	7	74927	00678	0	99322	54
7	39 4	20 56	24466	8	75534	25146	8	74854	00681	0	99319	53
8	38 56	21 4	24536	9	75464	25219	9	74781	00683	0	99317	52
9	38 48	21 12	24607	10	75393	25292	11	74708	00685	0	99315	51
10	10 38 40	1 21 20	9.24677	11	10.75323	9.25365	12	10.74635	10.00687	0	9.99313	50
11	38 32	21 28	24748	13	75252	25437	13	74563	00690	0	99310	49
12	38 24	21 36	24818	14	75182	25510	14	74490	00692	0	99308	48
13	38 16	21 44	24888	15	75112	25582	15	74418	00694	1	99306	47
14	38 8	21 52	24958	16	75042	25655	16	74345	00696	1	99304	46
15	10 38 0	1 22 0	9.25028	17	10.74972	9.25727	18	10.74273	10.00699	1	9.99301	45
16	37 52	22 8	25098	18	74902	25799	19	74201	00701	1	99299	44
17	37 44	22 16	25168	19	74832	25871	20	74129	00703	1	99297	43
18	37 36	22 24	25237	20	74763	25943	21	74057	00706	1	99294	42
19	37 28	22 32	25307	22	74693	26015	22	73985	00708	1	99292	41
20	10 37 20	1 22 40	9.25376	23	10.74624	9.26086	24	10.73914	10.00710	1	9.99290	40
21	37 12	22 48	25445	24	74555	26158	25	73842	00712	1	99288	39
22	37 4	22 56	25514	25	74486	26229	26	73771	00715	1	99285	38
23	36 56	23 4	25583	26	74417	26301	27	73699	00717	1	99283	37
24	36 48	23 12	25652	27	74348	26372	28	73628	00719	1	99281	36
25	10 36 40	1 23 20	9.25721	28	10.74279	9.26443	29	10.73557	10.00722	1	9.99278	35
26	36 32	23 28	25790	30	74210	26514	31	73486	00724	1	99276	34
27	36 24	23 36	25858	31	74142	26585	32	73415	00726	1	99274	33
28	36 16	23 44	25927	32	74073	26655	33	73345	00729	1	99271	32
29	36 8	23 52	25995	33	74005	26726	34	73274	00731	1	99269	31
30	10 36 0	1 24 0	9.26063	34	10.73937	9.26797	35	10.73203	10.00733	1	9.99267	30
31	35 52	24 8	26131	35	73869	26867	36	73133	00736	1	99264	29
32	35 44	24 16	26199	36	73801	26937	38	73063	00738	1	99262	28
33	35 36	24 24	26267	38	73733	27008	39	72992	00740	1	99260	27
34	35 28	24 32	26335	39	73665	27078	40	72922	00743	1	99257	26
35	10 35 20	1 24 40	9.26403	40	10.73597	9.27148	41	10.72852	10.00745	1	9.99255	25
36	35 12	24 48	26470	41	73530	27218	42	72782	00748	1	99252	24
37	35 4	24 56	26538	42	73462	27288	44	72712	00750	1	99250	23
38	34 56	25 4	26605	43	73395	27357	45	72643	00752	1	99248	22
39	34 48	25 12	26672	44	73328	27427	46	72573	00755	2	99245	21
40	10 34 40	1 25 20	9.26739	45	10.73261	9.27496	47	10.72504	10.00757	2	9.99243	20
41	34 32	25 28	26806	47	73194	27566	48	72434	00759	2	99241	19
42	34 24	25 36	26873	48	73127	27635	49	72365	00762	2	99238	18
43	34 16	25 44	26940	49	73060	27704	51	72296	00764	2	99236	17
44	34 8	25 52	27007	50	72993	27773	52	72227	00767	2	99233	16
45	10 34 0	1 26 0	9.27073	51	10.72927	9.27842	53	10.72158	10.00769	2	9.99231	15
46	33 52	26 8	27140	52	72860	27911	54	72089	00771	2	99229	14
47	33 44	26 16	27206	53	72794	27980	55	72020	00774	2	99226	13
48	33 36	26 24	27273	55	72727	28049	56	71951	00776	2	99224	12
49	33 28	26 32	27339	56	72661	28117	58	71883	00779	2	99221	11
50	10 33 20	1 26 40	9.27405	57	10.72595	9.28186	59	10.71814	10.00781	2	9.99219	10
51	33 12	26 48	27471	58	72529	28254	60	71746	00783	2	99217	9
52	33 4	26 56	27537	59	72463	28323	61	71677	00786	2	99214	8
53	32 56	27 4	27602	60	72398	28391	62	71609	00788	2	99212	7
54	32 48	27 12	27668	61	72332	28459	63	71541	00791	2	99209	6
55	10 32 40	1 27 20	9.27734	63	10.72266	9.28527	65	10.71473	10.00793	2	9.99207	5
56	32 32	27 28	27799	64	72201	28595	66	71405	00796	2	99204	4
57	32 24	27 36	27864	65	72136	28662	67	71338	00798	2	99202	3
58	32 16	27 44	27930	66	72070	28730	68	71270	00800	2	99200	2
59	32 8	27 52	27995	67	72005	28798	69	71202	00803	2	99197	1
60	32 0	28 0	28060	68	71940	28865	71	71135	00805	2	99195	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
100°			A		A	B		B	C		C	79°

Seconds of time		1^s	2^s	3^s	4^s	5^s	6^s	7^s
Prop. parts of cols.	A	9	17	26	34	43	51	60
	B	9	18	26	35	44	53	62
	C	0	1	1	1	1	2	2

TABLE 44.

Log. Sines, Tangents, and Secants.

11° | 168°

M.	Hour A. M.	Hour P. M.	Sine. (A)	Diff.	Cosecant. (A)	Tangent. (B)	Diff.	Cotangent. (B)	Secant. (C)	Diff.	Cosine. (C)	M.
0	10 32 0	1 28 0	9.28060	0	10.71940	9.28865	0	10.71135	10.00805	0	9.99195	60
1	31 52	28 8	28125	1	71875	28933	1	71067	00808	0	99192	59
2	31 44	28 16	28190	2	71810	29000	2	71000	00810	0	99190	58
3	31 36	28 24	28254	3	71746	29067	3	70933	00813	0	99187	57
4	31 28	28 32	28319	4	71681	29134	4	70866	00815	0	99185	56
5	10 31 20	1 28 40	9.28384	5	10.71616	9.29201	5	10.70799	10.00818	0	9.99182	55
6	31 12	28 48	28448	6	71552	29268	6	70732	00820	0	99180	54
7	31 4	28 56	28512	7	71488	29335	8	70665	00823	0	99177	53
8	30 56	29 4	28577	8	71423	29402	9	70598	00825	0	99175	52
9	30 48	29 12	28641	9	71359	29468	10	70532	00828	0	99172	51
10	10 30 40	1 29 20	9.28705	10	10.71295	9.29535	11	10.70465	10.00830	0	9.99170	50
11	30 32	29 28	28769	11	71231	29601	12	70399	00833	0	99167	49
12	30 24	29 36	28833	12	71167	29668	13	70332	00835	1	99165	48
13	30 16	29 44	28896	13	71104	29734	14	70266	00838	1	99162	47
14	30 8	29 52	28960	14	71040	29800	15	70200	00840	1	99160	46
15	10 30 0	1 30 0	9.29024	16	10.70976	9.29866	16	10.70134	10.00843	1	9.99157	45
16	29 52	30 8	29087	17	70913	29932	17	70068	00845	1	99155	44
17	29 44	30 16	29150	18	70850	29998	18	70002	00848	1	99152	43
18	29 36	30 24	29214	19	70786	30064	19	69936	00850	1	99150	42
19	29 28	30 32	29277	20	70723	30130	20	69870	00853	1	99147	41
20	10 29 20	1 30 40	9.29340	21	10.70660	9.30195	22	10.69805	10.00855	1	9.99145	40
21	29 12	30 48	29403	22	70597	30261	23	69739	00858	1	99142	39
22	29 4	30 56	29466	23	70534	30326	24	69674	00860	1	99140	38
23	28 56	31 4	29529	24	70471	30391	25	69609	00863	1	99137	37
24	28 48	31 12	29591	25	70409	30457	26	69543	00865	1	99135	36
25	10 28 40	1 31 20	9.29654	26	10.70346	9.30522	27	10.69478	10.00868	1	9.99132	35
26	28 32	31 28	29716	27	70284	30587	28	69413	00870	1	99130	34
27	28 24	31 36	29779	28	70221	30652	29	69348	00873	1	99127	33
28	28 16	31 44	29841	29	70159	30717	30	69283	00876	1	99124	32
29	28 8	31 52	29903	30	70097	30782	31	69218	00878	1	99122	31
30	10 28 0	1 32 0	9.29966	31	10.70034	9.30846	32	10.69154	10.00881	1	9.99119	30
31	27 52	32 8	30028	32	69972	30911	33	69089	00883	1	99117	29
32	27 44	32 16	30090	33	69910	30975	35	69025	00886	1	99114	28
33	27 36	32 24	30151	34	69849	31040	36	68960	00888	1	99112	27
34	27 28	32 32	30213	35	69787	31104	37	68896	00891	1	99109	26
35	10 27 20	1 32 40	9.30275	36	10.69725	9.31168	38	10.68832	10.00894	2	9.99106	25
36	27 12	32 48	30336	37	69664	31233	39	68767	00896	2	99104	24
37	27 4	32 56	30398	38	69602	31297	40	68703	00899	2	99101	23
38	26 56	33 4	30459	39	69541	31361	41	68639	00901	2	99099	22
39	26 48	33 12	30521	40	69479	31425	42	68575	00904	2	99096	21
40	10 26 40	1 33 20	9.30582	41	10.69418	9.31489	43	10.68511	10.00907	2	9.99093	20
41	26 32	33 28	30643	42	69357	31552	44	68448	00909	2	99091	19
42	26 24	33 36	30704	43	69296	31616	45	68384	00912	2	99088	18
43	26 16	33 44	30765	45	69235	31679	46	68321	00914	2	99086	17
44	26 8	33 52	30826	46	69174	31743	47	68257	00917	2	99083	16
45	10 26 0	1 34 0	9.30887	47	10.69113	9.31806	49	10.68194	10.00920	2	9.99080	15
46	25 52	34 8	30947	48	69053	31870	50	68130	00922	2	99078	14
47	25 44	34 16	31008	49	68992	31933	51	68067	00925	2	99075	13
48	25 36	34 24	31068	50	68932	31996	52	68004	00928	2	99072	12
49	25 28	34 32	31129	51	68871	32059	53	67941	00930	2	99070	11
50	10 25 20	1 34 40	9.31189	52	10.68811	9.32122	54	10.67878	10.00933	2	9.99067	10
51	25 12	34 48	31250	53	68750	32185	55	67815	00936	2	99064	9
52	25 4	34 56	31310	54	68690	32248	56	67752	00938	2	99062	8
53	24 56	35 4	31370	55	68630	32311	57	67689	00941	2	99059	7
54	24 48	35 12	31430	56	68570	32373	58	67627	00944	2	99056	6
55	10 24 40	1 35 20	9.31490	57	10.68510	9.32436	59	10.67564	10.00946	2	9.99054	5
56	24 32	35 28	31549	58	68451	32498	60	67502	00949	2	99051	4
57	24 24	35 36	31609	59	68391	32561	61	67439	00952	2	99048	3
58	24 16	35 44	31669	60	68331	32623	63	67377	00954	2	99046	2
59	24 8	35 52	31728	61	68272	32685	64	67315	00957	3	99043	1
60	24 0	36 0	31788	62	68212	32747	65	67253	00960	3	99040	0
M.	Hour P. M.	Hour A. M.	Cosine. (A)	Diff.	Secant. (A)	Cotangent. (B)	Diff.	Tangent. (B)	Cosecant. (C)	Diff.	Sine. (C)	M.

101° | 78°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	8	16	23	31	39	47	54
	B	8	16	24	32	40	49	57
	C	0	1	1	1	2	2	2

TABLE 44.

Log. Sines, Tangents, and Secants.

12°			A		A	B		B	C		C	167°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	10 24 0	1 36 0	9.31788	0	10.68212	9.32747	0	10.67253	10.00960	0	9.99040	60
1	23 52	36 8	31847	1	68153	32810	1	67190	00962	0	99038	59
2	23 44	36 16	31907	2	68093	32872	2	67128	00965	0	99035	58
3	23 36	36 24	31966	3	68034	32933	3	67067	00968	0	99032	57
4	23 28	36 32	32025	4	67975	32995	4	67005	00970	0	99030	56
5	10 23 20	1 36 40	9.32084	5	10.67916	9.33057	5	10.66943	10.00973	0	9.99027	55
6	23 12	36 48	32143	6	67857	33119	6	66881	00976	0	99024	54
7	23 4	36 56	32202	7	67798	33180	7	66820	00978	0	99022	53
8	22 56	37 4	32261	8	67739	33242	8	66758	00981	0	99019	52
9	22 48	37 12	32319	9	67681	33303	9	66697	00984	0	99016	51
10	10 22 40	1 37 20	9.32378	10	10.67622	9.33365	10	10.66635	10.00987	0	9.99013	50
11	22 32	37 28	32437	10	67563	33426	11	66574	00989	1	99011	49
12	22 24	37 36	32495	11	67505	33487	12	66513	00992	1	99008	48
13	22 16	37 44	32553	12	67447	33548	13	66452	00995	1	99005	47
14	22 8	37 52	32612	13	67388	33609	14	66391	00998	1	99002	46
15	10 22 0	1 38 0	9.32670	14	10.67330	9.33670	15	10.66330	10.01000	1	9.99000	45
16	21 52	38 8	32728	15	67272	33731	16	66269	01003	1	98997	44
17	21 44	38 16	32786	16	67214	33792	17	66208	01006	1	98994	43
18	21 36	38 24	32844	17	67156	33853	18	66147	01009	1	98991	42
19	21 28	38 32	32902	18	67098	33913	19	66087	01011	1	98989	41
20	10 21 20	1 38 40	9.32960	19	10.67040	9.33974	20	10.66026	10.01014	1	9.98986	40
21	21 12	38 48	33018	20	66982	34034	21	65966	01017	1	98983	39
22	21 4	38 56	33075	21	66925	34095	22	65905	01020	1	98980	38
23	20 56	39 4	33133	22	66867	34155	23	65845	01022	1	98978	37
24	20 48	39 12	33190	23	66810	34215	24	65785	01025	1	98975	36
25	10 20 40	1 39 20	9.33248	24	10.66752	9.34276	25	10.65724	10.01028	1	9.98972	35
26	20 32	39 28	33305	25	66695	34336	26	65664	01031	1	98969	34
27	20 24	39 36	33362	26	66638	34396	27	65604	01033	1	98967	33
28	20 16	39 44	33420	27	66580	34456	28	65544	01036	1	98964	32
29	20 8	39 52	33477	28	66523	34516	29	65484	01039	1	98961	31
30	10 20 0	1 40 0	9.33534	29	10.66466	9.34576	30	10.65424	10.01042	1	9.98958	30
31	19 52	40 8	33591	29	66409	34635	31	65365	01045	1	98955	29
32	19 44	40 16	33647	30	66353	34695	32	65305	01047	1	98953	28
33	19 36	40 24	33704	31	66296	34755	33	65245	01050	2	98950	27
34	19 28	40 32	33761	32	66239	34814	34	65186	01053	2	98947	26
35	10 19 20	1 40 40	9.33818	33	10.66182	9.34874	35	10.65126	10.01056	2	9.98944	25
36	19 12	40 48	33874	34	66126	34933	36	65067	01059	2	98941	24
37	19 4	40 56	33931	35	66069	34992	37	65008	01062	2	98938	23
38	18 56	41 4	33987	36	66013	35051	38	64949	01064	2	98936	22
39	18 48	41 12	34043	37	65957	35111	39	64889	01067	2	98933	21
40	10 18 40	1 41 20	9.34100	38	10.65900	9.35170	40	10.64830	10.01070	2	9.98930	20
41	18 32	41 28	34156	39	65844	35229	41	64771	01073	2	98927	19
42	18 24	41 36	34212	40	65788	35288	42	64712	01076	2	98924	18
43	18 16	41 44	34268	41	65732	35347	43	64653	01079	2	98921	17
44	18 8	41 52	34324	42	65676	35405	44	64595	01081	2	98919	16
45	10 18 0	1 42 0	9.34380	43	10.65620	9.35464	45	10.64536	10.01084	2	9.98916	15
46	17 52	42 8	34436	44	65564	35523	46	64477	01087	2	98913	14
47	17 44	42 16	34491	45	65509	35581	47	64419	01090	2	98910	13
48	17 36	42 24	34547	46	65453	35640	48	64360	01093	2	98907	12
49	17 28	42 32	34602	47	65398	35698	49	64302	01096	2	98904	11
50	10 17 20	1 42 40	9.34658	48	10.65342	9.35757	50	10.64243	10.01099	2	9.98901	10
51	17 12	42 48	34713	48	65287	35815	51	64185	01102	2	98898	9
52	17 4	42 56	34769	49	65231	35873	52	64127	01104	2	98896	8
53	16 56	43 4	34824	50	65176	35931	53	64069	01107	2	98893	7
54	16 48	43 12	34879	51	65121	35989	54	64011	01110	3	98890	6
55	10 16 40	1 43 20	9.34934	52	10.65066	9.36047	55	10.63953	10.01113	3	9.98887	5
56	16 32	43 28	34989	53	65011	36105	56	63895	01116	3	98884	4
57	16 24	43 36	35044	54	64956	36163	57	63837	01119	3	98881	3
58	16 16	43 44	35099	55	64901	36221	58	63779	01122	3	98878	2
59	16 8	43 52	35154	56	64846	36279	59	63721	01125	3	98875	1
60	16 0	44 0	35209	57	64791	36336	60	63664	01128	3	98872	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
102°			A		A	B		B	C		C	77°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	7	14	21	29	36	43	50
	B	7	15	22	30	37	45	52
	C	0	1	1	1	2	2	2

TABLE 44.

Log. Sines, Tangents, and Secants.

13°			A		A	B		B	C		C	166°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	10 16 0	1 44 0	9.35209	0	10.64791	9.36336	0	10.63664	10.01128	0	9.98872	60
1	15 52	44 8	35263	1	64737	36394	1	63606	01131	0	98869	59
2	15 44	44 16	35318	2	64682	36452	2	63548	01133	0	98867	58
3	15 36	44 24	35373	3	64627	36509	3	63491	01136	0	98864	57
4	15 28	44 32	35427	4	64573	36566	4	63434	01139	0	98861	56
5	10 15 20	1 44 40	9.35481	4	10.64519	9.36624	5	10.63376	10.01142	0	9.98858	55
6	15 12	44 48	35536	5	64464	36681	6	63319	01145	0	98855	54
7	15 4	44 56	35590	6	64410	36738	6	63262	01148	0	98852	53
8	14 56	45 4	35644	7	64356	36795	7	63205	01151	0	98849	52
9	14 48	45 12	35698	8	64302	36852	8	63148	01154	0	98846	51
10	10 14 40	1 45 20	9.35752	9	10.64248	9.36909	9	10.63091	10.01157	1	9.98843	50
11	14 32	45 28	35806	10	64194	36966	10	63034	01160	1	98840	49
12	14 24	45 36	35860	11	64140	37023	11	62977	01163	1	98837	48
13	14 16	45 44	35914	11	64086	37080	12	62920	01166	1	98834	47
14	14 8	45 52	35968	12	64032	37137	13	62863	01169	1	98831	46
15	10 14 0	1 46 0	9.36022	13	10.63978	9.37193	14	10.62807	10.01172	1	9.98828	45
16	13 52	46 8	36075	14	63925	37250	15	62750	01175	1	98825	44
17	13 44	46 16	36129	15	63871	37306	16	62694	01178	1	98822	43
18	13 36	46 24	36182	16	63818	37363	17	62637	01181	1	98819	42
19	13 28	46 32	36236	17	63764	37419	18	62581	01184	1	98816	41
20	10 13 20	1 46 40	9.36289	18	10.63711	9.37476	19	10.62524	10.01187	1	9.98813	40
21	13 12	46 48	36342	18	63658	37532	19	62468	01190	1	98810	39
22	13 4	46 56	36395	19	63605	37588	20	62412	01193	1	98807	38
23	12 56	47 4	36449	20	63551	37644	21	62356	01196	1	98804	37
24	12 48	47 12	36502	21	63498	37700	22	62300	01199	1	98801	36
25	10 12 40	1 47 20	9.36555	22	10.63445	9.37756	23	10.62244	10.01202	1	9.98798	35
26	12 32	47 28	36608	23	63392	37812	24	62188	01205	1	98795	34
27	12 24	47 36	36660	24	63340	37868	25	62132	01208	1	98792	33
28	12 16	47 44	36713	25	63287	37924	26	62076	01211	1	98789	32
29	12 8	47 52	36766	25	63234	37980	27	62020	01214	1	98786	31
30	10 12 0	1 48 0	9.36819	26	10.63181	9.38035	28	10.61965	10.01217	2	9.98783	30
31	11 52	48 8	36871	27	63129	38091	29	61909	01220	2	98780	29
32	11 44	48 16	36924	28	63076	38147	30	61853	01223	2	98777	28
33	11 36	48 24	36976	29	63024	38202	31	61798	01226	2	98774	27
34	11 28	48 32	37028	30	62972	38257	32	61743	01229	2	98771	26
35	10 11 20	1 48 40	9.37081	31	10.62919	9.38313	32	10.61687	10.01232	2	9.98768	25
36	11 12	48 48	37133	32	62867	38368	33	61632	01235	2	98765	24
37	11 4	48 56	37185	32	62815	38423	34	61577	01238	2	98762	23
38	10 56	49 4	37237	33	62763	38479	35	61521	01241	2	98759	22
39	10 48	49 12	37289	34	62711	38534	36	61466	01244	2	98756	21
40	10 10 40	1 49 20	9.37341	35	10.62659	9.38589	37	10.61411	10.01247	2	9.98753	20
41	10 32	49 28	37393	36	62607	38644	38	61356	01250	2	98750	19
42	10 24	49 36	37445	37	62555	38699	39	61301	01254	2	98746	18
43	10 16	49 44	37497	38	62503	38754	40	61246	01257	2	98743	17
44	10 8	49 52	37549	39	62451	38808	41	61192	01260	2	98740	16
45	10 10 0	1 50 0	9.37600	39	10.62400	9.38863	42	10.61137	10.01263	2	9.98737	15
46	9 52	50 8	37652	40	62348	38918	43	61082	01266	2	98734	14
47	9 44	50 16	37703	41	62297	38972	44	61028	01269	2	98731	13
48	9 36	50 24	37755	42	62245	39027	45	60973	01272	2	98728	12
49	9 28	50 32	37806	43	62194	39082	45	60918	01275	2	98725	11
50	10 9 20	1 50 40	9.37858	44	10.62142	9.39136	46	10.60864	10.01278	3	9.98722	10
51	9 12	50 48	37909	45	62091	39190	47	60810	01281	3	98719	9
52	9 4	50 56	37960	46	62040	39245	48	60755	01285	3	98715	8
53	8 56	51 4	38011	47	61989	39299	49	60701	01288	3	98712	7
54	8 48	51 12	38062	47	61938	39353	50	60647	01291	3	98709	6
55	10 8 40	1 51 20	9.38113	48	10.61887	9.39407	51	10.60593	10.01294	3	9.98706	5
56	8 32	51 28	38164	49	61836	39461	52	60539	01297	3	98703	4
57	8 24	51 36	38215	50	61785	39515	53	60485	01300	3	98700	3
58	8 16	51 44	38266	51	61734	39569	54	60431	01303	3	98697	2
59	8 8	51 52	38317	52	61683	39623	55	60377	01306	3	98694	1
60	8 0	52 0	38368	53	61632	39677	56	60323	01310	3	98690	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
103°			A		A	B		B	C		C	76°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	7	13	20	26	33	39	46
	B	7	14	21	28	35	42	49
	C	0	1	1	2	2	2	3

TABLE 44.

Log. Sines, Tangents, and Secants.

14°			A		A	B		B	C		C	165°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	10 8 0	1 52 0	9.38368	0	10.61632	9.39677	0	10.60323	10.01310	0	9.98690	60
1	7 52	52 8	38418	1	61582	39731	1	60269	01313	0	98687	59
2	7 44	52 16	38469	2	61531	39785	2	60215	01316	0	98684	58
3	7 36	52 24	38519	2	61481	39838	3	60162	01319	0	98681	57
4	7 28	52 32	38570	3	61430	39892	3	60108	01322	0	98678	56
5	10 7 20	1 52 40	38620	4	10.61380	9.39945	4	10.60055	10.01325	0	9.98675	55
6	7 12	52 48	38670	5	61330	39999	5	60001	01329	0	98671	54
7	7 4	52 56	38721	6	61279	40052	6	59948	01332	0	98668	53
8	6 56	53 4	38771	7	61229	40106	7	59894	01335	0	98665	52
9	6 48	53 12	38821	7	61179	40159	8	59841	01338	0	98662	51
10	10 6 40	1 53 20	9.38871	8	10.61129	9.40212	9	10.59788	10.01341	1	9.98659	50
11	6 32	53 28	38921	9	61079	40266	10	59734	01344	1	98656	49
12	6 24	53 36	38971	10	61029	40319	10	59681	01348	1	98652	48
13	6 16	53 44	39021	11	60979	40372	11	59628	01351	1	98649	47
14	6 8	53 52	39071	11	60929	40425	12	59575	01354	1	98646	46
15	10 6 0	1 54 0	9.39121	12	10.60879	9.40478	13	10.59522	10.01357	1	9.98643	45
16	5 52	54 8	39170	13	60830	40531	14	59469	01360	1	98640	44
17	5 44	54 16	39220	14	60780	40584	15	59416	01364	1	98636	43
18	5 36	54 24	39270	15	60730	40636	16	59364	01367	1	98633	42
19	5 28	54 32	39319	15	60681	40689	17	59311	01370	1	98630	41
20	10 5 20	1 54 40	9.39369	16	10.60631	9.40742	17	10.59258	10.01373	1	9.98627	40
21	5 12	54 48	39418	17	60582	40795	18	59205	01377	1	98623	39
22	5 4	54 56	39467	18	60533	40847	19	59153	01380	1	98620	38
23	4 56	55 4	39517	19	60483	40900	20	59100	01383	1	98617	37
24	4 48	55 12	39566	20	60434	40952	21	59048	01386	1	98614	36
25	10 4 40	1 55 20	9.39615	20	10.60385	9.41005	22	10.58995	10.01390	1	9.98610	35
26	4 32	55 28	39664	21	60336	41057	23	58943	01393	1	98607	34
27	4 24	55 36	39713	22	60287	41109	23	58891	01396	1	98604	33
28	4 16	55 44	39762	23	60238	41161	24	58839	01399	2	98601	32
29	4 8	55 52	39811	24	60189	41214	25	58786	01403	2	98597	31
30	10 4 0	1 56 0	9.39860	24	10.60140	9.41266	26	10.58734	10.01406	2	9.98594	30
31	3 52	56 8	39909	25	60091	41318	27	58682	01409	2	98591	29
32	3 44	56 16	39958	26	60042	41370	28	58630	01412	2	98588	28
33	3 36	56 24	40006	27	59994	41422	29	58578	01416	2	98584	27
34	3 28	56 32	40055	28	59945	41474	30	58526	01419	2	98581	26
35	10 3 20	1 56 40	9.40103	29	10.59897	9.41526	30	10.58474	01422	2	9.98578	25
36	3 12	56 48	40152	29	59848	41578	31	58422	01426	2	98574	24
37	3 4	56 56	40200	30	59800	41629	32	58371	01429	2	98571	23
38	2 56	57 4	40249	31	59751	41681	33	58319	01432	2	98568	22
39	2 48	57 12	40297	32	59703	41733	34	58267	01435	2	98565	21
40	10 2 40	1 57 20	9.40346	33	10.59654	9.41784	35	10.58216	10.01439	2	9.98561	20
41	2 32	57 28	40394	33	59606	41836	36	58164	01442	2	98558	19
42	2 24	57 36	40442	34	59558	41887	36	58113	01445	2	98555	18
43	2 16	57 44	40490	35	59510	41939	37	58061	01449	2	98551	17
44	2 8	57 52	40538	36	59462	41990	38	58010	01452	2	98548	16
45	10 2 0	1 58 0	9.40586	37	10.59414	9.42041	39	10.57959	10.01455	2	9.98545	15
46	1 52	58 8	40634	37	59366	42093	40	57907	01459	3	98541	14
47	1 44	58 16	40682	38	59318	42144	41	57856	01462	3	98538	13
48	1 36	58 24	40730	39	59270	42195	42	57805	01465	3	98535	12
49	1 28	58 32	40778	40	59222	42246	43	57754	01469	3	98531	11
50	10 1 20	1 58 40	9.40825	41	10.59175	9.42297	43	10.57703	10.01472	3	9.98528	10
51	1 12	58 48	40873	42	59127	42348	44	57652	01475	3	98525	9
52	1 4	58 56	40921	42	59079	42399	45	57601	01479	3	98521	8
53	0 56	59 4	40968	43	59032	42450	46	57550	01482	3	98518	7
54	0 48	59 12	41016	44	58984	42501	47	57499	01485	3	98515	6
55	10 0 40	1 59 20	9.41063	45	10.58937	9.42552	48	10.57448	10.01489	3	9.98511	5
56	0 32	59 28	41111	46	58889	42603	49	57397	01492	3	98508	4
57	0 24	59 36	41158	46	58842	42653	50	57347	01495	3	98505	3
58	0 16	59 44	41205	47	58795	42704	50	57296	01499	3	98501	2
59	0 8	59 52	41252	48	58748	42755	51	57245	01502	3	98498	1
60	0 0	2 0 0	41300	49	58700	42805	52	57195	01506	3	98494	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
104°			A		A	B		B	C		C	75°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	6	12	18	24	31	37	43
	B	7	13	20	26	33	39	46
	C	0	1	1	2	2	2	3

TABLE 44.

Log. Sines, Tangents, and Secants.

15°			A		A	B		B	C		C	164°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	10 0 0	2 0 0	9. 41300	0	10. 58700	9. 42805	0	10. 57195	10. 01506	0	9. 98494	60
1	9 59 52	0 8	41347	1	58653	42856	1	57144	01509	0	98491	59
2	59 44	0 16	41394	2	58606	42906	2	57094	01512	0	98488	58
3	59 36	0 24	41441	2	58559	42957	2	57043	01516	0	98484	57
4	59 28	0 32	41488	3	58512	43007	3	56993	01519	0	98481	56
5	9 59 20	2 0 40	9. 41535	4	10. 58465	9. 43057	4	10. 56943	10. 01523	0	9. 98477	55
6	59 12	0 48	41582	5	58418	43108	5	56892	01526	0	98474	54
7	59 4	0 56	41628	5	58372	43158	6	56842	01529	0	98471	53
8	58 56	1 4	41675	6	58325	43208	7	56792	01533	0	98467	52
9	58 48	1 12	41722	7	58278	43258	7	56742	01536	1	98464	51
10	9 58 40	2 1 20	9. 41768	8	10. 58232	9. 43308	8	10. 56692	10. 01540	1	9. 98460	50
11	58 32	1 28	41815	8	58185	43358	9	56642	01543	1	98457	49
12	58 24	1 36	41861	9	58139	43408	10	56592	01547	1	98453	48
13	58 16	1 44	41908	10	58092	43458	11	56542	01550	1	98450	47
14	58 8	1 52	41954	11	58046	43508	11	56492	01553	1	98447	46
15	9 58 0	2 2 0	9. 42001	11	10. 57999	9. 43558	12	10. 56442	10. 01557	1	9. 98443	45
16	57 52	2 8	42047	12	57953	43607	13	56393	01560	1	98440	44
17	57 44	2 16	42093	13	57907	43657	14	56343	01564	1	98436	43
18	57 36	2 24	42140	14	57860	43707	15	56293	01567	1	98433	42
19	57 28	2 32	42186	14	57814	43756	16	56244	01571	1	98429	41
20	9 57 20	2 2 40	9. 42232	15	10. 57768	9. 43806	16	10. 56194	10. 01574	1	9. 98426	40
21	57 12	2 48	42278	16	57722	43855	17	56145	01578	1	98422	39
22	57 4	2 56	42324	17	57676	43905	18	56095	01581	1	98419	38
23	56 56	3 4	42370	17	57630	43954	19	56046	01585	1	98415	37
24	56 48	3 12	42416	18	57584	44004	20	55996	01588	1	98412	36
25	9 56 40	2 3 20	9. 42461	19	10. 57539	9. 44053	20	10. 55947	10. 01591	1	9. 98409	35
26	56 32	3 28	42507	20	57493	44102	21	55898	01595	2	98405	34
27	56 24	3 36	42553	21	57447	44151	22	55849	01598	2	98402	33
28	56 16	3 44	42599	21	57401	44201	23	55799	01602	2	98398	32
29	56 8	3 52	42644	22	57356	44250	24	55750	01605	2	98395	31
30	9 56 0	2 4 0	9. 42690	23	10. 57310	9. 44299	25	10. 55701	10. 01609	2	9. 98391	30
31	55 52	4 8	42735	24	57265	44348	25	55652	01612	2	98388	29
32	55 44	4 16	42781	24	57219	44397	26	55603	01616	2	98384	28
33	55 36	4 24	42826	25	57174	44446	27	55554	01619	2	98381	27
34	55 28	4 32	42872	26	57128	44495	28	55505	01623	2	98377	26
35	9 55 20	2 4 40	9. 42917	27	10. 57083	9. 44544	29	10. 55456	10. 01627	2	9. 98373	25
36	55 12	4 48	42962	27	57038	44592	29	55408	01630	2	98370	24
37	55 4	4 56	43008	28	56992	44641	30	55359	01634	2	98366	23
38	54 56	5 4	43053	29	56947	44690	31	55310	01637	2	98363	22
39	54 48	5 12	43098	30	56902	44738	32	55262	01641	2	98359	21
40	9 54 40	2 5 20	9. 43143	30	10. 56857	9. 44787	33	10. 55213	10. 01644	2	9. 98356	20
41	54 32	5 28	43188	31	56812	44836	34	55164	01648	2	98352	19
42	54 24	5 36	43233	32	56767	44884	34	55116	01651	2	98349	18
43	54 16	5 44	43278	33	56722	44933	35	55067	01655	3	98345	17
44	54 8	5 52	43323	33	56677	44981	36	55019	01658	3	98342	16
45	9 54 0	2 6 0	9. 43367	34	10. 56633	9. 45029	37	10. 54971	10. 01662	3	9. 98338	15
46	53 52	6 8	43412	35	56588	45078	38	54922	01666	3	98334	14
47	53 44	6 16	43457	36	56543	45126	38	54874	01669	3	98331	13
48	53 36	6 24	43502	36	56498	45174	39	54826	01673	3	98327	12
49	53 28	6 32	43546	37	56454	45222	40	54778	01676	3	98324	11
50	9 53 20	2 6 40	9. 43591	38	10. 56409	9. 45271	41	10. 54729	10. 01680	3	9. 98320	10
51	53 12	6 48	43635	39	56365	45319	42	54681	01683	3	98317	9
52	53 4	6 56	43680	39	56320	45367	43	54633	01687	3	98313	8
53	52 56	7 4	43724	40	56276	45415	43	54585	01691	3	98309	7
54	52 48	7 12	43769	41	56231	45463	44	54537	01694	3	98306	6
55	9 52 40	2 7 20	9. 43813	42	10. 56187	9. 45511	45	10. 54489	10. 01698	3	9. 98302	5
56	52 32	7 28	43857	43	56143	45559	46	54441	01701	3	98299	4
57	52 24	7 36	43901	43	56099	45606	47	54394	01705	3	98295	3
58	52 16	7 44	43946	44	56054	45654	47	54346	01709	3	98291	2
59	52 8	7 52	43990	45	56010	45702	48	54298	01712	3	98288	1
60	52 0	8 0	44034	46	55966	45750	49	54250	01716	4	98284	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
105°			A		A	B		B	C		C	74°

Seconds of time		1^s	2^s	3^s	4^s	5^s	6^s	7^s
Prop. parts of cols.	A	6	11	17	23	28	34	40
	B	6	12	18	25	31	37	43
	C	0	1	1	2	2	3	3

TABLE 44.

Log. Sines, Tangents, and Secants.

16°			A		A	B		B	C		C	163°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	9 52 0	2 8 0	9.44034	0	10.55966	9.45750	0	10.54250	10.01716	0	9.98284	60
1	51 52	8 8	44078	1	55922	45797	1	54203	01719	0	98281	59
2	51 44	8 16	44122	1	55878	45845	2	54155	01723	0	98277	58
3	51 36	8 24	44166	2	55834	45892	2	54108	01727	0	98273	57
4	51 28	8 32	44210	3	55790	45940	3	54060	01730	0	98270	56
5	9 51 20	2 8 40	9.44253	4	10.55747	9.45987	4	10.54013	10.01734	0	9.98266	55
6	51 12	8 48	44297	4	55703	46035	5	53965	01738	0	98262	54
7	51 4	8 56	44341	5	55659	46082	5	53918	01741	0	98259	53
8	50 56	9 4	44385	6	55615	46130	6	53870	01745	0	98255	52
9	50 48	9 12	44428	6	55572	46177	7	53823	01749	1	98251	51
10	9 50 40	2 9 20	9.44472	7	10.55528	9.46224	8	10.53776	10.01752	1	9.98248	50
11	50 32	9 28	44516	8	55484	46271	9	53729	01756	1	98244	49
12	50 24	9 36	44559	9	55441	46319	9	53681	01760	1	98240	48
13	50 16	9 44	44602	9	55398	46366	10	53634	01763	1	98237	47
14	50 8	9 52	44646	10	55354	46413	11	53587	01767	1	98233	46
15	9 50 0	2 10 0	9.44689	11	10.55311	9.46460	12	10.53540	10.01771	1	9.98229	45
16	49 52	10 8	44733	11	55267	46507	12	53493	01774	1	98226	44
17	49 44	10 16	44776	12	55224	46554	13	53446	01778	1	98222	43
18	49 36	10 24	44819	13	55181	46601	14	53399	01782	1	98218	42
19	49 28	10 32	44862	14	55138	46648	15	53352	01785	1	98215	41
20	9 49 20	2 10 40	9.44905	14	10.55095	9.46694	15	10.53306	10.01789	1	9.98211	40
21	49 12	10 48	44948	15	55052	46741	16	53259	01793	1	98207	39
22	49 4	10 56	44992	16	55008	46788	17	53212	01796	1	98204	38
23	48 56	11 4	45035	16	54965	46835	18	53165	01800	1	98200	37
24	48 48	11 12	45077	17	54923	46881	19	53119	01804	1	98196	36
25	9 48 40	2 11 20	9.45120	18	10.54880	9.46928	19	10.53072	10.01808	2	9.98192	35
26	48 32	11 28	45163	18	54837	46975	20	53025	01811	2	98189	34
27	48 24	11 36	45206	19	54794	47021	21	52979	01815	2	98185	33
28	48 16	11 44	45249	20	54751	47068	22	52932	01819	2	98181	32
29	48 8	11 52	45292	21	54708	47114	22	52886	01823	2	98177	31
30	9 48 0	2 12 0	9.45334	21	10.54666	9.47160	23	10.52840	10.01826	2	9.98174	30
31	47 52	12 8	45377	22	54623	47207	24	52793	01830	2	98170	29
32	47 44	12 16	45419	23	54581	47253	25	52747	01834	2	98166	28
33	47 36	12 24	45462	23	54538	47299	26	52701	01838	2	98162	27
34	47 28	12 32	45504	24	54496	47346	26	52654	01841	2	98159	26
35	9 47 20	2 12 40	9.45547	25	10.54453	9.47392	27	10.52608	10.01845	2	9.98155	25
36	47 12	12 48	45589	26	54411	47438	28	52562	01849	2	98151	24
37	47 4	12 56	45632	26	54368	47484	29	52516	01853	2	98147	23
38	46 56	13 4	45674	27	54326	47530	29	52470	01856	2	98144	22
39	46 48	13 12	45716	28	54284	47576	30	52424	01860	2	98140	21
40	9 46 40	2 13 20	9.45758	28	10.54242	9.47622	31	10.52378	10.01864	2	9.98136	20
41	46 32	13 28	45801	29	54199	47668	32	52332	01868	3	98132	19
42	46 24	13 36	45843	30	54157	47714	32	52286	01871	3	98129	18
43	46 16	13 44	45885	31	54115	47760	33	52240	01875	3	98125	17
44	46 8	13 52	45927	31	54073	47806	34	52194	01879	3	98121	16
45	9 46 0	2 14 0	9.45969	32	10.54031	9.47852	35	10.52148	10.01883	3	9.98117	15
46	45 52	14 8	46011	33	53989	47897	36	52103	01887	3	98113	14
47	45 44	14 16	46053	33	53947	47943	36	52057	01890	3	98110	13
48	45 36	14 24	46095	34	53905	47989	37	52011	01894	3	98106	12
49	45 28	14 32	46136	35	53864	48035	38	51965	01898	3	98102	11
50	9 45 20	2 14 40	9.46178	36	10.53822	9.48080	39	10.51920	10.01902	3	9.98098	10
51	45 12	14 48	46220	36	53780	48126	39	51874	01906	3	98094	9
52	45 4	14 56	46262	37	53738	48171	40	51829	01910	3	98090	8
53	44 56	15 4	46303	38	53697	48217	41	51783	01913	3	98087	7
54	44 48	15 12	46345	38	53655	48262	42	51738	01917	3	98083	6
55	9 44 40	2 15 20	9.46386	39	10.53614	9.48307	43	10.51693	10.01921	3	9.98079	5
56	44 32	15 28	46428	40	53572	48353	43	51647	01925	3	98075	4
57	44 24	15 36	46469	41	53531	48398	44	51602	01929	4	98071	3
58	44 16	15 44	46511	41	53489	48443	45	51557	01933	4	98067	2
59	44 8	15 52	46552	42	53448	48489	46	51511	01937	4	98063	1
60	44 0	16 0	46594	43	53406	48534	46	51466	01940	4	98060	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
106°			A		A	B		B	C		C	73°

Seconds of time		1ˢ	2ˢ	3ˢ	4ˢ	5ˢ	6ˢ	7ˢ
Prop. parts of cols.	A	5	11	16	21	27	32	37
	B	6	12	17	23	29	35	41
	C	0	1	1	2	2	3	3

TABLE 44.

Log. Sines, Tangents, and Secants.

17°			A		A	B		B	C		C	162°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	9 44 0	2 16 0	9.46594	0	10.53406	9.48534	0	10.51466	10.01940	0	9.98060	60
1	43 52	16 8	46635	1	53365	48579	1	51421	01944	0	98056	59
2	43 44	16 16	46676	1	53324	48624	1	51376	01948	0	98052	58
3	43 36	16 24	46717	2	53283	48669	2	51331	01952	0	98048	57
4	43 28	16 32	46758	3	53242	48714	3	51286	01956	0	98044	56
5	9 43 20	2 16 40	9.46800	3	10.53200	9.48759	4	10.51241	10.01960	0	9.98040	55
6	43 12	16 48	46841	4	53159	48804	4	51196	01964	0	98036	54
7	43 4	16 56	46882	5	53118	48849	5	51151	01968	0	98032	53
8	42 56	17 4	46923	5	53077	48894	6	51106	01971	1	98029	52
9	42 48	17 12	46964	6	53036	48939	7	51061	01975	1	98025	51
10	9 42 40	2 17 20	9.47005	7	10.52995	9.48984	7	10.51016	10.01979	1	9.98021	50
11	42 32	17 28	47045	7	52955	49029	8	50971	01983	1	98017	49
12	42 24	17 36	47086	8	52914	49073	9	50927	01987	1	98013	48
13	42 16	17 44	47127	9	52873	49118	10	50882	01991	1	98009	47
14	42 8	17 52	47168	9	52832	49163	10	50837	01995	1	98005	46
15	9 42 0	2 18 0	9.47209	10	10.52791	9.49207	11	10.50793	10.01999	1	9.98001	45
16	41 52	18 8	47249	11	52751	49252	12	50748	02003	1	97997	44
17	41 44	18 16	47290	11	52710	49296	12	50704	02007	1	97993	43
18	41 36	18 24	47330	12	52670	49341	13	50659	02011	1	97989	42
19	41 28	18 32	47371	13	52629	49385	14	50615	02014	1	97986	41
20	9 41 20	2 18 40	9.47411	13	10.52589	9.49430	15	10.50570	10.02018	1	9.97982	40
21	41 12	18 48	47452	14	52548	49474	15	50526	02022	1	97978	39
22	41 4	18 56	47492	15	52508	49519	16	50481	02026	1	97974	38
23	40 56	19 4	47533	15	52467	49563	17	50437	02030	2	97970	37
24	40 48	19 12	47573	16	52427	49607	18	50393	02034	2	97966	36
25	9 40 40	2 19 20	9.47613	17	10.52387	9.49652	18	10.50348	10.02038	2	9.97962	35
26	40 32	19 28	47654	17	52346	49696	19	50304	02042	2	97958	34
27	40 24	19 36	47694	18	52306	49740	20	50260	02046	2	97954	33
28	40 16	19 44	47734	19	52266	49784	21	50216	02050	2	97950	32
29	40 8	19 52	47774	19	52226	49828	21	50172	02054	2	97946	31
30	9 40 0	2 20 0	9.47814	20	10.52186	9.49872	22	10.50128	10.02058	2	9.97942	30
31	39 52	20 8	47854	21	52146	49916	23	50084	02062	2	97938	29
32	39 44	20 16	47894	21	52106	49960	24	50040	02066	2	97934	28
33	39 36	20 24	47934	22	52066	50004	24	49996	02070	2	97930	27
34	39 28	20 32	47974	23	52026	50048	25	49952	02074	2	97926	26
35	9 39 20	2 20 40	9.48014	23	10.51986	9.50092	26	10.49908	10.02078	2	9.97922	25
36	39 12	20 48	48054	24	51946	50136	26	49864	02082	2	97918	24
37	39 4	20 56	48094	25	51906	50180	27	49820	02086	2	97914	23
38	38 56	21 4	48133	25	51867	50223	28	49777	02090	3	97910	22
39	38 48	21 12	48173	26	51827	50267	29	49733	02094	3	97906	21
40	9 38 40	2 21 20	9.48213	27	10.51787	9.50311	29	10.49689	10.02098	3	9.97902	20
41	38 32	21 28	48252	27	51748	50355	30	49645	02102	3	97898	19
42	38 24	21 36	48292	28	51708	50398	31	49602	02106	3	97894	18
43	38 16	21 44	48332	29	51668	50442	32	49558	02110	3	97890	17
44	38 8	21 52	48371	29	51629	50485	32	49515	02114	3	97886	16
45	9 38 0	2 22 0	9.48411	30	10.51589	9.50529	33	10.49471	10.02118	3	9.97882	15
46	37 52	22 8	48450	31	51550	50572	34	49428	02122	3	97878	14
47	37 44	22 16	48490	31	51510	50616	35	49384	02126	3	97874	13
48	37 36	22 24	48529	32	51471	50659	35	49341	02130	3	97870	12
49	37 28	22 32	48568	33	51432	50703	36	49297	02134	3	97866	11
50	9 37 20	2 22 40	9.48607	33	10.51393	9.50746	37	10.49254	10.02139	3	9.97861	10
51	37 12	22 48	48647	34	51353	50789	37	49211	02143	3	97857	9
52	37 4	22 56	48686	35	51314	50833	38	49167	02147	3	97853	8
53	36 56	23 4	48725	35	51275	50876	39	49124	02151	4	97849	7
54	36 48	23 12	48764	36	51236	50919	40	49081	02155	4	97845	6
55	9 36 40	2 23 20	9.48803	37	10.51197	9.50962	40	10.49038	10.02159	4	9.97841	5
56	36 32	23 28	48842	37	51158	51005	41	48995	02163	4	97837	4
57	36 24	23 36	48881	38	51119	51048	42	48952	02167	4	97833	3
58	36 16	23 44	48920	39	51080	51092	43	48908	02171	4	97829	2
59	36 8	23 52	48959	39	51041	51135	43	48865	02175	4	97825	1
60	36 0	24 0	48998	40	51002	51178	44	48822	02179	4	97821	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
107°			A		A	B		B	C		C	72°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	5	10	15	20	25	30	35
	B	6	11	17	22	28	33	39
	C	0	1	1	2	2	3	3

TABLE 44.

Log. Sines, Tangents, and Secants.

18°			A		A	B		B	C		C	161°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	9 36 0	2 24 0	9.48998	0	10.51002	9.51178	0	10.48822	10.02179	0	9.97821	60
1	35 52	24 8	49037	1	50963	51221	1	48779	02183	0	97817	59
2	35 44	24 16	49076	1	50924	51264	1	48736	02188	0	97812	58
3	35 36	24 24	49115	2	50885	51306	2	48694	02192	0	97808	57
4	35 28	24 32	49153	3	50847	51349	3	48651	02196	0	97804	56
5	9 35 20	2 24 40	9.49192	3	10.50808	9.51392	3	10.48608	10.02200	0	9.97800	55
6	35 12	24 48	49231	4	50769	51435	4	48565	02204	0	97796	54
7	35 4	24 56	49269	4	50731	51478	5	48522	02208	0	97792	53
8	34 56	25 4	49308	5	50692	51520	6	48480	02212	1	97788	52
9	34 48	25 12	49347	6	50653	51563	6	48437	02216	1	97784	51
10	9 34 40	2 25 20	9.49385	6	10.50615	9.51606	7	10.48394	10.02221	1	9.97779	50
11	34 32	25 28	49424	7	50576	51648	8	48352	02225	1	97775	49
12	34 24	25 36	49462	8	50538	51691	8	48309	02229	1	97771	48
13	34 16	25 44	49500	8	50500	51734	9	48266	02233	1	97767	47
14	34 8	25 52	49539	9	50461	51776	10	48224	02237	1	97763	46
15	9 34 0	2 26 0	9.49577	9	10.50423	9.51819	10	10.48181	10.02241	1	9.97759	45
16	33 52	26 8	49615	10	50385	51861	11	48139	02246	1	97754	44
17	33 44	26 16	49654	11	50346	51903	12	48097	02250	1	97750	43
18	33 36	26 24	49692	11	50308	51946	13	48054	02254	1	97746	42
19	33 28	26 32	49730	12	50270	51988	13	48012	02258	1	97742	41
20	9 33 20	2 26 40	9.49768	13	10.50232	9.52031	14	10.47969	10.02262	1	9.97738	40
21	33 12	26 48	49806	13	50194	52073	15	47927	02266	1	97734	39
22	33 4	26 56	49844	14	50156	52115	15	47885	02271	2	97729	38
23	32 56	27 4	49882	14	50118	52157	16	47843	02275	2	97725	37
24	32 48	27 12	49920	15	50080	52200	17	47800	02279	2	97721	36
25	9 32 40	2 27 20	9.49958	16	10.50042	9.52242	17	10.47758	10.02283	2	9.97717	35
26	32 32	27 28	49996	16	50004	52284	18	47716	02287	2	97713	34
27	32 24	27 36	50034	17	49966	52326	19	47674	02292	2	97708	33
28	32 16	27 44	50072	18	49928	52368	20	47632	02296	2	97704	32
29	32 8	27 52	50110	18	49890	52410	20	47590	02300	2	97700	31
30	9 32 0	2 28 0	9.50148	19	10.49852	9.52452	21	10.47548	10.02304	2	9.97696	30
31	31 52	28 8	50185	20	49815	52494	22	47506	02309	2	97691	29
32	31 44	28 16	50223	20	49777	52536	22	47464	02313	2	97687	28
33	31 36	28 24	50261	21	49739	52578	23	47422	02317	2	97683	27
34	31 28	28 32	50298	21	49702	52620	24	47380	02321	2	97679	26
35	9 31 20	2 28 40	9.50336	22	10.49664	9.52661	24	10.47339	10.02326	2	9.97674	25
36	31 12	28 48	50374	23	49626	52703	25	47297	02330	3	97670	24
37	31 4	28 56	50411	23	49589	52745	26	47255	02334	3	97666	23
38	30 56	29 4	50449	24	49551	52787	27	47213	02338	3	97662	22
39	30 48	29 12	50486	25	49514	52829	27	47171	02343	3	97657	21
40	9 30 40	2 29 20	9.50523	25	10.49477	9.52870	28	10.47130	10.02347	3	9.97653	20
41	30 32	29 28	50561	26	49439	52912	29	47088	02351	3	97649	19
42	30 24	29 36	50598	26	49402	52953	29	47047	02355	3	97645	18
43	30 16	29 44	50635	27	49365	52995	30	47005	02360	3	97640	17
44	30 8	29 52	50673	28	49327	53037	31	46963	02364	3	97636	16
45	9 30 0	2 30 0	9.50710	28	10.49290	9.53078	31	10.46922	10.02368	3	9.97632	15
46	29 52	30 8	50747	29	49253	53120	32	46880	02372	3	97628	14
47	29 44	30 16	50784	30	49216	53161	33	46839	02377	3	97623	13
48	29 36	30 24	50821	30	49179	53202	34	46798	02381	3	97619	12
49	29 28	30 32	50858	31	49142	53244	34	46756	02385	3	97615	11
50	9 29 20	2 30 40	9.50896	31	10.49104	9.53285	35	10.46715	10.02390	4	9.97610	10
51	29 12	30 48	50933	32	49067	53327	36	46673	02394	4	97606	9
52	29 4	30 56	50970	33	49030	53368	36	46632	02398	4	97602	8
53	28 56	31 4	51007	33	48993	53409	37	46591	02403	4	97597	7
54	28 48	31 12	51043	34	48957	53450	38	46550	02407	4	97593	6
55	9 28 40	2 31 20	9.51080	35	10.48920	9.53492	38	10.46508	10.02411	4	9.97589	5
56	28 32	31 28	51117	35	48883	53533	39	46467	02416	4	97584	4
57	28 24	31 36	51154	36	48846	53574	40	46426	02420	4	97580	3
58	28 16	31 44	51191	37	48809	53615	41	46385	02424	4	97576	2
59	28 8	31 52	51227	37	48773	53656	41	46344	02429	4	97571	1
60	28 0	32 0	51264	38	48736	53697	42	46303	02433	4	97567	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
108°			A		A	B		B	C		C	71°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	5	9	14	19	24	28	33
	B	5	10	16	21	26	31	37
	C	1	1	2	2	3	3	4

Log. Sines, Tangents, and Secants.

19°			A		A	B		B	C		C	160°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	9 28 0	2 32 0	9.51264	0	10.48736	9.53697	0	10.46303	10.02433	0	9.97567	60
1	27 52	32 8	51301	1	48699	53738	1	46262	02437	0	97563	59
2	27 44	32 16	51338	1	48662	53779	1	46221	02442	0	97558	58
3	27 36	32 24	51374	2	48626	53820	2	46180	02446	0	97554	57
4	27 28	32 32	51411	2	48589	53861	3	46139	02450	0	97550	56
5	9 27 20	2 32 40	9.51447	3	10.48553	9.53902	3	10.46098	10.02455	0	9.97545	55
6	27 12	32 48	51484	4	48516	53943	4	46057	02459	0	97541	54
7	27 4	32 56	51520	4	48480	53984	5	46016	02464	1	97536	53
8	26 56	33 4	51557	5	48443	54025	5	45975	02468	1	97532	52
9	26 48	33 12	51593	5	48407	54065	6	45935	02472	1	97528	51
10	9 26 40	2 33 20	9.51629	6	10.48371	9.54106	7	10.45894	10.02477	1	9.97523	50
11	26 32	33 28	51666	7	48334	54147	7	45853	02481	1	97519	49
12	26 24	33 36	51702	7	48298	54187	8	45813	02485	1	97515	48
13	26 16	33 44	51738	8	48262	54228	9	45772	02490	1	97510	47
14	26 8	33 52	51774	8	48226	54269	9	45731	02494	1	97506	46
15	9 26 0	2 34 0	9.51811	9	10.48189	9.54309	10	10.45691	10.02499	1	9.97501	45
16	25 52	34 8	51847	10	48153	54350	11	45650	02503	1	97497	44
17	25 44	34 16	51883	10	48117	54390	11	45610	02508	1	97492	43
18	25 36	34 24	51919	11	48081	54431	12	45569	02512	1	97488	42
19	25 28	34 32	51955	11	48045	54471	13	45529	02516	1	97484	41
20	9 25 20	2 34 40	9.51991	12	10.48009	9.54512	13	10.45488	10.02521	1	9.97479	40
21	25 12	34 48	52027	12	47973	54552	14	45448	02525	2	97475	39
22	25 4	34 56	52063	13	47937	54593	15	45407	02530	2	97470	38
23	24 56	35 4	52099	14	47901	54633	15	45367	02534	2	97466	37
24	24 48	35 12	52135	14	47865	54673	16	45327	02539	2	97461	36
25	9 24 40	2 35 20	9.52171	15	10.47829	9.54714	17	10.45286	10.02543	2	9.97457	35
26	24 32	35 28	52207	15	47793	54754	17	45246	02547	2	97453	34
27	24 24	35 36	52242	16	47758	54794	18	45206	02552	2	97448	33
28	24 16	35 44	52278	17	47722	54835	19	45165	02556	2	97444	32
29	24 8	35 52	52314	17	47686	54875	19	45125	02561	2	97439	31
30	9 24 0	2 36 0	9.52350	18	10.47650	9.54915	20	10.45085	10.02565	2	9.97435	30
31	23 52	36 8	52385	18	47615	54955	21	45045	02570	2	97430	29
32	23 44	36 16	52421	19	47579	54995	21	45005	02574	2	97426	28
33	23 36	36 24	52456	20	47544	55035	22	44965	02579	2	97421	27
34	23 28	36 32	52492	20	47508	55075	23	44925	02583	3	97417	26
35	9 23 20	2 36 40	9.52527	21	10.47473	9.55115	23	10.44885	10.02588	3	9.97412	25
36	23 12	36 48	52563	21	47437	55155	24	44845	02592	3	97408	24
37	23 4	36 56	52598	22	47402	55195	25	44805	02597	3	97403	23
38	22 56	37 4	52634	23	47366	55235	25	44765	02601	3	97399	22
39	22 48	37 12	52669	23	47331	55275	26	44725	02606	3	97394	21
40	9 22 40	2 37 20	9.52705	24	10.47295	9.55315	27	10.44685	10.02610	3	9.97390	20
41	22 32	37 28	52740	24	47260	55355	27	44645	02615	3	97385	19
42	22 24	37 36	52775	25	47225	55395	28	44605	02619	3	97381	18
43	22 16	37 44	52811	26	47189	55434	29	44566	02624	3	97376	17
44	22 8	37 52	52846	26	47154	55474	29	44526	02628	3	97372	16
45	9 22 0	2 38 0	9.52881	27	10.47119	9.55514	30	10.44486	10.02633	3	9.97367	15
46	21 52	38 8	52916	27	47084	55554	31	44446	02637	3	97363	14
47	21 44	38 16	52951	28	47049	55593	31	44407	02642	3	97358	13
48	21 36	38 24	52986	29	47014	55633	32	44367	02647	4	97353	12
49	21 28	38 32	53021	29	46979	55673	33	44327	02651	4	97349	11
50	9 21 20	2 38 40	9.53056	30	10.46944	9.55712	33	10.44288	10.02656	4	9.97344	10
51	21 12	38 48	53092	30	46908	55752	34	44248	02660	4	97340	9
52	21 4	38 56	53126	31	46874	55791	35	44209	02665	4	97335	8
53	20 56	39 4	53161	32	46839	55831	35	44169	02669	4	97331	7
54	20 48	39 12	53196	32	46804	55870	36	44130	02674	4	97326	6
55	9 20 40	2 39 20	9.53231	33	10.46769	9.55910	37	10.44090	10.02678	4	9.97322	5
56	20 32	39 28	53266	33	46734	55949	37	44051	02683	4	97317	4
57	20 24	39 36	53301	34	46699	55989	38	44011	02688	4	97312	3
58	20 16	39 44	53336	34	46664	56028	39	43972	02692	4	97308	2
59	20 8	39 52	53370	35	46630	56067	39	43933	02697	4	97303	1
60	20 0	40 0	53405	36	46595	56107	40	43893	02701	4	97299	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
109°			A		A	B		B	C		C	70°

Seconds of time	1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols. A	4	9	13	18	22	27	31
Prop. parts of cols. B	5	10	15	20	25	30	35
Prop. parts of cols. C	1	1	2	2	3	3	4

TABLE 44.

Log. Sines, Tangents, and Secants.

20°			A		A	B		B	C		C	159°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	9 20 0	2 40 0	9.53405	0	10.46595	9.56107	0	10.43893	10.02701	0	9.97299	60
1	19 52	40 8	53440	1	46560	56146	1	43854	02706	0	97294	59
2	19 44	40 16	53475	1	46525	56185	1	43815	02711	0	97289	58
3	19 36	40 24	53509	2	46491	56224	2	43776	02715	0	97285	57
4	19 28	40 32	53544	2	46456	56264	3	43736	02720	0	97280	56
5	9 19 20	2 40 40	9.53578	3	10.46422	9.56303	3	10.43697	10.02724	0	9.97276	55
6	19 12	40 48	53613	3	46387	56342	4	43658	02729	0	97271	54
7	19 4	40 56	53647	4	46353	56381	4	43619	02734	1	97266	53
8	18 56	41 4	53682	5	46318	56420	5	43580	02738	1	97262	52
9	18 48	41 12	53716	5	46284	56459	6	43541	02743	1	97257	51
10	9 18 40	2 41 20	9.53751	6	10.46249	9.56498	6	10.43502	10.02748	1	9.97252	50
11	18 32	41 28	53785	6	46215	56537	7	43463	02752	1	97248	49
12	18 24	41 36	53819	7	46181	56576	8	43424	02757	1	97243	48
13	18 16	41 44	53854	7	46146	56615	8	43385	02762	1	97238	47
14	18 8	41 52	53888	8	46112	56654	9	43346	02766	1	97234	46
15	9 18 0	2 42 0	9.53922	8	10.46078	9.56693	10	10.43307	10.02771	1	9.97229	45
16	17 52	42 8	53957	9	46043	56732	10	43268	02776	1	97224	44
17	17 44	42 16	53991	10	46009	56771	11	43229	02780	1	97220	43
18	17 36	42 24	54025	10	45975	56810	12	43190	02785	1	97215	42
19	17 28	42 32	54059	11	45941	56849	12	43151	02790	1	97210	41
20	9 17 20	2 42 40	9.54093	11	10.45907	9.56887	13	10.43113	10.02794	2	9.97206	40
21	17 12	42 48	54127	12	45873	56926	13	43074	02799	2	97201	39
22	17 4	42 56	54161	12	45839	56965	14	43035	02804	2	97196	38
23	16 56	43 4	54195	13	45805	57004	15	42996	02808	2	97192	37
24	16 48	43 12	54229	14	45771	57042	15	42958	02813	2	97187	36
25	9 16 40	2 43 20	9.54263	14	10.45737	9.57081	16	10.42919	10.02818	2	9.97182	35
26	16 32	43 28	54297	15	45703	57120	17	42880	02822	2	97178	34
27	16 24	43 36	54331	15	45669	57158	17	42842	02827	2	97173	33
28	16 16	43 44	54365	16	45635	57197	18	42803	02832	2	97168	32
29	16 8	43 52	54399	16	45601	57235	19	42765	02837	2	97163	31
30	9 16 0	2 44 0	9.54433	17	10.45567	9.57274	19	10.42726	10.02841	2	9.97159	30
31	15 52	44 8	54466	17	45534	57312	20	42688	02846	2	97154	29
32	15 44	44 16	54500	18	45500	57351	21	42649	02851	3	97149	28
33	15 36	44 24	54534	19	45466	57389	21	42611	02855	3	97145	27
34	15 28	44 32	54567	19	45433	57428	22	42572	02860	3	97140	26
35	9 15 20	2 44 40	9.54601	20	10.45399	9.57466	22	10.42534	10.02865	3	9.97135	25
36	15 12	44 48	54635	20	45365	57504	23	42496	02870	3	97130	24
37	15 4	44 56	54668	21	45332	57543	24	42457	02874	3	97126	23
38	14 56	45 4	54702	21	45298	57581	24	42419	02879	3	97121	22
39	14 48	45 12	54735	22	45265	57619	25	42381	02884	3	97116	21
40	9 14 40	2 45 20	9.54769	23	10.45231	9.57658	26	10.42342	10.02889	3	9.97111	20
41	14 32	45 28	54802	23	45198	57696	26	42304	02893	3	97107	19
42	14 24	45 36	54836	24	45164	57734	27	42266	02898	3	97102	18
43	14 16	45 44	54869	24	45131	57772	28	42228	02903	3	97097	17
44	14 8	45 52	54903	25	45097	57810	28	42190	02908	3	97092	16
45	9 14 0	2 46 0	9.54936	25	10.45064	9.57849	29	10.42151	10.02913	4	9.97087	15
46	13 52	46 8	54969	26	45031	57887	30	42113	02917	4	97083	14
47	13 44	46 16	55003	26	44997	57925	30	42075	02922	4	97078	13
48	13 36	46 24	55036	27	44964	57963	31	42037	02927	4	97073	12
49	13 28	46 32	55069	28	44931	58001	31	41999	02932	4	97068	11
50	9 13 20	2 46 40	9.55102	28	10.44898	9.58039	32	10.41961	10.02937	4	9.97063	10
51	13 12	46 48	55136	29	44864	58077	33	41923	02941	4	97059	9
52	13 4	46 56	55169	29	44831	58115	33	41885	02946	4	97054	8
53	12 56	47 4	55202	30	44798	58153	34	41847	02951	4	97049	7
54	12 48	47 12	55235	30	44765	58191	35	41809	02956	4	97044	6
55	9 12 40	2 47 20	9.55268	31	10.44732	9.58229	35	10.41771	10.02961	4	9.97039	5
56	12 32	47 28	55301	32	44699	58267	36	41733	02965	4	97035	4
57	12 24	47 36	55334	32	44666	58304	37	41696	02970	4	97030	3
58	12 16	47 44	55367	33	44633	58342	37	41658	02975	5	97025	2
59	12 8	47 52	55400	33	44600	58380	38	41620	02980	5	97020	1
60	12 0	48 0	55433	34	44567	58418	39	41582	02985	5	97015	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
110°			A		A	B		B	C		C	69°

Seconds of time.......		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	4	8	13	17	21	25	30
	B	5	10	14	19	24	29	34
	C	1	1	2	2	3	4	4

TABLE 44.

Log. Sines, Tangents, and Secants.

21°			A		A	B		B	C		C	158°
M.	Hour A.M.	Hour P.M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	9 12 0	2 48 0	9.55433	0	10.44567	9.58418	0	10.41582	10.02985	0	9.97015	60
1	11 52	48 8	55466	1	44534	58455	1	41545	02990	0	97010	59
2	11 44	48 16	55499	1	44501	58493	1	41507	02995	0	97005	58
3	11 36	48 24	55532	2	44468	58531	2	41469	02999	0	97001	57
4	11 28	48 32	55564	2	44436	58569	2	41431	03004	0	96996	56
5	9 11 20	2 48 40	9.55597	3	10.44403	9.58606	3	10.41394	10.03009	0	9.96991	55
6	11 12	48 48	55630	3	44370	58644	4	41356	03014	0	96986	54
7	11 4	48 56	55663	4	44337	58681	4	41319	03019	1	96981	53
8	10 56	49 4	55695	4	44305	58719	5	41281	03024	1	96976	52
9	10 48	49 12	55728	5	44272	58757	6	41243	03029	1	96971	51
10	9 10 40	2 49 20	9.55761	5	10.44239	9.58794	6	10.41206	10.03034	1	9.96966	50
11	10 32	49 28	55793	6	44207	58832	7	41168	03038	1	96962	49
12	10 24	49 36	55826	6	44174	58869	7	41131	03043	1	96957	48
13	10 16	49 44	55858	7	44142	58907	8	41093	03048	1	96952	47
14	10 8	49 52	55891	7	44109	58944	9	41056	03053	1	96947	46
15	9 10 0	2 50 0	9.55923	8	10.44077	9.58981	9	10.41019	10.03058	1	9.96942	45
16	9 52	50 8	55956	9	44044	59019	10	40981	03063	1	96937	44
17	9 44	50 16	55988	9	44012	59056	10	40944	03068	1	96932	43
18	9 36	50 24	56021	10	43979	59094	11	40906	03073	1	96927	42
19	9 28	50 32	56053	10	43947	59131	12	40869	03078	2	96922	41
20	9 9 20	2 50 40	9.56085	11	10.43915	9.59168	12	10.40832	10.03083	2	9.96917	40
21	9 12	50 48	56118	11	43882	59205	13	40795	03088	2	96912	39
22	9 4	50 56	56150	12	43850	59243	14	40757	03093	2	96907	38
23	8 56	51 4	56182	12	43818	59280	14	40720	03097	2	96903	37
24	8 48	51 12	56215	13	43785	59317	15	40683	03102	2	96898	36
25	9 8 40	2 51 20	9.56247	13	10.43753	9.59354	15	10.40646	10.03107	2	9.96893	35
26	8 32	51 28	56279	14	43721	59391	16	40609	03112	2	96888	34
27	8 24	51 36	56311	14	43689	59429	17	40571	03117	2	96883	33
28	8 16	51 44	56343	15	43657	59466	17	40534	03122	2	96878	32
29	8 8	51 52	56375	16	43625	59503	18	40497	03127	2	96873	31
30	9 8 0	2 52 0	9.56408	16	10.43592	9.59540	19	10.40460	10.03132	2	9.96868	30
31	7 52	52 8	56440	17	43560	59577	19	40423	03137	3	96863	29
32	7 44	52 16	56472	17	43528	59614	20	40386	03142	3	96858	28
33	7 36	52 24	56504	18	43496	59651	20	40349	03147	3	96853	27
34	7 28	52 32	56536	18	43464	59688	21	40312	03152	3	96848	26
35	9 7 20	2 52 40	9.56568	19	10.43432	9.59725	22	10.40275	10.03157	3	9.96843	25
36	7 12	52 48	56599	19	43401	59762	22	40238	03162	3	96838	24
37	7 4	52 56	56631	20	43369	59799	23	40201	03167	3	96833	23
38	6 56	53 4	56663	20	43337	59835	23	40165	03172	3	96828	22
39	6 48	53 12	56695	21	43305	59872	24	40128	03177	3	96823	21
40	9 6 40	2 53 20	9.56727	21	10.43273	9.59909	25	10.40091	10.03182	3	9.96818	20
41	6 32	53 28	56759	22	43241	59946	25	40054	03187	3	96813	19
42	6 24	53 36	56790	22	43210	59983	26	40017	03192	3	96808	18
43	6 16	53 44	56822	23	43178	60019	27	39981	03197	4	96803	17
44	6 8	53 52	56854	24	43146	60056	27	39944	03202	4	96798	16
45	9 6 0	2 54 0	9.56886	24	10.43114	9.60093	28	10.39907	10.03207	4	9.96793	15
46	5 52	54 8	56917	25	43083	60130	28	39870	03212	4	96788	14
47	5 44	54 16	56949	25	43051	60166	29	39834	03217	4	96783	13
48	5 36	54 24	56980	26	43020	60203	30	39797	03222	4	96778	12
49	5 28	54 32	57012	26	42988	60240	30	39760	03228	4	96772	11
50	9 5 20	2 54 40	9.57044	27	10.42956	9.60276	31	10.39724	10.03233	4	9.96767	10
51	5 12	54 48	57075	27	42925	60313	31	39687	03238	4	96762	9
52	5 4	54 56	57107	28	42893	60349	32	39651	03243	4	96757	8
53	4 56	55 4	57138	28	42862	60386	33	39614	03248	4	96752	7
54	4 48	55 12	57169	29	42831	60422	33	39578	03253	4	96747	6
55	9 4 40	2 55 20	9.57201	29	10.42799	9.60459	34	10.39541	10.03258	5	9.96742	5
56	4 32	55 28	57232	30	42768	60495	35	39505	03263	5	96737	4
57	4 24	55 36	57264	30	42736	60532	35	39468	03268	5	96732	3
58	4 16	55 44	57295	31	42705	60568	36	39432	03273	5	96727	2
59	4 8	55 52	57326	32	42674	60605	36	39395	03278	5	96722	1
60	4 0	56 0	57358	32	42642	60641	37	39359	03283	5	96717	0
M.	Hour P.M.	Hour A.M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
111°			A		A	B		B	C		C	68°

Second of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	4	8	12	16	20	24	28
	B	5	9	14	19	23	28	32
	C	1	1	2	2	3	4	4

TABLE 44.

Log. Sines, Tangents, and Secants.

22°			A		A	B		B	C		C	157°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	9 4 0	2 56 0	9.57358	0	10.42642	9.60641	0	10.39359	10.03283	0	9.96717	60
1	3 52	56 8	57389	1	42611	60677	1	39323	03289	0	96711	59
2	3 44	56 16	57420	1	42580	60714	1	39286	03294	0	96706	58
3	3 36	56 24	57451	2	42549	60750	2	39250	03299	0	96701	57
4	3 28	56 32	57482	2	42518	60786	2	39214	03304	0	96696	56
5	9 3 20	2 56 40	9.57514	3	10.42486	9.60823	3	10.39177	10.03309	0	9.96691	55
6	3 12	56 48	57545	3	42455	60859	4	39141	03314	1	96686	54
7	3 4	56 56	57576	4	42424	60895	4	39105	03319	1	96681	53
8	2 56	57 4	57607	4	42393	60931	5	39069	03324	1	96676	52
9	2 48	57 12	57638	5	42362	60967	5	39033	03330	1	96670	51
10	9 2 40	2 57 20	9.57669	5	10.42331	9.61004	6	10.38996	10.03335	1	9.96665	50
11	2 32	57 28	57700	6	42300	61040	7	38960	03340	1	96660	49
12	2 24	57 36	57731	6	42269	61076	7	38924	03345	1	96655	48
13	2 16	57 44	57762	7	42238	61112	8	38888	03350	1	96650	47
14	2 8	57 52	57793	7	42207	61148	8	38852	03355	1	96645	46
15	9 2 0	2 58 0	9.57824	8	10.42176	9.61184	9	10.38816	10.03360	1	9.96640	45
16	1 52	58 8	57855	8	42145	61220	10	38780	03366	1	96634	44
17	1 44	58 16	57885	9	42115	61256	10	38744	03371	1	96629	43
18	1 36	58 24	57916	9	42084	61292	11	38708	03376	2	96624	42
19	1 28	58 32	57947	10	42053	61328	11	38672	03381	2	96619	41
20	9 1 20	2 58 40	9.57978	10	10.42022	9.61364	12	10.38636	10.03386	2	9.96614	40
21	1 12	58 48	58008	11	41992	61400	13	38600	03392	2	96608	39
22	1 4	58 56	58039	11	41961	61436	13	38564	03397	2	96603	38
23	0 56	59 4	58070	12	41930	61472	14	38528	03402	2	96598	37
24	0 48	59 12	58101	12	41899	61508	14	38492	03407	2	96593	36
25	9 0 40	2 59 20	9.58131	13	10.41869	9.61544	15	10.38456	10.03412	2	9.96588	35
26	0 32	59 28	58162	13	41838	61579	15	38421	03418	2	96582	34
27	0 24	59 36	58192	14	41808	61615	16	38385	03423	2	96577	33
28	0 16	59 44	58223	14	41777	61651	17	38349	03428	2	96572	32
29	0 8	59 52	58253	15	41747	61687	17	38313	03433	3	96567	31
30	9 0 0	3 0 0	9.58284	15	10.41716	9.61722	18	10.38278	10.03438	3	9.96562	30
31	8 59 52	0 8	58314	16	41686	61758	18	38242	03444	3	96556	29
32	59 44	0 16	58345	16	41655	61794	19	38206	03449	3	96551	28
33	59 36	0 24	58375	17	41625	61830	20	38170	03454	3	96546	27
34	59 28	0 32	58406	17	41594	61865	20	38135	03459	3	96541	26
35	8 59 20	3 0 40	9.58436	18	10.41564	9.61901	21	10.38099	10.03465	3	9.96535	25
36	59 12	0 48	58467	18	41533	61936	21	38064	03470	3	96530	24
37	59 4	0 56	58497	19	41503	61972	22	38028	03475	3	96525	23
38	58 56	1 4	58527	19	41473	62008	23	37992	03480	3	96520	22
39	58 48	1 12	58557	20	41443	62043	23	37957	03486	3	96514	21
40	8 58 40	3 1 20	9.58588	20	10.41412	9.62079	24	10.37921	10.03491	3	9.96509	20
41	58 32	1 28	58618	21	41382	62114	24	37886	03496	4	96504	19
42	58 24	1 36	58648	21	41352	62150	25	37850	03502	4	96498	18
43	58 16	1 44	58678	22	41322	62185	26	37815	03507	4	96493	17
44	58 8	1 52	58709	22	41291	62221	26	37779	03512	4	96488	16
45	8 58 0	3 2 0	9.58739	23	10.41261	9.62256	27	10.37744	10.03517	4	9.96483	15
46	57 52	2 8	58769	23	41231	62292	27	37708	03523	4	96477	14
47	57 44	2 16	58799	24	41201	62327	28	37673	03528	4	96472	13
48	57 36	2 24	58829	24	41171	62362	29	37638	03533	4	96467	12
49	57 28	2 32	58859	25	41141	62398	29	37602	03539	4	96461	11
50	8 57 20	3 2 40	9.58889	25	10.41111	9.62433	30	10.37567	10.03544	4	9.96456	10
51	57 12	2 48	58919	26	41081	62468	30	37532	03549	4	96451	9
52	57 4	2 56	58949	26	41051	62504	31	37496	03555	5	96445	8
53	56 56	3 4	58979	27	41021	62539	32	37461	03560	5	96440	7
54	56 48	3 12	59009	27	40991	62574	32	37426	03565	5	96435	6
55	8 56 40	3 3 20	9.59039	28	10.40961	9.62609	33	10.37391	10.03571	5	9.96429	5
56	56 32	3 28	59069	28	40931	62645	33	37355	03576	5	96424	4
57	56 24	3 36	59098	29	40902	62680	34	37320	03581	5	96419	3
58	56 16	3 44	59128	29	40872	62715	35	37285	03587	5	96413	2
59	56 8	3 52	59158	30	40842	62750	35	37250	03592	5	96408	1
60	56 0	4 0	59188	31	40812	62785	36	37215	03597	5	96403	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
112°			A		A	B		B	C		C	67°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	4	8	11	15	19	23	27
	B	4	9	13	18	22	27	31
	C	1	1	2	3	3	4	5

Log. Sines, Tangents, and Secants.

23°			A		A	B		B	C		C	156°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	8 56 0	3 4 0	9.59188	0	10.40812	9.62785	0	10.37215	10.03597	0	9.96403	60
1	55 52	4 8	59218	0	40782	62820	1	37180	03603	0	96397	59
2	55 44	4 16	59247	1	40753	62855	1	37145	03608	0	96392	58
3	55 36	4 24	59277	1	40723	62890	2	37110	03613	0	96387	57
4	55 28	4 32	59307	2	40693	62926	2	37074	03619	0	96381	56
5	8 55 20	3 4 40	9.59336	2	10.40664	9.62961	3	10.37039	10.03624	0	9.96376	55
6	55 12	4 48	59366	3	40634	62996	3	37004	03630	1	96370	54
7	55 4	4 56	59396	3	40604	63031	4	36969	03635	1	96365	53
8	54 56	5 4	59425	4	40575	63066	5	36934	03640	1	96360	52
9	54 48	5 12	59455	4	40545	63101	5	36899	03646	1	96354	51
10	8 54 40	3 5 20	9.59484	5	10.40516	9.63135	6	10.36865	10.03651	1	9.96349	50
11	54 32	5 28	59514	5	40486	63170	6	36830	03657	1	96343	49
12	54 24	5 36	59543	6	40457	63205	7	36795	03662	1	96338	48
13	54 16	5 44	59573	6	40427	63240	7	36760	03667	1	96333	47
14	54 8	5 52	59602	7	40398	63275	8	36725	03673	1	96327	46
15	8 54 0	3 6 0	9.59632	7	10.40368	9.63310	9	10.36690	10.03678	1	9.96322	45
16	53 52	6 8	59661	8	40339	63345	9	36655	03684	1	96316	44
17	53 44	6 16	59690	8	40310	63379	10	36621	03689	2	96311	43
18	53 36	6 24	59720	9	40280	63414	10	36586	03695	2	96305	42
19	53 28	6 32	59749	9	40251	63449	11	36551	03700	2	96300	41
20	8 53 20	3 6 40	9.59778	10	10.40222	9.63484	12	10.36516	10.03706	2	9.96294	40
21	53 12	6 48	59808	10	40192	63519	12	36481	03711	2	96289	39
22	53 4	6 56	59837	11	40163	63553	13	36447	03716	2	96284	38
23	52 56	7 4	59866	11	40134	63588	13	36412	03722	2	96278	37
24	52 48	7 12	59895	12	40105	63623	14	36377	03727	2	96273	36
25	8 52 40	3 7 20	9.59924	12	10.40076	9.63657	14	10.36343	10.03733	2	9.96267	35
26	52 32	7 28	59954	13	40046	63692	15	36308	03738	2	96262	34
27	52 24	7 36	59983	13	40017	63726	16	36274	03744	2	96256	33
28	52 16	7 44	60012	14	39988	63761	16	36239	03749	3	96251	32
29	52 8	7 52	60041	14	39959	63796	17	36204	03755	3	96245	31
30	8 52 0	3 8 0	9.60070	15	10.39930	9.63830	17	10.36170	10.03760	3	9.96240	30
31	51 52	8 8	60099	15	39901	63865	18	36135	03766	3	96234	29
32	51 44	8 16	60128	15	39872	63899	18	36101	03771	3	96229	28
33	51 36	8 24	60157	16	39843	63934	19	36066	03777	3	96223	27
34	51 28	8 32	60186	16	39814	63968	20	36032	03782	3	96218	26
35	8 51 20	3 8 40	9.60215	17	10.39785	9.64003	20	10.35997	10.03788	3	9.96212	25
36	51 12	8 48	60244	17	39756	64037	21	35963	03793	3	96207	24
37	51 4	8 56	60273	18	39727	64072	21	35928	03799	3	96201	23
38	50 56	9 4	60302	18	39698	64106	22	35894	03804	3	96196	22
39	50 48	9 12	60331	19	39669	64140	22	35860	03810	4	96190	21
40	8 50 40	3 9 20	9.60359	19	10.39641	9.64175	23	10.35825	10.03815	4	9.96185	20
41	50 32	9 28	60388	20	39612	64209	24	35791	03821	4	96179	19
42	50 24	9 36	60417	20	39583	64243	24	35757	03826	4	96174	18
43	50 16	9 44	60446	21	39554	64278	25	35722	03832	4	96168	17
44	50 8	9 52	60474	21	39526	64312	25	35688	03838	4	96162	16
45	8 50 0	3 10 0	9.60503	22	10.39497	9.64346	26	10.35654	10.03843	4	9.96157	15
46	49 52	10 8	60532	22	39468	64381	26	35619	03849	4	96151	14
47	49 44	10 16	60561	23	39439	64415	27	35585	03854	4	96146	13
48	49 36	10 24	60589	23	39411	64449	28	35551	03860	4	96140	12
49	49 28	10 32	60618	24	39382	64483	28	35517	03865	4	96135	11
50	8 49 20	3 10 40	9.60646	24	10.39354	9.64517	29	10.35483	10.03871	5	9.96129	10
51	49 12	10 48	60675	25	39325	64552	29	35448	03877	5	96123	9
52	49 4	10 56	60704	25	39296	64586	30	35414	03882	5	96118	8
53	48 56	11 4	60732	26	39268	64620	31	35380	03888	5	96112	7
54	48 48	11 12	60761	26	39239	64654	31	35346	03893	5	96107	6
55	8 48 40	3 11 20	9.60789	27	10.39211	9.64688	32	10.35312	10.03899	5	9.96101	5
56	48 32	11 28	60818	27	39182	64722	32	35278	03905	5	96095	4
57	48 24	11 36	60846	28	39154	64756	33	35244	03910	5	96090	3
58	48 16	11 44	60875	28	39125	64790	33	35210	03916	5	96084	2
59	48 8	11 52	60903	29	39097	64824	34	35176	03921	5	96079	1
60	48 0	12 0	60931	29	39069	64858	35	35142	03927	6	96073	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
113°			A		A	B		B	C		C	66°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	4	7	11	15	18	22	25
	B	4	9	13	17	22	26	31
	C	1	1	2	3	3	4	5

TABLE 44.

Log. Sines, Tangents, and Secants.

24°			A		A	B		B	C		C	155°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	8 48 0	3 12 0	9.60931	0	10.39069	9.64858	0	10.35142	10.03927	0	9.96073	60
1	47 52	12 8	60960	0	39040	64892	1	35108	03933	0	96067	59
2	47 44	12 16	60988	1	39012	64926	1	35074	03938	0	96062	58
3	47 36	12 24	61016	1	38984	64960	2	35040	03944	0	96056	57
4	47 28	12 32	61045	2	38955	64994	2	35006	03950	0	96050	56
5	8 47 20	3 12 40	9.61073	2	10.38927	9.65028	3	10.34972	10.03955	0	9.96045	55
6	47 12	12 48	61101	3	38899	65062	3	34938	03961	1	96039	54
7	47 4	12 56	61129	3	38871	65096	4	34904	03966	1	96034	53
8	46 56	13 4	61158	4	38842	65130	4	34870	03972	1	96028	52
9	46 48	13 12	61186	4	38814	65164	5	34836	03978	1	96022	51
10	8 46 40	3 13 20	9.61214	5	10.38786	9.65197	6	10.34803	10.03983	1	9.96017	50
11	46 32	13 28	61242	5	38758	65231	6	34769	03989	1	96011	49
12	46 24	13 36	61270	6	38730	65265	7	34735	03995	1	96005	48
13	46 16	13 44	61298	6	38702	65299	7	34701	04000	1	96000	47
14	46 8	13 52	61326	6	38674	65333	8	34667	04006	1	95994	46
15	8 46 0	3 14 0	9.61354	7	10.38646	9.65366	8	10.34634	10.04012	1	9.95988	45
16	45 52	14 8	61382	7	38618	65400	9	34600	04018	2	95982	44
17	45 44	14 16	61411	8	38589	65434	9	34566	04023	2	95977	43
18	45 36	14 24	61438	8	38562	65467	10	34533	04029	2	95971	42
19	45 28	14 32	61466	9	38534	65501	11	34499	04035	2	95965	41
20	8 45 20	3 14 40	9.61494	9	10.38506	9.65535	11	10.34465	10.04040	2	9.95960	40
21	45 12	14 48	61522	10	38478	65568	12	34432	04046	2	95954	39
22	45 4	14 56	61550	10	38450	65602	12	34398	04052	2	95948	38
23	44 56	15 4	61578	11	38422	65636	13	34364	04058	2	95942	37
24	44 48	15 12	61606	11	38394	65669	13	34331	04063	2	95937	36
25	8 44 40	3 15 20	9.61634	12	10.38366	9.65703	14	10.34297	10.04069	2	9.95931	35
26	44 32	15 28	61662	12	38338	65736	15	34264	04075	2	95925	34
27	44 24	15 36	61689	12	38311	65770	15	34230	04080	3	95920	33
28	44 16	15 44	61717	13	38283	65803	16	34197	04086	3	95914	32
29	44 8	15 52	61745	13	38255	65837	16	34163	04092	3	95908	31
30	8 44 0	3 16 0	9.61773	14	10.38227	9.65870	17	10.34130	10.04098	3	9.95902	30
31	43 52	16 8	61800	14	38200	65904	17	34096	04103	3	95897	29
32	43 44	16 16	61828	15	38172	65937	18	34063	04109	3	95891	28
33	43 36	16 24	61856	15	38144	65971	18	34029	04115	3	95885	27
34	43 28	16 32	61883	16	38117	66004	19	33996	04121	3	95879	26
35	8 43 20	3 16 40	9.61911	16	10.38089	9.66038	20	10.33962	10.04127	3	9.95873	25
36	43 12	16 48	61939	17	38061	66071	20	33929	04132	3	95868	24
37	43 4	16 56	61966	17	38034	66104	21	33896	04138	4	95862	23
38	42 56	17 4	61994	18	38006	66138	21	33862	04144	4	95856	22
39	42 48	17 12	62021	18	37979	66171	22	33829	04150	4	95850	21
40	8 42 40	3 17 20	9.62049	18	10.37951	9.66204	22	10.33796	10.04156	4	9.95844	20
41	42 32	17 28	62076	19	37924	66238	23	33762	04161	4	95839	19
42	42 24	17 36	62104	19	37896	66271	23	33729	04167	4	95833	18
43	42 16	17 44	62131	20	37869	66304	24	33696	04173	4	95827	17
44	42 8	17 52	62159	20	37841	66337	25	33663	04179	4	95821	16
45	8 42 0	3 18 0	9.62186	21	10.37814	9.66371	25	10.33629	10.04185	4	9.95815	15
46	41 52	18 8	62214	21	37786	66404	26	33596	04190	4	95810	14
47	41 44	18 16	62241	22	37759	66437	26	33563	04196	5	95804	13
48	41 36	18 24	62268	22	37732	66470	27	33530	04202	5	95798	12
49	41 28	18 32	62296	23	37704	66503	27	33497	04208	5	95792	11
50	8 41 20	3 18 40	9.62323	23	10.37677	9.66537	28	10.33463	10.04214	5	9.95786	10
51	41 12	18 48	62350	24	37650	66570	28	33430	04220	5	95780	9
52	41 4	18 56	62377	24	37623	66603	29	33397	04225	5	95775	8
53	40 56	19 4	62405	24	37595	66636	30	33364	04231	5	95769	7
54	40 48	19 12	62432	25	37568	66669	30	33331	04237	5	95763	6
55	8 40 40	3 19 20	9.62459	25	10.37541	9.66702	31	10.33298	10.04243	5	9.95757	5
56	40 32	19 28	62486	26	37514	66735	31	33265	04249	5	95751	4
57	40 24	19 36	62513	26	37487	66768	32	33232	04255	5	95745	3
58	40 16	19 44	62541	27	37459	66801	32	33199	04261	6	95739	2
59	40 8	19 52	62568	27	37432	66834	33	33166	04267	6	95733	1
60	40 0	20 0	62595	28	37405	66867	33	33133	04272	6	95728	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
114°			A		A	B		B	C		C	65°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	3	7	10	14	17	21	24
	B	4	8	13	17	21	25	29
	C	1	1	2	3	4	4	5

Log. Sines, Tangents, and Secants.

25°			A		A	B		B	C		C	154°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	8 40 0	3 20 0	9. 62595	0	10. 37405	9. 66867	0	10. 33133	10. 04272	0	9. 95728	60
1	39 52	20 8	62622	0	37378	66900	1	33100	04278	0	95722	59
2	39 44	20 16	62649	1	37351	66933	1	33067	04284	0	95716	58
3	39 36	20 24	62676	1	37324	66966	2	33034	04290	0	95710	57
4	39 28	20 32	62703	2	37297	66999	2	33001	04296	0	95704	56
5	8 39 20	3 20 40	9. 62730	2	10. 37270	9. 67032	3	10. 32968	10. 04302	1	9. 95698	55
6	39 12	20 48	62757	3	37243	67065	3	32935	04308	1	95692	54
7	39 4	20 56	62784	3	37216	67098	4	32902	04314	1	95686	53
8	38 56	21 4	62811	4	37189	67131	4	32869	04320	1	95680	52
9	38 48	21 12	62838	4	37162	67163	5	32837	04326	1	95674	51
10	8 38 40	3 21 20	9. 62865	4	10. 37135	9. 67196	5	10. 32804	10. 04332	1	9. 95668	50
11	38 32	21 28	62892	5	37108	67229	6	32771	04337	1	95663	49
12	38 24	21 36	62918	5	37082	67262	7	32738	04343	1	95657	48
13	38 16	21 44	62945	6	37055	67295	7	32705	04349	1	95651	47
14	38 8	21 52	62972	6	37028	67327	8	32673	04355	1	95645	46
15	8 38 0	3 22 0	9. 62999	7	10. 37001	9. 67360	8	10. 32640	10. 04361	2	9. 95639	45
16	37 52	22 8	63026	7	36974	67393	9	32607	04367	2	95633	44
17	37 44	22 16	63052	8	36948	67426	9	32574	04373	2	95627	43
18	37 36	22 24	63079	8	36921	67458	10	32542	04379	2	95621	42
19	37 28	22 32	63106	8	36894	67491	10	32509	04385	2	95615	41
20	8 37 20	3 22 40	9. 63133	9	10. 36867	9. 67524	11	10. 32476	10. 04391	2	9. 95609	40
21	37 12	22 48	63159	9	36841	67556	11	32444	04397	2	95603	39
22	37 4	22 56	63186	10	36814	67589	12	32411	04403	2	95597	38
23	36 56	23 4	63213	10	36787	67622	12	32378	04409	2	95591	37
24	36 48	23 12	63239	11	36761	67654	13	32346	04415	2	95585	36
25	8 36 40	3 23 20	9. 63266	11	10. 36734	9. 67687	14	10. 32313	10. 04421	3	9. 95579	35
26	36 32	23 28	63292	11	36708	67719	14	32281	04427	3	95573	34
27	36 24	23 36	63319	12	36681	67752	15	32248	04433	3	95567	33
28	36 16	23 44	63345	12	36655	67785	15	32215	04439	3	95561	32
29	36 8	23 52	63372	13	36628	67817	16	32183	04445	3	95555	31
30	8 36 0	3 24 0	9. 63398	13	10. 36602	9. 67850	16	10. 32150	10. 04451	3	9. 95549	30
31	35 52	24 8	63425	14	36575	67882	17	32118	04457	3	95543	29
32	35 44	24 16	63451	14	36549	67915	17	32085	04463	3	95537	28
33	35 36	24 24	63478	15	36522	67947	18	32053	04469	3	95531	27
34	35 28	24 32	63504	15	36496	67980	18	32020	04475	3	95525	26
35	8 35 20	3 24 40	9. 63531	15	10. 36469	9. 68012	19	10. 31988	10. 04481	4	9. 95519	25
36	35 12	24 48	63557	16	36443	68044	20	31956	04487	4	95513	24
37	35 4	24 56	63583	16	36417	68077	20	31923	04493	4	95507	23
38	34 56	25 4	63610	17	36390	68109	21	31891	04500	4	95500	22
39	34 48	25 12	63636	17	36364	68142	21	31858	04506	4	95494	21
40	8 34 40	3 25 20	9. 63662	18	10. 36338	9. 68174	22	10. 31826	10. 04512	4	9. 95488	20
41	34 32	25 28	63689	18	36311	68206	22	31794	04518	4	95482	19
42	34 24	25 36	63715	19	36285	68239	23	31761	04524	4	95476	18
43	34 16	25 44	63741	19	36259	68271	23	31729	04530	4	95470	17
44	34 8	25 52	63767	19	36233	68303	24	31697	04536	4	95464	16
45	8 34 0	3 26 0	9. 63794	20	10. 36206	9. 68336	24	10. 31664	10. 04542	5	9. 95458	15
46	33 52	26 8	63820	20	36180	68368	25	31632	04548	5	95452	14
47	33 44	26 16	63846	21	36154	68400	25	31600	04554	5	95446	13
48	33 36	26 24	63872	21	36128	68432	26	31568	04560	5	95440	12
49	33 28	26 32	63898	22	36102	68465	27	31535	04566	5	95434	11
50	8 33 20	3 26 40	9. 63924	22	10. 36076	9. 68497	27	10. 31503	10. 04573	5	9. 95427	10
51	33 12	26 48	63950	23	36050	68529	28	31471	04579	5	95421	9
52	33 4	26 56	63976	23	36024	68561	28	31439	04585	5	95415	8
53	32 56	27 4	64002	23	35998	68593	29	31407	04591	5	95409	7
54	32 48	27 12	64028	24	35972	68626	29	31374	04597	5	95403	6
55	8 32 40	3 27 20	9. 64054	24	10. 35946	9. 68658	30	10. 31342	10. 04603	6	9. 95397	5
56	32 32	27 28	64080	25	35920	68690	30	31310	04609	6	95391	4
57	32 24	27 36	64106	25	35894	68722	31	31278	04616	6	95384	3
58	32 16	27 44	64132	26	35868	68754	31	31246	04622	6	95378	2
59	32 8	27 52	64158	26	35842	68786	32	31214	04628	6	95372	1
60	32 0	28 0	64184	26	35816	68818	33	31182	04634	6	95366	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
115°			A		A	B		B	C		C	64°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	3	7	10	13	17	20	23
	B	4	8	12	16	20	24	28
	C	1	2	2	3	4	5	5

TABLE 44.

Log. Sines, Tangents, and Secants.

26°			A		A	B		B	C		C	153°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	8 32 0	3 28 0	9.64184	0	10.35816	9.68818	0	10.31182	10.04634	0	9.95366	60
1	31 52	28 8	64210	0	35790	68850	1	31150	04640	0	95360	59
2	31 44	28 16	64236	1	35764	68882	1	31118	04646	0	95354	58
3	31 36	28 24	64262	1	35738	68914	2	31086	04652	0	95348	57
4	31 28	28 32	64288	2	35712	68946	2	31054	04659	0	95341	56
5	8 31 20	3 28 40	9.64313	2	10.35687	9.68978	3	10.31022	10.04665	1	9.95335	55
6	31 12	28 48	64339	3	35661	69010	3	30990	04671	1	95329	54
7	31 4	28 56	64365	3	35635	69042	4	30958	04677	1	95323	53
8	30 56	29 4	64391	3	35609	69074	4	30926	04683	1	95317	52
9	30 48	29 12	64417	4	35583	69106	5	30894	04690	1	95310	51
10	8 30 40	3 29 20	9.64442	4	10.35558	9.69138	5	10.30862	10.04696	1	9.95304	50
11	30 32	29 28	64468	5	35532	69170	6	30830	04702	1	95298	49
12	30 24	29 36	64494	5	35506	69202	6	30798	04708	1	95292	48
13	30 16	29 44	64519	5	35481	69234	7	30766	04714	1	95286	47
14	30 8	29 52	64545	6	35455	69266	7	30734	04721	1	95279	46
15	8 30 0	3 30 0	9.64571	6	10.35429	9.69298	8	10.30702	10.04727	2	9.95273	45
16	29 52	30 8	64596	7	35404	69329	8	30671	04733	2	95267	44
17	29 44	30 16	64622	7	35378	69361	9	30639	04739	2	95261	43
18	29 36	30 24	64647	8	35353	69393	9	30607	04746	2	95254	42
19	29 28	30 32	64673	8	35327	69425	10	30575	04752	2	95248	41
20	8 29 20	3 30 40	9.64698	8	10.35302	9.69457	11	10.30543	10.04758	2	9.95242	40
21	29 12	30 48	64724	9	35276	69488	11	30512	04764	2	95236	39
22	29 4	30 56	64749	9	35251	69520	12	30480	04771	2	95229	38
23	28 56	31 4	64775	10	35225	69552	12	30448	04777	2	95223	37
24	28 48	31 12	64800	10	35200	69584	13	30416	04783	3	95217	36
25	8 28 40	3 31 20	9.64826	11	10.35174	9.69615	13	10.30385	10.04789	3	9.95211	35
26	28 32	31 28	64851	11	35149	69647	14	30353	04796	3	95204	34
27	28 24	31 36	64877	11	35123	69679	14	30321	04802	3	95198	33
28	28 16	31 44	64902	12	35098	69710	15	30290	04808	3	95192	32
29	28 8	31 52	64927	12	35073	69742	15	30258	04815	3	95185	31
30	8 28 0	3 32 0	9.64953	13	10.35047	9.69774	16	10.30226	10.04821	3	9.95179	30
31	27 52	32 8	64978	13	35022	69805	16	30195	04827	3	95173	29
32	27 44	32 16	65003	14	34997	69837	17	30163	04833	3	95167	28
33	27 36	32 24	65029	14	34971	69868	17	30132	04840	3	95160	27
34	27 28	32 32	65054	14	34946	69900	18	30100	04846	4	95154	26
35	8 27 20	3 32 40	9.65079	15	10.34921	9.69932	18	10.30068	10.04852	4	9.95148	25
36	27 12	32 48	65104	15	34896	69963	19	30037	04859	4	95141	24
37	27 4	32 56	65130	16	34870	69995	20	30005	04865	4	95135	23
38	26 56	33 4	65155	16	34845	70026	20	29974	04871	4	95129	22
39	26 48	33 12	65180	16	34820	70058	21	29942	04878	4	95122	21
40	8 26 40	3 33 20	9.65205	17	10.34795	9.70089	21	10.29911	10.04884	4	9.95116	20
41	26 32	33 28	65230	17	34770	70121	22	29879	04890	4	95110	19
42	26 24	33 36	65255	18	34745	70152	22	29848	04897	4	95103	18
43	26 16	33 44	65281	18	34719	70184	23	29816	04903	5	95097	17
44	26 8	33 52	65306	19	34694	70215	23	29785	04910	5	95090	16
45	8 26 0	3 34 0	9.65331	19	10.34669	9.70247	24	10.29753	10.04916	5	9.95084	15
46	25 52	34 8	65356	19	34644	70278	24	29722	04922	5	95078	14
47	25 44	34 16	65381	20	34619	70309	25	29691	04929	5	95071	13
48	25 36	34 24	65406	20	34594	70341	25	29659	04935	5	95065	12
49	25 28	34 32	65431	21	34569	70372	26	29628	04941	5	95059	11
50	8 25 20	3 34 40	9.65456	21	10.34544	9.70404	26	10.29596	10.04948	5	9.95052	10
51	25 12	34 48	65481	22	34519	70435	27	29565	04954	5	95046	9
52	25 4	34 56	65506	22	34494	70466	27	29534	04961	5	95039	8
53	24 56	35 4	65531	22	34469	70498	28	29502	04967	6	95033	7
54	24 48	35 12	65556	23	34444	70529	28	29471	04973	6	95027	6
55	8 24 40	3 35 20	9.65580	23	10.34420	9.70560	29	10.29440	10.04980	6	9.95020	5
56	24 32	35 28	65605	24	34395	70592	30	29408	04986	6	95014	4
57	24 24	35 36	65630	24	34370	70623	30	29377	04993	6	95007	3
58	24 16	35 44	65655	25	34345	70654	31	29346	04999	6	95001	2
59	24 8	35 52	65680	25	34320	70685	31	29315	05005	6	94995	1
60	24 0	36 0	65705	25	34295	70717	32	29283	05012	6	94988	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
116°			A		A	B		B	C		C	63°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	3	6	10	13	16	19	22
	B	4	8	12	16	20	24	28
	C	1	2	2	3	4	5	6

TABLE 44.

Log. Sines, Tangents, and Secants.

27°			A		A	B		B	C		C	152°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	8 24 0	3 36 0	9.65705	0	10.34295	9.70717	0	10.29283	10.05012	0	9.94988	60
1	23 52	36 8	65729	0	34271	70748	1	29252	05018	0	94982	59
2	23 44	36 16	65754	1	34246	70779	1	29221	05025	0	94975	58
3	23 36	36 24	65779	1	34221	70810	2	29190	05031	0	94969	57
4	23 28	36 32	65804	2	34196	70841	2	29159	05038	0	94962	56
5	8 23 20	3 36 40	9.65828	2	10.34172	9.70873	3	10.29127	10.05044	1	9.94956	55
6	23 12	36 48	65853	2	34147	70904	3	29096	05051	1	94949	54
7	23 4	36 56	65878	3	34122	70935	4	29065	05057	1	94943	53
8	22 56	37 4	65902	3	34098	70966	4	29034	05064	1	94936	52
9	22 48	37 12	65927	4	34073	70997	5	29003	05070	1	94930	51
10	8 22 40	3 37 20	9.65952	4	10.34048	9.71028	5	10.28972	10.05077	1	9.94923	50
11	22 32	37 28	65976	4	34024	71059	6	28941	05083	1	94917	49
12	22 24	37 36	66001	5	33999	71090	6	28910	05089	1	94911	48
13	22 16	37 44	66025	5	33975	71121	7	28879	05096	1	94904	47
14	22 8	37 52	66050	6	33950	71153	7	28847	05102	2	94898	46
15	8 22 0	3 38 0	9.66075	6	10.33925	9.71184	8	10.28816	10.05109	2	9.94891	45
16	21 52	38 8	66099	6	33901	71215	8	28785	05115	2	94885	44
17	21 44	38 16	66124	7	33876	71246	9	28754	05122	2	94878	43
18	21 36	38 24	66148	7	33852	71277	9	28723	05129	2	94871	42
19	21 28	38 32	66173	8	33827	71308	10	28692	05135	2	94865	41
20	8 21 20	3 38 40	9.66197	8	10.33803	9.71339	10	10.28661	10.05142	2	9.94858	40
21	21 12	38 48	66221	8	33779	71370	11	28630	05148	2	94852	39
22	21 4	38 56	66246	9	33754	71401	11	28599	05155	2	94845	38
23	20 56	39 4	66270	9	33730	71431	12	28569	05161	3	94839	37
24	20 48	39 12	66295	10	33705	71462	12	28538	05168	3	94832	36
25	8 20 40	3 39 20	9.66319	10	10.33681	9.71493	13	10.28507	10.05174	3	9.94826	35
26	20 32	39 28	66343	11	33657	71524	13	28476	05181	3	94819	34
27	20 24	39 36	66368	11	33632	71555	14	28445	05187	3	94813	33
28	20 16	39 44	66392	11	33608	71586	14	28414	05194	3	94806	32
29	20 8	39 52	66416	12	33584	71617	15	28383	05201	3	94799	31
30	8 20 0	3 40 0	9.66441	12	10.33559	9.71648	15	10.28352	10.05207	3	9.94793	30
31	19 52	40 8	66465	13	33535	71679	16	28321	05214	3	94786	29
32	19 44	40 16	66489	13	33511	71709	16	28291	05220	4	94780	28
33	19 36	40 24	66513	13	33487	71740	17	28260	05227	4	94773	27
34	19 28	40 32	66537	14	33463	71771	17	28229	05233	4	94767	26
35	8 19 20	3 40 40	9.66562	14	10.33438	9.71802	18	10.28198	10.05240	4	9.94760	25
36	19 12	40 48	66586	15	33414	71833	19	28167	05247	4	94753	24
37	19 4	40 56	66610	15	33390	71863	19	28137	05253	4	94747	23
38	18 56	41 4	66634	15	33366	71894	20	28106	05260	4	94740	22
39	18 48	41 12	66658	16	33342	71925	20	28075	05266	4	94734	21
40	8 18 40	3 41 20	9.66682	16	10.33318	9.71955	21	10.28045	10.05273	4	9.94727	20
41	18 32	41 28	66706	17	33294	71986	21	28014	05280	4	94720	19
42	18 24	41 36	66731	17	33269	72017	22	27983	05286	5	94714	18
43	18 16	41 44	66755	17	33245	72048	22	27952	05293	5	94707	17
44	18 8	41 52	66779	18	33221	72078	23	27922	05300	5	94700	16
45	8 18 0	3 42 0	9.66803	18	10.33197	9.72109	23	10.27891	10.05306	5	9.94694	15
46	17 52	42 8	66827	19	33173	72140	24	27860	05313	5	94687	14
47	17 44	42 16	66851	19	33149	72170	24	27830	05320	5	94680	13
48	17 36	42 24	66875	19	33125	72201	25	27799	05326	5	94674	12
49	17 28	42 32	66899	20	33101	72231	25	27769	05333	5	94667	11
50	8 17 20	3 42 40	9.66922	20	10.33078	9.72262	26	10.27738	10.05340	5	9.94660	10
51	17 12	42 48	66946	21	33054	72293	26	27707	05346	6	94654	9
52	17 4	42 56	66970	21	33030	72323	27	27677	05353	6	94647	8
53	16 56	43 4	66994	21	33006	72354	27	27646	05360	6	94640	7
54	16 48	43 12	67018	22	32982	72384	28	27616	05366	6	94634	6
55	8 16 40	3 43 20	9.67042	22	10.32958	9.72415	28	10.27585	10.05373	6	9.94627	5
56	16 32	43 28	67066	23	32934	72445	29	27555	05380	6	94620	4
57	16 24	43 36	67090	23	32910	72476	29	27524	05386	6	94614	3
58	16 16	43 44	67113	23	32887	72506	30	27494	05393	6	94607	2
59	16 8	43 52	67137	24	32863	72537	30	27463	05400	6	94600	1
60	16 0	44 0	67161	24	32839	72567	31	27433	05407	7	94593	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
117°			A		A	B		B	C		C	62°

Seconds of time		1^s	2^s	3^s	4^s	5^s	6^s	7^s
Prop. parts of cols.	A	3	6	9	12	15	18	21
	B	4	8	12	15	19	23	27
	C	1	2	2	3	4	5	6

TABLE 44.

Log. Sines, Tangents, and Secants.

28°			A		A	B		B	C		C	151°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	8 16 0	3 44 0	9.67161	0	10.32839	9.72567	0	10.27433	10.05407	0	9.94593	60
1	15 52	44 8	67185	0	32815	72598	1	27402	05413	0	94587	59
2	15 44	44 16	67208	1	32792	72628	1	27372	05420	0	94580	58
3	15 36	44 24	67232	1	32768	72659	2	27341	05427	0	94573	57
4	15 28	44 32	67256	2	32744	72689	2	27311	05433	0	94567	56
5	8 15 20	3 44 40	9.67280	2	10.32720	9.72720	3	10.27280	10.05440	1	9.94560	55
6	15 12	44 48	67303	2	32697	72750	3	27250	05447	1	94553	54
7	15 4	44 56	67327	3	32673	72780	4	27220	05454	1	94546	53
8	14 56	45 4	67350	3	32650	72811	4	27189	05460	1	94540	52
9	14 48	45 12	67374	3	32626	72841	5	27159	05467	1	94533	51
10	8 14 40	3 45 20	9.67398	4	10.32602	9.72872	5	10.27128	10.05474	1	9.94526	50
11	14 32	45 28	67421	4	32579	72902	6	27098	05481	1	94519	49
12	14 24	45 36	67445	5	32555	72932	6	27068	05487	1	94513	48
13	14 16	45 44	67468	5	32532	72963	7	27037	05494	1	94506	47
14	14 8	45 52	67492	5	32508	72993	7	27007	05501	2	94499	46
15	8 14 0	3 46 0	9.67515	6	10.32485	9.73023	8	10.26977	10.05508	2	9.94492	45
16	13 52	46 8	67539	6	32461	73054	8	26946	05515	2	94485	44
17	13 44	46 16	67562	7	32438	73084	9	26916	05521	2	94479	43
18	13 36	46 24	67586	7	32414	73114	9	26886	05528	2	94472	42
19	13 28	46 32	67609	7	32391	73144	10	26856	05535	2	94465	41
20	8 13 20	3 46 40	9.67633	8	10.32367	9.73175	10	10.26825	10.05542	2	9.94458	40
21	13 12	46 48	67656	8	32344	73205	11	26795	05549	2	94451	39
22	13 4	46 56	67680	9	32320	73235	11	26765	05555	3	94445	38
23	12 56	47 4	67703	9	32297	73265	12	26735	05562	3	94438	37
24	12 48	47 12	67726	9	32274	73295	12	26705	05569	3	94431	36
25	8 12 40	3 47 20	9.67750	10	10.32250	9.73326	13	10.26674	10.05576	3	9.94424	35
26	12 32	47 28	67773	10	32227	73356	13	26644	05583	3	94417	34
27	12 24	47 36	67796	10	32204	73386	14	26614	05590	3	94410	33
28	12 16	47 44	67820	11	32180	73416	14	26584	05596	3	94404	32
29	12 8	47 52	67843	11	32157	73446	15	26554	05603	3	94397	31
30	8 12 0	3 48 0	9.67866	12	10.32134	9.73476	15	10.26524	10.05610	3	9.94390	30
31	11 52	48 8	67890	12	32110	73507	16	26493	05617	4	94383	29
32	11 44	48 16	67913	12	32087	73537	16	26463	05624	4	94376	28
33	11 36	48 24	67936	13	32064	73567	17	26433	05631	4	94369	27
34	11 28	48 32	67959	13	32041	73597	17	26403	05638	4	94362	26
35	8 11 20	3 48 40	9.67982	14	10.32018	9.73627	18	10.26373	10.05645	4	9.94355	25
36	11 12	48 48	68006	14	31994	73657	18	26343	05651	4	94349	24
37	11 4	48 56	68029	14	31971	73687	19	26313	05658	4	94342	23
38	10 56	49 4	68052	15	31948	73717	19	26283	05665	4	94335	22
39	10 48	49 12	68075	15	31925	73747	20	26253	05672	4	94328	21
40	8 10 40	3 49 20	9.68098	16	10.31902	9.73777	20	10.26223	10.05679	5	9.94321	20
41	10 32	49 28	68121	16	31879	73807	21	26193	05686	5	94314	19
42	10 24	49 36	68144	16	31856	73837	21	26163	05693	5	94307	18
43	10 16	49 44	68167	17	31833	73867	22	26133	05700	5	94300	17
44	10 8	49 52	68190	17	31810	73897	22	26103	05707	5	94293	16
45	8 10 0	3 50 0	9.68213	17	10.31787	9.73927	23	10.26073	10.05714	5	9.94286	15
46	9 52	50 8	68237	18	31763	73957	23	26043	05721	5	94279	14
47	9 44	50 16	68260	18	31740	73987	24	26013	05727	5	94273	13
48	9 36	50 24	68283	19	31717	74017	24	25983	05734	5	94266	12
49	9 28	50 32	68305	19	31695	74047	25	25953	05741	6	94259	11
50	8 9 20	3 50 40	9.68328	19	10.31672	9.74077	25	10.25923	10.05748	6	9.94252	10
51	9 12	50 48	68351	20	31649	74107	26	25893	05755	6	94245	9
52	9 4	50 56	68374	20	31626	74137	26	25863	05762	6	94238	8
53	8 56	51 4	68397	21	31603	74166	27	25834	05769	6	94231	7
54	8 48	51 12	68420	21	31580	74196	27	25804	05776	6	94224	6
55	8 8 40	3 51 20	9.68443	21	10.31557	9.74226	28	10.25774	10.05783	6	9.94217	5
56	8 32	51 28	68466	22	31534	74256	28	25744	05790	6	94210	4
57	8 24	51 36	68489	22	31511	74286	29	25714	05797	7	94203	3
58	8 16	51 44	68512	22	31488	74316	29	25684	05804	7	94196	2
59	8 8	51 52	68534	23	31466	74345	30	25655	05811	7	94189	1
60	8 0	52 0	68557	23	31443	74375	30	25625	05818	7	94182	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M
118°			A		A	B		B	C		C	61°

Seconds of time		1ˢ	2ˢ	3ˢ	4ˢ	5ˢ	6ˢ	7ˢ
Prop. parts of cols.	A	3	6	9	12	15	17	20
	B	4	8	11	15	19	23	26
	C	1	2	3	3	4	5	6

TABLE 44.

Log. Sines, Tangents, and Secants.

29°			A		A	B		B	C		C	150°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	8 8 0	3 52 0	9.68557	0	10.31443	9.74375	0	10.25625	10.05818	0	9.94182	60
1	7 52	52 8	68580	0	31420	74405	0	25595	05825	0	94175	59
2	7 44	52 16	68603	1	31397	74435	1	25565	05832	0	94168	58
3	7 36	52 24	68625	1	31375	74465	1	25535	05839	0	94161	57
4	7 28	52 32	68648	1	31352	74494	2	25506	05846	0	94154	56
5	8 7 20	3 52 40	9.68671	2	10.31329	9.74524	2	10.25476	10.05853	1	9.94147	55
6	7 12	52 48	68694	2	31306	74554	3	25446	05860	1	94140	54
7	7 4	52 56	68716	3	31284	74583	3	25417	05867	1	94133	53
8	6 56	53 4	68739	3	31261	74613	4	25387	05874	1	94126	52
9	6 48	53 12	68762	3	31238	74643	4	25357	05881	1	94119	51
10	8 6 40	3 53 20	9.68784	4	10.31216	9.74673	5	10.25327	10.05888	1	9.94112	50
11	6 32	53 28	68807	4	31193	74702	5	25298	05895	1	94105	49
12	6 24	53 36	68829	4	31171	74732	6	25268	05902	1	94098	48
13	6 16	53 44	68852	5	31148	74762	6	25238	05910	2	94090	47
14	6 8	53 52	68875	5	31125	74791	7	25209	05917	2	94083	46
15	8 6 0	3 54 0	9.68897	6	10.31103	9.74821	7	10.25179	10.05924	2	9.94076	45
16	5 52	54 8	68920	6	31080	74851	8	25149	05931	2	94069	44
17	5 44	54 16	68942	6	31058	74880	8	25120	05938	2	94062	43
18	5 36	54 24	68965	7	31035	74910	9	25090	05945	2	94055	42
19	5 28	54 32	68987	7	31013	74939	9	25061	05952	2	94048	41
20	8 5 20	3 54 40	9.69010	7	10.30990	9.74969	10	10.25031	10.05959	2	9.94041	40
21	5 12	54 48	69032	8	30968	74998	10	25002	05966	3	94034	39
22	5 4	54 56	69055	8	30945	75028	11	24972	05973	3	94027	38
23	4 56	55 4	69077	9	30923	75058	11	24942	05980	3	94020	37
24	4 48	55 12	69100	9	30900	75087	12	24913	05988	3	94012	36
25	8 4 40	3 55 20	9.69122	9	10.30878	9.75117	12	10.24883	10.05995	3	9.94005	35
26	4 32	55 28	69144	10	30856	75146	13	24854	06002	3	93998	34
27	4 24	55 36	69167	10	30833	75176	13	24824	06009	3	93991	33
28	4 16	55 44	69189	10	30811	75205	14	24795	06016	3	93984	32
29	4 8	55 52	69212	11	30788	75235	14	24765	06023	3	93977	31
30	8 4 0	3 56 0	9.69234	11	10.30766	9.75264	15	10.24736	10.06030	4	9.93970	30
31	3 52	56 8	69256	12	30744	75294	15	24706	06037	4	93963	29
32	3 44	56 16	69279	12	30721	75323	16	24677	06045	4	93955	28
33	3 36	56 24	69301	12	30699	75353	16	24647	06052	4	93948	27
34	3 28	56 32	69323	13	30677	75382	17	24618	06059	4	93941	26
35	8 3 20	3 56 40	9.69345	13	10.30655	9.75411	17	10.24589	10.06066	4	9.93934	25
36	3 12	56 48	69368	13	30632	75441	18	24559	06073	4	93927	24
37	3 4	56 56	69390	14	30610	75470	18	24530	06080	4	93920	23
38	2 56	57 4	69412	14	30588	75500	19	24500	06088	5	93912	22
39	2 48	57 12	69434	15	30566	75529	19	24471	06095	5	93905	21
40	8 2 40	3 57 20	9.69456	15	10.30544	9.75558	20	10.24442	10.06102	5	9.93898	20
41	2 32	57 28	69479	15	30521	75588	20	24412	06109	5	93891	19
42	2 24	57 36	69501	16	30499	75617	21	24383	06116	5	93884	18
43	2 16	57 44	69523	16	30477	75647	21	24353	06124	5	93876	17
44	2 8	57 52	69545	16	30455	75676	22	24324	06131	5	93869	16
45	8 2 0	3 58 0	9.69567	17	10.30433	9.75705	22	10.24295	10.06138	5	9.93862	15
46	1 52	58 8	69589	17	30411	75735	23	24265	06145	5	93855	14
47	1 44	58 16	69611	17	30389	75764	23	24236	06153	6	93847	13
48	1 36	58 24	69633	18	30367	75793	24	24207	06160	6	93840	12
49	1 28	58 32	69655	18	30345	75822	24	24178	06167	6	93833	11
50	8 1 20	3 58 40	9.69677	19	10.30323	9.75852	25	10.24148	10.06174	6	9.93826	10
51	1 12	58 48	69699	19	30301	75881	25	24119	06181	6	93819	9
52	1 4	58 56	69721	19	30279	75910	26	24090	06189	6	93811	8
53	0 56	59 4	69743	20	30257	75939	26	24061	06196	6	93804	7
54	0 48	59 12	69765	20	30235	75969	27	24031	06203	6	93797	6
55	8 0 40	3 59 20	9.69787	20	10.30213	9.75998	27	10.24002	10.06211	7	9.93789	5
56	0 32	59 28	69809	21	30191	76027	28	23973	06218	7	93782	4
57	0 24	59 36	69831	21	30169	76056	28	23944	06225	7	93775	3
58	0 16	59 44	69853	22	30147	76086	29	23914	06232	7	93768	2
59	0 8	59 52	69875	22	30125	76115	29	23885	06240	7	93760	1
60	0 0	4 0 0	69897	22	30103	76144	29	23856	06247	7	93753	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
119°			A		A	B		B	C		C	60°

Seconds of time		1^s	2^s	3^s	4^s	5^s	6^s	7^s
Prop. parts of cols.	A	3	6	8	11	14	17	20
	B	4	7	11	15	18	22	26
	C	1	2	3	4	4	5	6

TABLE 44.

Log. Sines, Tangents, and Secants.

30°			A		A	B		B	C		C	149°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	8 0 0	4 0 0	9. 69897	0	10. 30103	9. 76144	0	10. 23856	10. 06247	0	9. 93753	60
1	7 59 52	0 8	69919	0	30081	76173	0	23827	06254	0	93746	59
2	59 44	0 16	69941	1	30059	76202	1	23798	06262	0	93738	58
3	59 36	0 24	69963	1	30037	76231	1	23769	06269	0	93731	57
4	59 28	0 32	69984	1	30016	76261	2	23739	06276	0	93724	56
5	7 59 20	4 0 40	9. 70006	2	10. 29994	9. 76290	2	10. 23710	10. 06283	1	9. 93717	55
6	59 12	0 48	70028	2	29972	76319	3	23681	06291	1	93709	54
7	59 4	0 56	70050	3	29950	76348	3	23652	06298	1	93702	53
8	58 56	1 4	70072	3	29928	76377	4	23623	06305	1	93695	52
9	58 48	1 12	70093	3	29907	76406	4	23594	06313	1	93687	51
10	7 58 40	4 1 20	9. 70115	4	10. 29885	9. 76435	5	10. 23565	10. 06320	1	9. 93680	50
11	58 32	1 28	70137	4	29863	76464	5	23536	06327	1	93673	49
12	58 24	1 36	70159	4	29841	76493	6	23507	06335	1	93665	48
13	58 16	1 44	70180	5	29820	76522	6	23478	06342	2	93658	47
14	58 8	1 52	70202	5	29798	76551	7	23449	06350	2	93650	46
15	7 58 0	4 2 0	9. 70224	5	10. 29776	9. 76580	7	10. 23420	10. 06357	2	9. 93643	45
16	57 52	2 8	70245	6	29755	76609	8	23391	06364	2	93636	44
17	57 44	2 16	70267	6	29733	76639	8	23361	06372	2	93628	43
18	57 36	2 24	70288	6	29712	76668	9	23332	06379	2	93621	42
19	57 28	2 32	70310	7	29690	76697	9	23303	06386	2	93614	41
20	7 57 20	4 2 40	9. 70332	7	10. 29668	9. 76725	10	10. 23275	10. 06394	2	9. 93606	40
21	57 12	2 48	70353	8	29647	76754	10	23246	06401	3	93599	39
22	57 4	2 56	70375	8	29625	76783	11	23217	06409	3	93591	38
23	56 56	3 4	70396	8	29604	76812	11	23188	06416	3	93584	37
24	56 48	3 12	70418	9	29582	76841	12	23159	06423	3	93577	36
25	7 56 40	4 3 20	9. 70439	9	10. 29561	9. 76870	12	10. 23130	10. 06431	3	9. 93569	35
26	56 32	3 28	70461	9	29539	76899	13	23101	06438	3	93562	34
27	56 24	3 36	70482	10	29518	76928	13	23072	06446	3	93554	33
28	56 16	3 44	70504	10	29496	76957	13	23043	06453	3	93547	32
29	56 8	3 52	70525	10	29475	76986	14	23014	06461	4	93539	31
30	7 56 0	4 4 0	9. 70547	11	10. 29453	9. 77015	14	10. 22985	10. 06468	4	9. 93532	30
31	55 52	4 8	70568	11	29432	77044	15	22956	06475	4	93525	29
32	55 44	4 16	70590	11	29410	77073	15	22927	06483	4	93517	28
33	55 36	4 24	70611	12	29389	77101	16	22899	06490	4	93510	27
34	55 28	4 32	70633	12	29367	77130	16	22870	06498	4	93502	26
35	7 55 20	4 4 40	9. 70654	13	10. 29346	9. 77159	17	10. 22841	10. 06505	4	9. 93495	25
36	55 12	4 48	70675	13	29325	77188	17	22812	06513	4	93487	24
37	55 4	4 56	70697	13	29303	77217	18	22783	06520	5	93480	23
38	54 56	5 4	70718	14	29282	77246	18	22754	06528	5	93472	22
39	54 48	5 12	70739	14	29261	77274	19	22726	06535	5	93465	21
40	7 54 40	4 5 20	9. 70761	14	10. 29239	9. 77303	19	10. 22697	10. 06543	5	9. 93457	20
41	54 32	5 28	70782	15	29218	77332	20	22668	06550	5	93450	19
42	54 24	5 36	70803	15	29197	77361	20	22639	06558	5	93442	18
43	54 16	5 44	70824	15	29176	77390	21	22610	06565	5	93435	17
44	54 8	5 52	70846	16	29154	77418	21	22582	06573	5	93427	16
45	7 54 0	4 6 0	9. 70867	16	10. 29133	9. 77447	22	10. 22553	10. 06580	6	9. 93420	15
46	53 52	6 8	70888	16	29112	77476	22	22524	06588	6	93412	14
47	53 44	6 16	70909	17	29091	77505	23	22495	06595	6	93405	13
48	53 36	6 24	70931	17	29069	77533	23	22467	06603	6	93397	12
49	53 28	6 32	70952	18	29048	77562	24	22438	06610	6	93390	11
50	7 53 20	4 6 40	9. 70973	18	10. 29027	9. 77591	24	10. 22409	10. 06618	6	9. 93382	10
51	53 12	6 48	70994	18	29006	77619	25	22381	06625	6	93375	9
52	53 4	6 56	71015	19	28985	77648	25	22352	06633	6	93367	8
53	52 56	7 4	71036	19	28964	77677	26	22323	06640	7	93360	7
54	52 48	7 12	71058	19	28942	77706	26	22294	06648	7	93352	6
55	7 52 40	4 7 20	9. 71079	20	10. 28921	9. 77734	26	10. 22266	10. 06656	7	9. 93344	5
56	52 32	7 28	71100	20	28900	77763	27	22237	06663	7	93337	4
57	52 24	7 36	71121	20	28879	77791	27	22209	06671	7	93329	3
58	52 16	7 44	71142	21	28858	77820	28	22180	06678	7	93322	2
59	52 8	7 52	71163	21	28837	77849	28	22151	06686	7	93314	1
60	52 0	8 0	71184	21	28816	77877	29	22123	06693	7	93307	0
M.	Hour P. M	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
120°			A		A	B		B	C		C	59°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	3	5	8	11	13	16	19
	B	4	7	11	14	18	22	25
	C	1	2	3	4	5	6	7

TABLE 44.

Log. Sines, Tangents, and Secants.

31°			A		A	B		B	C		C	148°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	7 52 0	4 8 0	9.71184	0	10.28816	9.77877	0	10.22123	10.06693	0	9.93307	60
1	51 52	8 8	71205	0	28795	77906	0	22094	06701	0	93299	59
2	51 44	8 16	71226	1	28774	77935	1	22065	06709	0	93291	58
3	51 36	8 24	71247	1	28753	77963	1	22037	06716	0	93284	57
4	51 28	8 32	71268	1	28732	77992	2	22008	06724	1	93276	56
5	7 51 20	4 8 40	9.71289	2	10.28711	9.78020	2	10.21980	10.06731	1	9.93269	55
6	51 12	8 48	71310	2	28690	78049	3	21951	06739	1	93261	54
7	51 4	8 56	71331	2	28669	78077	3	21923	06747	1	93253	53
8	50 56	9 4	71352	3	28648	78106	4	21894	06754	1	93246	52
9	50 48	9 12	71373	3	28627	78135	4	21865	06762	1	93238	51
10	7 50 40	4 9 20	9.71393	3	10.28607	9.78163	5	10.21837	10.06770	1	9.93230	50
11	50 32	9 28	71414	4	28586	78192	5	21808	06777	1	93223	49
12	50 24	9 36	71435	4	28565	78220	6	21780	06785	2	93215	48
13	50 16	9 44	71456	4	28544	78249	6	21751	06793	2	93207	47
14	50 8	9 52	71477	5	28523	78277	7	21723	06800	2	93200	46
15	7 50 0	4 10 0	9.71498	5	10.28502	9.78306	7	10.21694	10.06808	2	9.93192	45
16	49 52	10 8	71519	5	28481	78334	8	21666	06816	2	93184	44
17	49 44	10 16	71539	6	28461	78363	8	21637	06823	2	93177	43
18	49 36	10 24	71560	6	28440	78391	9	21609	06831	2	93169	42
19	49 28	10 32	71581	7	28419	78419	9	21581	06839	2	93161	41
20	7 49 20	4 10 40	9.71602	7	10.28398	9.78448	9	10.21552	10.06846	3	9.93154	40
21	49 12	10 48	71622	7	28378	78476	10	21524	06854	3	93146	39
22	49 4	10 56	71643	8	28357	78505	10	21495	06862	3	93138	38
23	48 56	11 4	71664	8	28336	78533	11	21467	06869	3	93131	37
24	48 48	11 12	71685	8	28315	78562	11	21438	06877	3	93123	36
25	7 48 40	4 11 20	9.71705	9	10.28295	9.78590	12	10.21410	10.06885	3	9.93115	35
26	48 32	11 28	71726	9	28274	78618	12	21382	06892	3	93108	34
27	48 24	11 36	71747	9	28253	78647	13	21353	06900	3	93100	33
28	48 16	11 44	71767	10	28233	78675	13	21325	06908	4	93092	32
29	48 8	11 52	71788	10	28212	78704	14	21296	06916	4	93084	31
30	7 48 0	4 12 0	9.71809	10	10.28191	9.78732	14	10.21268	10.06923	4	9.93077	30
31	47 52	12 8	71829	11	28171	78760	15	21240	06931	4	93069	29
32	47 44	12 16	71850	11	28150	78789	15	21211	06939	4	93061	28
33	47 36	12 24	71870	11	28130	78817	16	21183	06947	4	93053	27
34	47 28	12 32	71891	12	28109	78845	16	21155	06954	4	93046	26
35	7 47 20	4 12 40	9.71911	12	10.28089	9.78874	17	10.21126	10.06962	5	9.93038	25
36	47 12	12 48	71932	12	28068	78902	17	21098	06970	5	93030	24
37	47 4	12 56	71952	13	28048	78930	17	21070	06978	5	93022	23
38	46 56	13 4	71973	13	28027	78959	18	21041	06986	5	93014	22
39	46 48	13 12	71994	13	28006	78987	18	21013	06993	5	93007	21
40	7 46 40	4 13 20	9.72014	14	10.27986	9.79015	19	10.20985	10.07001	5	9.92999	20
41	46 32	13 28	72034	14	27966	79043	19	20957	07009	5	92991	19
42	46 24	13 36	72055	14	27945	79072	20	20928	07017	5	92983	18
43	46 16	13 44	72075	15	27925	79100	20	20900	07024	6	92976	17
44	46 8	13 52	72096	15	27904	79128	21	20872	07032	6	92968	16
45	7 46 0	4 14 0	9.72116	15	10.27884	9.79156	21	10.20844	10.07040	6	9.92960	15
46	45 52	14 8	72137	16	27863	79185	22	20815	07048	6	92952	14
47	45 44	14 16	72157	16	27843	79213	22	20787	07056	6	92944	13
48	45 36	14 24	72177	16	27823	79241	23	20759	07064	6	92936	12
49	45 28	14 32	72198	17	27802	79269	23	20731	07071	6	92929	11
50	7 45 20	4 14 40	9.72218	17	10.27782	9.79297	24	10.20703	10.07079	6	9.92921	10
51	45 12	14 48	72238	18	27762	79326	24	20674	07087	7	92913	9
52	45 4	14 56	72259	18	27741	79354	25	20646	07095	7	92905	8
53	44 56	15 4	72279	18	27721	79382	25	20618	07103	7	92897	7
54	44 48	15 12	72299	19	27701	79410	26	20590	07111	7	92889	6
55	7 44 40	4 15 20	9.72320	19	10.27680	9.79438	26	10.20562	10.07119	7	9.92881	5
56	44 32	15 28	72340	19	27660	79466	26	20534	07126	7	92874	4
57	44 24	15 36	72360	20	27640	79495	27	20505	07134	7	92866	3
58	44 16	15 44	72381	20	27619	79523	27	20477	07142	7	92858	2
59	44 8	15 52	72401	20	27599	79551	28	20449	07150	8	92850	1
60	44 0	16 0	72421	21	27579	79579	28	20421	07158	8	92842	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
121°			A		A	B		B	C		C	58°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	3	5	8	10	13	15	18
	B	4	7	11	14	18	21	25
	C	1	2	3	4	5	6	7

TABLE 44.

Log. Sines, Tangents, and Secants.

32°			A		A	B		B	C		C	147°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	7 44 0	4 16 0	9.72421	0	10.27579	9.79579	0	10.20421	10.07158	0	9.92842	60
1	43 52	16 8	72441	0	27559	79607	0	20393	07166	0	92834	59
2	43 44	16 16	72461	1	27539	79635	1	20365	07174	0	92826	58
3	43 36	16 24	72482	1	27518	79663	1	20337	07182	0	92818	57
4	43 28	16 32	72502	1	27498	79691	2	20309	07190	1	92810	56
5	7 43 20	4 16 40	9.72522	2	10.27478	9.79719	2	10.20281	10.07197	1	9.92803	55
6	43 12	16 48	72542	2	27458	79747	3	20253	07205	1	92795	54
7	43 4	16 56	72562	2	27438	79776	3	20224	07213	1	92787	53
8	42 56	17 4	72582	3	27418	79804	4	20196	07221	1	92779	52
9	42 48	17 12	72602	3	27398	79832	4	20168	07229	1	92771	51
10	7 42 40	4 17 20	9.72622	3	10.27378	9.79860	5	10.20140	10.07237	1	9.92763	50
11	42 32	17 28	72643	4	27357	79888	5	20112	07245	1	92755	49
12	42 24	17 36	72663	4	27337	79916	6	20084	07253	2	92747	48
13	42 16	17 44	72683	4	27317	79944	6	20056	07261	2	92739	47
14	42 8	17 52	72703	5	27297	79972	7	20028	07269	2	92731	46
15	7 42 0	4 18 0	9.72723	5	10.27277	9.80000	7	10.20000	10.07277	2	9.92723	45
16	41 52	18 8	72743	5	27257	80028	7	19972	07285	2	92715	44
17	41 44	18 16	72763	6	27237	80056	8	19944	07293	2	92707	43
18	41 36	18 24	72783	6	27217	80084	8	19916	07301	2	92699	42
19	41 28	18 32	72803	6	27197	80112	9	19888	07309	3	92691	41
20	7 41 20	4 18 40	9.72823	7	10.27177	9.80140	9	10.19860	10.07317	3	9.92683	40
21	41 12	18 48	72843	7	27157	80168	10	19832	07325	3	92675	39
22	41 4	18 56	72863	7	27137	80195	10	19805	07333	3	92667	38
23	40 56	19 4	72883	8	27117	80223	11	19777	07341	3	92659	37
24	40 48	19 12	72902	8	27098	80251	11	19749	07349	3	92651	36
25	7 40 40	4 19 20	9.72922	8	10.27078	9.80279	12	10.19721	10.07357	3	9.92643	35
26	40 32	19 28	72942	9	27058	80307	12	19693	07365	3	92635	34
27	40 24	19 36	72962	9	27038	80335	13	19665	07373	4	92627	33
28	40 16	19 44	72982	9	27018	80363	13	19637	07381	4	92619	32
29	40 8	19 52	73002	10	26998	80391	13	19609	07389	4	92611	31
30	7 40 0	4 20 0	9.73022	10	10.26978	9.80419	14	10.19581	10.07397	4	9.92603	30
31	39 52	20 8	73041	10	26959	80447	14	19553	07405	4	92595	29
32	39 44	20 16	73061	11	26939	80474	15	19526	07413	4	92587	28
33	39 36	20 24	73081	11	26919	80502	15	19498	07421	4	92579	27
34	39 28	20 32	73101	11	26899	80530	16	19470	07429	5	92571	26
35	7 39 20	4 20 40	9.73121	12	10.26879	9.80558	16	10.19442	10.07437	5	9.92563	25
36	39 12	20 48	73140	12	26860	80586	17	19414	07445	5	92555	24
37	39 4	20 56	73160	12	26840	80614	17	19386	07454	5	92546	23
38	38 56	21 4	73180	13	26820	80642	18	19358	07462	5	92538	22
39	38 48	21 12	73200	13	26800	80669	18	19331	07470	5	92530	21
40	7 38 40	4 21 20	9.73219	13	10.26781	9.80697	19	10.19303	10.07478	5	9.92522	20
41	38 32	21 28	73239	14	26761	80725	19	19275	07486	6	92514	19
42	38 24	21 36	73259	14	26741	80753	20	19247	07494	6	92506	18
43	38 16	21 44	73278	14	26722	80781	20	19219	07502	6	92498	17
44	38 8	21 52	73298	15	26702	80808	20	19192	07510	6	92490	16
45	7 38 0	4 22 0	9.73318	15	10.26682	9.80836	21	10.19164	10.07518	6	9.92482	15
46	37 52	22 8	73337	15	26663	80864	21	19136	07527	6	92473	14
47	37 44	22 16	73357	16	26643	80892	22	19108	07535	6	92465	13
48	37 36	22 24	73377	16	26623	80919	22	19081	07543	6	92457	12
49	37 28	22 32	73396	16	26604	80947	23	19053	07551	7	92449	11
50	7 37 20	4 22 40	9.73416	17	10.26584	9.80975	23	10.19025	10.07559	7	9.92441	10
51	37 12	22 48	73435	17	26565	81003	24	18997	07567	7	92433	9
52	37 4	22 56	73455	17	26545	81030	24	18970	07575	7	92425	8
53	36 56	23 4	73474	18	26526	81058	25	18942	07584	7	92416	7
54	36 48	23 12	73494	18	26506	81086	25	18914	07592	7	92408	6
55	7 36 40	4 23 20	9.73513	18	10.26487	9.81113	26	10.18887	10.07600	7	9.92400	5
56	36 32	23 28	73533	19	26467	81141	26	18859	07608	8	92392	4
57	36 24	23 36	73552	19	26448	81169	26	18831	07616	8	92384	3
58	36 16	23 44	73572	19	26428	81196	27	18804	07624	8	92376	2
59	36 8	23 52	73591	20	26409	81224	27	18776	07633	8	92367	1
60	36 0	24 0	73611	20	26389	81252	28	18748	07641	8	92359	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
122°			A		A	B		B	C		C	57°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	5	7	10	12	15	17
	B	3	7	10	14	17	21	24
	C	1	2	3	4	5	6	7

TABLE 44.

Log. Sines, Tangents, and Secants.

33°			A		A	B		B	C		C	146°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	7 36 0	4 24 0	9.73611	0	10.26389	9.81252	0	10.18748	10.07641	0	9.92359	60
1	35 52	24 8	73630	0	26370	81279	0	18721	07649	0	92351	59
2	35 44	24 16	73650	1	26350	81307	1	18693	07657	0	92343	58
3	35 36	24 24	73669	1	26331	81335	1	18665	07665	0	92335	57
4	35 28	24 32	73689	1	26311	81362	2	18638	07674	1	92326	56
5	7 35 20	4 24 40	9.73708	2	10.26292	9.81390	2	10.18610	10.07682	1	9.92318	55
6	35 12	24 48	73727	2	26273	81418	3	18582	07690	1	92310	54
7	35 4	24 56	73747	2	26253	81445	3	18555	07698	1	92302	53
8	34 56	25 4	73766	3	26234	81473	4	18527	07707	1	92293	52
9	34 48	25 12	73785	3	26215	81500	4	18500	07715	1	92285	51
10	7 34 40	4 25 20	9.73805	3	10.26195	9.81528	5	10.18472	10.07723	1	9.92277	50
11	34 32	25 28	73824	3	26176	81556	5	18444	07731	2	92269	49
12	34 24	25 36	73843	4	26157	81583	5	18417	07740	2	92260	48
13	34 16	25 44	73863	4	26137	81611	6	18389	07748	2	92252	47
14	34 8	25 52	73882	4	26118	81638	6	18362	07756	2	92244	46
15	7 34 0	4 26 0	9.73901	5	10.26099	9.81666	7	10.18334	10.07765	2	9.92235	45
16	33 52	26 8	73921	5	26079	81693	7	18307	07773	2	92227	44
17	33 44	26 16	73940	5	26060	81721	8	18279	07781	2	92219	43
18	33 36	26 24	73959	6	26041	81748	8	18252	07789	3	92211	42
19	33 28	26 32	73978	6	26022	81776	9	18224	07798	3	92202	41
20	7 33 20	4 26 40	9.73997	6	10.26003	9.81803	9	10.18197	10.07806	3	9.92194	40
21	33 12	26 48	74017	7	25983	81831	10	18169	07814	3	92186	39
22	33 4	26 56	74036	7	25964	81858	10	18142	07823	3	92177	38
23	32 56	27 4	74055	7	25945	81886	11	18114	07831	3	92169	37
24	32 48	27 12	74074	8	25926	81913	11	18087	07839	3	92161	36
25	7 32 40	4 27 20	9.74093	8	10.25907	9.81941	11	10.18059	10.07848	3	9.92152	35
26	32 32	27 28	74113	8	25887	81968	12	18032	07856	4	92144	34
27	32 24	27 36	74132	9	25868	81996	12	18004	07864	4	92136	33
28	32 16	27 44	74151	9	25849	82023	13	17977	07873	4	92127	32
29	32 8	27 52	74170	9	25830	82051	13	17949	07881	4	92119	31
30	7 32 0	4 28 0	9.74189	10	10.25811	9.82078	14	10.17922	10.07889	4	9.92111	30
31	31 52	28 8	74208	10	25792	82106	14	17894	07898	4	92102	29
32	31 44	28 16	74227	10	25773	82133	15	17867	07906	4	92094	28
33	31 36	28 24	74246	10	25754	82161	15	17839	07914	5	92086	27
34	31 28	28 32	74265	11	25735	82188	16	17812	07923	5	92077	26
35	7 31 20	4 28 40	9.74284	11	10.25716	9.82215	16	10.17785	10.07931	5	9.92069	25
36	31 12	28 48	74303	11	25697	82243	16	17757	07940	5	92060	24
37	31 4	28 56	74322	12	25678	82270	17	17730	07948	5	92052	23
38	30 56	29 4	74341	12	25659	82298	17	17702	07956	5	92044	22
39	30 48	29 12	74360	12	25640	82325	18	17675	07965	5	92035	21
40	7 30 40	4 29 20	9.74379	13	10.25621	9.82352	18	10.17648	10.07973	6	9.92027	20
41	30 32	29 28	74398	13	25602	82380	19	17620	07982	6	92018	19
42	30 24	29 36	74417	13	25583	82407	19	17593	07990	6	92010	18
43	30 16	29 44	74436	14	25564	82435	20	17565	07998	6	92002	17
44	30 8	29 52	74455	14	25545	82462	20	17538	08007	6	91993	16
45	7 30 0	4 30 0	9.74474	14	10.25526	9.82489	21	10.17511	10.08015	6	9.91985	15
46	29 52	30 8	74493	15	25507	82517	21	17483	08024	6	91976	14
47	29 44	30 16	74512	15	25488	82544	22	17456	08032	7	91968	13
48	29 36	30 24	74531	15	25469	82571	22	17429	08041	7	91959	12
49	29 28	30 32	74549	16	25451	82599	22	17401	08049	7	91951	11
50	7 29 20	4 30 40	9.74568	16	10.25432	9.82626	23	10.17374	10.08058	7	9.91942	10
51	29 12	30 48	74587	16	25413	82653	23	17347	08066	7	91934	9
52	29 4	30 56	74606	17	25394	82681	24	17319	08075	7	91925	8
53	28 56	31 4	74625	17	25375	82708	24	17292	08083	7	91917	7
54	28 48	31 12	74644	17	25356	82735	25	17265	08092	8	91908	6
55	7 28 40	4 31 20	9.74662	17	10.25338	9.82762	25	10.17238	10.08100	8	9.91900	5
56	28 32	31 28	74681	18	25319	82790	26	17210	08109	8	91891	4
57	28 24	31 36	74700	18	25300	82817	26	17183	08117	8	91883	3
58	28 16	31 44	74719	18	25281	82844	27	17156	08126	8	91874	2
59	28 8	31 52	74737	19	25263	82871	27	17129	08134	8	91866	1
60	28 0	32 0	74756	19	25244	82899	27	17101	08143	8	91857	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
123°			A			B		B	C		C	56°

Seconds of time	1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols. A	2	5	7	10	12	14	17
Prop. parts of cols. B	3	7	10	14	17	21	24
Prop. parts of cols. C	1	2	3	4	5	6	7

6583—06——41

TABLE 44.

Log. Sines, Tangents, and Secants.

34°			A		A	B		B	C		C	145°
M.	Hour A.M.	Hour P.M.	Sine.	Diff.	Cosecant	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	7 28 0	4 32 0	9.74756	0	10.25244	9.82899	0	10.17101	10.08143	0	9.91857	60
1	27 52	32 8	74775	0	25225	82926	0	17074	08151	0	91849	59
2	27 44	32 16	74794	1	25206	82953	1	17047	08160	0	91840	58
3	27 36	32 24	74812	1	25188	82980	1	17020	08168	0	91832	57
4	27 28	32 32	74831	1	25169	83008	2	16992	08177	1	91823	56
5	7 27 20	4 32 40	9.74850	2	10.25150	9.83035	2	10.16965	10.08185	1	9.91815	55
6	27 12	32 48	74868	2	25132	83062	3	16938	08194	1	91806	54
7	27 4	32 56	74887	2	25113	83089	3	16911	08202	1	91798	53
8	26 56	33 4	74906	2	25094	83117	4	16883	08211	1	91789	52
9	26 48	33 12	74924	3	25076	83144	4	16856	08219	1	91781	51
10	7 26 40	4 33 20	9.74943	3	10.25057	9.83171	5	10.16829	10.08228	1	9.91772	50
11	26 32	33 28	74961	3	25039	83198	5	16802	08237	2	91763	49
12	26 24	33 36	74980	4	25020	83225	5	16775	08245	2	91755	48
13	26 16	33 44	74999	4	25001	83252	6	16748	08254	2	91746	47
14	26 8	33 52	75017	4	24983	83280	6	16720	08262	2	91738	46
15	7 26 0	4 34 0	9.75036	5	10.24964	9.83307	7	10.16693	10.08271	2	9.91729	45
16	25 52	34 8	75054	5	24946	83334	7	16666	08280	2	91720	44
17	25 44	34 16	75073	5	24927	83361	8	16639	08288	2	91712	43
18	25 36	34 24	75091	6	24909	83388	8	16612	08297	3	91703	42
19	25 28	34 32	75110	6	24890	83415	9	16585	08305	3	91695	41
20	7 25 20	4 34 40	9.75128	6	10.24872	9.83442	9	10.16558	10.08314	3	9.91686	40
21	25 12	34 48	75147	6	24853	83470	9	16530	08323	3	91677	39
22	25 4	34 56	75165	7	24835	83497	10	16503	08331	3	91669	38
23	24 56	35 4	75184	7	24816	83524	10	16476	08340	3	91660	37
24	24 48	35 12	75202	7	24798	83551	11	16449	08349	3	91651	36
25	7 24 40	4 35 20	9.75221	8	10.24779	9.83578	11	10.16422	10.08357	4	9.91643	35
26	24 32	35 28	75239	8	24761	83605	12	16395	08366	4	91634	34
27	24 24	35 36	75258	8	24742	83632	12	16368	08375	4	91625	33
28	24 16	35 44	75276	9	24724	83659	13	16341	08383	4	91617	32
29	24 8	35 52	75294	9	24706	83686	13	16314	08392	4	91608	31
30	7 24 0	4 36 0	9.75313	9	10.24687	9.83713	14	10.16287	10.08401	4	9.91599	30
31	23 52	36 8	75331	9	24669	83740	14	16260	08409	4	91591	29
32	23 44	36 16	75350	10	24650	83768	14	16232	08418	5	91582	28
33	23 36	36 24	75368	10	24632	83795	15	16205	08427	5	91573	27
34	23 28	36 32	75386	10	24614	83822	15	16178	08435	5	91565	26
35	7 23 20	4 36 40	9.75405	11	10.24595	9.83849	16	10.16151	10.08444	5	9.91556	25
36	23 12	36 48	75423	11	24577	83876	16	16124	08453	5	91547	24
37	23 4	36 56	75441	11	24559	83903	17	16097	08462	5	91538	23
38	22 56	37 4	75459	12	24541	83930	17	16070	08470	5	91530	22
39	22 48	37 12	75478	12	24522	83957	18	16043	08479	6	91521	21
40	7 22 40	4 37 20	9.75496	12	10.24504	9.83984	18	10.16016	10.08488	6	9.91512	20
41	22 32	37 28	75514	13	24486	84011	18	15989	08496	6	91504	19
42	22 24	37 36	75533	13	24467	84038	19	15962	08505	6	91495	18
43	22 16	37 44	75551	13	24449	84065	19	15935	08514	6	91486	17
44	22 8	37 52	75569	13	24431	84092	20	15908	08523	6	91477	16
45	7 22 0	4 38 0	9.75587	14	10.24413	9.84119	20	10.15881	10.08531	7	9.91469	15
46	21 52	38 8	75605	14	24395	84146	21	15854	08540	7	91460	14
47	21 44	38 16	75624	14	24376	84173	21	15827	08549	7	91451	13
48	21 36	38 24	75642	15	24358	84200	22	15800	08558	7	91442	12
49	21 28	38 32	75660	15	24340	84227	22	15773	08567	7	91433	11
50	7 21 20	4 38 40	9.75678	15	10.24322	9.84254	23	10.15746	10.08575	7	9.91425	10
51	21 12	38 48	75696	16	24304	84280	23	15720	08584	7	91416	9
52	21 4	38 56	75714	16	24286	84307	23	15693	08593	8	91407	8
53	20 56	39 4	75733	16	24267	84334	24	15666	08602	8	91398	7
54	20 48	39 12	75751	17	24249	84361	24	15639	08611	8	91389	6
55	7 20 40	4 39 20	9.75769	17	10.24231	9.84388	25	10.15612	10.08619	8	9.91381	5
56	20 32	39 28	75787	17	24213	84415	25	15585	08628	8	91372	4
57	20 24	39 36	75805	17	24195	84442	26	15558	08637	8	91363	3
58	20 16	39 44	75823	18	24177	84469	26	15531	08646	8	91354	2
59	20 8	39 52	75841	18	24159	84496	27	15504	08655	9	91345	1
60	20 0	40 0	75859	18	24141	84523	27	15477	08664	9	91336	0
M.	Hour P.M.	Hour A.M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
124°			A		A	B		B	C		C	55

Seconds of time		1^s	2^s	3^s	4^s	5^s	6^s	7^s
Prop. parts of cols.	A	2	5	7	9	11	14	16
	B	3	7	10	14	17	20	24
	C	1	2	3	4	5	7	8

Log. Sines, Tangents, and Secants.

35°			A		A	B		B	C		C	144°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	7 20 0	4 40 0	9.75859	0	10.24141	9.84523	0	10.15477	10.08664	0	9.91336	60
1	19 52	40 8	75877	0	24123	84550	0	15450	08672	0	91328	59
2	19 44	40 16	75895	1	24105	84576	1	15424	08681	0	91319	58
3	19 36	40 24	75913	1	24087	84603	1	15397	08690	0	91310	57
4	19 28	40 32	75931	1	24069	84630	2	15370	08699	1	91301	56
5	7 19 20	4 40 40	9.75949	1	10.24051	9.84657	2	10.15343	10.08708	1	9.91292	55
6	19 12	40 48	75967	2	24033	84684	3	15316	08717	1	91283	54
7	19 4	40 56	75985	2	24015	84711	3	15289	08726	1	91274	53
8	18 56	41 4	76003	2	23997	84738	4	15262	08734	1	91266	52
9	18 48	41 12	76021	3	23979	84764	4	15236	08743	1	91257	51
10	7 18 40	4 41 20	9.76039	3	10.23961	9.84791	4	10.15209	10.08752	2	9.91248	50
11	18 32	41 28	76057	3	23943	84818	5	15182	08761	2	91239	49
12	18 24	41 36	76075	4	23925	84845	5	15155	08770	2	91230	48
13	18 16	41 44	76093	4	23907	84872	6	15128	08779	2	91221	47
14	18 8	41 52	76111	4	23889	84899	6	15101	08788	2	91212	46
15	7 18 0	4 42 0	9.76129	4	10.23871	9.84925	7	10.15075	10.08797	2	9.91203	45
16	17 52	42 8	76146	5	23854	84952	7	15048	08806	2	91194	44
17	17 44	42 16	76164	5	23836	84979	8	15021	08815	3	91185	43
18	17 36	42 24	76182	5	23818	85006	8	14994	08824	3	91176	42
19	17 28	42 32	76200	6	23800	85033	8	14967	08833	3	91167	41
20	7 17 20	4 42 40	9.76218	6	10.23782	9.85059	9	10.14941	10.08842	3	9.91158	40
21	17 12	42 48	76236	6	23764	85086	9	14914	08851	3	91149	39
22	17 4	42 56	76253	6	23747	85113	10	14887	08859	3	91141	38
23	16 56	43 4	76271	7	23729	85140	10	14860	08868	3	91132	37
24	16 48	43 12	76289	7	23711	85166	11	14834	08877	4	91123	36
25	7 16 40	4 43 20	9.76307	7	10.23693	9.85193	11	10.14807	10.08886	4	9.91114	35
26	16 32	43 28	76324	8	23676	85220	12	14780	08895	4	91105	34
27	16 24	43 36	76342	8	23658	85247	12	14753	08904	4	91096	33
28	16 16	43 44	76360	8	23640	85273	12	14727	08913	4	91087	32
29	16 8	43 52	76378	9	23622	85300	13	14700	08922	4	91078	31
30	7 16 0	4 44 0	9.76395	9	10.23605	9.85327	13	10.14673	10.08931	5	9.91069	30
31	15 52	44 8	76413	9	23587	85354	14	14646	08940	5	91060	29
32	15 44	44 16	76431	9	23569	85380	14	14620	08949	5	91051	28
33	15 36	44 24	76448	10	23552	85407	15	14593	08958	5	91042	27
34	15 28	44 32	76466	10	23534	85434	15	14566	08967	5	91033	26
35	7 15 20	4 44 40	9.76484	10	10.23516	9.85460	16	10.14540	10.08977	5	9.91023	25
36	15 12	44 48	76501	11	23499	85487	16	14513	08986	5	91014	24
37	15 4	44 56	76519	11	23481	85514	16	14486	08995	6	91005	23
38	14 56	45 4	76537	11	23463	85540	17	14460	09004	6	90996	22
39	14 48	45 12	76554	12	23446	85567	17	14433	09013	6	90987	21
40	7 14 40	4 45 20	9.76572	12	10.23428	9.85594	18	10.14406	10.09022	6	9.90978	20
41	14 32	45 28	76590	12	23410	85620	18	14380	09031	6	90969	19
42	14 24	45 36	76607	12	23393	85647	19	14353	09040	6	90960	18
43	14 16	45 44	76625	13	23375	85674	19	14326	09049	6	90951	17
44	14 8	45 52	76642	13	23358	85700	20	14300	09058	7	90942	16
45	7 14 0	4 46 0	9.76660	13	10.23340	9.85727	20	10.14273	10.09067	7	9.90933	15
46	13 52	46 8	76677	14	23323	85754	20	14246	09076	7	90924	14
47	13 44	46 16	76695	14	23305	85780	21	14220	09085	7	90915	13
48	13 36	46 24	76712	14	23288	85807	21	14193	09094	7	90906	12
49	13 28	46 32	76730	14	23270	85834	22	14166	09104	7	90896	11
50	7 13 20	4 46 40	9.76747	15	10.23253	9.85860	22	10.14140	10.09113	8	9.90887	10
51	13 12	46 48	76765	15	23235	85887	23	14113	09122	8	90878	9
52	13 4	46 56	76782	15	23218	85913	23	14087	09131	8	90869	8
53	12 56	47 4	76800	16	23200	85940	24	14060	09140	8	90860	7
54	12 48	47 12	76817	16	23183	85967	24	14033	09149	8	90851	6
55	7 12 40	4 47 20	9.76835	16	10.23165	9.85993	24	10.14007	10.09158	8	9.90842	5
56	12 32	47 28	76852	17	23148	86020	25	13980	09168	8	90832	4
57	12 24	47 36	76870	17	23130	86046	25	13954	09177	9	90823	3
58	12 16	47 44	76887	17	23113	86073	26	13927	09186	9	90814	2
59	12 8	47 52	76904	17	23096	86100	26	13900	09195	9	90805	1
60	12 0	48 0	76922	18	23078	86126	27	13874	09204	9	90796	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
125°			A		A	B		B	C		C	54°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	4	7	9	11	13	16
	B	3	7	10	13	17	20	23
	C	1	2	3	5	6	7	8

TABLE 44.

Log. Sines, Tangents, and Secants.

36°			A		A	B		B	C		C	143°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	7 12 0	4 48 0	9.76922	0	10.23078	9.86126	0	10.13874	10.09204	0	9.90796	60
1	11 52	48 8	76939	0	23061	86153	0	13847	09213	0	90787	59
2	11 44	48 16	76957	1	23043	86179	1	13821	09223	0	90777	58
3	11 36	48 24	76974	1	23026	86206	1	13794	09232	0	90768	57
4	11 28	48 32	76991	1	23009	86232	2	13768	09241	1	90759	56
5	7 11 20	4 48 40	9.77009	1	10.22991	9.86259	2	10.13741	10.09250	1	9.90750	55
6	11 12	48 48	77026	2	22974	86285	3	13715	09259	1	90741	54
7	11 4	48 56	77043	2	22957	86312	3	13688	09269	1	90731	53
8	10 56	49 4	77061	2	22939	86338	4	13662	09278	1	90722	52
9	10 48	49 12	77078	3	22922	86365	4	13635	09287	1	90713	51
10	7 10 40	4 49 20	9.77095	3	10.22905	9.86392	4	10.13608	10.09296	2	9.90704	50
11	10 32	49 28	77112	3	22888	86418	5	13582	09306	2	90694	49
12	10 24	49 36	77130	3	22870	86445	5	13555	09315	2	90685	48
13	10 16	49 44	77147	4	22853	86471	6	13529	09324	2	90676	47
14	10 8	49 52	77164	4	22836	86498	6	13502	09333	2	90667	46
15	7 10 0	4 50 0	9.77181	4	10.22819	9.86524	7	10.13476	10.09343	2	9.90657	45
16	9 52	50 8	77199	5	22801	86551	7	13449	09352	2	90648	44
17	9 44	50 16	77216	5	22784	86577	7	13423	09361	3	90639	43
18	9 36	50 24	77233	5	22767	86603	8	13397	09370	3	90630	42
19	9 28	50 32	77250	5	22750	86630	8	13370	09380	3	90620	41
20	7 9 20	4 50 40	9.77268	6	10.22732	9.86656	9	10.13344	10.09389	3	9.90611	40
21	9 12	50 48	77285	6	22715	86683	9	13317	09398	3	90602	39
22	9 4	50 56	77302	6	22698	86709	10	13291	09408	3	90592	38
23	8 56	51 4	77319	7	22681	86736	10	13264	09417	4	90583	37
24	8 48	51 12	77336	7	22664	86762	11	13238	09426	4	90574	36
25	7 8 40	4 51 20	9.77353	7	10.22647	9.86789	11	10.13211	10.09435	4	9.90565	35
26	8 32	51 28	77370	7	22630	86815	11	13185	09445	4	90555	34
27	8 24	51 36	77387	8	22613	86842	12	13158	09454	4	90546	33
28	8 16	51 44	77405	8	22595	86868	12	13132	09463	4	90537	32
29	8 8	51 52	77422	8	22578	86894	13	13106	09473	5	90527	31
30	7 8 0	4 52 0	9.77439	9	10.22561	9.86921	13	10.13079	10.09482	5	9.90518	30
31	7 52	52 8	77456	9	22544	86947	14	13053	09491	5	90509	29
32	7 44	52 16	77473	9	22527	86974	14	13026	09501	5	90499	28
33	7 36	52 24	77490	9	22510	87000	15	13000	09510	5	90490	27
34	7 28	52 32	77507	10	22493	87027	15	12973	09520	5	90480	26
35	7 7 20	4 52 40	9.77524	10	10.22476	9.87053	15	10.12947	10.09529	5	9.90471	25
36	7 12	52 48	77541	10	22459	87079	16	12921	09538	6	90462	24
37	7 4	52 56	77558	11	22442	87106	16	12894	09548	6	90452	23
38	6 56	53 4	77575	11	22425	87132	17	12868	09557	6	90443	22
39	6 48	53 12	77592	11	22408	87158	17	12842	09566	6	90434	21
40	7 6 40	4 53 20	9.77609	11	10.22391	9.87185	18	10.12815	10.09576	6	9.90424	20
41	6 32	53 28	77626	12	22374	87211	18	12789	09585	6	90415	19
42	6 24	53 36	77643	12	22357	87238	18	12762	09595	7	90405	18
43	6 16	53 44	77660	12	22340	87264	19	12736	09604	7	90396	17
44	6 8	53 52	77677	13	22323	87290	19	12710	09614	7	90386	16
45	7 6 0	4 54 0	9.77694	13	10.22306	9.87317	20	10.12683	10.09623	7	9.90377	15
46	5 52	54 8	77711	13	22289	87343	20	12657	09632	7	90368	14
47	5 44	54 16	77728	13	22272	87369	21	12631	09642	7	90358	13
48	5 36	54 24	77744	14	22256	87396	21	12604	09651	7	90349	12
49	5 28	54 32	77761	14	22239	87422	22	12578	09661	8	90339	11
50	7 5 20	4 54 40	9.77778	14	10.22222	9.87448	22	10.12552	10.09670	8	9.90330	10
51	5 12	54 48	77795	15	22205	87475	22	12525	09680	8	90320	9
52	5 4	54 56	77812	15	22188	87501	23	12499	09689	8	90311	8
53	4 56	55 4	77829	15	22171	87527	23	12473	09699	8	90301	7
54	4 48	55 12	77846	15	22154	87554	24	12446	09708	8	90292	6
55	7 4 40	4 55 20	9.77862	16	10.22138	9.87580	24	10.12420	10.09718	9	9.90282	5
56	4 32	55 28	77879	16	22121	87606	25	12394	09727	9	90273	4
57	4 24	55 36	77896	16	22104	87633	25	12367	09737	9	90263	3
58	4 16	55 44	77913	16	22087	87659	26	12341	09746	9	90254	2
59	4 8	55 52	77930	17	22070	87685	26	12315	09756	9	90244	1
60	4 0	56 0	77946	17	22054	87711	26	12289	09765	9	90235	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
126°			A		A	B		B	C		C	53°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	4	6	9	11	13	15
	B	3	7	10	13	17	20	23
	C	1	2	4	5	6	7	8

TABLE 44.

Log. Sines, Tangents, and Secants.

37°			A		A	B		B	C		C	142°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	7 4 0	4 56 0	9.77946	0	10.22054	9.87711	0	10.12289	10.09765	0	9.90235	60
1	3 52	56 8	77963	0	22037	87738	0	12262	09775	0	90225	59
2	3 44	56 16	77980	1	22020	87764	1	12236	09784	0	90216	58
3	3 36	56 24	77997	1	22003	87790	1	12210	09794	0	90206	57
4	3 28	56 32	78013	1	21987	87817	2	12183	09803	1	90197	56
5	7 3 20	4 56 40	9.78030	1	10.21970	9.87843	2	10.12157	10.09813	1	9.90187	55
6	3 12	56 48	78047	2	21953	87869	3	12131	09822	1	90178	54
7	3 4	56 56	78063	2	21937	87895	3	12105	09832	1	90168	53
8	2 56	57 4	78080	2	21920	87922	3	12078	09841	1	90159	52
9	2 48	57 12	78097	2	21903	87948	4	12052	09851	1	90149	51
10	7 2 40	4 57 20	9.78113	3	10.21887	9.87974	4	10.12026	10.09861	2	9.90139	50
11	2 32	57 28	78130	3	21870	88000	5	12000	09870	2	90130	49
12	2 24	57 36	78147	3	21853	88027	5	11973	09880	2	90120	48
13	2 16	57 44	78163	4	21837	88053	6	11947	09889	2	90111	47
14	2 8	57 52	78180	4	21820	88079	6	11921	09899	2	90101	46
15	7 2 0	4 58 0	9.78197	4	10.21803	9.88105	7	10.11895	10.09909	2	9.90091	45
16	1 52	58 8	78213	4	21787	88131	7	11869	09918	3	90082	44
17	1 44	58 16	78230	5	21770	88158	7	11842	09928	3	90072	43
18	1 36	58 24	78246	5	21754	88184	8	11816	09937	3	90063	42
19	1 28	58 32	78263	5	21737	88210	8	11790	09947	3	90053	41
20	7 1 20	4 58 40	9.78280	5	10.21720	9.88236	9	10.11764	10.09957	3	9.90043	40
21	1 12	58 48	78296	6	21704	88262	9	11738	09966	3	90034	39
22	1 4	58 56	78313	6	21687	88289	10	11711	09976	4	90024	38
23	0 56	59 4	78329	6	21671	88315	10	11685	09986	4	90014	37
24	0 48	59 12	78346	7	21654	88341	10	11659	09995	4	90005	36
25	7 0 40	4 59 20	9.78362	7	10.21638	9.88367	11	10.11633	10.10005	4	9.89995	35
26	0 32	59 28	78379	7	21621	88393	11	11607	10015	4	89985	34
27	0 24	59 36	78395	7	21605	88420	12	11580	10024	4	89976	33
28	0 16	59 44	78412	8	21588	88446	12	11554	10034	5	89966	32
29	0 8	59 52	78428	8	21572	88472	13	11528	10044	5	89956	31
30	7 0 0	5 0 0	9.78445	8	10.21555	9.88498	13	10.11502	10.10053	5	9.89947	30
31	6 59 52	0 8	78461	9	21539	88524	14	11476	10063	5	89937	29
32	59 44	0 16	78478	9	21522	88550	14	11450	10073	5	89927	28
33	59 36	0 24	78494	9	21506	88577	14	11423	10082	5	89918	27
34	59 28	0 32	78510	9	21490	88603	15	11397	10092	5	89908	26
35	6 59 20	5 0 40	9.78527	10	10.21473	9.88629	15	10.11371	10.10102	6	9.89898	25
36	59 12	0 48	78543	10	21457	88655	16	11345	10112	6	89888	24
37	59 4	0 56	78560	10	21440	88681	16	11319	10121	6	89879	23
38	58 56	1 4	78576	10	21424	88707	17	11293	10131	6	89869	22
39	58 48	1 12	78592	11	21408	88733	17	11267	10141	6	89859	21
40	6 58 40	5 1 20	9.78609	11	10.21391	9.88759	17	10.11241	10.10151	6	9.89849	20
41	58 32	1 28	78625	11	21375	88786	18	11214	10160	7	89840	19
42	58 24	1 36	78642	12	21358	88812	18	11188	10170	7	89830	18
43	58 16	1 44	78658	12	21342	88838	19	11162	10180	7	89820	17
44	58 8	1 52	78674	12	21326	88864	19	11136	10190	7	89810	16
45	6 58 0	5 2 0	9.78691	12	10.21309	9.88890	20	10.11110	10.10199	7	9.89801	15
46	57 52	2 8	78707	13	21293	88916	20	11084	10209	7	89791	14
47	57 44	2 16	78723	13	21277	88942	20	11058	10219	8	89781	13
48	57 36	2 24	78739	13	21261	88968	21	11032	10229	8	89771	12
49	57 28	2 32	78756	13	21244	88994	21	11006	10239	8	89761	11
50	6 57 20	5 2 40	9.78772	14	10.21228	9.89020	22	10.10980	10.10248	8	9.89752	10
51	57 12	2 48	78788	14	21212	89046	22	10954	10258	8	89742	9
52	57 4	2 56	78805	14	21195	89073	23	10927	10268	8	89732	8
53	56 56	3 4	78821	15	21179	89099	23	10901	10278	9	89722	7
54	56 48	3 12	78837	15	21163	89125	24	10875	10288	9	89712	6
55	6 56 40	5 3 20	9.78853	15	10.21147	9.89151	24	10.10849	10.10298	9	9.89702	5
56	56 32	3 28	78869	15	21131	89177	24	10823	10307	9	89693	4
57	56 24	3 36	78886	16	21114	89203	25	10797	10317	9	89683	3
58	56 16	3 44	78902	16	21098	89229	25	10771	10327	9	89673	2
59	56 8	3 52	78918	16	21082	89255	26	10745	10337	10	89663	1
60	56 0	4 0	78934	16	21066	89281	26	10719	10347	10	89653	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
127°			A		A	B		B	C		C	52°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	4	6	8	10	12	14
	B	3	7	10	13	16	20	23
	C	1	2	4	5	6	7	8

TABLE 44.

Log. Sines, Tangents, and Secants.

38°			A		A	B		B	C		C	141°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	6 56 0	5 4 0	9.78934	0	10.21066	9.89281	0	10.10719	10.10347	0	9.89653	60
1	55 52	4 8	78950	0	21050	89307	0	10693	10357	0	89643	59
2	55 44	4 16	78967	1	21033	89333	1	10667	10367	0	89633	58
3	55 36	4 24	78983	1	21017	89359	1	10641	10376	1	89624	57
4	55 28	4 32	78999	1	21001	89385	2	10615	10386	1	89614	56
5	6 55 20	5 4 40	9.79015	1	10.20985	9.89411	2	10.10589	10.10396	1	9.89604	55
6	55 12	4 48	79031	2	20969	89437	3	10563	10406	1	89594	54
7	55 4	4 56	79047	2	20953	89463	3	10537	10416	1	89584	53
8	54 56	5 4	79063	2	20937	89489	3	10511	10426	1	89574	52
9	54 48	5 12	79079	2	20921	89515	4	10485	10436	2	89564	51
10	6 54 40	5 5 20	9.79095	3	10.20905	9.89541	4	10.10459	10.10446	2	9.89554	50
11	54 32	5 28	79111	3	20889	89567	5	10433	10456	2	89544	49
12	54 24	5 36	79128	3	20872	89593	5	10407	10466	2	89534	48
13	54 16	5 44	79144	3	20856	89619	6	10381	10476	2	89524	47
14	54 8	5 52	79160	4	20840	89645	6	10355	10486	2	89514	46
15	6 54 0	5 6 0	9.79176	4	10.20824	9.89671	6	10.10329	10.10496	3	9.89504	45
16	53 52	6 8	79192	4	20808	89697	7	10303	10505	3	89495	44
17	53 44	6 16	79208	5	20792	89723	7	10277	10515	3	89485	43
18	53 36	6 24	79224	5	20776	89749	8	10251	10525	3	89475	42
19	53 28	6 32	79240	5	20760	89775	8	10225	10535	3	89465	41
20	6 53 20	5 6 40	9.79256	5	10.20744	9.89801	9	10.10199	10.10545	3	9.89455	40
21	53 12	6 48	79272	6	20728	89827	9	10173	10555	4	89445	39
22	53 4	6 56	79288	6	20712	89853	10	10147	10565	4	89435	38
23	52 56	7 4	79304	6	20696	89879	10	10121	10575	4	89425	37
24	52 48	7 12	79319	6	20681	89905	10	10095	10585	4	89415	36
25	6 52 40	5 7 20	9.79335	7	10.20665	9.89931	11	10.10069	10.10595	4	9.89405	35
26	52 32	7 28	79351	7	20649	89957	11	10043	10605	4	89395	34
27	52 24	7 36	79367	7	20633	89983	12	10017	10615	5	89385	33
28	52 16	7 44	79383	7	20617	90009	12	09991	10625	5	89375	32
29	52 8	7 52	79399	8	20601	90035	13	09965	10636	5	89364	31
30	6 52 0	5 8 0	9.79415	8	10.20585	9.90061	13	10.09939	10.10646	5	9.89354	30
31	51 52	8 8	79431	8	20569	90086	13	09914	10656	5	89344	29
32	51 44	8 16	79447	8	20553	90112	14	09888	10666	5	89334	28
33	51 36	8 24	79463	9	20537	90138	14	09862	10676	6	89324	27
34	51 28	8 32	79478	9	20522	90164	15	09836	10686	6	89314	26
35	6 51 20	5 8 40	9.79494	9	10.20506	9.90190	15	10.09810	10.10696	6	9.89304	25
36	51 12	8 48	79510	10	20490	90216	16	09784	10706	6	89294	24
37	51 4	8 56	79526	10	20474	90242	16	09758	10716	6	89284	23
38	50 56	9 4	79542	10	20458	90268	16	09732	10726	6	89274	22
39	50 48	9 12	79558	10	20442	90294	17	09706	10736	7	89264	21
40	6 50 40	5 9 20	9.79573	11	10.20427	9.90320	17	10.09680	10.10746	7	9.89254	20
41	50 32	9 28	79589	11	20411	90346	18	09654	10756	7	89244	19
42	50 24	9 36	79605	11	20395	90371	18	09629	10767	7	89233	18
43	50 16	9 44	79621	11	20379	90397	19	09603	10777	7	89223	17
44	50 8	9 52	79636	12	20364	90423	19	09577	10787	7	89213	16
45	6 50 0	5 10 0	9.79652	12	10.20348	9.90449	19	10.09551	10.10797	8	9.89203	15
46	49 52	10 8	79668	12	20332	90475	20	09525	10807	8	89193	14
47	49 44	10 16	79684	12	20316	90501	20	09499	10817	8	89183	13
48	49 36	10 24	79699	13	20301	90527	21	09473	10827	8	89173	12
49	49 28	10 32	79715	13	20285	90553	21	09447	10838	8	89162	11
50	6 49 20	5 10 40	9.79731	13	10.20269	9.90578	22	10.09422	10.10848	8	9.89152	10
51	49 12	10 48	79746	14	20254	90604	22	09396	10858	9	89142	9
52	49 4	10 56	79762	14	20238	90630	22	09370	10868	9	89132	8
53	48 56	11 4	79778	14	20222	90656	23	09344	10878	9	89122	7
54	48 48	11 12	79793	14	20207	90682	23	09318	10888	9	89112	6
55	6 48 40	5 11 20	9.79809	15	10.20191	9.90708	24	10.09292	10.10899	9	9.89101	5
56	48 32	11 28	79825	15	20175	90734	24	09266	10909	9	89091	4
57	48 24	11 36	79840	15	20160	90759	25	09241	10919	10	89081	3
58	48 16	11 44	79856	15	20144	90785	25	09215	10929	10	89071	2
59	48 8	11 52	79872	16	20128	90811	26	09189	10940	10	89060	1
60	48 0	12 0	79887	16	20113	90837	26	09163	10950	10	89050	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
128°			A		A	B		B	C		C	51°

Seconds of time		1^s	2^s	3^s	4^s	5^s	6^s	7^s
Prop. parts of cols.	A	2	4	6	8	10	12	14
	B	3	6	10	13	16	19	23
	C	1	3	4	5	6	8	9

TABLE 44.

Log. Sines, Tangents, and Secants.

39°			A		A	B		B	C		C	140°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	6 48 0	5 12 0	9. 79887	0	10. 20113	9. 90837	0	10. 09163	10. 10950	0	9. 89050	60
1	47 52	12 8	79903	0	20097	90863	0	09137	10960	0	89040	59
2	47 44	12 16	79918	1	20082	90889	1	09111	10970	0	89030	58
3	47 36	12 24	79934	1	20066	90914	1	09086	10980	1	89020	57
4	47 28	12 32	79950	1	20050	90940	2	09060	10991	1	89009	56
5	6 47 20	5 12 40	9. 79965	1	10. 20035	9. 90966	2	10. 09034	10. 11001	1	9. 88999	55
6	47 12	12 48	79981	2	20019	90992	3	09008	11011	1	88989	54
7	47 4	12 56	79996	2	20004	91018	3	08982	11022	1	88978	53
8	46 56	13 4	80012	2	19988	91043	3	08957	11032	1	88968	52
9	46 48	13 12	80027	2	19973	91069	4	08931	11042	2	88958	51
10	6 46 40	5 13 20	9. 80043	3	10. 19957	9. 91095	4	10. 08905	10. 11052	2	9. 88948	50
11	46 32	13 28	80058	3	19942	91121	5	08879	11063	2	88937	49
12	46 24	13 36	80074	3	19926	91147	5	08853	11073	2	88927	48
13	46 16	13 44	80089	3	19911	91172	6	08828	11083	2	88917	47
14	46 8	13 52	80105	4	19895	91198	6	08802	11094	2	88906	46
15	6 46 0	5 14 0	9. 80120	4	10. 19880	9. 91224	6	10. 08776	10. 11104	3	9. 88896	45
16	45 52	14 8	80136	4	19864	91250	7	08750	11114	3	88886	44
17	45 44	14 16	80151	4	19849	91276	7	08724	11125	3	88875	43
18	45 36	14 24	80166	5	19834	91301	8	08699	11135	3	88865	42
19	45 28	14 32	80182	5	19818	91327	8	08673	11145	3	88855	41
20	6 45 20	5 14 40	9. 80197	5	10. 19803	9. 91353	9	10. 08647	10. 11156	3	9. 88844	40
21	45 12	14 48	80213	5	19787	91379	9	08621	11166	4	88834	39
22	45 4	14 56	80228	6	19772	91404	9	08596	11176	4	88824	38
23	44 56	15 4	80244	6	19756	91430	10	08570	11187	4	88813	37
24	44 48	15 12	80259	6	19741	91456	10	08544	11197	4	88803	36
25	6 44 40	5 15 20	9. 80274	6	10. 19726	9. 91482	11	10. 08518	10. 11207	4	9. 88793	35
26	44 32	15 28	80290	7	19710	91507	11	08493	11218	5	88782	34
27	44 24	15 36	80305	7	19695	91533	12	08467	11228	5	88772	33
28	44 16	15 44	80320	7	19680	91559	12	08441	11239	5	88761	32
29	44 8	15 52	80336	7	19664	91585	12	08415	11249	5	88751	31
30	6 44 0	5 16 0	9. 80351	8	10. 19649	9. 91610	13	10. 08390	10. 11259	5	9. 88741	30
31	43 52	16 8	80366	8	19634	91636	13	08364	11270	5	88730	29
32	43 44	16 16	80382	8	19618	91662	14	08338	11280	6	88720	28
33	43 36	16 24	80397	8	19603	91688	14	08312	11291	6	88709	27
34	43 28	16 32	80412	9	19588	91713	15	08287	11301	6	88699	26
35	6 43 20	5 16 40	9. 80428	9	10. 19572	9. 91739	15	10. 08261	10. 11312	6	9. 88688	25
36	43 12	16 48	80443	9	19557	91765	15	08235	11322	6	88678	24
37	43 4	16 56	80458	9	19542	91791	16	08209	11332	6	88668	23
38	42 56	17 4	80473	10	19527	91816	16	08184	11343	7	88657	22
39	42 48	17 12	80489	10	19511	91842	17	08158	11353	7	88647	21
40	6 42 40	5 17 20	9. 80504	10	10. 19496	9. 91868	17	10. 08132	10. 11364	7	9. 88636	20
41	42 32	17 28	80519	10	19481	91893	18	08107	11374	7	88626	19
42	42 24	17 36	80534	11	19466	91919	18	08081	11385	7	88615	18
43	42 16	17 44	80550	11	19450	91945	18	08055	11395	7	88605	17
44	42 8	17 52	80565	11	19435	91971	19	08029	11406	8	88594	16
45	6 42 0	5 18 0	9. 80580	12	10. 19420	9. 91996	19	10. 08004	10. 11416	8	9. 88584	15
46	41 52	18 8	80595	12	19405	92022	20	07978	11427	8	88573	14
47	41 44	18 16	80610	12	19390	92048	20	07952	11437	8	88563	13
48	41 36	18 24	80625	12	19375	92073	21	07927	11448	8	88552	12
49	41 28	18 32	80641	13	19359	92099	21	07901	11458	9	88542	11
50	6 41 20	5 18 40	9. 80656	13	10. 19344	9. 92125	21	10. 07875	10. 11469	9	9. 88531	10
51	41 12	18 48	80671	13	19329	92150	22	07850	11479	9	88521	9
52	41 4	18 56	80686	13	19314	92176	22	07824	11490	9	88510	8
53	40 56	19 4	80701	14	19299	92202	23	07798	11501	9	88499	7
54	40 48	19 12	80716	14	19284	92227	23	07773	11511	9	88489	6
55	6 40 40	5 19 20	9. 80731	14	10. 19269	9. 92253	24	10. 07747	10. 11522	10	9. 88478	5
56	40 32	19 28	80746	14	19254	92279	24	07721	11532	10	88468	4
57	40 24	19 36	80762	15	19238	92304	24	07696	11543	10	88457	3
58	40 16	19 44	80777	15	19223	92330	25	07670	11553	10	88447	2
59	40 8	19 52	80792	15	19208	92356	25	07644	11564	10	88436	1
60	40 0	20 0	80807	15	19193	92381	26	07619	11575	10	88425	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
129°			A		A	B		B	C		C	50°

Seconds of time.......		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	4	6	8	10	12	13
	B	3	6	10	13	16	19	23
	C	1	3	4	5	7	8	9

TABLE 44.

Log. Sines, Tangents, and Secants.

40°			A		A	B		B	C		C	139°
M.	Hour A.M.	Hour P.M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	6 40 0	5 20 0	9.80807	0	10.19193	9.92381	0	10.07619	10.11575	0	9.88425	60
1	39 52	20 8	80822	0	19178	92407	0	07593	11585	0	88415	59
2	39 44	20 16	80837	0	19163	92433	1	07567	11596	0	88404	58
3	39 36	20 24	80852	1	19148	92458	1	07542	11606	1	88394	57
4	39 28	20 32	80867	1	19133	92484	2	07516	11617	1	88383	56
5	6 39 20	5 20 40	9.80882	1	10.19118	9.92510	2	10.07490	10.11628	1	9.88372	55
6	39 12	20 48	80897	1	19103	92535	3	07465	11638	1	88362	54
7	39 4	20 56	80912	2	19088	92561	3	07439	11649	1	88351	53
8	38 56	21 4	80927	2	19073	92587	3	07413	11660	1	88340	52
9	38 48	21 12	80942	2	19058	92612	4	07388	11670	2	88330	51
10	6 38 40	5 21 20	9.80957	2	10.19043	9.92638	4	10.07362	10.11681	2	9.88319	50
11	38 32	21 28	80972	3	19028	92663	5	07337	11692	2	88308	49
12	38 24	21 36	80987	3	19013	92689	5	07311	11702	2	88298	48
13	38 16	21 44	81002	3	18998	92715	6	07285	11713	2	88287	47
14	38 8	21 52	81017	3	18983	92740	6	07260	11724	3	88276	46
15	6 38 0	5 22 0	9.81032	4	10.18968	9.92766	6	10.07234	10.11734	3	9.88266	45
16	37 52	22 8	81047	4	18953	92792	7	07208	11745	3	88255	44
17	37 44	22 16	81061	4	18939	92817	7	07183	11756	3	88244	43
18	37 36	22 24	81076	4	18924	92843	8	07157	11766	3	88234	42
19	37 28	22 32	81091	5	18909	92868	8	07132	11777	3	88223	41
20	6 37 20	5 22 40	9.81106	5	10.18894	9.92894	9	10.07106	10.11788	4	9.88212	40
21	37 12	22 48	81121	5	18879	92920	9	07080	11799	4	88201	39
22	37 4	22 56	81136	5	18864	92945	9	07055	11809	4	88191	38
23	36 56	23 4	81151	6	18849	92971	10	07029	11820	4	88180	37
24	36 48	23 12	81166	6	18834	92996	10	07004	11831	4	88169	36
25	6 36 40	5 23 20	9.81180	6	10.18820	9.93022	11	10.06978	10.11842	4	9.88158	35
26	36 32	23 28	81195	6	18805	93048	11	06952	11852	5	88148	34
27	36 24	23 36	81210	7	18790	93073	12	06927	11863	5	88137	33
28	36 16	23 44	81225	7	18775	93099	12	06901	11874	5	88126	32
29	36 8	23 52	81240	7	18760	93124	12	06876	11885	5	88115	31
30	6 36 0	5 24 0	9.81254	7	10.18746	9.93150	13	10.06850	10.11895	5	9.88105	30
31	35 52	24 8	81269	8	18731	93175	13	06825	11906	6	88094	29
32	35 44	24 16	81284	8	18716	93201	14	06799	11917	6	88083	28
33	35 36	24 24	81299	8	18701	93227	14	06773	11928	6	88072	27
34	35 28	24 32	81314	8	18686	93252	14	06748	11939	6	88061	26
35	6 35 20	5 24 40	9.81328	9	10.18672	9.93278	15	10.06722	10.11949	6	9.88051	25
36	35 12	24 48	81343	9	18657	93303	15	06697	11960	6	88040	24
37	35 4	24 56	81358	9	18642	93329	16	06671	11971	7	88029	23
38	34 56	25 4	81372	9	18628	93354	16	06646	11982	7	88018	22
39	34 48	25 12	81387	10	18613	93380	17	06620	11993	7	88007	21
40	6 34 40	5 25 20	9.81402	10	10.18598	9.93406	17	10.06594	10.12004	7	9.87996	20
41	34 32	25 28	81417	10	18583	93431	17	06569	12015	7	87985	19
42	34 24	25 36	81431	10	18569	93457	18	06543	12025	8	87975	18
43	34 16	25 44	81446	11	18554	93482	18	06518	12036	8	87964	17
44	34 8	25 52	81461	11	18539	93508	19	06492	12047	8	87953	16
45	6 34 0	5 26 0	9.81475	11	10.18525	9.93533	19	10.06467	10.12058	8	9.87942	15
46	33 52	26 8	81490	11	18510	93559	20	06441	12069	8	87931	14
47	33 44	26 16	81505	12	18495	93584	20	06416	12080	8	87920	13
48	33 36	26 24	81519	12	18481	93610	20	06390	12091	9	87909	12
49	33 28	26 32	81534	12	18466	93636	21	06364	12102	9	87898	11
50	6 33 20	5 26 40	9.81549	12	10.18451	9.93661	21	10.06339	10.12113	9	9.87887	10
51	33 12	26 48	81563	13	18437	93687	22	06313	12123	9	87877	9
52	33 4	26 56	81578	13	18422	93712	22	06288	12134	9	87866	8
53	32 56	27 4	81592	13	18408	93738	23	06262	12145	10	87855	7
54	32 48	27 12	81607	13	18393	93763	23	06237	12156	10	87844	6
55	6 32 40	5 27 20	9.81622	14	10.18378	9.93789	23	10.06211	10.12167	10	9.87833	5
56	32 32	27 28	81636	14	18364	93814	24	06186	12178	10	87822	4
57	32 24	27 36	81651	14	18349	93840	24	06160	12189	10	87811	3
58	32 16	27 44	81665	14	18335	93865	25	06135	12200	10	87800	2
59	32 8	27 52	81680	15	18320	93891	25	06109	12211	11	87789	1
60	32 0	28 0	81694	15	18306	93916	26	06084	12222	11	87778	0
M.	Hour P.M.	Hour A.M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
130°			A		A	B		B	C		C	49°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	4	6	7	9	11	13
	B	3	6	10	13	16	19	22
	C	1	3	4	5	7	8	9

TABLE 44.

Log. Sines, Tangents, and Secants.

41°			A		A	B		B	C		C	138°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	6 32 0	5 28 0	9.81694	0	10.18306	9.93916	0	10.06084	10.12222	0	9.87778	60
1	31 52	28 8	81709	0	18291	93942	0	06058	12233	0	87767	59
2	31 44	28 16	81723	0	18277	93967	1	06033	12244	0	87756	58
3	31 36	28 24	81738	1	18262	93993	1	06007	12255	1	87745	57
4	31 28	28 32	81752	1	18248	94018	2	05982	12266	1	87734	56
5	6 31 20	5 28 40	9.81767	1	10.18233	9.94044	2	10.05956	10.12277	1	9.87723	55
6	31 12	28 48	81781	1	18219	94069	3	05931	12288	1	87712	54
7	31 4	28 56	81796	2	18204	94095	3	05905	12299	1	87701	53
8	30 56	29 4	81810	2	18190	94120	3	05880	12310	1	87690	52
9	30 48	29 12	81825	2	18175	94146	4	05854	12321	2	87679	51
10	6 30 40	5 29 20	9.81839	2	10.18161	9.94171	4	10.05829	10.12332	2	9.87668	50
11	30 32	29 28	81854	3	18146	94197	5	05803	12343	2	87657	49
12	30 24	29 36	81868	3	18132	94222	5	05778	12354	2	87646	48
13	30 16	29 44	81882	3	18118	94248	6	05752	12365	2	87635	47
14	30 8	29 52	81897	3	18103	94273	6	05727	12376	3	87624	46
15	6 30 0	5 30 0	9.81911	4	10.18089	9.94299	6	10.05701	10.12387	3	9.87613	45
16	29 52	30 8	81926	4	18074	94324	7	05676	12399	3	87601	44
17	29 44	30 16	81940	4	18060	94350	7	05650	12410	3	87590	43
18	29 36	30 24	81955	4	18045	94375	8	05625	12421	3	87579	42
19	29 28	30 32	81969	5	18031	94401	8	05599	12432	4	87568	41
20	6 29 20	5 30 40	9.81983	5	10.18017	9.94426	8	10.05574	10.12443	4	9.87557	40
21	29 12	30 48	81998	5	18002	94452	9	05548	12454	4	87546	39
22	29 4	30 56	82012	5	17988	94477	9	05523	12465	4	87535	38
23	28 56	31 4	82026	5	17974	94503	10	05497	12476	4	87524	37
24	28 48	31 12	82041	6	17959	94528	10	05472	12487	4	87513	36
25	6 28 40	5 31 20	9.82055	6	10.17945	9.94554	11	10.05446	10.12499	5	9.87501	35
26	28 32	31 28	82069	6	17931	94579	11	05421	12510	5	87490	34
27	28 24	31 36	82084	6	17916	94604	11	05396	12521	5	87479	33
28	28 16	31 44	82098	7	17902	94630	12	05370	12532	5	87468	32
29	28 8	31 52	82112	7	17888	94655	12	05345	12543	5	87457	31
30	6 28 0	5 32 0	9.82126	7	10.17874	9.94681	13	10.05319	10.12554	6	9.87446	30
31	27 52	32 8	82141	7	17859	94706	13	05294	12566	6	87434	29
32	27 44	32 16	82155	8	17845	94732	14	05268	12577	6	87423	28
33	27 36	32 24	82169	8	17831	94757	14	05243	12588	6	87412	27
34	27 28	32 32	82184	8	17816	94783	14	05217	12599	6	87401	26
35	6 27 20	5 32 40	9.82198	8	10.17802	9.94808	15	10.05192	10.12610	7	9.87390	25
36	27 12	32 48	82212	9	17788	94834	15	05166	12622	7	87378	24
37	27 4	32 56	82226	9	17774	94859	16	05141	12633	7	87367	23
38	26 56	33 4	82240	9	17760	94884	16	05116	12644	7	87356	22
39	26 48	33 12	82255	9	17745	94910	17	05090	12655	7	87345	21
40	6 26 40	5 33 20	9.82269	10	10.17731	9.94935	17	10.05065	10.12666	7	9.87334	20
41	26 32	33 28	82283	10	17717	94961	17	05039	12678	8	87322	19
42	26 24	33 36	82297	10	17703	94986	18	05014	12689	8	87311	18
43	26 16	33 44	82311	10	17689	95012	18	04988	12700	8	87300	17
44	26 8	33 52	82326	10	17674	95037	19	04963	12712	8	87288	16
45	6 26 0	5 34 0	9.82340	11	10.17660	9.95062	19	10.04938	10.12723	8	9.87277	15
46	25 52	34 8	82354	11	17646	95088	20	04912	12734	9	87266	14
47	25 44	34 16	82368	11	17632	95113	20	04887	12745	9	87255	13
48	25 36	34 24	82382	11	17618	95139	20	04861	12757	9	87243	12
49	25 28	34 32	82396	12	17604	95164	21	04836	12768	9	87232	11
50	6 25 20	5 34 40	9.82410	12	10.17590	9.95190	21	10.04810	10.12779	9	9.87221	10
51	25 12	34 48	82424	12	17576	95215	22	04785	12791	10	87209	9
52	25 4	34 56	82439	12	17561	95240	22	04760	12802	10	87198	8
53	24 56	35 4	82453	13	17547	95266	22	04734	12813	10	87187	7
54	24 48	35 12	82467	13	17533	95291	23	04709	12825	10	87175	6
55	6 24 40	5 35 20	9.82481	13	10.17519	9.95317	23	10.04683	10.12836	10	9.87164	5
56	24 32	35 28	82495	13	17505	95342	24	04658	12847	10	87153	4
57	24 24	35 36	82509	14	17491	95368	24	04632	12859	11	87141	3
58	24 16	35 44	82523	14	17477	95393	25	04607	12870	11	87130	2
59	24 8	35 52	82537	14	17463	95418	25	04582	12881	11	87119	1
60	24 0	36 0	82551	14	17449	95444	25	04556	12893	11	87107	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
131°			A		A	B		B	C		C	48°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	4	5	7	9	11	12
	B	3	6	10	13	16	19	22
	C	2	3	4	6	7	8	10

TABLE 44.

Log. Sines, Tangents, and Secants.

42°			A		A	B		B	C		C	137°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	6 24 0	5 36 0	9. 82551	0	10. 17449	9. 95444	0	10. 04556	10. 12893	0	9. 87107	60
1	23 52	36 8	82565	0	17435	95469	0	04531	12904	0	87096	59
2	23 44	36 16	82579	0	17421	95495	1	04505	12915	0	87085	58
3	23 36	36 24	82593	1	17407	95520	1	04480	12927	1	87073	57
4	23 28	36 32	82607	1	17393	95545	2	04455	12938	1	87062	56
5	6 23 20	5 36 40	9. 82621	1	10. 17379	9. 95571	2	10. 04429	10. 12950	1	9. 87050	55
6	23 12	36 48	82635	1	17365	95596	3	04404	12961	1	87039	54
7	23 4	36 56	82649	2	17351	95622	3	04378	12972	1	87028	53
8	22 56	37 4	82663	2	17337	95647	3	04353	12984	2	87016	52
9	22 48	37 12	82677	2	17323	95672	4	04328	12995	2	87005	51
10	6 22 40	5 37 20	9. 82691	2	10. 17309	9. 95698	4	10. 04302	10. 13007	2	9. 86993	50
11	22 32	37 28	82705	3	17295	95723	5	04277	13018	2	86982	49
12	22 24	37 36	82719	3	17281	95748	5	04252	13030	2	86970	48
13	22 16	37 44	82733	3	17267	95774	5	04226	13041	3	86959	47
14	22 8	37 52	82747	3	17253	95799	6	04201	13053	3	86947	46
15	6 22 0	5 38 0	9. 82761	3	10. 17239	9. 95825	6	10. 04175	10. 13064	3	9. 86936	45
16	21 52	38 8	82775	4	17225	95850	7	04150	13076	3	86924	44
17	21 44	38 16	82788	4	17212	95875	7	04125	13087	3	86913	43
18	21 36	38 24	82802	4	17198	95901	8	04099	13098	3	86902	42
19	21 28	38 32	82816	4	17184	95926	8	04074	13110	4	86890	41
20	6 21 20	5 38 40	9. 82830	5	10. 17170	9. 95952	8	10. 04048	10. 13121	4	9. 86879	40
21	21 12	38 48	82844	5	17156	95977	9	04023	13133	4	86867	39
22	21 4	38 56	82858	5	17142	96002	9	03998	13145	4	86855	38
23	20 56	39 4	82872	5	17128	96028	10	03972	13156	4	86844	37
24	20 48	39 12	82885	6	17115	96053	10	03947	13168	5	86832	36
25	6 20 40	5 39 20	9. 82899	6	10. 17101	9. 96078	11	10. 03922	10. 13179	5	9. 86821	35
26	20 32	39 28	82913	6	17087	96104	11	03896	13191	5	86809	34
27	20 24	39 36	82927	6	17073	96129	11	03871	13202	5	86798	33
28	20 16	39 44	82941	6	17059	96155	12	03845	13214	5	86786	32
29	20 8	39 52	82955	7	17045	96180	12	03820	13225	6	86775	31
30	6 20 0	5 40 0	9. 82968	7	10. 17032	9. 96205	13	10. 03795	10. 13237	6	9. 86763	30
31	19 52	40 8	82982	7	17018	96231	13	03769	13248	6	86752	29
32	19 44	40 16	82996	7	17004	96256	14	03744	13260	6	86740	28
33	19 36	40 24	83010	8	16990	96281	14	03719	13272	6	86728	27
34	19 28	40 32	83023	8	16977	96307	14	03693	13283	7	86717	26
35	6 19 20	5 40 40	9. 83037	8	10. 16963	9. 96332	15	10. 03668	10. 13295	7	9. 86705	25
36	19 12	40 48	83051	8	16949	96357	15	03643	13306	7	86694	24
37	19 4	40 56	83065	8	16935	96383	16	03617	13318	7	86682	23
38	18 56	41 4	83078	9	16922	96408	16	03592	13330	7	86670	22
39	18 48	41 12	83092	9	16908	96433	16	03567	13341	8	86659	21
40	6 18 40	5 41 20	9. 83106	9	10. 16894	9. 96459	17	10. 03541	10. 13353	8	9. 86647	20
41	18 32	41 28	83120	9	16880	96484	17	03516	13365	8	86635	19
42	18 24	41 36	83133	10	16867	96510	18	03490	13376	8	86624	18
43	18 16	41 44	83147	10	16853	96535	18	03465	13388	8	86612	17
44	18 8	41 52	83161	10	16839	96560	19	03440	13400	8	86600	16
45	6 18 0	5 42 0	9. 83174	10	10. 16826	9. 96586	19	10. 03414	10. 13411	9	9. 86589	15
46	17 52	42 8	83188	11	16812	96611	19	03389	13423	9	86577	14
47	17 44	42 16	83202	11	16798	96636	20	03364	13435	9	86565	13
48	17 36	42 24	83215	11	16785	96662	20	03338	13446	9	86554	12
49	17 28	42 32	83229	11	16771	96687	21	03313	13458	9	86542	11
50	6 17 20	5 42 40	9. 83242	11	10. 16758	9. 96712	21	10. 03288	10. 13470	10	9. 86530	10
51	17 12	42 48	83256	12	16744	96738	22	03262	13482	10	86518	9
52	17 4	42 56	83270	12	16730	96763	22	03237	13493	10	86507	8
53	16 56	43 4	83283	12	16717	96788	22	03212	13505	10	86495	7
54	16 48	43 12	83297	12	16703	96814	23	03186	13517	10	86483	6
55	6 16 40	5 43 20	9. 83310	13	10. 16690	9. 96839	23	10. 03161	10. 13528	11	9. 86472	5
56	16 32	43 28	83324	13	16676	96864	24	03136	13540	11	86460	4
57	16 24	43 36	83338	13	16662	96890	24	03110	13552	11	86448	3
58	16 16	43 44	83351	13	16649	96915	25	03085	13564	11	86436	2
59	16 8	43 52	83365	14	16635	96940	25	03060	13575	11	86425	1
60	16 0	44 0	83378	14	16622	96966	25	03034	13587	12	86413	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
132°			A		A	B		B	C		C	47°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	3	5	7	9	10	12
	B	3	6	10	13	16	19	22
	C	1	3	4	6	7	9	10

TABLE 44.

Log. Sines, Tangents, and Secants.

43°			A		A	B		B	C		C	136°
M.	Hour A.M.	Hour P.M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	6 16 0	5 44 0	9.83378	0	10.16622	9.96966	0	10.03034	10.13587	0	9.86413	60
1	15 52	44 8	83392	0	16608	96991	0	03009	13599	0	86401	59
2	15 44	44 16	83405	0	16595	97016	1	02984	13611	0	86389	58
3	15 36	44 24	83419	1	16581	97042	1	02958	13623	1	86377	57
4	15 28	44 32	83432	1	16568	97067	2	02933	13634	1	86366	56
5	6 15 20	5 44 40	9.83446	1	10.16554	9.97092	2	10.02908	10.13646	1	9.86354	55
6	15 12	44 48	83459	1	16541	97118	3	02882	13658	1	86342	54
7	15 4	44 56	83473	2	16527	97143	3	02857	13670	1	86330	53
8	14 56	45 4	83486	2	16514	97168	3	02832	13682	2	86318	52
9	14 48	45 12	83500	2	16500	97193	4	02807	13694	2	86306	51
10	6 14 40	5 45 20	9.83513	2	10.16487	9.97219	4	10.02781	10.13705	2	9.86295	50
11	14 32	45 28	83527	2	16473	97244	5	02756	13717	2	86283	49
12	14 24	45 36	83540	3	16460	97269	5	02731	13729	2	86271	48
13	14 16	45 44	83554	3	16446	97295	5	02705	13741	3	86259	47
14	14 8	45 52	83567	3	16433	97320	6	02680	13753	3	86247	46
15	6 14 0	5 46 0	9.83581	3	10.16419	9.97345	6	10.02655	10.13765	3	9.86235	45
16	13 52	46 8	83594	4	16406	97371	7	02629	13777	3	86223	44
17	13 44	46 16	83608	4	16392	97396	7	02604	13789	3	86211	43
18	13 36	46 24	83621	4	16379	97421	8	02579	13800	4	86200	42
19	13 28	46 32	83634	4	16366	97447	8	02553	13812	4	86188	41
20	6 13 20	5 46 40	9.83648	4	10.16352	9.97472	8	10.02528	10.13824	4	9.86176	40
21	13 12	46 48	83661	5	16339	97497	9	02503	13836	4	86164	39
22	13 4	46 56	83674	5	16326	97523	9	02477	13848	4	86152	38
23	12 56	47 4	83688	5	16312	97548	10	02452	13860	5	86140	37
24	12 48	47 12	83701	5	16299	97573	10	02427	13872	5	86128	36
25	6 12 40	5 47 20	9.83715	6	10.16285	9.97598	11	10.02402	10.13884	5	9.86116	35
26	12 32	47 28	83728	6	16272	97624	11	02376	13896	5	86104	34
27	12 24	47 36	83741	6	16259	97649	11	02351	13908	5	86092	33
28	12 16	47 44	83755	6	16245	97674	12	02326	13920	6	86080	32
29	12 8	47 52	83768	6	16232	97700	12	02300	13932	6	86068	31
30	6 12 0	5 48 0	9.83781	7	10.16219	9.97725	13	10.02275	10.13944	6	9.86056	30
31	11 52	48 8	83795	7	16205	97750	13	02250	13956	6	86044	29
32	11 44	48 16	83808	7	16192	97776	13	02224	13968	6	86032	28
33	11 36	48 24	83821	7	16179	97801	14	02199	13980	7	86020	27
34	11 28	48 32	83834	8	16166	97826	14	02174	13992	7	86008	26
35	6 11 20	5 48 40	9.83848	8	10.16152	9.97851	15	10.02149	10.14004	7	9.85996	25
36	11 12	48 48	83861	8	16139	97877	15	02123	14016	7	85984	24
37	11 4	48 56	83874	8	16126	97902	16	02098	14028	7	85972	23
38	10 56	49 4	83887	8	16113	97927	16	02073	14040	8	85960	22
39	10 48	49 12	83901	9	16099	97953	16	02047	14052	8	85948	21
40	6 10 40	5 49 20	9.83914	9	10.16086	9.97978	17	10.02022	10.14064	8	9.85936	20
41	10 32	49 28	83927	9	16073	98003	17	01997	14076	8	85924	19
42	10 24	49 36	83940	9	16060	98029	18	01971	14088	8	85912	18
43	10 16	49 44	83954	10	16046	98054	18	01946	14100	9	85900	17
44	10 8	49 52	83967	10	16033	98079	19	01921	14112	9	85888	16
45	6 10 0	5 50 0	9.83980	10	10.16020	9.98104	19	10.01896	10.14124	9	9.85876	15
46	9 52	50 8	83993	10	16007	98130	19	01870	14136	9	85864	14
47	9 44	50 16	84006	10	15994	98155	20	01845	14149	9	85851	13
48	9 36	50 24	84020	11	15980	98180	20	01820	14161	10	85839	12
49	9 28	50 32	84033	11	15967	98206	21	01794	14173	10	85827	11
50	6 9 20	5 50 40	9.84046	11	10.15954	9.98231	21	10.01769	10.14185	10	9.85815	10
51	9 12	50 48	84059	11	15941	98256	22	01744	14197	10	85803	9
52	9 4	50 56	84072	12	15928	98281	22	01719	14209	10	85791	8
53	8 56	51 4	84085	12	15915	98307	22	01693	14221	11	85779	7
54	8 48	51 12	84098	12	15902	98332	23	01668	14234	11	85766	6
55	6 8 40	5 51 20	9.84112	12	10.15888	9.98357	23	10.01643	10.14246	11	9.85754	5
56	8 32	51 28	84125	12	15875	98383	24	01617	14258	11	85742	4
57	8 24	51 36	84138	13	15862	98408	24	01592	14270	11	85730	3
58	8 16	51 44	84151	13	15849	98433	24	01567	14282	12	85718	2
59	8 8	51 52	84164	13	15836	98458	25	01542	14294	12	85706	1
60	8 0	52 0	84177	13	15823	98484	25	01516	14307	12	85693	0
M.	Hour P.M.	Hour A.M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
133°			A		A	B		B	C		C	46°

Seconds of time........		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	3	5	7	8	10	12
	B	3	6	9	13	16	19	22
	C	2	3	5	6	8	9	11

TABLE 44.

Log. Sines, Tangents, and Secants.

44°			A		A	B		B	C		C	135°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	6 8 0	5 52 0	9. 84177	0	10. 15823	9. 98484	0	10. 01516	10. 14307	0	9. 85693	60
1	7 52	52 8	84190	0	15810	98509	0	01491	14319	0	85681	59
2	7 44	52 16	84203	0	15797	98534	1	01466	14331	0	85669	58
3	7 36	52 24	84216	1	15784	98560	1	01440	14343	1	85657	57
4	7 28	52 32	84229	1	15771	98585	2	01415	14355	1	85645	56
5	6 7 20	5 52 40	9. 84242	1	10. 15758	9. 98610	2	10. 01390	10. 14368	1	9. 85632	55
6	7 12	52 48	84255	1	15745	98635	3	01365	14380	1	85620	54
7	7 4	52 56	84269	2	15731	98661	3	01339	14392	1	85608	53
8	6 56	53 4	84282	2	15718	98686	3	01314	14404	2	85596	52
9	6 48	53 12	84295	2	15705	98711	4	01289	14417	2	85583	51
10	6 6 40	5 53 20	9. 84308	2	10. 15692	9. 98737	4	10. 01263	10. 14429	2	9. 85571	50
11	6 32	53 28	84321	2	15679	98762	5	01238	14441	2	85559	49
12	6 24	53 36	84334	3	15666	98787	5	01213	14453	2	85547	48
13	6 16	53 44	84347	3	15653	98812	5	01188	14466	3	85534	47
14	6 8	53 52	84360	3	15640	98838	6	01162	14478	3	85522	46
15	6 6 0	5 54 0	9. 84373	3	10. 15627	9. 98863	6	10. 01137	10. 14490	3	9. 85510	45
16	5 52	54 8	84385	3	15615	98888	7	01112	14503	3	85497	44
17	5 44	54 16	84398	4	15602	98913	7	01087	14515	4	85485	43
18	5 36	54 24	84411	4	15589	98939	8	01061	14527	4	85473	42
19	5 28	54 32	84424	4	15576	98964	8	01036	14540	4	85460	41
20	6 5 20	5 54 40	9. 84437	4	10. 15563	9. 98989	8	10. 01011	10. 14552	4	9. 85448	40
21	5 12	54 48	84450	5	15550	99015	9	00985	14564	4	85436	39
22	5 4	54 56	84463	5	15537	99040	9	00960	14577	5	85423	38
23	4 56	55 4	84476	5	15524	99065	10	00935	14589	5	85411	37
24	4 48	55 12	84489	5	15511	99090	10	00910	14601	5	85399	36
25	6 4 40	5 55 20	9. 84502	5	10. 15498	9. 99116	11	10. 00884	10. 14614	5	9. 85386	35
26	4 32	55 28	84515	6	15485	99141	11	00859	14626	5	85374	34
27	4 24	55 36	84528	6	15472	99166	11	00834	14639	6	85361	33
28	4 16	55 44	84540	6	15460	99191	12	00809	14651	6	85349	32
29	4 8	55 52	84553	6	15447	99217	12	00783	14663	6	85337	31
30	6 4 0	5 56 0	9. 84566	6	10. 15434	9. 99242	13	10. 00758	10. 14676	6	9. 85324	30
31	3 52	56 8	84579	7	15421	99267	13	00733	14688	6	85312	29
32	3 44	56 16	84592	7	15408	99293	13	00707	14701	7	85299	28
33	3 36	56 24	84605	7	15395	99318	14	00682	14713	7	85287	27
34	3 28	56 32	84618	7	15382	99343	14	00657	14726	7	85274	26
35	6 3 20	5 56 40	9. 84630	8	10. 15370	9. 99368	15	10. 00632	10. 14738	7	9. 85262	25
36	3 12	56 48	84643	8	15357	99394	15	00606	14750	7	85250	24
37	3 4	56 56	84656	8	15344	99419	16	00581	14763	8	85237	23
38	2 56	57 4	84669	8	15331	99444	16	00556	14775	8	85225	22
39	2 48	57 12	84682	8	15318	99469	16	00531	14788	8	85212	21
40	6 2 40	5 57 20	9. 84694	9	10. 15306	9. 99495	17	10. 00505	10. 14800	8	9. 85200	20
41	2 32	57 28	84707	9	15293	99520	17	00480	14813	8	85187	19
42	2 24	57 36	84720	9	15280	99545	18	00455	14825	9	85175	18
43	2 16	57 44	84733	9	15267	99570	18	00430	14838	9	85162	17
44	2 8	57 52	84745	9	15255	99596	19	00404	14850	9	85150	16
45	6 2 0	5 58 0	9. 84758	10	10. 15242	9. 99621	19	10. 00379	10. 14863	9	9. 85137	15
46	1 52	58 8	84771	10	15229	99646	19	00354	14875	10	85125	14
47	1 44	58 16	84784	10	15216	99672	20	00328	14888	10	85112	13
48	1 36	58 24	84796	10	15204	99697	20	00303	14900	10	85100	12
49	1 28	58 32	84809	11	15191	99722	21	00278	14913	10	85087	11
50	6 1 20	5 58 40	9. 84822	11	10. 15178	9. 99747	21	10. 00253	10. 14926	10	9. 85074	10
51	1 12	58 48	84835	11	15165	99773	21	00227	14938	11	85062	9
52	1 4	58 56	84847	11	15153	99798	22	00202	14951	11	85049	8
53	0 56	59 4	84860	11	15140	99823	22	00177	14963	11	85037	7
54	0 48	59 12	84873	12	15127	99848	23	00152	14976	11	85024	6
55	6 0 40	5 59 20	9. 84885	12	10. 15115	9. 99874	23	10. 00126	10. 14988	11	9. 85012	5
56	0 32	59 28	84898	12	15102	99899	24	00101	15001	12	84999	4
57	0 24	59 36	84911	12	15089	99924	24	00076	15014	12	84986	3
58	0 16	59 44	84923	12	15077	99949	24	00051	15026	12	84974	2
59	0 8	59 52	84936	13	15064	99975	25	00025	15039	12	84961	1
60	0 0	6 0 0	84949	13	15051	10. 00000	25	00000	15051	12	84949	0
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
134°			A		A	B		B	C		C	45°

Seconds of time		1s	2s	3s	4s	5s	6s	7s
Prop. parts of cols.	A	2	3	5	6	8	10	11
	B	3	6	9	13	16	19	22
	C	2	3	5	6	8	9	11

Index to Part I - see p 333/9
Contents Part II p 343

Index to app. IV Tides p 266-2